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ROCZNIK METEOROLOGICZNY

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ANNUAIRE MÉTÉOROLOGIQUE

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WARSZAWA 1966
WYDAWNICTWA KOMUNIKACJI i ŁĄCZNOŚCI

AMERICAN GEOPHYSICAL UNION
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WYDAWNICTWA KOMUNIKACJI i ŁĄCZNOŚCI – WARSZAWA 1966

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PRZEDMOWA

Układ *Rocznika meteorologicznego 1962* jest taki sam jak rocznika 1961. Materiał obserwacyjny zestawiono w czterech tablicach.

Tablica pierwsza zawiera codzienne spostrzeżenia meteorologiczne, w tablicy drugiej podano wyniki miesięczne i roczne spostrzeżeń meteorologicznych, w tablicy trzeciej zestawiono daty ostatnich przymrozków wiosennych i pierwszych przymrozków jesiennych (według spostrzeżeń dokonywanych w klatce meteorologicznej — 2 m nad powierzchnią gruntu), zaś w tablicy czwartej — dzienne i miesięczne sumy godzin usłonecznienia.

Uzupełnienie stanowią objaśnienia, wykaz symboli meteorologicznych, skorowidz i mapa rozmieszczenia stacji.

Rocznik został opracowany w Ośrodku Gromadzenia i Rozpowszechniania Danych Państwowego Instytutu Hydrologiczno-Meteorologicznego pod kierownictwem i redakcją mgr Feliksa Janiszewskiego.

Doc. dr ZDZISŁAW KACZMAREK

Dyrektor
Państwowego Instytutu
Hydrologiczno-Meteorologicznego

PRÉFACE

La composition de l'*Annuaire Météorologipue 1962* est analogue à celle de l'annuaire pour 1961. Le matériel d'observations y est recueilli sous forme de quatre tableaux.

La première table englobe des observations journalières des stations météorologiques, la seconde cite des résultats mensuels et annuels des observations météorologiques, la troisième table présente les dates des dernières gelées printanières ainsi que les premières gelées d'automne d'après les observations executées dans l'abri météorologique (2 mètres au dessus de la surface du sol), la quatrième table — valeurs diurnes et mensuels d'insolation en heures.

Les explications, le relevé des symboles météorologiques, répertoire et la carte de la dislocation des stations constituent le complément à ces tables.

L'Annuaire a été élaboré dans le Centre de Rassemblement et de Distribution des Données de l'Institut Hydrologique et Météorologique d'État sous la direction et redaction de M. Feliks Janiszewski.

Doc. dr ZDZISŁAW KACZMAREK

Directeur
de l'Institut Hydrologique
et Météorologique d'État

OBJAŚNIENIA

Użyte w niniejszym roczniku symbole mają następujące znaczenie:

φ — szerokość geograficzna.

λ — długość geograficzna.

H_s — wysokość terenu ogródka meteorologicznego nad średnim poziomem morza.

H_b — wysokość barometru nad średnim poziomem morza.

Dla stacji posiadających barometry H_s i H_b zostały wyznaczne za pomocą niwelacji, dla pozostałych stacji H_s wyznaczono z mapy topograficznej.

h_w — wysokość wiatromierza nad powierzchnią gruntu.

m — w połączeniu z literowym symbolem elementu oznacza wartość średnią miesięczną (np. U_m oznacza średnią miesięczną wilgotność względną).

P — ciśnienie atmosferyczne w milibarach, zredukowane do 0° i do ciężkości normalnej.

$P_{o,m}$ — wartość średnia miesięczna ciśnienia atmosferycznego, sprowadzona do średniego poziomu morza.

T — temperatura w °C.

Temperaturę wyznaczano za pomocą termometrów umieszczonych w klatce meteorologicznej typu angielskiego na wysokości 2 m nad powierzchnią gruntu. Skrajne dobowe wartości temperatur odnoszą się do okresu od III obserwacji dnia poprzedniego do III obserwacji danego dnia.

$\overline{Max}$ — średnia miesięczna z wartości temperatur maksymalnych dobowych.

$\overline{Min}$ — średnia miesięczna z wartości temperatur minimalnych dobowych.

e — prężność pary wodnej w milibarach

U — wilgotność względna w procentach.

Δ — niedosyt wilgotności w milibarach.

N — zachmurzenie w skali 11-stopniowej (przy tym 0 oznacza niebo bezchmurne, zaś 10 — niebo całkowicie pokryte chmurami).

W tablicy I rocznika obok wartości zachmurzenia podane są za pomocą symboli również dane o zjawiskach zaobserwowanych podczas obserwacji terminowych.

D — kierunek wiatru.

v — prędkość wiatru w m/sek.

n_D — częstotliwość występowania poszczególnych kierunków wiatru.

v_{mD} — średnia prędkość wiatru wg kierunków.

Obserwacje nad wiatrem były dokonywane (z nielicznymi wyjątkami) przy użyciu wiatromierzy Wilda.

R — wysokość opadu w milimetrach.

Wysokość opadu odnosi się do okresu od I (porannej) obserwacji jednego dnia do I obserwacji dnia następnego i jest podawana pod datą dnia poprzedniego. Obserwacje te były dokonywane za pomocą deszczomierzy Hellmanna o powierzchni otworu 200 cm², umieszczonych na wysokości 1 m nad powierzchnią gruntu, z wyjątkiem części stacji górskich, położonych powyżej 500 m nad poziomem morza, gdzie używa się deszczomierzy typu górskiego, mających powierzchnię otworu 500 cm² i umieszczonych na wysokości 1,5 m nad powierzchnią gruntu.

V — widzialność z II terminu obserwacji, wyrażona w następującej skali międzynarodowej:

0 — przedmioty są niewidoczne już z odległości mniejszej od 50 m;

1 — przedmioty są widoczne z odległości 50 m, lecz niewidoczne z odległości 200 m;

2 — przedmioty są widoczne z odległości 200 m, lecz niewidoczne z odległości 500 m;

3 — przedmioty są widoczne z odległości 500 m, lecz niewidoczne z odległości 1 km;

4 — przedmioty są widoczne z odległości 1 km, lecz niewidoczne z odległości 2 km;

5 — przedmioty są widoczne z odległości 2 km, lecz niewidoczne z odległości 4 km;

6 — przedmioty są widoczne z odległości 4 km, lecz niewidoczne z odległości 10 km;

7 — przedmioty są widoczne z odległości 10 km, lecz niewidoczne z odległości 20 km;

8 — przedmioty są widoczne z odległości 20 km, lecz niewidoczne z odległości 50 km;

9 — przedmioty są widoczne z odległości 50 km i więcej.

h — grubość pokrywy śnieżnej w centymetrach wg obserwacji dokonywanych w I terminie.

pł. — śnieg w płatach.

Usłonecznienie — w godzinach. Obserwacji dokonywano za pomocą heliografów Campbell—Stokes'a.

n — liczba dni z poszczególnymi zjawiskami.

Za dzień z mgłą przyjęto w niniejszym roczniku dzień, w którym to zjawisko powodowało zmniejszenie się widzialności poniżej 1 km.

Za dni pogodne uważa się takie, w których średnia wartość zachmurzenia wyznaczona z trzech terminów jest mniejsza od 2.0, zaś za dni pochmurne — w których wartość ta jest większa od 8.0.

I, II, III — terminy obserwacji (7^h, 13^h i 21^h średniego miejscowego czasu słonecznego).

Dies — średnia dobowa, obliczona dla temperatury według wzoru:

śr. = 1/4 (I + II + 2 × III), a dla pozostałych elementów śr. = 1/3 (I + II + III).

Natężenie zjawisk oznaczono za pomocą małych cyferek: ^{0}, ^{1} albo ^{2} umieszczonych z prawej strony u góry odpowiedniego symbolu („^{0}" oznacza zjawisko o natężeniu słabym, „^{1}" o natężeniu umiarkowanym, a „^{2}" o natężeniu silnym; w przypadku mgły cyferki te oznaczają odpowiednio: mgłę umiarkowaną, mgłę gęstą i mgłę bardzo gęstą).

Do oznaczania czasu obok godzin i minut użyto następujących symboli:

n — czas od III obserwacji dnia poprzedniego do I obserwacji dnia danego,

na — czas od północy do I obserwacji dnia danego,

a — czas między I a II terminem obserwacji,

p — czas między II a III terminem obserwacji,

np — czas od III obserwacji do północy.

Przerwy w czasie trwania zjawiska oznaczono wielokropkiem (...) lub skrótem „z prz.".

Kropka (.) postawiona na miejscu wartości liczbowej oznacza brak zjawiska, kreska (—) zaś brak danych, wartości wątpliwe podano ze znakiem zapytania (?), wartości oszacowane podano w nawiasach.

NOTE EXPLICATIVE

Les symboles employés dans le présent annuaire signifient ce qui suit:

φ — latitude géographique.

λ — longitude géographique.

H_s — hauteur du terrain du jardin météorologique, au-dessus du niveau moyen de la mer.

H_b — hauteur du baromètre au-dessus du niveau de la mer.

Pour les stations disposant d'un baromètre H_s et H_b, ces données ont été déterminées à l'aide de nivellement, pour les autres stations H_s elles l'ont été d'après la carte topograhique.

h_w — hauteur d'une girouette au-dessus du sol.

m — joint à une lettre-symbole de l'élément, indique la valeur mensuelle moyenne (p.e. U_m — indique la valeur mensuelle moyenne de l'humidité relative).

P — pression atmosphérique en millibars, réduite à 0° et à la gravité normale.

$P_{o,m}$ — moyenne d'une valeur mensuelle de la pression atmosphérique réduite au niveau moyen de la mer.

T — température en C°.

La température a été mesurée à l'aide de thermomètres installés dans un abri météorologique du type anglais à une hauteur de 2 mètres au-dessus du sol. Les températures diurnes extrêmes se rapportent à une période partant de la III-ème observation du jour précédent à la III-ème observation du jour donné.

$\overline{Max}$ — valeur mensuelle moyenne des maxima des températures diurnes.

$\overline{Min}$ — valeur mensuelle moyenne des valeurs minima des températures diurnes.

e — tension de vapeur, en millibars.

U — humidité relative en %.

Δ — déficit de l'humidité en millibars.

N — nébulosité en échelle 11° (0 signifie ciel serein, 10 — ciel entièrement couvert par les nuages). Dans la table I de l'annuaire, à côté des valeurs de la nébulosité, figurent aussi les données se rapportant aux phénomènes remarqués au cours des observations normales, et consignées à l'aide de symboles.

D — direction du vent.

v — vitesse du vent en m/sec.

n_D — fréquence de l'apparition des directions du vent.

v_{mD} — vitesse moyenne du vent selon la direction. Les observations sur le vent ont été faites (avec quelques exceptions) à l'aide d'une girouette, modèle Wild.

R — hauteur de la précipitation en mm. L'hauteur de la précipitation se rapporte à la période comprise entre la première observation (matinale) d'un jour et l'observation du jour suivant. Elle se trouve inscrite à la date du jour précédent. Ces observations ont été faites à l'aide de pluviomètres, modèle Hellmann, dont la superficie de l'ouverture mesure 200 cm², placés à 1 m au-dessus du sol, à l'exception, toutefois, de certaines stations de montagne, situées à une hauteur qui dépasse 500 m au-dessus du niveau de la mer, où l'on emploie des pluviomètres, de type montagnard, à orifice mesurant 500 cm² et placés à une hauter de 1,5 m au-dessus du sol.

V — visibilité à l'heure de la II-ème observation, exprimée d'après l'échelle internationale:

0 — les objets sont invisibles déjà à une distance inférieure à 50 m;

1 — les objets sont visibles à 50 m, mais invisibles à 200 m de distance;

2 — les objets sont visibles à 200 m, mais invisibles à 500 m de distance;

3 — les objets sont visibles à 500 m, mais invisibles à 1000 m de distance;

4 — les objets sont visibles à 1 km, mais invisibles à 2 km;

5 — les objets sont visibles à 2 km, mais invisibles à 4 km;

6 — les objets sont visibles à 4 km, mais invisibles à 10 km;

7 — les objets sont visibles à 10 km, mais invisibles à 20 km;

8 — les objets sont visibles à 20 km, mais invisibles à 50 km;

9 — les objets sont visibles à partir de 50 km de distance.

h — épaisseur de la couche de neige en centimètres selon l'observation enregistrée dans le premier délai.

pl. — neige éparse.

Insolation — en heures. Les observations effectuées à l'aide d'héliographes Campbell — Stokes.

n — nombre des jours avec phénomènes particuliers.

Dans le présent annuaire, on entend par jour avec brouillard le jour où ce phénomène entraine une diminution de visibilité au-dessous de 1 km.

Dans le présent annuaire, on entend par jours sereins les jours dont la valeur moyenne de nébulosité, résultant de trois delais, est inférieure à 2.0 et par jours couverts les jours où cette valeur est supérieure à 8.0.

I, II, III — les délais d'observations (7^h, 13^h et 21^h du temps moyen solaire local).

Dies — moyenne diurne, calculée pour la température d'après la formule:

$m = 1/4\ (I + II + 2 \times III)$, et pour les autres éléments $m = 1/3\ (I + II + III)$.

L'intensité du phénomène est marquée en petits chiffres: ^{0}, ^{1} ou ^{2} placés du coté droit en haut du symbole respectif: („^{0}" indique le phénomène dont l'intensité est faible, „^{1}" modérée et „^{2}" forte; en cas de brouillard modéré, brouillard épais et brouillard très épais).

Pour indiquer le temps (à part les heures et les minutes), on a utilisé les symboles suivants:

n — le temps écoulé depuis la III-ème observation du jour précédent jusqu'à la I-ère observation du jour donné.

na — le temps écoulé depuis minuit jusqu'à l'observation du jour donné,

a — intervalle de temps entre la I-ère et la II-ème observation,

p — intervalle de temps entre la II-ème et la III-ème observation,

np — intervalle de temps entre la III-ème observation et minuit.

Les intervalles de temps, dans la durée d'un phénomène sont indiqués par des points de suspension (...) ou par une abréviation „z prz.".

Un point (.) mis à la place d'une valeur numérique marque l'absence d'un phénomène; un trait d'union (—) indique le défaut de données; un point d'interrogation (?) signale les valeurs douteuses; les parenthèses enferment les valeurs éstimées.

WYKAZ SYMBOLI METEOROLOGICZNYCH

- deszcz
- deszcz marznący
- mżawka
- mżawka marznąca
- śnieg
- śnieg z deszczem
- krupy śnieżne
- śnieg ziarnisty
- ziarna lodowe
- grad
- słupki lodowe
- (pod symbolem opadu) opad przelotny
- mgła
- mgła lodowa
- mgła, niebo widoczne
- mgła w ławicach
- zamglenie
- mgła przyziemna
- morze mgieł
- zamieć śnieżna niska
- zamieć śnieżna wysoka
- pył wodny
- rosa
- szron
- sadź
- gołoledź
- trąba
- zmętnienie opalizujące
- zmętnienie pyłowe
- dymy
- zamieć pyłowa niska lub zamieć piaskowa niska
- zamieć pyłowa wysoka lub zamieć piaskowa wysoka
- wichura pyłowa lub wichura piaskowa
- wir pyłowy lub wir piaskowy
- halo słoneczne
- halo księżycowe
- wieniec wokół Słońca
- wieniec wokół Księżyca
- iryzacja
- gloria
- tęcza
- biała tęcza
- pierścień Bishopa
- miraż
- burza
- burza odległa
- błyskawica
- ognie św. Elma
- zorza polarna
- pokrywa śnieżna
- Słońce
- wiatr 10—15 m/sek
- wiatr > 15 m/sek
- ( ) przejrzyste powietrze
- dni pogodne
- dni pochmurne

ALFABETYCZNY SPIS STACJI METEOROLOGICZNYCH
LISTE ALPHABÉTIQUE DES STATIONS MÉTÉOROLOGIQUES

Nr	Stacja - Station	Miesiące Mois	Strona - Page Tabl. I	Tabl. II	Tabl. III	Tabl. IV 2)	φ N	λ E Gr.	H_s	H_b	Dorzecze - Bassin
1	Aleksandrowice	I-XII	-	372	414	-	49°48	19°00'	398	403,4	Wisła
2	Antołówka 1)	I-XII	-	406	414	-	49 18	19 59	918	-	Dunajec
3	Babia Góra 1)	I-XII	-	386	414	-	49 35	19 31	1180	-	Skawa
4	Baligród	I-XII	-	404	414	-	49 20	22 17	450	-	San
5	Bartoszyce	I-XII	-	218	414	-	54 15	20 48	60	-	Łyna
6	Barwinek	I-XII	-	400	414	-	49 26	21 41	420	-	Wisłoka
7	Belsk	I-XII	-	292	414	420(37)	51 50	20 48	180	-	Wisła
8	Biała Podlaska	I-XII	-	290	414	-	52 01	23 08	145	-	Bug
9	Białowieża	I-XII	-	264	414	420(42)	52 42	23 51	163	163,7	Narew
10	Biały Kościół	I-XII	-	356	414	-	50 10	19 50	400	-	Wisła
11	Białystok	I-XII	-	256	414	420(17)	53 07	23 11	139	140,8	Narew
12	Biebrza	I-XII	-	240	414	420(16)	53 39	22 36	117	-	Biebrza
13	Biecz	I-XII	-	376	414	-	49 44	21 15	260	-	Wisłoka
14	Bielsk Podlaski	I-XII	-	262	414	-	52 47	23 11	145	-	Narew
15	Bieruń Stary	I-XII	-	360	414	-	50 05	19 05	236	239,0	Wisła
16	Biłgoraj	I-XII	-	338	414	-	50 33	22 43	190	-	San
17	Bircza	I-XII	-	380	414	-	49 41	22 29	300	-	San
18	Biskupiec	I-XII	-	234	414	-	53 52	20 57	160	-	Łyna
19	Bochnia-Chodenice	I-XII	-	366	414	-	49 59	20 24	200	-	Raba
20	Bodzentyn	I-XII	-	320	414	-	50 57	20 57	270	-	Kamienna
21	Bolesławiec	VIII-XII	-	308	414	-	51 16	15 35	208	-	Bóbr
22	Borusewa	I-XII	-	352	414	-	50 17	20 47	170	-	Wisła
23	Brwinów	I-XII	-	286	414	420(32)	52 08	20 43	96	98,0	Bzura
24	Brzegi Dolne	I-XII	-	396	414	-	49 27	22 38	420	-	Strwiąż
25	Brzesna	I-XII	-	384	414	-	49 36	20 37	320	-	Dunajec
26	Bukowina Tatrzańska 1).	I-XII	-	402	414	-	49 21	20 07	880	-	Dunajec
27	Busko-Zdrój	I-XII	-	342	414	-	50 27	20 43	225	-	Nida
28	Bydgoszcz	I-XII	-	254	414	-	53 07	17 58	70	70,5	Brda
29	Bydgoszcz, IMiUZ	I-XII	-	254	414	420(13)	53 08	18 01	47	-	Brda
30	Bystrzyca Kłodzka	I-XII	-	348	414	-	50 18	16 39	370	-	Nysa Kłodzka
31	Bytom	I-XII	-	346	414	-	50 21	18 55	300	-	Przemsza
32	Chełm Lubelski	I-XII	-	314	414	420(46)	51 07	23 30	208	209,6	Bug
33	Chodzież	I-XII	-	258	414	-	52 59	16 54	100	-	Noteć
34	Chojnice	I-XII	50	238	414	420(6)	53 42	17 33	172	177,2	Brda
35	Chorzelów	I-XII	-	348	414	-	50 21	21 27	170	-	Wisła
36	Ciechocinek	I-XII	-	260	414	420(26)	52 53	18 48	44	-	Wisła
37	Cieplice Śl.-Zdrój ...	I-XII	-	324	414	-	50 52	15 41	345	-	Bóbr
38	Cieszyn	I-XII	-	374	414	420(55)	49 45	18 38	300	-	Olza
39	Cieszyn-Bobrek	I-XII	-	376	414	-	49 45	18 39	300	-	Olza
40	Ciężkowice	I-XII	-	374	414	-	49 47	20 58	280	-	Dunajec
41	Czarna Dąbrówka	I-XII	-	214	414	-	54 21	17 34	120	-	Łupawa
42	Czarniecka Góra	I-XII	-	314	414	-	51 08	20 31	256	-	Pilica
43	Czarny Dunajec	I-XII	-	394	414	-	49 27	19 51	676	-	Dunajec
44	Czernichów	I-XII	-	366	414	-	50 00	19 41	218	-	Wisła
45	Częstochowa	I-XII	-	328	414	-	50 49	19 06	261	262,7	Warta
46	Czorsztyn	I-XII	-	396	414	-	49 26	20 19	496	-	Dunajec
47	Czorsztyn-Nadzamcze 1).	I-XII	-	396	414	-	49 26	20 20	650	-	Dunajec
48	Darłowo	I-XII	-	212	414	-	54 27	16 23	3	-	Wieprza
49	Dębica	I-XII	-	362	414	-	50 03	21 24	205	-	Wisłoka
50	Długopole	I-XII	-	352	414	-	50 15	16 38	420	-	Nysa Kłodzka
51	Dobrogoszcz	I-XII	-	330	414	-	50 46	17 01	175	-	Oława
52	Dolina Chochołowska 1).	I-XII	-	406	414	-	49 15	19 49	1028	-	Dunajec
53	Dolina Pięciu Stawów .	I-XII	-	410	414	-	49 13	20 03	1668	-	Dunajec
54	Drawno	I-XII	-	252	414	-	53 13	15 46	82	-	Drawa
55	Duszniki-Zdrój 1)	I-XII	-	344	414	-	50 24	16 24	540	-	Nysa Kłodzka
56	Dynów	I-XII	-	372	414	-	49 48	22 14	276	-	San
57	Dziwnów	I-XII	-	228	414	-	54 01	14 44	7	7,1	Przymorze
58	Elbląg	I-XII	-	222	414	-	54 10	19 26	38	42,8	Elbląska
59	Felin	I-XII	-	310	414	-	51 14	22 38	215	-	Wieprz
60	Garlica Murowana	I-XII	-	358	414	-	50 09	19 56	270	-	Prądnik
61	Gdańsk-Nowy Port	I-XII	-	212	414	-	54 24	18 40	7	-	Wisła
62	Gdańsk-Siedlce	I-XII	-	214	414	-	54 21	18 36	72	-	Wisła
63	Gdańsk-Wrzeszcz	I-XII	14	212	414	-	54 23	18 36	13	12,4	Wisła

1) Podane w roczniku wysokości opadów otrzymano za pomocą deszczomierza o powierzchni otworu 500 cm².
2) W nawiasach podane są numery, pod którymi figurują stacje w tabl.IV.

Nr	Stacja - Station	Miesiące Mois	Strona - Page Tabl. I	Tabl. II	Tabl. III	Tabl. IV 2)	φ N	λ E Gr.	H_s	H_b	Dorzecze - Bassin
64	Gdynia	I-XII	-	210	414	420(8)	54°31	18°34	2	14,5	Przymorze
65	Giżycko	I-XII	-	226	414	-	54 03	21 46	132	-	Węgorapa
66	Gliwice	I-XII	-	350	414	-	50 18	18 40	220	-	Kłodnica
67	Głodowo	I-XII	-	262	414	-	52 50	19 15	129	-	Wisła
68	Głogów	I-XII	-	298	414	-	51 39	16 06	112	-	Odra
69	Głubczyce	I-XII	-	354	414	-	50 12	17 49	290	-	Odra
70	Głuchołazy	I-XII	-	350	414	-	50 18	17 23	344	-	Nysa Kłodzka
71	Gniezno	I-XII	-	270	414	-	52 33	17 36	110	-	Wełna
72	Goczałkowice	I-XII	-	368	414	-	49 57	18 55	260	-	Wisła
73	Gołdap	I-XII	-	216	414	-	54 19	22 19	150	-	Węgorapa
74	Gorzów Wlkp.	I-XII	-	264	414	420(18)	52 44	15 15	65	59,7	Warta
75	Gorzyń	I-XII	-	268	414	-	52 34	15 54	60	-	Warta
76	Goszyce	I-XII	-	356	414	-	50 11	20 08	260	-	Wisła
77	Góra Św.Anny	I-XII	-	340	414	-	50 27	18 10	370	-	Odra
78	Grabowiec	I-XII	-	316	414	-	51 06	21 23	210	-	Wisła
79	Grabownica	I-XII	-	302	414	-	51 28	17 27	119	-	Barycz
80	Grodków	I-XII	-	334	414	-	50 41	17 23	176	-	Nysa Kłodzka
81	Grudziądz	I-XII	-	244	414	-	53 30	18 46	40	-	Wisła
82	Gryfice	I-XII	-	232	414	-	53 55	15 13	40	-	Rega
83	Gubałówka 1)	I-XII	-	404	414	420(63)	49 18	19 56	1000	-	Dunajec
84	Hala Gąsienicowa 1)	I-XII	-	408	414	420(64)	49 15	20 00	1520	1520,8	Dunajec
85	Hala Ornak 1)	I-XII	-	408	414	-	49 14	19 51	1110	-	Dunajec
86	Hel	I-XII	-	208	414	420(7)	54 36	18 49	1	2,6	Przymorze
87	Kopowo	I-XII	-	218	414	-	54 16	18 14	220	-	Radunia
88	Horyniec	I-XII	-	356	414	-	50 11	23 21	240	-	San
89	Inowrocław	I-XII	-	262	414	-	52 48	18 14	90	-	Noteć
90	Istebna-Kubalonka 1)	I-XII	-	382	414	420(56)	49 36	18 54	800	-	Olza
91	Istebna-Stecówka 1)	I-XII	-	384	414	-	49 35	18 57	750	-	Wisła
92	Istebna-Zaolzie 1)	I-XII	-	384	414	-	49 34	18 56	580	-	Olza
93	Iwonicz-Zdrój	I-XII	-	388	414	420(68)	49 34	21 48	410	403,3	Wisłok
94	Jabłonka 1)	I-XII	-	392	414	420(58)	49 28	19 43	620	-	Czarna Orawa
95	Jabłonowo Pom.	I-XII	-	246	414	-	53 24	19 10	97	-	Osa
96	Jakubowice	I-XII	-	364	414	-	50 01	17 51	319	-	Odra
97	Janów Lubelski	I-VII,IX-XII	-	332	414	-	50 43	22 25	230	-	San
98	Jarosław	I-XII	-	364	414	-	50 01	22 42	204	-	San
99	Jasło	I-XII	-	378	414	-	49 44	21 28	240	-	Wisłoka
100	Jastrowie	I-XII	-	246	415	-	53 25	16 48	120	-	Gwda
101	Jastrzębie-Zdrój	I-XII	-	368	415	-	49 57	18 34	227	-	Olza
102	Jazy	I-XII	-	234	415	-	53 53	23 22	120	-	Niemen
103	Jelenia Góra	I-XII	122	322	415	-	50 54	15 48	342	343,9	Bóbr
104	Jeziory	I-XII	-	280	415	-	52 16	16 48	84	-	Warta
105	Kalisz	I-XII	-	296	415	420(39)	51 44	18 05	140	143,1	Prosna
106	Kamienica	I-XII	-	386	415	-	49 35	20 21	460	-	Dunajec
107	Kamienica Królewska....	I-XII	-	214	415	-	54 23	17 54	160	-	Łupawa
108	Kamień Krajeński	I-XII	-	244	415	-	53 32	17 32	124	-	Brda
109	Karpacz 1)	I-XII	-	328	415	-	50 46	15 45	700	708,0	Bóbr
110	Kartuzy	I-XII	-	216	415	-	54 20	18 12	220	-	Radunia
111	Kasprowy Wierch 1)	I-XII	194	408	415	420(65)	49 14	19 59	1991	1988,8	Dunajec
112	Katowice	I-XII	-	354	415	-	50 14	19 02	284	284,1	Przemsza
113	Kętrzyn	I-XII	-	224	415	-	54 06	21 21	110	107,4	Łyna
114	Kielce	I-XII	-	324	415	-	50 51	20 37	268	270,1	Nida
115	Kisielnica	I-XII	-	250	415	-	53 15	22 07	140	-	Narew
116	Klimczok 1)	I-XII	-	376	415	-	49 44	19 00	1010	-	Wisła
117	Kłodzko	I-XII	-	342	415	-	50 26	16 39	316	320,1	Nysa Kłodzka
118	Kmiecin	VII-XII	-	220	415	-	54 11	19 10	0	-	Wisła
119	Kobylec	I-XII	-	260	415	-	52 51	17 12	90	-	Wełna
120	Kolbuszowa	I-XII	-	354	415	-	50 14	21 47	208	-	Wisła
121	Kolno	I-XII	-	248	415	-	53 25	21 56	128	-	Pisa
122	Koło	I-XII	-	282	415	-	52 12	18 38	95	-	Warta
123	Kołobrzeg	I-XII	-	220	415	420(2)	54 11	15 35	3	5,4	Parsęta
124	Kołobrzeg-Wydma	I-XII	-	220	415	-	54 11	15 33	5	-	Parsęta
125	Kołuda Wielka	I-XII	-	264	415	-	52 44	18 09	85	-	Noteć
126	Komańcza.....	I-XII	-	404	415	-	49 20	22 04	470	-	San
127	Kończewice	I-XII	-	252	415	-	53 11	18 33	94	-	Wisła
128	Kopna Góra	I-XII	-	252	415	-	53 15	23 29	160	-	Narew
129	Korfantów	I-XII	-	340	415	-	50 29	17 36	200	-	Nysa Kłodzka
130	Koszalin	I-XII	-	218	415	-	54 12	16 10	33	33,9	Przymorze
131	Kościerzyna	I-XII	-	222	415	-	54 08	17 58	180	-	Wierzyca
132	Kórnik	I-XII	-	282	415	420(23)	52 15	17 06	77	-	Warta

Nr	Stacja - Station	Miesiące Mois	Strona - Page Tabl. I	Tabl. II	Tabl. III	Tabl. IV 2)	φ N	λ E Gr.	H_s	H_b	Dorzecze - Bassin
133	Kraków-Chełm	I-XII	-	362	415	-	50°04'	19°51'	225	-	Rudawa
134	Kraków-Czyżyny	I-XII	-	360	415	-	50 05	20 01	213	213,4	Prądnik
135	Kraków-Nowa Huta	I-XII	-	362	415	-	50 04	20 05	195	-	Wisła
136	Kraków,Obserw.Astr.UJ .	I-XII	158	362	415	420(54)	50 04	19 58	206	219,8	Wisła
137	Krasnystaw	I-XII	-	318	415	-	50 59	23 10	190	-	Wieprz
138	Kraśnik Dolny	I-XII	-	308	415	-	51 17	15 36	180	-	Bóbr
139	Kraśnik Lebelski	I-XII	-	320	415	-	50 55	22 12	250	-	Wisła
140	Krosno	I-XII	-	380	415	-	49 41	21 45	282	-	Wisłok
141	Krościenko.....	I-XII	-	396	415	-	49 27	20 25	440	-	Dunajec
142	Krynica 1).....	I-XII	-	398	415	420(59)	49 26	20 58	613	-	Poprad
143	Krynica-Góra Parkowa 1).	I-XII	-	398	415	420(60)	49 25	20 58	740	-	Poprad
144	Krynica Morska	I-XII	-	214	415	-	54 23	19 27	4	-	Zalew Wiślany
145	Krzemień	I-XII	-	270	415	-	52 33	22 30	111	-	Bug
146	Krzyż.....	I-XII	-	260	415	-	52 53	16 01	31	-	Noteć
147	Kudowa-Zdrój	I-XII	-	340	415	420(50)	50 27	16 16	385	-	Łaba
148	Kuźnice 1).....	I-XII	-	406	415	-	49 16	19 59	1023	-	Dunajec
149	Kwidzyń	I-XII	-	236	415	-	53 44	18 55	15	-	Wisła
150	Laskowice Oławskie	I-XII	-	316	415	420(25)	51 03	17 21	135	-	Widawa
151	Lądek-Zdrój 1).....	I-XII	-	346	415	-	50 21	16 53	460	-	Nysa Kłodzka
152	Legionowo	I-XII	-	274	415	420(28)	52 24	20 58	93	103,7	Wisła
153	Legnica	I-XII	-	310	415	-	51 13	16 10	121	126,3	Kaczawa
154	Lesko	I-XII	-	394	415	420(69)	49 28	22 20	386	-	San
155	Leskowiec 1).....	I-XII	-	372	415	-	49 48	19 27	870	-	Skawa
156	Leszno-Strzyżewice	I-XII	-	292	415		51 50	16 32	91	-	Barycz
157	Leżajsk	I-XII	-	354	415	-	50 15	22 26	190	-	San
158	Lębork	I-XII	-	210	415	-	54 33	17 45	18	21,8	Łeba
159	Libertów	I-XII	-	368	415	-	49 58	19 53	320	-	Wisła
160	Lidzbark	I-XII	-	250	415	-	53 16	19 50	150	-	Drwęca
161	Lidzbark Warmiński	I-XII	-	222	415	-	54 08	20 36	90	-	Łyna
162	Limanowa	I-XII	-	378	415	-	49 42	20 25	440	-	Dunajec
163	Lipki	I-XII	-	250	415	-	53 21	14 58	30	-	Odra
164	Lipowa	I-XII	-	326	415	-	50 50	21 27	245	-	Wisła
165	Lubaczów	I-XII	-	358	415	-	50 09	23 08	214	-	San
166	Lublin	I-XII	-	310	415	-	51 14	22 34	171	176,7	Wieprz
167	Lubliniec	I-XII	-	334	415	-	50 40	18 41	256	-	Mała Panew
168	Luboń Wielki 1).....	I-XII	-	382	415	-	49 39	19 59	1023	-	Raba
169	Łagiewniki	I-XII	-	266	415	-	52 40	18 19	80	-	Noteć
170	Łącko	I-XII	-	390	415	-	49 33	20 26	360	-	Dunajec
171	Łeba	I-XII	-	208	415	-	54 46	17 34	2	-	Łeba
172	Łosice	I-XII	-	284	415	-	52 12	22 43	153	-	Bug
173	Łowicz	I-XII	-	286	415	-	52 07	19 56	95	-	Bzura
174	Łódź-Lublinek	I-XII	98	296	415	420(38)	51 44	19 24	187	187,7	Ner
175	Łódź-Ruda Pabianicka ..	I-XII	-	296	415	-	51 42	19 27	181	-	Ner
176	Łysa Polana 1).....	I-XII	-	406	415	-	49 16	20 07	988	-	Dunajec
177	Maków Podhalański	I-XII	-	376	415	-	49 44	19 40	350	-	Skawa
178	Malbork	I-XII	-	228	415	-	54 02	19 02	20	-	Wisła
179	Maniowy 1).....	I-XII	-	394	415	-	49 28	20 15	520	-	Dunajec
180	Miastko	I-XII	-	230	415	-	54 00	16 58	145	-	Wieprza
181	Miechów	I-XII	-	346	415	-	50 22	20 02	292	-	Wisła
182	Mielec	I-XII	-	350	415	-	50 18	21 27	168	170,2	Wisłoka
183	Międzybrodzie Bialskie.	I-XII	-	374	415	-	49 47	19 12	320	-	Soła
184	Międzylesie	I-XII	-	-	-	420(31)	52 12	21 11	90	-	Wisła
185	Międzyzdroje	I-XII	-	230	415	420(3)	53 56	14 27	10	-	Przymorze
186	Mikołajki	I-XII	-	234	415	420(15)	53 47	21 35	127	131,1	Pisa
187	Mława	I-XII	-	254	415	-	53 07	20 22	141	145,8	Wkra
188	Młochów	I-XII	-	288	415	420(35)	52 03	20 47	141	-	Bzura
189	Morąg	VII-XII	-	232	415	-	53 55	19 56	113	-	Drwęca
190	Morskie Oko 1).....	I-XII	-	410	415	-	49 12	20 04	1400	-	Dunajec
191	Motycz	I-XII	-	308	415	-	51 15	22 25	213	-	Wieprz
192	Mszana Dolna	I-XII	-	380	415	-	49 40	20 05	410	-	Raba
193	Muszyna	I-XII	-	402	415	420(61)	49 21	20 53	445	447,1	Poprad
194	Myczkowce	I-XII	-	400	415	-	49 26	22 25	410	-	San
195	Myślenice	I-XII	-	370	415	-	49 49	19 56	295	-	Raba
196	Myślenickie Turnie 1)...	I-XII	-	408	415	-	49 15	19 59	1360	-	Dunajec
197	Nasyałów	I-XII	-	316	415	-	51 05	17 43	151	-	Widawa
198	Nidzica	I-XII	-	248	415	-	53 22	20 25	170	-	Wkra
199	Niepokalanów	I-XII	-	284	415	-	52 12	20 25	92	-	Bzura
200	Niska	I-XII	-	338	415	-	50 31	22 09	164	-	San
201	Nowa Wieś	I-XII	-	302	415	-	51 27	22 45	179	-	Wieprz

Nr	Stacja - Station	Miesiące Mois	Strona - Page Tabl. I	Tabl. II	Tabl. III	Tabl. IV 2)	φ N	λ E Gr.	H_s	H_b	Dorzecze - Bassin
202	Nowe Miasto n.P.	I-XII	-	300	415	-	51°37'	20°35'	155	-	Pilica
203	Nowogard	I-XII	-	240	415	-	53 40	15 07	60	-	Przymorze
204	Nowy Dwór Gdański	I-XII	-	218	416	-	54 13	19 08	0	-	Wisła
205	Nowy Dwór Mazowiecki ..	I-XII	-	274	416	-	52 26	20 43	70	-	Wisła
206	Nowy Sącz	I-XII	-	382	416	-	49 37	20 42	292	295,4	Dunajec
207	Nowy Targ 1)	I-XII	-	392	416	-	49 29	20 02	600	-	Dunajec
208	Nur	I-XII	-	266	416	-	52 40	22 19	110	-	Bug
209	Obidowa 1)	I-XII	-	388	416	-	49 33	19 58	800	-	Raba
210	Oborniki Śląskie	I-XII	-	308	416	420(24)	51 18	16 55	180	-	Odra
211	Ochaby	I-XII	-	370	416	-	49 51	18 46	270	-	Wisła
212	Olecko	I-XII	-	228	416	-	54 03	22 30	181	177,7	Biebrza
213	Olesno	I-XII	-	322	416	-	50 53	18 25	238	-	Stobrawa
214	Olkusz	I-XII	-	352	416	-	50 17	19 34	360	-	Przemsza
215	Olsztyn-Dajtki	I-XII	38	236	416	-	53 46	20 25	133	135,4	Łyna
216	Oława-Zwierzyniec	I-XII	-	320	416	-	50 57	17 18	137	-	Odra
217	Opoczno	I-XII	-	306	416	-	51 23	20 16	180	-	Pilica
218	Opole	I-XII	-	334	416	420(49)	50 40	17 58	176	177,9	Odra
219	Opole Lubelskie	I-XII	-	312	416	-	51 09	21 59	149	-	Wisła
220	Orneta	I-XII	-	224	416	-	54 07	20 07	70	-	Pasłęka
221	Osowiec	I-XII	-	244	416	-	53 29	22 39	110	-	Biebrza
222	Ostrołęka	I-XII	-	256	416	-	53 05	21 34	95	96,3	Narew
223	Ostroszowice	I-XII	-	336	416	-	50 39	16 38	375	-	Nysa Kłodzka
224	Ostrowy	I-XII	-	276	416	-	52 18	19 10	120	-	Bzura
225	Ostróda	I-XII	-	240	416	-	53 42	19 58	106	-	Drwęca
226	Ostrów Wlkp.	I-XII	-	298	416	-	51 39	17 49	126	-	Prosna
227	Ostrzeszów	I-XII	-	304	416	-	51 26	17 56	198	-	Prosna
228	Otmuchów	I-XII	-	340	416	-	50 28	17 10	211	-	Nysa Kłodzka
229	Ożańsk	I-XII	-	364	416	-	50 01	22 35	250	-	San
230	Paproć	I-XII	-	276	416	-	52 19	16 08	75	-	Obra
231	Pętkowo	I-XII	-	282	416	-	52 12	17 15	86	-	Warta
232	Piaszczyna	I-XII	-	228	416	-	54 01	17 10	175	-	Brda
233	Piotrków Trybunalski ..	I-XII	-	304	416	-	51 25	19 42	200	-	Pilica
234	Pisz	I-XII	-	242	416	-	53 38	21 48	118	-	Pisa
235	Piwniczna	I-XII	-	398	416	-	49 26	20 42	380	-	Poprad
236	Pleszew	I-XII	-	292	416	-	51 54	17 47	120	-	Prosna
237	Plewiska	I-XII	-	-	-	420(22)	52 22	16 48	80	-	Warta
238	Płock-Radziwie	I-XII	-	270	416	-	52 32	19 40	63	63,8	Wisła
239	Płocko	I-XII	-	222	416	-	54 09	16 50	125	-	Wieprza
240	Polanica-Zdrój	I-XII	-	344	416	420(51)	50 24	16 30	400	-	Nysa Kłodzka
241	Połczyn-Zdrój	I-XII	-	236	416	-	53 46	16 06	50	-	Parsęta
242	Porąbka	I-XII	-	370	416	-	49 49	19 13	315	-	Soła
243	Poronin 1)	I-XII	-	402	416	-	49 20	20 02	800	-	Dunajec
244	Poświętne	I-XII	-	266	416	-	52 38	20 23	101	-	Wkra
245	Poturzyn	I-XII	-	338	416	-	50 34	23 56	240	-	Bug
246	Poznań-Ławica	I-XII	74	274	416	420(21)	52 25	16 50	86	92,1	Warta
247	Poznań-Sołacz	I-XII	-	272	416	-	52 26	16 54	71	-	Warta
248	Prabuty	I-XII	-	238	416	420(12)	53 44	19 13	98	-	Wisła
249	Prudnik	I-XII	-	348	416	-	50 19	17 34	265	-	Odra
250	Przasnysz	I-XII	-	258	416	-	53 01	20 53	120	-	Narew
251	Przebędowo	I-XII	-	268	416	420(19)	52 35	17 01	82	-	Warta
252	Przedbórz	I-XII	-	316	416	-	51 05	19 53	235	-	Pilica
253	Przehyba 1)	I-XII	-	394	416	-	49 28	20 34	1175	-	Poprad
254	Przelewice	I-XII	-	256	416	-	53 06	15 05	60	-	Odra
255	Przemyśl	I-XII	170	372	416	-	49 48	22 46	237	238,9	San
256	Przybroda	I-XII	-	272	416	420(20)	52 31	16 40	88	-	Warta
257	Pszczela Wola	I-XII	-	314	416	-	51 07	22 31	195	-	Wieprz
258	Pszczyna	I-XII	-	366	416	-	50 00	18 55	270	-	Wisła
259	Ptaszkowa 1)	I-XII	-	386	416	-	49 36	20 53	522	-	Dunajec
260	Puck	I-XII	-	208	416	-	54 43	18 25	1	-	Przymorse
261	Puczniew	I-XII	-	294	416	-	51 47	19 05	142	-	Ner
262	Puławy	I-XII	-	306	416	420(45)	51 25	21 58	142	155,2	Wisła
263	Pułtusk	I-XII	-	264	416	-	52 42	21 06	80	-	Narew
264	Raba Wyżna 1)	I-XII	-	386	416	-	49 34	19 53	600	-	Raba
265	Rabka	I-XII	-	384	416	420(57)	49 36	19 58	512	552,5	Raba
266	Racibórz	I-XII	-	360	416	-	50 05	18 13	189	192,6	Odra
267	Radom	I-XII	-	304	416	-	51 25	21 07	178	-	Wisła
268	Radostowo	I-XII	-	230	416	420(11)	53 59	18 45	40	-	Wisła
269	Radzyń Podlaski	I-XII	-	294	416	-	51 48	22 38	151	-	Wieprz
270	Reguły	I-XII	-	284	416	-	52 10	20 51	98	-	Bzura
271	Resko	I-XII	-	234	416	420(4)	53 46	15 25	55	56,2	Rega

Nr	Stacja - Station	Miesiące Mois	Strona - Page Tabl. I	Tabl. II	Tabl. III	Tabl. IV 2)	φ N	λ E Gr.	H_s	H_b	Dorzecze - Basin
272	Rosnowo	I-XII	-	226	416	-	54°04'	16°18'	62	-	Parsęta
273	Rozewie	I-XII	-	208	416	-	54 50	18 20	54	-	Przymorze
274	Rożnów	I-XII	-	374	416	-	49 46	20 41	300	-	Dunajec
275	Różanystok	I-XII	-	242	416	-	53 38	23 24	160	-	Biebrza
276	Rybnik	I-XII	-	358	416	-	50 06	18 33	243	-	Odra
277	Rymanów-Zdrój	I-XII	-	390	416	-	49 33	21 51	360	-	Wisłok
278	Rzeszów-Jasionka	I-XII	-	360	416	-	50 06	22 03	200	201,7	Wisłok
279	Sandomierz	I-XII	146	334	416	-	50 41	21 45	202	200,3	Wisła
280	Sanok	I-XII	-	388	416	-	49 34	22 12	314	-	San
281	Sejny	I-XII	-	224	416	-	54 06	23 21	130	-	Niemen
282	Siedlce	I-XII	-	284	416	-	52 11	22 16	146	149,1	Liwiec
283	Siejnik	I-XII	-	230	416	-	54 01	22 29	170	-	Biebrza
284	Sielec	I-XII	-	348	416	-	50 19	20 25	202	-	Wisła
285	Siemianice	I-XII	-	312	416	-	51 11	18 09	182	-	Prosna
286	Siemiatycze	I-XII	-	274	416	-	52 26	22 52	145	-	Bug
287	Sieniawa 1)	I-XII	-	392	416	-	49 32	19 55	578	-	Raba
288	Sieradz	I-XII	-	300	416	-	51 36	18 44	137	-	Warta
289	Silniczka	I-XII	-	320	416	-	50 55	19 46	215	-	Pilica
290	Sinołęka	I-XII	-	282	416	-	52 13	21 55	160	-	Liwiec
291	Skierniewice	I-XII	-	290	416	420(36)	51 58	20 10	128	129,5	Bzura
292	Skroniów	I-XII	-	336	416	420(52)	50 38	20 16	256	-	Nida
293	Słubice	I-XII	-	276	416	-	52 21	14 36	20	22,2	Odra
294	Słupca	I-XII	-	276	416	-	52 17	17 52	90	-	Warta
295	Słupia Nowa	I-XII	-	324	416	-	50 52	21 05	307	-	Kamienna
296	Słupsk	I-XII	-	212	416	-	54 28	17 01	16	-	Słupia
297	Smolice	I-XII	-	298	416	-	51 42	17 11	107	-	Baryca
298	Sobieszyn	I-XII	-	300	416	420(44)	51 36	22 10	159	-	Wieprz
299	Sobótka	I-XII	-	322	416	-	50 54	16 45	204	-	Bystrzyca
300	Sokołowsko 1)	I-XII	-	332	416	-	50 41	16 14	570	-	Nysa Kłodzka
301	Sokółka	I-XII	-	248	416	-	53 24	23 30	180	-	Narew
302	Spalona 1)	I-XII	-	350	416	-	50 17	16 33	790	-	Nysa Kłodzka
303	Stańcowa 1)	I-XII	-	388	416	-	49 33	19 32	850	-	Czarna Orawa
304	Stare Pole	I-XII	-	226	416	420(10)	54 04	19 13	3	-	Wisła
305	Stary Sącz	I-XII	-	390	416	-	49 33	20 39	320	-	Poprad
306	Staszów	I-XII	-	336	416	-	50 34	21 10	193	-	Wisła
307	Strzelna	I-XII	-	292	416	-	51 49	19 54	194	-	Bzura
308	Strzyżów	I-XII	-	326	416	-	50 51	24 02	185	-	Bug
309	Suchedniów I	I-XII	-	318	417	-	51 03	20 50	272	-	Kamienna
310	Suchedniów II	IX-XII	-	318	417	-	51 02	20 50	278	-	Kamienna
311	Sulejów	I-XII	-	306	417	-	51 22	19 53	186	-	Pilica
312	Sulęcin	I-XII	-	272	417	-	52 26	15 07	80	-	Warta
313	Suwałki	I-XII	26	224	417	420(14)	54 06	22 57	165	169,6	Niemen
314	Szamotuły	I-XII	-	268	417	-	52 37	16 34	70	-	Warta
315	Szczawnica	I-XII	-	398	417	-	49 26	20 29	500	-	Dunajec
316	Szczawno-Zdrój	I-XII	-	328	417	420(47)	50 48	16 16	415	-	Bystrzyca
317	Szczecin-Dąbie	I-XII	62	246	417	-	53 24	14 37	1	6,9	Odra
318	Szczecin-Niebuszewo ...	I-XII	-	244	417	-	53 28	14 33	69	-	Odra
319	Szczecinek	I-XII	-	238	417	420(5)	53 43	16 41	137	142,6	Gwda
320	Szczekociny	I-XII	-	336	417	-	50 38	19 49	262	-	Pilica
321	Szczerców	I-XII	-	306	417	-	51 20	19 07	160	-	Warta
322	Szczuczyn	I-XII	-	242	417	-	53 34	22 17	130	-	Biebrza
323	Szczytno	I-XII	-	242	417	-	53 34	21 02	144	-	Narew
324	Szepietowo	I-XII	-	262	417	420(41)	52 51	22 33	150	-	Bug
325	Szklarska Poręba 1)	I-XII	-	326	417	-	50 50	15 32	640	-	Bóbr
326	Szprotawa	I-XII	-	300	417	-	51 34	15 32	122	-	Bóbr
327	Szrenica 1)	I-XII	-	328	417	-	50 48	15 31	1323	1363,6	Bóbr
328	Szymanów	I-XII	-	312	417	-	51 08	16 29	145	-	Odra
329	Śliwice	I,III-XII	-	238	417	-	53 43	18 11	115	-	Czarna Woda
330	Śnieżka 1)	I-XII	134	330	417	420(48)	50 44	15 44	1603	1610,6	Bóbr
331	Śrem	I-XII	-	288	417	-	52 05	17 01	85	-	Warta
332	Świbno	I-XII	-	216	417	420(9)	54 20	18 56	3	-	Wisła
333	Świder	I-XII	-	286	417	420(33)	52 07	21 15	94	-	Świder
334	Świdnica	I-XII	-	324	417	-	50 51	16 29	230	-	Bystrzyca
335	Świdwin	I-XII	-	236	417	-	53 46	15 46	94	-	Rega
336	Świebodzin	I-XII	-	280	417	-	52 15	15 32	78	-	Odra
337	Świeradów-Zdrój	I-XII	-	322	417	-	50 54	15 20	549	-	Bóbr
338	Świerklaniec	I-XII	-	342	417	420(53)	50 26	18 57	284	-	Przemsza
339	Święty Krzyż	I-XII	-	326	417	-	50 51	21 03	575	-	Kamienna
340	Świnoujście	I-XII	-	232	417	-	53 55	14 14	6	5,4	Przymorze
341	Tarnobrzeg	I-XII	-	338	417	-	50 34	21 40	175	-	Wisła

Nr	Stacja - Station	Miesiące Mois	Strona - Page Tabl. I	Tabl. II	Tabl. III	Tabl. IV 2)	φ N	λ E Gr.	H_s	H_b	Dorzecze - Bassin
342	Tarnogród	I-XII	-	346	417	-	50°22′	22°45′	217	-	San
343	Tarnów	I-XII	-	364	417	-	50 02	20 59	209	209,1	Dunajec
344	Tczew	I-XII	-	226	417	-	54 05	18 48	10	-	Wisła
345	Terespol	I-XII	-	288	417	420(43)	52 05	23 37	133	135,0	Bug
346	Tęgoborze	I-XII	-	378	417	-	49 43	20 39	272	-	Dunajec
347	Tolkmicko	I-XII	-	216	417	-	54 19	19 32	1	-	Zalew Wiślany
348	Tomaszów Lubelski	I-XII	-	342	417	-	50 27	23 25	273	-	Bug
349	Topola-Błonie	I-XII	-	288	417	420(34)	52 05	19 11	109	-	Ner
350	Toruń-Wrzsy.....	I-XII	-	256	417	-	53 03	18 35	69	70,2	Wisła
351	Trzcińsko-Zdrój	I-XII	-	258	417	-	52 58	14 36	60	-	Odra
352	Trzebiechów	I-XII	-	290	417	-	52 01	15 44	55	-	Obrzyca
353	Trzebież	I-XII	-	240	417	-	53 40	14 31	1	-	Zalew Szczeciński
354	Trzebinia	I-XII	-	356	417	-	50 10	19 28	320	-	Wisła
355	Trzemeszno	I-XII	-	270	417	-	52 34	17 49	105	-	Noteć
356	Turbacz 1)	I-XII	-	390	417	-	49 33	20 07	1308	-	Raba
357	Tychy	I-XII	-	358	417	-	50 08	18 59	280	-	Wisła
358	Tykocin	I-XII	-	252	417	-	53 12	22 47	120	-	Narew
359	Ustka	I-XII	-	210	417	420(1)	54 35	16 52	6	8,1	Słupia
360	Ustka-Wydma	I-XII	-	210	417	-	54 35	16 52	7	-	Słupia
361	Ustrzyki Górne 1)	I-XII	-	410	417	-	49 07	22 40	650	-	San
362	Wadowice	I-XII	-	368	417	-	49 53	19 31	260	-	Skawa
363	Wałcz	I-XII	-	250	417	-	53 17	16 28	111	113,8	Gwda
364	Warka	I-XII	-	294	417	-	51 47	21 12	120	-	Pilica
365	Warszawa-Bielany	I-XII	86	278	417	420(29)	52 17	20 58	98	104,7	Wisła
366	Warszawa, Inst.Geogr.UW	I-XII	-	278	417	-	52 14	21 01	108	-	Wisła
367	Warszawa, Min.Kom.	I-XII	-	-	-	420(30)	52 13	21 01	?	-	Wisła
368	Warszawa, Obserw.Astr.UW	I-XII	-	278	417	-	52 13	21 02	110	114,8	Wisła
369	Warszawa-Okęcie	I-XII	-	280	417	-	52 09	20 59	106	106,9	Wisła
370	Warszawa, St.Pomp.Rz. .	I-VI,VIII-XII	-	278	417	-	52 13	21 03	85	-	Wisła
371	Wądołki Borowe	I-XII	-	258	417	-	52 57	22 13	130	-	Narew
372	Werbkowice	I-XII	-	330	417	420(66)	50 45	23 46	204	-	Bug
373	Wielichowo	I-XII	-	286	417	-	52 07	16 21	65	-	Obra
374	Wieliczka	I-XII	-	366	417	-	50 00	20 03	225	-	Wisła
375	Wieliszew	I-XII	-	272	417	-	52 27	20 58	78	-	Bug
376	Wieluń	I-XII	-	310	417	420(40)	51 13	18 35	195	198,4	Warta
377	Wieniec-Zdrój	I-XII	-	266	417	-	52 40	19 00	82	-	Wisła
378	Wierzchowo	I-XII	-	246	417	-	53 27	16 06	140	-	Drawa
379	Więcławice	I-XII	-	260	417	420(27)	52 51	18 19	90	-	Noteć
380	Wińsko	I-XII	-	302	417	-	51 28	16 37	180	-	Barycz
381	Wirty	I-XII	-	232	417	-	53 54	18 23	121	-	Wierzyca
382	Wisła	I-XII	-	380	417	-	49 39	18 52	430	-	Wisła
383	Wisznice	I-XII	-	296	417	-	51 47	23 13	152	-	Bug
384	Witów 1)	I-XII	-	402	417	-	49 20	19 50	835	-	Dunajec
385	Włodawa	I-XII	-	302	417	-	51 33	23 33	175	175,9	Bug
386	Wojcieszów Górny	I-XII	-	318	417	-	50 57	15 55	358	-	Kaczawa
387	Wolbrom	I-XII	-	344	417	-	50 23	19 45	373	-	Przemsza
388	Wrocław-Gądów Mały	I-XII	110	314	417	-	51 08	16 59	116	118,6	Odra
389	Wyrzysk	I-XII	-	254	417	-	53 09	17 16	90	-	Noteć
390	Wysowa 1)	I-XII	-	400	417	-	49 26	21 11	525	-	Wisłoka
391	Wyszków	I-XII	-	268	417	-	52 35	21 27	96	-	Bug
392	Zakopane 1)	I-XII	182	404	417	420(62)	49 18	19 57	844	838,2	Dunajec
393	Zakrzów	I-XII	-	352	417	-	50 16	18 09	217	-	Odra
394	Zamość	I-XII	-	330	417	-	50 44	23 15	219	218,8	Wieprz
395	Zamość-Zamczysko	IX-XII	-	332	417	-	50 44	23 15	212	-	Wieprz
396	Zawodzie	I-XII	-	248	417	-	53 23	21 24	122	-	Narew
397	Zawoja 1)	I-XII	-	382	417	-	49 37	19 31	670	-	Skawa
398	Zawołocze	I-XII	-	304	417	-	51 26	23 34	165	-	Bug
399	Ząbkowice	I-XII	-	344	417	-	50 22	19 17	314	-	Przemsza
400	Zbąszyń	I-XII	-	280	417	-	52 15	15 56	57	-	Odra
401	Zdanów	I-XII	-	332	417	420(67)	50 43	21 33	236	-	Wisła
402	Zgorzelec	I-XII	-	312	417	-	51 08	15 02	219	217,9	Nysa Łużycka
403	Zielona Góra	I-XII	-	290	417	-	51 56	15 30	180	173,8	Odra
404	Zwardoń 1)	I-XII	-	392	417	-	49 30	18 59	690	-	Soła
405	Żarnowa	I-XII	-	370	417	-	49 52	21 50	256	-	Wisłok
406	Żary	I-XII	-	298	417	-	51 38	15 08	162	-	Bóbr
407	Żegiestów-Zdrój	I-XII	-	400	417	-	49 22	20 49	440	-	Poprad
408	Żelechów	I-XII	-	294	417	-	51 49	21 54	175	-	Wisła
409	Żelisławki	I-XII	-	220	417	-	54 10	18 39	68	-	Wisła
410	Żywiec-Sporysz	I-XII	-	378	417	-	49 41	19 13	360	-	Soła

1962

TABLICA I

SPOSTRZEŻENIA CODZIENNE STACJI METEOROLOGICZNYCH

OBSERVATIONS DIURNES DE STATIONS MÉTÉOROLOGIQUES

1. Gdańsk-Wrzeszcz
2. Suwałki
3. Olsztyn-Dajtki
4. Chojnice
5. Szczecin-Dąbie
6. Poznań-Ławica
7. Warszawa-Bielany
8. Łódź-Lublinek
9. Wrocław-Gądów Mały
10. Jelenia Góra
11. Śnieżka, Obserwatorium Wysokogórskie
12. Sandomierz
13. Kraków, Obserwatorium Astronomiczne UJ
14. Przemyśl
15. Zakopane
16. Kasprowy Wierch, Obserwatorium Wysokogórskie

Gdańsk - Wrzeszcz φ = 54°23' λ = 18°36' Styczeń - Janvier 1962

DNI	CIŚNIENIE P= 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	95.3	96.2	99.4	97.0	5.0	3.0	2.2	3.1	5.2	-2.6	89	77	75	80	1.0	1.7	1.8	1.5	9	9	7	SSW 8	SW 12	SW 10
2	104.6	108.3	112.7	108.5	0.6	-0.5	-3.0	-1.5	2.3	-3.7	81	74	77	77	1.3	1.6	1.1	1.3	10	9	0	WNW 9	NW 9	W 4
3	112.1	117.4	122.3	117.3	1.0	2.4	-0.1	0.8	2.8	-5.1	85	82	90	86	1.0	1.3	0.7	1.0	9	9	0	WNW 12	NW 6	W 3
4	123.1	122.6	120.6	122.1	-0.5	0.4	1.4	0.7	1.4	-1.5	90	89	92	90	0.6	0.7	0.6	0.6	10	10	9	SW 3	W 5	W 12
5	118.1	116.2	111.2	115.2	2.1	2.6	-0.4	1.0	4.2	-0.6	93	88	92	91	0.5	1.0	0.5	0.7	10	10	10	W 9	WSW 5	SW 7
6	104.2	102.9	103.2	103.4	0.8	1.6	2.7	2.0	2.8	-2.4	86	85	86	86	0.9	1.1	1.0	1.0	10 ●	10 ⁂	9	SW 14	WSW 12	W 8
7	111.7	118.5	122.6	117.6	1.6	2.3	-0.2	0.9	3.2	-0.4	85	86	88	86	1.1	1.0	0.7	0.9	4	9	0	NW 8	N 8	SW 4
8	120.4	121.2	121.5	121.0	1.3	2.8	2.0	2.0	3.1	-2.5	85	89	89	88	1.0	0.8	0.8	0.9	10	10	10	SW 1	SW 1	SW 2
9	117.1	112.5	109.9	113.2	1.3	2.6	1.2	1.6	2.9	0.4	94	89	83	89	0.4	0.8	1.2	0.8	10	9	9	S 3	S 4	S 4
10	107.1	104.4	100.4	104.0	1.8	1.4	-0.4	0.6	2.0	-0.7	87	81	84	84	0.9	1.3	0.9	1.0	10	9	9	S 3	S 5	SSE 7
11	99.7	97.4	95.2	96.8	3.9	3.0	4.5	4.0	4.5	-0.8	82	79	79	80	1.5	1.6	1.8	1.6	6	10	10	SSW 7	SSE 6	S 6
12	97.8	99.1	91.6	96.2	5.8	5.1	1.5	3.5	6.7	1.1	77	78	94	83	2.1	2.0	0.4	1.5	8	9	10	SSW 9	SSW 4	SSE 4
13	81.9	83.1	86.7	83.9	1.6	4.6	4.5	3.8	4.9	0.9	93	73	60	75	0.6	2.3	3.3	2.1	10	1	9	S 3	SW 10	SW 13
14	91.5	94.3	97.5	94.4	3.0	3.6	3.2	3.2	4.6	2.1	74	76	79	76	2.0	1.9	1.6	1.8	4	9 ●	10	SW 7	SW 9	SW 4
15	102.4	107.2	112.0	107.2	3.4	4.3	2.6	3.2	4.5	2.3	88	71	89	83	0.9	2.4	0.8	1.4	10 ●	9	3	SW 5	WSW 8	SW 3
16	115.7	113.9	110.2	113.3	2.8	2.7	3.4	3.1	3.7	1.2	76	77	66	73	1.9	1.7	2.6	2.1	5	10	10	SSW 3	S 6	S 7
17	108.5	109.9	111.4	109.9	2.0	3.7	3.0	2.9	4.3	1.5	89	87	79	85	0.8	1.1	1.6	1.2	10 ⁂	10	10	SW 5	SW 6	S 5
18	109.3	107.8	108.4	108.5	3.0	4.4	3.8	3.8	4.7	1.4	79	71	85	78	1.6	2.5	1.2	1.8	10	10	10	S 3	S 6	SW 9
19	111.1	111.2	104.3	108.9	4.3	4.9	3.2	3.9	5.4	2.0	84	73	91	83	1.4	2.4	0.7	1.5	9	4	10	SSW 5	SW 7	SE 5
20	100.9	104.5	113.7	106.4	4.2	5.7	5.2	5.1	6.0	1.7	84	77	84	82	1.3	2.1	1.4	1.6	10 ●	9	9	SW 8	WSW 14	WSW 6
21	111.4	114.7	111.3	112.5	5.5	5.6	4.3	4.9	5.6	3.6	78	72	95	82	1.9	2.5	0.4	1.6	6	9	10 ●	WSW 12	WSW 9	SE 3
22	104.5	97.4	97.4	99.8	7.0	7.4	5.7	6.4	8.6	3.4	90	84	68	81	1.0	1.6	3.0	1.9	10	10	6	S 6	SE 5	S 10
23	102.1	104.7	105.4	104.1	4.0	4.7	3.5	3.9	5.7	2.5	67	62	83	71	2.6	3.2	1.3	2.4	7	8	9 ●	SSW 9	SW 10	SW 10
24	109.1	110.2	110.6	110.0	3.5	3.9	2.6	3.2	4.5	1.5	80	78	88	82	1.5	1.8	1.0	1.4	5	9	10	WSW 6	SW 4	SW 2
25	107.2	105.3	108.2	106.9	1.8	2.2	2.1	2.0	2.9	0.9	93	93	91	92	0.6	0.6	0.6	0.6	10	10	10 ●	SSE 2	ESE 2	NE 5
26	114.8	115.9	112.8	114.5	1.6	2.8	0.8	1.5	2.9	-0.3	85	69	88	81	1.1	2.4	0.8	1.4	10 ⁂	2	9	NNE 5	WNW 4	C 0
27	108.2	109.4	108.1	108.6	0.5	2.3	1.6	1.5	3.1	-0.3	96	86	94	92	0.2	1.0	0.4	0.5	10 ⁂	10	10 ●	S 1	NW 8	NW 4
28	107.7	111.4	118.1	112.4	-0.6	-2.1	-2.0	-1.7	2.0	-4.2	77	94	77	83	1.3	0.3	1.3	1.0	10 ⁂	10 ⁂	10 ⁂	NW 12	N 12	NE 12
29	125.5	130.5	135.2	130.4	-3.1	-4.8	-6.1	-5.0	-1.7	-6.2	75	86	73	78	1.2	0.6	1.0	0.9	10 ⁂	9 ⁂	9	NE 12	NE 9	ENE 6
30	138.4	140.6	140.7	139.9	-7.2	-7.5	-6.3	-6.8	-5.7	-9.1	79	82	81	81	0.7	0.6	0.7	0.7	10	10	10	NE 3	ENE 2	SE 2
31	138.9	137.3	133.4	136.5	-14.6	-9.7	-12.2	-12.2	-6.3	-15.9	87	75	81	81	0.3	0.7	0.4	0.5	0	0	0	SSE 1	S 2	S 1
M	109.7	110.5	110.8	110.3	1.5	2.1	1.1	1.4	3.3	-1.0	84	80	83	82	1.1	1.5	1.1	1.2	8.5	8.5	8.0	6.3	6.8	5.7

Luty - Février

1	125.4	117.4	114.5	118.4	-13.4	-7.4	-8.7	-9.6	-6.6	-14.5	88	65	83	79	0.3	1.2	0.5	0.7	0	0	7	S 3	SSE 2	SSE 3
2	115.8	114.7	118.4	115.6	-11.1	-4.3	-2.2	-5.0	-2.1	-11.5	86	91	85	87	0.4	0.4	0.8	0.5	0	10 ⁂	10	S 2	S 2	SSW 2
3	122.3	123.5	122.2	122.7	-1.9	2.0	-1.2	-0.6	2.7	-5.0	90	76	85	84	0.5	1.7	0.8	1.0	10	9	5	SW 1	SW 1	SW 6
4	111.8	111.0	113.6	112.1	-0.7	2.2	2.2	1.5	3.4	-1.7	81	86	80	82	1.1	1.1	1.5	1.2	10	4	2	S 8	WSW 8	W 8
5	110.3	101.0	95.0	102.1	-0.1	0.3	2.1	1.1	2.6	-2.1	88	88	95	90	0.8	0.7	0.4	0.6	9	10 ⁂	9 ⁂	SSW 4	SSE 7	SW 8
6	100.9	108.9	115.1	108.3	1.3	1.8	1.3	1.4	2.7	0.7	91	76	81	83	0.6	1.7	1.3	1.2	10 ⁂	10	1	NW 10	NW 12	WNW 5
7	114.4	112.4	109.6	112.1	1.3	2.1	1.9	1.8	2.2	0.3	87	91	94	91	0.9	0.6	0.4	0.6	9	10	10	SSE 3	S 3	S 3
8	106.9	107.7	109.7	108.1	1.8	2.2	3.8	2.9	4.1	1.4	91	91	90	91	0.7	0.7	0.8	0.7	10	10	10	S 5	S 3	SW 3
9	114.1	121.0	126.9	120.7	2.0	2.0	-0.6	0.7	3.9	-1.5	85	85	85	85	1.1	1.1	0.8	1.0	9	9	0	WSW 4	N 7	W 2
10	126.9	124.7	121.6	124.4	0.8	2.9	3.1	2.5	3.7	-2.4	77	79	86	81	1.5	1.6	1.0	1.4	9	10 ●	10	SW 6	SSW 3	SW 8
11	114.8	114.9	117.0	115.6	3.1	4.3	3.0	3.4	4.4	2.2	88	68	72	76	0.9	2.7	2.1	1.9	10 ●	6	9	SW 5	W 9	W 8
12	98.7	78.1	69.5	82.1	1.4	3.0	4.0	3.1	5.2	0.0	70	91	67	76	2.1	0.7	2.6	1.8	10 ⁂	10 ●	9	SSW 12	SW 17	SW 17
13	74.8	78.4	81.9	78.4	1.0	1.2	-1.0	0.0	4.1	-1.6	75	59	67	67	1.7	2.8	1.9	2.1	10	1	1	W 17	WNW 11	WSW 9
14	87.6	91.9	100.3	93.3	-3.1	0.2	-1.8	-1.6	0.7	-3.5	86	85	90	87	0.7	1.0	0.5	0.7	3	7	5	SW 3	NE 5	NNE 8
15	107.7	111.9	114.9	111.5	-1.8	-1.3	-4.8	-3.2	-0.9	-5.3	83	84	71	79	0.9	0.9	1.2	1.0	5	8	8	N 12	N 13	W 5
16	93.5	77.8	73.3	81.5	-3.0	3.4	1.4	0.8	4.3	-7.1	88	86	92	89	0.6	1.1	0.6	0.8	10 ⁂	10 ●	10 ⁂	S 9	WSW 10	WSW 16
17	72.3	80.9	93.3	82.2	2.6	-0.4	-2.7	-0.8	3.3	-3.4	75	80	78	78	1.9	1.2	1.1	1.4	3	9 ⁂	10 ⁂	W 16	NW 17	NW 15
18	103.7	110.8	116.3	130.3	-3.7	-2.7	-2.3	-2.8	-1.6	-3.1	83	95	72	83	0.8	0.2	1.5	0.8	10 ⁂	9 ⁂	10	N 15	NNW 15	NW 4
19	114.2	112.8	111.7	112.9	-1.6	0.6	3.2	1.4	3.4	-3.4	86	82	88	85	0.7	1.1	0.9	0.9	10	10	10	WSW 3	S 3	NW 5
20	109.6	108.4	112.9	110.3	3.3	5.0	4.4	4.3	5.6	2.7	83	83	58	73	1.3	1.5	3.5	2.1	10	9	9	WNW 7	W 13	N 14
21	119.5	124.3	131.2	125.0	-0.5	-0.4	-1.3	-0.9	4.3	-1.6	84	78	84	82	1.0	1.3	0.9	1.1	10 ⁂	10	10	N 15	NNE 15	NNE 12
22	136.0	137.1	137.6	136.9	-3.1	-2.6	-1.3	-2.1	-1.1	-4.8	79	89	70	79	1.0	0.6	1.7	1.1	10 ⁂	10 ⁂	10 ⁂	NE 6	NE 6	NE 8
23	135.2	131.2	129.0	131.8	-0.4	0.9	0.5	0.4	1.4	-4.3	72	71	70	71	1.6	1.9	1.9	1.8	7	9	4	N 10	NNE 12	NNE 9
24	125.3	125.5	126.7	125.8	-2.0	-3.0	-3.4	-3.0	0.5	-4.3	81	77	72	77	1.0	1.1	1.3	1.1	10 ⁂	9	10	NE 9	ENE 9	ENE 9
25	128.3	130.2	129.7	129.4	-6.6	-4.9	-3.6	-4.7	-3.3	-8.1	80	64	92	79	0.7	1.5	0.4	0.9	10 ⁂	7	10 ⁂	E 7	SE 6	E 8
26	127.7	126.5	126.2	126.8	-1.9	-1.9	-2.4	-2.2	-1.5	-4.0	85	83	74	81	0.8	0.9	1.3	1.0	10	10 ⁂	10	ENE 8	ENE 7	ESE 2
27	124.6	123.5	122.1	123.4	-3.4	-2.3	-3.1	-3.0	-1.8	-3.8	81	76	77	78	0.9	1.3	1.1	1.1	10	9	6	ESE 1	NE 3	ESE 2
28	118.8	117.2	114.6	116.9	-8.8	-3.9	-3.7	-3.0	-3.1	-9.5	86	75	78	80	0.4	1.1	1.0	0.8	1	10	10	C 0	ENE 2	NE 3
29																								
30																								
31																								
M	112.0	111.6	112.7	112.1	-1.7	0.0	-0.3	-0.7	1.3	-3.6	83	80	80	81	1.0	1.2	1.2	1.1	8.0	8.4	7.7	7.2	7.9	7.2

Gdańsk - Wrzeszcz H_s=13m H_k=12,4 m h_w=15,5m Styczeń - Janvier 1962

DNI	WIDZIALNOŚĆ	OPAD	GRUBOŚĆ LODU	POGODA
1	8	0.6	11	•°2^35-3^50 ▽°14^40-15^10 •°15^40-18^21 ▽°18^40-20^30; ≫9^50-24 = 0^00-3^35
2	7	0.0	«	*11^40-12^45; ≫0^00-40
3	7	•	3	≫3^10-10^30; =16^40-24
4	7	•	3	≫20^40-24; = 0^00-3^30 14^15-20^40
5	6	0.0	pł.	≫0^00-20; = 7^40-14^35
6	6	0.7	pł.	•°5^35-7^40 •9^40 11^20-12^10 *°-16^35; ≫3^35-15^10
7	7	0.2	pł.	*°9^07-30
8	6	•	pł.	= 7^15-14^40
9	3	0.0	•	•'7^19-30 •-8^15 = 6^40-8^15 ≡°-8^45 = -24
10	6	•	•	= 0^00-2^40 7^40-24
11	6	•	•	= 0^00-3^30 12^15 -2^40
12	7	3.4		= 14^30-24
13	7	0.6	•	•°1^40-2^30 *°4^20 *°-6^35 •°-8^10 ▽°11^08-40; ≫12^20-24; = 0^00-7^30
14	7	0.0	•	•°8^05 13^10; ≫0^00-3^20
15	7	0.0	•	•°1^05-3^40 6^35-8^45
16	6	0.3	•	= 9^40-15^30
17	7	0.0	•	•°3^35-4^40 *°-7^45; = 15^20-24; ⊟ 20^40-24
18	6	0.0	•	•°18^35 ... 19^02; = 0^00-3^30 7^30-24; ⊟ 0^00-20
19	7	2.:	•	▽°-°21^45-24; = 0^00-11^10 15^35-21^45
20	8	3.3	•	▽°0^00-1^50 2^15-35 •°4^20-50 5^10-6^10 ▽°•°-9^20 ▽°9^35 10^15 15^10-16^15 19^15-40; ≫1^15-50 10^40-17^40
21	8	1.1	•	•°19^20-22^40 •23^05-35; ≫6°-12^15; ⊕12^15-14^10
22	6	0.2	•	•°0^45-2^05 14^40-15^50 ▽°16^30-50; ≫20^30-24; = 7^20-14^15
23	7	1.7	•	•°11^04 ... 12^10 ▽°18^14-23^15; ≫0^00-6^40 11^30-21^30
24	7	0.0	•	▽°0^45-3^20 9^20-45
25	3	3.3	•	•°16^10-17^35 *°-17^45 •°-22^40; = 1^40-23^40
26	8	0.9	•	*°6^35-7^15 ▽°9^10-10^05
27	7	2.0	1	*°-1 2^35-6^35 *°-7^25 •16^07-35 *'-17^10 •-1 ... 21^10 *°-21^30 ▽°-23^18
28	5	8.0	pł.	▽°-1 3^38 ... 11^50 ▽°-2 24; ≫3^30-8^20 ⊘-10^45 ≫-24
29	7	0.5	12	▽°-1 0^00-11^10 ▽°-1 16^45 ▽°17^20-18^40; ≫0^00-2^45; 4^10-12^40
30	7	0.0	16	▽°0^40-1^40; 9^45 ... 11^40; = 11^40-12^30; np
31	6	•	15	= 0^00-24
Σ	—	29.0	—	UWAGI.

Luty - Février

1	6	•	13	= 0^00-11^45 ∞ -15^40 = -24
2	6	0.0	11	*°-1 12^45-18^40; = 0^00-24
3	6	•	10	= 0^00-23^40
4	6	0.1	7	*'8^30-10^20; = 4^45-14^30
5	5	5.6	5	*°-1 12^15-19^35 *°-21^15 ▽°22^40-24; = 5^30-12^15
6	7	0.3	5	*°0^00-1^30 *'-9^20; ≫1^20-8^20 ⊘-10^45 ≫-14^35
7	6	0.0	4	•°14^40 ... 15^05; = 6^30-24
8	5	0.2	pł.	•°10^05-11^40 ▽°23^50-40; = 0^00-24
9	7	0.2	pł.	•°9^40-11^45; = 0^00-40 18^30 24
10	6	0.0	pł.	*°10^35 ... 12^10 •°12^35 ... 13^15; 19^07-20; ≫19^20-20^15; = na,n-24
11	7	0.1	pł.	•°5^30 8^40-10^20; ≫12^30-24; = 0^00-9^40
12	6	13.4	•	*°-1 6^40-11^40 *'-12^40 •°-1-17^45 ▽°21^48-24; ≫0^00-1^20 6^20-9^20 ⊘-24
13	8	0.1	3	▽°0^00-10 ▽°2 1^35-2^45 ▽'5^40-6^15 ▽°8^35-9^05 ▽°-1 9^15-10^06; ⊘ 0^00-9^40 ≫-15^10
14	7	1.5	4	▽°-2 12^20 ... 24
15	7	0.6	8	▽°0^00 ... 1^45; 6^10 ... 8^10 ▽°-1 13^18 ... 20^10; +'1^00-3^30 +°-6^40 +'-8^30; ≫0^15-16^30
16	6	5.4	9	*°-1 4^40-11^35 *°-12^15 •°-1-16^18 ▽°18^30-40 ▽°19^20-20^05 *°20^15-24; ≫ ⊘ 8^35-24
17	6	0.5	pł.	*°0^00-30 1^10-3^30 ▽'8^40-10^20 ▽°-1-18^50 ▽°19^35-24; ⊘ 0^00-24
18	7	3.3	6	▽°0^00-2^38 *°-1-7^05 ▽°-1 8^15-14^40 ▽°15^40-17^20; +°14^40-18^15; ⊘ 0^00-16^28 ≫-18^30
19	7	0.0	8	▽°13^40-20^20; = 13^15-20^45
20	7	0.1	pł.	•°10^20 12^10; ⊘-≫9^20-19^30 20^20-24
21	7	0.0	pł.	▽°4^05-15 4^40-9^05 *'-°9^15-12^20 *°13^05-14^40; ⊘ 0^00-16^40 ≫-22^30
22	6	0.1	pł.	*°6^40-7^35; 10^20-24; = 9^20-14^30
23	8	0.0	pł.	*°0^00-15; ≫4^40-20^40
24	7	0.2	pł.	*°5^15 ... 8^10-10^40 ▽°-1 14^05 ... 18^35
25	6	0.8	pł.	*°6^30 ... 9^35 *'19^08-21^05 *°23^40-24; ∞ 9^35-15^30 ∞ -19^08
26	5	0.0	4	*°0^00-2^38 12^45-13^40; = 6^30-15^40 17^45-24
27	7	0.0	3	*°8^40 ... 10^20; = 0^00-10^20
28	6	0.0	1	= 3^35-24
29				
30				
31				
Σ	—	32.5	—	UWAGI.

Gdańsk - Wrzeszcz φ = 54°23' λ = 18°36' Marzec - Mars 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	112.5	111.8	109.6	111.3	-4.7	-2.9	-4.2	-4.0	-1.8	-5.4	81	71	72	75	0.8	1.4	1.2	1.1	10	7	0	C 0	ENE 4	C 0
2	106.0	103.9	102.8	104.2	-10.7	-4.1	-5.4	-5.4	-2.7	-11.1	83	75	79	79	0.4	1.1	1.0	0.8	3	9	10 *	C 0	S 1	SSW 1
3	102.8	103.0	102.8	102.9	-4.3	0.0	-1.6	-1.9	0.8	-6.0	86	76	90	84	0.6	1.5	0.5	0.9	10	10 *	10	C 0	S 2	C 0
4	98.5	96.8	96.4	97.2	-1.6	1.5	0.3	0.1	1.9	-2.6	94	70	86	83	0.3	2.0	0.8	1.0	10	10	10	C 0	W 3	N 6
5	99.9	101.4	99.9	100.4	-0.7	-1.1	-2.2	-1.6	0.7	-2.2	83	81	89	84	1.0	1.1	0.6	0.9	10	10	10 *	NE 7	NE 7	NE 7
6	95.3	98.8	110.5	101.5	-1.2	-0.9	-2.2	-1.6	-0.6	-3.1	93	95	81	90	0.4	0.3	1.0	0.6	10 *	10 *	10	NNE 10	N 12	NW 5
7	118.3	120.9	123.8	121.0	-6.0	-0.2	-3.0	-3.0	0.5	-6.6	74	52	84	70	1.0	2.9	0.8	1.6	2	4	3	W 3	W 4	C 0
8	124.4	123.3	126.1	124.6	-2.0	1.9	-4.0	-2.2	2.5	-4.8	87	73	82	81	0.7	1.9	0.5	1.0	9	9	0	SW 1	W 9	WNW 3
9	127.3	126.2	121.3	124.9	-8.6	-1.5	-4.7	-4.9	-1.0	-9.5	86	76	88	83	0.4	1.4	0.5	0.8	3	3	6	C 0	SSE 3	SE 4
10	113.3	110.2	107.6	110.4	-2.1	2.4	0.4	0.3	2.8	-5.9	77	65	76	73	1.2	2.6	1.5	1.8	9	6	9	S 8	S 7	SSE 3
11	103.1	103.3	103.5	103.3	1.9	4.4	1.3	2.2	4.9	0.3	85	87	98	90	1.0	1.1	0.1	0.7	10	10	10 ●≡	S 1	SW 2	C 0
12	101.8	99.9	97.4	99.7	0.1	-0.6	-2.0	-1.1	1.4	-2.2	98	93	92	94	0.2	0.4	0.5	0.4	10 ●	10 *	10 *	NNE 5	NE 6	NNE 10
13	98.7	102.3	107.1	102.7	-3.6	-3.6	-5.5	-4.6	-1.7	-6.0	87	94	85	89	0.6	0.3	0.6	0.5	10 *	10 *	10 *	NNE 17	N 15	NW 7
14	110.6	113.4	116.6	113.5	-7.7	-1.9	-4.8	-4.8	-1.1	-9.7	67	63	62	64	1.1	2.0	1.6	1.6	2	6	0	W 7	W 9	WSW 5
15	117.9	118.8	122.5	119.7	-10.3	-0.8	-4.8	-5.2	-0.1	-13.2	84	65	71	73	0.4	2.0	1.2	1.2	4	3	10	SE 1	S 4	SSE 2
16	126.0	126.3	125.2	125.8	-9.3	-1.6	-4.4	-4.9	-1.2	-10.7	76	71	74	74	0.7	1.5	1.1	1.1	4	9	10	C 0	NNE 3	N 3
17	120.6	118.7	117.5	118.9	-0.7	-0.2	-0.5	-0.5	0.0	-5.2	75	63	70	69	1.4	2.2	1.8	1.8	10	8	7	NNE 8	NNE 9	NNE 9
18	116.5	118.1	118.9	117.8	-0.4	1.1	-4.8	-2.2	1.3	-4.9	70	66	74	70	1.7	2.2	1.1	1.7	5	3	1	NNE 9	N 9	NNW 3
19	119.0	118.6	118.1	118.6	-4.0	1.6	-1.8	-1.5	2.1	-9.1	84	58	81	74	0.7	2.9	1.0	1.5	7	6	9	W 2	SW 4	W 1
20	118.3	118.2	118.4	118.3	-6.1	2.4	-1.0	-1.4	3.2	-6.6	89	58	89	79	0.4	3.1	0.7	1.4	0	3	0	C 0	SSW 4	C 0
21	117.7	116.4	115.4	116.5	-6.5	1.7	-0.8	-1.6	2.1	-7.1	97	67	71	78	0.1	2.3	1.7	1.4	6 ≡	4	9	C 0	SSE 4	S 3
22	113.9	113.1	111.2	112.7	-6.5	0.1	-4.2	-3.7	0.8	-8.1	78	58	79	72	0.8	2.6	0.9	1.4	0	0	0	SSE 1	SSE 3	C 0
23	110.4	111.6	112.7	111.6	-7.3	-1.0	-1.8	-3.0	-0.3	-8.3	88	65	67	73	0.4	2.0	1.8	1.4	0	1	0	C 0	NE 4	NE 3
24	114.3	116.4	118.8	116.5	-1.3	0.1	-3.0	-1.8	0.3	-6.9	70	61	77	69	1.7	2.5	1.1	1.8	9	5	0	NE 5	NNE 5	N 1
25	120.0	119.9	118.2	119.4	-4.3	2.4	-1.3	-1.1	3.4	-5.4	84	54	83	74	0.7	3.3	1.0	1.7	4	3	0	SW 1	SW 3	C 0
26	115.9	114.7	112.7	114.4	0.4	5.3	0.6	1.7	5.5	-4.5	72	41	67	60	1.8	5.2	2.1	3.0	7	3	0	C 0	S 5	S 4
27	109.3	107.2	105.3	107.3	-3.1	2.3	-0.5	-0.4	2.9	-3.9	84	52	58	65	0.8	3.4	2.5	2.2	7	9	10	SSE 2	S 8	SSE 5
28	101.4	100.9	102.3	101.5	-2.5	-0.8	-0.6	-1.1	0.1	-3.0	67	87	95	83	1.7	0.7	0.3	0.9	10	10	10 *	SE 4	SSE 2	C 0
29	104.3	104.4	102.1	103.6	0.1	1.1	0.4	0.5	2.0	-3.7	90	81	82	84	0.7	1.2	1.1	1.0	10	10	0	NNE 2	C 0	SSE 1
30	95.3	93.7	91.8	93.6	0.6	1.4	3.2	2.1	3.3	-1.2	88	98	100	95	0.8	0.2	0.0	0.3	10 ●	10 ●	10	SE 3	SE 3	SSE 3
31	83.8	82.3	92.5	86.2	3.1	6.6	4.2	4.5	7.6	1.3	100	97	66	88	0.0	0.3	2.8	1.0	10 ●	10 ●	0	SSE 3	S 3	SW 3
M	110.2	110.1	110.6	110.3	-3.5	0.5	-1.8	-1.6	1.3	-5.7	83	71	80	78	0.8	1.9	1.1	1.3	6.8	6.8	5.6	3.2	5.1	3.0

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1	98.6	101.4	102.4	100.8	1.8	5.9	1.9	2.9	7.8	0.3	78	65	91	78	1.6	3.2	0.6	1.8	2	9	3	SW 2	S 3	S 3
2	102.3	102.8	106.3	103.8	2.1	7.5	3.9	4.4	7.9	1.1	82	57	75	71	1.3	4.5	2.0	2.6	6	6	0	SW 5	SW 10	SW 7
3	105.0	103.2	100.4	102.9	3.8	9.9	7.5	7.2	13.2	1.9	87	64	72	74	1.1	4.3	3.0	2.8	10	10	1	SSW 7	S 8	SSE 3
4	96.2	96.0	93.0	95.1	5.8	11.6	8.3	8.5	12.1	4.2	73	60	78	70	2.5	5.4	2.5	3.5	9	9	10	SSE 4	SSE 3	C 0
5	89.1	86.6	86.8	87.5	5.1	4.4	5.9	5.3	8.4	3.5	97	98	95	97	0.3	0.2	0.5	0.3	10 ●	10 ●	10	C 0	N 1	C 0
6	91.2	96.1	102.3	96.5	3.2	6.5	2.0	3.4	7.8	1.5	95	81	100	92	0.4	1.9	0.0	0.8	10	9	10 ≡	SW 2	E 2	C 0
7	106.2	106.9	104.4	105.8	1.8	7.0	3.5	4.0	7.6	1.1	89	49	68	69	0.8	5.1	2.5	2.8	3	6	2	WNW 5	NW 10	SSW 1
8	98.4	99.9	100.3	99.5	5.8	8.4	9.0	8.0	10.3	1.9	83	87	85	87	1.1	1.4	1.7	1.4	9	10 ●	10 ●	SW 5	SW 3	S 3
9	105.3	107.7	113.0	108.0	6.9	10.3	5.3	7.0	11.9	5.0	72	48	72	64	2.7	6.4	2.5	3.9	3	9	2	SSW 7	SW 9	C 0
10	115.8	118.2	121.1	118.4	4.9	8.6	2.4	4.6	10.0	1.2	81	51	93	75	1.7	5.5	0.6	2.6	0	9	4	WSW 3	SW 7	C 0
11	122.1	121.5	120.3	121.3	3.9	12.1	7.0	7.5	13.4	0.6	77	38	71	62	1.9	8.7	2.9	4.5	5	6	1	C 0	S 3	C 0
12	117.2	114.6	114.3	115.4	7.4	15.7	5.1	8.3	16.5	4.8	61	29	95	62	4.0	12.6	0.4	5.7	2	7	10 ●	SW 3	SW 7	C 0
13	113.6	113.6	114.7	114.0	5.2	7.5	4.4	5.4	9.5	3.7	80	65	82	76	1.8	3.7	1.5	2.3	9	9	10	WSW 3	NE 4	NE 2
14	116.0	119.8	129.5	120.4	3.1	2.9	2.9	3.0	4.8	1.9	88	93	93	91	0.9	0.5	0.5	0.6	10	10 ●	10	W 7	N 9	NNE 8
15	128.1	128.5	128.9	128.5	3.4	3.7	5.3	4.4	5.3	2.3	86	90	89	88	1.1	0.8	1.0	1.0	10	10	10	NNE 9	NE 7	NE 4
16	127.3	125.8	123.2	125.4	5.3	6.3	5.9	5.8	8.4	4.2	95	92	95	94	0.4	0.7	0.5	0.5	10	10	1	NE 4	NE 7	N 2
17	122.4	120.8	118.2	120.5	6.1	20.4	15.7	14.5	22.0	3.5	98	44	65	69	0.1	13.5	6.2	6.6	1	10	10	C 0	SE 7	SSE 4
18	115.8	113.5	112.9	114.1	11.9	20.1	13.1	14.6	21.1	10.7	80	45	76	67	2.8	12.9	3.6	6.4	9	9	9	SSE 2	S 6	C 0
19	112.7	112.7	114.5	113.3	12.5	20.7	10.0	13.3	21.8	9.8	77	47	87	70	3.4	12.8	1.6	5.9	10	10	9	C 0	S 4	NE 1
20	116.7	118.0	118.1	117.6	8.2	12.7	7.9	9.2	14.6	6.7	94	77	93	88	0.6	3.4	0.7	1.6	10	6	9	NE 3	NNE 5	N 2
21	117.1	116.2	118.8	117.4	9.7	20.4	13.9	14.5	25.1	6.9	92	62	76	77	0.9	9.1	3.9	4.6	6	7	7	C 0	NNE 3	NW 3
22	121.1	121.4	120.6	121.0	8.5	9.5	7.3	8.2	13.9	7.0	97	92	99	96	0.3	1.0	0.1	0.5	10 ≡	10	10 ≡	NNE 1	NE 3	C 0
23	118.7	120.1	123.7	120.8	10.6	12.2	6.3	8.8	18.8	5.3	95	78	95	89	0.7	3.2	0.4	1.4	2	1	9	SE 2	NE 5	N 6
24	127.2	128.3	128.1	127.9	6.6	8.9	7.1	7.4	10.0	3.6	88	81	83	84	1.1	2.2	1.8	1.7	3	0	1	NE 5	NNE 7	N 3
25	128.4	127.1	123.6	126.4	10.5	19.3	15.1	15.0	20.4	6.3	85	52	66	68	1.9	10.8	5.8	6.2	1	1	0	C 0	E 5	C 0
26	119.8	116.8	112.0	116.2	14.3	17.7	11.5	13.8	19.6	11.4	79	53	60	64	3.4	9.5	5.5	6.1	9	0	3	C 0	NW 7	WSW 5
27	107.4	108.7	105.2	107.1	8.3	6.3	8.0	7.6	11.5	4.6	79	89	74	81	2.3	1.0	2.8	2.0	10	10 ●	10	NE 5	N 8	NE 2
28	100.6	102.1	104.4	102.4	5.3	6.5	4.4	5.2	9.4	3.4	89	85	92	89	1.0	1.5	0.7	1.1	7	9	10 ●	N 5	N 12	NNE 5
29	105.3	105.9	107.5	106.2	5.2	5.8	2.8	4.2	7.4	1.7	70	67	76	71	2.6	3.0	1.9	2.5	9	4	9	N 7	N 9	NE 7
30	108.9	111.3	113.6	111.3	1.6	1.4	-0.4	0.6	4.1	-0.7	72	85	90	82	1.9	1.0	0.6	1.2	10	9 *	5	N 8	NNE 9	NW 3
31																								
M	111.8	112.2	112.6	112.2	6.3	10.3	6.8	7.6	12.3	4.0	84	67	83	78	1.6	5.0	1.9	2.8	6.8	7.3	6.5	3.5	6.1	2.3

Gdańsk - Wrzeszcz $H_s = 13m$ $H_t = 12{,}4m$ $h_w = 15{,}5m$ Marzec - Mars 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	7	.	1	*°0^35...2^35;=0^00-9^40;18^20-24
2	5	0.0	pł.	*°20^40...22^40;=0^00-24
3	6	0.4	pł.	*°12^10-13^00;21^30-23^35;=0^00-10^45∞-12^45=-24
4	6	.	2	*°0^35-3^40;=0^00-24
5	6	3.0	pł.	*°16^42...21^35*-24;=0^00-16^45
6	4	5.2	3	*°-2 0^00-18^20*°21^20-23^35;≫5^15-17^20
7	8	0.0	18	⚧°17^05-19^10
8	7	0.0	17	⚧°14^25-15^05
9	6	.	14	=6^10-24
10	7	0.6	5	•°23^35-24;=0^00-5^40
11	6	3.3	4	•°0^00-2^25;7^15...10^50;16^20-22^40•°-24;=5^35-19^15≡°-22^25=-24
12	6	8.3	pł.	•°0^00-7^20•°-8^40*°-13^40*°-2 14^05-24;↓-2 20^40-24;≫-≫20^40-24;=0^00-13^40
13	4	3.3	30	*'0^00-5^35*2-0 6^45-12^30*'12^40-14^35⚧'19^20-35;20^10-21^30;22^40-23^10;↓2 0^00-15^40↓2 15^40-18^25;≫-≫0^00-17^35
14	8	.	35	⚧'-0 0^18-2^20⚧'2^35-4^25
15	6	.	24	=5^30-10^30∞-21^30;⊖22^35-24
16	6	.	22	∞5^15-6^30=-24;⊖0^00-3^40
17	8	.	20	=0^00-2^50
18	8	0.0	18	
19	7	0.0	14	⚧°5^45-6^40;16^07-20;=19^40-23^15
20	8	0.0	10	⚧'16^35-58;=6^30-9^30;19^35-24
21	6	.	7	=0^00-6^15≡°-7^25=-12^40∞-19^45;⊖2^30-5^30
22	7	.	6	=5^30-11^40;20^40-24
23	7	.	5	=0^00-8^40;⊔0-1 2-8
24	7	.	5	
25	7	.	5	=20^40-24
26	7	.	3	=0^00-2^30-6^40-8^40∞16^45-18^50=-20^30
27	7	.	pł.	=4^30-8^40
28	5	2.1	pł.	*-0 9^05-10^20;14^40-17^10*°18^40-20^15;20^40-22^10;=10^20-24
29	6	0.0	4	=0^00-24
30	4	2.7	pł.	•°6^08...7^05*°-1-10^20•°-11^35•°-13^20;=0^00-13^20≡°-2-20^20=-22^30='-24
31	5	0.8	pł.	•-0 6^10-9^35•°-11^10•°-13^20⚧°13^40-14^15;≫13^45-16^50;≡0^00-3^20=-6^10
Σ	—	29.7	—	UWAGI

Kwiecień - Avril

1	7	0.0	pł.	⚧°17^03-30
2	8	1.0	pł.	⚧°0^15-40⚧'13^40-14^05;≫12^40-14^15
3	7	0.0	.	•°7^35-9^15
4	7	0.4	.	•°22^30-24
5	4	12.4	.	•°0^00-1^00...1^40•0-1 5^15-13^40 13^50...18^20;=5^15-19^05≡'-2-19^25=-24
6	7	.	.	=0^00-6^35;18^40-20^17≡'-0-24;⊕15^30-17^20
7	8	0.0	.	≫10^20-13^40;≡°0^00-15=-0^45
8	6	0.4	.	≡°3^20-5^15⚧°7^05-20•°11^35...14^40 20^38...22^40;23^05-24;=14^40-20^38
9	8	0.3	.	•°0^00-2^10⚧°15^12-30;16^17-17^10;=4^25-6^15
10	8	.	.	=18^40-24;⊔°2-7
11	7	.	.	=0^00-3^35;4^45-7^40∞18^30-20^40=-21^45;⊔°0^00-7
12	8	2.9	.	•°-1 17^05...18^35-24
13	7	0.1	.	•°0^00-2^40;14^20-17^05;=2^40-4^15;⊕°7^30-9^10
14	7	0.0	.	•°7^32...8^40-10^10...20^40
15	7	.	.	
16	6	.	.	=4^40-24
17	7	.	.	=0^00-3^15≡°-6^40=-9^40;⊕°11^20-15^15
18	7	.	.	=4^40-9^20 17^40-24
19	7	.	.	=0^00-9^40∞-12^35;16^45-18^30=-24
20	6	.	.	=0^00-24;⌓°2-8
21	6	.	.	=0^00-9^10∞-13^40=18^15-24
22	6	.	.	=0^00-6^30≡°-7^15=-15^20≡°-1-24
23	7	.	.	≡'0^00-40=-9^40∞-12^10=20^35-24
24	7	.	.	=0^00-6^10 8^40-10^10;⌓°1-8
25	7	0.0	.	=3^35-8^40∞19^15-21^40=-24
26	8	.	.	⚧°5^20-30=0^00-40
27	6	3.6	.	•°-1 7^40-9^40•°-11^30...13^20;=7^15-11^30
28	8	3.0	.	⚧°6^05-45;11^45-12^03•°16^07-18^10;18^35...19^30•'-0-21^40;≫10^15-16^35
29	8	.	.	
30	8	1.0	.	⚥°10^15...11^40⚧°12^25...14^35⚥°14^45-15^05⚧°15^15...17^10
31				
Σ	—	25.1	—	UWAGI

Gdańsk - Wrzeszcz φ = 54°23' λ = 18°36' Maj - Mai 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	109.4	106.3	105.0	106.9	2.0	5.2	1.5	2.4	6.5	-1.1	76	57	72	68	1.7	5.8	1.9	2.5	10	7	2	WSW 1	NNE 8	NNW 2
2	102.5	104.0	106.6	104.4	1.4	3.9	5.7	3.2	4.7	0.4	92	87	80	86	0.6	1.1	1.6	1.1	9	10●	10	NW 4	N 7	W 3
3	106.7	106.1	105.7	106.2	3.4	7.7	5.8	4.7	9.0	2.1	85	53	92	77	1.2	4.9	0.7	2.3	7	7	9	C 0	SSW 4	N 2
4	105.6	104.7	107.1	105.1	3.5	7.0	3.5	4.4	7.8	1.2	100	77	86	88	0.0	2.3	1.0	1.1	10≡	7	5	N 2	NNE 7	N 3
5	109.7	112.8	115.5	112.7	4.7	6.3	5.2	4.4	6.8	1.8	73	73	90	79	2.3	2.5	0.8	1.9	7	8	0	W 4	NE 5	C 0
6	118.1	117.7	115.8	117.2	7.6	14.0	10.2	10.5	15.2	1.3	66	31	48	48	3.5	11.1	6.4	7.0	0	6	3	SSW 5	SSE 4	SSE 2
7	111.7	111.4	111.7	111.6	7.8	11.6	12.9	11.3	14.2	6.1	85	90	93	89	1.8	1.3	1.1	1.4	10●	9	10	SSE 4	S 3	SSE 2
8	110.1	110.4	110.3	110.3	10.4	15.2	8.5	10.6	16.3	8.4	100	78	94	91	0.0	3.9	0.6	1.5	10≡	9	10	C 0	ENE 2	C 0
9	111.0	111.9	111.5	111.5	8.3	13.2	7.4	9.1	13.6	6.7	93	75	99	89	0.8	3.8	0.2	1.6	10	9	0≡	NE 2	NE 1	C 0
10	107.6	106.7	108.4	107.6	7.6	12.4	9.4	9.6	15.6	5.2	99	96	93	96	0.1	0.5	0.8	0.5	10≡	10●	9	C 0	SSE 2	C 0
11	109.1	110.4	111.0	110.2	10.1	10.4	7.7	9.0	13.3	7.4	85	87	96	89	2.0	1.6	0.5	1.4	9	7	3	WSW 3	NE 4	C 0
12	112.8	114.3	116.3	114.5	8.4	8.4	6.5	7.4	9.3	6.3	99	92	99	97	0.1	0.9	0.2	0.4	10≡	10	10	NE 2	NE 4	NE 3
13	116.4	115.7	112.6	114.9	7.2	10.3	10.1	9.4	10.7	5.9	100	91	99	97	0.0	1.1	0.2	0.4	10≡	9(R)	2	N 2	NE 4	C 0
14	108.2	103.7	97.5	103.1	9.8	10.1	9.2	9.6	10.5	5.7	99	100	97	99	0.1	0.0	0.3	0.1	10≡	10●	10●	N 4	N 6	NNE12
15	95.1	98.9	102.3	98.8	7.7	7.5	7.7	7.6	9.4	7.0	100	94	87	94	0.0	0.6	1.3	0.6	10●	10●	10●	N 17	NNW15	NNW 9
16	104.7	108.2	110.4	107.8	7.7	11.3	7.5	8.5	12.1	5.5	84	64	68	72	1.6	4.8	3.4	3.3	9	9	1	NW 8	W 9	SW 4
17	108.9	108.5	107.6	108.3	8.1	12.5	6.8	8.6	14.3	3.9	81	71	94	82	2.1	4.2	0.6	2.3	10	4	10●	SW 2	SW 3	N 2
18	110.6	112.9	115.2	112.9	9.2	10.0	10.0	9.8	13.8	5.7	84	71	71	75	1.8	3.6	3.6	3.0	9	9●	1	NW 5	SW 3	SW 3
19	115.6	112.7	107.8	112.0	12.5	18.8	15.4	15.5	19.3	7.8	60	40	60	53	5.8	13.1	7.0	8.6	0	4	9	C 0	SSE 7	SSE 4
20	105.4	109.0	111.2	108.5	10.7	11.9	10.5	10.9	15.4	9.6	96	82	94	91	0.5	2.5	0.8	1.3	10●	10●	9	S 3	W 5	C 0
21	113.9	114.8	114.1	114.3	9.6	11.4	9.4	10.0	13.2	5.6	79	76	78	78	2.6	3.3	2.6	2.8	7	5	7	W 4	NE 5	ENE 2
22	110.7	109.2	109.8	109.9	11.0	16.2	12.6	13.1	16.8	6.2	71	57	67	65	3.8	7.9	4.9	5.5	9	10	10	SSE 1	SSE 5	SW 3
23	112.2	111.0	112.6	111.9	12.2	17.4	10.3	12.6	18.2	10.2	83	51	83	72	2.4	9.8	2.1	4.8	9	9	10●	S 4	SW 8	WNW 2
24	114.3	114.3	113.7	114.1	10.8	15.6	13.2	13.2	17.1	8.3	68	39	59	55	4.2	10.8	6.3	7.1	2	8	5	SW 5	SW 6	S 4
25	113.4	113.8	115.2	114.1	11.4	13.2	9.6	11.0	13.8	6.5	66	56	74	65	4.6	6.8	3.2	4.9	1	3	10	NE 3	NE 5	N 2
26	114.3	113.7	111.2	113.1	9.8	10.4	9.6	9.8	11.8	6.4	92	91	99	94	0.9	1.1	0.2	0.7	10	10	10●	N 5	NNE 6	NE 7
27	111.4	113.9	115.6	113.6	12.5	14.6	10.9	12.2	15.3	9.4	83	62	89	78	2.4	6.3	1.4	3.4	7	9	10	S 4	SW 5	NNE 2
28	116.9	116.0	113.4	115.4	11.0	13.5	10.3	11.3	14.5	7.8	79	67	73	73	2.7	5.2	3.3	3.7	7	7	9	S 2	NE 5	NE 5
29	111.3	113.1	114.0	112.8	10.1	13.5	9.3	10.6	14.4	8.2	93	66	85	81	0.8	5.3	1.7	2.6	10●	9	2	SE 2	WSW 3	SW 2
30	113.6	112.8	114.8	113.7	11.5	15.3	8.9	11.2	17.8	6.0	77	54	62	64	3.2	8.0	4.4	5.2	1	7	6	SW 4	WNW 8	WSW 3
31	113.5	110.3	107.8	110.5	9.7	14.1	8.1	10.0	14.8	7.2	72	50	85	69	3.4	8.0	1.6	4.3	7	10	3	W 3	S 4	SW 3
M	110.4	110.6	110.7	110.6	8.6	11.7	8.6	9.4	13.1	5.8	84	70	83	79	1.8	4.5	2.1	2.8	7.7	8.1	6.6	3.4	5.3	2.8

Czerwiec - Juin

1	107.5	113.0	114.9	111.8	7.5	10.9	7.8	8.5	13.0	4.9	76	54	83	71	2.5	5.9	1.8	3.4	5	9	4	WSW 8	WNW 7	C 0
2	115.2	117.1	120.3	117.5	7.3	10.2	6.6	7.7	11.0	3.6	84	77	93	85	1.6	2.8	0.7	1.7	10●	9	4	C 0	E 2	C 0
3	125.1	124.2	125.3	124.2	8.6	10.4	6.9	8.2	10.9	3.4	81	54	82	72	2.2	5.7	1.7	3.2	6	6	3	NE 5	NNE 4	NNW 3
4	125.8	126.1	125.4	125.8	8.3	11.5	9.1	9.5	14.1	5.1	62	38	70	57	4.2	8.5	3.6	5.4	9	5	8	NNE 8	N 9	N 9
5	125.4	126.7	127.4	126.5	9.1	10.2	8.1	8.9	11.6	6.9	70	70	70	70	3.6	3.7	3.3	3.5	7	6	3	N 9	N 12	NNE 8
6	129.0	130.2	129.2	129.3	8.8	10.7	8.2	9.0	11.2	7.0	69	63	73	68	3.5	4.8	3.0	3.8	2	0	0	NNE 9	NNE 9	N 7
7	130.4	131.0	129.6	130.3	9.9	12.9	9.1	10.2	13.5	6.2	76	50	68	65	3.0	7.5	3.7	4.7	8	1	0	NE 7	NNE 8	N 3
8	128.2	125.8	120.3	124.8	13.4	17.5	15.4	15.4	20.9	5.4	42	43	32	39	9.0	11.4	11.9	10.8	0	7	3	N 4	ENE 4	WSW 6
9	114.5	114.9	114.8	114.7	14.7	13.6	9.9	12.0	18.5	9.8	76	81	79	79	4.0	3.0	2.5	3.2	9	7	2	W 9	NNE 9	C 0
10	112.5	110.2	108.5	110.4	12.6	19.5	13.6	14.8	21.2	7.0	53	44	71	56	6.9	12.7	4.5	8.0	7	7	4	SW 3	SW 3	C 0
11	105.0	104.0	105.4	104.8	14.1	15.4	10.9	12.8	18.9	10.8	62	81	68	70	6.1	3.4	4.1	4.5	2	9	6	C 0	W 5	WSW 4
12	106.5	109.7	112.4	109.5	11.6	12.5	11.3	11.7	14.4	9.6	84	80	70	78	2.1	2.9	4.1	3.0	9	5	5	NW 6	NE 8	WNW 1
13	113.7	115.1	115.5	114.8	13.1	15.9	12.7	13.6	18.2	8.4	67	56	80	68	5.0	8.0	2.9	5.3	1	4	9	W 6	NE 6	C 0
14	113.0	111.8	112.3	112.4	15.6	22.8	16.1	17.6	24.2	9.1	63	36	68	56	6.5	17.6	5.8	10.0	6	5	10	S 3	S 7	N 1
15	116.1	117.0	116.8	116.6	18.8	25.0	20.1	21.0	28.0	13.3	60	44	67	57	8.6	17.7	7.8	11.4	3	2	6	NW 4	S 4	C 0
16	118.2	116.4	116.7	117.1	19.7	26.3	16.5	19.8	27.3	16.4	77	54	89	73	5.3	15.8	2.2	7.8	7	4	10●R	C 0	E 4	C 0
17	117.4	119.7	120.3	119.1	16.2	17.4	13.3	15.0	20.3	13.1	78	67	73	73	4.0	6.6	4.2	4.9	3	9	3	WNW 7	WNW 6	W 2
18	120.0	119.2	117.8	119.0	15.1	19.6	14.4	15.9	21.0	9.9	68	48	78	65	5.5	11.8	3.6	7.0	1	2	3	W 3	N 3	C 0
19	115.8	113.1	108.8	112.6	16.3	25.2	20.9	20.9	26.0	10.6	70	44	59	58	5.7	17.9	10.2	11.3	8	4	8	SSE 2	SSE 6	SSE 5
20	112.4	114.5	114.5	113.8	15.7	17.9	14.3	15.6	21.3	13.9	82	73	87	81	3.2	5.6	2.2	3.7	9	7	8	NW 5	SE 3	NNE 2
21	115.1	116.5	118.0	116.3	17.6	17.9	16.3	17.0	20.4	12.3	57	63	68	63	8.6	7.6	6.0	7.4	6	10	9	SW 5	W 8	W 3
22	120.4	119.6	118.9	119.6	17.3	23.3	19.2	19.8	24.6	12.1	66	49	76	64	6.7	14.4	5.2	8.8	9	9	9	SW 3	SSW 6	S 1
23	118.0	118.8	117.7	118.2	16.4	16.7	15.3	15.9	19.7	15.1	93	78	73	82	1.3	4.2	4.4	3.3	10	10	3	N 1	NE 2	S 2
24	116.3	114.9	111.8	114.4	16.8	21.8	16.5	17.9	22.4	12.9	71	42	69	61	5.3	15.0	5.9	8.8	2	7	10	W 5	W 6	NNE 1
25	110.1	111.0	112.9	111.3	15.3	15.2	13.0	14.1	17.3	12.8	54	62	60	59	8.0	6.5	6.1	6.9	1	10●	2	SW 8	WSW10	WSW 7
26	112.3	112.8	110.8	112.0	12.4	15.7	12.6	13.3	17.2	9.6	62	55	88	68	5.5	8.1	1.7	5.1	8	6	10	WSW 7	WNW 7	C 0
27	105.4	105.2	105.3	105.4	10.8	14.3	10.3	11.5	15.6	9.0	95	63	88	82	0.7	6.2	1.4	2.8	10●	9	10	C 0	SW 9	W 6
28	105.1	104.9	102.6	104.2	10.8	12.7	10.4	11.1	13.2	9.7	84	62	85	77	2.2	5.5	1.9	3.2	9	9	9	W 7	SW 8	S 1
29	102.3	103.8	104.3	103.3	12.3	11.7	12.1	12.0	14.4	9.2	73	89	94	85	3.9	1.3	0.8	2.1	8	10●	10●	W 7	NW 7	NW 5
30	107.8	109.3	111.6	109.6	12.3	14.6	13.1	13.3	18.9	9.6	80	78	79	79	2.9	3.6	3.1	3.2	6	8	2	NW 5	NE 5	W 7
31																								
M	115.4	115.9	115.7	115.7	13.3	16.3	12.8	13.8	18.3	9.6	71	60	75	69	4.6	8.2	4.0	5.6	6.0	6.5	5.8	4.9	6.3	2.8

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ LODU h	POGODA
1	8	0.0	•	⚲°7^30-40
2	7	0.7	•	⚲'6^40-45 ⚹°8^20-9^40 •°...15^10
3	8	0.4	•	⚲°10^20...19^05; =21^15-24
4	8	•	•	=0^00-5^15 ≡°-7^35 =-8^25; 19^40-24
5	8	•	•	=0^00-1^40; 21^40-24
6	8	0.1	•	=0^00-2^30; ⊔'3-6
7	6	9.2	•	•°5^35...7^30-10^20; 15^05-40; =10^20-24
8	7	0.3	•	•°-2^15-5^15; =0^00-5^20 ≡°-1-8^35 =-11^40; 17^15-23^40 ≡'-24
9	6	•	•	•°0^40-3^40; ≡'0^00-40 =-19^45 ≡°-1-21^35 =-24
10	5	6.1	•	•°9^35...11^05 •'-14^05 ⚲°15^40-16^10; 22^20-35; 23^50-24; =0^00-2^15 ≡°-1-7^20 =-9^35; np; ⌂°na
11	7	0.0	•	⚲°0^00-05...10^15-25; =17^40-24
12	5	4.9	•	•°13^40-14^15 •℞°14^15-40 W-NE ⚲°-15^10; =0^00-6^15 ≡°-8^45 =-18^05 ≡°-1-20^40 =-np ≡'-°-24; ⌂°na
13	6	0.3	•	•°13^35-15^05 ⚲°15^40-16^15; 17^15-25; (℞)12^45-13^10 SE-NE; ≡°na =na ≡°-1 3^35-7^45 =-15^15; n-np ≡'-24
14	5	29.7	•	•°-1 8^10-24; ⚲-⚲ 20^05-24; ≡'-2 0^00-1^35 =-3^40 ≡°-1-9^35
15	6	12.4	•	•°-1 0^00-14^20...23^45; ⚲-⚲ 0^00-14^10
16	7	•	•	
17	7	9.4	•	•°9^45-11^10 ⚲°-1 18^40-20^05 •°20^15-22^10
18	7	0.0	•	⚲°12^18-13^05
19	7	4.2	•	
20	7	1.7	•	•°4^40...5^30 •'-6^20 •°-13^35; =20^40-21^45
21	8	•	•	
22	7	0.1	•	•°16^27...17^25; =4^30-8^35
23	7	0.8	•	•°20^10...24; =5^30-8^40
24	8	•	•	•°0^00...1^00-2^45
25	8	•	•	
26	7	10.0	•	•°-1 4^10-24; =3^35-12^30
27	8	•	•	•°0^00-2^10; =2^10-5^15
28	8	5.6	•	•°23^15-45 ⚲'-24; =3^40-7^10; ⌂2-8
29	8	0.0	•	⚲'0^00-1^35 ⚲°-3^35 •°6^40-8^40; =5^15-10^30
30	8	0.3	•	⚲°14^40-15^05; 15^25-40; 16^20-35
31	8	1.0	•	⚲'1^45-2^05 ⚲°-1 15^50...19^25
Σ	—	97.2	—	UWAGI

Czerwiec - Juin

1	8	0.0	•	⚲°6^05-20; 9^15-35; ∩'6^05-10
2	7	4.9	•	⚲°4^45-5^10 •°7^35...11^30; 12^45 ⚲°-1 14^15-15^15; 18^20-19^20; =21^20-24
3	8	0.3	•	⚲°9^37-50; =0^00-3^35
4	8	•	•	•°2^42...3^05 •'-3^15 •°4^40...6^25; ⊕°14^25-15^05
5	8	•	•	⚲12^15-21^15
6	8	•	•	
7	8	•	•	
8	8	•	•	
9	7	•	•	
10	8	•	•	
11	7	5.8	•	⚲°-1 12^03-13^25 ⚲°15^46-16^30; (℞) SW 11^45-℞'12^10-13^10-N
12	8	0.1	•	⚲°3^18-30; 15^50-16^05; 16^10-20
13	8	•	•	
14	7	0.0	•	⚲°17^47-18^03; =21^45-24
15	7	0.1	•	⚲°23^05-30; =0^00-1^30; 20^40-24
16	7	15.3	•	(℞) NW 14^45-•℞°16^50-17^30 SE ⚲°-17^35 (℞) W 20^35-•℞°20^45-23^40 SE ⚲'-24; =0^00-3^40
17	7	•	•	⚲'0^00-1^10 •°1^45...2^45; =1^10-7^15
18	8	•	•	
19	7	2.4	•	
20	8	0.0	•	•℞°0^15-1^12 SW-W ⚲°-2^40; 5^10-6^40; 17^50-18^05
21	7	0.0	•	⚲°10^15-35
22	8	0.2	•	=20^20-24
23	7	1.2	•	•°5^40-7^35; 8^35...9^40; =0^00-9^30
24	8	•	•	
25	7	0.3	•	⚲°13^32-14^45; 17^12-23; 19^08-20; ⚲10^30-14^35; 16^40-20^35
26	8	4.9	•	•°17^35-19^18
27	8	2.3	•	•°-1 5^10-8^30; 8^40...9^10 ⚲°12^40-50; 16^30...21^38; =3^48-9^50; ⌂na
28	8	0.0	•	⚲°5^22...7^10; 10^20-35
29	7	11.3	•	⚲°-1 10^25-22^40
30	8	•	•	
31				
Σ	—	47.1	-	UWAGI

Gdańsk-Wrzeszcz φ=54°23' λ=18°36' Lipiec-Juillet 1962

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D.v I	II	III
1	111.7	112.4	111.8	112.0	12.0	16.7	14.1	14.2	18.7	9.9	79	54	70	68	3.0	8.7	4.8	5.5	7	8	4	WSW 6	WSW 5	WNW 2
2	109.3	108.1	103.7	107.0	14.0	17.1	13.3	14.4	17.8	10.6	81	56	84	74	3.0	8.5	2.5	4.7	7	6	10●	W 5	SW 8	SW 5
3	98.1	96.8	96.3	97.1	11.2	10.7	10.0	10.5	14.5	9.3	85	89	82	85	2.0	1.5	2.2	1.9	9	9	5	S 4	NW 2	C 0
4	95.0	94.7	95.8	95.2	9.7	10.1	10.4	10.2	12.3	7.8	78	87	90	85	2.6	1.6	1.3	1.8	9	10●	7	S 3	S 6	SSW 4
5	100.2	101.9	105.3	102.5	10.8	15.5	12.0	12.6	17.6	7.4	80	58	86	75	2.6	7.4	2.0	4.0	7	9	7	SSW 7	SW 8	SSW 4
6	107.4	109.5	111.8	109.6	12.3	17.5	12.9	13.9	18.4	9.9	85	53	75	71	2.2	9.3	3.8	5.1	9	9	5	SSW 7	SW 9	SSW 2
7	111.9	112.0	113.3	112.4	12.2	14.9	12.7	13.1	17.8	9.0	82	73	85	80	2.5	4.5	2.5	3.1	7	7	7	S 3	SW 6	C 0
8	115.0	116.5	118.4	116.6	12.6	14.6	12.0	12.8	15.3	9.8	86	76	90	84	2.1	4.0	1.3	2.5	9	7	3	SE 2	NE 3	C 0
9	119.5	119.1	117.4	118.7	12.8	16.0	13.4	13.9	17.8	8.4	84	67	88	80	2.4	6.0	1.8	3.4	6	3	9	C 0	NE 6	NW 5
10	113.5	112.3	111.0	112.3	15.2	22.4	16.1	17.4	22.7	11.3	74	45	73	64	4.4	15.0	4.9	8.1	1	6	9	W 8	NW 9	NW 5
11	109.3	108.6	107.3	108.4	16.5	16.6	14.1	15.3	20.0	12.6	75	79	84	79	4.8	4.1	2.5	3.8	2	5	8	N 5	NE 5	N 5
12	105.1	104.1	104.3	104.5	14.9	18.1	15.1	15.8	20.6	12.4	87	72	91	83	2.2	5.8	1.5	3.2	10	8	10●	C 0	W 5	S 2
13	102.6	103.3	104.8	103.6	14.5	15.4	14.8	14.9	16.3	13.9	91	88	89	89	1.5	2.1	1.8	1.8	10●	10	9	SW 3	NE 2	NNW 3
14	104.7	104.9	105.3	105.0	14.2	14.8	13.9	14.2	16.4	11.3	88	86	87	87	2.0	2.4	2.2	2.2	7	10	9	NW 4	NE 5	NNW 3
15	104.7	105.2	106.7	105.5	14.5	15.9	14.5	14.8	17.4	11.9	84	80	85	83	2.7	3.6	2.5	2.9	7	9●	10	NW 4	N 3	NE 4
16	107.9	110.0	111.2	109.7	14.5	16.9	14.4	15.0	17.8	11.8	88	58	80	75	2.0	8.0	3.2	4.4	4	4	0	N 4	NE 4	NE 3
17	113.5	114.6	115.9	114.7	14.9	17.9	13.7	15.0	18.5	10.0	85	60	73	73	2.5	8.2	4.2	5.0	2	1	0	C 0	NE 7	NNE 1
18	117.0	117.0	116.7	116.9	15.7	18.0	14.9	15.9	18.8	9.1	77	65	78	73	4.1	7.2	3.6	5.0	0	3	3	NNE 4	NE 7	NNE 3
19	116.5	117.2	116.6	116.8	16.7	18.4	15.1	16.3	19.2	11.6	80	74	83	79	3.9	5.5	3.0	4.1	1	2	0	NNW 6	NE 8	C 0
20	116.1	114.6	114.8	115.2	17.0	26.2	19.2	20.4	26.5	10.4	57	38	80	58	8.3	20.9	4.4	11.2	7	5	8	S 2	SW 4	C 0
21	115.7	113.0	110.2	113.0	18.6	26.6	22.4	22.5	28.0	10.5	76	47	55	59	5.1	18.4	12.2	11.9	2	2	10	C 0	S 3	SSE 3
22	113.4	113.7	114.5	113.9	19.1	22.9	16.4	18.7	23.3	13.1	62	53	93	69	8.5	13.2	1.3	7.7	9	7	5	W 3	E 5	S 3
23	116.5	117.3	118.1	117.3	17.6	22.3	14.1	17.0	23.0	13.1	76	41	83	67	4.7	15.8	2.7	7.7	3	8	10●	W 5	SW 7	W 7
24	118.8	120.3	120.4	119.8	14.7	15.3	13.5	14.2	18.0	12.6	75	76	74	75	4.1	4.3	4.0	4.1	2	9	3	W 7	W 8	W 8
25	122.0	121.8	120.5	121.4	14.1	18.4	13.5	14.9	19.3	10.5	76	48	78	67	3.9	11.0	3.4	6.1	2	7	4	WNW 5	NW 4	C 0
26	117.0	115.9	113.3	115.4	15.0	19.3	16.5	16.8	21.6	9.8	77	60	95	77	3.8	9.0	1.0	4.6	6	8	10	SSE 2	NNE 5	NE 3
27	111.5	110.7	110.4	110.9	16.3	17.0	13.8	15.2	22.1	13.5	98	88	95	94	0.4	2.4	0.7	1.2	10●	9	10●	NE 2	NE 7	NNW 8
28	114.6	115.8	117.7	116.0	14.9	18.0	12.9	14.7	18.8	12.2	85	48	71	68	2.5	10.7	4.3	5.8	5	5	0	NW 7	N 9	WNW 4
29	118.2	118.1	119.3	118.5	14.9	16.1	12.7	14.1	19.2	10.4	72	77	89	79	4.7	4.2	1.6	3.5	0	7●	1	WNW 5	NE 7	C 0
30	120.1	120.4	119.8	120.1	15.1	16.6	12.8	14.3	19.2	10.0	79	59	89	76	3.7	7.9	1.6	4.4	4	9	7	SW 2	NNW 4	C 0
31	119.7	118.0	116.1	117.9	14.4	22.3	15.9	17.1	22.8	9.9	82	50	91	74	2.9	13.3	1.6	5.9	2	7	9	S 1	S 7	C 0
M	111.8	111.9	111.9	111.9	14.5	17.7	14.2	15.2	19.3	10.8	80	65	83	76	3.4	7.9	2.9	4.7	5.4	6.7	6.2	3.7	5.7	2.8

Sierpień-Août

1	113.0	113.0	112.4	112.8	15.4	17.8	15.7	16.2	19.6	13.7	79	63	77	73	3.7	7.6	4.1	5.1	7	6	1	W 6	WNW 7	WSW 6
2	112.2	113.1	113.1	112.8	15.5	17.0	14.7	15.7	20.2	13.3	76	59	76	70	4.3	8.4	4.0	5.6	6	7	7	W 5	WSW 7	W 2
3	113.1	113.9	114.7	113.9	15.7	18.2	14.1	15.5	19.6	13.0	80	67	81	76	3.5	7.0	3.1	4.5	5	4	2	W 5	ENE 5	NE 2
4	113.6	112.1	112.4	112.7	15.2	19.2	16.5	16.8	20.4	9.8	78	74	90	81	3.9	5.8	2.0	3.9	6	10	9	C 0	ENE 2	WSW 1
5	113.1	110.2	107.2	110.2	16.4	19.1	15.1	16.4	20.6	13.6	82	68	98	83	3.2	7.0	0.4	3.5	3	10●	10	C 0	SSE 3	C 0
6	108.3	109.3	109.8	109.1	15.9	20.7	15.7	17.0	20.9	13.4	84	52	82	73	2.9	11.7	3.2	5.9	4	6	10	WNW 3	WNW 4	C 0
7	106.8	102.9	99.6	103.1	15.8	19.1	17.3	17.4	20.5	12.3	82	90	92	88	3.2	2.1	1.6	2.3	9	10●	9	C 0	E 3	WSW 9
8	106.0	109.4	113.1	109.5	14.5	18.1	15.2	15.8	19.6	13.1	74	49	61	61	4.3	10.6	6.7	7.2	1	7	2	SSW 8	SW 10	SW 4
9	118.3	120.6	121.3	120.1	12.7	16.0	12.6	13.5	18.6	10.6	78	59	79	72	3.3	7.5	3.1	4.6	3	9	3	SW 6	NW 7	SW 1
10	120.2	116.5	111.7	116.1	14.0	20.3	18.0	17.6	21.9	9.6	69	52	59	60	4.9	11.5	8.4	8.3	1	10	10●	SW 2	S 5	SSW 4
11	111.2	111.6	112.3	111.7	14.4	19.5	17.9	17.4	20.6	14.1	72	48	77	66	4.6	11.8	4.8	7.1	9	7	9	SW 4	W 7	C 0
12	113.7	113.5	114.3	113.8	18.4	27.1	18.7	20.7	28.4	15.6	76	46	83	68	5.1	19.4	3.8	9.4	1	1	2	SW 4	SW 6	N 3
13	116.6	117.4	118.6	117.5	17.1	20.5	13.4	16.1	27.9	13.1	76	66	70	71	4.7	8.1	4.7	5.8	3	8	1	N 5	NE 5	NW 3
14	118.9	118.6	117.5	118.3	11.8	17.3	11.8	13.2	19.0	9.1	80	59	73	71	2.8	8.0	3.8	4.9	3	3	3	W 2	NE 2	NW 3
15	115.6	111.3	105.8	110.9	12.4	17.5	15.9	15.4	18.1	9.1	80	59	89	76	2.9	8.2	2.0	4.4	10	9	10	S 1	E 4	SSW 3
16	105.9	107.7	110.4	108.0	17.0	23.6	15.7	18.0	23.7	15.1	87	56	96	80	2.6	12.9	0.7	5.4	6	6	10●	WSW 1	NW 6	SSE 3
17	110.8	111.9	110.7	111.1	16.6	19.8	16.9	17.6	21.4	14.5	89	73	88	83	2.2	6.3	2.3	3.6	9	6	10	SW 2	E 2	ENE 3
18	106.7	107.3	109.2	107.7	15.4	16.1	14.5	15.1	19.5	14.1	92	88	86	89	1.3	2.1	2.4	1.9	9	10●	9	S 2	WSW 7	W 4
19	108.8	110.1	111.2	110.0	15.4	16.8	14.6	14.8	18.3	12.6	85	78	92	85	2.3	4.2	1.3	2.6	9	9	10	SW 3	W 8	NW 5
20	112.2	114.7	115.4	114.1	14.7	15.7	14.5	14.8	17.2	13.2	98	94	87	93	0.4	1.1	2.2	1.2	10●	10●	10	N 5	N 8	N 4
21	114.2	113.2	112.1	113.2	14.9	17.6	13.3	14.8	18.7	11.0	83	79	92	85	2.9	4.2	1.3	2.8	3	9	1	NW 2	NE 4	C 0
22	110.9	112.5	112.0	111.8	14.1	19.8	15.9	16.4	20.1	11.4	95	61	81	79	0.7	9.1	3.5	4.4	10	6	9	SSE 2	NW 7	C 0
23	109.1	110.8	111.9	110.6	12.5	15.1	13.2	13.5	17.5	11.9	88	78	85	84	1.7	3.9	2.3	2.6	5	9	1	SW 5	WSW 7	SW 5
24	107.3	100.9	101.3	103.2	11.4	15.2	14.9	14.1	17.2	10.4	91	89	89	90	1.2	1.9	1.8	1.6	10●	10●	6	S 5	SSW 7	WSW 3
25	104.7	106.0	108.5	106.4	13.8	16.4	15.4	14.2	18.1	12.3	81	70	84	78	3.0	5.6	2.5	3.7	9	10●	3	SW 7	SW 9	WSW 7
26	111.2	114.5	115.9	113.9	12.1	16.1	13.1	13.6	18.2	11.2	86	57	82	75	2.0	7.9	2.8	4.2	6●	6	0	WSW 7	W 8	SW 3
27	110.4	105.9	106.8	107.7	11.4	20.5	15.6	15.8	20.8	9.3	85	56	64	68	2.0	10.7	6.4	6.4	9	10●	7	SSE 6	SW 9	WSW 6
28	108.6	111.3	112.8	110.9	13.0	14.3	13.1	13.4	16.8	12.1	73	74	76	74	4.1	4.3	3.6	4.0	9	7	1	WSW 10	WSW 10	SW 7
29	112.3	112.0	112.5	112.3	13.1	15.5	12.1	13.2	17.1	11.1	84	76	83	81	2.5	4.3	2.3	3.0	9	9	0	SW 5	W 5	W 6
30	114.0	116.1	114.3	114.9	12.1	16.4	12.8	13.5	17.1	10.9	84	65	72	74	2.2	6.5	3.6	4.1	7	6	9	W 7	W 9	WSW 4
31	106.9	107.2	111.3	108.5	11.7	12.3	11.4	11.7	14.7	8.8	81	74	91	82	2.6	3.7	1.2	2.5	6	9	2	WSW 7	WNW 9	NW 6
M	111.4	111.5	111.6	111.5	14.3	18.0	14.8	15.5	19.6	12.0	82	67	82	77	2.9	7.2	3.1	4.4	6.4	7.7	5.7	4.1	6.2	3.5

Gdańsk - Wrzeszcz H_s=13m H_t=12,4m h_w=15,5m Liniec - Juillet 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB ŚNIEGU h	POGODA
1	8	•	•	
2	8	2.1	•	•°21^35-23^40
3	8	3.0	•	•°0^08-2^40;2^48-5^20 ▽°-'11^20..13^40
4	7	2.1	•	▽°-'10^20...15^05 ▽°21^15-30
5	8	2.9	•	▽°14^20-27 ▽°-'16^45-17^20 ▽°17^35-18^15
6	8	•	•	
7	8	0.0	•	▽°13^35-50;15^50-16^10
8	8	•	•	△°23-24
9	8	•	•	△°-'0^00-8^00
10	8	•	•	
11	8	0.5	•	▽°23^25-24
12	8	2.0	•	▽°0^00-1^35;14^12-17;19^35-20^07 •°21^25-22^40;=6^45-8^30
13	7	2.2	•	•°7^10-10^40 ▽°15^05-20 ▽°-'15^40-16^20
14	7	1.9	•	▽'11^15-50
15	7	1.4	•	▽°10^45-55 ▽°-'13^35-16^35; △°na
16	7	•	•	
17	8	•	•	
18	8	•	•	△°3-8
19	8	•	•	△°0^00-8
20	8	•	•	=20^20-23^10
21	6	0.0	•	=4^35-9^45∞-16^30
22	8	24.0	•	•°5^35...6^10 •ꞁ15^05-16^45 NW-SE ▽°-°20^03-40; ⟍15^05-35
23	8	0.2	•	▽°21^12-22^35
24	8	0.1	•	▽°12^20-30;13^10-20
25	8	•	•	△°5-7
26	7	3.8	•	•°-'17^15...19^35-21^20 ▽°23^35-24;=5^15-10^15∞-11^20; △°3-8
27	7	8.0	•	▽°0^00-20;1^25-2^25 •°5^40-7^35 •°-8^25 ▽°18^20-45 •°21^10-24; ꞁ'18^45-19^10 SW-N;=8^25-10^40
28	8	1.0	•	•°0^00-15 ▽°-'4^40-5^35;9^30...10^45 ▽°13^30-40
29	8	0.0	•	▽°13^15-50
30	8	0.3	•	▽°12^25-40;14^05-40
31	7	3.1	•	▽°-°15^25-45 ▽°16^20-35;=21^30-24; △°0^00-9^00
Σ	—	58.6	—	UWAGI.

Sierpień - Août

1	8	2.2	•	•°2^50-3^55 ▽°6^25-7^20 ▽'11^13-40 ▽°11^50-12^05;=0^00-1^20
2	8	•	•	
3	8	•	•	
4	7	0.3	•	•°14^05 18^35;=20^10-23^40
5	7	18.9	•	▽°-'13^20...20^30 ▽°23^45-24; ꞁ²17^05-35 NW-SE;=3^20-8^20;20^30-24; △°3-8
6	8	•	•	▽°0^00-45 ▽'2^10-20;=0^00-8^40
7	6	53.8	•	•ꞁ°16^15-17^10 SW-N ▽²-17^35 •ꞁ°17^35-19^05 W-NW ▽°23^10-30;=4^40-11^25; △°4-9
8	8	•	•	⟫9^30-18^25
9	8	•	•	
10	7	0.0	•	•°20^50-23^35; ⊕°10^30-12^40
11	8	•	•	
12	8	•	•	
13	8	•	•	△°2-8
14	8	•	•	
15	8	2.4	•	▽°-'14^15-15^20;=7^30-11^40; △°1^00-7^00
16	7	10.2	•	▽²20^50-21^25 ▽°-22^15; ꞁ20^55-21^25 W-NW;=4^20-9^40
17	7	1.1	•	•°21^25-24;=5^30-7^30
18	7	1.2	•	•°0^00-4^0 11^08...14^35 ▽°19^25-20^20;=4^30-10^30
19	8	0.5	•	▽°10^33-11^07;16^25-35;20^40-21^05
20	6	0.0	•	•°6^05...8^15 •°13^35-19^25;=19^25-24
21	8	0.0	•	=0^00-20
22	8	4.0	•	•°6^25-7^15;8^25-9^15 •'-10^25;=5^35-8^10
23	8	0.9	•	•'2^25-3^40;4^05-6^35 ▽°12^35-13^20;17^45-18^10
24	6	5.6	•	•°6^05-16^05 •'-17^40 •°-18^15
25	7	0.0	•	▽°13^40-14^03;16^38-17^07
26	8	0.0	•	▽°0^48-1^05;3^30-45;7^20-28;7^44-8^02;12^07-23
27	7	0.0	•	•°13^42-14^25;16^10-20;=6^20-8^40
28	8	0.9	•	▽°-'8^21-9^18 ▽°10^15-27 ▽'12^02-35 ▽°22^25-23^12; ⟫7^15-17^15
29	8	0.0	•	▽°13^03-08;15^40-50
30	8	0.0	•	▽'1^35-45
31	8	5.6	•	▽°4^10-25 ▽°-'8^46-9^38;10^23-11^45 ▽°14^06-15
Σ	—	107.6	—	UWAGI.

Gdańsk - Wrzeszcz φ = 54°23' λ = 18°36' Wrzesień - Septembre 1962

Dni	Ciśnienie P = 900 + I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność względna U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	115.3	117.2	119.4	117.3	11.6	17.3	11.8	13.1	18.3	9.7	89	54	87	77	1.5	9.0	1.8	4.1	1	4	3	NW 4	NW 6	W 3
2	119.4	119.7	118.2	119.1	11.9	16.3	12.6	13.4	19.0	10.5	89	63	86	79	1.5	6.9	2.1	3.5	5	9	2	WSW 6	W 7	WSW 3
3	117.6	117.6	116.7	117.3	13.2	20.7	13.4	15.2	21.0	9.7	83	57	92	77	2.6	10.5	1.3	4.8	9	2	9	SW 5	N 3	C 0
4	112.0	107.7	105.6	108.4	12.7	25.2	18.8	18.9	27.2	7.4	85	47	70	67	2.3	16.9	6.5	8.6	0	1	9	SSE 3	S 6	C 0
5	98.0	100.4	100.9	99.8	15.9	21.0	14.8	16.6	21.4	13.8	84	63	72	73	2.9	9.3	4.7	5.6	9	9	2	S 3	SW 8	SSW 4
6	99.6	101.7	99.5	100.3	13.7	17.1	14.3	14.8	17.7	11.3	79	60	78	72	3.4	7.8	3.6	4.9	5	9	10	SW 6	WSW 7	SW 3
7	90.2	90.2	97.2	92.5	16.6	16.9	12.2	14.5	18.3	11.4	82	73	83	79	3.5	5.2	2.4	3.7	9	9	1	SW 7	SW 8	SW 5
8	102.5	104.8	106.9	104.7	10.2	14.6	11.0	11.7	15.5	9.3	77	53	81	70	2.8	7.8	2.4	4.3	1	8	9	SW 7	WSW10	WSW 6
9	113.1	116.3	118.6	116.0	10.9	13.7	10.8	12.0	16.7	9.4	87	61	82	77	1.6	6.9	2.3	3.6	1	6	9	W 5	NNW 8	SSW 3
10	116.2	112.1	111.2	113.2	11.6	20.7	14.3	15.2	21.8	10.2	77	40	74	64	3.1	14.6	4.3	7.3	10	1	4	SSW 3	SW 8	S 2
11	107.1	105.0	112.2	108.1	15.3	15.8	12.3	13.9	16.8	11.4	73	89	82	81	4.8	1.9	2.5	3.1	10	10	1	SW 4	SW 6	W 6
12	108.1	100.5	95.9	101.5	10.2	19.0	16.6	15.6	21.6	8.1	92	76	74	81	0.9	5.2	5.0	3.7	9	9	6●	SSE 5	SSW10	WSW14
13	108.4	111.9	114.2	111.2	11.4	16.2	11.5	12.6	16.9	9.2	82	43	78	68	2.5	10.6	3.0	5.4	1	3	2	W 8	W 9	W 8
14	116.8	119.3	120.0	118.7	11.1	14.6	9.9	11.4	15.6	9.0	80	50	86	72	2.6	8.3	1.8	4.2	4	7	0	W 8	WNW 9	WSW 3
15	119.4	118.4	114.3	117.4	9.7	14.2	10.3	11.1	14.7	7.5	88	55	82	75	1.4	7.3	2.2	3.6	7	10	2	SW 2	S 3	C 0
16	108.2	106.0	106.9	107.0	7.2	21.4	15.1	14.7	21.7	4.3	97	54	94	82	0.3	11.6	1.0	4.3	1	9	10●	S 3	S 3	SSW 1
17	109.2	110.8	111.4	110.5	11.8	14.6	11.0	12.1	15.4	9.7	94	63	91	83	0.8	6.2	1.1	2.7	9	10	10	WNW 3	NW 3	C 0
18	110.5	110.1	106.5	109.0	6.8	13.2	10.1	10.0	13.8	5.8	97	66	73	79	0.3	5.1	3.4	2.9	7	9	10●	C 0	NNE 6	NNE 9
19	104.4	107.5	111.3	107.7	8.7	10.9	8.4	9.1	11.4	8.0	93	84	86	88	0.7	2.1	1.5	1.4	10●	10	10●	NW 6	WNW 7	W 6
20	111.1	111.6	112.5	111.7	9.7	12.0	9.2	10.0	13.3	7.4	91	69	84	81	1.1	4.3	1.8	2.4	9	9	10	WSW 5	W 7	W 5
21	112.2	112.8	113.6	112.9	10.1	12.5	9.3	10.3	13.8	8.0	90	59	85	78	1.3	6.0	1.7	3.0	9	10	9●	WNW 7	NW 8	NW 7
22	115.5	117.4	117.7	116.9	9.0	12.8	9.4	10.2	13.7	7.7	89	60	83	77	1.3	5.9	2.0	3.1	5	8	9	NW 7	NNW 9	WNW 4
23	113.5	111.4	114.4	113.1	9.6	10.7	8.1	9.1	11.8	7.7	93	86	94	91	0.8	1.8	0.6	1.1	10	10●	2	WSW 4	W 5	W 2
24	119.6	122.2	125.8	122.5	8.3	12.8	8.0	9.3	13.4	7.4	94	72	92	86	0.7	4.1	0.9	1.9	5	3	0	NW 2	NNE 8	NW 2
25	128.7	129.8	128.7	129.1	5.8	15.3	9.1	9.8	16.8	4.3	97	62	93	84	0.3	6.7	0.8	2.6	0	4	0	C 0	S 3	C 0
26	128.0	126.5	124.2	126.2	5.3	16.3	10.7	10.8	17.0	4.0	95	54	78	76	0.4	8.4	2.9	3.9	0	3	0	SSE 2	SE 6	SE 3
27	122.5	119.9	118.3	120.2	4.8	14.2	11.0	10.2	15.3	3.7	94	66	85	82	0.6	5.4	1.9	2.6	0	3	10	C 0	ENE 5	ESE 1
28	116.4	115.8	115.1	115.8	11.2	12.8	11.7	11.8	13.1	10.4	94	91	89	91	0.8	1.4	1.5	1.2	10●	10	10	C 0	NE 3	ESE 2
29	113.6	113.7	114.9	114.1	11.5	12.5	12.2	12.1	13.0	10.9	97	95	98	97	0.4	0.7	0.3	0.5	10●	10	10	ENE 3	NE 3	C 0
30	117.2	118.5	119.3	118.3	11.5	15.8	10.4	12.0	17.0	10.2	99	80	99	93	0.2	3.5	0.2	1.3	9	9	0	C 0	SE 3	C 0
31																								
M	112.5	112.6	113.0	112.7	10.6	15.8	11.6	12.4	16.8	8.6	89	65	84	79	1.6	6.7	2.2	3.5	5.8	7.1	5.6	3.9	6.3	3.4

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1	120.6	121.4	123.2	121.7	9.9	18.4	15.0	14.6	19.4	8.1	99	70	86	85	0.2	6.5	2.4	3.0	8	9	9	C 0	SSE 4	SSE 2
2	124.9	125.3	125.2	125.1	12.4	20.2	13.6	15.0	20.7	12.1	95	69	91	85	0.7	7.5	1.5	3.2	10	5	0	SSE 4	SSE 5	SSE 2
3	124.4	123.2	123.1	123.6	8.9	20.4	14.2	14.4	20.7	8.5	99	60	83	81	0.2	9.5	2.7	4.1	8	5	0	SSE 2	SSE 5	S 3
4	121.9	121.5	120.8	121.4	10.3	19.4	16.6	15.7	20.3	9.9	97	64	80	80	0.3	8.2	3.9	4.1	3	8	10	S 3	SSE 4	S 3
5	121.6	122.3	123.2	122.4	14.0	16.1	13.6	14.3	16.8	13.2	94	86	99	93	0.9	2.5	0.2	1.2	10	10	10	C 0	N 1	C 0
6	124.5	127.0	130.2	127.2	12.7	13.2	11.8	12.4	13.8	11.7	96	94	95	95	0.5	0.9	0.6	0.7	10	10●	10●	N 4	N 7	NW 3
7	132.0	133.8	134.9	133.6	10.7	13.9	9.5	10.9	14.9	9.1	86	63	91	80	1.8	5.9	1.1	2.9	9	5	6	C 0	WNW 1	C 0
8	135.2	135.4	134.2	134.9	6.6	13.6	7.2	8.6	14.6	5.2	94	75	96	88	0.5	3.9	0.5	1.6	4	6	0	WSW 3	ENE 2	C 0
9	132.5	132.0	130.1	131.5	7.0	16.0	7.6	9.6	16.1	4.8	97	73	97	90	0.3	4.5	0.3	1.7	0	0	0≡	C 0	C 0	C 0
10	127.7	126.4	123.9	126.0	3.6	10.8	6.3	6.8	11.9	2.7	97	95	98	97	0.3	0.7	0.1	0.4	0≡	9	0	C 0	SSE 4	C 0
11	121.0	117.8	115.4	118.1	1.1	14.3	9.8	8.8	15.0	0.4	100	71	86	86	0.0	4.8	1.7	2.2	0≡	0	0	C 0	C 0	NNW 4
12	115.9	118.7	121.5	118.7	9.1	12.3	8.3	9.5	12.7	8.1	85	66	73	75	1.8	4.8	3.0	3.2	9	6	5	NW 3	NNE 7	NE 3
13	122.2	120.9	115.9	119.7	4.1	13.2	6.0	7.3	13.5	3.5	87	48	86	74	1.1	7.8	1.3	3.4	1	1	0	SW 3	S 4	C 0
14	108.8	109.4	114.8	111.0	5.7	11.3	9.1	8.8	11.5	4.1	91	71	57	73	0.9	3.9	5.0	3.3	3	10	10	SW 3	W 4	NNE 9
15	121.3	124.2	125.5	123.7	2.9	8.9	3.1	4.5	9.4	2.8	72	43	73	63	2.1	6.5	2.1	3.6	1	3	2	W 3	N 8	SW 2
16	122.2	119.9	118.7	120.3	5.3	10.6	9.3	8.6	12.2	2.4	59	52	78	63	3.7	6.1	2.6	4.1	6	9	9	SW 7	WSW 5	SW 6
17	118.4	119.6	118.5	118.8	9.7	11.4	10.7	10.6	12.2	8.4	92	82	84	86	0.9	2.5	2.1	1.8	9	10●	9	WSW 5	W 9	WSW 4
18	114.2	110.9	103.6	109.6	11.8	13.1	13.4	12.9	13.6	9.9	82	79	74	78	2.5	3.1	4.0	3.2	10	9	9	W 10	W 14	W 14
19	106.7	109.0	108.2	108.0	9.6	12.3	9.2	10.1	13.7	8.7	88	60	89	79	1.5	5.8	1.2	2.8	1	9	9	WNW 6	WNW 8	WNW 5
20	114.9	120.3	125.5	120.2	5.8	9.3	4.0	5.8	9.8	3.6	82	51	74	69	1.7	5.7	2.1	3.2	1	4	0	NW 6	N 9	WNW 5
21	125.7	125.3	126.3	125.8	5.3	10.6	9.9	8.9	11.1	2.4	81	85	86	84	1.7	2.0	1.8	1.8	3	9	9	S 2	WNW 3	W 3
22	126.5	126.1	124.8	125.8	9.3	11.3	9.5	9.9	11.4	9.1	92	72	79	81	0.9	3.8	2.5	2.4	9	10	10	WSW 3	WSW 6	SSW 3
23	122.6	122.4	121.0	122.0	9.7	10.7	9.3	9.8	11.0	8.4	83	80	83	82	2.0	2.6	2.0	2.2	10	10	10	WNW 5	W 5	SW 3
24	117.2	117.5	118.9	117.9	5.1	9.5	8.7	8.0	10.3	4.8	90	78	88	85	0.9	2.7	1.3	1.6	9	10	10	C 0	W 3	WSW 5
25	117.8	116.9	115.3	116.7	7.3	9.6	11.1	9.8	11.2	7.1	90	77	71	79	1.1	2.8	3.9	2.6	9	9	9	SSW 3	SW 5	SW 7
26	113.4	111.2	108.0	110.9	5.3	11.2	10.1	9.2	11.9	4.6	87	68	77	77	1.1	4.2	2.9	2.7	0	0	4	S 5	S 5	S 5
27	106.8	112.8	116.7	112.1	7.3	8.3	2.1	5.0	12.9	2.0	90	54	78	74	1.1	5.0	1.5	2.5	10●	1	0	NW 8	NNW 9	SW 1
28	111.8	107.9	107.5	109.1	1.7	6.0	5.2	4.5	6.7	-2.0	87	80	80	82	0.9	1.9	1.8	1.5	10●	9	9	SSE 2	SW 2	S 3
29	109.4	110.9	113.9	111.4	2.1	9.0	4.9	5.2	9.7	1.8	96	73	89	85	0.3	3.4	1.0	1.6	9	9	0	C 0	SSW 2	SW 3
30	113.5	113.0	110.1	112.2	3.9	7.9	3.3	4.7	9.7	0.8	92	76	93	87	0.7	2.5	0.5	1.2	5	6	4	SW 5	SW 6	S 4
31	107.3	108.0	110.1	108.5	5.6	8.4	2.3	4.2	9.3	1.1	91	75	91	86	0.7	2.7	0.6	1.3	9	9	0	S 5	SE 3	C 0
M	119.4	119.7	119.6	119.6	7.2	12.3	8.9	9.3	13.2	5.7	89	71	84	81	1.1	4.3	1.9	2.4	6.0	6.8	5.3	3.2	4.9	3.3

Gdańsk - Wrzeszcz $H_s = 13m$ $H_b = 12{,}4m$ $h_w = 15{,}5m$ Wrzesień - Septembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	•	•	
2	8	•	•	△°4-8
3	8	•	•	△°2-8
4	7	•	•	=5^30-9^30∞-18^40-19^45=-24; △°3-7
5	8	0.0	•	⚲°10^18-20 19^05-10; =0^00-9^20
6	8	2.2	•	⚲°13^15-25
7	7	0.8	•	•°0^35-4^50 ⚲^0-1 12^12...15^15 ⚲°19^10-20
8	8	0.0	•	⚲°15^45-16^05, 20^46-21^10; ≫9^30-14^40
9	8	•	•	
10	8	•	•	
11	6	1.1	•	•°9^35-12^20 •'13^05-40 ⚲°14^40-15^10, 15^32-45; =12^20-15^30
12	7	2.7	•	•°9^02-11^10, 14^37-50, 15^05-15 ⚲°16^45-17^25, 21^40-22^05; ☈°16^45-17^30 NW-E; ≫13^10-14^30, 19^10-24; =6^20-10^00
13	8	•	•	≫0^00-2^30, 14^30-17^20
14	8	•	•	△°23-24
15	8	•	•	△^0-1 0^00-9
16	7	4.9	•	•°15^15...19^10-20^25 21^35-24; =19^10-24; △^0-1 0^00-10
17	8	•	•	•°0^00-4^20; =0^00-8^40
18	8	17.5	•	•^0-1 19^45-24; =5^10-9^20; △' 3-11
19	7	5.8	•	•^1-0 0^00-13^35 ⚲^1-0 15^20-18^25 ⚲' 21^20-22^15
20	8	0.0	•	⚲' 1^40-2^25 ⚲°12^45-13^05 17^10-17, 18^05-15, 20^48-21^13; =6^20-8^40
21	8	2.8	•	⚲°0^45-1^10, 8^07-30, 20^25-45, 21^35-22^05 ⚲' -22^50
22	8	0.8	•	⚲°2^20-35, 10^21-11^05
23	7	3.6	•	⚲°6^35-7^15 •°11^10-15^05 ⚲°15^45...18^05; ∩'16^40-55
24	8	•	•	⚲^0-1 1^20-2^05 ⚲°2^15-25, 5^40-6^05
25	7	•	•	=7^15-9^20, 20^30-24; △' 0^00-10 △° 22-24
26	7	•	•	=0^00-11^10; △^0-1 0^00-10
27	8	0.0	•	=6^30-10^15; △° 3-9
28	6	1.6	•	•°2^35-5^15 7^20-9^15; =6^10-24
29	6	0.7	•	•°4^20-12^20 •°16^15-19^20; =0^00-24
30	6	•	•	=0^00-18^05 ≡^0-1 19^45=-24
31				
Σ	—	44.5	—	UWAGI.

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1	6	•	•	=0^00-14^45∞-16^45=-24
2	6	•	•	=0^00-13^40 17^30-24; △^0-1 19^00-24
3	7	•	•	=0^00-11^35 17^20-20^45; △^1-2 0^00-10
4	7	0.0	•	•°19^20-28; =0^20-12^30∞14^20-16^40=-24; △°0^00-9
5	6	3.7	•	•°1^07-2^10 ⚲' 9^10-45; =0^00-19^15 ≡°19^35=-24
6	6	0.0	•	•°1^20-4^50, 5^40-6^40 •°7^45-9^10, 20^45-21^40; =0^00-24
7	7	0.0	•	=0^00-5^15
8	6	•	•	=5^20-24; △' 1-10 △° 20-24
9	6	•	•	=0^00-17^20 ≡°-18^15=-20^45 ≡^0-1 -24; △^0-1 0^00-11
10	4	•	•	≡' 0^00-7^25=-9^45 ≡°-11^40=-15^50 ≡^0-2 -20^10=-24
11	6	•	•	=0^00-5^20 ≡^0-2 -10^15=≡°-24
12	8	•	•	=0^00-8^10; △' 22-24
13	8	•	•	=16^30-24; △' 0^00-9
14	6	0.4	•	•^1-0 16^05-18^35; =0^00-24; △°2-8
15	8	•	•	=0^00-1^30; ☋°21^30-22^30
16	8	•	•	☋°2^30-4^10
17	7	0.0	•	•°11^40-13^25 •°14^25-15^20, 18^45-19^30; =16^30-24
18	7	0.5	•	•°7^35...8^20, 9^25...11^10 •°21^37...24; ≫7^10-8^30, 12^10-24; =0^00-9^25, 16^10-21^37
19	8	2.1	•	•°0^00-20 ⚲°18^40-20^07; ≫0^00-1^30
20	8	0.1	•	⚲°9^25-50, 10^35-50, 15^05-10; ∩15^00-08
21	7	•	•	
22	7	•	•	=7^20-9^30
23	7	•	•	=8^20-10^40, 15^15-20^30
24	6	•	•	=5^25-24
25	6	•	•	=0^00-21^40
26	6	0.8	•	=5^30-24
27	8	0.9	•	•°5^35-7^35 ⚲°10^30-40; =0^00-5^35
28	7	0.2	•	•°6^30-7^35 •°-9^35; =6^20-12^30, 22^30-24; ∪² na
29	7	•	•	=0^00-11^35, 16^20-24; △°20-24; ⊕°8^30-9^15
30	7	•	•	=0^00-11^30, 18^40-24; △°0^00-7
31	6	1.1	•	=0^00-24
Σ	—	9.6	—	UWAGI.

Gdańsk-Wrzeszcz $\varphi = 54°23'$ $\lambda = 18°36'$ Listopad-Novembre 1962

DNI	CIŚNIENIE P= 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	109.3	108.8	108.7	108.9	4.8	6.7	8.8	7.3	9.2	2.1	97	96	97	97	0.3	0.4	0.3	0.3	10 ●	10 ●	10 ,	C 0	N 3	NE 5
2	108.3	110.1	113.0	110.5	9.8	10.6	8.9	9.6	11.0	8.6	100	97	97	98	0.0	0.4	0.3	0.2	10 , ≡	10	10	N 6	C 0	S 3
3	115.3	115.9	116.3	115.8	7.9	7.8	7.7	7.8	9.2	7.3	94	94	94	94	0.6	0.6	0.6	0.6	10	10 ●	10	S 3	SSE 3	SE 2
4	115.4	115.3	115.4	115.4	8.4	10.3	9.1	9.2	12.2	6.8	97	82	93	91	0.3	2.2	0.8	1.1	10	9	9	SSE 2	S 7	S 7
5	114.3	114.2	114.5	114.3	10.6	10.8	7.5	9.1	11.2	7.3	88	84	93	88	1.5	2.2	0.8	1.5	10	10	0	SSE 5	SSE 7	SSE 2
6	114.1	114.1	115.4	114.5	5.1	8.4	7.1	6.4	9.2	3.0	86	62	66	71	1.0	4.1	3.5	2.9	0	1	5	SE 2	SE 5	SE 3
7	117.7	119.4	120.8	119.3	4.8	8.4	6.1	6.4	9.4	4.4	78	69	73	73	1.9	3.4	2.5	2.6	8	9	3	SE 7	SE 4	SSE 2
8	120.4	118.4	118.4	119.1	3.1	7.8	5.7	5.6	8.5	3.0	81	69	86	79	1.4	3.3	1.3	2.0	3	0	0	SE 1	SE 3	SE 1
9	118.2	120.3	122.5	120.3	2.7	5.8	5.1	4.7	7.4	1.6	96	83	83	87	0.2	1.5	1.5	1.1	1	9	10	E 1	E 8	E 9
10	123.9	125.3	126.7	125.3	3.8	3.1	2.4	2.9	5.3	1.9	82	73	72	76	1.5	2.1	2.1	1.9	10	10	10	E 9	ENE 8	E 9
11	127.1	125.9	124.5	125.8	1.8	1.6	1.8	1.8	2.7	1.1	78	94	93	88	1.6	0.4	0.6	0.9	10	10 ●*	10 ●*	E 9	E 6	E 8
12	123.1	122.3	120.2	121.9	0.7	1.8	1.3	1.3	2.3	0.4	94	83	89	89	0.4	1.2	0.8	0.8	10 ●*	10	10	ESE 5	SE 4	ESE 4
13	118.3	119.0	120.0	119.1	1.8	3.0	2.6	2.5	3.2	0.7	98	88	95	94	0.2	0.9	0.4	0.5	10 ,	10	10	SE 2	S 2	C 0
14	119.3	118.4	116.4	118.0	2.7	6.5	2.1	3.4	6.7	1.9	95	78	98	90	0.4	2.2	0.1	0.9	10	9	10	C 0	SSW 1	SSW 3
15	109.4	105.3	101.6	105.4	4.3	6.6	5.1	5.3	6.7	1.8	97	79	81	86	0.3	2.0	1.7	1.3	10	7	6	S 4	S 6	SSW 6
16	101.8	104.5	107.0	104.5	2.6	4.1	0.9	2.1	5.2	0.8	82	74	83	80	1.3	2.2	1.1	1.5	9	6	3	SW 7	W 6	WSW 7
17	110.0	111.7	112.8	111.5	-0.5	1.8	-0.6	0.0	2.1	-5.2	90	78	83	84	0.6	1.6	1.0	1.1	1	6	9	SW 4	SW 8	S 3
18	109.6	106.7	103.9	106.7	-1.2	1.2	1.1	0.6	1.3	-3.1	82	75	83	80	1.0	1.7	1.1	1.3	10	10	10	SE 2	ESE 5	SE 1
19	97.0	98.2	104.3	99.8	0.6	2.8	3.1	2.4	3.4	0.4	98	91	86	93	0.1	0.7	1.0	0.6	10 *	10	9	SE 2	SW 7	SSW 2
20	105.6	106.2	104.9	105.6	1.4	2.7	2.1	2.1	3.3	0.2	94	93	95	94	0.4	0.5	0.4	0.4	9	10 ●	10 ●	SSW 1	C 0	W 4
21	107.7	109.9	111.3	109.6	1.3	1.6	0.4	0.9	2.6	0.3	87	78	88	84	0.9	1.6	0.8	1.1	9	9	9	S 2	S 2	C 0
22	111.2	112.2	114.3	112.6	-1.4	1.3	1.1	0.5	2.2	-1.9	87	87	90	88	0.7	0.9	0.6	0.7	9	10	10	C 0	C 0	C 0
23	116.0	118.1	122.0	118.7	0.9	0.6	0.8	0.8	1.7	0.1	98	86	88	91	0.1	0.9	0.8	0.6	10	10	9	C 0	S 2	S 2
24	125.5	127.6	129.8	127.6	-2.9	-1.1	-1.2	-1.6	0.9	-3.2	88	89	93	90	0.5	0.6	0.4	0.5	3	0	10	SW 3	SW 3	C 0
25	129.8	127.5	127.0	128.1	0.1	0.1	0.6	0.4	0.8	-1.7	88	84	88	87	0.8	1.0	0.8	0.9	10	10	10	SSW 1	S 4	S 1
26	129.3	130.3	130.2	129.9	2.3	3.8	2.9	3.0	4.7	0.6	93	83	93	90	0.5	1.3	0.5	0.8	10	3	10	SW 1	SW 3	C 0
27	128.6	127.8	125.1	127.2	4.2	6.0	4.9	5.0	6.1	2.9	93	92	92	92	0.5	0.8	0.7	0.7	10	10	10	SW 3	SW 3	S 2
28	119.3	118.8	119.8	119.3	5.8	6.4	5.5	5.8	6.6	4.7	86	87	95	89	1.3	1.3	0.4	1.0	10	10	8	SW 3	WNW 8	W 2
29	118.7	116.6	108.2	114.5	3.7	5.5	6.4	5.5	7.2	3.1	92	91	91	91	0.7	0.8	0.9	0.8	4	10	10 ●	WSW 5	SW 4	WSW 8
30	107.7	110.7	119.7	112.7	3.7	3.9	2.6	3.2	6.7	0.5	90	88	75	84	0.8	1.0	1.9	1.2	8	9	7	WNW 6	NNW 3	N 4
31																								
M	115.7	116.0	116.5	116.1	3.0	4.7	3.7	3.8	5.6	1.7	90	84	88	87	0.7	1.5	1.0	1.1	8.1	8.2	8.2	3.2	4.2	3.3

Grudzień - Décembre

DNI	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	129.2	133.5	138.2	133.6	-0.3	0.7	-1.8	-0.8	2.5	-2.2	90	81	81	84	0.6	1.2	1.0	0.9	9 *	1	0	NW 6	NW 7	WNW 4
2	139.0	138.6	136.7	138.1	-1.9	1.4	-1.4	-0.8	1.7	-3.0	83	78	86	82	0.9	1.6	0.8	1.1	4	4	9	W 4	W 7	WSW 9
3	134.3	132.6	128.5	131.8	-3.0	-1.4	-2.6	-2.4	-0.4	-5.5	77	74	79	77	1.1	1.4	1.1	1.2	3	4	7	WSW 7	SW 2	C 0
4	123.2	120.5	117.5	120.4	1.4	4.1	3.4	3.1	5.1	-3.0	92	80	83	85	0.6	1.6	1.3	1.2	10	5	7	WSW 2	W 6	W 9
5	120.7	124.5	127.2	124.1	4.9	6.1	4.7	5.1	6.5	3.4	86	85	89	87	1.3	1.4	0.9	1.2	10	10	9	N 7	NW 3	W 3
6	126.0	125.0	124.2	125.1	2.2	3.7	1.3	2.1	4.9	1.2	93	87	89	90	0.6	1.1	0.8	0.8	10	10	4	WSW 8	SW 5	WNW 4
7	122.1	122.8	125.5	123.5	0.6	4.8	2.6	2.6	6.6	-0.6	73	52	93	73	1.8	4.2	0.6	2.2	0	1	10	N 1	WNW 5	W 3
8	127.3	126.3	121.2	124.9	2.5	1.3	1.6	1.8	3.3	0.2	84	76	69	76	1.2	1.6	2.2	1.7	10	8	9	SW 3	S 3	S 4
9	106.9	100.6	92.0	99.8	3.4	2.9	2.4	2.8	3.5	-1.5	68	60	82	70	2.5	3.0	1.3	2.3	9	9	10	SSW 8	SW 8	SW 9
10	89.9	91.1	94.9	92.0	3.0	4.2	4.3	4.0	4.4	1.4	86	84	90	87	1.1	1.3	0.8	1.1	9	9	6	SW 8	SW 9	W 5
11	98.3	98.9	94.9	97.4	2.5	3.2	3.1	3.0	4.6	1.8	88	88	88	88	0.9	0.9	0.9	0.9	9 ●	9 ●	10	W 7	WSW 5	SSW 3
12	87.4	87.1	88.3	87.6	3.6	5.1	5.5	4.9	5.5	2.5	90	86	84	87	0.8	1.3	1.4	1.2	10 ●	10	10	SSW 7	SSW 7	S 3
13	94.1	95.7	96.7	95.5	4.2	2.7	0.8	2.1	5.6	0.5	90	95	98	94	0.8	0.4	0.2	0.5	10	10 ●	10	S 2	SE 2	C 0
14	99.5	100.5	99.3	99.8	0.8	1.8	0.5	0.9	2.3	-0.2	94	91	82	89	0.4	0.7	1.1	0.7	6	9	7	C 0	WSW 4	WSW 5
15	87.6	79.0	76.8	81.1	-0.9	0.2	1.9	0.8	2.5	-1.8	89	90	89	89	0.6	0.6	0.8	0.7	10	10 *	10	S 6	SSE 5	SSW 2
16	71.7	73.6	80.2	75.2	1.3	1.1	2.3	1.8	2.6	1.0	94	96	77	89	0.4	0.2	1.7	0.8	10	10 ,	9	S 2	C 0	NE 2
17	88.0	91.8	95.6	91.8	0.6	0.1	-1.6	-0.6	2.6	-2.1	98	96	90	95	0.1	0.3	0.5	0.3	10 ●*	10 *	10 *	N 1	NE 1	C 0
18	97.4	98.5	101.2	99.0	-2.6	-2.3	-4.2	-3.3	-1.4	-5.1	93	96	91	93	0.3	0.3	0.4	0.3	10 *	10 *	10 *	C 0	C 0	C 0
19	104.8	108.3	113.1	109.4	-6.7	-6.5	-5.5	-6.0	-3.8	-8.3	86	86	87	86	0.5	0.5	0.5	0.5	10	10	10	C 0	C 0	C 0
20	121.1	123.3	124.7	123.0	-6.7	-9.9	-14.1	-11.2	-5.1	-15.1	86	78	83	82	0.5	0.6	0.3	0.5	9	3	0	NE 2	SSE 1	C 0
21	122.7	123.0	126.1	123.9	-17.1	-13.0	-13.5	-14.3	-11.5	-18.6	85	73	80	79	0.2	0.6	0.4	0.4	0	6	9	C 0	C 0	C 0
22	133.4	138.3	143.7	138.5	-11.6	-8.0	-12.0	-10.9	-7.2	-14.6	89	81	74	81	0.3	0.6	0.6	0.5	9 *	8	0	C 0	ENE 4	C 0
23	147.2	148.1	149.4	148.2	-12.4	-8.3	-12.1	-11.2	-5.0	-15.3	89	83	89	87	0.3	0.5	0.3	0.4	10	1	0	C 0	C 0	C 0
24	146.7	144.3	142.5	144.5	-8.8	-2.7	-3.9	-4.8	-2.1	-14.1	86	82	85	84	0.4	0.9	0.7	0.7	9	9 *	10	C 0	C 0	C 0
25	137.8	133.2	126.3	132.4	-5.9	-3.9	-5.1	-5.0	-2.6	-7.2	81	71	85	79	0.7	1.3	0.6	0.9	9	2	10	SSW 1	C 0	C 0
26	117.8	113.8	111.0	114.2	-8.4	-8.0	-10.8	-9.5	-4.8	-10.8	83	78	80	80	0.5	0.7	0.5	0.6	10	10 *	7	S 2	SSW 3	C 0
27	108.9	109.0	110.0	109.3	-9.2	-7.9	-8.5	-8.5	-7.8	-13.1	88	73	83	81	0.4	0.9	0.5	0.6	10	5	10 *	C 0	S 2	S 1
28	109.2	109.4	110.9	109.8	-7.7	-5.5	-5.7	-6.2	-5.3	-8.5	87	80	82	83	0.4	0.8	0.7	0.6	9	4	6	C 0	C 0	SW 4
29	111.1	108.8	107.4	109.1	-4.8	-5.4	-7.2	-6.2	-4.6	-9.0	91	85	88	88	0.4	0.6	0.4	0.5	10 *	10 *	10 *	C 0	SSE 2	C 0
30	109.1	112.6	117.0	112.9	-3.6	-1.4	-4.2	-3.4	-0.7	-8.6	85	66	84	78	0.7	1.9	0.7	1.1	10	3	9	NW 3	NE 2	C 0
31	120.8	123.8	125.9	123.5	-6.9	-5.2	-10.8	-8.4	-3.7	-10.8	74	65	80	73	0.9	1.4	0.5	0.9	10	9	9	SSE 2	ENE 5	SE 1
M	114.0	114.1	114.5	114.2	-2.8	-1.5	-2.9	-2.5	-0.1	-5.4	86	81	85	84	0.7	1.1	0.8	0.9	8.5	7.1	7.6	2.9	3.2	2.3

Gdańsk - Wrzeszcz $H_s = 13m$ $H_t = 12{,}4\,m$ $h_w = 15{,}5m$ Listopad - Novembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ LODU h	POGODA
1	4	23.7	•	•0-1 14^45-13^25 •° 14^45-24; = 0^00-24
2	6	0.0	•	•° 0^00-10^40, 15^40-19^35; = 0^00-6^45 ≡0-1 10^25 = -16^10 ≡° 16^50 = -24
3	5	1.6	•	•0-1 11^25-15^20; = 0^00-24
4	6	•	•	= 0^00-24; ⌓° 17-22
5	6	•	•	= 0^00-24; ⌓' 23-24
6	7	•	•	= 0^00-4^0 6^40-9^30; ⌓' 0^00-5; ⊽° 19^15-20^30
7	7	•	•	= 15^30-24
8	7	•	•	= 0^00-11^40, 16^20-24; ⌓° 21-24
9	7	•	•	≫ 18^10-20^20; = 0^00-7^40; ⌓0-1 0^00-8
10	8	•	•	≫ 7^10-10^30
11	6	6.0	•	*0-1 8^35-12^35 *° -14^10 •0-1 -18^20 *' -19^40 *° -24
12	7	2.1	•	*° 0^00-2^15 •° ... 3^40 *° 4^40-7^40 •° -8^35 *° 14^36-20^20, 21^35-23^40; = 8^35-12^40
13	6	0.0	•	*° 0^43-2^35 •° -9^35; = 9^35-24
14	6	0.2	•	= 0^00-17^15 ≡° -18^10 = -24
15	6	0.0	•	•° 1^20-3^15 9^20-10^35; = 0^00-4^30 6^30-24
16	8	0.0	•	⊽° 17^07-20; = 0^00-9^40; ⊔' nr
17	8	•	•	= 17^35-24; ⊔1-3 0^00-10 ⊔' nr
18	7	1.9	•	*° 22^40-24; = 0^00-7^30; ⊔' 0^00-10
19	7	0.7	1	*° 0^00-4^5 ⊼° -2^35 *0-2 4^50-10^40; = 10^40-12^50, 13^30-24
20	5	3.8	•	•° 12^35-24; = 0^00-8^10 ≡° -11^25 = -12^35; ⌓° 4-8
21	7	•	•	•° 0^00-1^25; = 1^25-11^40, 16^45-24
22	5	2.8	•	*° 22^35-23^20 •° -24; = 0^00-24
23	6	•	•	•° 0^00-1^10 *' -1^30 *' -4^35; = 0^00-24
24	6	•	•	= 0^00-24
25	6	•	•	= 0^00-7^30, 8^15-24; ⊔° 0^00-9
26	6	•	•	= 0^00-24
27	6	•	•	= 0^00-24
28	7	1.7	•	⊽° 16^45-17^05 •° 22^05-24; = 0^00-6^30
29	6	5.9	•	•° 0^00-0^20 ... 2^40 •° 15^35-16^50 •° -24; = 10^40-13^30
30	7	13.8	•	•0-1 0^00-3^30 *' 4^40-5^20 •° 8^10-10^25 *' -11^05 *0-1 13^20 ... 16^15 *' 16^05-10 *° 16^35-17^15 *' -17^30 *° -18^10 *' 18^30-40 *2 21^20-40 *2 -22^05 *' -22^10 *° 22^50-23^15 *0-2 -24
31				
Σ	—	64.2	—	UWAGI

Grudzień - Décembre

1	8	0.5	•	*° ⊽ 0^00-20 *' 1^15-35 *0-1 ⊽ 2^05, 3^15 *° 4^05-20 *0-2 6^45-9^08 *° 16^15-17^15
2	8	•	2	
3	7	•	2	
4	6	•	1	= 2^30-15^30
5	6	•	•	= 7^25-13^40, 15^30-24
6	7	•	•	= 0^00-9^30, 13^20-24
7	7	•	•	= 0^00-8^30, 15^30-24; ⊔° 3-11
8	6	•	•	= 0^00-22^30
9	7	2.1	•	*° 13^05-14^40; = 3^30-5^30, 14^40-24
10	7	0.9	•	•° 0^36-2^40 *° -3^35 *° ⊽ 7^25-8^10, 16^20-40; ≫ 0^30-4^40; = 0^00-3^50
11	7	1.1	•	*° ⊽ 6^05-20, 6^45-7^10, 11^04-25, 12^40-14^20 •° ... 15^15 •' 22^25-40 •° 23^35 ... 24; ⊽° 0^30-1^35
12	7	0.2	•	•° 0^00-6^10 ... 8^15, 14^40 ... 17^25-18^20, 23^10 ... 24; = 18^20-24
13	4	5.7	•	•° 0^00-1^35, 11^35-13^45 *° -14^35 *° -14^50 *1-0 -16^35 *° -19^40; = 0^00-14^35 ≡° -16^40 = -24
14	6	0.0	•	*° ⊽ 12^20-35; = 0^00-2^30, 6^30-22^30
15	5	0.9	•	*° 7^35-10^20 *' -11^20 *° -14^40; = 6^30-17^30; ⊽° 3^30-4^20
16	4	1.9	1	•° 12^05 ... 13^40 *° -14^15, 23^10-24
17	4	13.8	pł.	*° 0^00-2^35, 4^20-5^05 *' -5^30 *° -10^20 *0-1 ... 24; = 2^35-24
18	5	6.7	18	*' 0^00-17^15 *2-0 ⊽ -22^35 *° -24; = 0^00-24
19	5	•	28	*° 0^00-3^35, 5^05-6^40; = 0^00-3^35, 6^40-24
20	5	•	25	= 0^00-7^20, 9^45-24
21	5	0.2	25	= 0^00-24
22	8	0.0	20	*° 0^35 ... 6^30 *° ⊽ -7^25; = 0^00-9^40, 19^20-24
23	5	•	16	= 0^00-9^50 ≡° -11^45 = -13^20, 15^35-24
24	6	0.2	14	*° 11^15-12^45, 15^10; = 0^00-3^35, 9^25-24
25	7	0.0	13	*° 16^15 ... 20^20; = 0^00-3^30, 6^35-11^30, 19^30-24
26	6	0.0	13	*° 9^35 ... 13^25; = 0^00-20, 8^30, 9^35, 17^20-24
27	5	0.2	13	*° 18^20-24; = 0^00-24
28	5	0.0	13	*° 0^00-6^20, 10^35-12^40; = 0^00-18^30
29	5	1.8	13	*° 6^25-21^40; = 21^40-24
30	7	0.3	16	*° ⊽ 13^20-14^10, 17^35-19^25; = 0^00-10^30
31	7	0.0	17	*° 0^10 ... 2^40, 9^20-11^25; = 7^20-9^20, 16^10-24
Σ	—	36.5	—	UWAGI

Suwałki $\varphi = 54°06'$ $\lambda = 22°57'$ Styczeń - Janvier 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA t I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	81.0	82.0	81.9	81.6	0.5	1.9	0.6	0.9	2.1	-0.1	100	82	79	87	0.0	1.3	1.4	0.9	10 ≡	10	6	SSW 6	SSW 8	SW 10
2	81.6	83.1	88.1	84.3	-0.5	-0.3	-2.6	-1.5	0.7	-2.7	84	94	89	89	1.0	0.4	0.6	0.7	10	10 ✱	10 ✱	WSW 7	WSW 8	WNW 7
3	88.4	92.6	99.8	93.6	-3.1	0.3	0.3	-0.6	1.1	-3.5	90	94	90	91	0.5	0.3	0.6	0.5	10 ✱	4 ⊙	10	WNW 6	NW 4	NW 3
4	102.5	102.0	98.3	100.9	-0.8	-2.4	-1.2	-1.4	1.1	-3.2	87	93	97	92	0.7	0.3	0.2	0.4	10	10	10 ,	W 7	WSW 9	WNW 5
5	96.9	95.1	90.2	94.1	0.2	0.2	-0.4	-0.1	0.6	-1.2	98	100	90	96	0.1	0.0	0.6	0.2	10 ,	10 ,	10	WSW 4	WSW 5	WSW 7
6	84.4	83.9	81.3	83.2	-2.6	-1.3	-1.1	-1.5	-0.4	-3.5	93	95	95	94	0.3	0.3	0.3	0.3	10 ✱	10 ,	10 ✱	WSW 8	SW 6	SW 6
7	86.3	92.6	101.1	93.3	1.1	0.5	-1.4	-0.3	1.5	-1.5	94	94	78	89	0.4	0.3	1.2	0.6	10	10 ✱	10	WNW 5	NW 5	NW 3
8	102.8	101.8	102.2	102.3	-3.9	-1.4	-0.2	-1.4	0.0	-5.4	94	92	98	95	0.3	0.4	0.1	0.3	5	10	10	SW 5	SSW 7	SW 3
9	100.7	98.6	95.4	98.2	-0.2	0.4	-2.9	-1.4	0.8	-2.9	98	100	84	94	0.1	0.0	0.8	0.3	10	10 ≡	0	SW 4	SSW 4	S 7
10	91.9	90.3	87.7	90.0	-4.3	-2.7	-5.3	-4.4	-2.2	-7.0	84	78	87	83	0.7	1.1	0.5	0.8	10	10	5	S 5	S 5	S 5
11	84.6	85.5	81.5	83.9	-1.9	0.7	2.3	0.8	2.5	-5.8	87	81	77	82	0.7	1.2	1.7	1.2	10	3 ⊙	10	SSW 7	S 4	S 8
12	82.5	83.1	80.0	81.9	1.7	2.3	1.1	1.6	2.6	1.1	94	95	100	96	0.4	0.4	0.0	0.3	10	10 ●	10 ≡	S 7	SSW 5	S 5
13	68.8	67.7	72.3	69.6	0.9	1.9	1.3	1.4	2.5	0.4	92	93	91	92	0.5	0.5	0.6	0.5	10	9	8	SSE 8	SSW 8	S 8
14	75.5	76.8	79.8	77.4	-0.6	1.5	0.9	0.7	2.3	-0.8	92	83	87	87	0.4	1.1	0.9	0.8	6	10	10	SSW 7	SSW 5	SW 7
15	82.2	86.5	92.2	87.0	0.4	1.5	0.7	0.8	2.1	0.4	96	92	94	94	0.3	0.5	0.4	0.4	10 ✱	9 ●✱	6	SW 6	WSW 5	SW 4
16	96.0	97.8	95.8	96.5	1.3	1.3	0.1	0.7	1.7	0.1	92	87	88	89	0.5	0.9	0.8	0.7	10	10	10	WSW 5	SW 5	SSW 6
17	91.8	92.0	94.4	92.7	0.4	0.5	1.1	0.8	1.4	-0.4	80	96	87	88	1.3	0.2	0.9	0.8	10	10 ✱	10	SSW 7	SW 7	SW 6
18	93.3	92.0	90.7	92.0	-0.7	-0.1	-0.5	-0.4	1.3	-1.8	85	84	86	85	0.8	1.0	0.9	0.9	9	10	9	S 5	SSW 4	SSW 4
19	92.6	93.3	90.7	92.2	1.3	1.4	0.7	1.0	1.6	-0.6	94	96	98	96	0.4	0.3	0.1	0.3	10	10	10	WSW 5	SW 5	SSW 7
20	83.1	82.4	90.6	85.4	2.5	2.5	1.9	2.2	3.0	0.7	89	88	87	88	0.8	0.9	0.9	0.9	6	10	10	SW 7	WSW 10	W 6
21	90.3	91.6	94.5	92.1	1.5	3.0	0.9	1.6	3.5	0.8	87	83	94	88	0.9	1.3	0.4	0.9	10 ●✱	9	10	SW 10	W 10	SW 3
22	89.1	85.0	81.2	85.1	2.5	4.0	3.5	3.4	4.6	0.3	100	98	95	98	0.0	0.1	0.4	0.2	10 ≡	10 ,	9	SSW 3	SSW 5	SSW 7
23	84.5	87.0	89.8	87.1	1.7	2.9	1.9	2.1	3.6	1.2	83	67	80	77	1.1	2.4	1.4	1.6	8	4 ⊙	9	SSW 10	WSW 10	SSW 11
24	90.0	90.8	91.3	90.7	1.2	2.7	0.7	1.3	2.8	0.4	92	77	94	88	0.5	1.7	0.4	0.9	10 ●	6 ⊙	10	SW 6	WSW 6	SW 4
25	91.2	89.2	87.3	89.2	0.1	0.8	-0.5	0.0	1.0	-1.0	82	77	90	83	1.2	1.5	0.6	1.1	10	10	10 ✱	WSW 1	SE 4	SSE 6
26	90.7	92.9	92.5	92.0	-2.3	-1.3	-2.5	-2.2	-0.2	-3.1	89	80	95	88	0.6	1.1	0.3	0.7	3	6 ⊙	8	NNE 3	NW 5	WSW 3
27	89.6	88.3	86.3	88.1	-3.4	-1.1	-0.7	-1.5	-0.4	-3.9	94	93	99	95	0.3	0.4	0.0	0.2	8	10 ✱	10 ≡	SW 3	SW 3	SW 2
28	84.1	84.7	92.4	87.1	-0.7	-5.1	-7.5	-5.2	-0.6	-7.5	93	88	84	88	0.4	0.5	0.5	0.5	10	10 ✱	0 ↔	WNW 5	NNE 8	NNE 10
29	101.3	106.7	112.9	107.0	-8.9	-10.3	-13.5	-11.6	-7.5	-13.7	83	77	84	81	0.5	0.6	0.4	0.5	10 ✱	6 ⊙	0	NNE 8	NE 8	NE 7
30	116.7	118.6	120.0	118.4	-18.1	-13.1	-17.1	-16.4	-12.5	-18.1	90	76	80	82	0.2	0.5	0.3	0.3	0	0 ⊙	0	NE 1	NE 1	C 0
31	119.0	118.1	114.8	117.3	-19.1	-12.5	-15.9	-15.8	-10.4	-19.6	89	77	91	86	0.1	0.5	0.2	0.3	0	0 ⊙	0	NE 1	C 0	NNE 1
M	90.8	91.4	92.2	91.4	-1.7	-0.7	-1.8	-1.5	0.3	-3.3	90	87	89	89	0.5	0.7	0.6	0.6	8.5	8.3	7.7	5.5	5.8	5.5

Luty - Février

1	107.6	101.5	98.5	102.5	-18.0	-8.6	-8.5	-10.9	-8.3	-18.4	90	77	89	85	0.2	0.7	0.3	0.4	0	1 ⊙	10	E 2	SE 7	SE 6
2	96.3	96.8	100.4	97.8	-7.9	-5.1	-8.3	-7.4	-4.9	-10.4	87	78	89	85	0.4	0.9	0.3	0.5	10	10	7	SSE 5	SSE 6	S 2
3	102.9	104.0	103.7	103.5	-10.1	-5.1	-11.3	-9.4	-4.4	-12.2	94	80	93	89	0.2	0.8	0.2	0.4	10	6 ⊙	10	C 0	S 2	C 0
4	97.9	93.3	93.7	95.0	-10.3	-4.5	-1.9	-4.6	-1.7	-13.7	97	98	92	96	0.1	0.1	0.4	0.2	10	10	10	S 1	SSW 5	SW 5
5	94.0	89.4	82.3	88.6	-1.9	-2.5	-2.3	-2.2	-0.6	-3.9	92	98	96	95	0.4	0.1	0.3	0.3	10	10	10 ✱	SW 4	S 5	SE 8
6	79.4	81.1	90.8	83.8	0.3	0.7	-1.1	-0.3	1.1	-2.6	94	96	97	96	0.3	0.2	0.2	0.2	10 ●	10 ✱	10 ✱	S 5	WNW 2	NW 8
7	95.9	97.1	96.0	96.3	-1.5	1.4	-4.9	-2.5	1.6	-5.6	94	74	88	85	0.3	1.8	0.5	0.9	9	8 ⊙	0	WNW 2	WSW 4	SW 4
8	93.9	93.2	93.3	93.5	-5.1	-0.4	-1.7	-2.2	0.0	-5.8	88	76	94	86	0.5	1.4	0.3	0.7	8	10	10 ✱	S 6	SSE 9	S 6
9	95.2	97.8	102.8	98.6	-0.4	0.6	0.3	0.2	1.1	-1.7	100	100	94	98	0.0	0.0	0.3	0.1	10 ≡	10 ≡	9	S 3	S 2	S 2
10	108.0	107.8	105.1	107.0	-4.5	-1.3	-0.7	-1.8	0.5	-6.9	93	82	89	88	0.3	1.0	0.6	0.6	4	8 ⊙	10 ✱	C 0	SSW 4	SSW 7
11	97.7	93.4	94.9	95.3	-0.1	0.3	0.5	0.3	1.1	-0.7	98	98	86	94	0.2	0.1	0.8	0.4	10 ,	10 ✱	10 ✱	SSW 10	SW 7	SW 8
12	87.6	69.3	52.8	69.9	-2.4	-1.3	1.7	-0.1	2.1	-3.0	93	97	94	95	0.3	0.2	0.4	0.3	9	10 ✱	10	S 8	SSW 15	WSW 15
13	51.9	55.7	62.3	56.6	-0.7	0.1	-4.3	-2.3	1.9	-4.5	93	78	79	83	0.4	1.4	0.9	0.9	10 ✱	10	0	WSW 11	WSW 12	SW 5
14	67.6	70.9	75.6	71.4	-8.7	-2.1	-5.3	-5.4	-1.1	-9.6	95	75	82	84	0.2	1.3	0.7	0.7	1	5	10	C 0	W 1	NW 5
15	80.8	83.4	89.7	84.6	-6.1	-5.9	-9.7	-7.8	-3.4	-9.7	86	89	81	85	0.5	0.4	0.5	0.5	10 ✱	10 ✱	0	NNW 7	NNW 7	NW 5
16	83.6	68.0	56.5	69.4	-9.1	-5.9	1.3	-3.1	2.1	-14.7	92	92	87	90	0.3	0.3	0.9	0.5	9	10 ✱	10 ●	SSW 7	S 14	WSW 10
17	50.5	55.6	61.6	55.9	0.2	-0.9	-2.9	-1.6	1.4	-3.1	96	87	95	93	0.3	0.7	0.2	0.4	10 ✱	9	10 ✱	SW 10	W 9	SW 13
18	70.4	78.0	89.0	79.1	-4.1	-4.1	-5.3	-4.7	-2.5	-5.3	96	91	87	91	0.2	0.4	0.5	0.4	10 ✱	10 ✱	10 ✱	NW 12	NW 10	NNW 10
19	92.8	93.7	93.4	93.3	-9.5	-3.4	-7.1	-6.8	-2.1	-13.6	91	79	91	87	0.3	1.0	0.3	0.5	4 ⊙	4 ⊙	10	WNW 2	W 1	C 0
20	89.1	85.7	83.8	86.2	-1.3	1.3	0.9	0.4	2.0	-7.4	97	94	94	95	0.2	0.4	0.4	0.3	10 ,	10 ✱	10 ✱	SW 4	SW 6	NW 8
21	89.9	96.4	106.2	97.5	-2.3	-4.7	-5.7	-4.6	1.1	-5.8	91	88	87	89	0.5	0.5	0.5	0.5	10 ✱	10 ✱	10 ✱	NNW 8	N 10	NNE 7
22	112.4	113.1	113.6	113.0	-6.7	-6.5	-10.7	-8.6	-5.6	-10.8	88	89	87	88	0.4	0.4	0.4	0.4	10 ✱	10 ✱	0	NNE 6	N 6	N 3
23	108.0	106.5	104.9	106.5	-8.7	-7.3	-7.3	-7.6	-6.6	-11.7	86	82	82	83	0.4	0.6	0.6	0.5	10 ✱	9	10	N 7	N 9	NNE 3
24	102.0	103.2	107.0	104.1	-6.9	-6.5	-7.6	-7.2	-5.7	-8.3	91	86	82	86	0.3	0.5	0.6	0.5	10 ✱	10 ✱	10 ✱	NNE 8	NE 10	E 10
25	110.3	110.6	109.2	110.0	-10.8	-5.7	-4.1	-6.2	-3.9	-11.9	90	72	80	81	0.3	1.1	0.9	0.8	10 ✱	2 ⊙	5	ENE 4	ENE 7	ENE 8
26	107.3	106.5	105.7	106.5	-5.1	-4.1	-5.1	-4.8	-2.8	-5.2	83	80	80	81	0.7	0.9	0.8	0.8	10	10 ✱	10	E 6	E 5	E 4
27	104.8	103.7	102.2	103.6	-6.6	-4.4	-10.8	-8.2	-4.2	-10.8	83	74	87	81	0.6	1.1	0.4	0.7	10	4 ⊙	0	C 0	E 3	NE 1
28	99.1	96.5	93.6	96.4	-16.9	-6.8	-14.7	-13.3	-6.5	-18.6	90	72	91	84	0.2	1.0	0.2	0.5	9	0 ⊙	0	C 0	E 1	C 0
29																								
30																								
31																								
M	92.0	91.2	91.7	91.6	-5.9	-5.3	-4.9	-4.8	-1.7	-8.4	92	85	88	88	0.3	0.7	0.5	0.5	8.7	8.1	7.5	4.9	6.4	5.8

Suwałki $H_r = 165m$ $H_b = 169.6m$ $h_w = 13m$ Styczeń - Janvier 1962

DZIEŃ	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7.	0.1	8	*°23 10-24; ≡z-a 0 00-8 45 = -10 30; ≫ a, p... np
2	5	1.3	9	*°0 00-1 25, 8 20-14 45 *1-0 16 35-21 20 *° np; = 8 10-14 25; ≫ na
3	7	0.3	11	*°5 35-6 45 *0-1 7 15-11 40; = 9 30-11 30
4	7	0.2	12	♎°19 10-20 05 ♈°-24
5	5	0.8	10	♈°0 00-7 30 ♋°-16 45; = 16 45-24
6	5	7.7	11	♎°4 10-6 20 *°-8 35 ♈°-14 50 ♎°-15 20 *0-1-22 35; = na, np; ~°8 35-14 50
7	7	0.0	14	*°2 30-3 10, 11 37-12 35; = 0 00-3 15
8	7	.	13	= 14 15-24
9	3	0.0	11	♋°8 10-11 50; =, ≡1-0 0 00-24
10	6	.	10	= 9 14-13 30
11	6	0.1	10	•°21 55... 23 15; = 6 15-13 30
12	6	2.6	6	•°0 35-1 56, 8 35... 14 30 •0-1-18 35; = 8 30-20 20 ≡°-24
13	7	2.5	4	*1-0 7 35-11 40 ♈° 14 40-15 10; ≡°; = 0 00-6 20; ≫ a, p, np
14	7	0.0	3	= 10 25-12 30, 21 45-24
15	6	1.1	1	*°5 40-8 40 ♈°9 30-11 45 ♈°-12 40 ♈°13 40-50; = a; ϖ°17 35-18 15
16	7	0.0	2	♈°6 40-7 30 ♈°-8 10; = 6 30-13 10; ω°17 40-18 30 ϖ°-21 00
17	5	3.0	pż.	*1-0 8 03-15 35 ♋°15 50-16 35; = 15 35-19 20; ≫ na, a
18	6	.	3	= 7 10-24
19	5	2.9	3	= 0 00-20 40; ≡1-0-24
20	6	3.4	pż.	•°2 10-3 40 9 05 19 10 *'11 35-45 ♈°19 20-42; ≡°; = na = a-p; ≫ 8 35-19 10
21	7	0.0	pż.	♈°1 08-20 ♈°6 30-7 20; = 23 30-24; ≫ 5 40-8 30, 9 15-13 50
22	5	1.2	pż.	♋°11 40-12 20... 13 35 •°18 20-19 40; =, ≡1-0 0 00-23 30
23	2	0.6	.	♈°23 40-24; ≫ 2 20-15 50 20 15-24
24	7	0.0	.	♈°3 35... 9 45 ♈°13 35-15 25, 16 45-17 35; = 7 30-8 00; ≫ 0 00-3 40
25	7	0.3	.	♈°19 10-20 05 *°-24
26	8	0.4	1	*°0 00-2 45 8 10 9 15 ♈'-11 10 ♈°19 45-20 20
27	6	0.5	2	*°8 10-20 15, 21 30-23 10; = ≡°6 20-24
28	5	0.5	2	*°3 30, 5 10 ♈°; *1-0 7 15-13 20 *1-0 13 25-20 10 ↔'-21 20; ⊥'13 50-23 45; = na; ≫ p-np
29	7	0.0	4	♈°4 04-7 20 *0-1-11 10 ♈°12 50-13 40, 14 05-15 10 *°23 45-24
30	7	.	5	*°0 00-35
31	7	0.0	5	*°8 30-10 35 ↔°-11 45; = 16 05-18 45
Σ	–	29.5	—	UWAGI: W ciągu całego roku wartości ciśnienia powietrza są za niskie przeciętnie o ok 0,3 mb.

Luty - Février

1	8	0.0	5	*°17 45-18 20
2	6	0.0	5	*°8 30-9 15... 10 40; = 8 10-15 30
3	6	.	4	= 6 10-15 45 ≡'-20 25 = -24
4	6	0.1	3	*°13 30-16 25; = 0 00-6 50 ≡1-0-9 45 = -24
5	5	2.4	3	*°19 40-24, ⊥°20 35-24; =, ≡°0 00-15 30 ≫ 15 36-19 20
6	6	1.5	10	*0-1 0 00-5 15 •°6 10-7 20 *°-14 50, 15 05 18 05-21 40, ⊥° 0 00-3 45
7	7	.	11	
8	7	3.4	11	*°17 30-24; = 8 20-11 00
9	3	1.7	12	*°0 00-2 35 •°7 15-45 *°-9 45 *1-0 p, np, ≡0-1; = 1 00-24
10	8	0.4	13	*°0 00-1 05, 18 45-19 35, 20 05... 21 40; = 7 10-8 15 ≡z-8 45 = np
11	5	5.8	11	*°0 10-2 10 ♋1-0-7 40 ♈°-8 50 •°11 10-16 35 20 20-24; = na - p; ≫ na, a ~°a
12	3	10.4	13	*°0 00-1 50 *'9 30-17 35 *°-18 35 •0-1-20 15 ⊥'9 45-18 35; ≫ - ≫ 7 20-24
13	8	0.0	16	*'0 10-1 35 *°4 10-5 15 ♈°6 15-7 05 ♈0-2 12 40-13 25 ⊥'4 40-5 45; ≫ - ≫ 0 00-14 20
14	6	0.0	16	= 7 20-20 10 ϖ19 30-20 28
15	6	0.0	16	♈°1 04-45 2 35-5 10 *0-1-5 10 ♈°-16 10, 16 17-17 10 ⊥1-0 13 45-18 30; ≫ p
16	5	7.9	18	*0-1 9 20-18 45 ♈°20 05-40 ♈1-0-24; ⊥'9 50-18 45; ≫ a - np
17	7	10.3	21	♈0-1 *0-1 0 00... 12 10 ♈0-1 13 20-16 20 *'-24; ⊥'16 30-24; ≫ na... a, 18 10-24
18	3	1.6	35	*'0 00-13 30 *°-21 30 ⊥1-0 0 00-22 40; ≫ 0 00-21 30
19	6	0.8	45	*°20 38... 21 20, 22 05-24; = 6 19-13 10
20	6	2.0	46	*°0 00-6 10 ♋°-8 30 ♋°-10 40 •°... 12 15 *°-13 30 •°-20 15 *°-21 30 ♈°-23 10 ♈°-24
21	5	0.2	40	♈°♈°0 00-3 00 *0-1-14 45 ♈°16 45-17 36 *°-19 30, 20 26... 24; ⊥1-0 a - p, p; ≫ a - p
22	6	1.4	37	*°0 00... 9 38 ♈°; *°11 05... 13 16 ♈°14 10-20 ↔'14 40-15 15 ♈°16 05-25; = a - np
23	8	0.2	38	*°5 20-8 40 23 10-24; = na, ϖ'0 15-1 25
24	6	0.2	38	*°0 00... 12 15 *0-1-19 45 24, ⊥°15 00-24; ≫ a - p, p - np
25	6	0.0	38	*°0 00-1 45, 6 15-7 50; ⊥°0 00-1 45; = 8 15-22 40
26	6	0.3	38	*°7 50-13 00... 14 50
27	7	.	38	
28	6	0.1	36	*°7 35... 8 10-9 25 ↔'-9 40; = 3 20-24; V°na-9 00
29				
30				
31				
Σ	–	50.7	—	UWAGI:

Suwałki φ = 54°06' λ = 22°57' Marzec-Mars 1962

Dni	Ciśnienie P = 900 + I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność wzgl. U I	II	III	Dies	Niedosyt wilgotności I	II	III	Dies	Zachmurzenie i pogoda N.w I	II	III	Kierunek i prędkość wiatru D.v I	II	III
1	91.5	91.0	89.9	90.8	-17.9	-6.0	-11.1	-11.5	-4.7	-19.2	90	74	93	86	0.2	1.0	0.2	0.5	0 ⊙	5 ⊙	0	C 0	E 3	C 0
2	87.1	85.4	84.2	85.6	-16.4	-6.0	-12.0	-11.6	-4.4	-18.2	95	76	93	88	0.1	0.9	0.2	0.4	0 ⊙	5 ⊙	10	C 0	W 2	C 0
3	84.0	84.5	85.4	84.6	-8.4	-2.7	-2.7	-4.1	-2.2	-12.0	89	78	78	82	0.3	1.1	1.1	0.8	10	10	10	C 0	SW 4	SSW 2
4	82.3	77.9	75.7	78.6	-4.1	-1.1	-1.2	-1.9	0.6	-6.0	94	93	97	95	0.3	0.4	0.2	0.3	10 *	10 *	10 *	SSE 4	ESE 3	C 0
5	78.2	80.8	80.6	79.9	-5.5	-3.0	-3.0	-3.1	-1.0	-4.3	94	90	95	93	0.3	0.5	0.3	0.4	10	10 *	10	N 4	NE 4	NE 7
6	72.0	70.0	82.6	74.9	0.3	0.9	-3.5	-1.4	1.5	-3.5	98	98	90	95	0.1	0.1	0.5	0.2	10 ●	10 ●=	10	E 4	E 2	W 6
7	94.1	97.6	101.8	97.8	-6.2	-2.9	-7.6	-6.1	-2.6	-7.6	92	77	90	86	0.3	1.1	0.3	0.6	8 *	7 ⊙	0	SW 2	NW 6	NW 1
8	103.9	102.6	98.9	101.8	-12.9	-2.0	-2.8	-5.1	-1.5	-13.1	96	75	84	85	0.1	1.4	0.8	0.8	0 ⊙	6 ⊙	10 *	C 0	SW 5	NW 10
9	106.6	108.5	107.1	107.4	-7.0	-3.9	-9.3	-7.4	-2.8	-10.3	93	66	82	80	0.2	1.5	0.5	0.7	10	0 ⊙	0	NE 4	NE 3	ESE 5
10	101.7	97.5	93.8	97.7	-7.1	-1.1	-2.0	-3.0	0.8	-10.2	74	61	64	66	0.9	2.2	1.9	1.7	9 ⊙	9	10	SE 10	SE 12	SSE 11
11	88.6	85.8	84.5	86.3	-2.1	1.2	1.4	0.5	1.9	-2.4	92	81	94	89	0.4	1.3	0.4	0.7	10	10	10	SSE 10	S 7	S 1
12	82.2	79.5	75.1	78.9	0.9	1.1	0.4	0.7	2.7	0.3	98	98	92	96	0.1	0.1	0.5	0.2	10	10 ●	10	S 2	S 2	S 4
13	69.0	71.0	78.3	72.8	-0.9	-5.6	-7.9	-5.6	0.5	-7.9	96	92	87	92	0.2	0.3	0.4	0.3	10 *	10 *	10 *	NE 2	NNW 7	WNW 9
14	85.4	90.2	95.7	90.4	-6.5	-4.0	-9.3	-7.3	-3.3	-9.4	91	70	95	85	0.3	1.3	0.2	0.6	10 *	8 ⊙	0	W 4	W 6	SW 4
15	99.3	101.1	102.9	101.1	-13.1	-4.9	-6.7	-7.8	-3.1	-14.3	92	73	75	80	0.2	1.1	0.9	0.7	6	9	10	SW 2	NW 3	NNE 1
16	104.0	103.7	99.0	102.2	-7.3	-6.6	-6.9	-6.9	-5.8	-8.5	68	67	61	65	1.1	1.2	1.4	1.2	10	10	10	NNE 4	NE 6	N 11
17	92.8	89.0	88.5	90.1	-7.3	-3.5	-4.7	-5.0	-2.4	-7.6	90	78	69	79	0.3	1.0	1.3	0.9	10 *	10	10	N 14	NE 12	N 12
18	90.0	91.8	94.2	92.0	-7.9	-2.5	-4.9	-5.0	-0.6	-8.4	78	82	73	78	0.7	0.9	1.1	0.9	4 ⊙	1 ⊙	9	N 9	NW 8	NW 6
19	97.0	98.0	98.8	97.9	-7.7	-2.6	-5.9	-5.5	-0.7	-10.1	90	73	76	80	0.3	1.4	0.9	0.9	9	4 ⊙	4	SW 2	SW 3	C 0
20	99.5	100.3	101.1	100.3	-11.2	-0.8	-7.3	-6.6	0.1	-12.6	90	58	71	73	0.3	2.4	1.0	1.2	1 ⊙	4 ⊙	0	C 0	SSW 8	C 0
21	100.3	98.9	97.3	98.8	-12.1	-1.5	-7.9	-7.4	-0.4	-13.7	93	52	84	76	0.2	2.7	0.5	1.1	8 ⊙	8 ⊙	0	C 0	SSW 3	C 0
22	95.0	93.1	91.4	93.2	-11.5	-2.6	-5.9	-6.5	-1.4	-12.0	93	75	81	83	0.2	1.3	0.7	0.7	4 ⊙	6 ⊙	9	SE 1	E 4	E 3
23	89.2	88.9	89.8	89.3	-5.4	-0.8	-1.7	-2.4	-0.4	-6.3	90	85	90	88	0.4	0.9	0.6	0.6	10 *	9	10 *	NE 3	NE 4	NE 3
24	91.5	92.9	95.9	93.4	-4.3	-1.3	-4.5	-3.6	-0.8	-4.8	82	64	74	73	0.8	2.0	1.1	1.3	10 *	9 ⊙	0	N 2	N 4	WNW 2
25	99.0	100.0	99.1	99.4	-7.9	-1.2	-5.1	-4.8	0.1	-9.1	87	56	90	78	0.4	2.4	0.4	1.1	1 ⊙	1 ⊙	0	SW 2	SW 2	SW 2
26	98.1	97.2	96.0	97.1	-8.5	0.3	-4.9	-4.5	1.6	-10.3	92	61	78	77	0.3	2.4	0.9	1.2	8	5 ⊙	0	C 0	SW 5	SW 2
27	94.0	91.7	89.0	91.6	-7.5	-0.3	-5.7	-5.8	0.3	-9.4	90	63	71	75	0.3	2.3	1.3	1.3	0 ⊙	1 ⊙	0	SW 2	SE 10	SE 3
28	86.1	84.8	84.8	85.2	-7.4	1.0	-2.5	-2.8	1.6	-8.3	82	57	78	72	0.6	2.9	1.1	1.5	9 ⊙	4 ⊙	5	E 3	SE 7	SE 2
29	83.9	84.4	85.1	84.5	-2.8	0.5	-0.7	-0.9	1.7	-3.2	91	75	97	88	0.5	1.6	0.2	0.8	10	10	10	SE 2	C 0	C 0
30	82.0	78.7	78.4	79.0	-1.9	2.1	1.0	0.6	2.9	-3.3	90	87	100	92	0.5	0.9	0.0	0.5	2 ⊙	10 ●	10 =	SE 5	SE 6	SE 3
31	72.8	69.7	73.4	72.0	1.2	3.3	2.1	2.2	5.3	0.8	100	98	91	96	0.0	0.1	0.6	0.2	10 =	10 ●	0	SE 4	SE 6	SW 5
M	90.4	89.9	90.2	90.2	-6.9	-1.8	-4.5	-4.4	-0.5	-8.5	90	75	84	83	0.4	1.3	0.7	0.8	7.1	7.1	6.0	3.3	5.1	3.7

Kwiecień - Avril

1	79.7	82.9	84.2	82.3	0.9	3.0	0.5	1.2	4.4	-0.4	94	90	98	94	0.4	0.8	0.1	0.4	10	9	10	WSW 3	WSW 5	WSW 3
2	83.7	85.3	86.9	85.3	0.7	4.7	2.1	2.4	5.3	-0.9	88	67	87	81	0.7	2.8	0.9	1.5	10	8 ⊙	10	SW 4	SW 9	SW 5
3	89.7	89.3	87.2	88.7	0.9	2.9	5.5	3.7	6.5	-0.1	90	95	78	88	0.6	0.4	1.9	1.0	10	10 ●	0	SW 5	SSW 7	S 8
4	84.3	81.4	78.6	81.4	3.0	9.7	4.6	5.5	11.0	1.9	90	56	85	77	0.8	5.3	1.3	2.5	8 ⊙	8 ⊙	9	S 8	SSE 10	S 5
5	74.1	71.8	71.6	72.5	5.9	9.1	4.6	6.0	10.8	3.2	80	65	90	78	1.9	4.1	0.8	2.3	8	9	10 ●	SSE 5	SE 10	SE 9
6	73.1	77.1	81.1	77.1	4.3	7.7	5.3	5.6	8.6	3.4	100	91	97	96	0.0	0.9	0.3	0.4	10 =	10	10	SE 2	SE 5	SE 1
7	80.1	79.4	83.3	80.9	1.0	3.2	0.5	1.3	5.3	0.4	100	81	82	88	0.0	1.5	1.1	0.9	10 ●	10	3	NW 9	WNW 10	WNW 7
8	83.5	83.0	84.9	83.8	0.0	3.3	6.3	4.0	6.7	-1.6	90	98	95	94	0.6	0.1	0.4	0.4	8	10	10	SSW 5	SSW 7	SSW 6
9	86.9	90.3	95.7	90.3	5.3	11.4	7.7	8.0	13.2	5.2	95	69	68	77	0.4	4.2	3.4	2.7	10 ●	9	10	S 5	SSW 7	SW 2
10	96.8	98.2	101.3	98.8	4.3	11.1	6.3	7.0	12.3	2.3	87	57	86	77	1.1	5.7	1.2	2.7	9	9	6	C 0	C 0	C 0
11	102.4	102.0	100.7	101.7	4.1	12.7	8.1	8.2	13.8	1.5	83	48	76	69	1.4	7.7	2.5	3.9	5	4	10	C 0	N 2	NNE 3
12	98.2	96.0	94.1	96.1	5.0	15.1	8.7	9.4	16.4	2.9	97	59	90	82	0.3	7.0	1.0	2.8	6 ⊙	8	6	C 0	SE 4	C 0
13	93.0	93.3	92.1	92.8	6.1	12.1	6.1	7.6	12.3	5.8	98	56	83	79	0.1	6.2	1.6	2.6	8	10	10 ●	SSW 2	NW 1	N 5
14	90.7	94.0	100.3	95.0	5.5	5.9	5.1	5.4	7.2	4.2	98	98	95	97	0.1	0.2	0.4	0.2	10 ●	10 ●	10 ●	N 3	N 5	NNW 4
15	105.0	107.1	108.2	106.8	4.5	6.4	5.9	5.7	6.9	4.4	98	94	94	95	0.1	0.6	0.6	0.4	10 ●	10	10	NNE 7	NE 9	NE 9
16	108.4	108.2	107.6	108.1	5.1	8.2	7.5	7.1	11.8	5.0	98	83	86	89	0.2	1.8	1.5	1.2	10 ●	9	2	ENE 7	E 6	E 7
17	108.0	106.9	105.2	106.7	5.1	19.1	11.1	11.6	19.3	4.3	98	56	81	78	0.2	9.8	2.4	4.1	10	3 ⊙	9	E 3	ESE 7	ESE 2
18	102.2	99.3	98.1	99.9	8.9	18.4	12.7	13.2	19.7	7.4	85	55	82	74	1.7	9.6	2.6	4.6	10	9	10	SE 5	SSE 9	S 3
19	96.8	96.4	96.1	96.4	9.4	19.3	12.7	13.5	20.2	7.7	89	49	85	74	1.3	11.4	2.3	5.0	10	9	9	S 2	SSE 4	C 0
20	96.2	97.1	98.0	97.1	9.8	21.9	15.0	15.4	22.7	6.8	97	45	86	76	0.3	14.3	2.4	5.7	8 ⊙	10 ⊙	5	C 0	N 4	NNE 3
21	99.4	99.2	99.5	99.4	12.1	24.1	16.9	17.5	25.0	10.1	91	43	76	70	1.2	17.1	4.6	7.6	9 ⊙	6 ⊙	7	NE 1	E 1	C 0
22	99.6	99.9	100.7	100.1	13.1	23.7	14.9	16.6	24.6	10.6	94	54	69	72	0.9	13.6	5.2	6.6	6 ⊙	9 ⊙	0	C 0	C 0	ENE 3
23	101.3	100.7	100.7	100.9	12.8	24.6	18.1	18.4	25.7	9.7	87	42	74	68	1.9	18.0	5.5	8.5	2 ⊙	5 ⊙	8	E 2	SE 4	C 0
24	105.4	107.1	108.0	106.9	10.7	16.9	12.1	13.0	18.2	9.7	76	52	66	65	3.1	9.2	4.8	5.7	1 ⊙	0 ⊙	0	NE 6	NE 7	NE 4
25	110.3	109.5	107.0	108.9	10.4	17.5	10.9	12.4	18.7	5.3	70	33	67	57	3.8	13.4	4.3	7.2	3 ⊙	1 ⊙	0	ENE 4	E 3	NE 1
26	102.9	97.2	91.3	97.1	9.9	12.7	11.9	11.6	17.3	5.1	68	82	87	79	3.9	2.6	1.8	2.8	2 ⊙	10	6	SSW 3	SSE 8	SSW 2
27	86.3	84.0	81.3	83.9	7.3	7.9	4.2	5.9	11.9	3.1	87	89	95	90	1.3	1.2	0.4	1.0	9	10 ●	10 ●	WSW 3	WNW 3	WNW 9
28	78.9	78.5	79.3	78.9	4.3	6.3	3.9	4.6	8.9	2.6	82	78	92	84	1.5	2.1	0.7	1.4	10	9	10 ●	W 3	WNW 4	WNW 6
29	80.2	81.8	84.2	82.1	3.7	7.0	3.3	4.3	8.5	3.0	88	60	85	78	1.0	4.0	1.2	2.1	10	8 ⊙	10	WNW 6	W 7	WNW 2
30	85.6	87.7	90.5	87.9	1.7	4.8	1.4	2.3	5.7	0.8	83	56	81	73	1.1	3.8	1.3	2.1	9	10	4	NW 4	W 1	NW 3
31																								
M	92.8	92.8	93.2	92.9	5.9	11.7	7.8	8.3	13.3	4.1	89	67	84	80	1.1	6.0	2.0	3.0	8.0	8.1	7.1	3.6	5.3	3.7

Suwałki H_s=165m H_t=169,6m h_w=13m Marzec - Mars 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	7	•	36	=0^00-11^10
2	6	•	34	=4^20-24
3	6	0.3	32	*°7^20...40; =0^00-24
4	6	0.3	33	*°-1 2^40-7^40 *° 8^03-12^45, 18^10-24; =0^00-24
5	6	5.5	32	*°0^00-3^45, 7^05...2^42 ⚲°20^45-23^15 ⚲°-24; =0^00-24; ~° np
6	3	9.7	28	⚲°0^00-5^50 •°-15^35 ⚲°16^10-17^15; =, ≡°0^00-14^40; ~°0^00-9^00
7	7	0.2	24	⚲°6^20-8^35 9^15-11^15
8	7	0.6	21	⚲'14^10-15^20 ⚲°...21^20; =6^10-10^30; ≫20^15-21^10
9	7	•	22	
10	8	•	21	≫6^10-24
11	6	0.1	21	*°7^40...10^50 ⚲1-0 15^50-17^15 •°22^10...24; ≫0^00-7^30; =a-np
12	5	3.0	18	•°0^00...1^45 9^12-13^40 *°22^30-24; =na-np
13	5	2.4	20	*°-1 0^00-15^45, 16^15-24; ⊥° np; ≫np; =na-p
14	8	0.0	24	*°0^00-9^15 ⚲°13^45-14^57, 15^15-40; ⊥° na
15	7	•	24	⊠°19^40-23^45
16	8	0.2	24	*°23^40-24; ⊥° 23^40-24; ≫19^30-24
17	7	0.0	24	*°0^00-10^30...12^20; ⊥° 0^00-22^00; ≫-⚲ 0^00-4^40 ≫-24
18	9	0.2	24	⚲'14^40-15^50; ≫0^00-5^30, 8^05-10^20
19	8	•	24	≡°7^35-10^30
20	8	•	16	
21	7	•	12	
22	7	0.0	10	=6^20-9^20
23	7	0.0	8	*°5^20-8^50, 11^20...12^25, 15^45...17^10, 18^15-24
24	7	0.0	8	*°5^30...7^10; =18^30-20^45
25	7	•	7	=5^20-8^00, 20^10-24
26	6	•	7	=0^00-13^10
27	7	•	6	≫10^30-14^15
28	8	•	5	
29	7	•	5	=22^10-24
30	6	2.7	5	•°11^30-13^40 *°-14^25 *°-16^35 •°-19^20; =0^00-18^35 ≡1-0-24
31	5	7.0	3	•°0^15-1^35, 7^40-17^30 •°-18^15; ≡°-1 0^00-11^45 =-20^10
Σ	—	32.2	—	UWAGI

Kwiecień - Avril

1	7	0.0	3	•°3^35-5^40, 18^30-19^20; =1^10-5^30, 19^20-21^30
2	8	0.0	pł.	⚲'4^35-5^03 ⚲°-5^25-6^20; =na
3	6	0.4	pł.	⚲°5^45-6^05 ⚲°9^15-11^30 •°-14^35; =na-a
4	8	0.0	pł.	≫10^15-14^20
5	7	6.6	pł.	⚲°1^50-2^15, 10^43-50 p... •°19^25-24; ≫12^00-19^15
6	7	0.8	pł.	•°0^00-6^15; =3^40-6^30 ≡°-9^45 =21^30-24
7	8	4.2	•	•°3^40-4^15 •°-1 8^30 *1-0-11^15; ≫8^30-18^15; =0^00-11^15
8	5	4.5	•	*°7^40...8^30 *°-10^25 •°-11^25, 13^20-19^30, 22^40-24; =8^15-11^40 ≡°-12^35 =-24
9	8	0.0	•	•°0^00-7^15; =0^00-9^00
10	7	•	•	•°0^20...1^45
11	7	•	•	=0^00-4^15
12	7	3.6	•	▲'16^10-13 ⚲'16^10-17^20 ⚲°19^10-20^05; ⊠'14^45-17^15 NW-SE; =3^30-8^00
13	7	11.4	•	⚲°0^25-3^30, 13^15-14^25, 15^05-16^10, 19^20-21^35 •'-24; =0^00-9^00
14	6	1.6	•	•°0^00-12^20...13^35 •°19^15-24; =6^15-14^40, 18^25-24
15	7	0.0	•	•°0^00-1^45, 4^20-7^20, 7^40-9^45; ≫p, p-np; =, ≡°0^00-12^15
16	7	0.0	•	•°4^15-8^25; =3^30-8^25
17	7	•	•	=3^15-10^20
18	7	•	•	=7^08-8^00
19	7	•	•	⌓°1-9
20	7	•	•	=2^15-11^15; ⌓°2-11; ⊠°21^30-22^15 23^35-24
21	7	0.1	•	⚲21^15-20 22^15-20; ⊠°22^10-23^40 SE-NW; =5^20-8^00; ⌓°1-8; ⊠°na
22	7	•	•	(⊠)°12^40-14^35; =6^10-8^00; ⌓°1-9
23	7	•	•	⌓°2-9, 21-24
24	8	•	•	=2^30-6^40; ⌓°0-8
25	8	•	•	⌓°1-9^00
26	7	1.6	•	•°-1 10^25-12^35 ⚲°17^35-55 18^05-20; (⊠)°16^30-17^05 SSW-SSE; ⌓°1-8
27	6	2.1	•	•°11^02...17^10 •°-1 18^30-23^15...24; =4^40-9^10
28	8	0.1	•	•°0^00...45 ⚲°11^10...24
29	7	0.5	•	⚲°0^00-1^15, 1^25-2^20, 10^45...11^35 ▲°-11^42
30	8	•	•	
31				
Σ	—	37.5	—	UWAGI

Suwałki φ = 54°06' λ = 22°57' Maj - Mai 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D.v I	II	III
1	87.6	84.0	82.1	84.6	-0.1	2.9	0.7	1.0	4.3	-2.0	86	60	90	79	0.9	3.0	0.6	1.5	9	10	2	NW 6	NW 6	W 3
2	80.9	82.8	85.9	83.2	1.2	4.9	3.1	3.1	7.5	-1.0	90	55	84	76	0.7	4.0	1.2	2.0	10	10	9	SW 6	SW 8	W 1
3	88.9	88.7	87.5	88.4	1.0	8.3	3.1	3.9	9.6	-2.4	100	58	91	83	0.0	4.6	0.6	1.7	10 ≡	5 ⊙	8	C 0	SW 5	C 0
4	82.8	81.5	84.0	82.8	5.1	9.2	4.6	5.9	10.4	-1.4	75	60	92	76	2.2	4.6	0.7	2.5	5 ⊙	9 ⊙	3	C 0	C 0	NW 2
5	88.4	91.9	95.3	91.9	5.7	7.5	3.3	4.4	9.6	2.7	90	64	78	77	0.8	3.8	1.7	2.1	10	9	3	W 4	WSW 2	W 1
6	99.2	99.9	99.1	99.4	5.3	11.3	6.9	7.6	12.9	2.1	89	54	88	77	1.0	6.2	1.1	2.8	10	10 ●	2	C 0	SE 4	C 0
7	97.1	95.3	94.4	95.6	7.6	15.7	10.1	10.9	16.4	-0.2	87	42	77	69	1.3	10.4	2.9	4.9	8	8 ⊙	8	SE 2	SE 4	C 0
8	92.3	91.6	89.8	91.2	10.5	13.1	13.3	12.6	16.9	8.7	88	86	85	86	1.5	2.1	2.3	2.0	10	9	10	S 4	C 0	C 0
9	89.2	91.1	91.3	90.5	10.7	11.4	9.7	10.4	15.0	9.6	91	78	89	86	1.2	3.0	1.2	1.8	10	9	2	NW 3	NW 5	NW 2
10	89.4	88.1	88.3	88.6	10.7	17.7	14.1	14.2	17.9	2.1	84	49	68	67	2.1	8.2	5.1	5.1	5 ⊙	9	10	C 0	NE 2	W 4
11	88.4	89.7	90.5	89.5	11.1	14.9	9.3	11.2	15.8	9.1	89	59	83	77	1.5	6.9	2.0	3.5	8	9	0	W 3	NW 5	WNW 3
12	92.2	93.7	95.6	93.8	10.3	15.6	10.6	11.8	17.4	4.8	83	44	68	65	2.1	9.9	4.1	5.4	7 ⊙	9 ⊙	0	NNW 2	NNW 2	N 1
13	97.7	96.9	95.1	96.6	11.7	17.2	14.4	14.4	18.4	3.4	72	46	69	62	3.7	10.6	5.1	6.5	3 ⊙	9	10	C 0	E 3	C 0
14	90.2	85.4	74.5	83.4	11.5	12.9	12.3	12.2	15.0	8.2	82	93	96	90	2.5	1.1	0.5	1.4	10	10 ●	10 ●	SE 4	ENE 7	E 9
15	70.3	71.3	73.7	71.8	9.5	11.5	10.6	10.6	13.6	9.0	93	76	96	88	0.8	3.3	0.5	1.5	10 ●	10	10 ●	SE 3	SE 2	NW 7
16	77.0	81.1	87.1	81.7	7.9	8.1	7.8	7.9	10.6	7.7	96	91	82	90	0.4	0.9	2.0	1.1	10 ●	10 ●	10	NW 7	WNW 8	NW 10
17	89.5	89.9	89.4	89.6	7.3	11.1	8.4	8.8	12.7	4.8	73	67	94	78	2.7	4.3	0.6	2.5	1 ⊙	10 ●	9	WSW 6	WSW 6	C 0
18	88.0	92.1	95.3	91.8	6.9	12.0	7.6	8.5	12.6	6.7	92	59	83	78	0.7	5.7	1.7	2.7	10 ●	9 ●	0	WNW 7	W 4	SW 3
19	98.0	97.3	94.9	96.7	8.5	15.6	10.2	11.1	17.0	3.3	85	45	68	66	1.7	9.7	3.9	5.1	4 ⊙	7 ⊙	8	W 3	SW 4	S 2
20	89.2	87.7	88.8	88.6	13.5	19.9	8.7	12.7	20.0	8.1	63	54	96	71	5.7	10.6	0.4	5.6	9	10	10 ●	SE 8	SSE 10	NW 7
21	93.1	94.3	93.2	93.5	8.7	13.5	9.9	10.5	14.4	6.9	85	65	78	76	1.6	5.5	2.7	3.3	10	9 ⊙	10	W 6	NW 5	NW 4
22	91.0	92.9	94.9	92.9	8.1	8.1	5.5	6.8	9.9	5.5	91	94	98	94	0.9	0.6	0.1	0.5	10 ●	10 ●	8	NW 3	SW 3	SW 2
23	94.9	95.4	94.1	94.8	11.2	16.3	14.9	14.3	17.4	5.4	92	61	71	75	1.0	7.2	4.8	4.3	10	10	10	SW 4	SSW 6	SSW 4
24	95.0	96.3	95.9	95.7	9.7	14.7	12.2	12.2	15.6	9.6	93	57	86	79	0.8	7.2	2.0	3.3	10 ●	9	10 ●	C 0	W 2	SW 2
25	94.0	94.1	94.5	94.2	9.0	10.3	10.1	9.9	12.2	8.7	95	96	96	96	0.7	0.5	0.5	0.6	10 ●	10 ●	10	N 3	NW 3	C 0
26	93.4	92.6	91.5	92.5	8.8	10.7	11.7	10.7	11.9	8.0	99	94	99	97	0.1	0.9	0.1	0.4	10 ●	10	10 ●	NE 3	ENE 5	NE 2
27	93.5	95.3	95.7	94.8	12.9	18.9	14.4	15.2	20.4	11.4	99	71	92	87	0.2	6.3	1.3	2.6	10	8 ⊙	10 ●	NE 3	C 0	C 0
28	95.5	95.9	93.3	94.9	12.3	16.5	14.1	14.2	17.4	11.3	95	79	84	86	0.7	4.1	2.5	2.4	10	10	10	NNE 3	WNW 3	N 3
29	91.1	93.6	94.3	93.0	13.3	16.2	11.5	13.1	18.3	8.8	92	64	82	79	1.3	6.7	2.5	3.5	5	6 ⊙	7	C 0	SW 7	WNW 1
30	95.0	95.4	94.4	94.9	10.9	11.2	9.2	10.1	14.3	5.5	89	85	95	90	1.4	2.0	0.6	1.3	10	10	10	SW 3	SW 3	SE 2
31	95.5	93.7	88.7	92.7	8.1	11.3	9.9	9.8	14.1	4.0	97	84	89	90	0.3	2.2	1.3	1.3	9	10 ●	10	C 0	SW 5	WNW 4
M	90.6	91.0	90.7	90.8	8.6	12.5	9.4	10.0	14.2	5.4	88	67	85	80	1.4	5.0	1.8	2.7	8.5	9.1	7.4	3.1	4.2	2.5

Czerwiec - Juin

1	87.6	91.3	95.5	91.5	8.4	9.3	6.6	7.7	11.8	6.4	82	67	82	77	2.0	3.8	1.7	2.5	8	7	7	SW 7	W 9	C 0
2	95.5	96.7	99.0	97.1	7.7	11.1	8.7	9.0	11.8	4.4	84	58	82	75	1.6	5.5	1.9	3.0	10	10	7	ENE 1	E 3	C 0
3	101.4	102.5	102.5	102.1	9.4	13.1	8.9	10.1	15.0	2.2	79	55	88	74	2.5	6.9	1.4	3.6	8 ⊙	9	9	C 0	N 4	NW 3
4	102.0	100.9	98.9	100.6	8.1	12.3	11.2	10.7	12.7	6.6	76	60	55	64	2.5	5.8	6.0	4.8	9	10 ●	10 ●	N 5	N 6	NNE 5
5	98.1	100.2	100.5	99.6	7.3	9.5	9.3	8.8	11.4	6.0	87	75	62	75	1.3	3.0	4.4	2.9	10 ●	10 ●	10	N 4	NE 9	N 8
6	100.2	102.9	104.7	102.6	5.8	9.9	7.3	7.6	11.9	4.8	57	42	70	56	4.0	7.1	3.0	4.7	9	9	10	NNE 10	NNE 12	E 8
7	107.1	106.8	105.8	106.6	8.2	14.7	11.3	11.4	16.1	5.7	57	56	67	53	4.7	10.7	4.4	6.6	7 ⊙	3 ⊙	1	NNE 5	N 9	NNW 2
8	106.1	104.4	100.2	103.6	12.9	17.6	12.9	14.1	19.6	6.4	69	45	65	60	4.6	11.1	5.3	7.0	1 ⊙	7	3	NNW 1	NW 4	W 2
9	93.2	91.1	91.9	92.1	11.7	19.9	10.9	13.4	20.4	9.0	80	49	53	61	2.8	11.9	6.1	6.9	9	8 ⊙	0	W 5	W 10	NW 3
10	92.6	91.5	90.0	91.4	9.9	16.5	13.1	13.2	17.4	5.4	74	40	74	63	3.1	11.4	4.0	6.2	1 ⊙	6 ⊙	10	NW 5	N 8	C 0
11	87.0	84.5	85.1	85.5	11.5	19.5	11.7	13.6	19.7	11.3	79	48	94	74	2.8	11.8	0.8	5.1	10 ●	9 ⊙	10	SSW 4	SSW 9	C 0
12	87.1	88.2	90.2	88.5	9.7	14.1	9.7	10.8	15.0	7.8	86	64	78	76	1.7	5.8	2.6	3.4	10	9	3	SW 4	SW 5	WNW 3
13	93.3	94.2	95.3	94.3	10.9	16.3	11.5	12.6	17.4	5.7	81	45	61	62	2.4	10.3	5.4	6.0	2 ⊙	6 ⊙	3	WNW 3	W 3	WNW 2
14	96.6	95.4	94.5	95.5	12.7	19.3	13.9	15.0	20.8	5.0	48	45	68	54	7.7	12.4	5.1	8.4	9	9	3	SW 3	SW 5	SW 2
15	95.3	97.6	98.7	97.2	16.1	21.8	17.9	18.4	23.0	10.7	68	50	74	64	5.8	12.9	5.4	8.0	7	8	6	NW 3	W 9	C 0
16	99.0	99.2	97.3	98.5	16.7	24.9	19.5	20.2	26.8	14.2	81	56	80	72	3.7	14.0	4.5	7.4	8	8 ⊙	7	W 2	WSW 3	SSW 1
17	95.9	97.6	99.4	97.6	18.1	19.7	14.6	16.8	21.0	14.0	87	65	79	77	2.7	8.1	3.4	4.7	10	8	9	W 4	WNW 9	WNW 5
18	100.8	100.3	99.1	100.1	12.1	19.5	15.5	15.6	21.1	9.0	87	53	68	69	1.8	10.7	5.7	6.1	9	6	4	C 0	S 2	C 0
19	99.1	97.6	94.7	97.1	16.1	22.3	16.9	18.0	23.6	7.3	72	35	71	59	5.1	17.5	5.5	9.4	5 ⊙	9 ⊙	1	S 1	S 3	SSE 2
20	93.1	94.2	96.3	94.6	17.9	15.7	12.5	14.6	22.3	12.5	74	94	88	85	5.4	1.1	1.7	2.7	8	10	9	SSE 2	NW 9	C 0
21	97.3	97.6	98.4	97.8	15.2	21.3	15.2	16.7	22.4	9.4	81	45	89	72	3.4	14.0	1.9	6.4	6 ⊙	9 ⊙	9 ●	SW 4	SW 5	C 0
22	100.9	101.6	100.4	101.0	15.3	20.9	17.3	17.7	22.7	11.8	63	50	85	66	6.5	12.3	2.9	7.2	5 ⊙	5 ⊙	10	WNW 3	W 3	C 0
23	99.3	98.2	98.0	98.5	19.5	18.3	13.9	16.4	24.7	13.7	75	93	92	87	5.7	1.4	1.3	2.8	8 ⊙	10 ● R	10	SSW 3	NW 5	C 0
24	97.4	96.5	94.0	96.0	13.3	20.1	16.2	16.4	21.4	9.5	87	44	87	73	2.0	13.1	2.3	5.8	9	8	3	SW 5	SW 6	SW 1
25	90.7	90.8	92.7	91.4	15.1	17.5	10.7	13.3	18.5	10.6	69	48	84	67	3.3	10.4	2.1	5.9	9 ⊙	8	3	WNW 8	WSW 10	SW 4
26	93.3	93.7	92.8	93.3	11.1	13.7	12.3	12.4	16.1	8.4	72	53	80	68	3.7	7.3	2.9	4.6	8 ●	9	6	WSW 8	SW 7	C 0
27	89.9	87.9	87.1	88.3	13.5	17.2	11.3	13.3	18.3	7.5	66	59	74	66	3.3	8.0	3.4	3.6	8	9	4	S 6	SW 9	SW 3
28	86.4	86.0	85.6	86.0	10.6	11.2	9.3	10.2	15.1	9.2	90	88	86	88	1.3	1.7	1.7	1.6	8	9 ●	9	SW 6	SW 7	SSW 3
29	82.8	82.5	83.7	83.0	9.7	12.3	9.8	10.4	13.4	8.0	86	68	92	82	1.7	4.7	0.9	2.4	10	8	9	SW 3	WSW 4	WNW 3
30	85.1	86.8	88.8	86.9	10.6	14.3	11.7	12.1	16.9	6.3	86	62	83	77	1.8	6.1	2.3	3.4	7	9	9	WNW 4	WNW 6	WNW 5
31																								
M	95.1	95.3	95.4	95.3	12.2	16.5	12.4	13.4	18.3	8.3	76	56	77	70	3.5	8.7	3.3	3.2	7.3	8.2	6.7	4.0	5.4	2.2

Suwałki $H_s = 165m$ $H_w = 169{,}6m$ $h_w = 13m$ Maj - Mai 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ LODU h	POGODA
1	8	0.0	•	$\overset{x}{\Delta}{}^{\circ}8^{40}...10^{55}\overset{\bullet}{\nabla}{}^{\circ}11^{45}...12^{25}\overset{x}{\Delta}{}^{\circ}16^{45-50}\overset{\bullet}{\nabla}{}^{\circ}17^{35}...18^{20};\smile^{\circ}na$
2	8	•	•	$\overset{x}{\Delta}{}^{\circ}5^{50}...6^{10}$
3	8	0.0	•	$\overset{\bullet}{\nabla}{}^{\circ}8^{10}-9^{45};10^{20}-11^{25};=,\equiv{}^{\circ}3^{30}-8^{00};\smile'na-a$
4	8	1.6	•	$\overset{\bullet}{\nabla}{}^{\circ}9^{15-40};10^{20}-11^{55};=np;\smile^{\circ}na$
5	7	0.0	•	$=0^{00}-6^{10};np;\triangle^{\circ}22-24$
6	6	0.0	•	$\overset{\bullet}{\nabla}{}^{\circ}6^{30}-7^{45};12^{15}-13^{40};=0^{00}-8^{00};\triangle^{\circ}na$
7	8	0.0	•	$\bullet{}^{\circ}23^{40}-24;=2^{15}-6^{10};\smile^{\circ}na$
8	6	0.0	•	$\bullet{}^{\circ}0^{00}-1^{10}...2^{15};9^{40}-11^{28}...12^{05};=na-p,p-24$
9	7	0.0	•	$\bullet{}^{\circ}6^{30}-8^{05};=0^{00}-3^{30}\equiv{}^{\circ}-4^{40}=-8^{00}19^{30}-24$
10	8	0.7	•	$\bullet{}^{\circ}21^{40}-22^{10}...24;=0^{00}-7^{20};\triangle^{\circ}na-a$
11	7	0.0	•	$\bullet{}^{\circ}0^{00}...3^{35}\overset{\bullet}{\nabla}{}^{\circ}16^{20-20};=na-a,np;\triangle'np$
12	7	•	•	$=na-8;\triangle'na-8^{00}$
13	8	•	•	$\triangle'na-8$
14	6	12.1	•	$\bullet{}^{0-1}10^{20}-16^{25};18^{35}-22^{15};\gg17^{20}-19^{40};=p-24$
15	8	11.1	•	$\bullet{}^{\circ}0^{20}-4^{40}5^{35}-6^{05}\bullet...7^{15}\bullet,\bullet{}^{\circ}8^{15}-11^{55}\overset{\bullet}{\nabla}{}^{2-0}16^{10}-19^{45}\overset{\bullet}{\nabla}{}^{\circ},\bullet,\bullet{}^{\circ}20^{15}-24;=na$
16	6	0.3	•	$\bullet{}^{\circ}0^{00}-4^{30}...6^{10}-15^{15}...16^{45};\gg18^{20}-24$
17	6	8.8	•	$\overset{\bullet}{\nabla}{}^{\circ}12^{20}-13^{20}\bullet{}^{\circ}23^{15}-24;\gg0^{00-20};=13^{20}-24$
18	8	0.0	•	$\bullet{}^{2-0}0^{00}...8^{05}\overset{\bullet}{\nabla}{}^{\circ}11^{45}...15^{05};18^{03-07};=0^{00}-8^{00}$
19	8	•	•	$=4^{15}-5^{20};\triangle'na-a$
20	7	16.9	•	$\overset{\bullet}{\nabla}{}^{\circ}14^{52}-15^{15}\bullet{}^{0-2}-23^{10}...24;\gg4^{15}-8^{30};11^{05}-13^{35}$
21	8	6.1	•	$\bullet{}^{\circ}0^{00}...^{50};=7^{20}-8^{00}$
22	6	4.9	•	$\bullet{}^{0-1}1^{05}-14^{45}\bullet{}^{\circ}22^{30}...24;=20^{10}-24$
23	7	3.8	•	$\bullet{}^{\circ}0^{00}...1^{25};=0^{00}-12^{15};19^{30}-24$
24	7	5.6	•	$\overset{\bullet}{\nabla}{}^{1}2^{15-30}\bullet{}^{0-1}3^{10}-4^{12}...5^{10}\bullet,\bullet{}^{\circ}-5^{40}\bullet{}^{\circ}-7^{35};18^{10}...20^{30}-24;=0^{00}-8^{00}$
25	6	8.5	•	$\bullet{}^{\circ}0^{00}-9^{30}...10^{20}-17^{15}...18^{20};=20^{10}-24$
26	7	3.3	•	$\bullet{}^{0-1}2^{15}-10^{30}\bullet{}^{\circ}13^{01-30};14^{03-25};18^{45}-22^{10};=0^{00}-10^{40};17^{50}-24$
27	7	7.3	•	$\overset{\bullet}{\nabla}{}^{\circ}16^{10}-18^{06};19^{05}-20^{10};21^{10-45};22^{05-40};\mathfrak{K}^{\circ}W-E\ p;=,\equiv'0^{00}-10^{10}$
28	7	2.1	•	$\overset{\bullet}{\nabla}{}^{\circ}0^{05}...7^{25};13^{30}-14^{30};np...;\mathfrak{K}\ 2^{00-40}W-E$
29	7	•	•	$\overset{\bullet}{\nabla}{}^{\circ}2^{05-20};3^{25}-4^{30};\triangle'np$
30	6	2.7	•	$\bullet{}^{\circ}10^{05}-12^{30}...13^{10}\overset{\bullet}{\nabla}{}^{\circ}19^{15}-20^{40};\mathfrak{K}^{\circ}17^{45}-18^{40}W-E;\equiv{}^{\circ}2^{40}-6^{35}=-p,np;\triangle'0-a$
31	6	9.2	•	$\overset{\bullet}{\nabla}7^{50}-9^{15};12^{50}-14^{35};18^{05}-20^{15}\overset{\bullet}{\nabla}21^{45}-23^{45};\mathfrak{K}'21^{45}-22^{10}W-E;=na$
Σ	—	105.0	—	UWAGI.

Czerwiec - Juin

1	8	•	•	$\overset{\bullet}{\nabla}{}'0^{00}-2^{50};\gg11^{40}-12^{35};=3^{15}-7^{10};\triangle'np$
2	8	•	•	$\triangle'0-8$
3	8	0.4	•	$\overset{\bullet}{\nabla}{}^{\circ}11^{50}-13^{20};15^{15}...19^{25};\triangle^{\circ}na-a$
4	7	2.7	•	$\bullet{}^{\circ}12^{40}-18^{50}\overset{\bullet}{\nabla}{}^{\circ}20^{40}-21^{05}\bullet{}^{\circ}-24;\gg p;\cap{}^{\circ}20^{45-52}$
5	7	2.6	•	$\bullet{}^{\circ}0^{00}-16^{35};\gg17^{30}-18^{50}$
6	8	0.0	•	$\bullet{}^{\circ}2^{10-25};23^{40}-24;\gg2^{00}-19^{30}$
7	8	•	•	$\bullet{}^{\circ}0^{00}-2^{20}$
8	8	•	•	$\triangle^{\circ}na-a$
9	6	•	•	$\gg13^{15}-14^{10};=8^{30}-11^{20};\triangle^{\circ}na$
10	8	0.0	•	$\triangle^{\circ}na-a$
11	8	4.3	•	$\overset{\bullet}{\nabla}{}^{\circ}7^{35-50}a\overset{\bullet}{\nabla}{}^{2}17^{45}-18^{35}\overset{\bullet}{\nabla}{}^{\circ}np;\mathfrak{K}^{\circ}14^{40}-16^{40}W-E;17^{50}-18^{45}W-E$
12	8	1.5	•	$\overset{\bullet}{\nabla}{}^{\circ}2^{04-45}\overset{\bullet}{\nabla}{}^{1-0}14^{40}...18^{20};=na-a$
13	7	•	•	
14	8	•	•	$\triangle^{\circ}na-a$
15	6	•	•	$=8^{15}-15^{10}$
16	7	0.7	•	$=7^{10}-10^{40};21^{10}-24$
17	6	•	•	$\overset{\bullet}{\nabla}{}^{\circ}5^{05}-6^{07};\mathfrak{K}^{\circ}4^{40}-5^{35}W-E;\gg12^{30}-13^{45};=0^{00}-a\infty-p=p-24$
18	8	•	•	$\triangle^{\circ}np$
19	7	•	•	$=5^{20}-7^{30};\triangle'0-7$
20	8	13.8	•	$\overset{\bullet}{\nabla}{}^{2}12^{05-15}\overset{\bullet}{\nabla}{}'12^{30-45};14^{45}-15^{53};\mathfrak{K}^{\circ}10^{40}-11^{45}W-E;=np$
21	7	0.1	•	$\overset{\bullet}{\nabla}{}^{\circ}16^{55}...21^{45};=na-a,np;\triangle^{2}na-a$
22	8	•	•	$\overset{\bullet}{\nabla}{}^{\circ}1^{15}-2^{25}$
23	6	15.4	•	$\overset{\bullet}{\nabla}{}^{\circ}12^{30}-15^{35}\overset{\bullet}{\nabla}{}^{\circ}19^{09-20}\overset{\bullet}{\nabla}{}^{0-1}22^{50}-24;\mathfrak{K}'12^{30}-15^{35}NW-SE\ \lessdot\ na\ S;=p$
24	8	3.4	•	$\overset{\bullet}{\nabla}{}^{\circ}0^{00-10}\bullet{}^{\circ}-1^{20};=3^{40}-5^{30}$
25	8	0.2	•	$\overset{\bullet}{\nabla}{}^{\circ}2^{04-25}\overset{\bullet}{\nabla}{}^{2}3^{10}-4^{10};\gg12^{55}-16^{05};\cap19^{05-25}$
26	8	•	•	
27	8	1.4	•	$\overset{\bullet}{\nabla}{}^{2}11^{10-45}14^{33}-15^{10};16^{01-10}$
28	6	2.2	•	$\overset{\bullet}{\nabla}{}^{\circ}1^{50}...18^{25};22^{35}-23^{40};\cap19^{25-55}$
29	7	3.5	•	$\bullet{}^{\circ}2^{30}-3^{20}\bullet{}^{\circ}-5^{15}\overset{\bullet}{\nabla}{}^{0-1}10^{40}...21^{01};=2^{20}-9^{30}$
30	8	•	•	$\overset{\bullet}{\nabla}{}^{2}2^{05-25};\equiv'4^{30}-5^{30}$
31				
Σ	—	52.2	—	UWAGI.

Suwałki — φ = 54°06' — λ = 22°57' — Lipiec – Juillet 1962

DNI	CIŚNIENIE P = 900 – I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N_w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D_v I	II	III
1	89.7	90.8	91.3	90.6	12.5	17.2	12.5	13.7	18.4	10.3	80	60	80	73	2.9	7.8	2.9	4.5	7 ⊙	8 ⊙	1	W 9	W 8	W 5
2	91.2	89.7	87.1	89.3	11.2	17.5	12.6	13.5	18.3	7.5	97	54	81	77	0.3	9.1	2.7	4.0	6 ⊙	8 ⊙	7	W 4	WSW 7	W 1
3	81.8	80.1	78.7	80.2	11.0	10.9	9.2	10.1	13.9	8.0	85	94	95	91	1.9	0.8	0.6	1.1	10	10 ●	9	S 8	SSW 3	C 0
4	78.2	80.2	82.1	80.2	8.1	9.8	11.3	10.1	14.7	5.3	97	87	76	87	0.3	1.6	3.3	1.7	10	9 ●	10	SSW 3	SSW 5	S 3
5	84.6	86.8	88.7	86.7	11.9	14.3	13.0	13.0	15.3	10.1	75	59	75	70	3.5	6.6	3.8	4.6	7	10	9	SSW 6	SSW 6	S 1
6	91.2	92.6	94.2	92.7	12.2	17.1	11.2	12.9	18.5	9.2	78	58	89	75	3.2	8.1	1.5	4.3	9	9	3	SSW 4	S 6	C 0
7	94.5	94.1	94.2	94.3	11.1	18.1	10.8	12.7	19.0	5.6	95	59	89	81	0.7	8.4	1.5	3.5	9	9	4	C 0	SW 5	E 1
8	94.8	95.2	96.3	95.4	13.4	18.1	13.8	14.8	18.3	6.6	77	56	82	72	3.5	9.2	2.9	5.2	5	9	9	C 0	NW 4	NW 4
9	97.0	96.3	94.6	96.0	12.8	18.2	12.8	14.2	19.6	10.3	88	68	81	79	1.8	6.8	2.8	3.8	9	8	3	WNW 4	NW 7	WNW 8
10	90.0	88.1	85.2	87.8	11.4	16.2	12.4	13.1	16.8	9.5	88	72	96	85	1.7	5.1	0.5	2.4	10	10	10 ●	WNW 8	N 10	WNW 8
11	85.9	86.7	86.4	86.3	13.1	15.3	13.7	14.0	15.8	12.3	91	82	90	88	1.4	3.2	1.6	2.1	10	10	9	NW 5	W 6	WSW 3
12	85.6	86.1	85.5	85.7	13.0	17.3	14.0	14.6	18.2	11.8	88	67	92	82	1.8	6.5	1.3	3.2	10	9	4	WNW 3	WNW 5	C 0
13	85.2	84.7	84.3	84.7	12.3	18.9	13.6	14.6	19.6	8.7	99	62	93	85	0.2	8.2	1.1	3.2	10 ≡	7	10 ●	C 0	WSW 5	NW 2
14	82.9	82.0	82.8	82.6	13.2	16.0	13.4	14.0	18.3	11.1	91	77	91	86	1.4	4.2	1.4	2.3	8	8	9	W 1	NW 4	WNW 5
15	83.1	84.5	86.3	84.6	13.1	15.6	14.2	14.3	17.0	12.2	88	75	93	85	1.8	4.4	1.1	2.4	10	10	7	W 5	W 8	NW 2
16	88.3	89.3	90.3	89.3	12.8	16.6	13.4	14.0	16.9	7.0	95	71	91	86	0.7	5.5	1.4	2.5	10	9	8	C 0	C 0	C 0
17	92.1	92.9	94.9	93.3	12.2	19.0	13.8	14.7	19.8	6.3	93	53	83	76	1.0	10.4	2.7	4.7	9	7 ⊙	3	NW 2	NW 4	NNW 2
18	95.6	95.0	94.3	95.0	16.3	20.9	17.3	18.0	22.2	9.3	70	55	73	66	5.6	11.2	5.2	7.3	4 ⊙	8	6	N 4	NNE 7	N 4
19	93.9	94.0	94.8	94.2	15.7	22.5	15.8	17.4	23.9	14.2	86	63	73	75	2.4	9.9	4.4	5.6	8 ⊙	7 ⊙	2	NNE 4	NNE 7	N 2
20	96.8	96.3	96.6	96.6	19.0	23.1	18.2	19.6	25.3	9.8	60	47	73	61	8.9	14.9	5.3	9.7	1 ⊙	5 ⊙	2	NNW 3	NE 2	C 0
21	97.1	96.6	95.7	96.5	18.3	25.1	18.9	20.3	27.2	11.3	71	52	82	68	6.0	15.1	3.9	8.3	8	8	6	SW 2	WSW 3	SSW 2
22	95.8	95.7	96.5	96.0	20.4	23.8	16.7	19.4	25.6	16.6	63	72	99	78	8.9	8.2	0.2	5.8	9	10	5	S 6	WSW 4	C 0
23	96.8	98.2	98.7	97.9	18.6	19.0	15.6	17.2	21.4	12.8	89	77	79	82	2.3	5.0	3.7	3.7	8	10 ●	4	WNW 4	WNW 5	NW 1
24	98.8	99.1	100.2	99.4	15.4	18.2	12.9	14.8	19.5	9.0	83	57	92	77	3.0	9.0	1.3	4.4	5	8	6	C 0	WSW 7	W 3
25	100.3	101.2	101.9	101.1	12.8	18.7	12.4	14.1	20.6	9.5	91	53	88	77	1.4	10.2	1.7	4.4	9	4 ⊙	1	WSW 6	WSW 8	NNW 1
26	100.7	98.4	95.3	98.1	15.0	24.9	20.5	20.2	26.0	7.0	76	45	67	63	4.0	17.2	7.9	9.7	7 ⊙	8 ⊙	10	NNE 3	SW 4	S 1
27	91.7	92.0	90.3	91.3	18.2	22.0	16.8	18.4	24.8	16.1	95	72	94	87	1.1	7.2	1.2	3.2	10 ≡	9	10 ● R_4	WSW 3	NW 4	SW 2
28	88.9	91.7	93.8	91.3	12.3	16.2	11.2	12.8	17.1	11.1	89	68	92	83	1.3	5.8	1.0	2.8	10	9	8	WNW 8	WNW 10	WNW 6
29	96.3	96.8	98.2	97.1	12.8	16.0	11.8	13.1	17.8	9.5	81	60	83	75	2.8	7.4	2.3	4.2	5 ⊙	6 ⊙	1	WNW 5	NW 7	WNW 2
30	100.7	100.9	100.8	100.8	11.8	18.2	12.4	13.7	20.5	6.7	88	55	86	76	1.6	9.3	2.0	4.3	3	6 ⊙	4	WNW 3	E 4	C 0
31	101.5	100.8	99.3	100.5	14.3	19.0	14.8	15.7	20.8	7.2	82	55	74	70	2.9	10.0	4.3	5.7	4 ⊙	9 ⊙	8	S 1	SW 4	C 0
M	92.0	92.2	92.2	92.1	13.8	18.2	13.9	15.0	19.7	9.7	85	64	85	78	2.6	7.9	2.5	4.3	7.7	8.3	6.1	3.7	5.3	2.2

Sierpień – Août

1	95.1	93.4	92.7	93.7	14.6	16.6	12.9	14.2	17.7	7.2	76	74	89	80	4.0	5.0	1.6	3.5	5 ⊙	10	3	SW 4	SW 3	W 2
2	91.1	92.8	93.7	92.5	14.0	17.2	14.2	14.9	19.0	11.8	80	65	82	76	3.2	6.9	2.9	4.3	5	7	6	W 7	W 8	WSW 2
3	93.2	93.9	95.1	94.1	13.2	19.0	13.4	14.8	20.4	11.5	88	60	86	78	1.8	8.9	2.1	4.3	10	7 ⊙	4	WSW 1	W 5	C 0
4	96.1	95.3	94.2	95.2	12.2	21.8	17.4	17.2	22.4	7.4	90	58	94	81	1.4	10.9	1.3	4.5	9	9	10 ●	C 0	SW 4	C 0
5	93.6	92.9	89.0	91.8	16.6	21.6	18.4	18.8	23.4	14.2	96	74	94	88	0.8	6.8	1.3	3.0	9	8	10 ●	WNW 1	SW 2	S 2
6	87.2	90.5	91.1	89.6	16.1	19.1	15.0	16.3	21.1	14.8	97	64	97	86	0.6	7.9	0.5	3.0	10 ●	8	9	W 4	W 3	C 0
7	90.6	88.7	81.3	86.9	16.8	23.7	21.3	20.8	25.8	12.5	87	67	88	81	2.5	9.6	3.0	5.0	8 ⊙	8 ⊙	10 ● R_4	SSW 3	SE 8	S 9
8	90.2	92.7	96.0	93.0	15.2	20.1	14.1	15.9	21.6	14.0	85	52	79	72	2.6	11.3	3.4	5.8	10	6	2	SW 8	SW 9	SW 1
9	99.4	101.1	102.0	100.8	14.0	18.8	12.4	14.4	19.7	9.9	78	51	89	73	3.6	10.6	1.6	5.3	2 ⊙	6 ⊙	4	SW 2	SW 5	W 2
10	103.2	101.6	96.3	100.4	12.0	18.5	13.7	14.4	20.4	6.5	88	57	83	76	1.7	9.3	2.7	4.6	4	7	6	C 0	SW 4	S 3
11	92.1	93.0	94.5	93.2	15.4	18.3	15.2	16.0	19.3	12.9	85	55	77	72	2.6	9.5	4.1	5.4	10	9 ⊙	9	SW 5	W 5	SW 3
12	96.8	97.3	96.3	96.8	16.7	23.8	20.0	20.1	25.1	12.6	73	49	74	66	4.8	14.9	6.2	8.6	1 ⊙	8 ⊙	0	SW 3	SW 6	SSW 3
13	96.3	96.3	97.7	96.8	18.2	24.3	15.6	18.4	25.0	13.8	82	58	73	72	3.7	12.6	4.4	6.9	4 ⊙	2 ⊙	4	W 2	W 6	NW 2
14	98.5	97.6	96.6	97.6	13.2	19.0	11.8	14.0	20.3	8.8	78	46	81	68	3.3	12.0	2.6	6.0	5 ⊙	1 ⊙	1	NW 2	NW 3	NW 2
15	97.2	93.3	90.9	94.3	10.4	17.6	14.3	14.2	20.3	2.9	90	48	90	76	1.3	10.3	1.6	4.5	4 ⊙	9 ⊙	10	C 0	SE 2	ESE 4
16	87.0	89.0	91.2	89.1	16.5	21.4	17.8	18.4	23.6	13.3	100	64	84	83	0.0	9.2	3.2	4.1	10 ≡	8	7	SW 3	WSW 3	C 0
17	92.8	93.4	92.8	93.0	17.6	22.5	16.2	18.1	24.0	13.5	89	61	96	82	2.2	10.6	0.8	4.3	2 ⊙	6 ⊙	8	C 0	SSW 4	NE 3
18	90.7	88.0	89.4	89.4	14.8	21.7	15.1	16.7	21.9	13.4	98	78	97	91	0.3	5.8	0.6	2.2	10 ●	10	10	NE 3	W 3	WSW 2
19	89.4	89.7	88.9	89.3	13.4	16.0	13.2	14.0	16.9	12.7	94	79	91	88	0.9	3.8	1.4	2.0	10	9 ⊙	10	WNW 2	W 6	W 4
20	87.4	90.2	92.9	90.2	15.0	17.1	13.2	14.6	19.5	12.5	91	75	87	84	1.5	4.9	2.0	2.8	9	10	0	N 9	N 8	N 4
21	93.5	93.4	93.5	93.3	11.4	18.5	13.3	14.1	19.4	9.3	100	61	84	82	0.0	8.3	2.3	3.6	10 ≡	3 ⊙	0	N 3	N 1	N 1
22	93.4	93.5	94.0	93.6	12.6	18.2	13.2	14.3	20.0	9.2	95	69	94	86	0.7	6.4	0.9	2.7	10	10	10	C 0	S 3	NW 1
23	91.5	91.7	93.1	92.1	12.9	16.6	12.3	13.5	17.0	11.0	98	68	89	85	0.4	6.1	1.3	2.7	10	8	4	S 3	WSW 8	W 4
24	92.2	88.4	83.1	87.9	11.0	12.8	15.6	13.8	15.7	8.9	95	95	95	94	0.6	1.1	0.9	0.9	6	10 ●	10	SW 6	SE 6	SW 8
25	86.8	88.1	89.4	88.1	13.2	17.0	11.7	13.4	17.5	11.3	91	61	94	82	1.4	7.6	0.8	3.3	8	9	10	SW 8	WSW 9	SSW 5
26	91.5	94.3	97.1	94.3	11.4	15.4	10.8	12.1	15.5	10.7	85	67	90	81	2.0	5.8	1.4	3.1	9	8	3	W 9	W 8	SW 2
27	96.9	92.1	88.2	92.4	10.4	20.0	17.6	16.4	20.9	6.1	92	51	76	73	1.0	11.4	4.7	5.7	8 ⊙	9 ⊙	10	S 2	SSE 10	SW 6
28	90.2	91.4	92.8	91.5	12.1	14.0	10.6	11.8	17.6	10.0	77	69	90	79	3.2	4.9	1.3	3.1	5	8	0	SW 8	SW 9	WSW 6
29	93.2	93.1	91.6	92.6	11.2	14.2	10.8	11.8	16.2	9.7	90	77	97	88	1.3	3.8	0.4	1.8	9	9 ⊙	9	WSW 7	WSW 6	W 2
30	92.0	93.8	95.0	93.6	11.0	12.6	10.2	11.0	14.9	9.9	95	95	95	95	0.6	0.7	0.6	0.6	9	9 ●	0	W 6	W 8	WSW 2
31	89.2	86.8	87.8	87.9	10.2	12.6	9.6	10.5	12.9	9.0	97	77	87	87	0.3	3.4	1.6	1.8	10	8 ⊙	0	SSW 6	W 6	W 6
M	92.8	92.9	92.3	92.7	13.7	18.4	14.2	15.1	19.8	10.7	89	65	88	81	1.8	7.8	2.1	3.9	7.5	7.8	5.8	3.8	3.6	2.9

Suwałki H_s = 165m H_t = 169,6m h_w = 13m Lipiec - Juillet 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	8	•	•	⌓° np
2	8	•	•	= 3^30-8^30; ⌓° 0-9
3	6	9.0	•	•° 8^25-14^30, 18^18-20^35
4	7	1.3	•	•° 9^01-11^15 ⚲°-1 13^00-45, 14^26-15^05; ≫ 17^05-25; ≡' 2^00-50 = -8^30
5	7	•	•	
6	7	7.1	•	⚲' 14^25-45 ⚲°-1 15^02-17^35 ⚲° 19^31-39; ⚠' 15^20-17^15, SW-NE; ≫ p
7	7	0.2	•	⚲° 11^35-12^30, 13^46-14^05; ⚠ 11^05-12^40, 13^45-14^35 (⚠) p W-E; = na-a
8	8	•	•	= na-a; ⌓° na-a
9	7	•	•	= 3^20-6^40
10	7	2.6	•	⚲° 11^50...17^05 •°-24; ≫ 13^25-14^10
11	8	0.0	•	⚲° 7^45-58, 9^05-40 •°-11^35 ⚲° 13^40-50, 14^15-15^05
12	8	0.1	•	⚲° 13^55-15^05, 20^07-10
13	8	1.6	•	⚲° 11^32-12^45, 15^58-16^09, 20^55-22^50; ≡' na, 5^56-8^20
14	8	0.4	•	⚲° 1^45-2^45 ⚲' 12^05-40, 13^02-10, 19^24-20^08; ≫ 18^09-25; = na
15	7	0.0	•	⚲° 14^02-10, 14^33-45; ⌓' np
16	8	•	•	≡' 0^45-6^45 = -7^30; ⌓' 0-8, np
17	8	•	•	= 0^10-4^15 ≡² -6^20 = -8^10; ⌓² na-a
18	8	•	•	⌓ na
19	8	•	•	⌓ np
20	8	•	•	⌓ na-a
21	7	•	•	
22	7	0.6	•	⚲° 14^25-16^28; = 19^10-22^35 ≡' -24; ⌓' np
23	7	0.1	•	•° 9^18-40 ⚲° 10^35-50 13^45-14^05; ≡² 0^00-6^40 = -8^30; ⌓² 0-10
24	7	0.9	•	⚲° 9^30-44, 14^01 20^05; = 2^30-10^10 19^20-23^10
25	8	•	•	⌓' np
26	8	4.7	•	⚲° 23^25-24; ⚠° 23^25-24 S-W; ⌓² na-a
27	6	6.4	•	⚲' na ⚲° 20^40-22^28, 23^50-24; ⚠° 0^00-50 S-N ⚠' 20^45-22^35 SW-NE; ≫ 17^30-19^20; ≡' 4^00-14^05
28	8	5.0	•	⚲° 0^00-10 •° 2^35...3^25 ⚲° 5^10-6^30 ⚲°-1 13^50, 23^38
29	7	0.0	•	⚲° 11^25, 16^04
30	8	•	•	⌓° 2-8, 21-24
31	8	•	•	(⚠)° 15^45-17^40 N-S; ⌓° 0-8 ⌓' 22^00-24
Σ	—	40.0	—	UWAGI:

Sierpień - Août

1	7	2.4	•	•° 9^40-10^25 ⚲° 11^07...15^55; ⌓² 0-9
2	8	•	•	⚲° 0^45-2^30
3	7	•	•	
4	7	6.4	•	⚲° 15^50-16^45 •° 17^03...19^10-45 ⚲°-1 21^30-23^35; = 2^00-7^30
5	6	8.1	•	•° 19^25...20^45, 21^15-22^10 ⚲' -24; ⚠° 22^10-24 W-E; = 0^40-2^50 ≡² -7^15 = -15^05
6	7	•	•	⚲° 0^00-2^15 •° 6^20-7^10...40; ⚠° 0^00-10 W-E; = a; ⌓' np
7	7	8.9	•	⚲° 14^35-15^15 ⚲' 21^15-24; ⚠° 21^05-22^45 SE-NE; 23^50-24 SE-NE; ≫ 18^05-21^15; = a; ⌓' na-a
8	8	•	•	⚲° 0^00-2^25; ⚠' 0^00-2^25 SE-NE; ≫ 15^10-18^40; ⌓' np
9	8	•	•	⌓' 0-9
10	8	•	•	= 6^10-8^30
11	7	•	•	≫ 16^25-17^30, 18^05-20
12	7	•	•	⌓° 2-7
13	7	•	•	= 4^30-9^00; ⌓ 4-9
14	8	•	•	⌓° na-a, np
15	8	16.9	•	⚲' 19^55-20^15; = 5^15-8^25; ⌓° 0-8
16	7	0.0	•	⚲² 1^10-3^25; ⚠' 1^30-2^45 NE-SE; ≡² 4^50-8^40 = -10^30; np
17	7	5.3	•	⚲° 5^05-12; = 0^00-9^30, 20^20-21^00; ⌓' na
18	7	5.8	•	•° 4^40-6^15 ⚲°-0 20^56; ⚠° 6^25-7^40 SW-W, 8^05-45 SW-NW, 13^55-15^02 E-W, 18^04-45 W-E; = a-p
19	7	1.7	•	⚲° 23^40-24; = 1^20-10^25
20	7	•	•	⚲° 0^00-2^10 •° 2^10-4^35, 5^45...6^30; ⌓' np
21	7	•	•	= 0^10-6^20 ≡° -7^45 = -9^30; ⌓² 0-9
22	8	6.3	•	⚲° 15^15-17^05 •° -21^50, 23^40-24; = 16^30-21^40, np; ⌓° na-a
23	7	5.9	•	•° 0^00-15, 2^05-28 ⚲° 10^10-11^05 ⚲²-0 16^01-20 ⚲' 18^43-50; ⚠' 15^45-16^25, SW-NE; =, ≡° 0^00-12^30
24	6	6.6	•	•° 10^40-19^35, 21^01-20, 22^30-24; ≫ 14^15-15^20; = 15^05-24
25	7	3.3	•	•° 0^00-40 ⚲° 15^05-12 ⚲°-1 18^02...23^15; ⚠ 19^25-35 SW-NE; ≫ 12^15-50, 15^15-16^15; = na, ∩ 18^05-12
26	8	5.0	•	⚲' 13^37-42, 14^03-10; ≫ 12^10-13^10
27	7	•	•	≫ 13^40-15^40; = 6^15-9^05
28	8	0.0	•	⚲' 14^00-10, 14^49-55 ⚲° 17^53-18^04; ≫ 14^35-18^45
29	7	4.2	•	⚲° 9^40-10^05, 17^30-18^10 •' -19^40 ⚲° 22^40-50; = 19^40-24
30	6	3.7	•	⚲°-0 10^35-11^40 ⚲° 12^25-15^02 ⚲' 16^15-35; = 0^00-4^10
31	7	12.0		⚲° 4^35-40 •° 6^10-35 •° -7^10 ⚲°-1 8^12...18^50
Σ	—	100.3	—	UWAGI.

Suwałki φ=54°06' λ=22°57' Wrzesień-Septembre 1962

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI I	II	III	Dies	ZACHMURZENIE N I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	91.5	93.4	97.2	94.0	10.5	13.3	10.0	11.0	15.3	8.3	87	61	89	79	1.6	6.0	1.3	3.0	8	8⊙	0	NW 7	WNW 9	WNW 4
2	100.1	100.2	98.7	99.7	9.0	14.0	12.6	12.0	15.4	7.2	95	63	85	81	0.7	5.9	2.2	2.9	10≡	10	10	SSW 3	WSW 6	WSW 2
3	97.2	98.1	98.9	98.1	9.8	17.0	11.6	12.5	17.7	8.8	92	70	95	86	0.9	5.8	0.6	2.4	9	9	0	WSW 3	WSW 4	C 0
4	97.1	93.6	90.6	93.8	12.4	22.4	15.0	16.2	22.9	8.5	95	50	87	77	0.7	13.6	2.2	5.5	2⊙	0⊙	0	SSE 3	SSE 7	C 0
5	85.7	82.8	83.3	83.9	13.6	24.9	16.2	17.7	25.4	11.0	89	54	92	78	1.8	14.7	1.6	6.0	2⊙	0⊙	10	S 1	SSW 8	SSW 6
6	83.5	83.7	84.0	83.7	12.2	17.2	12.4	13.6	18.3	10.5	86	57	85	76	2.0	8.5	2.2	4.2	3⊙	7⊙	0	SW 8	SW 9	SSW 3
7	76.4	74.3	77.4	76.0	13.2	17.8	13.0	14.2	17.9	9.4	98	76	88	87	0.4	5.0	1.8	2.4	10●	10	10	S 5	SW 8	WSW 5
8	83.1	86.1	88.5	85.9	9.8	13.6	8.4	10.0	14.9	8.4	77	54	82	71	2.8	7.2	2.0	4.0	7⊙	7⊙	0	WSW 9	SW 9	C 0
9	92.3	95.4	98.9	95.5	8.6	14.2	11.0	11.2	15.5	6.3	90	58	79	76	1.1	6.8	2.7	3.5	7	9	9	WSW 4	WSW 7	W 4
10	99.7	98.2	95.4	97.8	8.8	15.8	12.8	12.6	17.9	6.9	93	61	68	74	0.8	6.9	4.7	4.1	9	8⊙	0	SW 5	SSW10	S 4
11	91.4	89.4	88.4	89.7	9.8	14.7	13.2	12.7	15.8	7.1	86	84	88	86	1.7	2.7	1.8	2.1	9	10●	10●	SSW 3	SSW 6	W 9
12	93.4	88.6	78.4	86.8	9.0	13.8	15.8	13.6	17.6	7.4	96	86	87	90	0.5	2.2	2.2	1.6	10	10●	7	SW 4	S 5	WSW 5
13	85.2	88.7	92.2	88.7	9.4	13.7	9.0	10.3	15.8	8.5	78	48	88	71	2.6	8.1	1.4	4.0	4⊙	8⊙	0	WNW 9	WNW12	WSW 4
14	94.4	96.2	99.0	96.5	9.4	12.4	7.0	9.0	14.1	6.8	88	60	90	79	1.4	5.8	1.0	2.7	8	6●	0	W 6	W 7	W 2
15	100.3	100.6	97.5	99.5	4.7	13.2	10.0	9.5	14.4	3.7	100	66	78	81	0.0	5.1	2.7	2.6	10≡	7	9	WSW 2	WSW 5	SSW 4
16	93.3	90.8	89.8	91.3	8.0	18.2	12.6	12.8	19.0	5.3	84	61	89	78	1.6	8.3	1.6	3.8	3⊙	4⊙	9	S 3	SE 7	SSE 2
17	88.2	90.3	91.2	89.9	12.0	13.4	11.4	12.0	14.3	11.0	95	84	93	91	0.7	2.5	1.0	1.4	9	10	10●	C 0	NNW 2	NNW 2
18	88.5	88.7	82.0	86.4	10.0	12.3	11.2	11.2	12.4	9.9	93	81	96	90	0.8	2.7	0.5	1.3	10●	10	10●	NNE 4	NNW 5	NNE 6
19	79.5	86.0	90.7	85.4	9.6	9.1	8.0	8.7	11.7	8.0	92	87	90	90	1.0	1.6	1.0	1.2	10	9	10	SW 9	SW 10	WSW 7
20	92.3	92.9	92.0	92.4	6.3	10.0	6.3	7.2	11.1	5.1	91	78	89	86	0.8	2.7	1.0	1.5	9	10	5	SW 5	SSW 8	SSW 5
21	89.7	89.4	89.8	89.6	7.5	10.2	7.6	8.2	11.0	6.2	90	78	93	87	1.1	2.7	0.7	1.5	10	10	9	WSW 8	W 8	WSW 6
22	91.3	92.9	94.0	92.7	7.5	9.5	8.6	8.6	11.0	7.2	93	76	88	86	0.8	2.8	1.4	1.7	10	9●	10	WNW 5	WNW 3	WNW 4
23	93.1	92.4	93.9	93.1	7.2	9.8	6.3	7.4	11.1	6.1	97	78	91	89	0.3	2.7	0.8	1.3	10●	10●	0	WNW 1	W 4	C 0
24	97.7	101.1	105.4	101.1	5.4	11.8	5.0	6.8	13.5	2.3	97	81	95	91	0.3	2.6	0.4	1.1	9	9●	0	C 0	WNW 5	C 0
25	110.0	111.7	111.6	111.1	1.0	14.8	6.8	7.4	15.0	0.3	100	52	91	81	0.0	8.0	0.9	3.0	10≡⊙	6⊙	0	C 0	ESE 3	C 0
26	111.1	109.6	106.9	109.2	5.6	14.7	8.6	9.4	15.3	4.2	94	53	81	76	0.6	7.8	2.2	3.5	3⊙	6⊙	0	ESE 1	E 6	E 3
27	102.8	101.0	99.3	101.0	6.2	10.9	10.4	9.5	11.4	4.7	89	85	87	87	1.0	1.9	1.6	1.5	2⊙	10	10	NE 2	ENE 3	E 4
28	97.5	96.9	95.9	96.8	8.8	12.3	9.8	10.2	13.0	8.4	89	82	88	86	1.2	2.5	1.4	1.7	10	10	6	ENE 3	E 3	NNE 4
29	94.8	95.0	96.3	95.4	9.2	11.7	11.0	10.7	12.0	8.9	99	91	99	96	0.1	1.1	0.1	0.4	10●	10	10	NE 2	ENE 2	C 0
30	98.2	100.0	101.8	100.0	10.3	16.2	10.4	11.8	16.7	10.2	100	74	97	90	0.0	4.7	0.3	1.7	10≡	9⊙	0	C 0	ENE 2	C 0
31																								
M	93.3	93.6	93.6	93.5	8.8	14.1	10.4	10.9	15.2	7.2	92	70	88	83	1.0	5.3	1.5	2.6	7.8	8.0	5.1	3.8	6.0	3.2

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1	104.1	104.8	106.5	105.1	6.0	17.4	10.0	10.8	18.8	5.0	100	66	99	88	0.0	6.8	0.2	2.3	10≡	5⊙	10≡	C 0	SSE 1	C 0
2	108.1	109.0	108.8	108.6	6.7	17.4	10.2	11.1	18.3	6.4	100	69	95	88	0.0	6.3	0.6	2.3	5≡	9	0	C 0	C 0	C 0
3	108.9	108.8	107.5	108.4	6.8	17.6	8.9	10.6	17.8	5.9	100	59	93	84	0.0	8.2	0.8	3.0	10≡	6⊙	0	C 0	SE 6	SE 1
4	106.3	105.8	104.7	105.6	5.6	17.1	9.2	10.5	17.4	4.4	100	66	96	87	0.0	6.7	0.4	2.4	4≡⊙	9⊙	0	C 0	SSE 5	SSE 1
5	103.9	103.7	103.9	103.8	7.2	15.3	11.8	11.5	15.8	5.7	100	78	95	91	0.0	3.9	0.6	1.5	10≡	10	10●	C 0	SSE 3	C 0
6	104.3	106.3	108.0	106.2	9.8	14.4	9.5	10.8	14.8	9.5	96	87	100	94	0.5	2.2	0.0	0.9	10	10	0≡	C 0	W 3	C 0
7	110.8	113.3	114.4	112.8	11.9	12.8	11.0	11.7	13.9	9.1	99	86	87	91	0.1	2.1	1.6	1.3	10	10	10	WNW 2	NNW 2	NNW 1
8	114.9	115.3	113.6	114.6	9.8	11.1	8.7	9.6	11.7	8.5	83	73	86	81	2.0	3.6	1.5	2.4	10	10	0	WNW 1	WNW 3	NW 1
9	112.2	111.5	110.1	111.3	8.7	10.6	8.8	9.2	11.8	5.7	86	76	88	83	1.5	3.1	1.4	2.0	10	9	9	NNW 3	W 3	C 0
10	107.7	106.7	104.4	106.3	7.3	11.8	5.2	7.4	13.8	5.1	88	70	95	84	1.2	4.1	0.4	1.9	10	0⊙	0	C 0	WSW 2	C 0
11	101.6	99.7	95.1	98.8	1.6	9.2	2.4	3.9	10.8	1.1	100	91	100	97	0.0	1.1	0.0	0.4	10≡	10	0≡	C 0	SW 3	C 0
12	95.8	96.6	100.6	97.0	6.8	10.8	3.8	6.3	11.5	2.2	96	55	85	79	0.5	5.9	1.2	2.5	10	8⊙	8	W 1	WNW 3	N 2
13	102.5	101.7	98.5	100.9	3.1	10.6	2.0	4.4	11.4	1.8	90	50	91	77	0.8	6.4	0.7	2.6	8	6	0	C 0	SW 2	C 0
14	90.4	87.9	92.0	90.1	3.2	11.4	5.8	6.6	11.9	-0.3	83	67	80	77	1.3	4.4	1.8	2.5	8	9	10	C 0	WNW 5	N 5
15	98.7	101.3	104.3	101.4	0.6	7.4	0.6	2.3	8.2	-0.4	84	46	79	70	1.0	5.6	1.4	2.7	3⊙	6⊙	3	WSW 3	WNW 4	C 0
16	103.5	101.7	99.4	101.5	-0.4	6.8	5.6	4.4	8.5	-2.0	90	56	67	71	0.6	4.4	2.9	2.6	9	9	10	WSW 3	WNW 5	SW 3
17	98.3	99.1	97.8	98.4	5.8	9.8	8.8	8.3	9.9	5.1	86	83	89	86	1.3	2.0	1.2	1.5	10	10	10	WSW 4	WSW 6	SSW 4
18	93.9	91.2	83.1	89.4	9.0	11.3	11.0	10.6	11.5	8.1	90	80	87	89	1.1	2.6	1.6	1.8	10●	10	10	WSW 6	W 9	WSW 9
19	82.1	85.7	86.6	84.8	8.2	10.2	7.4	8.3	11.3	6.5	81	66	84	77	2.1	4.2	1.6	2.6	6	9	10	W 8	W 8	W 5
20	89.3	95.5	102.3	95.7	5.2	7.2	2.4	4.3	8.2	2.3	83	50	87	73	1.5	5.2	1.0	2.6	9	8	0	WNW 6	NNW 9	WNW 5
21	104.1	103.9	104.5	104.2	1.3	9.9	8.4	7.0	10.2	0.0	89	72	93	85	0.8	3.4	0.7	1.6	7	10	10	SW 3	WSW10	WNW 4
22	105.3	105.0	104.3	104.9	6.6	12.0	8.5	8.9	12.0	6.2	96	66	94	85	0.4	4.8	0.6	1.9	4⊙	6	10	W 3	WNW 5	W 3
23	101.8	101.8	101.4	101.7	7.2	8.6	7.8	7.8	8.7	6.4	86	85	93	88	1.5	1.7	0.8	1.3	10●	10	10	SW 3	SW 3	SW 4
24	97.7	97.0	98.0	97.6	6.4	10.0	6.2	7.2	10.4	5.3	84	68	83	78	1.6	3.9	1.6	2.4	10	10	10	SW 5	WSW 5	W 4
25	99.4	99.4	98.7	99.2	6.6	7.0	6.1	6.4	7.4	6.0	93	93	89	92	0.7	0.7	1.0	0.8	10	10	10	SW 2	SW 4	SSW 5
26	97.4	96.2	94.1	95.9	2.4	8.0	4.2	4.7	8.5	2.1	91	66	90	82	0.7	3.7	0.8	1.7	3⊙	0⊙	0	SW 4	S 8	S 4
27	88.9	90.2	96.2	91.8	4.2	6.8	2.6	4.0	9.0	2.3	88	91	91	90	0.9	0.9	0.7	0.8	3	10●	2	SSW 7	SW 4	WNW 1
28	95.0	92.1	89.6	92.2	0.4	3.9	7.2	4.7	7.2	0.1	100	97	94	97	0.0	0.3	0.6	0.3	10≡	10●	10●	C 0	SSE 5	ESE 4
29	90.4	91.3	94.0	91.9	4.6	6.2	4.6	5.0	7.2	4.4	95	89	92	92	0.4	1.0	0.7	0.7	10	10	10	C 0	W 2	W 3
30	95.4	95.8	94.9	95.4	3.4	7.7	-1.4	2.1	8.9	-1.6	98	77	100	92	0.1	2.4	0.0	0.8	8≡	6⊙	10≡	NNW 2	SSW 3	C 0
31	92.0	91.4	92.6	92.0	2.4	6.2	6.0	5.2	7.1	-1.6	98	89	95	94	0.2	1.0	0.5	0.6	10	10	10●	S 3	S 4	S 3
M	100.1	100.3	100.3	100.2	5.4	10.5	6.6	7.3	11.4	3.8	92	73	90	85	0.7	3.6	0.9	1.7	8.4	8.2	6.2	2.2	4.4	2.3

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	8	0.9	•	⛆°11^18-12^10 13^03-08 15^25-16^10 16^50-18^07; ⌓'np
2	7	0.2	•	⛆°11^05-35 •°13^40-14^10; =4^35-6^20 ≡'-7^40 =-a; ⌓² na-a
3	8	0.2	•	⛆°7^55-8^10; =21^30-23^40 ≡'-24; ⌓° na-a ⌓' np
4	7	•	•	≡'0^00-6^40 =-9^40; ⌓' na-a ⌓° np
5	7	2.9	•	⛆°15^35-40 ⛆^0-1 16^25-17^10 ⛆' 19^25-20^35; ⚐°16^05-17^40 SW-NE; =p; ⌓° na-a
6	7	0.4	•	⛆°9^20-45; ⤳ 12^05-13^10 15^05-17^20
7	7	6.5	•	•^0-1 6^10-11^10 •° 14^30 17^10 ⛆^1-2 -17^48; ⚐ 17^15-55 SW-NE; ⤳ 16^35-17^10 ⤳-⤳ 17^20-45 ⌒ 17^50-59
8	8	0.3	•	⛆°23^10-20; ⤳ 16^10-17^45
9	8	0.0	•	⛆°0^10-25; 14^10-42; =6^20-10^10; ⌓° np
10	7	•	•	⤳ 12^30-13^45; =5^25-8^20; ⌓² 0-9
11	6	6.3	•	•° 12^20 13^10 •^0-1 -19^38 ⛆°20^45-21^10 •°-22^05; ⌓° na-a
12	7	7.6	•	•^0-1 11^40-13^05 14^30-16^55 ⛆°17^30-45 ⛆^0-1 20^24-50; ⚐°20^23-21^40 S-N; ⤳ p; =na-a
13	8	0.0	•	⛆°2^02-20 5^30-38 11^35-40 15^50-16^05; ⤳ a,a-p; ⌓' np
14	6	2.7	•	⛆^1-0 12^15 15^05; ▲° 12^17-18 ▲' 12^33-36 ▲° 14^25-28; ⤳ 9^30-50 11^30-12^20; ⌓' na-a
15	8	•	•	≡'3^50-10^40 =-11^20; ⌓' na-a ⌓° np
16	7	3.3	•	•° 17^45 18^08; ⌓' na-a
17	7	7.6	•	⛆^1-0 1^35 3^20 ⛆°8^30-35 21^20-23^00 •°-24; ⚐°1^45-2^20 3^00-40 W-E, W-E; =na-a
18	7	23.9	•	•^0-1 0^00-5^40 •°6^20 9^58 •^0-2 17^25-23^10
19	8	2.8	•	•°8^40-10^20 11^15 ⛆°12^35-40 13^20-25 16^45-17^40 18^20-19^35 21^45-22^25; ⤳ 4^30 15^30
20	7	1.2	•	⛆°18^30-45 22^35-23^50; ⤳ 12^15-13^45
21	7	2.5	•	⛆°1^45 9^15 •° 12^40 ⛆°16^00 20^40; ⤳ 12^30-13^15
22	7	6.7	•	⛆°5^40-55 8^35-45 11^45-13^40 16^01-13 17^45-55 19^10-25 •° 21^45 22^10-24
23	7	0.9	•	•°0^00-13^05 ⛆°13^15-30 16^00-25 17^15-30
24	8	0.0	•	⛆°13^25-14^02 15^10-12; =7^10-9^45 np
25	8	•	•	=0^00-6^00 ≡'-9^30; ⌣° 0-6
26	8	•	•	=5^10-8^40; ⌓² 2-10
27	7	0.0	•	•° 17^05-40; ⌓² 2-10
28	7	0.0	•	
29	6	0.0	•	•°6^30 13^05 18^02-19^05; =5^30-8^45 =^1-0 -10^40 =-24
30	7	•	•	=0^00-5^40 ≡'-8^45 =-9^15 17^10-24; ⌓° p-np
31			•	
Σ	—	76.9	—	UWAGI

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1	1	•	•	=0^00-50 ≡^0-2 -8^50 =-9^30 16^15-18^20 ≡^1-2 -24
2	7	•	•	≡°0^00-7^50 =-8^30 17^30-20^20; ⌓° 19-24
3	7	•	•	=1^15-4^45 ≡^1-2 -7^45 =-9^30 19^40-24; ⌓° na,p-24
4	7	•	•	=0^00-5^10 ≡'-7^40 =-8^30 20^10-21^50 ≡'-24; ⌓' 0^00-a,p-np
5	6	1.0	•	•°20^40-21^05 •° 23^45-24; ≡^1-2 0^00-9^40 =-np
6	7	0.2	•	•°1^00...45 3^05 14^15; =na-12^45 18^30-19^45 ≡^1-0 -24
7	6	•	•	≡°0^00-4^10 =-19^30
8	7	•	•	=5^20-8^00 23^30-24; ⌓° na-a, np
9	7	•	•	=0^00-5^15 17^10-24; ⌓° na
10	7	•	•	=0^00-3^30 5^15-a 17^30-24; ⌓° p-24
11	5	•	•	=0^00-1^02 ≡^1-2 -10^50 =-18^35 ≡'-24; ⌓° na,p
12	8	•	•	≡'0^00-1^40 =-8^00
13	8	•	•	=16^45-24; ⌓° na-a,p-24
14	7	0.1	•	⛆°17^01-18^10 19^35-20^15; ⌓' na ⌣° na
15	8	0.0	•	⛆°13^40-46; ⌣' na-a, np
16	8	•	•	⌣' na-a
17	7	0.7	•	•°8^25 10^17 •° 12^35 13^36 •° 14^45-15^10 •° 17^25 21^48 24
18	7	1.4	•	•°0^00-5^35 6^20...40-7^35 •°-10^45 •° 14^40 15^10; ⤳ np; =na-a
19	8	0.0	•	•°0^05-3^15 ⛆°10^08-25; ⤳ 13^25-15^30; ⌓° np
20	8	0.0	•	⛆°5^15-25; ⤳ 9^20-10^45; ⌓° na
21	8	0.3	•	•°15^01 16^05-20^20; ⤳ 10^55-13^50; =16^40-24; ⌣° 3^00-a
22	8	0.0	•	•°0^00-1^40; =0^00-8^05
23	6	0.0	•	•°5^10-7^50 12^10-25 23^40 24; =8^10-15^20 21^30-24
24	7	•	•	•°0^00-2^10; =0^00-3^45 16^10-24
25	5	•	•	=0^00-24
26	7	•	•	=0^00-11^15 20^10-24; ⌓° na-a ⌓' 20-24
27	5	0.5	•	•°11^30-13^35; =0^00-14^30; ⌓' 0^00-7^50; p-24
28	5	7.2	•	⛆°10^10-12^10 •°-24; =5^10-20 ≡'-9^40 =-24; ⌓' na
29	6	0.3	•	•°0^00-6^10 7^05-8^20 •° 10^32-11^20 •° 16^45 18^10-19^45; =0^00-24
30	6	•	•	=0^00-4^45 ≡^0-1 -8^45 =-17^10 ≡^1-2 -24
31	6	0.5	•	•^1-0 20^15-22^40; ≡^2-0 0^00-5^45 =-24
Σ	—	12.2	—	UWAGI

Suwałki φ = 54°06' λ = 22°57' Listopad - Novembre 1962

DNI	CIŚNIENIE P − 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	91.4	89.5	90.0	90.3	7.1	9.9	10.8	9.6	11.0	5.9	100	95	90	95	0.0	0.6	1.4	0.7	10 ⚲	10 ⚲	0	SE 5	SE 6	SE 7
2	90.7	93.1	95.0	92.9	10.8	11.4	11.4	11.2	11.9	10.5	94	90	95	93	0.9	1.4	0.7	1.0	10	10	10	SE 3	SE 6	SE 3
3	96.3	96.9	98.3	97.2	10.0	11.4	9.8	10.2	11.6	9.8	100	100	96	99	0.0	0.0	0.5	0.2	10 ⚲ ≡	10 ⚲ ≡	10	C 0	SE 1	SE 2
4	98.6	99.6	100.5	99.6	10.7	11.2	9.8	10.4	11.4	9.0	100	96	92	96	0.0	0.5	0.9	0.5	10 ≡	10	10 ⚲	SE 3	SE 5	SE 5
5	99.9	100.0	101.1	100.3	7.8	11.4	4.8	7.2	11.4	4.5	91	52	70	71	0.9	6.5	2.6	3.3	10	0 ⊙	0	SE 7	SE 8	SE 8
6	101.0	101.0	103.3	101.8	0.4	9.2	5.0	4.9	9.3	0.2	82	43	55	60	1.1	6.6	3.9	3.9	0	2 ○	4	SE 4	SE 10	SE 10
7	105.3	105.8	106.9	106.0	1.2	8.5	2.0	3.4	8.7	0.8	79	44	71	65	1.4	6.3	2.1	3.3	2	3 ○	0	SE 7	SE 9	SE 6
8	105.3	102.6	102.6	103.5	-1.6	7.4	2.3	2.6	8.2	-1.8	89	62	93	81	0.6	3.9	0.5	1.7	0	2 ○	0	SE 4	SE 7	SE 2
9	102.3	102.4	104.0	102.9	1.0	5.4	1.8	2.5	5.8	0.2	100	74	83	86	0.0	2.4	1.2	1.2	10 ≡	9	10	E 6	E 7	E 8
10	105.1	105.2	106.0	105.4	-0.2	1.6	0.4	0.6	1.8	-0.6	78	65	67	70	1.3	2.4	2.1	1.9	10	9	10	E 10	E 10	E 10
11	107.6	108.3	108.4	108.1	0.4	1.4	0.3	0.6	1.7	-0.2	78	72	71	74	1.4	1.9	1.8	1.7	10	10	10	E 10	E 10	E 10
12	107.8	105.6	103.7	105.7	-1.0	1.0	-0.8	-0.4	1.7	-1.4	91	73	85	83	0.5	1.8	0.9	1.1	10	10	10	SE 9	SE 8	SE 8
13	101.5	102.3	102.5	102.1	-0.4	0.0	0.2	0.0	0.3	-1.4	90	94	100	95	0.6	0.4	0.0	0.3	10 ●	10	10 ≡	SE 5	SE 5	SE 4
14	100.4	99.8	98.3	99.5	0.3	1.6	2.2	1.6	2.3	0.1	98	94	100	97	0.1	0.4	0.0	0.2	10 ●	10	10 ⚲ ≡	SE 3	SE 2	SE 3
15	93.3	89.9	85.4	89.5	2.2	5.9	5.3	4.2	5.5	2.0	100	100	97	99	0.0	0.0	0.3	0.1	10 ⚲ ≡	10 ⚲ ≡	10 ●	SE 5	S 4	SE 6
16	82.5	84.6	86.5	84.5	3.4	2.4	0.0	1.4	6.2	-0.1	88	80	90	86	0.9	1.5	0.6	1.0	10	10	4	W 3	SW 4	W 2
17	89.4	91.7	95.7	92.3	-1.7	-0.4	-2.0	-1.5	0.4	-2.4	90	86	83	86	0.6	0.8	0.9	0.8	10	10	10	WSW 5	W 3	SW 4
18	95.9	92.8	90.8	93.2	-2.2	-0.8	-0.2	-0.8	-0.1	-2.5	85	81	86	84	0.8	1.1	0.8	0.9	10	10	10	SE 8	SE 12	SE 10
19	83.6	82.9	88.9	85.1	0.4	5.4	2.1	2.5	6.0	-0.4	94	86	93	91	0.4	1.3	0.5	0.7	10 ○	10	10	SE 10	S 8	S 3
20	85.3	85.2	80.9	83.9	4.0	7.4	8.6	7.2	8.9	1.3	98	96	96	97	0.1	0.5	0.5	0.4	10	10 ○	10 ○	C 0	E 3	SE 6
21	88.0	90.0	91.6	89.9	2.4	2.4	0.6	1.5	9.2	0.4	95	84	88	89	0.4	1.2	0.8	0.8	10	8	10	W 3	W 2	N 2
22	89.1	88.9	93.5	90.5	1.1	2.6	1.8	1.8	2.9	0.1	92	84	87	88	0.5	1.2	0.9	0.9	10	10	10	N 5	NNW 5	SW 3
23	99.1	100.3	102.5	100.6	-0.2	0.6	0.2	0.2	1.9	-1.5	98	98	96	97	0.1	0.1	0.3	0.2	10 ✳	10 ✳	10 ✳	S 4	S 1	SW 1
24	104.7	106.5	109.4	106.9	-0.6	-0.7	-1.0	-0.8	0.4	-1.3	89	87	85	87	0.6	0.7	0.9	0.7	10	10	10	W 2	NW 2	NW 1
25	110.2	109.7	108.5	109.5	-5.0	-2.6	-0.8	-2.3	-0.7	-5.1	95	100	95	97	0.2	0.0	0.3	0.2	10 ≡	8 ≡ ⊙	10	C 0	SW 1	SW 1
26	109.6	110.5	110.6	110.2	-3.2	2.4	0.2	-0.1	3.5	-3.5	97	77	98	91	0.1	1.7	0.1	0.6	0	0 ⊙	10	C 0	SW 2	SW 2
27	108.8	108.5	106.7	108.0	0.4	2.2	2.0	1.6	2.2	-0.2	94	96	100	97	0.4	0.3	0.0	0.2	10 ⚲	10 ⚲	10 ⚲ ≡	SW 2	SW 2	SW 3
28	99.4	97.2	98.1	98.2	2.5	3.2	3.0	2.9	3.7	2.0	96	88	95	93	0.3	0.9	0.4	0.5	10	10 ⚲	10	SW 8	SW 5	WSW 3
29	98.3	97.4	89.9	95.2	1.8	3.0	3.8	3.1	3.9	1.5	94	84	95	91	0.4	1.2	0.4	0.7	10	10	10 ●	C 0	SW 5	SW 4
30	84.6	89.4	96.5	90.2	2.4	0.7	-2.0	-0.2	5.2	-2.1	91	81	79	84	0.7	1.2	1.1	1.0	10 ●	8	0	W 5	NW 4	W 6
31																								
M	97.8	97.9	98.5	98.1	1.8	4.1	2.7	2.8	5.2	0.8	92	82	88	87	0.5	1.6	0.9	1.0	8.7	8.3	7.9	4.5	5.2	4.8

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1	105.0	109.2	114.4	109.5	-4.6	-1.0	-3.6	-3.2	-0.7	-5.7	91	73	80	81	0.4	1.6	0.9	1.0	5	3 ⊙	0	C 0	NW 7	NW 4
2	116.0	116.1	115.0	115.7	-2.8	1.3	0.0	-0.4	1.5	-4.6	91	79	86	85	0.5	1.4	0.8	0.9	6	8 ⊙	10 ✳	WSW 2	WSW 6	WSW 7
3	112.7	110.9	108.0	110.5	-2.2	-0.8	-3.0	-2.2	0.0	-3.1	83	69	77	76	0.9	1.8	1.1	1.3	10	10	10	WSW 7	SW 6	WSW 3
4	102.4	100.5	96.9	99.9	-2.6	-0.8	-0.4	-1.0	-0.3	-4.5	91	91	92	91	0.5	0.5	0.5	0.5	10 ⚲	10 ⚲	10	SW 5	WSW 3	SW 4
5	95.9	101.0	105.1	100.7	2.0	2.6	2.6	2.4	3.1	-1.0	87	95	91	91	0.9	0.4	0.7	0.7	10	10	10 ⚲	NW 4	NW 3	W 2
6	104.8	103.7	102.8	103.8	2.0	1.4	1.2	1.4	3.0	-1.1	94	100	94	96	0.4	0.0	0.4	0.3	10 ⚲	10 ⚲ ≡	10 ⚲	WSW 5	WSW 6	WSW 6
7	100.7	100.4	102.6	101.2	-1.0	2.4	2.6	1.6	3.1	-1.2	87	70	84	80	0.7	2.2	1.2	1.4	9	6 ⊙	10	WSW 7	SW 6	NW 5
8	105.9	107.3	105.2	106.1	0.8	2.8	-0.4	0.7	3.0	-0.5	85	70	86	80	1.0	2.2	0.8	1.3	9	10	8	C 0	WNW 2	WSW 7
9	96.0	86.9	79.3	87.4	-3.6	1.0	0.8	-0.2	1.1	-3.7	94	73	90	86	0.3	1.8	0.7	0.9	6	8 ⊙	10	S 4	SSW10	SSW11
10	73.6	74.7	76.7	75.0	1.8	1.3	2.0	1.8	2.9	0.3	80	91	91	87	1.5	0.6	0.7	0.9	10 ●	10 ✳	10	WSW12	SSW12	SW 8
11	77.3	79.0	79.7	78.7	1.8	2.1	-0.2	0.9	2.6	-0.3	89	78	94	87	0.8	1.5	0.4	0.9	10	5 ⊙	9	SW 5	SW 3	SSW 6
12	74.5	73.7	74.7	74.3	0.4	0.7	0.8	0.7	1.5	-0.2	90	94	85	90	0.6	0.4	1.0	0.7	10 ✳	10 ●	10 ●	S 8	SSW 8	S 7
13	78.0	79.4	79.3	78.9	-0.5	0.2	0.4	0.1	1.1	-0.6	88	78	82	83	0.7	1.4	1.1	1.1	10	10	10	S 4	S 3	S 2
14	79.7	80.0	79.7	79.8	0.4	0.6	0.6	0.6	1.1	0.2	90	96	100	95	0.6	0.3	0.0	0.3	10 ✳	10 ✳	10 ≡	S 2	C 0	S 3
15	74.6	68.0	60.4	67.7	-1.2	-2.0	-2.0	-1.8	0.6	-2.5	89	79	92	87	0.6	1.1	0.5	0.7	10 ✳	7 ⊙	10 ✳	SW 4	SSE 5	SSW 4
16	55.7	56.4	59.7	57.3	-0.2	0.1	-1.2	-0.6	0.5	-2.3	96	94	93	94	0.2	0.4	0.4	0.3	10 ✳	10	10 ✳	SSE 2	SSE 2	SSE 2
17	66.4	69.6	74.9	70.3	-2.4	-3.4	-5.0	-4.0	-0.6	-5.0	93	92	90	92	0.3	0.4	0.4	0.4	10	10 ✳	10 ✳	NNE 5	N 6	NNE 2
18	76.9	77.7	80.3	78.3	-6.4	-6.7	-8.1	-7.3	-4.9	-9.0	89	86	90	88	0.4	0.5	0.3	0.4	10 ✳	9 ✳	10 ✳	NE 2	NNE 1	NE 1
19	84.3	87.4	94.3	88.7	-9.2	-10.1	-16.3	-13.0	-8.1	-16.3	88	81	81	83	0.4	0.5	0.5	0.4	10	10 ✳	0	NE 3	NE 3	N 2
20	100.6	103.0	105.2	102.9	-19.9	-15.6	-18.7	-18.2	-15.1	-20.8	83	81	89	84	0.2	0.3	0.1	0.2	1	9	0	C 0	NNE 3	NE 1
21	104.0	102.8	105.6	104.1	-18.2	-16.3	-19.3	-18.3	-16.2	-20.0	90	81	83	85	0.2	0.3	0.3	0.3	8	3 ⊙	0	NNE 2	NE 5	NE 2
22	111.1	115.7	120.8	115.9	-19.5	-15.3	-20.6	-19.0	-15.1	-20.6	83	68	75	75	0.2	0.6	0.3	0.4	0	0 ⊙	0	NNE 2	NNE 4	NNE 6
23	124.7	126.3	127.5	126.2	-17.6	-11.9	-15.7	-15.2	-11.8	-21.8	79	75	86	80	0.3	0.6	0.3	0.4	0	0 ⊙	0	NNE 3	NNE 4	N 1
24	124.9	123.2	122.3	123.5	-7.7	-5.4	-5.4	-6.0	-4.0	-16.2	81	75	90	82	0.6	1.0	0.4	0.7	10	3 ⊙	10	C 0	NNE 1	C 0
25	117.3	113.4	106.7	112.5	-5.0	-4.2	-6.0	-5.3	-3.8	-6.2	85	84	89	86	0.6	0.7	0.4	0.6	10 ✳	10 ✳	10 ✳	NNW 1	C 0	C 0
26	98.3	95.0	92.5	95.3	-7.3	-10.5	-14.5	-11.7	-5.7	-14.5	85	80	87	84	0.5	0.5	0.3	0.4	10 ✳	9 ✳	10 ↔	SSW 2	SSW 2	C 0
27	90.4	90.4	92.0	90.9	-12.8	-10.9	-11.1	-11.5	-10.9	-14.6	88	73	83	81	0.3	0.7	0.4	0.5	10 ✳	8 ⊙	10 ✳	C 0	C 0	C 0
28	91.4	91.4	92.6	91.8	-11.1	-8.5	-7.8	-8.8	-7.7	-11.3	86	83	87	85	0.4	0.5	0.4	0.4	10 ✳	10 ✳	10 ✳	C 0	SSW 3	SSW 3
29	93.3	92.2	87.9	91.1	-7.6	-7.3	-8.8	-8.1	-6.8	-10.3	87	85	89	87	0.4	0.5	0.4	0.4	10	10 ✳	10 ✳	SSW 2	S 4	S 4
30	87.1	90.2	95.1	90.8	-7.9	-9.5	-11.3	-10.0	-7.7	-14.3	90	85	90	88	0.3	0.4	0.3	0.3	10 ⚲	2 ⊙	10 ✳	W 2	NNW 2	NNE 4
31	99.2	101.7	104.6	101.8	-16.1	-16.1	-19.1	-17.6	-11.1	-19.1	76	76	77	76	0.4	0.4	0.3	0.4	7 ↔	6 ↔	0	NNE 1	NE 2	C 0
M	94.3	94.4	94.9	94.5	-5.7	-4.3	-6.0	-5.6	-3.4	-8.1	87	82	87	85	0.5	0.8	0.5	0.6	8.4	7.6	7.6	3.1	3.9	3.3

Suwałki H_0 = 165m H_0 = 169,6m h_w = 13m Listopad - Novembre 1962

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ LODU h	POGODA
1	5	0.1	•	•°6^20-13^25; =0^00-6^35 ≡°-9^00 =-14^20; 16^10-24
2	6	0.3	•	•°22^45-23^20 •'-24; =0^00-2^10; 6^15-23^40 ≡°-24
3	1	0.6	•	•°0^00-2^40...46 6^20-7^40; 12^20-18^15; ≡°0^00-1^45 =-3^10 ≡°-2-18^45 =...24
4	6	0.2	•	•°7^35-8^10; 10^35-11^45; 20^20-21^35; =0^00-2^50 ≡'-2-9^25 =-17^30
5	8	•	•	=4^15-9^15
6	7	•	•	≫9^10-24; ⌣°3-8
7	7	•	•	≫9^15-12^10; ⌣°3-9
8	7	•	•	=8^15-10^30; ⌣°2-9
9	7	0.0	•	•°16^45-17^10; ≫13^30-15^45; =1^15-5^35 ≡°-7^40 =-10^30; ⌣° na
10	7	•	•	≫2^55-5^10; 6^56-7^10; 10^45-17^10; 19^10-22^40
11	8	0.0	•	*°13^10-15^45; ≫4^15-7^45; 12^15-13^45; 19^10-24
12	7	3.3	•	*°1^15...2^20; 16^10-18^20 △°-19^35 •°-20^05; ≫3^55-4^00
13	5	0.2	pł.	⛈°1^05-3^40; 5^35-6^20 •°-8^20 ⛈°-11^45; =0^30-14^45 ≡'-°-24; ∼°1^05-14^00
14	5	1.2	•	•°3^50-4^50 •°...8^05; 9^25-10^48 •°'16^40-24; ≡°0^00-2^40 =-12^40 ≡°-2-24
15	3	13.3	•	•°-0^00-7^05 •°-8^10 •°-15^30 •°-24; ≡°0^00-3^15 =-5^30 ≡°-2-14^45 =-24
16	6	0.1	•	•°0^00-6^10; 7^15-8^30; 8^50-9^25; =0^00-24; ⊟ 21^35-22^20
17	7	•	•	=0^00-20; ⌣'na-p; ⊟ 0^15-40
18	7	2.2	•	≫8^10-10^50 ≫-≋-15^30 ≫-24
19	7	8.4	pł.	*°-1 3^50-5^40 •°-7^45; 7^55-8^50 *°9^10-10^15 •°-11^25 22^35-24; ≫0^00-9^30
20	5	10.5	•	•°-1 0^00-5^35; 8^45-10^30 •°-11^35 •°-1 12^15-24; ≡'-°; =5^50-24
21	6	•	•	•°0^00-1^25; =0^00-20^10
22	7	0.3	•	
23	5	2.2	•	*°5^45-14^40; 19^30-23^30...24; ≡'1^38-2^25 ≡²-5^40 =-24
24	6	•	1	*°0^00...1^30-3^45; =0^00-24
25	2	•	•	=0^00-6^35 ≡°-2-13^40 =-24; ⌣'na-24
26	6	0.0	•	•°17^40-20^10; =; ≡°0^00-24; ⌣°0^00-a
27	5	0.9	•	•°3^45-13^15; 17^40-18^25; 20^15-24; =0^00-14^50 ≡°-2-21^30 =-24
28	6	1.2	•	•°0^00-11^50...15^20 •'-16^40 •'19^25-20^45; =0^00-24
29	7	5.7	•	•°13^45-14^40; 16^40...18^10-24; ≫20^30-24; =0^00-11^30
30	8	1.1	•	•°0^00-7^40 ⛆8^50-9^40 ⛆10^45-11^02; 11^45-50; ≫0^00-45; 2^10-55
31				
Σ	—	51.8	—	UWAGI

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1	8	•	•	⌣'2-11; 17-24
2	8	0.0	•	*°17^30...18^15; 20^15...22^10; ⌣'0^00-17^00
3	7	0.4	•	
4	5	0.0	•	⛆°1^35-10^50 •°-12^30; =1^25-24; ∼°2^40-15^00
5	6	0.0	•	•°17^25-18^30; 20^05-22^40 •'-24; =na, a-p, np ≡°22^40-23^45 =-24
6	3	0.4	•	•'0^00-1^20 •°-2^05...9^30; 12^25-21^10; =; ≡°0^00-24
7	7	•	•	=0^00-12^10; 14^45-24
8	7	•	•	=0^00-2^30
9	6	0.0	•	≫9^40-14^35; 20^05-24; =1^00-21^10
10	7	0.3	•	•°6^20-7^25 ⛆°11^45-12^15 ⛆°-13^30 ⛆°-15^35; ≫-≋ 0^00-6^43 ≫-18^15
11	7	2.9	•	⛆°0^05-1^00 ⛆°-1^25 •°7^10-8^00 ⛆°-8^50 ⛆°13^50...16^42 *°21^40-24; =np; ⌣°np
12	5	2.3	1	*°0^00-1^25 •°-4^15 *°-12^10 •°...13^45 *°..14^20; 18^20-19^10 •°...21^35; =0^00-23^10
13	7	0.9	1	*°16^40-18^20; 23^45-24; =15^30-18^35
14	5	3.4	2	*°0^00-3^45; 6^10-10^30 •°21^20-22^50 *°-23^15; =0^00-17^40 ≡²-0-22^50 =-24
15	7	2.8	2	*°3^15-7^35; 14^20-24; =0^00-1^15; 22^10-24
16	7	0.0	5	*°0^00-2^25; 5^05-9^55; 19^30-22^10; 23^25-24; =0^00-9^55
17	6	0.4	5	*°0^00-40; 10^25-13^40; 14^15-16^45; 19^40-24; =a, a-24
18	6	0.4	6	*°0^00-12^30...15^10; 20^10...24; =0^00-12^00
19	6	0.4	6	*°0^00...6^30; 8^05-15^05...16^45
20	8	•	7	
21	7	•	7	
22	8	•	7	
23	7	0.0	7	=23^40-24
24	8	0.1	7	*°0^00-6^35; 8^02...9^55; 21^15...24
25	6	0.7	7	*°0^00...7^10-16^40; 18^25-24; =8^30-24
26	7	0.2	8	*°0^00-4^40 5^05...17^10 ↔°20^10-21^10 *°...24
27	6	0.2	9	*°0^00...2^15-10^40; 14^25...20^05-24; =10^10-24
28	6	0.1	10	*°0^00-16^40; 20^10-24; =0^00-24
29	6	0.8	10	*°0^00-6^10; 9^25-13^35; 18^20-24; =0^00-24
30	6	0.0	11	*°0^00-2^10 ⛆°2^45-6^40 *°9^30...11^10; 20^15-24; =0^00-24; V°19^15-24
31	6	0.0	11	*°0^00-4^10 ↔°-7^40; 10^16-14^45; =0^00-24; V°0^00-24
Σ	—	16.7	—	UWAGI

Olsztyn-Dajtki φ=53°46' λ=20°25' Styczeń - Janvier 1962

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D.v I	II	III
1	83.7	85.7	86.1	85.2	2.3	2.6	1.4	1.9	3.9	-1.5	93	70	72	78	0.5	2.2	1.9	1.5	10	9	9	SSW 6	WSW 9	SW 6
2	88.2	90.7	95.4	91.4	-0.6	-0.8	-2.5	-1.6	1.5	-2.7	88	95	78	87	0.7	0.3	1.1	0.7	10	10 ✳	9	SW 5	W 7	W 5
3	96.2	99.9	106.0	100.7	-3.9	0.7	0.0	-0.8	1.5	-6.2	89	90	96	92	0.5	0.6	0.2	0.4	9	6 ✳	9	W 7	W 4	W 4
4	108.0	106.8	105.3	106.7	-1.8	-0.7	-0.9	-1.1	0.3	-2.8	94	87	97	93	0.3	0.7	0.2	0.4	10	10	10 ●	W 5	WSW 6	WSW 5
5	103.2	101.6	96.1	100.3	-0.9	-0.3	-1.8	-1.2	0.0	-1.8	97	98	98	98	0.2	0.2	0.1	0.2	10 ●	10 ●	10	WSW 5	WSW 5	SW 6
6	91.1	89.7	87.9	89.6	-5.1	-1.8	0.2	-1.1	0.5	-3.9	93	98	100	97	0.4	0.1	0.0	0.2	10 ✳	10 ●	10	SW 7	SW 6	W 6
7	93.4	100.3	106.7	100.1	1.1	1.0	0.2	0.6	1.6	0.1	96	94	98	96	0.2	0.4	0.1	0.2	10	9	8	W 5	W 4	W 3
8	106.4	106.1	106.6	106.4	-2.3	-0.1	0.5	-0.4	0.7	-4.9	98	94	100	97	0.1	0.4	0.0	0.2	10	10	10	SW 2	SW 3	SW 1
9	103.9	101.0	97.3	100.7	0.9	1.4	-1.4	-0.1	1.7	-1.5	96	92	78	89	0.2	0.6	1.2	0.7	10	10	0	SSW 2	S 5	S 5
10	94.1	92.0	88.8	91.6	-0.8	-0.3	-2.4	-1.5	-0.1	-3.2	87	84	82	84	0.7	1.0	0.9	0.9	10	9	6	S 3	S 5	S 6
11	87.5	86.7	82.1	85.4	1.9	3.0	3.6	3.0	3.8	-2.4	82	74	76	77	1.3	2.0	1.9	1.7	10	4 ⊙	10	S 6	S 4	S 7
12	85.3	86.0	80.6	84.0	4.0	3.4	1.5	2.6	4.1	1.3	83	91	100	91	1.3	0.7	0.0	0.7	10	10	10	S 4	SW 4	S 3
13	69.3	71.5	74.9	71.9	1.1	2.9	3.0	2.5	3.2	0.8	98	89	71	86	0.1	0.8	2.2	1.0	10 ✳	10	7	S 6	SW 5	SW 6
14	78.5	81.1	84.0	81.2	0.3	2.1	1.8	1.5	3.0	0.0	86	84	83	84	0.8	1.2	1.2	1.1	3	10	9	SW 5	SW 7	SW 4
15	87.2	92.0	96.9	92.0	2.2	2.1	2.1	2.1	2.6	1.3	93	96	95	95	0.6	0.3	0.4	0.4	10	10 ●	10	WSW 4	WSW 5	SW 3
16	101.1	101.6	98.6	100.4	1.5	2.1	1.4	1.6	2.3	0.5	92	80	76	83	0.5	1.4	1.7	1.2	10	10	9	SW 5	SW 5	SSW 5
17	95.4	96.3	98.0	96.6	0.8	1.6	1.6	1.4	2.5	0.7	96	91	80	89	0.3	0.7	1.4	0.8	10 ✳	10 ✳	4	SW 4	SSW 4	SW 4
18	96.4	94.8	94.8	95.3	-0.3	1.6	1.6	1.1	2.5	-0.5	86	80	83	83	0.9	1.4	1.2	1.2	4	9	9	S 3	S 5	S 4
19	97.1	97.5	92.9	95.8	2.2	3.0	1.8	2.2	3.0	0.9	95	88	100	94	0.4	0.9	0.0	0.4	10	7	10 ═	WSW 4	SW 4	S 4
20	88.3	89.7	98.0	92.0	2.8	3.9	3.2	3.3	4.7	1.8	89	90	95	91	0.8	0.8	0.4	0.7	9 ●	9 ●	10 ●	SW 6	WSW 7	W 6
21	96.6	99.5	98.3	98.1	2.9	4.0	1.8	2.6	4.1	0.4	95	87	98	93	0.4	1.1	0.2	0.6	10 ●	7	10 ●	WSW 7	WSW 5	SSW 3
22	91.9	86.9	85.6	88.1	5.4	6.6	5.4	5.7	7.2	1.6	98	87	75	87	0.2	1.3	2.3	1.3	10 ●	8	9	SW 3	S 3	S 6
23	89.5	92.1	92.9	91.5	2.4	3.4	2.6	2.8	5.4	2.2	79	71	77	76	1.6	2.2	1.7	1.8	9	5 ⊙	9	SW 7	SW 8	SW 6
24	95.1	95.7	96.1	95.6	2.4	2.0	1.4	1.8	2.7	1.1	91	93	87	90	0.7	0.6	0.9	0.7	9 ●	9 ✳	10	SW 6	WSW 5	SW 3
25	93.3	90.2	90.2	91.2	-0.4	1.4	0.4	0.4	1.6	-0.7	98	94	100	97	0.1	0.4	0.0	0.2	10	10 ✳	10 ✳	SE 3	ESE 5	NE 2
26	97.1	99.6	97.9	98.2	-2.5	0.1	-2.5	-1.8	0.6	-4.4	95	81	98	91	0.3	1.2	0.1	0.5	9	2	2	N 1	W 2	SW 1
27	94.0	92.3	91.3	92.5	-1.2	-0.3	0.4	-0.2	0.8	-2.6	97	98	98	98	0.2	0.2	0.1	0.2	10 ✳	10 ●	10 ✳	SW 1	SW 1	SW 1
28	90.5	91.3	98.9	93.6	-2.7	-4.2	-6.8	-5.1	0.5	-7.1	86	87	80	84	0.7	0.6	0.7	0.7	9	9 ✳	9	W 7	NNE 10	N 8
29	106.9	112.0	116.7	111.9	-8.5	-9.4	-12.6	-10.8	-6.6	-13.0	80	82	85	82	0.6	0.5	0.4	0.5	10 ✳	6 ✳	0	NNE 8	NNE 7	NE 4
30	120.4	120.2	124.0	121.5	-15.8	-11.0	-16.4	-14.9	-9.9	-17.2	86	80	85	84	0.3	0.5	0.2	0.3	10	0	0	C 0	E 3	NE 1
31	122.7	121.7	118.2	120.9	-20.9	-12.1	-16.1	-16.3	-9.4	-23.0	89	78	86	84	0.1	0.5	0.2	0.3	0	0	0	C 0	E 2	C 0
M	95.2	95.9	96.4	95.8	-1.0	0.3	-0.9	-0.6	1.3	-2.8	91	87	88	89	0.5	0.8	0.7	0.7	9.1	8.0	7.7	4.4	5.0	4.1

Luty - Février

1	109.4	102.6	100.0	104.0	-15.6	-8.0	-9.3	-10.6	-7.3	-17.6	81	75	85	80	0.3	0.8	0.4	0.5	0	3	0	SE 1	E 4	SE 4
2	99.4	100.0	103.7	101.0	-11.5	-5.5	-7.2	-6.0	-3.7	-13.3	90	80	90	87	0.3	0.8	0.3	0.5	10	6	0	S 3	SSW 4	SSW 2
3	106.5	108.4	107.7	107.5	-5.6	0.1	-3.8	-3.3	1.2	-9.1	90	75	87	84	0.4	1.6	0.6	0.9	9	9	0	SSW 1	WSW 2	SW 1
4	100.4	97.2	98.9	98.8	-3.3	-2.0	-1.2	-1.9	-0.5	-4.6	90	89	95	91	0.5	0.6	0.3	0.5	9	10 ✳	0	SW 6	S 6	SW 5
5	97.5	90.0	82.5	90.0	-2.8	-0.9	-0.7	-1.3	0.0	-3.7	97	95	97	96	0.1	0.3	0.2	0.2	10	10	10 ✳	SW 5	S 4	S 4
6	83.0	89.8	98.2	90.3	0.6	0.2	0.1	0.2	1.5	-0.8	96	92	90	93	0.3	0.5	0.6	0.5	10 ✳	10 ✳	10	W 8	W 9	WNW 5
7	100.4	100.0	97.2	99.3	-1.8	1.8	0.7	0.4	2.0	-1.8	92	80	90	87	0.4	1.5	0.6	0.8	9	9	10 ✳	WSW 2	S 4	SSE 6
8	94.4	94.5	95.9	94.9	-0.6	-0.1	0.8	0.2	0.8	-1.0	75	82	98	85	1.4	1.1	0.2	0.9	10	10 ✳	10	SSE 5	S 4	S 3
9	98.7	103.1	110.3	104.0	1.3	1.6	0.1	0.8	1.8	-0.4	100	91	90	94	0.0	0.7	0.6	0.4	10	10	10	SW 2	W 3	WNW 4
10	112.8	111.6	108.7	111.0	-3.2	1.3	0.8	-0.1	1.7	-3.4	97	77	92	89	0.1	1.5	0.5	0.7	10	10	10 ● ✳	SW 2	SSW 5	SW 5
11	101.3	99.7	102.0	101.0	1.2	0.8	0.6	0.8	2.0	0.4	92	98	78	89	0.5	0.2	1.4	0.7	10 ●	10 ● ✳	8	SW 6	WSW 6	WSW 7
12	89.8	71.0	59.1	73.3	0.2	0.4	1.6	1.0	4.4	-0.8	75	96	89	87	1.5	0.3	0.8	0.9	10 ✳	10 ✳	9	SW 7	S 10	SW 9
13	60.4	63.3	67.7	63.8	0.7	0.7	-1.7	-0.5	2.5	-2.0	75	60	71	69	1.6	2.6	1.6	1.9	9	3	0	SW 12	W 9	W 4
14	72.1	75.6	82.4	76.7	-3.9	0.3	-4.1	-2.9	1.1	-4.3	96	72	89	86	0.2	1.7	0.5	0.8	4	4 ⊙	0	SW 3	N 3	NW 3
15	88.3	92.3	97.3	92.6	-4.1	-2.8	-4.7	-4.1	-2.3	-5.7	68	80	88	79	1.4	1.0	0.5	1.0	10	9	9	N 6	NNW 7	WNW 5
16	85.5	69.4	61.8	72.2	-6.4	-2.4	1.0	-1.7	2.6	-8.6	78	98	90	89	0.8	0.1	0.7	0.5	10	10 ✳	9	S 8	SSW 10	W 7
17	57.4	63.5	73.5	64.8	1.3	-1.6	-3.9	-2.0	2.0	-4.2	91	91	94	92	0.6	0.4	0.3	0.4	9	10 ✳	10 ✳	WNW 10	W 10	WNW 10
18	82.4	89.2	97.8	89.8	-3.5	-2.9	-3.8	-3.5	-2.6	-4.4	94	93	85	91	0.3	0.3	0.7	0.4	10 ✳	10 ✳	8	WNW 10	NW 11	NW 9
19	98.8	98.2	97.0	98.0	-8.6	-0.7	-0.6	-2.6	-0.5	-8.9	92	79	99	90	0.3	1.2	0.0	0.5	5	10	10 ✳	WNW 3	SW 3	SW 3
20	95.1	92.3	94.3	93.9	1.9	2.3	2.2	2.2	3.0	-0.6	96	95	84	92	0.3	0.4	1.2	0.6	10	10 ●	10 ●	WSW 4	W 5	W 8
21	99.0	103.8	112.3	105.0	-1.7	-2.9	-4.8	-3.6	2.2	-4.9	94	82	78	85	0.3	0.9	0.9	0.7	10 ✳	10 ✳	10	WNW 9	N 9	NE 8
22	117.5	118.7	120.0	118.7	-5.8	-4.9	-8.0	-6.7	-4.4	-9.1	84	78	81	81	0.6	0.9	0.6	0.7	10 ✳	9 ✳	9	NNE 6	NNE 7	NNE 3
23	115.7	112.9	110.9	113.2	-4.8	-4.6	-5.7	-5.2	-4.0	-9.0	81	76	87	81	0.8	1.0	0.5	0.8	8	9	10	NNW 5	NNW 6	N 4
24	107.2	106.8	109.1	107.7	-6.6	-4.6	-6.6	-6.1	-4.4	-7.4	88	76	86	83	0.4	1.0	0.5	0.6	10 ✳	9	8 ✳	NE 4	N 9	NE 6
25	111.4	113.3	112.2	112.3	-9.2	-5.8	-5.0	-6.2	-5.0	-9.7	88	77	90	85	0.4	0.9	0.4	0.6	10 ✳	4 ⊙	10 ✳	E 7	E 6	NE 6
26	110.4	109.5	109.2	109.7	-4.0	-5.2	-3.9	-5.8	-2.9	-5.3	91	86	82	86	0.4	0.7	0.8	0.6	10 ✳	10 ✳	10	NE 5	NNE 5	E 3
27	107.9	107.0	105.6	106.8	-4.8	-5.0	-8.8	-6.4	-2.6	-9.1	83	75	86	81	0.7	1.2	0.4	0.8	10	9	0	E 5	E 4	E 1
28	102.4	100.3	98.2	100.3	-11.5	-5.9	-11.7	-10.2	-4.9	-14.0	93	79	86	86	0.2	0.8	0.3	0.4	10	4	0	E 2	E 2	C 0
29																								
30																								
31																								
M	96.6	95.9	96.9	96.5	-4.0	-1.9	-3.1	-3.0	-0.6	-5.8	88	83	88	86	0.3	0.9	0.6	0.7	9.0	8.5	6.8	5.2	6.0	4.8

Olsztyn - Dajtki $H_s = 133m$ $H_t = 135{,}4m$ $h_w = 12m$ Styczeń - Janvier 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU s	POGODA
1	7	•	8	≡°0^00-1^20 =-10^30
2	6	1.0	7	*°-¹9^45-15^42
3	6	0.4	8	*°-¹7^25-12^40
4	7	0.0	8	☁18^16-24; =1^30-7^40; 17^30-24; ~18^16-24
5	4	0.0	8	☁0^00-18^50; =0^00-24; ~0^00-24
6	4	5.2	8	*°6^30-8^20 △-10^50 ☁-13^35 *°-¹-20^35; =0^00-24; ~0^00-23^00
7	8	0.5	9	*°0^00...4^50 •°8^22...9^15 ⚥°10^45-11^10; 13^54-14^15; =0^00-7^30
8	5	0.0	8	*°9^03-10^50; =3^40-4^30; 8^30-21^40 ≡'-24
9	6	•	8	☁°3^50-5^50; ≡'0^00-2^40 =-19^30
10	6	•	8	=7^30-24
11	7	•	8	=0^00-10^20; 14^30-24
12	6	3.8	6	=0^00-24
13	7	0.0	pł.	•°3^53-4^20 ⚥°-7^18 •°...8^45; 11^50-12^25; =0^00-12^30
14	7	0.0	pł.	⚥°12^55-13^25
15	6	0.5	pł.	•°3^52-4^13 ⚥°9^40-11^20 △-11^25 ⚥°-14^25; =14^20-24
16	6	0.0	pł.	=0^00-19^30
17	6	1.6	1	*°6^07-11^05 ⚥-13^45; =6^07-17^30
18	6	0.0	pł.	•°22^55-23^20; =8^30-24
19	6	1.6	pł.	•'23^50-24; =0^00-18^45 ≡°-21^50 =-24
20	7	7.4	•	•-°0^00-2^20 ⚥°6^40...23^14; =0^00-4^30
21	7	2.6	•	•°5^49-7^15 7^35-8^26; 20^35-24; =5^50-12^30 15^30-24
22	7	0.5	•	•°0^00-2^20 ☁°5^53-6^50 •°16^52-17^40; =0^00-12^30
23	7	0.8	•	⚥°21^45-22^05; 22^50-23^15 ⚥°-24
24	6	0.4	•	⚥°0^00-1^05 ⚥°5^55-7^10 ⚥°10^25-12^45; =11^30-24
25	5	2.0	•	⚥°11^54-14^10; =0^00-15^45 ≡°-17^50 =-24
26	8	0.8	2	*°0^00-2^20 ⚥°8^54-9^10; =0^00-3^30
27	5	4.9	3	⚥°4^55-7^05; 7^15-8^05 *°-¹9^20-12^25 ☁°-14^20 *°-15^05; 18^40-22^08; =5^30-15^06
28	6	1.4	8	*°1^37-2^48 ⚥°-¹7^10-16^36 ⚥12^50-17^15 ⚥-24
29	7	0.2	12	⚥'1^06-2^35 ⚥°4^11-11^38; 12^09-53 *°13^07...20^05; ⚥0^00-11^50; =14^30-19^30
30	7	•	12	=7^30-10^20
31	7	•	12	=7^30-10^20; 16^30-24
Σ	—	39.6	—	UWAGI.

Luty - Février

1	7	•	12	=0^00-12^20
2	6	0.0	11	*°10^54-11^20; =7^30-24
3	6	•	10	=0^00-24
4	5	0.1	9	*°10^54-13^49; =0^00-24
5	5	5.8	8	*°-¹15^20-21^48; =0^00-6^45 ≡°-9^35 =-22^30
6	4	2.8	13	⚥°0^55-1^40 ⚥°-¹11^36 *'-15^25 ⚥°16^40-17^23; =15^25-19^30
7	7	0.2	15	*°15^40-22^20 △-23^05; =15^30-21^30
8	6	2.1	14	*°-¹11^51-19^40 ☁20^33-24; =19^40-20^45 ≡°-24
9	7	0.3	13	☁0^00-2^46 ⚥°12^12-35 ⚥°13^05-17^20; ≡°-¹0^00-4^40 =-11^30
10	7	0.4	12	*°13^40-17^50 ⚥°-24; =4^40-11^30; 13^40-24
11	3	2.2	10	⚥°0^00-3^40 •°-5^10...6^55 ☁°8^35-9^15 *☁°-10^20 ⚥°-¹-13^10; =0^00-15^30
12	3	6.3	10	*°6^35-7^10 7^55...8^40 *'-14^45 ⚥°-15^58 •°-¹-20^05; ⚥8^40-14^45
13	8	0.0	8	⚥°5^45-6^20; 11^40-50; =0^00-6^30
14	8	0.0	7	⚥°16^07-30
15	8	0.0	6	⚥°0^41-44; 8^20-35; 12^51...16^08
16	3	7.4	7	*°-¹7^38-15^40 •°-16^25 ⚥°-17^52 *°21^54-22^45; ⚥8^20-14^40
17	6	1.5	10	⚥°0^45-6^05 ⚥°-¹9^56...24; ⚥13^20-15^10 ⚥-24
18	3	2.8	18	⚥°0^00-4^50 *°-¹-16^40 ⚥°-19^20; ⚥0^00-24
19	8	1.0	22	*°15^50-22^35 ☁°-24; ⚥°0^00-1^15; =22^30-24
20	6	1.6	20	☁0^00-4^40 7^45-8^55; 10^25-13^10 •°-15^05; 19^40-22^50 *°-23^45; =0^00-6^30
21	6	0.4	18	*°0^50-16^20; ⚥6^40-16^35
22	7	0.0	16	*°5^50-9^52; 12^30...16^10
23	8	0.0	15	
24	7	0.3	14	*°3^52-9^40 ⚥°14^54...24; ⚥13^10-17^00
25	7	1.2	15	⚥°0^00-5^50 *°9^10; 17^10-24
26	5	0.2	16	*°0^00-14^55; =16^30-24
27	6	•	16	=0^00-13^30; 17^10-24
28	7	•	15	=0^00-12^20; 19^40-24
29				
30				
31				
Σ	—	36.6	—	UWAGI.

Olsztyn-Dajtki φ=53°46' λ=20°25' Marzec - Mars 1962

Dni	Ciśnienie P=900 I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność względna U I	II	III	Dies	Niedosyt wilgotności I	II	III	Dies	Zachmurzenie i pogoda N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	96.0	95.2	93.8	95.0	-16.2	-4.9	-9.0	-9.8	-4.2	-17.0	86	73	82	80	0.2	1.1	0.5	0.6	0	0	0	C 0	E 5	E 1
2	90.2	88.6	87.3	88.7	-16.6	-6.4	-5.3	-8.4	-4.4	-17.5	85	78	82	82	0.2	0.8	0.7	0.6	0	9	10	C 0	E 1	S 1
3	87.4	88.2	88.2	87.9	-6.1	-0.4	-2.3	-2.8	0.5	-7.5	92	68	83	81	0.3	1.9	0.9	1.0	10	9	10	C 0	SW 1	C 0
4	83.8	81.4	80.3	81.8	-2.7	0.2	-1.3	-1.3	1.1	-3.0	95	98	99	97	0.2	0.1	0.1	0.1	10	9 ✳	10 ✳	SE 1	ESE 1	E 2
5	82.8	84.4	82.9	83.4	-2.3	-2.4	-2.7	-2.5	-1.1	-3.4	93	89	95	92	0.4	0.5	0.2	0.4	10 ✳	10	10	NE 4	NE 4	NE 4
6	76.2	78.8	91.8	82.3	-1.0	-3.0	-1.1	-1.6	-0.7	-3.2	97	90	89	92	0.2	0.5	0.6	0.4	10 ●	10 ✳	10 ✳	NE 5	NW 6	NW 6
7	100.5	103.8	107.3	103.9	-4.4	-1.7	-6.9	-5.0	-1.1	-7.4	86	79	94	86	0.6	1.1	0.2	0.6	10 ✳	8	0	WNW 6	NNW 3	C 0
8	108.8	107.5	108.4	108.2	-12.4	-1.5	-4.4	-5.7	-0.5	-13.3	93	82	89	88	0.2	1.0	0.5	0.6	2	2	0	C 0	SW 3	W 5
9	111.2	111.6	107.8	110.2	-7.7	-3.3	-4.9	-5.2	-1.2	-10.3	96	83	83	87	0.1	0.8	0.7	0.5	10 ═	4	0	E 1	E 3	SE 2
10	101.2	98.2	94.5	98.0	-4.5	0.2	-1.1	-1.6	1.4	-5.4	84	62	73	73	0.7	2.4	1.6	1.6	7	8	3	SSE 6	SSE 5	SSE 4
11	89.9	89.0	88.3	89.1	0.8	3.6	2.5	2.4	3.8	-1.5	88	81	95	88	0.8	1.5	0.4	0.9	10 ●	10	10	S 3	SW 3	SW 1
12	84.9	82.4	78.1	81.8	1.1	3.2	0.6	1.4	4.7	0.6	100	91	100	97	0.0	0.7	0.0	0.2	10	10	10 ✳ ●	C 0	E 1	NE 1
13	76.7	81.2	88.1	82.0	-5.5	-4.9	-5.5	-5.4	0.8	-5.9	92	93	92	92	0.3	0.3	0.3	0.3	10 ✳	10 ✳	10 ✳	WNW 7	NNW 9	WNW 6
14	93.3	97.0	101.2	97.2	-7.9	-3.9	-7.7	-6.8	-2.7	-8.4	90	68	79	79	0.3	1.4	0.7	0.8	3	6	1	W 7	W 8	SW 3
15	103.4	104.8	107.0	105.1	-17.6	-2.1	-9.2	-9.5	-1.6	-18.4	90	50	70	70	0.2	2.6	0.9	1.2	2	8	10	C 0	S 3	C 0
16	108.5	108.6	106.4	107.8	-10.3	-3.9	-5.5	-6.3	-3.5	-13.1	81	59	62	67	0.5	1.9	1.5	1.3	10	10	10	NNW 1	N 5	N 7
17	100.6	97.9	97.6	98.7	-6.0	-2.3	-2.6	-3.4	-1.7	-6.4	53	55	65	58	1.8	2.4	1.8	2.0	9	8	8	N 9	N 8	N 9
18	97.7	99.7	101.3	99.6	-4.6	0.3	-4.1	-3.1	0.9	-7.4	91	60	84	78	0.4	2.4	0.7	1.2	0	8	8	N 4	N 7	NW 4
19	102.4	103.3	102.8	102.8	-6.9	-0.8	-4.3	-4.1	0.2	-6.9	94	58	70	74	0.2	2.4	1.3	1.3	4	5	3	NW 3	NW 3	C 0
20	103.0	103.6	103.7	103.4	-7.5	0.0	-2.3	-3.0	0.8	-8.3	90	65	74	76	0.3	2.1	1.4	1.3	1	8	8	SSW 1	SW 4	S 1
21	102.6	101.7	100.9	101.7	-5.8	1.8	-4.5	-3.2	2.0	-6.8	84	52	67	68	0.6	3.4	1.4	1.8	9	1	0	SE 1	SSE 1	SE 2
22	98.1	96.3	94.8	96.4	-11.3	-1.6	-5.1	-5.8	-0.4	-12.2	93	63	73	76	0.2	2.0	1.1	1.1	1	1	0	SE 1	E 4	NE 2
23	93.5	93.4	94.9	93.9	-11.0	-0.4	-3.7	-4.7	-0.2	-13.1	93	68	83	81	0.2	1.9	0.8	1.0	9	6	10	NE 2	N 4	N 2
24	96.5	98.8	101.8	99.0	-5.8	-0.3	-6.3	-4.7	0.0	-6.6	89	65	78	77	0.4	2.1	0.8	1.1	10 ✳	8	0	NNW 3	N 5	WNW 3
25	104.3	104.4	102.9	103.9	-6.1	1.2	-3.2	-2.8	2.7	-9.5	94	58	83	78	0.2	2.9	0.8	1.3	9	1	0	C 0	SW 1	C 0
26	101.5	100.4	98.9	100.3	-3.8	2.0	-2.2	-1.6	3.7	-5.6	87	62	70	73	0.6	2.7	1.6	1.6	9	3	0	C 0	S 3	S 1
27	95.5	93.4	91.2	93.4	-6.1	1.8	-2.4	-2.3	2.4	-7.2	79	47	57	61	0.8	3.7	2.2	2.2	3	10	0	SE 1	SE 3	SE 6
28	87.1	86.1	87.1	86.8	-4.1	2.1	-0.1	-0.6	2.4	-5.2	75	66	98	80	1.1	2.4	0.2	1.2	7	9	10	ESE 5	SE 4	SE 1
29	87.9	89.1	88.2	88.4	0.0	1.8	0.1	0.5	2.1	-0.3	96	83	80	86	0.2	1.2	1.3	0.9	10	10	0	W 1	W 1	SE 1
30	82.0	79.7	78.2	80.0	-0.4	1.4	1.6	1.0	2.9	-1.6	90	98	100	96	0.6	0.2	0.0	0.3	10	10 ✳	0 ═	E 3	SE 3	ESE 1
31	72.4	70.2	78.3	73.6	3.3	6.2	1.6	3.2	8.3	1.6	100	100	93	98	0.0	0.0	0.6	0.2	10 ●	10 ●	2	SE 4	S 4	W 1
M	94.2	94.2	94.6	94.3	-6.1	-0.6	-3.3	-3.3	0.6	-7.5	89	72	82	81	0.4	1.6	0.8	0.9	6.9	7.1	4.9	2.5	3.8	2.5

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1	84.4	86.5	88.8	86.6	1.1	4.3	0.9	1.8	4.9	0.0	98	84	94	92	0.1	1.4	0.4	0.6	4	10	2	SW 3	SW 3	SW 4
2	88.9	89.7	92.2	90.3	0.8	5.3	2.2	2.6	6.8	-0.3	86	69	91	82	0.9	2.8	0.7	1.5	8	7	9	W 4	SW 6	SW 5
3	92.7	92.0	88.9	91.2	2.2	6.2	6.3	5.2	10.1	0.8	95	91	76	87	0.4	0.9	2.2	1.2	10 ●	10 ●	0	SW 3	SSW 5	S 4
4	84.8	83.1	79.7	82.5	5.2	11.0	5.9	7.0	11.4	3.8	70	57	76	68	2.6	5.7	2.3	3.5	8	9	0	S 5	S 5	C 0
5	74.5	72.0	72.6	73.0	5.7	10.0	7.0	7.4	10.6	5.4	97	74	97	89	0.3	3.2	0.3	1.3	10 ●	10 ●	10 ●	SE 1	S 3	SE 2
6	76.4	79.9	85.0	80.4	1.9	11.6	5.4	6.1	11.9	1.6	100	56	97	84	0.0	5.9	0.3	2.1	10 ═	7 ⊙	7	S 2	S 2	N 3
7	88.7	89.4	89.9	89.3	1.5	4.8	0.4	1.8	5.9	0.1	91	61	84	79	0.6	3.4	1.0	1.7	8	9	0	NW 4	NW 9	W 2
8	85.5	86.3	88.3	86.8	2.5	6.5	8.0	6.2	8.4	-1.1	98	99	90	96	0.1	0.2	1.0	0.4	10 ●	10 ●	10 ●	SW 2	SW 4	SW 4
9	90.2	94.0	97.8	94.0	6.9	11.2	5.8	7.4	11.9	5.3	92	54	77	74	0.7	6.2	2.1	3.0	4 ⊙	6	4	SW 3	SW 6	SW 1
10	101.0	102.8	105.7	103.2	2.4	11.6	3.2	5.1	11.9	0.0	98	39	81	73	0.2	8.3	1.5	3.3	6	4 ⊙	0	SE 1	S 2	C 0
11	107.4	107.4	105.4	106.7	2.5	6.0	4.7	4.5	7.5	-1.2	96	83	94	91	0.3	1.6	0.5	0.8	10	10 ●	2	W 1	W 1	N 1
12	102.1	100.8	98.3	100.4	4.1	11.9	7.1	7.6	14.5	2.2	97	56	85	79	0.3	6.1	1.5	2.6	4	9	0	W 1	WSW 2	SW 1
13	97.9	98.0	97.6	97.8	2.5	7.9	5.1	5.2	8.7	-1.6	100	67	87	85	0.0	3.5	1.1	1.5	10 ═	10	10 ●	C 0	N 1	N 2
14	97.3	100.4	106.5	101.4	3.1	3.9	5.0	4.2	5.2	2.2	97	97	94	96	0.2	0.3	0.5	0.3	10 ●	10 ●	10	N 5	N 4	N 5
15	109.5	110.6	111.3	110.5	3.8	6.8	6.0	5.6	7.9	2.2	98	91	95	95	0.1	0.9	0.5	0.5	10	10	10	NE 3	NE 3	NE 4
16	110.8	109.9	108.6	109.8	5.9	12.2	11.0	10.0	14.6	5.4	98	74	80	84	0.2	3.7	2.6	2.2	10	6	0	ENE 6	E 6	E 6
17	108.6	107.4	106.0	107.3	9.9	21.6	15.7	15.7	22.7	7.5	87	34	79	66	1.6	17.0	3.9	7.5	0	5	10	SE 5	SE 5	SE 4
18	102.7	100.7	99.3	100.9	12.3	20.8	15.8	16.2	21.6	11.0	79	40	62	60	3.0	14.8	6.7	8.2	9	10	10	SE 4	SSE 4	SE 1
19	98.6	98.9	99.1	98.9	11.2	20.9	13.8	14.9	21.6	9.2	80	49	80	70	2.6	12.5	3.2	6.1	10	10	10	S 2	SSW 3	C 0
20	100.5	101.4	101.7	101.2	10.6	23.4	17.0	17.0	24.4	7.2	96	43	73	71	0.5	16.3	5.3	7.4	10	0	3	C 0	NNW 1	NE 1
21	102.2	102.1	102.7	102.3	13.8	26.5	18.1	19.1	27.0	12.4	91	23	59	58	1.5	26.7	8.4	12.2	9	2	6	E 1	S 4	SW 1
22	104.7	104.4	104.4	104.5	7.7	18.9	14.0	13.6	21.6	6.8	100	66	88	85	0.0	7.5	2.0	3.2	10 ═	0	0	NNW 3	N 3	NE 1
23	104.0	103.9	105.7	104.5	12.4	25.8	11.3	15.2	27.1	7.8	99	34	89	74	0.2	21.8	1.5	7.8	3	8	4	C 0	SW 2	NW 3
24	109.6	110.6	111.5	110.6	8.3	19.6	13.3	13.7	21.1	6.7	100	47	71	73	0.0	12.2	4.5	5.6	10 ═	0	0	NNE 2	NE 3	NE 3
25	113.2	112.0	109.7	111.6	11.6	20.7	15.1	15.6	22.6	5.7	70	33	51	52	4.0	16.3	8.5	9.6	0	0	0	E 3	E 4	SSE 1
26	105.3	100.6	96.9	101.0	13.1	22.6	7.5	12.7	22.7	7.3	56	46	86	63	6.7	14.9	1.5	7.7	6	9	3	S 3	W 3	SW 3
27	91.4	90.5	90.0	90.6	7.7	5.5	4.0	5.3	9.4	2.1	90	97	95	94	1.0	0.3	0.4	0.6	10	10 ●	3	W 2	NW 5	W 5
28	84.0	84.1	86.7	84.9	4.9	8.6	4.0	5.4	9.3	3.4	94	56	92	81	0.6	4.9	0.6	2.0	9	9	9	N 2	NW 6	N 4
29	87.4	88.8	90.7	89.0	3.8	4.4	1.8	3.0	7.3	1.5	80	69	89	79	1.6	2.6	0.8	1.7	9	8	6	NW 6	NW 6	NW 3
30	91.4	95.7	96.9	94.0	1.2	2.9	-1.9	0.1	3.9	-2.4	81	69	93	81	1.3	2.3	0.3	1.3	9	9	3	NW 2	W 4	NW 2
31																								
M	96.5	96.7	97.3	96.8	6.0	12.4	7.8	8.5	13.8	3.7	90	62	83	78	1.1	7.5	2.2	3.6	7.9	7.2	4.8	2.6	3.8	2.3

Olsztyn-Dajtki $H_s = 133m$ $H_b = 135{,}4m$ $h_w = 12m$ Marzec - Mars 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ POKRYWY SNIEGU h	POGODA
1	6	•	15	=0^00-24
2	6	•	15	=0^00-24
3	6	•	15	*°7^55-9^38; =0^00-24
4	4	1.2	15	*°7^20-13^05 13^35; 16^51-21^25; =0^00-24
5	6	9.8	17	*°6^25-10^40 ≈ 21^40-22^35 ≈-24; =0^00-24
6	5	7.0	18	≈0^00-11^40 *-12^30 *°-1-24; =0^00-24
7	6	0.1	19	*°0^00-10^42; =0^00-13^30
8	7	0.0	19	⚡°14^56-15^38; 15^55-16^40; =7^30-8^36 ≡°-10^45 =-12^10
9	7	0.0	19	⚡9^42-11^36; =5^30-6^40 ≡°-8^45 =-12^10
10	7	0.0	19	
11	6	0.6	17	•°6^25-8^25; 14^52-17^40; =7^30-24
12	4	8.6	14	•°14^50-20^35 *°-23^40 *°-24; =0^00-6^40 ≡°-10^50 =-16^45 ≡°-23^45 =-24
13	3	3.1	17	*°-1 0^00-17^35 ⚡°-1 20^34-24; ⊥ 8^40-17^45; =0^00-17^20
14	8	0.0	24	⚡°0^00-2^25; 3^54-7^05; 7^10-8^02
15	7	•	23	⊂20^20-24
16	7	•	22	
17	8	•	21	⊥ 6^40-24
18	8	0.0	20	⊥ 0^00-2^40
19	8	•	19	⚡°1^06-08; 5^55-6^14
20	8	•	17	
21	8	•	15	
22	7	•	14	=6^10-11^30
23	6	0.0	10	=9^30-24
24	7	•	9	*°6^15-7^45; =0^00-10^40
25	7	•	8	
26	7	•	7	=5^30-12^15
27	7	•	5	⊕11^30-15^30
28	7	2.8	5	⚡'13^15-14^40 ⚡°16^10 *22^56-24; =16^10-22^56
29	6	0.0	5	*°0^00-5^20; 7^35-8^52; =5^20-7^35; 8^52-24
30	5	2.0	5	•°7^20-8^25 *°-11^05 *°-12^20 •-13^38; 18^54-19^40; =0^00-14^35 ≡°-2-24
31	4	2.0	4	•°5^50-7^20 ... 15^40; =°0^00-4^40 =-15^40
Σ	—	37.2	—	UWAGI.

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1	7	1.2	3	•°0^56-3^50 ⚡°12^20-25; 13^03-14^25 ⚡°-14^40 ⚡°-15^10; =18^20-24
2	8	1.0	2	⚡°0^53-3^36 ⚡°14^54-15^04; 16^35-45 21^02-07; =0^00-5^10
3	6	1.6	pł.	⚡°1^36-40 •°5^55-12^52; =12^52-13^30
4	7	0.2	pł.	
5	7	5.6	pł.	•°0^50-2^45; 4^55-6^20 ... 7^10; 12^25-21^53; =21^53-23^45 ≡°-24
6	8	•	pł.	≡°-1 0^00-9^05 =-9^40; 20^20-21^40 ≡°-24
7	8	0.4	pł.	≡°0^00-2^45 =-6^20
8	4	2.7	•	•°5^50-7^40; 10^40-12^06 •°-13^40 •°14^50-18^20 •°-21^10 •°-23^48; =6^20-7^40 ≡°-8^45 =-24
9	8	•	•	•°2^50-4^20; =0^00-5^30
10	8	0.0	•	=4^30-7^20
11	6	0.8	•	•°5^56-6^55; 8^54-9^40 ... 10^10-13^04 ... 14^53; =6^35-19^10
12	7	•	•	=5^30-8^30; 20^10-24
13	7	2.4	•	•19^52-24; =0^00-4^40 ≡°-8^30 =-11^30
14	6	0.5	•	•°0^00-11^40 ... 13^10-16^50; =2^30-24
15	6	0.0	•	•°1^06-2^20; 7^05-8^54; =0^00-24
16	6	•	•	=0^00-13^10; 18^30-24
17	7	•	•	=0^00-7^20
18	7	•	•	=4^30-9^20
19	7	•	•	=20^15-24
20	6	•	•	=0^00-9^30 ≈ -15^10 =20^10-24
21	7	•	•	=0^00-8^20 ≈ -12^30; ⌒ 2^20-8^00
22	7	•	•	=1^30-3^45 ≡°-1 8^50 =-9^40; 22^46-24
23	7	•	•	=0^00-4^50 ≡°-6^40 =-10^30; 22^30-24; ⌒ °1^00-9^00
24	7	•	•	=0^00-4^40 ≡°-7^20 =-9^20
25	8	•	•	⌒ °1^50-8^00
26	7	0.0	•	⚡°9^05-12 ⚡^48-50; ⚡°8^40-9^05 SW
27	7	5.2	•	•°7^40-8^40 9^20 ⚡°-18^07; 22^38-24; =2^30-10^30; ⌒ '1^00-7^40
28	8	0.2	•	⚡°0^00-1^15 ▲°9^51-56 ⚡°10^07 ... 11^23; 16^54-17^17; 21^38-22^15
29	8	0.3	•	⚡°5^55-6^05; 12^52-13^10 ⚡-13^48 ⚡°15^42-16^27
30	8	0.0	•	⚡7^30-46; 8^45-9^05
31				
Σ	—	22.1	—	UWAGI.

Olsztyn-Dajtki φ=53°46' λ=20°25' Maj-Mai 1962

DNI	CIŚNIENIE P=900 I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D.v I	II	III
1	93.7	89.9	88.7	90.8	-0.1	2.9	-0.3	0.6	4.5	-2.4	94	81	88	88	0.4	1.4	0.8	0.9	10 ✳	10 ✳	8	W 4	W 5	NW 3
2	86.6	87.8	91.1	88.5	1.2	4.9	1.5	2.3	5.9	-0.7	85	65	98	83	1.1	3.0	0.1	1.4	7	10 ●	5	WSW 3	WNW 4	W 1
3	92.4	91.7	91.1	91.7	3.0	7.4	5.0	5.1	9.3	-0.8	93	47	81	74	0.6	5.4	1.6	2.5	8	9	9	E 1	SSW 3	WSW 1
4	87.0	87.3	90.4	88.2	5.2	6.8	2.1	4.0	9.9	-0.5	87	64	96	82	1.1	3.6	0.3	1.7	6	9	9	C 0	NW 3	NW 3
5	93.8	96.8	99.8	96.8	3.4	6.9	2.4	3.8	8.4	2.1	86	63	82	77	1.1	3.7	1.3	3.0	10	9	3	W 2	W 1	NNW 1
6	103.3	103.3	102.2	102.9	4.0	11.9	7.2	7.6	14.2	-3.5	79	41	63	61	1.7	8.2	3.8	4.6	0	4	2	C 0	E 1	S 1
7	98.7	97.9	97.7	98.1	9.4	10.8	9.6	9.8	12.5	2.6	65	74	96	78	4.1	3.4	0.5	2.7	9	10 ●	10	SSE 2	SSE 2	S 1
8	95.3	95.1	94.1	94.8	9.5	16.0	12.5	12.6	18.6	8.6	100	78	87	88	0.0	4.0	1.9	2.0	10 ● ═	9	10	SSW 1	NW 1	NW 3
9	94.8	96.1	95.9	95.6	9.3	13.8	9.2	10.4	15.9	8.6	99	70	92	87	0.1	4.7	0.9	1.9	9	9	3	NNW 2	W 4	C 0
10	92.9	91.6	93.2	92.6	8.1	16.8	11.0	11.7	16.9	3.7	100	62	99	87	0.0	7.3	0.1	2.5	10	10	10	SE 2	S 2	W 2
11	94.0	94.0	95.4	94.5	9.3	15.1	9.3	10.8	16.0	5.6	97	58	97	84	0.3	7.2	0.3	2.6	4	8	7	W 1	W 3	W 1
12	97.1	98.4	99.7	98.4	8.3	13.3	10.2	10.5	16.3	4.7	100	69	90	86	0.0	4.8	1.2	2.0	4 ═	9	2	NW 1	NE 2	NW 1
13	100.8	99.5	98.1	99.5	9.2	17.5	10.7	12.0	18.1	4.3	87	54	92	78	1.5	9.1	1.0	3.9	10	10	9	NE 1	SE 4	ENE 1
14	92.4	86.5	75.3	84.7	10.4	12.6	12.6	12.0	13.5	7.9	95	95	99	96	0.6	0.7	0.2	0.5	10	10 ●	10 ●	E 2	ENE 4	N 6
15	74.7	77.6	83.1	78.5	10.2	9.3	6.5	8.1	12.7	6.5	97	99	99	98	0.3	0.1	0.2	0.2	10 ●	10 ●	10 ●	NW 3	WNW 6	NW 7
16	86.4	90.7	94.9	90.7	6.5	7.9	8.1	7.6	10.5	5.8	97	91	75	88	0.3	0.9	2.7	1.3	10 ●	10	7	WNW 7	WNW 7	W 4
17	95.0	93.9	92.5	93.8	8.1	13.2	9.1	9.9	14.1	4.6	78	64	95	79	2.4	5.5	0.7	2.9	9	8	10 ● ⚑	SW 3	SSW 5	S 2
18	95.3	97.3	100.6	97.7	8.2	11.2	7.4	8.6	12.8	6.4	92	82	93	89	0.9	2.5	0.8	1.4	9	8	0	W 3	SW 3	SW 2
19	101.8	99.9	95.6	99.1	9.3	17.5	14.8	14.1	18.4	3.4	87	41	56	61	1.6	11.7	7.4	6.9	2	4	9	S 1	SSW 5	E 3
20	90.8	93.0	95.9	93.2	11.3	9.3	7.4	8.8	14.8	7.4	89	97	99	95	1.5	0.3	0.2	0.7	10 ●	10 ●	10 ●	SSE 2	NW 5	W 2
21	98.6	99.3	98.5	98.8	9.4	14.1	10.5	11.1	14.9	7.0	84	48	68	67	1.9	8.4	4.1	4.8	7	4	9	WNW 3	NNW 3	NE 1
22	96.4	96.8	96.8	96.7	8.7	11.4	10.0	10.0	14.0	7.2	84	63	86	78	1.8	5.0	1.8	2.9	10	9	9	SW 1	S 2	SE 3
23	98.9	98.4	97.6	98.3	11.5	17.7	13.7	14.2	18.5	8.9	90	52	81	74	1.4	9.7	3.0	4.7	5	9	10	SW 3	SW 5	SW 2
24	99.7	100.3	99.9	100.0	10.9	14.9	12.0	12.4	15.8	9.5	86	41	64	64	1.8	10.0	5.1	5.6	9	9	9	WSW 2	W 5	S 2
25	98.3	98.7	99.0	98.7	9.3	13.4	10.4	10.9	15.6	8.7	89	62	81	77	1.3	5.8	2.4	3.2	10 ●	10	9	SW 1	S 1	NW 1
26	97.8	96.5	94.6	96.3	9.8	10.2	11.1	10.6	11.2	6.9	95	96	99	97	0.6	0.4	0.2	0.4	10 ●	10 ●	10 ●	NE 1	NE 3	E 3
27	97.5	99.2	100.4	99.0	11.4	15.3	12.8	13.1	17.2	10.3	91	71	89	84	1.2	5.1	1.6	2.6	6	10	9 ●	S 1	S 2	WSW 1
28	100.7	100.2	96.9	99.3	9.5	16.4	13.4	13.2	17.4	6.5	100	65	80	82	0.0	6.5	3.2	3.2	10 ═	8	10 ●	N 2	NNW 2	NE 4
29	96.4	97.9	99.0	97.8	10.0	15.6	9.7	11.2	16.7	9.2	95	62	93	83	0.7	6.7	0.8	2.7	10	6	4	WSW 3	SW 5	SW 1
30	99.6	98.8	100.2	99.5	10.4	14.3	8.5	10.4	16.7	6.5	88	61	85	78	1.4	6.3	1.7	3.1	9	8	10	SW 2	WSW 4	W 3
31	99.0	97.0	92.8	96.3	10.4	11.3	10.2	10.5	13.8	5.4	83	78	91	84	2.1	3.0	1.1	2.1	7	10 ●	10	SW 2	SW 3	SW 2
M	95.2	95.2	95.2	95.2	8.2	12.2	9.0	9.6	14.0	5.2	90	68	87	82	1.1	5.0	1.6	2.6	8.1	8.7	7.6	2.0	3.4	2.2

Czerwiec-Juin

1	95.5	97.7	99.4	96.9	6.6	10.7	7.9	8.3	12.6	4.7	78	55	80	71	2.1	5.8	2.0	3.3	7	8	6	WSW 6	W 8	N 3
2	99.4	100.6	103.8	101.3	7.5	11.2	8.0	8.7	13.3	2.5	89	64	92	82	1.2	4.8	0.9	2.3	9	8	9	C 0	WNW 4	NW 2
3	106.6	107.0	108.0	107.2	7.5	12.0	9.0	9.4	14.3	1.1	86	53	77	72	1.5	6.6	2.6	3.6	1	7	9	NW 2	N 3	N 2
4	107.3	106.7	106.1	106.7	9.0	14.2	9.3	10.4	14.9	7.3	86	48	69	68	1.6	8.4	3.7	4.6	8	9	9	NW 4	NNE 7	NNW 4
5	105.5	105.7	107.6	106.3	7.5	13.6	8.8	9.7	13.9	5.9	80	62	64	69	2.1	6.0	4.0	4.0	9	10	7	N 7	N 8	N 5
6	108.7	109.3	110.0	109.3	8.2	13.1	9.0	9.8	14.1	5.8	48	44	71	54	5.7	8.4	3.4	5.8	8	6 ⊙	8	NNE 9	NNE 9	N 4
7	112.4	112.6	112.0	112.3	8.5	14.9	9.1	10.4	16.5	6.2	70	48	74	64	3.3	8.8	3.1	5.1	7	4	0	N 4	NE 6	NNW 3
8	111.9	110.2	105.1	109.1	10.2	18.3	14.7	14.5	19.6	4.1	88	50	60	66	1.4	10.4	6.7	6.2	0 ⊙	1 ⊙	2	NW 2	WNW 2	W 1
9	99.5	97.9	98.2	98.5	14.0	19.6	9.2	13.0	20.0	9.0	71	60	61	64	4.6	9.2	4.5	6.1	7	8	2	W 5	W 6	NW 3
10	97.9	96.2	93.6	95.9	11.4	18.9	14.6	14.9	20.1	2.2	71	41	66	59	3.9	12.9	5.7	7.5	2 ⊙	4	6	NW 1	SE 1	SW 1
11	90.6	89.1	90.9	90.2	15.1	17.2	10.0	13.1	19.4	9.9	66	61	96	74	5.8	7.6	0.5	4.6	4	10	9	SW 2	WSW 3	NW 1
12	91.7	93.5	96.5	95.9	9.0	10.9	9.6	9.8	15.0	6.8	99	91	83	91	0.2	1.1	2.1	1.1	10 ●	9 ●	3	SW 2	W 3	NW 1
13	98.5	99.6	100.2	99.4	10.7	17.3	11.7	12.8	18.0	5.3	87	52	78	72	1.7	9.4	2.9	4.7	3 ⊙	7	9	W 3	NW 5	C 0
14	99.9	98.6	97.7	98.7	15.3	20.4	17.8	17.9	21.8	8.1	66	41	57	55	6.0	14.2	8.7	9.6	8	7 ⊙	9	SW 1	SSW 3	S 1
15	100.8	102.5	102.5	101.9	16.8	23.0	19.5	19.7	25.6	11.0	71	48	70	63	5.5	14.7	6.9	9.0	6 ⊙	4 ⊙	4	W 3	NW 4	SW 1
16	103.5	102.4	99.4	101.8	17.5	27.7	22.5	22.6	28.9	16.4	91	43	63	66	1.8	21.2	9.9	11.0	10	9	9	W 1	SW 2	S 1
17	101.8	103.5	104.6	103.3	17.1	19.1	11.0	14.6	22.5	11.0	93	66	89	83	1.4	7.5	1.3	3.5	10	7	2	W 2	NW 5	NW 2
18	105.1	104.1	102.7	104.0	13.8	20.6	15.2	16.2	22.2	5.4	72	44	63	60	4.4	13.6	6.3	8.1	3 ⊙	2 ⊙	3	W 2	NE 2	N 1
19	101.9	100.3	96.2	99.5	17.4	24.9	20.5	20.8	25.2	6.9	64	37	53	51	7.2	19.8	11.4	12.8	4 ⊙	9	4	SE 1	S 2	SE 1
20	96.4	100.3	99.8	98.8	17.5	17.5	17.2	17.4	20.6	14.0	94	73	75	81	1.2	5.5	4.9	3.9	10 ●	8	8	W 2	WNW 2	S 2
21	101.6	101.5	102.8	102.0	17.0	21.3	16.6	17.9	23.1	12.9	74	48	85	69	5.1	13.3	2.9	7.1	2 ⊙	8 ●	8	SSW 2	W 6	W 1
22	103.4	105.6	104.2	103.1	16.4	22.3	20.0	19.7	24.9	11.2	66	47	72	62	6.3	14.4	6.6	9.1	2 ⊙	7	4	W 2	NW 2	WSW 1
23	102.7	102.9	103.4	103.0	20.8	20.7	13.8	17.3	24.6	13.7	72	72	94	79	7.0	6.8	0.9	4.9	8	8	10 ⚑	SSW 1	WNW 4	C 0
24	101.9	100.5	96.6	99.7	14.5	21.8	19.5	18.8	22.7	9.8	94	46	75	72	0.9	14.1	5.7	6.9	3	6	9	W 2	SW 3	SW 1
25	95.8	96.8	98.9	97.2	15.8	17.8	11.0	13.9	19.5	10.8	61	45	84	63	6.9	11.3	2.1	6.8	4	9	4	W 6	W 8	W 4
26	98.3	98.3	95.8	97.5	10.8	15.4	13.7	13.4	16.7	8.6	74	54	70	66	3.4	8.0	4.7	5.4	4	6	10	W 5	WSW 5	C 0
27	91.9	91.7	91.2	91.6	11.0	13.9	10.1	11.3	16.6	9.1	97	84	95	92	0.3	2.3	0.7	1.2	10 ●	8	10 ●	S 1	SW 4	SW 3
28	90.9	90.9	89.0	90.3	11.4	11.8	9.0	10.3	14.0	8.8	84	63	93	80	2.2	5.0	0.8	2.7	9	10	9	W 4	SW 3	SW 3
29	87.2	87.7	89.1	88.0	9.4	11.8	10.3	10.6	14.0	8.1	96	88	96	93	0.3	1.6	0.3	0.9	9	10 ●	9	W 5	W 3	W 4
30	90.9	93.4	95.7	93.3	10.3	15.2	10.4	11.6	16.9	9.9	92	60	91	81	1.0	7.0	1.1	3.0	9	8	4	W 6	W 5	NW 2
31																								
M	100.0	100.2	100.0	100.1	12.6	17.2	13.0	14.0	19.0	8.2	79	56	77	71	3.2	9.3	3.9	5.3	6.2	7.2	6.3	3.1	4.3	1.9

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚNIEGU P	POGODA
1	7	1.1	.	$\overset{*}{\nabla}{}^{\circ}5^{40}\text{-}7^{10}$ $\overset{*}{\nabla}{}^{\circ}9^{40}\overset{*}{\nabla}{}^{\circ}10^{51}\text{-}14^{10}$; $\sqcup{}^{\circ}2^{00}\text{-}7^{00}$
2	8	0.4	.	$*{}^{\circ}0^{52}\text{-}3^{25}\overset{*}{\nabla}{}^{\circ}12^{35\text{-}54}$; $14^{40}\text{-}15^{05}$; $16^{50}\text{-}17^{55}$
3	8	0.8	.	$\overset{*}{\nabla}{}^{\circ}7^{40}\text{-}8^{05}$; $9^{11\text{-}18}$; $10^{02\text{-}15}$ $\overset{*}{\nabla}10^{03\ldots08}\overset{*}{\nabla}17^{45\text{-}53}$; $20^{25}\text{-}21^{02}\sqcup{}^{\circ}1^{00}\text{-}6^{00}$
4	7	1.1	.	$*11^{34\text{-}55}\overset{*}{\nabla}{}^{\circ}16^{08\text{-}45}$; $=3^{30}\text{-}7^{30}$
5	7	.	.	
6	8	.	.	$=1^{30}\text{-}7^{40}$; $\sqcup{}^{\circ}7^{05}\text{-}7^{00}$ $\triangle{}^{\circ}23^{00}\text{-}24$
7	7	2.2	.	$\bullet{}^{\circ}11^{19}\text{-}13^{05}$ $14^{30}\text{-}16^{40}$; $=16^{40}\text{-}24$; $\triangle{}^{\circ}0^{00}\text{-}7^{00}$
8	6	5.4	.	$\bullet{}^{0\text{-}1}5^{50}\text{-}10^{03}$; $=0^{00}\text{-}1^{15}$ $\equiv{}^{0\text{-}3}\text{-}7^{40}$ $=\text{-}17^{30}$; $19^{30}\text{-}24$
9	7	.	.	$=0^{00\text{-}50}\equiv{}^{\circ}\text{-}4^{20}=\text{-}12^{10}$; $20^{10}\text{-}24$; $\triangle{}^{\circ}np$
10	7	1.8	.	$\overset{*}{\nabla}{}^{\circ}13^{55}\text{-}15^{20}$ $\bullet{}^{\circ}\text{-}16^{50}\overset{*}{\nabla}{}^{\circ}21^{48}\text{-}22^{05}$; $\equiv{}^{0\text{-}1}0^{45}\text{-}5^{50}=\text{-}9^{30}$; $p\equiv19^{45}\text{-}20^{25}=\text{-}24$; $\triangle{}^{\circ}0^{00}\text{-}8^{00}$; $\oplus6^{10}\text{-}8^{10}$
11	8	1.7	.	$\overset{*}{\nabla}{}^{\circ}9^{47}\text{-}10^{04}$; $16^{03\text{-}13}$; $18^{03}\text{-}20^{08}$; $\mathbb{R}^{\circ}16^{03\text{-}25}$ NW-NE, $17^{41}\text{-}19^{10}$ SE; $=$, $\equiv{}^{\circ}0^{00}\text{-}7^{40}$; np
12	7	0.2	.	$\overset{*}{\nabla}{}^{\circ}10^{08\text{-}25}$; $12^{32\text{-}46}$; $15^{55}\text{-}16^{00}$; $(\mathbb{R})10^{40}\text{-}11^{40}$ E-W, $15^{20}\text{-}17^{43}$ NW-SW; $\equiv$, $=0^{00}\text{-}12^{30}$; np
13	7	4.5	.	$\overset{*}{\nabla}{}^{0\text{-}1}12^{18}\ldots17^{42}$; $\mathbb{R}^{\circ}14^{38}\text{-}15^{40}$ SE-NW, $16^{20}\text{-}17^{35}$ SSW-N; $\equiv{}^{\circ}0^{00}\text{-}4^{45}=\text{-}6^{20}$; $18^{30}\text{-}24$ $\triangle{}^{0\text{-}2}0^{00}\text{-}8^{00}$
14	6	21.2	.	$\bullet{}^{0\text{-}1}8^{52}\ldots12^{10}\text{-}22^{20}\ldots24$; $=0^{00}\text{-}24$
15	6	12.1	.	$\bullet{}^{\circ}0^{00}\ldots5^{20}\bullet{}^{0\text{-}1}\text{-}24$; $=0^{00}\text{-}24$
16	6	0.2	.	$\bullet{}^{\circ}0^{00}\text{-}9^{30}\ldots12^{25}$; $=0^{00}\text{-}14^{30}$
17	7	6.7	.	$\overset{*}{\nabla}{}^{\circ}19^{50}\text{-}23^{10}\overset{*}{\nabla}{}^{1}\text{-}23^{40}$; $\mathbb{R}^{\circ}19^{45}\text{-}20^{41}$ SW-NE; $\triangle{}^{\circ}2^{00}\text{-}9^{00}$
18	7	1.5	.	$\overset{*}{\nabla}{}^{\circ}11^{20\text{-}55}$; $14^{05\text{-}18}$; $15^{45}\text{-}16^{20}$; $\mathbb{R}^{\circ}11^{56}\text{-}12^{40}$ W-E; $=1^{30}\text{-}7^{30}$; $\triangle{}^{\circ}20^{00}\text{-}24$
19	8	0.4	.	$=4^{30}\text{-}7^{30}$; $\triangle{}^{0\text{-}1}0^{00}\text{-}10^{00}$
20	6	15.8	.	$\bullet{}^{0\text{-}1}5^{54}\text{-}9^{25}\ldots14^{10}\text{-}21^{20}$; $=0^{00}\text{-}24$
21	8	.	.	$=0^{00}\text{-}7^{30}$
22	7	0.5	.	$\bullet{}^{\circ}7^{40}\ldots8^{10}$; $9^{35}\ldots10^{10}$; $18^{02}\text{-}19^{35}\overset{*}{\nabla}{}^{\circ}22^{20\text{-}30}$; $\triangle{}^{\circ}1^{00}\text{-}7^{40}$
23	7	0.4	.	$\bullet{}^{\circ}19^{50}\ldots21^{53}$; $=0^{30}\text{-}9^{30}$; $19^{30}\text{-}24$
24	7	0.4	.	$\bullet{}^{\circ}2^{50}\ldots4^{10}$; $23^{52}\text{-}24$; $=0^{00}\text{-}7^{30}$
25	7	1.0	.	$\bullet{}^{\circ}0^{00}\text{-}7^{20}$
26	6	8.1	.	$\bullet{}^{\circ}3^{55}\text{-}16^{40}$ $17^{45}\ldots18^{10}\bullet{}^{1\text{-}0}\text{-}24$; $=1^{30}\text{-}24$; $\triangle{}^{1}0^{00}\text{-}3^{55}$
27	7	0.4	.	$\bullet{}^{\circ}0^{00}\text{-}10^{15}$; $21^{13}\text{-}24$; $=0^{00}\text{-}3^{25}$
28	6	8.2	.	$\bullet{}^{\circ}0^{00\text{-}10}$; $21^{55}\ldots22^{05}$; $23^{40}\ldots24$; $=0^{10}\text{-}5^{43}\equiv{}^{1\text{-}0}\text{-}9^{45}=\text{-}14^{30}$
29	7	1.0	.	$\bullet{}^{\circ}0^{00\text{-}05}\bullet{}^{1}\text{-}1^{25}\overset{*}{\nabla}{}^{1}18^{04\text{-}30}\overset{*}{\nabla}{}^{\circ}19^{55}\text{-}20^{10}$; $=3^{30}\text{-}10^{30}$; $21^{30}\text{-}24$
30	7	0.7	.	$\overset{*}{\nabla}{}^{\circ}17^{55}\text{-}18^{10}$; $20^{03\text{-}25}$ $=0^{00}\text{-}8^{50}$; $21^{15}\text{-}24$
31	7	0.6	.	$\overset{*}{\nabla}{}^{\circ}10^{55}$ 15^{05}; $18^{54}\text{-}19^{35}$; $20^{45}\text{-}21^{35}$; $=0^{00}\text{-}7^{30}$; $21^{30}\text{-}24$
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1	8	.	.	$=0^{00}\text{-}5^{30}$
2	8	0.0	.	$\overset{*}{\nabla}{}^{\circ}15^{45}\text{-}16^{05}$; $18^{40}\text{-}19^{05}$; $\triangle{}^{0\text{-}1}0^{00}\text{-}11^{00}$
3	8	2.3	.	$\overset{*}{\nabla}{}^{\circ}15^{49\text{-}52}$; $16^{40}\text{-}17^{06}$; $=2^{30}\text{-}3^{50}\equiv{}^{\circ}\text{-}4^{40}=\text{-}5^{50}$
4	8	.	.	$\overset{*}{\nabla}{}^{\circ}1^{44}\text{-}4^{22}$
5	8	0.0	.	$\overset{*}{\nabla}{}^{\circ}13^{50\text{-}53}$
6	8	.	.	
7	8	.	.	
8	8	.	.	$\triangle{}^{\circ}2^{00}\text{-}10^{00}$
9	7	.	.	
10	8	.	.	
11	7	4.0	.	$\overset{*}{\nabla}{}^{\circ}15^{35}\text{-}16^{05}$; $18^{10}\text{-}19^{40}$; $21^{50}\text{-}22^{10}$; $=20^{20}\text{-}24$
12	7	2.7	.	$\overset{*}{\nabla}{}^{\circ}5^{55}\text{-}8^{20}$; $11^{36}\text{-}12^{03}\overset{*}{\nabla}{}^{1}13^{24\text{-}44}\overset{*}{\nabla}{}^{\circ}13^{50}\text{-}14^{20}$; $=0^{00}\text{-}3^{30}$
13	8	.	.	
14	8	.	.	$\triangle{}^{\circ}2^{00}\text{-}9^{00}$
15	7	0.5	.	
16	7	.	.	$\overset{*}{\nabla}{}^{\circ}4^{35}\text{-}5^{06}$; $=4^{40}\text{-}11^{30}$
17	7	.	.	$=4^{30}\text{-}9^{20}$; $\triangle{}^{\circ}22^{00}\text{-}24$
18	8	.	.	$=3^{20}\text{-}6^{30}$; $\triangle{}^{0\text{-}1}0^{00}\text{-}10^{00}$
19	8	1.5	.	
20	7	0.1	.	$\overset{*}{\nabla}{}^{\circ}3^{53}\text{-}4^{30}$; $7^{35}\text{-}9^{10}$; $\mathbb{R}4^{25\text{-}45}$ NW-SE; $=7^{30}\text{-}8^{20}$
21	7	0.0	.	$\overset{*}{\nabla}{}^{\circ}13^{34\text{-}40}$ $16^{45\text{-}47}$ $=21^{30}\text{-}24$; $\triangle{}^{\circ}np$
22	8	.	.	$=0^{00}\text{-}9^{30}$ $\triangle{}^{\circ}0^{00}\text{-}10^{00}$
23	7	9.0	.	$\overset{*}{\nabla}{}^{\circ}12^{20\text{-}23}$; $15^{40}\text{-}16^{20}\overset{*}{\nabla}{}^{0\text{-}1}20^{10}\text{-}23^{45}$; $\mathbb{R}^{\circ}21^{05}\text{-}22^{40}$ W-E; $=7^{30}\text{-}8^{30}\infty11^{20}\text{-}12^{10}$; $\triangle{}^{\circ}2^{00}\text{-}8^{00}$
24	7	0.0	.	$=2^{30}\text{-}3^{45}\equiv{}^{\circ}\text{-}5^{50}=\text{-}7^{20}$; $23^{30}\text{-}24$
25	8	2.0	.	$\overset{*}{\nabla}{}^{\circ}0^{41\text{-}44}\overset{*}{\nabla}{}^{0\text{-}1}15^{35}$; 19^{50}; $=0^{00}\text{-}7^{30}$
26	8	2.0	.	
27	7	2.7	.	$\bullet{}^{\circ}5^{53}\text{-}8^{40}$ $9^{15}\overset{*}{\nabla}{}^{\circ}13^{33\text{-}36}$; $14^{07\text{-}22}\overset{*}{\nabla}{}^{1}18^{54}\text{-}19^{07}$; $=9^{15}\text{-}10^{30}$
28	8	2.5	.	$\overset{*}{\nabla}{}^{\circ}0^{00\text{-}48}\bullet{}^{\circ}\text{-}2^{28}\overset{*}{\nabla}{}^{\circ}8^{25}\text{-}10^{43}$; $17^{19\text{-}30}$; $17^{45}\text{-}18^{28}$; $22^{52}\text{-}23^{15}$
29	7	7.3	.	$\overset{*}{\nabla}{}^{\circ}0^{07\text{-}33}$; $2^{20}\text{-}5^{40}$; $7^{47}\text{-}8^{04}$; $12^{20}\ldots23^{20}$
30	8	.	.	$\overset{*}{\nabla}{}^{\circ}0^{10}\text{-}1^{25}$; $2^{50}\text{-}3^{35}$
31				
Σ	—	36.6	—	UWAGI

Olsztyn-Dajtki φ=53°46' λ=20°25' Lipiec - Juillet 1962

DNI	CIŚNIENIE P-900 I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N.w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D.v I	II	III
1	96.4	96.9	97.1	96.8	12.2	16.9	11.8	15.2	18.7	9.6	75	53	78	69	3.5	8.9	3.0	5.1	7	5 ⊙	3	W 5	W 6	SW 2
2	95.5	93.9	91.4	93.6	11.0	16.4	11.2	12.4	18.5	9.1	91	66	79	79	1.1	6.3	2.8	3.4	7	4	5	SW 3	W 6	SW 2
3	84.5	82.8	82.2	83.2	8.9	10.5	9.8	9.8	15.1	8.8	97	82	88	89	0.3	2.3	1.4	1.3	10 ●	9 ●	6	W 3	SW 2	SW 1
4	81.4	82.1	83.9	82.5	8.6	12.4	10.2	10.4	13.9	7.6	94	68	87	83	0.6	4.7	1.6	2.3	9	8	10	SSW 1	SW 5	S 3
5	87.0	89.4	91.7	89.4	11.6	15.9	12.2	13.0	17.2	9.1	82	55	80	72	2.4	8.2	2.9	4.5	8	6	2	S 5	SW 3	S 1
6	94.4	96.0	97.4	95.9	12.6	15.9	13.8	13.5	18.3	9.0	85	71	74	77	2.2	4.6	4.1	3.6	3 ⊙	8	8	SW 4	WSW 3	SW 1
7	98.1	98.0	98.5	98.2	12.6	16.3	12.2	13.3	18.1	8.6	81	69	81	77	2.7	5.8	2.6	3.7	3	8	4	SW 2	SW 4	SW 1
8	99.8	100.5	102.3	100.9	11.9	16.4	12.0	13.1	18.0	10.1	90	59	84	78	1.3	7.6	2.2	3.7	9	6	4	W 2	NW 3	NW 3
9	104.0	103.3	101.3	102.9	10.3	16.1	11.0	12.1	18.1	8.2	91	60	84	78	1.1	7.4	2.1	3.5	10	7	2	NW 4	N 4	NW 3
10	97.7	96.1	94.3	96.0	13.6	18.1	13.4	14.6	21.5	10.2	83	64	96	81	2.7	7.5	0.6	3.6	4 ⊙	7	10 ●	WNW 5	W 7	W 4
11	93.3	92.7	91.9	92.6	13.6	20.1	13.0	14.9	21.0	12.6	92	53	92	79	1.3	11.1	1.3	4.6	10	5	4	W 5	W 7	NW 1
12	90.5	90.0	89.6	90.0	13.1	20.8	15.0	16.0	22.0	11.3	98	55	98	84	0.4	11.0	0.3	3.9	9	9	8	W 1	WSW 4	C 0
13	88.9	88.4	88.8	88.7	13.0	15.5	12.6	13.4	17.7	11.2	99	85	99	94	0.2	2.6	0.2	1.0	10 ●	10	10 ●	WSW 2	S 3	W 1
14	88.6	88.8	89.5	89.0	13.4	16.9	13.5	14.3	18.3	12.6	95	76	88	86	0.7	4.6	1.8	2.4	9	8	10	W 5	NW 3	NW 4
15	89.2	89.8	90.8	89.9	13.5	16.8	14.5	14.8	18.6	12.0	90	75	89	85	1.6	4.8	1.8	2.7	9	9	9	W 3	W 4	N 2
16	92.1	93.7	94.9	93.6	13.9	17.3	12.2	13.9	18.8	11.8	89	71	92	84	1.8	5.6	1.2	2.9	10	9	2	N 1	N 3	NNE 1
17	97.5	98.0	99.7	98.4	13.5	19.4	14.1	15.3	20.0	6.5	87	54	80	74	2.0	10.3	3.2	5.2	4	3	0	NNW 1	NW 2	N 3
18	100.8	100.0	99.6	100.1	12.6	19.6	16.3	16.2	21.4	9.4	96	62	81	80	0.5	8.6	3.4	4.2	10	7	3	N 1	N 4	N 3
19	99.4	99.4	100.6	99.8	14.9	22.2	14.9	16.7	23.0	10.8	90	55	82	76	1.6	12.0	3.1	5.6	8	8	2	N 3	N 5	NNW 2
20	101.3	100.9	100.2	100.8	13.6	23.6	18.0	18.3	25.4	10.4	99	49	75	74	0.2	15.0	5.2	6.8	4	4	2	C 0	NW 2	C 0
21	100.9	99.2	97.7	99.3	18.9	27.5	22.6	22.9	27.9	13.0	76	43	57	59	5.1	21.1	11.9	12.7	0	4 ⊙	8	C 0	SW 2	SSE 1
22	98.2	99.9	100.3	99.5	19.4	19.9	16.9	18.3	22.9	16.0	78	79	95	84	5.0	4.9	1.0	3.6	10	9	9	SW 2	NNW 2	SE 2
23	101.5	102.6	103.1	102.4	16.1	21.4	16.6	17.7	22.5	13.4	90	53	71	71	1.7	12.0	5.5	6.4	9	5	4	NW 2	NW 3	C 0
24	104.0	104.3	105.6	104.6	14.1	17.8	15.2	14.6	18.4	11.4	88	54	78	73	2.0	9.4	3.3	4.9	9	8	4	W 3	WSW 4	W 3
25	106.5	106.5	105.6	106.2	12.7	17.8	13.2	14.2	20.1	9.1	86	50	82	73	2.1	10.3	2.8	5.1	3	5	3	WSW 3	WNW 3	C 0
26	103.1	100.8	97.2	100.4	15.1	25.9	20.6	20.6	27.7	9.5	75	53	89	72	4.3	15.8	2.6	7.6	6	3	10 ●⚡	SE 1	E 3	NE 3
27	96.9	96.0	94.3	95.7	17.7	22.6	16.6	18.4	23.5	16.2	98	74	90	87	0.4	7.2	2.0	3.2	10	9	8	W 4	WSW 6	WSW 3
28	97.5	99.6	101.0	99.4	12.8	14.0	10.7	12.0	17.4	10.5	96	85	85	89	0.5	2.3	2.0	1.6	9 ●	7	7	WNW 5	WNW 4	WNW 3
29	102.3	102.2	103.4	102.6	13.1	17.6	11.5	13.4	18.8	9.3	91	60	88	80	1.4	8.1	1.7	3.7	1	5	0	WNW 3	W 5	C 0
30	105.4	104.7	104.7	104.9	12.5	18.5	11.9	13.7	20.6	5.6	96	55	93	81	0.5	9.6	1.0	3.7	2	6	6	W 1	WSW 1	C 0
31	104.9	104.3	102.1	103.8	13.6	21.6	14.9	16.2	22.0	9.1	90	51	83	75	1.6	12.7	2.9	5.7	6	6	6	N 1	S 3	SE 1
M	96.8	96.8	96.8	96.8	13.4	18.4	13.9	14.9	20.2	10.4	89	63	84	79	1.7	8.5	2.6	4.3	7.0	6.7	5.5	2.6	3.7	1.7

Sierpień - Août

1	98.5	98.4	97.8	98.2	14.9	14.8	14.6	14.7	18.5	12.1	87	80	86	84	2.2	3.3	2.4	2.6	9	9 ●	8	SW 2	W 5	SW 2
2	97.4	98.1	98.0	97.8	13.9	17.4	15.3	15.5	19.1	11.7	91	68	84	81	1.5	6.4	2.8	3.6	3	9	9	W 5	W 5	W 1
3	97.9	98.6	99.3	98.6	14.7	19.0	14.0	15.4	20.6	12.6	84	64	91	80	2.7	7.9	1.5	4.0	8	8	0	WSW 2	NW 3	C 0
4	98.8	97.7	97.5	98.0	13.7	20.2	17.5	17.2	25.2	10.9	91	90	100	94	1.5	2.5	0.0	1.3	9	10	10 ●	N 1	E 2	SW 1
5	98.2	96.2	92.0	95.5	16.5	21.3	16.1	17.5	22.0	15.1	97	74	98	90	0.6	6.7	0.4	2.6	10	9	8	NW 2	SW 1	S 2
6	92.7	94.3	94.9	94.0	15.5	19.4	16.5	17.0	21.3	14.9	96	68	85	83	0.8	7.2	2.9	3.6	9	9	9	WNW 2	WSW 3	W 1
7	93.4	89.4	85.9	89.6	16.0	21.5	18.4	18.6	25.8	11.9	94	85	92	90	1.2	3.9	1.7	2.3	9	10	6	W 1	SSE 2	SW 6
8	93.9	96.1	99.9	96.6	14.9	18.9	14.1	15.5	20.5	13.7	82	56	75	71	3.1	9.5	4.1	5.6	7	4	1	SW 6	WSW 6	SW 1
9	104.0	105.7	106.8	105.5	12.7	17.0	10.9	12.9	18.4	10.6	81	56	85	74	2.8	8.5	1.9	4.4	2 ⊙	7	1	SW 2	W 4	WNW 1
10	106.4	103.8	98.6	102.9	11.8	20.4	18.0	17.0	21.4	5.9	87	51	64	67	1.8	11.8	7.4	7.0	0	8	10	S 1	S 4	S 3
11	96.7	97.7	98.5	97.6	15.5	17.8	16.4	16.5	19.9	15.0	84	60	87	77	2.8	8.2	2.5	4.5	10	8	9	SW 3	WSW 5	WSW 1
12	100.2	100.6	99.6	100.1	16.3	25.3	19.7	20.2	26.6	13.3	85	57	80	74	2.7	13.9	4.5	7.0	0 ⊙	3	0	SW 2	WSW 5	SW 1
13	101.0	101.4	102.8	101.7	16.6	23.5	13.5	16.8	23.9	12.8	92	64	86	81	1.6	10.3	2.1	4.7	1	1	2	NW 2	WNW 3	N 1
14	103.4	102.7	101.9	102.7	12.3	18.4	9.8	12.6	19.5	8.4	94	43	88	75	0.9	12.1	1.4	4.8	4 ⊙	2 ⊙	3	C 0	NW 4	NNW 2
15	100.7	97.5	92.5	96.9	10.3	17.7	15.3	14.6	18.0	5.9	99	66	91	85	0.1	6.8	1.5	2.8	9	10	10 ●	N 2	E 3	S 1
16	91.9	93.5	95.0	93.5	16.3	21.4	17.4	18.1	23.3	14.0	95	66	88	83	1.0	8.6	2.4	4.0	9	8	8	W 2	W 3	NNW 1
17	96.5	97.0	96.0	96.5	14.6	22.3	17.2	17.8	23.2	12.7	99	53	84	79	0.2	12.5	3.2	5.3	9	8	10 ●	NNW 1	WSW 3	NNE 1
18	92.5	92.1	94.3	93.0	15.6	18.8	13.7	15.4	20.6	13.6	99	80	91	90	0.2	4.3	1.3	2.0	10	10 ●	7	SE 1	SW 4	WSW 4
19	94.2	94.7	95.1	94.7	12.0	17.1	13.2	13.9	17.4	11.5	94	65	99	86	0.8	6.9	0.2	2.6	10	9	9	W 3	WNW 6	W 2
20	94.8	97.1	98.6	96.8	14.4	18.2	15.0	15.6	19.2	13.1	99	80	94	91	0.2	4.3	0.9	1.8	10	9	10	NNW 4	N 6	NW 4
21	98.2	97.8	97.3	97.8	14.4	19.4	13.6	15.2	19.6	13.5	95	64	93	84	0.7	8.0	1.1	3.3	9	7	3	NW 2	W 2	WSW 2
22	96.6	97.6	98.1	97.4	13.7	16.6	14.6	14.9	16.9	8.0	97	85	98	93	0.6	2.9	0.4	1.3	9	10	5	C 0	NW 2	SW 1
23	94.7	96.6	97.6	96.3	11.8	15.0	12.8	13.1	16.7	11.8	94	72	89	85	0.8	4.7	1.6	2.4	6	7	4	WSW 2	SW 5	SW 4
24	95.4	89.2	87.4	90.7	11.4	13.1	16.0	14.1	16.2	9.8	89	96	96	94	1.5	0.6	0.8	1.0	10 ●	10 ●	10 ●	SW 2	SW 4	SW 6
25	91.6	92.6	94.6	92.9	13.0	15.2	11.4	12.8	17.1	11.4	88	86	93	89	1.8	2.5	1.2	1.8	7	9	0	WSW 4	W 7	SW 6
26	97.1	100.3	102.1	99.8	11.2	15.9	12.2	12.9	17.4	10.3	85	62	80	76	2.0	6.8	2.9	3.9	7	4	0	WSW 4	SW 7	SW 1
27	98.7	95.4	93.1	95.1	12.3	22.3	17.6	17.4	22.4	8.4	76	49	57	61	3.4	13.7	8.6	8.6	2	7 ⊙	9	S 5	S 6	WSW 7
28	95.2	96.9	98.7	96.9	11.8	15.3	11.8	12.7	17.6	10.9	77	61	74	71	3.1	6.9	3.6	4.3	9	7	2	SW 9	WSW 8	SW 4
29	98.1	98.0	96.8	97.6	11.2	15.8	12.4	12.4	15.7	9.8	89	85	95	90	1.5	2.3	0.7	1.3	9	10	9	SW 4	SW 4	W 4
30	98.3	100.3	100.4	99.7	11.5	14.6	10.9	12.0	15.7	10.4	88	73	86	82	1.7	4.3	1.8	2.7	9	9	9	W 6	W 7	W 3
31	95.4	91.8	94.2	93.1	10.9	8.3	10.4	10.0	13.7	8.1	95	94	95	95	0.6	0.7	0.6	0.6	9	8 ●	10	SW 6	W 3	W 3
M	97.1	97.0	96.9	97.0	13.6	18.1	14.5	15.2	19.8	11.4	90	69	87	82	1.5	6.7	2.2	3.5	7.2	7.7	6.2	2.8	4.3	2.5

Olsztyn - Dajtki $H_s = 133m$ $H_b = 135{,}4m$ $h_w = 12m$ Lipiec - Juillet 1962

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ GU h	POGODA
1	8	•	•	$\bullet^{0-1}2^{55}\text{-}8^{51}$
2	8	5.1	•	
3	7	4.4	•	$\bullet^{0-1}2^{55}\text{-}8^{51}\ \blacktriangle^{0}12^{17-18}\ \bullet^{0}12^{16}\ 14^{37}\ 17^{13-31}$
4	8	2.2	•	$\bullet^{0}5^{06}\text{-}7^{35}\ \bullet^{0}14^{02}\ 18^{20}, 22^{40}\text{-}23^{20}$
5	8	•	•	$\bullet^{0}5^{50\text{-}55}$
6	8	0.2	•	$\bullet^{1}13^{13-16}, 15^{13-15}, \triangle^{0-1}0^{00}\text{-}10^{00}$
7	8	0.3	•	$\bullet^{0}13^{07-25}, =1^{30}\text{-}7^{30}, \triangle^{0}3^{00}\text{-}9^{00}$
8	8	0.6	•	$\bullet^{0}15^{52}\text{-}16^{20}, \triangle^{0}2^{00}\text{-}9^{00}, 22^{00}\text{-}24$
9	7	•	•	$=1^{30}\text{-}8^{30}, \triangle^{0}0^{00}\text{-}10^{00}$
10	8	1.5	•	$\bullet^{0}10^{52\text{-}55}\ \bullet^{0}19^{45}\text{-}21^{50}$
11	8	0.2	•	$\triangle^{0}22^{00}\text{-}24$
12	7	5.1	•	$\bullet^{0}4^{32\text{-}50}, 16^{52}\text{-}17^{46}, 20^{04}\text{-}21^{11}, \mathrm{R}\,16^{45}\text{-}17^{50}\ NW\text{-}SE, =20^{50}\text{-}24, \triangle^{1}0^{00}\text{-}4^{32}$
13	7	26.5	•	$\bullet^{0-1}6^{51}\text{-}8^{25}\ \bullet^{0}9^{08\text{-}25}, 10^{50}\text{-}12^{10}\ \bullet^{0-2}17^{40}\text{-}22^{20}\ \bullet^{0}22^{52}\text{-}24, \mathrm{R}^{0}13^{45}\text{-}14^{15}\ W\text{-}N\ \mathrm{R}^{1}17^{45}\text{-}18^{50}\ W\text{-}E, =0^{00}\text{-}8^{30}, 22^{20}\text{-}24$
14	7	•	•	$\bullet^{0-1}0^{00}\text{-}2^{20}\ \bullet^{0}3^{35}\text{-}4^{25}, =0^{00}\text{-}12^{30}$
15	7	0.2	•	$\bullet^{0}10^{22\text{-}40}$
16	7	•	•	$=1^{30}\text{-}10^{30}, \triangle^{0}3^{00}\text{-}9^{00}, 22^{00}\text{-}24$
17	8	•	•	$=3^{30}\text{-}7^{30}, \triangle^{1}2^{00}\text{-}9^{00}\ \triangle^{0}23^{00}\text{-}24$
18	8	•	•	$=3^{45}\text{-}5^{46}\ \equiv^{0}\text{-}6^{50}=\text{-}11^{15}, \triangle^{1}0^{00}\text{-}10^{00}$
19	7	•	•	$\triangle^{0}3^{00}\text{-}9^{00}$
20	8	•	•	$=5^{30}\text{-}6^{15}\ \equiv^{0}\text{-}7^{40}=\text{-}8^{40}, \triangle^{1}2^{00}\text{-}9^{00}\ \triangle^{0}22^{00}\text{-}24$
21	7	•	•	$=5^{40}\text{-}9^{30}, \triangle^{0}0^{00}\text{-}9^{00}$
22	7	10.4	•	$\bullet^{0-1}8^{03\text{-}40}\ \bullet^{0-2}18^{15\text{-}47}\ \bullet^{0}19^{15\text{-}19}, \mathrm{R}^{0}17^{46}\text{-}19^{18}\ W\text{-}E, 20^{45}\text{-}22^{40}\ SE\text{-}NW, =9^{30}\text{-}11^{30}$
23	8	•	•	$=1^{30}\text{-}8^{40}, \triangle^{1}22^{00}\text{-}24$
24	8	0.0	•	$\bullet^{0}16^{01\text{-}03}, \triangle^{1}0^{00}\text{-}10^{00}$
25	8	•	•	$\triangle^{0}4^{00}\text{-}10^{00}, 23^{00}\text{-}24$
26	7	23.8	•	$\bullet^{1-2}21^{15}\text{-}23^{25}, \mathrm{R}^{1}21^{10}\text{-}24\ S\text{-}N, \triangle^{0}0^{00}\text{-}9^{00}$
27	6	8.5	•	$\bullet^{0}0^{00\text{-}30}, 18^{15\text{-}30}\ \bullet^{0}18^{35}\text{-}19^{25}, \mathrm{R}^{1}0^{00}\text{-}1^{40}\ \mathrm{R}^{0}18^{10}\text{-}19^{30}, =2^{30}\text{-}4^{50}\ \equiv^{0}\text{-}6^{45}=\text{-}14^{30}, 18^{15}\text{-}24$
28	7	5.9	•	$\bullet^{0}1^{06}\text{-}5^{51}\ \bullet^{0-1}7^{06}, 13^{18}, \mathrm{R}^{0}13^{20\text{-}43}\ W\text{-}E, =0^{00}\text{-}5^{30}$
29	8	0.5	•	$\bullet^{0}10^{03}, 15^{15}, \triangle^{0}22^{00}\text{-}24$
30	8	1.4	•	$\bullet^{0}17^{44}\text{-}18^{08}\ \bullet^{1}\text{-}18^{11}, =4^{40}\text{-}8^{40}, \triangle^{1}0^{00}\text{-}11^{00}$
31	8	0.0	•	$\bullet^{0}11^{50}\text{-}12^{07}, 20^{10\text{-}25}, =4^{30}\text{-}7^{30}$
Σ	—	96.8	—	UWAGI

Sierpień - Août

1	7	1.6	•	$\bullet^{0}8^{56}\text{-}9^{35}\ 13^{14\text{-}50}, 14^{16\text{-}50}, \triangle^{0}22^{00}\text{-}24$
2	7	•	•	$=4^{30}\text{-}7^{20}, \triangle^{0}0^{00}\text{-}10^{00}, 21^{00}\text{-}24$
3	7	•	•	$\triangle^{0}0^{00}\text{-}11^{00}, 21^{00}\text{-}24$
4	7	19.4	•	$\bullet^{0}12^{10}, 15^{20}, 18^{50}\text{-}19^{02}\ \bullet^{0-2}19^{25}\text{-}20^{15}, 20^{40}\text{-}21^{55}, \mathrm{R}^{0}19^{05}\text{-}21^{45}\ SW\text{-}NE, =14^{30}\text{-}23^{50}\ \equiv^{0}\text{-}24, \triangle^{0}0^{00}\text{-}9^{00}$
5	7	9.0	•	$\bullet^{0-1}19^{20}\text{-}20^{25}, \mathrm{R}^{0}17^{40}\text{-}20^{40}\ SW\text{-}E, \equiv^{0}0^{00}\text{-}1^{45}=\text{-}9^{30}, 16^{30}\text{-}24$
6	7	•	•	$\bullet^{0-1}2^{05}\text{-}4^{10}, =0^{00}\text{-}10^{30}$
7	7	9.1	•	$\bullet^{0-1}13^{20\text{-}35}, 17^{37}\text{-}19^{25}\ \bullet^{0}23^{06\text{-}32}, \mathrm{R}^{0}18^{12\text{-}20}\ S\text{-}N, =0^{30}\text{-}9^{40}, \triangle^{0}0^{00}\text{-}9^{00}$
8	8	•	•	$\triangle^{0}22^{00}\text{-}24$
9	8	•	•	$\triangle^{0}0^{00}\text{-}11^{00}, 22^{00}\text{-}24$
10	8	0.0	•	$\bullet^{0}23^{54}\text{-}24, \triangle^{1}0^{00}\text{-}9^{00}$
11	7	•	•	$\bullet^{0}0^{00\text{-}05}, 2^{05}\text{-}40$
12	7	•	•	$\triangle^{0}1^{00}\text{-}11^{00}, 22^{00}\text{-}24$
13	8	•	•	$=0^{00}\text{-}9^{20}, \triangle^{0}0^{00}\text{-}8^{00}, 22^{00}\text{-}24$
14	8	•	•	$=4^{40}\text{-}6^{30}, \triangle^{1}0^{00}\text{-}10^{00}\ \triangle^{0}21^{00}\text{-}24$
15	7	4.0		$\bullet^{0}15^{54}\text{-}16^{25}, 21^{35}\text{-}22^{25}\ \bullet^{0}23^{34}, \mathrm{R}^{0}22^{25}\text{-}23^{47}\ SW\text{-}NE, =1^{10}\text{-}2^{45}\ \equiv^{0-1}\text{-}6^{36}=\text{-}8^{30}, \triangle^{0}0^{00}\text{-}9^{00}$
16	6	0.0	•	$\bullet^{0}20^{28\text{-}45}, =2^{20}\text{-}14^{30}, 19^{30}\text{-}24$
17	7	7.2	•	$\bullet^{0}21^{38}\text{-}24, \mathrm{R}^{0}21^{45}\text{-}22^{40}\ S\text{-}NE, =0^{00}\text{-}10^{20}, \triangle^{1}2^{00}\text{-}10^{00}$
18	5	7.3	•	$\bullet^{0}0^{10}\text{-}3^{50}\ \bullet^{0-1}13^{25}\text{-}16^{05}, \mathrm{R}^{0}13^{40}\text{-}14^{20}\ SW\text{-}NE, =2^{00}\text{-}10^{20}$
19	7	5.4	•	$\bullet^{0-1}13^{51}, 21^{07}$
20	7	•	•	$\bullet^{0}5^{50}\text{-}7^{20}, =0^{00}\text{-}10^{30}\ 19^{40}\text{-}24$
21	8	•	•	$=0^{00}\text{-}8^{30}, \triangle^{0}20^{30}\text{-}24$
22	6	15.7	•	$\bullet^{0}8^{25}\text{-}10^{20}\ \bullet^{0-1}13^{54}\text{-}15^{20}\ \bullet^{0}20^{45}\text{-}21^{15}, =0^{30}\text{-}4^{45}\ \equiv^{0}\text{-}5^{50}=\text{-}24, \triangle^{1}0^{00}\text{-}8^{00}$
23	8	1.9	•	$\bullet^{0}4^{15\text{-}35}\ \bullet^{0-1}5^{07}\text{-}6^{08}\ 6^{20}, 7^{23}\ \bullet^{0}11^{54}, 12^{05}, 15^{50}\text{-}16^{15}\ \bullet^{0}16^{40}\text{-}17^{05}\ \bullet^{0}22^{55}\text{-}23^{10}, \mathrm{R}^{0}4^{43}\text{-}5^{40}\ SW\text{-}NE, =0^{00}\text{-}7^{20}$
24	6	15.4	•	$\bullet^{0}7^{35}\text{-}17^{40}, 18^{50}\ 19^{30}\ \bullet^{0-1}0, 22^{25}\ \bullet^{0}23^{50\text{-}55}, =4^{40}\text{-}22^{00}$
25	7	6.3	•	$\bullet^{0}13^{25\text{-}34}, 16^{32\text{-}40}\ \bullet^{0}17^{34\text{-}37}\ \bullet^{0}19^{35}$
26	8	•	•	$\triangle^{0}22^{00}\text{-}24$
27	7	•	•	$\triangle^{1}0^{00}\text{-}9^{00}$
28	8	•	•	
29	7	0.6	•	$\bullet^{0}12^{54}\text{-}13^{20}, \bullet^{0}15^{25}\text{-}17^{50}=14^{30}\text{-}24$
30	8	2.6	•	$\bullet^{0}14^{35\text{-}42}, 15^{50}\text{-}16^{03}, =0^{00}\text{-}5^{30}$
31	7	10.1	•	$\bullet^{0}1^{50}\text{-}4^{40}\ \bullet^{0}6^{25\text{-}50}\ \bullet^{0-1}8^{15}\text{-}9^{40}, 11^{31}, 17^{10}\ \bullet^{0}20^{52}\text{-}21^{20}, =6^{10}\text{-}10^{40}$
Σ	—	115.6	—	UWAGI

Olsztyn-Dajtki φ=53°46' λ=20°25' Wrzesień-Septembre 1962

Dni	Ciśnienie P 900 + I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność względna U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie N.w I	II	III	Kierunek i prędkość wiatru D.v I	II	III
1	98.4	100.7	103.6	100.9	10.5	15.5	8.8	10.9	15.9	8.7	95	61	93	83	0.7	6.9	0.8	2.8	3	4 ⊙	1	W 4	WNW 8	WNW 3
2	104.9	104.9	103.1	104.3	9.4	16.2	12.3	12.6	17.2	7.9	99	63	83	82	0.2	6.8	2.4	3.1	9	10	0	SW 3	WSW 5	SW 1
3	102.5	102.8	102.0	102.4	10.8	18.3	12.1	13.3	19.7	9.1	92	61	93	82	1.0	8.1	1.0	3.4	8	3	1	WSW 1	NW 3	NW 2
4	98.9	95.2	91.7	95.3	13.0	25.0	19.0	19.0	25.7	9.8	83	46	74	68	2.6	17.1	5.8	8.5	0	0	0	S 2	S 5	S 1
5	86.5	87.1	87.7	87.1	15.8	20.4	14.4	16.2	22.0	13.7	80	70	88	79	3.5	7.1	2.0	4.2	3	8	0	S 3	W 5	SW 2
6	87.4	88.5	86.8	87.6	12.7	17.0	12.8	13.8	18.7	11.4	81	59	87	76	2.8	8.0	1.9	4.2	6	7	0	SW 2	SW 8	C 0
7	78.7	77.8	83.0	79.8	15.1	15.8	13.2	14.3	17.6	11.9	98	86	90	91	0.4	2.4	1.6	1.5	10	9	10	S 4	SW 4	WSW 4
8	88.8	91.3	92.7	90.9	9.0	13.3	8.8	10.0	15.4	8.2	85	61	89	78	1.7	6.0	1.2	3.0	1	9	0	WSW 7	WSW 8	SW 1
9	97.8	101.0	103.9	100.9	10.0	13.9	10.0	11.0	15.4	7.9	93	65	83	80	0.8	5.6	2.1	2.8	7	8	9	W 4	W 4	SW 2
10	103.2	100.5	98.3	100.7	10.8	19.4	13.4	14.2	20.5	9.6	86	44	75	68	1.8	12.6	3.8	6.1	9	0	0	SW 3	SSW 4	SW 2
11	94.3	92.4	96.5	94.4	12.4	13.9	13.5	13.3	15.8	10.4	82	100	87	90	2.6	0.0	2.0	1.5	9	10 ●	9	SSW 2	S 2	WNW 6
12	97.1	89.9	83.2	90.1	9.6	16.1	17.3	15.1	20.6	7.8	99	87	76	87	0.2	2.3	4.7	2.4	9	10	0	SW 2	S 6	C 0
13	92.8	96.0	99.0	95.9	9.6	14.8	10.0	11.1	17.3	8.6	87	58	82	76	1.6	7.0	2.2	3.6	2	6	0	W 6	W 8	W 5
14	101.2	103.1	104.7	103.0	9.0	12.2	7.8	9.2	14.6	7.8	90	73	87	83	1.1	3.8	1.4	2.1	2	7	2	W 6	WNW 7	WNW 2
15	104.8	103.9	100.3	103.0	7.1	14.4	8.9	9.8	14.7	5.2	100	58	88	82	0.0	6.8	1.4	2.7	8	10	4	WSW 1	SW 2	ESE 2
16	94.8	92.8	92.4	93.3	7.4	20.6	14.3	14.2	20.8	6.4	93	56	94	81	0.8	10.6	0.9	4.1	1	4	9	SE 1	S 4	C 0
17	93.2	95.2	95.9	94.8	12.9	14.1	11.0	12.2	14.8	10.8	96	83	94	91	0.6	2.7	0.8	1.4	9	10	10 ●	N 2	N 2	N 1
18	94.4	93.5	88.2	92.0	8.4	13.2	9.8	10.3	13.6	7.5	99	68	97	88	0.1	4.8	0.3	1.7	7	10	10 ●	NNW 2	N 6	N 7
19	87.5	91.9	95.8	91.7	8.3	9.1	7.2	8.0	9.8	7.2	99	95	97	97	0.2	0.7	0.3	0.4	10 ●	10 ●	9	W 6	W 6	SW 3
20	96.8	97.7	97.7	97.4	7.4	11.0	7.2	8.2	11.3	6.3	97	77	90	88	0.3	3.1	1.1	1.5	10	7	9	SW 4	SW 5	SW 4
21	96.2	96.5	97.2	96.6	8.1	10.8	8.3	8.9	11.2	6.8	96	80	94	90	0.5	2.6	0.7	1.3	10 ●	10	10	W 5	WNW 7	WNW 4
22	98.0	99.7	101.1	99.6	8.2	10.3	8.2	8.7	11.0	7.2	97	87	99	94	0.3	1.6	0.2	0.7	9	9	10 ●	WNW 3	W 5	W 3
23	98.8	96.7	98.0	97.8	7.3	10.0	8.4	8.5	10.2	7.0	99	95	99	98	0.1	0.7	0.1	0.3	9	10	9	W 1	SW 1	C 0
24	103.6	105.9	109.6	106.4	5.0	12.5	6.2	7.5	13.5	4.6	100	65	98	88	0.0	5.0	0.2	1.7	10 ≡	9 ●	0	C 0	W 3	NW 1
25	113.5	114.4	114.1	114.0	3.2	14.0	8.0	8.3	15.1	1.7	100	70	93	88	0.0	4.8	0.7	1.8	10 ≡	6	0	C 0	E 2	E 1
26	113.5	111.9	109.7	111.7	5.2	15.2	8.6	9.4	15.7	3.8	100	60	85	82	0.0	7.0	1.7	2.9	0	3	1	E 2	E 4	E 2
27	106.8	104.1	102.5	104.5	5.5	11.6	10.4	9.5	12.7	4.2	97	77	93	89	0.3	3.1	0.8	1.4	0	10	10	E 1	ENE 5	E 4
28	100.7	100.4	99.2	100.1	10.5	11.1	11.2	11.0	12.1	10.2	96	91	95	94	0.5	1.1	0.7	0.8	10	10	10	ENE 2	E 2	E 1
29	97.9	98.5	99.8	98.7	10.5	12.3	12.0	11.7	12.5	10.0	99	98	100	99	0.2	0.3	0.0	0.2	10 ●	10 ●	10 ●	E 2	E 2	C 0
30	102.2	103.8	105.0	103.7	11.2	15.1	8.4	10.8	17.2	8.3	100	81	97	93	0.0	3.4	0.3	1.2	10	5	0 ≡	C 0	SW 1	C 0
31																								
M	97.8	97.9	98.1	97.9	9.5	14.6	10.7	11.4	15.8	8.0	94	73	90	86	0.8	5.1	1.4	2.4	6.7	7.5	4.8	2.7	4.5	2.1

Październik-Octobre

1	106.8	107.7	109.6	108.0	6.0	19.4	11.6	12.2	19.4	4.6	100	61	96	86	0.0	8.8	0.5	3.1	0 ≡	2	9	C 0	SS 3	SE 1
2	110.7	111.9	111.4	111.3	10.6	17.8	12.4	13.3	19.0	10.4	99	75	94	89	0.2	5.2	0.9	2.1	10 ≡	9	0	SE 1	SSE 1	SE 1
3	111.0	110.5	109.6	110.4	9.8	19.4	12.4	13.5	19.8	8.7	99	60	85	81	0.1	8.9	2.2	3.7	0 ≡	4	0	SE 1	S 3	SE 2
4	108.6	108.5	107.5	108.2	8.6	19.5	11.9	13.0	19.7	8.0	99	62	95	85	0.2	8.7	0.7	3.2	6	3 ⊙	0	SE 1	S 3	C 0
5	106.5	107.1	107.3	107.0	11.6	16.8	12.3	13.2	18.5	11.4	99	82	100	94	0.1	3.5	0.0	1.2	10	9	9	S 1	SW 1	C 0
6	108.2	110.5	113.2	110.6	12.1	15.1	13.0	13.5	15.7	11.5	100	89	98	96	0.0	1.9	0.4	0.8	10 ● ≡	9	10	E 1	NNW 1	NNW 2
7	115.7	117.9	119.0	117.5	11.6	12.9	11.4	11.8	13.3	11.4	96	84	84	88	0.5	2.4	2.2	1.7	10	10	8	N 1	N 2	N 1
8	119.8	120.2	118.6	119.5	2.3	13.2	6.6	7.2	14.3	1.7	100	74	100	91	0.0	4.0	0.0	1.3	2 ≡	2 ⊙	0	C 0	W 3	C 0
9	117.3	116.6	114.6	116.2	4.6	10.2	3.4	5.4	11.8	2.9	100	91	100	97	0.0	1.1	0.0	0.4	10 ≡	10	0 ≡	C 0	NW 1	NW 1
10	112.5	111.0	108.6	110.7	5.6	13.9	4.7	7.2	14.8	1.0	100	66	100	89	0.0	5.4	0.0	1.8	9 ≡	0	0 ≡	C 0	WSW 1	C 0
11	105.5	103.1	99.8	102.8	0.9	13.7	4.6	6.0	14.9	-0.6	100	67	100	89	0.0	5.2	0.0	1.7	0 ≡	0	0 ≡	SSW 1	SW 2	C 0
12	99.5	101.9	105.2	102.2	7.4	10.9	6.9	8.0	11.9	2.7	100	77	81	86	0.0	3.0	1.8	1.6	10	10	7	SW 1	N 2	N 1
13	106.2	105.6	101.4	104.4	-1.2	12.3	4.5	5.0	13.0	-1.4	100	52	95	82	0.0	6.8	0.4	2.4	0	2 ⊙	0	C 0	SW 2	SSW 1
14	95.9	93.6	97.7	95.1	3.8	10.8	7.6	7.4	11.4	3.1	98	74	94	89	0.1	3.4	0.6	1.4	8	10	10 ●	SSW 1	WNW 6	NNW 3
15	104.4	107.5	109.7	107.2	0.8	7.8	0.9	2.6	9.0	-0.4	98	56	79	78	0.2	4.7	1.4	2.1	5	7	0	NNE 1	NW 4	W 1
16	108.2	106.2	104.0	106.1	0.9	9.5	6.2	5.7	10.0	-1.6	85	54	69	69	1.0	5.5	3.0	3.2	6	4	9	SW 2	SW 4	SW 3
17	103.6	104.8	103.3	103.9	6.9	9.8	8.9	8.6	10.4	5.9	100	96	92	96	0.0	0.5	0.9	0.3	10 ●	10 ●	10	WSW 4	WSW 4	WSW 5
18	99.6	97.3	90.0	95.6	10.2	11.8	11.2	11.1	11.9	8.9	91	83	88	87	1.1	2.3	1.7	1.7	10	10	10	WSW 5	WSW 5	WSW 7
19	90.1	92.9	92.5	91.8	8.9	11.5	9.1	9.6	12.3	8.8	92	63	74	76	0.9	5.0	3.1	3.0	5	8	10	WNW 6	NW 8	W 4
20	96.8	102.6	108.9	102.8	5.1	8.7	1.8	4.4	9.4	1.6	92	51	82	75	0.7	5.4	1.3	2.5	3	4	0	W 5	NW 9	NW 3
21	110.6	110.3	110.7	110.3	2.9	10.7	8.7	7.8	11.4	0.1	83	70	97	83	1.3	3.9	0.3	1.8	2	8	10 ●	SW 5	WSW 6	W 4
22	110.8	110.6	109.6	110.3	8.3	10.2	8.2	8.7	10.8	8.2	99	78	83	87	0.2	2.7	1.8	1.6	10 ●	10	10	W 3	W 4	W 2
23	107.0	107.3	105.9	106.7	7.3	8.1	7.8	7.8	8.3	7.3	90	94	96	93	1.0	0.6	0.5	0.7	10	10 ●	10	WSW 1	SW 3	SW 2
24	102.3	102.0	103.3	102.5	4.6	10.0	5.6	6.4	10.0	4.6	98	68	95	87	0.2	3.9	0.4	1.5	9	8	10	SW 4	SW 2	SW 3
25	103.6	103.0	102.2	102.9	5.8	8.4	8.4	7.8	9.4	5.5	98	87	83	89	0.1	1.4	1.8	1.1	10	8	10	SW 1	SSW 2	SW 3
26	100.2	98.1	96.0	98.1	3.8	10.3	7.8	7.4	10.6	3.5	90	67	80	79	0.8	4.1	2.1	2.3	0	0	0	SSW 2	S 3	S 3
27	91.8	96.3	101.2	96.4	6.0	7.3	-0.3	3.1	7.9	-1.5	83	90	98	90	1.6	1.0	0.1	0.9	7	8	0	SW 3	W 3	W 1
28	97.7	93.9	93.4	95.0	1.4	5.1	3.4	3.3	6.3	-4.7	96	100	97	98	0.3	0.0	0.3	0.2	9	10 ●	8	SE 1	S 2	SW 3
29	94.4	96.0	98.8	96.4	2.7	6.0	4.8	4.6	6.3	1.9	100	95	100	98	0.0	0.5	0.0	0.2	10 ≡ ●	10 ●	10	S 1	WSW 1	W 1
30	100.1	99.2	97.3	98.9	-0.8	9.2	4.0	4.1	9.6	-1.8	100	69	95	88	0.0	3.6	0.4	1.3	0 ≡	1	4	C 0	SW 4	S 1
31	93.7	94.2	95.1	94.3	4.9	7.3	7.0	6.6	7.5	2.3	95	88	93	92	0.5	1.2	0.7	0.8	10	9	10	S 4	SE 1	C 0
M	104.4	104.8	104.7	104.8	5.6	11.3	7.3	7.9	12.2	4.0	96	75	91	87	0.4	3.7	1.0	1.7	6.5	6.6	5.6	1.8	3.2	1.9

Olsztyn - Dajtki $H_s = 133m$ $H_o = 135{,}4m$ $h_w = 12m$ Wrzesień - Septembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU s	POGODA
1	8	0.8	•	$\overset{*}{\bar{\vee}}{}^{\circ}0^{46-50}, 1^{50}\cdot 2^{10}, 9^{20-21}, 11^{23-38}, \triangle' np$
2	7	•	•	$= 7^{30}\cdot 9^{20}, \triangle' 0^{00}\cdot 9^{00}$
3	8	•	•	$\triangle^{\circ} 2^{00}\cdot 9^{30}, 20^{00}\cdot 24$
4	7	•	•	$\triangle^{\circ-1} 0^{00}\cdot 9^{00} \triangle^{\circ} np$
5	7	0.0	•	$\overset{*}{\bar{\vee}}{}^{\circ} 14^{52}\cdot 15^{03}, = 5^{30}\cdot 12^{20}, \triangle' 0^{00}\cdot 10^{00}$
6	8	1.6	•	$\triangle^{\circ} 0^{00}\cdot 9^{00}, 21^{00}\cdot 24$
7	7	1.6	•	$\bullet^{\circ-1} 2^{25}\cdot 5^{20} \overset{*}{\bar{\vee}}{}^{\circ} 12^{35}\cdot 13^{20}, 15^{30-45}, 17^{56}\cdot 18^{50}, = 6^{30}\cdot 9^{40}, \triangle^{\circ} 0^{00}\cdot 2^{55}$
8	8	0.4	•	$\overset{*}{\bar{\vee}}{}^{\circ} 19^{55}\cdot 20^{10}$
9	8	0.0	•	$\overset{*}{\bar{\vee}}{}^{\circ} 12^{02-05}$
10	8	•	•	
11	6	2.8	•	$\bullet^{\circ} 9^{40}\cdot 15^{25}, = 9^{30}\cdot 20^{30}, \triangle^{\circ} 2^{00}\cdot 9^{00}$
12	6	3.3	•	$\bullet^{\circ} 11^{04} \ldots 12^{20} \overset{*}{\bar{\vee}}{}^{\circ} 18^{55}\cdot 19^{05} \overset{*}{\bar{\vee}}{}' \cdot 19^{25}, = 13^{20}\cdot 14^{20}, \triangle^{\circ} 0^{00}\cdot 11^{00}$
13	8	0.0	•	$\overset{*}{\bar{\vee}}{}' 0^{04-15} \overset{*}{\bar{\vee}}{}^{\circ} 12^{14-17} 14^{18-22}$
14	8	0.1	•	$\overset{*}{\bar{\vee}}{}^{\circ} 14^{02-07}, 17^{08-25}, \triangle^{\circ} 3^{00}\cdot 9^{00}$
15	8	•	•	$\triangle' 2^{00}\cdot 10^{30} \triangle^{\circ} 22^{00}\cdot 24$
16	7	4.7	•	$\bullet^{\circ} 22^{51}\cdot 24, = 20^{30}\cdot 24, \triangle^{\circ-1} 0^{00}\cdot 11^{00}$
17	7	1.5	•	$\bullet^{\circ} 0^{00}\cdot 3^{28} 5^{55}\cdot 6^{20}, 8^{00}\cdot 9^{40}, 19^{54}\cdot 24, = 0^{00}\cdot 12^{30}$
18	8	26.6	•	$\bullet^{\circ} 0^{00}\cdot 1^{40}, 16^{53}\cdot 19^{05} \bullet' \cdot 23^{40} \bullet^{\circ}\cdot 24, = 4^{40}\cdot 10^{30}$
19	6	7.3	•	$\blacksquare^{\circ-1} 0^{00}\cdot 15^{20} \ldots 16^{10} \overset{*}{\bar{\vee}}{}^{\circ} 18^{45}\cdot 21^{04}$
20	7	5.3	•	$\overset{*}{\bar{\vee}}{}^{\circ} 15^{20} \ldots 16^{40}, 20^{50}\cdot 21^{15}, 23^{18}\cdot 24, = 7^{10}\cdot 11^{20}$
21	8	5.7	•	$\overset{*}{\bar{\vee}}{}^{\circ} 0^{00-50}, 5^{40}\cdot 8^{20}, 11^{34} \ldots 13^{25}, 18^{52-54}, 21^{55}\cdot 22^{10}, 23^{47}\cdot 24.$
22	8	6.9	•	$\overset{*}{\bar{\vee}}{}^{\circ} 0^{00-25} \overset{*}{\bar{\vee}}{}^{\circ-1} 2^{00}\cdot 4^{50} \overset{*}{\bar{\vee}}{}^{\circ} 8^{06-10}, 12^{08-41}, 15^{41} \ldots 20^{50} \bullet^{\circ} 21^{06}\cdot 23^{10}, = 19^{30}\cdot 24$
23	7	4.3	•	$\bullet^{\circ-1} 0^{10}\cdot 5^{03} \overset{*}{\bar{\vee}}{}^{\circ} 6^{45-48} \overset{*}{\bar{\vee}}{}^{\circ-1} 11^{10}\cdot 18^{50}, = 0^{00}\cdot 6^{30}$
24	8	1.1	•	$\overset{*}{\bar{\vee}}{}^{\circ} 13^{35} \ldots 15^{20}, \equiv^{+0} 3^{50}\cdot 9^{30} = \cdot 10^{20}\cdot 19^{30}\cdot 24$
25	8	•	•	$= 0^{00}\cdot 1^{45} \equiv^{\circ-1}\cdot 10^{25} = \cdot 11^{15}, \triangle^{\circ-1} 19^{30}\cdot 24$
26	8	•	•	$= 4^{15}\cdot 9^{40}, \triangle' 0^{00}\cdot 10^{00}, 21^{00}\cdot 24$
27	7	0.0	•	$= 5^{40}\cdot 8^{35}, 15^{30}\cdot 24, \triangle 0^{00}\cdot 11^{00}$
28	5	1.6	•	$\bullet^{\circ} 1^{50}\cdot 5^{20}, 8^{56}\cdot 10^{10} \ldots 11^{56}, 19^{51}\cdot 20^{18} \bullet^{\circ} 23^{49}\cdot 24, = 0^{00}\cdot 24$
29	4	0.9	•	$\bullet^{\circ} 0^{00}\cdot 6^{40}, 7^{30}\cdot 8^{20} \ldots 22^{40}, = 0^{00}\cdot 24$
30	7	•	•	$\bullet' 0^{52}\cdot 2^{45}, = 0^{00}\cdot 12^{20}, 16^{30}\cdot 17^{50} \equiv^{\circ}\cdot 24$
31				
Σ	—	76.5	—	UWAGI

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1	6	•	•	$\equiv^{\circ-1} 0^{00}\cdot 7^{50} = \cdot 14^{15}, 16^{40}\cdot 24, \triangle^{\circ} 19^{00}\cdot 24$
2	6	•	•	$= 0^{00}\cdot 6^{10} \equiv^{\circ}\cdot 8^{45} = \cdot 24, \triangle^{\circ} 0^{00}\cdot 9^{00}, 21^{00}\cdot 24$
3	8	•	•	$= 0^{00}\cdot 5^{45} \equiv^{\circ}\cdot 7^{40} = \cdot 10^{20}, \triangle 0^{00}\cdot 9^{00}, 21^{00}\cdot 24$
4	7	0.0	•	$\bullet^{\circ} 22^{52}\cdot 24, = 4^{40}\cdot 8^{20}, 17^{20}\cdot 24, \triangle^{2} 0^{00}\cdot 11^{00} \triangle^{\circ} 17^{30}\cdot 23^{00}$
5	6	1.5	•	$\bullet^{\circ} 0^{00}\cdot 2^{40}, 7^{35} \ldots 8^{14}, = 0^{00}\cdot 13^{40}, 16^{50}\cdot 24, \triangle' 19^{00}\cdot 23^{00}$
6	6	0.0	•	$\bullet^{\circ} 0^{06}\cdot 1^{40} \ldots 4^{30}\cdot 8^{50}, = 0^{00}\cdot 5^{45} \equiv^{\circ}\cdot 9^{40}$
7	7	•	•	$= 1^{00}\cdot 12^{20}, 23^{40}\cdot 24, \triangle' 1^{00}\cdot 10^{00} \triangle^{\circ} 21^{00}\cdot 24$
8	7	•	•	$= 0^{00}\cdot 2^{50} \equiv'^{\circ}\cdot 7^{48} = \cdot 9^{20}, 17^{30}\cdot 21^{50} \equiv^{\circ-1}\cdot 24, \triangle' 0^{00}\cdot 1^{00} \triangle^{\circ-1} 17^{00}\cdot 24$
9	5	•	•	$\equiv^{\circ-2} 0^{00}\cdot 10^{45} = \cdot 17^{45} \equiv^{\circ-2}\cdot 24, \triangle' 0^{00}\cdot 15^{00} 20^{00}\cdot 24$
10	6	•	•	$\equiv^{\circ-2} 0^{00}\cdot 7^{10} = \cdot 13^{30}, 17^{30}\cdot 19^{40} \equiv^{\circ-1}\cdot 21^{30} = \cdot 23^{20} \equiv^{\circ}\cdot 24, \triangle' 0^{00}\cdot 10^{00}, 18^{00}\cdot 24$
11	7	•	•	$\equiv^{\circ-2} 0^{10}\cdot 9^{50} = \cdot 12^{20}, 17^{40}\cdot 19^{45} \equiv'^{-2}\cdot 24, \triangle' na \sqcup^{\circ}\cdot 9^{00} \triangle' 18^{00}\cdot 24$
12	7	•	•	$\equiv^{2\circ} 0^{00}\cdot 5^{30} = \cdot 11^{20}, \triangle^{2} 0^{00}\cdot 11^{00}$
13	8	•	•	$= 5^{30}\cdot 7^{15} \equiv^{\circ}\cdot 7^{50} = \cdot 10^{22}, 17^{30}\cdot 24, \triangle^{\circ} na \sqcup^{\circ}\cdot 9^{00} \triangle^{\circ} 19^{00}\cdot 24$
14	6	2.0	•	$\bullet^{\circ} 16^{15}\cdot 17^{50}, 18^{20}\cdot 20^{40}, = 0^{00}\cdot 24, \triangle^{\circ} 0^{00}\cdot 10^{00}$
15	8	•	•	$= 3^{30}\cdot 5^{20}, \sqcup^{\circ} 1^{00}\cdot 8^{00}, 20^{00}\cdot 24$
16	8	0.0	•	$\sqcup^{\circ} 0^{00}\cdot 9^{00}$
17	5	0.0	•	$\bullet^{\circ} 6^{10}\cdot 7^{20}, 8^{52}\cdot 10^{03}, 10^{58}\cdot 14^{30} \ldots 18^{20}, 21^{38}\cdot 24, = 5^{30}\cdot 24$
18	6	0.3	•	$\bullet^{\circ} 0^{00}\cdot 2^{20}, 7^{03}\cdot 10^{40}, = 0^{00}\cdot 24$
19	8	0.3	•	$\bullet^{\circ} 1^{05}\cdot 3^{40}, 21^{25} \ldots 24, = 0^{00}\cdot 24$
20	8	•	•	$\bullet^{\circ} 0^{00}, 1^{25}, \sqcup^{\circ} 21^{00}\cdot 24$
21	8	0.2	•	$\bullet^{\circ} 18^{07}\cdot 21^{30} \ldots 24, = 21^{10}\cdot 24, \sqcup^{\circ-1} 0^{00}\cdot 8^{00}$
22	7	0.0	•	$\bullet^{\circ} 0^{00} \ldots 1^{30}\cdot 6^{30} \ldots 8^{40}, = 0^{00}\cdot 10^{50}$
23	6	0.0	•	$\bullet^{\circ} 9^{50} \ldots 18^{10}, = 7^{15}\cdot 24$
24	7	•	•	$= 0^{00}\cdot 12^{10}, 13^{38}\cdot 24$
25	4	•	•	$= 0^{00}\cdot 24$
26	6	•	•	$= 0^{00}\cdot 12^{20} = \cdot 15^{30} = \cdot 24$
27	7	1.3	•	$\bullet^{\circ} 8^{54}\cdot 11^{40}, = 0^{00}\cdot 12^{10}, 23^{35}\cdot 24, \sqcup' 20^{00}\cdot 24$
28	5	3.4	•	$\bullet^{\circ} 8^{13}\cdot 14 \bullet^{\circ}\cdot 18^{10}, = 0^{00}\cdot 1^{10} \equiv'^{-0}\cdot 4^{20} = \cdot 21^{30}, \sqcup' 0^{00}\cdot 7^{00}$
29	4	0.4	•	$\bullet^{\circ} 6^{25}\cdot 7^{35}, 8^{06}\cdot 13^{40} \ldots 15^{30}, = 0^{30}\cdot 6^{18} \equiv^{\circ}\cdot 9^{40} = \cdot 17^{50} \equiv^{\circ-1}\cdot 20^{10}\cdot 24$
30	7	•	•	$= 0^{00}\cdot 1^{36} \equiv^{\circ-1}\cdot 8^{48} = \cdot 12^{10}$
31	6	0.1	•	$= 5^{30}\cdot 24, \triangle^{\circ} 1^{00}\cdot 10^{00}$
Σ	—	9.5	—	UWAGI

Olsztyn - Dajtki φ = 53°46' λ = 20°25' Listopad - Novembre 1962

DNI	CIŚNIENIE P - 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D.v I	II	III
1	92.8	92.2	91.7	92.2	7.2	9.3	9.1	8.7	9.5	6.7	100	100	100	100	0.0	0.0	0.0	0.0	10 ●	10 ⚲	10 ═	E 4	E 1	N 2
2	92.8	95.7	99.0	95.8	9.4	9.8	8.0	8.8	10.1	7.6	100	100	94	98	0.0	0.0	0.6	0.2	10	10 ⚲ ═	10	N 1	SSW 1	SW 2
3	100.6	101.2	101.6	101.1	6.8	7.5	5.6	5.4	8.0	5.4	100	93	100	98	0.0	0.8	0.0	0.3	10 ⚲	10	2 ═	SW 1	SSW 2	C 0
4	101.1	101.5	101.8	101.5	9.2	12.5	11.1	11.0	12.8	3.6	100	86	86	91	0.0	2.1	1.8	1.3	10 ═	9	10	SE 1	S 4	SSE 1
5	101.1	100.6	101.0	100.9	9.4	9.5	7.6	8.5	11.2	7.6	93	89	69	84	0.8	1.3	3.2	1.8	10	9	0	SE 5	SE 5	SE 5
6	100.2	100.0	102.4	100.9	2.3	9.7	6.5	6.2	10.4	1.9	80	46	58	61	1.4	6.5	4.1	4.0	0	2 ⊙	2	SE 4	ESE 8	SE 5
7	103.9	105.7	107.3	105.6	3.2	8.9	5.7	5.9	9.6	3.1	74	57	59	63	2.0	4.9	3.8	3.6	6	7	2	SE 5	ESE 6	SE 6
8	105.8	103.6	103.3	104.2	1.0	7.1	6.3	5.2	7.4	1.0	88	71	85	81	0.8	2.9	1.4	1.7	2	4	0	E 3	E 6	ESE 4
9	102.7	104.5	105.3	104.2	3.2	4.9	4.0	4.0	6.4	2.4	95	84	88	89	0.4	1.4	0.9	0.9	6	9	9	E 5	E 8	E 8
10	106.2	107.6	108.8	107.5	2.5	2.4	1.3	1.9	4.2	1.2	82	70	72	75	1.3	2.2	1.9	1.8	10	10	10	ENE 8	ENE 7	ENE 7
11	109.5	109.3	108.6	109.1	0.3	0.7	0.8	0.6	1.5	-0.1	100	98	98	99	0.0	0.1	0.2	0.1	10 ✳	10 ✳	10 ✳	ENE 7	ENE 7	E 7
12	107.4	106.5	104.2	106.0	0.9	0.4	0.6	0.6	1.3	0.3	90	90	94	91	0.6	0.6	0.4	0.5	10	10	10 ✳	E 9	E 8	E 5
13	103.1	104.1	104.7	104.0	1.4	2.9	3.4	2.8	3.7	0.6	100	100	100	100	0.0	0.0	0.0	0.0	10 ⚲	10 ═	10	SE 4	SSE 2	SSE 1
14	103.7	102.9	101.4	102.7	2.5	3.7	3.4	3.2	3.9	2.5	100	97	100	99	0.0	0.3	0.0	0.1	10	10	10 ═	SE 1	SE 1	SE 1
15	95.6	92.2	87.4	91.7	3.7	5.4	5.2	4.9	5.8	3.4	100	98	100	99	0.0	0.2	0.0	0.1	10	10	10 ●	S 2	SSW 3	SSW 1
16	87.6	89.6	91.8	89.7	1.0	2.9	0.0	1.0	5.3	0.0	90	83	86	86	0.7	1.3	0.9	1.0	6	9	3	SW 4	W 3	WSW 3
17	94.9	97.0	98.3	96.7	-1.6	-0.9	-1.2	-1.2	0.0	-2.1	96	91	86	91	0.2	0.5	0.8	0.5	9	10	9	WSW 4	WSW 5	SSW 2
18	95.3	92.3	89.9	92.5	-1.3	0.1	1.0	0.2	1.2	-2.2	82	78	87	82	1.0	1.4	0.9	1.1	10	10	10	ESE 6	SE 8	SE 5
19	82.8	84.6	91.1	86.2	1.2	4.5	2.7	2.8	4.5	0.2	98	93	89	93	0.2	0.5	0.8	0.5	10 ✳	10 ●	9	SE 4	S 8	S 3
20	89.7	89.2	87.6	88.8	1.3	2.7	0.4	1.2	2.7	0.3	100	100	100	100	0.0	0.0	0.0	0.0	9 ═	10 ●	10 ✳	NE 2	NNW 3	NNW 5
21	93.5	94.5	96.1	94.7	0.1	1.5	-1.0	-0.1	1.8	-1.0	90	87	89	89	0.7	0.9	0.7	0.8	10	1	10	W 3	SW 2	C 0
22	94.7	96.0	98.9	96.5	-2.0	0.4	-0.8	-0.8	0.8	-3.4	98	94	95	96	0.1	0.4	0.3	0.3	9	9	10	N 2	N 1	C 0
23	101.8	103.7	106.7	104.1	1.0	0.4	0.0	0.4	1.0	-1.0	94	82	84	87	0.4	1.1	1.0	0.8	10	8	10	S 1	SW 2	SSW 1
24	109.4	111.5	113.8	111.6	-0.6	-0.4	-3.2	-1.8	0.1	-3.5	90	84	95	90	0.6	0.9	0.2	0.6	10	10	6	C 0	W 2	W 1
25	114.6	113.6	112.5	113.6	-2.6	-1.8	-2.7	-2.4	-1.7	-4.2	89	90	95	91	0.6	0.5	0.2	0.4	10	10	10	SW 1	SW 2	SW 2
26	113.9	115.3	115.6	114.9	-5.6	1.0	0.8	-0.8	1.0	-5.9	95	88	98	94	0.2	0.8	0.2	0.4	2	10	10 ═	C 0	SW 1	SW 1
27	113.0	113.2	110.8	112.3	1.6	2.2	2.3	2.1	2.3	0.7	100	100	100	100	0.0	0.0	0.0	0.0	10 ⚲	10 ═	10 ⚲	SW 1	SW 1	SW 1
28	105.0	103.3	104.0	104.1	3.7	4.0	4.0	3.9	4.0	2.2	93	92	98	94	0.6	0.6	0.1	0.4	10	10	10 ⚲	WSW 5	W 5	W 3
29	103.0	102.4	94.9	100.1	2.6	4.2	5.6	4.5	5.7	2.5	100	88	95	94	0.0	0.9	0.4	0.4	10	9	10 ⚲	NW 1	W 3	SW 7
30	91.2	94.3	101.9	95.8	3.9	2.1	-0.2	1.4	5.7	-0.5	93	93	94	93	0.6	0.5	0.4	0.5	9	10 ●	9	WSW 7	NNW 3	NNE 3
31																								
M	100.6	100.9	101.4	101.0	2.2	3.9	2.8	2.9	4.7	0.9	94	87	90	90	0.4	1.1	0.8	0.8	8.6	8.9	8.0	3.4	3.9	3.1

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1	111.4	115.7	120.9	116.0	-3.2	-0.2	-1.8	-1.8	0.3	-5.8	90	92	94	92	0.5	0.5	0.3	0.4	3	6	0	W 3	N 2	W 1
2	122.5	123.2	122.0	122.6	-2.8	0.1	-2.1	-1.7	0.4	-3.4	91	86	87	88	0.5	0.9	0.6	0.7	3	5	9	WSW 3	W 5	W 6
3	119.3	117.7	113.0	116.7	-4.0	-2.3	-4.3	-3.7	-2.1	-4.7	82	74	89	82	0.8	1.4	0.5	0.9	6	8	6	SW 8	SW 5	SW 5
4	107.9	105.9	102.0	105.3	-2.8	-0.8	0.2	-0.8	0.3	-4.8	86	87	68	80	0.7	0.7	2.0	1.1	10	10	4	SW 3	WSW 4	WSW 5
5	102.9	107.4	110.9	107.1	2.4	4.3	3.7	3.5	4.4	-0.5	95	100	100	98	0.4	0.0	0.0	0.1	10	10	10	W 4	NW 2	WNW 3
6	110.6	110.1	109.0	109.9	1.4	0.5	0.2	0.6	3.7	0.2	96	100	98	98	0.3	0.0	0.1	0.1	10	10 ═	10	W 6	SW 6	SW 5
7	107.2	107.2	109.2	107.9	-1.6	0.4	-0.9	-0.8	0.8	-2.7	96	80	93	90	0.2	1.3	0.4	0.6	10	1 ⊙	10	SW 5	SW 4	W 2
8	111.4	111.8	108.8	110.7	0.7	2.0	-3.4	-1.0	2.0	-3.4	100	91	90	94	0.0	0.7	0.5	0.4	10	8	8	W 1	SW 2	SSW 3
9	97.0	89.0	81.6	89.2	-1.6	1.6	1.0	0.5	1.6	-3.6	86	74	71	77	0.7	1.8	1.9	1.5	3	10	10	SSW 5	SSW 9	SSW 6
10	78.0	78.7	80.6	79.1	2.1	2.4	2.4	2.3	3.1	0.1	84	96	98	93	1.2	0.3	0.2	0.6	10	10 ●	10 ●	SW 8	SW 8	SW 5
11	82.9	84.5	82.4	83.3	2.3	2.0	2.0	2.1	2.7	1.5	93	91	96	93	0.5	0.7	0.3	0.5	10	6	10 ●	W 5	SW 4	SW 6
12	76.1	75.3	76.4	75.9	1.6	3.2	2.9	2.6	3.2	1.1	98	93	83	91	0.2	0.5	1.3	0.7	10 ●	10 ●	10 ●	S 6	SW 6	SSW 6
13	80.4	80.8	81.5	80.9	1.9	1.0	1.1	1.3	3.5	0.6	85	94	90	90	1.0	0.4	0.6	0.7	10	10 ✳	10	SSW 4	SE 3	S 2
14	83.2	85.1	85.2	84.5	0.5	1.9	-0.8	0.2	1.9	-0.9	98	94	87	93	0.1	0.4	0.7	0.4	10	8	8	C 0	W 3	W 2
15	77.0	67.8	63.2	69.3	-2.2	-0.9	0.5	-0.5	0.5	-2.6	85	89	94	89	0.8	0.6	0.3	0.6	3	10 ✳	10	SW 5	S 5	SW 5
16	58.5	58.6	63.3	60.1	0.4	1.0	-0.2	0.2	1.0	-0.2	98	88	92	93	0.1	0.8	0.5	0.5	10	9	4	S 3	SE 3	NE 3
17	71.4	75.2	79.5	75.4	-0.1	-2.0	-2.8	-1.9	0.2	-3.0	92	94	88	91	0.5	0.4	0.6	0.5	10	10 ✳	10 ✳	NNE 3	NNE 2	N 2
18	81.2	81.9	84.4	82.5	-5.0	-5.1	-6.6	-5.8	-2.4	-7.1	95	95	91	94	0.2	0.2	0.3	0.2	9 ✳	9	10 ✳	C 0	N 1	N 2
19	88.1	91.3	98.0	92.5	-8.4	-7.1	-10.4	-9.1	-6.5	-10.7	92	88	90	90	0.3	0.4	0.3	0.3	10 ✳	10 ✳	10	N 1	N 4	NE 3
20	103.9	106.6	108.3	106.3	-16.8	-14.1	-16.1	-15.8	-10.2	-18.4	85	75	81	80	0.2	0.3	0.3	0.3	2	8	0	C 0	N 2	ESE 3
21	106.3	105.8	108.7	106.9	-17.6	-13.8	-16.6	-16.2	-13.8	-18.4	84	79	85	83	0.2	0.4	0.2	0.3	1	2	0	NE 3	E 3	NE 3
22	115.3	120.2	125.1	120.2	-19.6	-16.4	-17.4	-17.7	-15.7	-20.2	83	80	74	79	0.2	0.3	0.4	0.3	0	0	0	NE 3	NE 3	NE 3
23	128.7	130.3	131.5	130.2	-19.7	-13.6	-19.8	-18.2	-13.4	-22.0	83	71	83	79	0.2	0.6	0.2	0.3	0	0	0	NNE 3	NNE 2	N 2
24	129.3	127.8	126.2	127.8	-10.8	-7.1	-7.9	-8.4	-6.1	-20.9	87	82	93	87	0.4	0.6	0.2	0.4	10	8	10	N 1	N 2	C 0
25	121.0	117.1	110.2	116.1	-5.8	-4.2	-5.9	-5.4	-4.0	-8.0	89	87	94	90	0.4	0.6	0.2	0.4	10	6	10	C 0	E 1	S 2
26	102.4	98.7	95.7	98.9	-9.6	-11.8	-14.0	-12.4	-5.6	-15.3	82	82	87	84	0.5	0.4	0.3	0.4	10 ✳	10 ✳	9	SSW 3	SW 3	SW 1
27	93.8	93.9	95.1	94.3	-11.4	-8.7	-8.8	-9.4	-8.2	-14.0	90	89	89	89	0.3	0.4	0.4	0.4	10 ✳	10 ✳	10 ✳	SW 3	SSW 2	S 2
28	94.3	94.9	96.0	95.1	-8.2	-6.8	-6.5	-7.0	-6.3	-9.2	92	85	86	88	0.2	0.3	0.3	0.4	10 ✳	10 ✳	10 ✳	S 3	SW 4	SSW 3
29	95.7	93.5	91.0	93.4	-6.2	-6.2	-8.6	-7.4	-5.5	-8.9	89	86	89	88	0.4	0.5	0.4	0.4	10 ✳	9	10	SSE 3	SE 3	S 1
30	92.5	96.3	100.1	96.3	-8.6	-5.9	-9.1	-8.2	-5.7	-11.6	92	84	92	89	0.3	0.6	0.3	0.4	10	10 ⚠	10	W 3	WNW 5	NE 4
31	103.7	106.3	108.5	106.2	-13.6	-12.4	-17.8	-15.4	-8.6	-18.1	84	85	84	84	0.4	0.4	0.2	0.3	4	3	0	NE 3	NE 3	NE 1
M	98.5	98.7	99.0	98.7	-5.4	-5.8	-5.4	-5.0	-2.7	-7.6	90	87	88	88	0.4	0.6	0.5	0.5	7.5	7.6	7.4	3.3	3.6	3.2

Olsztyn-Dajtki $H_s = 133m$ $H_t = 135{,}4m$ $h_w = 12m$ Listopad - Novembre 1962

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	4	2.7	•	•°1^{25}-6^{40} 7^{50}-12^{30} •-17^{50} •°-21^{30}; =0^{00}-6^{45} ≡°-24
2	5	0.0	•	•°12^{35}-14^{35}; ≡°0^{00}-5^{40} =-7^{10} ≡°-13^{45} =-24
3	6	0.0	•	•°5^{51}-11^{40}; =0^{00}-19^{50} ≡°-21^{10} =-24
4	6	•	•	•°0^{50}-3^{20}; =0^{00}-6^{35} ≡°-11^{55} =-13^{30}
5	6	•	•	=7^{20}-17^{10}
6	8	•	•	
7	8	•	•	ϖ17^{40}-19^{30}
8	7	•	•	
9	6	•	•	=7^{30}-14^{20}
10	7	0.2	•	
11	5	3.7	•	*°4^{51}-24; =6^{15}-24
12	7	0.6	•	*°0^{00}-2^{20} •°12^{55}-15^{25} *°-19^{40} *°-23^{25} •-24; =0^{00}-12^{10}
13	5	1.3	•	•°0^{00}-11^{50} •°15^{35}-17^{20}, 18^{50}-19^{45}, 22^{54}-24; =5^{20}-6^{50} ≡°-20^{50} =-24
14	4	0.2	•	•°0^{00-40} 2^{40}-4^{20}; =, ≡°0^{00}-19^{10} ≡°-24
15	2	3.3	•	•°1^{33}-2^{10} •°-3^{35} •°7^{51}-8^{20} •°9^{53}-11^{45} •...16^{20}-24; ≡°=0^{00}-24
16	6	•	•	•°0^{00}-2^{40}; =0^{00}-13^{15}; ⌴°23^{00}-24
17	7	•	•	⌴°0^{00}-11^{00}
18	7	2.6	•	*°22^{52}-24
19	6	4.4	2	*°0^{00}-2^{20}; 3^{55}-7^{40} *°-8^{15} •°-12^{30}...13^{06}; =8^{15}-14^{30}
20	4	12.8	•	•°0^{03}-3^{20}...5^{10} •9^{52}-13^{20} *°13^{35}-15^{38} *°-24; =2^{30}-6^{30} ≡°-12^{20} =-24
21	6	•	3	*°0^{00-20} •°1^{10}-3^{25}; =0^{00}-24
22	6	0.9	2	=0^{00}-24
23	6	0.0	2	*°1^{50}-4^{20} •°8^{52}-9^{14}; =0^{00}-24
24	6	•	2	=0^{00}-24
25	6	•	2	=0^{00}-24
26	5	0.0	2	=0^{00}-13^{40} ≡°-20^{52} =-24
27	3	0.3	2	•°3^{46}-6^{40}, 7^{52}-12^{10}, 17^{55}-24; =0^{00}-6^{35} ≡°-19^{40} =-24
28	6	3.6	•	•°0^{00}-3^{25}, 12^{55}-16^{20}, 20^{35}-23^{40} •°-24; =0^{00}-24
29	7	7.3	•	•°0^{00}-6^{20}, 14^{56}-24; =0^{00}-12^{10}
30	7	1.2	•	•°0^{00}-5^{46} ▽°10^{30}-13^{40} ⚥°14^{50} ▽°-15^{26}; =5^{46}-7^{10}
31				
Σ	—	45.1	—	UWAGI.

Grudzień - Décembre

1	7	0.8	•	⚥°8^{15}-9^{03}, 9^{13}-10^{10}, 14^{45}-13^{20}; =7^{15}-10^{30}
2	8	•	2	
3	7	•	2	
4	5	0.2	2	=6^{30}-20^{20}
5	5	0.2	2	•°0^{40}-3^{25}, 10^{56}-12^{20}, 16^{45}-19^{25}; =2^{00}-24
6	3	0.0	•	•°16^{05}-21^{40}; =0^{00}-1^{20} 6^{20}-7^{45} ≡°-18^{52} =-24
7	7	•	•	=0^{00}-10^{25}, 14^{30}-24; ⌴°15^{00}-24
8	5	•	•	=0^{00}-7^{25} ≡°-10^{40} =-24; ⌴°0^{00}-8^{00} ⌴'21^{00}-24; ϖ18^{30}-21^{00}
9	6	1.6	•	*°18^{45}-20^{05}; =0^{00}-24; ⌴°0^{00}-13^{00}
10	6	2.5	•	•°1^{10}-3^{30} *°-4^{50} ▽°8^{55}-9^{05} ⚥'-12^{10} ▽°-14^{40}, 18^{40}-24; =0^{00}-3^{00}, 14^{40}-24
11	7	3.1	•	⚥°5^{46}...12^{20}, 17^{53}-22^{10} •-23^{20}; =0^{00}-1^{45}, 18^{30}-24
12	6	0.3	•	•°0^{50}-10^{56}, 11^{15}-11^{25}...13^{20}, 14^{40}-21^{38}; =0^{00}-13^{30}, 15^{20}-19^{30}
13	5	0.6	•	*°11^{20}-14^{10} •°-17^{20} *°-18^{50}; ≡8^{20}-24
14	6	0.0	•	*°17^{54}-19^{35}; =0^{00}-7^{15} =°-10^{50} =-20^{15}
15	5	2.3	•	*°-10^{25}-19^{40}
16	6	0.3	3	*°0^{50}-3^{20} 13^{08}-14^{52}, 17^{38}-18^{50} ⚥°-19^{12}; =7^{30}-24
17	6	1.3	3	⚥°0^{53}-2^{34} *°7^{25}-15^{50}, 16^{35}-24; =0^{00}-24
18	6	0.3	4	*°0^{00}-3^{30}...12^{40}, 19^{55}-24; =0^{00}-24
19	6	0.0	5	*°0^{00}-7^{20}, 11^{32}-15^{50}; =0^{00}-19^{30}
20	7	•	5	
21	7	•	5	
22	7	•	5	
23	7	•	5	
24	7	0.0	5	*°7^{50}-10^{52}; =9^{30}-11^{30}
25	7	0.3	5	*°8^{25}-10^{50} ⚥°12^{32}-13^{25}, 14^{50}-17^{18}
26	6	0.0	7	*°0^{50}-14^{45}
27	6	0.2	7	*°0^{20}-15^{38}, 21^{30}; =7^{15}-24
28	5	0.1	7	*°0^{00}-15^{40}...17^{30}-20^{10}...21^{10}; =0^{00}-24
29	5	0.6	7	*°-6^{55}-10^{40}...12^{50}; =0^{00}-24
30	6	0.0	7	△11^{56}-12^{40}; =0^{00}-24
31	7	•	7	=0^{00}-12^{10}, 16^{30}-24
Σ	—	15.1	—	UWAGI.

Chojnice φ = 53°42' λ = 17°33' Styczeń - Janvier 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	76.8	79.6	82.3	79.6	2.5	0.7	1.0	1.3	3.0	-1.2	86	92	81	86	1.0	0.5	1.3	0.9	4	10 *	10 ✱	SW 9	SW 14	W 16
2	86.2	89.2	93.7	89.7	-0.9	-1.4	-4.8	-3.0	1.2	-4.8	89	86	88	88	0.6	0.8	0.5	0.6	10 ●	10 *	0	W 10	WNW 4	WNW 2
3	94.6	97.9	102.3	98.3	-2.5	0.7	-0.4	-0.6	1.0	-6.3	91	94	88	91	0.5	0.4	0.7	0.5	10	10	10	WNW 4	NW 5	WNW 1
4	103.4	102.8	102.5	102.9	-1.0	-1.4	-1.2	-1.2	-0.4	-1.5	91	94	91	92	0.5	0.3	0.5	0.4	10	10	10	WSW 4	WSW 5	WNW 5
5	99.9	97.6	92.8	96.8	-0.5	-0.3	-3.6	-2.0	0.0	-3.6	94	94	94	94	0.4	0.4	0.3	0.4	10	10 ●	10	WNW 6	WSW 5	WSW 7
6	87.9	85.9	85.8	86.5	-2.2	-0.7	0.6	-0.4	0.8	-4.1	94	95	98	96	0.3	0.3	0.1	0.2	10	10 *	10	WSW10	WSW 9	W 9
7	95.4	99.4	102.9	98.6	0.8	0.6	-2.5	-0.9	1.4	-2.5	92	90	91	91	0.5	0.6	0.5	0.5	9	9	0	NW 5	NW 4	WSW 2
8	101.0	101.8	101.4	101.4	-0.5	0.6	0.4	0.2	1.0	-3.9	96	96	96	96	0.3	0.3	0.3	0.3	10 ≡	10 ≡	10	SW 3	SW 3	SW 3
9	96.2	92.3	90.0	92.8	1.0	1.2	0.6	0.8	1.5	0.3	96	90	84	90	0.3	0.7	1.0	0.7	10 ≡	9	10	S 3	S 5	SW 6
10	87.1	83.7	80.7	83.8	0.2	0.2	-1.0	-0.4	0.9	-1.2	88	82	83	84	0.7	1.1	1.0	0.9	10	9	10	S 3	SSE 5	SSE 5
11	81.0	77.1	74.4	77.5	2.1	2.3	3.8	3.0	4.1	-1.0	84	82	83	83	1.2	1.3	1.3	1.3	10	10	10	SSW 7	SSE10	SSW10
12	79.5	79.7	71.2	76.8	2.8	2.7	1.6	2.2	4.1	1.4	86	91	89	89	1.1	0.6	0.8	0.8	9	8	9	SW 8	SW 5	S 6
13	63.6	65.3	69.5	66.1	1.4	2.3	2.0	1.9	3.2	0.2	96	84	76	85	0.3	1.2	1.7	1.1	10	9	10	SW 6	SW 9	SW 10
14	73.3	76.6	79.1	76.3	0.9	1.2	0.9	1.0	2.1	0.3	75	89	94	86	1.6	0.8	0.4	0.9	9	10	10 ●	SW 7	SW 8	SW 6
15	84.4	88.8	93.7	89.0	1.6	1.9	1.2	1.5	2.3	0.8	93	91	89	91	0.6	0.6	0.8	0.7	10	10 ●	10	WSW 6	SW 5	W 4
16	96.1	94.6	90.7	93.8	0.2	0.9	1.3	0.9	2.1	-0.6	92	81	77	83	0.5	1.2	1.5	1.1	9	10	10	SW 4	SW 5	SSW 5
17	89.5	90.6	92.1	90.7	0.3	1.6	0.8	0.9	2.4	0.3	98	94	85	92	0.1	0.4	1.0	0.5	10 *	10	10	SW 5	SW 6	S 5
18	90.3	89.0	89.8	89.7	1.1	1.9	1.9	1.7	2.4	0.7	81	80	91	84	1.2	1.4	0.6	1.1	10	9	10	SSW 5	SW 6	SW 6
19	92.2	92.1	84.7	89.7	1.4	1.4	2.4	1.9	2.6	0.6	96	98	95	96	0.3	0.2	0.6	0.4	10	10 ≡	10 ●	WSW 5	SW 5	S 6
20	84.0	88.4	96.0	89.3	3.6	3.9	3.3	3.5	4.6	2.4	80	88	88	85	1.6	1.0	0.9	1.2	10 ●	10 ●	10	W 12	W 10	W 7
21	94.0	95.5	91.7	93.7	3.2	4.3	5.7	4.7	5.9	1.2	95	88	98	94	0.4	1.0	0.2	0.5	10 ●	10	10	W 5	W 3	SW 3
22	84.8	78.7	81.1	81.5	5.0	6.8	3.8	4.8	7.0	3.3	95	81	73	83	0.4	1.9	2.1	1.5	10	10 ●	8	SSW 3	S 7	W 14
23	84.8	86.5	87.7	86.3	2.2	2.9	1.8	2.2	4.0	1.3	78	81	91	83	1.6	1.4	0.7	1.2	8	9	10 ●	WSW12	SW 10	SW 12
24	90.7	91.2	90.1	90.7	1.4	2.1	1.2	1.5	2.6	0.4	85	93	96	91	1.0	0.5	0.3	0.6	10	10	10	SW 7	WSW 4	SW 2
25	85.5	83.4	87.0	85.3	0.7	0.8	0.2	0.5	1.4	0.2	94	98	98	97	0.4	0.2	0.1	0.2	10 ● *	10 ● ≡	10	SE 4	ESE 2	NE 2
26	94.9	96.3	92.7	94.6	0.3	1.8	-0.1	0.5	2.0	-0.4	94	78	90	87	0.3	1.6	0.7	0.9	10	6 ⦿	10	NW 2	NW 3	W 2
27	88.8	90.7	89.1	89.5	0.7	2.0	1.0	1.2	2.3	-0.2	94	85	92	90	0.4	1.1	0.5	0.7	10 *	10	2	W 5	NW 7	WNW 3
28	91.5	92.6	97.6	93.9	-2.3	-2.6	-4.0	-3.2	1.2	-4.7	85	83	87	85	0.8	0.9	0.6	0.8	10	10 *	10 *	NW 10	NNW14	N 8
29	103.9	108.4	112.8	108.4	-5.0	-4.3	-8.9	-6.8	-3.8	-9.0	85	75	83	81	0.6	1.1	0.5	0.7	9	9	8	N 6	NNE 7	ENE 3
30	115.7	118.0	118.7	117.3	-13.0	-7.8	-10.8	-10.6	-7.8	-13.7	80	73	87	80	0.5	0.9	0.4	0.6	0	0 ⦿	10	NE 4	NE 2	ENE 3
31	116.7	115.0	111.2	114.3	-13.6	-9.8	-12.3	-12.0	-8.8	-14.6	84	72	78	78	0.4	0.8	0.5	0.6	4	0 ⦿	0	NE 2	SE 1	SE 2
M	90.7	91.2	91.5	91.1	-0.3	0.5	-0.5	-0.2	1.5	-1.9	89	87	88	88	0.7	0.8	0.7	0.7	9.1	8.9	8.6	5.9	6.0	5.6

Luty - Février

1	101.1	94.7	95.1	96.3	-14.3	-8.0	-9.0	-10.1	-7.9	-14.3	83	75	82	80	0.3	0.8	0.5	0.5	0	0 ⦿	10	SE 3	SE 4	SSW 3
2	92.7	94.4	98.4	95.2	-11.8	-5.3	-4.1	-6.3	-4.0	-12.6	86	87	89	87	0.4	0.5	0.5	0.5	10	10 *	10	SSE 2	SSW 3	SW 3
3	102.2	103.6	102.3	102.8	-3.1	-1.3	-1.3	-1.8	-0.7	-4.2	93	93	86	91	0.4	0.4	0.8	0.5	10 ≡	10	10	SW 2	SW 3	SW 6
4	92.5	92.7	95.3	93.6	-2.3	0.3	-0.5	-0.8	2.1	-2.8	87	87	88	87	0.7	0.8	0.7	0.7	10	9	0	SSW 9	SW 5	W 3
5	89.9	79.0	77.6	82.2	-1.8	-1.3	1.2	-0.2	1.4	-3.4	98	90	96	95	0.1	0.5	0.3	0.3	10 ≡	10 *	10 ●	SW 5	SE 5	WSW 7
6	84.9	91.1	96.5	90.8	1.2	1.1	0.5	0.8	2.1	0.3	85	89	88	87	1.1	0.7	0.7	0.8	9	9	9	NW 12	NW 10	WNW 6
7	94.1	92.2	89.4	91.9	-0.4	0.7	1.1	0.6	1.2	-0.6	96	96	98	97	0.2	0.2	0.1	0.2	10	10 ≡	10	S 5	S 3	S 3
8	86.7	87.9	90.3	88.3	0.6	1.2	1.8	1.4	2.2	0.6	98	98	98	98	0.1	0.2	0.2	0.2	10 ●	10 ≡	10 ≡	S 4	SW 4	SW 4
9	95.1	101.7	107.4	101.4	0.7	0.8	-2.1	-0.7	1.8	-2.1	94	86	91	90	0.4	0.9	0.4	0.6	10	10	0	W 6	NW 5	NW 3
10	107.4	106.2	103.4	105.7	-1.0	0.6	0.8	0.3	1.6	-3.5	87	90	96	91	0.8	0.6	0.3	0.6	9	10 *	10 ●	SW 2	SW 4	SW 5
11	96.4	97.4	99.9	97.9	1.2	2.4	1.5	1.6	2.6	0.8	96	80	78	85	0.3	1.5	1.5	1.1	10 ●	9 ✱	8	SW 7	W 8	W 10
12	80.2	63.0	54.8	66.0	-0.7	1.7	1.3	0.9	3.5	-0.8	93	96	89	93	0.4	0.3	0.8	0.5	10 *	10 ✱ ●	10	SW 12	SW 14	SW 18
13	58.7	61.5	63.8	61.3	0.3	1.2	-1.3	-0.3	2.7	-1.5	72	55	82	70	1.7	3.0	1.0	1.9	2	1	10	W 18	WNW10	WSW 5
14	68.8	72.3	81.3	74.1	-2.1	-0.8	-4.9	-3.2	0.2	-5.2	89	79	86	85	0.5	1.2	0.6	0.8	10	9	2	W 7	NW 2	NNW 4
15	88.7	93.0	95.3	92.3	-5.7	-2.1	-7.3	-5.1	-2.1	-7.5	85	72	82	80	0.7	1.4	0.6	0.9	8	8 ⦿	0	NNW 8	NW 12	W 2
16	75.2	62.1	58.3	65.2	-4.3	1.8	1.8	0.3	3.0	-8.3	86	100	74	87	0.6	0.0	1.8	0.8	10 *	10 ●	10	S 18	SW 18	WSW16
17	57.8	63.3	75.2	65.4	1.6	0.0	-2.0	-0.6	2.0	-2.6	78	86	66	77	1.6	0.9	1.8	1.4	10	10	6	W 16	NW 18	NW 16
18	85.9	92.5	97.3	91.9	-5.8	-2.1	-2.7	-2.8	-1.3	-4.0	64	66	69	66	1.6	1.7	1.3	1.6	5	7	10	NW 14	NNW12	W 4
19	94.1	93.0	95.8	93.6	-2.5	1.6	2.4	1.0	2.6	-2.9	89	96	93	93	0.6	0.3	0.6	0.5	10	10 ●	10	SSW 2	W 3	WNW 7
20	92.7	90.9	94.2	92.6	2.0	2.5	2.1	2.2	3.9	1.7	89	91	73	85	0.8	0.6	1.8	1.1	10	10	8	W 6	W 9	NW 7
21	100.7	104.7	110.0	105.1	-1.6	-0.9	-1.6	-1.4	2.2	-1.7	82	85	73	80	1.0	0.8	1.4	1.1	10	10 *	10 *	NNW 9	NNW10	N 10
22	114.0	114.6	116.3	115.0	-4.3	-2.4	-4.3	-3.8	-1.3	-4.6	79	63	82	73	0.9	1.8	0.8	1.2	10 *	10 *	10 *	NE 5	NE 5	NE 6
23	114.7	110.3	107.5	110.9	-5.8	-0.3	-1.9	-2.0	-0.1	-5.3	78	68	77	74	1.0	1.9	1.2	1.4	10	10	8	N 4	NNW 6	NNE 5
24	103.0	102.3	103.8	103.1	-2.6	-3.9	-6.4	-4.8	-1.7	-6.5	83	73	81	79	0.9	1.2	0.7	0.9	10	9	7	NE 5	NE 8	NE 4
25	104.7	106.4	106.4	105.8	-8.5	-3.9	-6.6	-6.9	-3.6	-8.8	83	66	80	76	0.5	1.3	0.7	0.8	10 *	9 *	8	ENE 5	E 7	ENE 7
26	104.3	103.3	103.3	103.8	-4.8	-2.3	-3.7	-3.7	-2.3	-6.7	88	78	80	82	0.3	1.1	0.9	0.8	10	10 *	10	ENE 7	NE 4	ENE 2
27	102.3	101.0	99.6	101.0	-4.6	-2.7	-3.8	-4.7	-1.8	-5.8	88	75	82	82	0.5	1.2	0.7	0.8	10	10	0	ENE 3	ENE 5	ENE 3
28	96.0	94.9	93.3	94.7	-6.6	-2.3	-6.3	-5.4	-1.6	-7.5	78	61	81	73	0.8	2.0	0.7	1.2	10	3	10	ENE 2	NE 3	NE 3
29																								
30																								
31																								
M	92.3	91.8	93.2	92.4	-2.9	-0.9	-2.0	-2.0	0.2	-4.3	86	82	84	84	0.7	1.0	0.8	0.8	9.0	8.7	7.7	7.1	7.1	6.1

Chojnice $H_s = 172m$ $H_b = 177{,}2m$ $h_w = 12{,}5m$ Styczeń - Janvier 1962

DNI	WIDZIALNOŚĆ	OPAD	GRUBOŚĆ LODU	POGODA
1	6	1.0	1	$\bullet^{\circ}0^{50}$-1^{40} $\mathfrak{g}^{\circ}11^{45}$...$13^{40}$ $\Delta^{\circ}20^{50}$-21^{05}; $\gg 7^{30}$-20^{15} $\nwarrow$-24
2	7	0.0	1	$\mathfrak{z}$; $\mathfrak{g}^{-1-5}6^{30}$-$9^{35}$ $\Delta^{\circ}11^{50}$-12^{08} $\mathfrak{g}^{\circ}$-13^{15}; $\nwarrow 0^{00}$-6^{20} $\gg$-7^{30}; $= 6^{15}$-9^{40}; $\sim^{\circ}6^{30}$-11^{50}
3	6	0.0	1	$\mathfrak{g}^{\circ}7^{50}$-$9^{45}$; $= 7^{10}$-13^{30}; $\sim^{\circ}7^{50}$-11^{50}
4	5	•	pł.	$= 9^{20}$-21^{30}
5	5	0.2	pł.	$\mathfrak{g}^{-1}7^{40}$-15^{50}; $= 5^{10}$-24; $\sim^{-1}7^{40}$-24; $\vee 21^{43}$-24
6	5	1.4	pł.	$\mathfrak{g}^{\circ}7^{40}$-$11^{20}$ $*^{\circ}$-18^{35}; $\gg 6^{30}$-10^{30}; $= 0^{00}$-24; $\sim^{-1}0^{00}$-11^{20}; $\vee^{\circ}0^{00}$-18^{35}
7	7	•	pł.	$\bullet^{\circ}2^{45}$-5^{10}; $= 1^{00}$-5^{15}
8	3	0.2	pł.	$\mathfrak{g}^{\circ}9^{05}$-$11^{25}$; 13^{30}-16^{35}; 21^{35}-24; $=$ na, $6^{15-50} \equiv^{\circ} 13^{45} =$-24
9	6	•	pł.	$\mathfrak{g}^{\circ}0^{00}$-$2^{40}$; $= 1^{00}$-$2^{45} \equiv^{\circ}$-$7^{20} =$-17^{30}
10	6	•	pł.	$= 7^{10}$-16^{20}
11	6	0.2	pł.	$\bullet^{\circ}14^{50}$-16^{55}; $\gg 12^{10}$-15^{20}, 16^{30}-24; $=$ a-p, p
12	7	5.3	pł.	$\gg 0^{00}$-2^{30}
13	7	0.0	3	$\mathfrak{g}^{*}1^{00}$-2^{15} $\mathfrak{g}^{\circ}$-3^{30} $*^{\circ}$-5^{00} $\bullet^{\circ}$-6^{40} $\mathfrak{g}^{\circ}11^{53-55}$; $\gg 13^{15}$-16^{40}, 20^{30}-22^{15}
14	7	0.3	pł.	$\Delta^{\circ}7^{55}$-8^{05} $\mathfrak{g}^{\circ}8^{30}$-$9^{10}$ $\bullet^{\circ}20^{05}$-21^{40}; 23^{45}-24
15	6	1.4	pł.	$\bullet^{\circ}0^{00}$...2^{10} $\mathfrak{g}^{\circ}10^{45}$-$11^{42}$ $\bullet^{\circ}12^{50}$-13^{40}; 14^{55}-16^{20}; $=$ na-a, p, np
16	6	0.3	•	$= 0^{00}$...14^{15}
17	6	0.7	2	$*^{\circ-1}2^{50}$-7^{40} $*^{\circ}$-9^{20} $\bullet^{\circ}$...10^{50}; $= 9^{20}$-24
18	6	0.1	pł.	$\bullet^{\circ}18^{50}$-19^{30}...20^{40}; $= 0^{00}$-24
19	3	2.0	pł.	$\bullet^{\circ}20^{40}$-24; $\gg 22^{30}$-24; $= 0^{00}$-$7^{40} \equiv^{\circ}$-$13^{50} =$-24
20	7	4.9	pł.	$\bullet^{\circ}0^{00-50}$ $\mathfrak{g}^{\circ-1}4^{50}$...$13^{10}$ $\bullet^{\circ}13^{15}$-17^{18}; $\gg 0^{00}$-16^{30}; $=$ na
21	7	3.7	•	$\bullet^{\circ}4^{40}$-6^{15} $\mathfrak{g}^{\circ}$-7^{25} $\bullet^{\circ}15^{50}$-20^{30}; $= 4^{50}$-$11^{40} =, \equiv^{\circ}14^{40}$-24
22	6	0.7	•	$\mathfrak{g}^{\circ}12^{55}$...$18^{50}$; $\gg 16^{20}$-24; $= 0^{00}$-10^{30}
23	7	1.9	•	$\mathfrak{g}^{\circ}15^{45}$...24 $\mathfrak{g}^{\circ}19^{20}$-$20^{10}$; $\gg 0^{00}$-7^{20}, 12^{30}-24
24	7	0.5	•	$\mathfrak{g}^{\circ}0^{00}$-$1^{15}$ $\mathfrak{g}^{\circ}7^{20-35}$ $\mathfrak{g}^{\circ}8^{45}$-$9^{02}$ $\mathfrak{g}^{\circ}9^{42}$-$10^{21}$; $\gg 0^{00-30}$; $=$ p, np
25	1	6.4	•	$*^{\circ}3^{52}$-4^{20} $\mathfrak{g}^{\circ}6^{30}$-$7^{15}$ $*^{\circ}$-8^{45} Δ° 9^{02} $\mathfrak{g}^{\circ-2}10^{25}$-$11^{45}$ $\bullet^{\circ-1}$-16^{40} $\bullet^{\circ}17^{10}$-18^{40} $*^{\circ}$-19^{20} $*^{\circ}$-20^{35}; $= 0^{00}$-$9^{10} \equiv^{\circ-2}$-$16^{45} =$-24
26	7	0.5	•	$\mathfrak{g}^{\circ}13^{50}$-$14^{05}$; $= 0^{00}$-2^{30} a
27	7	1.8	1	$\mathfrak{g}^{\circ}1^{00}$-$2^{00}$ $*^{\circ}$-6^{50} $\mathfrak{g}^{\circ}7^{10}$-$10^{15}$ $\mathfrak{g}^{\circ}13^{55}$-$14^{45}$ $*^{\circ}15^{05}$-16^{20} $\bullet^{\circ}$-18^{35} $\mathfrak{g}^{\circ}19^{40}$-$20^{12}$
28	5	2.2	•	$\mathfrak{g}^{\circ-1}7^{55}$-$11^{40}$; 12^{50}-17^{35} $\mathfrak{g}^{\circ}20^{40}$-24; $\gg 4^{40}$-16^{30}
29	7	0.7	5	$\mathfrak{g}^{\circ}0^{00-45}$; 1^{40}-4^{35} $\mathfrak{g}^{\circ-1}7^{50}$-$11^{40}$ $\mathfrak{g}^{\circ}15^{05-15}$, 18^{50}-20^{10}
30	7	•	6	$\vee^{\circ}20^{30}$-24
31	6	•	6	$= 7^{15}$-14^{40}, 16^{15}-19^{10}; $\vee^{\circ}0^{00}$-9^{50}
Σ	—	36.4	—	UWAGI

Luty - Février

1	7	0.0	6	$\mathfrak{g}^{\circ}14^{45}$-$16^{25}$; $= 7^{30}$-12^{30}, 17^{20}-18^{30}
2	5	0.2	5	$*^{\circ}9^{50}$-15^{35}; $= 6^{15}$-$22^{45} \equiv^{\circ}$-24
3	5	•	6	$\equiv^{\circ-1}0^{00}$-$12^{50} =$-18^{30}; $\vee^{\circ}8^{50}$-12^{30}
4	6	0.0	5	$*^{\circ}7^{35}$-9^{15}; $= 9^{15}$-14^{30}
5	6	7.2	4	$\mathfrak{g}^{\circ}11^{45}$-$12^{30}$ $*^{\circ}$-16^{10} $*^{\circ}17^{00}$ $\bullet^{\circ}$-18^{10} $\bullet^{\circ}21^{45}$ $\mathfrak{g}^{\circ-1}$-24; $\gg$ np; $= 4^{30}$-$6^{30} \equiv^{\circ}$-$9^{50} =$-24; $\vee^{\circ}6^{30}$-9^{50}
6	7	•	6	$*^{\circ}1^{00}$-6^{10}; $\gg 0^{00}$-14^{15}
7	1	0.0	5	$\mathfrak{g}^{\circ}7^{40}$-$11^{55}$; $= 4^{20}$-$10^{45} \equiv^{\circ-2}$-$20^{50} =$-24
8	3	0.4	3	$\mathfrak{g}^{\circ}6^{30}$-$9^{50}$; $= 0^{00}$-$12^{50} \equiv^{\circ-1}$-24
9	7	0.0	2	$\mathfrak{g}^{\circ}8^{35}$-$9^{10}$ 9^{20}-10^{05}; $\equiv^{-1}0^{00}$-$3^{50} =$-10^{15}, 23^{15}-24
10	6	0.5	pł.	$\mathfrak{g}^{\circ}12^{40}$-$13^{07}$ $\mathfrak{g}^{\circ}19^{40}$-$21^{45}$; $=, \equiv^{\circ}0^{00}$-$2^{30} =$-16^{30}-17^{40}; $\vee^{\circ}0^{45}$-9^{50}
11	5	1.7	pł.	$\bullet^{\circ}6^{05}$-9^{15} $*^{\circ}$-9^{35} $*^{\circ}12^{45}$-13^{02}; $\gg 18^{30}$-24; $= 8^{00}$-10^{30}
12	6	6.4	pł.	$\mathfrak{g}^{\circ-2}6^{35}$-$11^{45}$ $\mathfrak{g}^{\circ}$-13^{05} $\mathfrak{g}^{\circ-2}$-16^{10} $\mathfrak{g}^{\circ}$-17^{25}, 22^{45}-23^{15}; $\gg 0^{00}$-3^{30} $\gg$-$\nwarrow 5^{15}$-24; $\downarrow^{-1}8^{40}$-11^{40}
13	8	•	pł.	$\mathfrak{g}^{\circ}2^{45}$-$3^{05}$; $\nwarrow 0^{00}$-10^{20} $\gg$-13^{20}
14	7	0.8	pł.	$\mathfrak{g}^{\circ}14^{40}$-$16^{04}$
15	7	0.9	1	$\mathfrak{g}^{\circ-1}7^{50}$-$9^{45}$; 10^{15}-11^{05} $\mathfrak{g}^{\circ}13^{05-25}$; $\gg 9^{20}$-16^{30}
16	6	3.6	2	$\mathfrak{g}^{\circ-1}3^{45}$-$8^{20}$ $*^{\circ}$-11^{30} $\bullet^{\circ-2}15^{35}$ $\mathfrak{g}^{\circ}16^{40}$...24; $\gg$-$\nwarrow 3^{30}$-24; $\downarrow^{1}6^{30}$-11^{30}
17	7	0.0	3	$\mathfrak{g}^{\circ}0^{00}$-$1^{00}$ $\mathfrak{g}^{\circ-2}$ $*^{\circ-0}$-4^{15} $\mathfrak{g}^{\circ-1}9^{55}$ 20^{05}; $\nwarrow 0^{00}$-24
18	7	0.7	4	$\mathfrak{g}^{\circ}9^{55}$-$10^{10}$; $\nwarrow 0^{00}$-5^{20} $\gg$-17^{20}
19	5	1.5	7	$*^{\circ}1^{40}$-6^{35} 7^{25}-11^{20} $\mathfrak{g}^{\circ}12^{30}$-$18^{10}$; $= 8^{00}$-18^{30}
20	7	0.0	2	$\mathfrak{g}^{\circ}1^{00-20}$ $\mathfrak{g}^{\circ}3^{45}$-$6^{15}$ 11^{15}-12^{10}
21	6	0.2	pł.	$\mathfrak{g}^{\circ}4^{55}$...24; $\gg 9^{30}$-22^{30}
22	6	0.1	1	$\mathfrak{g}^{\circ}1^{00}$-$3^{30}$; 6^{15}-9^{20}; 12^{10}-17^{40}, 18^{20}-23^{40}
23	7	•	1	
24	7	0.1	pł.	$\mathfrak{g}^{\circ}7^{50}$-$12^{20}$ $\mathfrak{g}^{\circ}16^{40-55}$ $\mathfrak{g}^{\circ}17^{30}$-$19^{20}$ 23^{40}-24
25	6	0.9	1	$\mathfrak{g}^{\circ}0^{00}$-$1^{15}$ $*^{\circ}6^{45}$-7^{20} $\mathfrak{g}^{\circ}$-15^{10}, 23^{50}-24
26	6	0.1	5	$\mathfrak{g}^{\circ}0^{00}$-$6^{15}$ $*^{\circ}7^{40}$-15^{20}; $= 5^{00}$-18^{45}
27	7	0.0	4	$\Delta^{\circ}8^{55}$-9^{10}; $= 6^{30}$-11^{30}
28	7	•	3	
29				
30				
31				
Σ	—	25.3	—	UWAGI

Chojnice φ = 53°42' λ = 17°33' Marzec - Mars 1962

Dni	Ciśnienie P = 900 I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność względna U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie i pogoda N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	91.4	90.1	88.4	90.0	-6.7	-2.1	-7.3	-5.8	-1.6	-7.3	80	70	82	77	0.7	1.5	0.6	0.9	10	0 ⊙	0	NE 5	ENE 2	ENE 1
2	84.7	82.9	82.7	83.4	-7.8	-3.3	-3.6	-4.6	-2.8	-8.9	84	72	83	80	0.5	1.4	0.8	0.9	10	9	10 *	E 1	E 3	S 3
3	82.6	82.2	81.8	82.2	-3.6	-0.6	-0.6	-1.4	0.2	-3.8	83	81	85	83	0.8	1.1	0.9	0.9	10	10 *	10 *	S 2	S 3	S 2
4	77.9	76.1	76.2	76.7	-1.9	0.0	-2.1	-1.5	0.2	-2.2	98	88	89	92	0.1	0.7	0.5	0.4	10 ≡	10	8	C 0	C 0	NE 2
5	78.6	78.9	77.3	78.3	-1.1	-1.7	-3.1	-2.2	-1.0	-3.3	89	79	90	86	0.6	1.1	0.5	0.7	10	10	10 △	NE 3	NE 5	NE 7
6	74.6	81.3	91.3	82.4	-2.5	-1.7	-4.5	-3.3	-1.5	-5.0	91	88	84	88	0.5	0.7	0.7	0.6	10 *	10 *	2	E 6	NNW 8	NW 6
7	98.1	100.2	103.2	100.5	-6.8	-0.6	-1.8	-2.8	0.2	-7.2	85	70	90	82	0.5	1.8	0.3	0.9	9	5	9	WNW 1	NW 3	NW 1
8	104.2	104.2	105.1	104.5	-3.4	1.0	-3.0	-2.1	1.6	-5.5	90	64	88	81	0.5	2.4	0.6	1.2	10	1	2	NNW 2	NNW 8	NW 1
9	105.1	103.5	97.5	102.0	-6.5	0.0	-3.7	-3.5	0.2	-8.3	81	60	85	75	0.7	2.4	0.7	1.3	10	7 ⊙	0	ESE 1	SE 4	SE 8
10	91.8	89.6	87.2	89.5	-3.1	1.7	0.5	-0.1	2.2	-4.0	75	63	79	72	1.2	2.5	1.3	1.7	3 ⊙	10	10	SSE 6	SE 5	S 3
11	83.4	83.9	83.5	83.6	1.1	1.9	2.0	1.8	2.6	0.3	85	91	96	91	1.0	0.6	0.3	0.6	10	10 ●	10 ≡	SSW 2	SSW 3	C 0
12	80.5	77.9	76.4	78.3	0.3	-0.1	-2.6	-1.2	2.2	-2.6	98	100	89	96	0.1	0.0	0.6	0.2	10 ● ≡	10 *	10 *	NE 2	NE 1	N 7
13	80.3	84.1	88.8	84.4	-4.3	-3.6	-8.5	-6.2	-2.6	-8.9	84	76	83	81	0.7	1.1	0.5	0.8	10	9 *	0	NW 8	NNW 12	WNW 2
14	91.9	94.1	96.8	94.3	-10.4	-2.6	-8.5	-7.5	-2.5	-11.1	84	71	65	73	0.4	1.6	1.1	1.0	2 ⊙	7 ⊙	2	W 5	WNW 7	C 0
15	96.0	97.3	101.3	98.2	-9.1	-0.6	-5.1	-5.0	-0.4	-10.0	76	60	66	67	0.7	2.3	1.4	1.5	5 ⊙	9 ⊙	10	SE 3	SSE 5	SE 2
16	104.1	104.8	103.9	104.3	-9.9	-1.5	-5.1	-5.4	-1.0	-11.1	81	44	54	60	0.5	3.1	1.9	1.8	10	9	10	SE 1	NE 5	NNE 1
17	99.4	97.2	97.4	98.0	-5.9	0.0	-3.5	-2.7	0.2	-6.0	89	51	85	75	0.5	3.0	0.7	1.4	10	10	10	N 2	NNE 7	N 4
18	97.0	97.9	98.5	97.8	-7.0	0.3	-4.2	-3.8	1.1	-7.5	85	62	79	75	0.5	2.3	0.9	1.2	2 ⊙	8	4	NNW 1	NW 5	NNW 2
19	98.4	98.6	98.1	98.4	-6.0	-0.3	-5.7	-3.4	0.2	-8.6	87	66	80	78	0.5	2.0	0.9	1.1	8	5 ⊙	3	C 0	S 4	SW 1
20	97.5	97.1	97.0	97.2	-6.3	1.5	-2.2	-2.3	1.7	-7.4	86	61	79	75	0.5	2.6	1.1	1.4	5 ⊙	5	0	C 0	SE 5	SE 1
21	95.7	95.3	94.3	95.1	-3.1	1.7	-2.7	-1.7	1.7	-4.1	90	61	82	78	0.5	2.7	0.9	1.4	10	10 ⊙	8	SE 1	SSE 4	SE 2
22	92.2	91.0	89.9	91.0	-8.0	-0.4	-3.9	-4.0	1.4	-8.6	84	66	71	74	0.5	2.0	1.3	1.3	0 ⊙	0 ⊙	0	SE 1	SE 2	C 0
23	89.3	89.7	91.8	90.3	-10.0	0.4	-4.3	-4.6	1.1	-10.6	84	55	72	70	0.4	2.8	1.2	1.5	0 ⊙	2 ⊙	2	NE 1	NNE 4	NE 3
24	93.7	95.6	98.4	95.9	-8.8	0.3	-3.0	-3.6	0.5	-9.5	86	59	75	73	0.4	2.5	1.2	1.4	9 ⊙	2 ⊙	0	N 3	N 1	N 1
25	99.6	99.0	97.5	98.7	-5.5	1.0	-0.9	-1.6	2.2	-7.8	90	64	79	78	0.4	2.4	1.2	1.3	7 ⊙	6 ⊙	0	C 0	SW 2	C 0
26	95.5	94.2	91.5	93.7	-1.0	3.5	-0.5	0.4	3.7	-3.1	81	50	66	66	1.1	3.9	2.0	2.3	2 ⊙	4 ⊙	0	C 0	S 3	SE 3
27	87.7	85.0	82.8	85.2	-3.9	1.5	-1.5	-1.4	1.7	-4.3	73	67	72	71	1.2	2.3	1.6	1.7	8 ⊙	10	0	SE 4	SE 5	SE 6
28	78.9	79.7	82.5	80.4	-2.5	1.1	-0.3	-0.5	1.5	-2.6	91	81	98	90	0.5	1.2	0.2	0.6	10 *	10	10	SE 4	SE 3	W 1
29	84.8	84.2	80.3	83.1	-1.1	0.7	-0.5	-0.4	2.8	-1.1	93	79	78	83	0.4	1.3	1.3	1.0	10	9	0	W 3	W 1	E 4
30	73.1	73.0	71.1	72.4	0.8	3.4	6.2	4.2	8.1	-0.5	94	98	97	96	0.4	0.1	0.3	0.3	10 ●	10 ≡	10	E 3	SE 4	SE 3
31	63.5	66.2	73.8	67.8	5.1	5.5	1.8	3.6	8.3	1.8	97	94	87	93	0.3	0.5	0.9	0.6	10 ● ≡	10	10	SE 3	WNW 7	C 0
M	89.4	89.5	89.9	89.6	-4.4	0.2	-2.6	-2.4	1.0	-5.8	86	71	81	79	0.6	1.8	0.9	1.1	7.7	7.3	5.2	2.3	4.2	2.5

Kwiecień - Avril

1	79.5	82.6	83.0	81.7	0.3	3.9	1.8	2.0	5.0	-0.2	90	82	85	86	0.6	1.5	1.1	1.1	6	8 ⊼ ⊙	10	C 0	SW 5	SW 4
2	84.0	84.5	88.3	85.6	0.8	4.7	1.2	2.0	6.4	0.3	92	78	89	86	0.5	1.9	0.8	1.1	10	9 ●	0	SW 6	W 9	SW 4
3	86.3	84.0	80.9	83.7	3.2	10.1	6.8	6.7	12.3	0.8	93	64	71	76	0.5	4.6	2.9	2.7	10 ●	9	0	SW 5	SSW 10	S 5
4	76.8	76.3	73.6	75.6	4.3	11.3	7.0	7.4	12.2	3.6	82	67	85	78	1.5	4.4	1.4	2.4	10	10	10 ●	S 6	SW 4	S 7
5	68.1	66.3	67.5	67.3	4.9	6.4	3.5	4.6	8.1	3.5	94	97	93	95	0.6	0.3	0.5	0.5	10 ●	10 ●	0	E 1	NE 1	C 0
6	71.7	76.2	82.6	76.8	0.3	6.0	4.0	3.6	10.0	-0.3	98	97	93	96	0.1	0.3	0.5	0.3	10 ≡	8	8	SW 1	N 1	NNW 4
7	87.8	87.7	84.6	86.7	0.8	4.5	1.5	2.1	6.1	0.3	92	65	85	81	0.5	2.9	1.0	1.5	9	6	0	WNW 4	WNW 8	S 2
8	79.9	81.3	81.3	80.8	5.5	7.9	7.8	7.2	8.6	1.5	89	91	89	90	1.0	0.9	1.2	1.0	10	10 ●	10 ●	SW 5	SW 6	SW 5
9	85.0	87.8	92.4	88.4	4.0	9.5	4.1	5.4	9.7	3.0	83	60	90	78	1.3	4.8	0.8	2.3	4 ⊖	9	0	SW 8	SW 10	C 0
10	95.5	98.6	100.8	98.3	0.9	6.3	3.4	3.5	7.7	0.3	92	69	80	80	0.3	2.9	1.6	1.7	0 ⊖	9	0	SW 3	SW 4	SW 1
11	101.9	101.3	100.2	101.1	2.2	10.2	6.9	6.6	11.4	1.0	80	51	67	66	1.5	6.1	3.3	3.6	4 ⊖	5	5	S 1	SSW 3	SE 2
12	97.7	94.8	94.0	95.5	4.2	13.8	7.1	8.0	14.4	2.3	80	47	94	74	1.6	8.4	0.6	3.3	0	9 ⊖	10 ●	SW 3	SW 6	NW 2
13	93.4	93.7	93.3	93.3	3.3	6.6	4.6	4.8	7.4	2.2	93	71	90	85	0.5	2.8	0.8	1.4	10	10	10	NW 2	SW 4	C 0
14	95.6	99.2	103.7	99.3	1.6	4.1	2.7	2.8	4.7	0.8	89	88	86	88	0.8	1.0	1.0	0.9	10	10	10	N 3	NNW 3	NE 3
15	105.8	105.3	105.4	105.6	3.3	5.1	6.8	5.1	6.3	2.5	79	84	91	85	1.5	1.4	0.9	1.3	10	10	10	NNE 8	NE 8	NNE 8
16	104.8	102.1	100.0	102.3	5.3	12.3	11.8	10.3	15.7	5.2	93	67	76	79	0.4	4.7	3.3	2.8	10	10	0	ENE 6	NE 9	E 7
17	101.1	99.2	97.1	99.1	10.0	20.2	14.9	15.0	20.2	7.5	89	41	61	64	1.3	14.1	6.5	7.3	3	9	10	E 3	SE 8	SE 4
18	94.6	93.3	92.4	93.4	11.6	18.5	16.2	15.6	19.6	9.9	71	44	58	58	3.9	11.9	7.7	7.8	10	10	10	ESE 4	SSE 7	SE 2
19	92.5	93.3	94.7	93.5	11.2	20.3	17.4	16.6	22.6	10.6	75	55	65	65	3.3	10.8	7.0	7.0	10	10	10	SE 1	S 1	S 1
20	96.7	97.3	97.5	97.2	10.9	20.7	14.6	15.2	22.1	9.9	90	57	74	74	1.3	10.5	4.3	5.4	10	8	6	NW 2	NW 3	ENE 3
21	97.2	96.8	99.3	97.8	12.2	24.1	12.3	15.2	24.4	9.8	86	41	81	69	2.0	17.7	2.7	7.5	3	0 ⊖	0	E 2	SSE 3	NW 3
22	100.2	99.8	99.3	99.8	7.5	20.2	14.3	14.1	22.1	6.4	100	51	80	77	0.0	11.5	3.2	4.9	10 ≡	0 ⊖	0	NNE 2	E 2	E 1
23	99.1	99.3	101.8	100.1	13.2	25.5	13.0	16.2	26.0	11.2	88	31	61	60	1.8	22.4	5.9	10.0	0 ⊖	1 ⊖	5	C 0	SW 3	NNE 2
24	105.2	105.8	106.6	105.9	8.5	19.8	12.3	13.2	20.6	6.8	81	58	76	65	2.1	14.2	3.4	6.6	5 ⊖	0 ⊖	4	NE 3	NE 3	NE 1
25	107.3	106.5	104.2	106.0	11.2	22.5	17.4	17.1	23.4	9.6	77	46	60	61	3.1	14.6	8.1	8.6	4 ⊖	2 ⊖	0	ENE 3	SE 4	SE 3
26	100.5	97.4	93.1	97.0	12.6	18.4	9.7	12.6	19.1	9.4	86	62	73	74	2.1	8.2	3.2	4.3	4 ⊖	2 ⊖	2	NW 1	NW 3	NW 1
27	88.1	90.5	87.1	88.6	7.7	5.9	6.6	6.7	10.0	4.6	77	86	81	81	2.4	1.3	1.8	1.8	9	10	9	WNW 5	NW 8	WNW 6
28	80.8	82.6	85.8	83.1	6.0	6.1	4.2	5.1	8.0	2.8	85	79	87	84	1.5	2.0	1.0	1.5	9	9	10	NW 5	NW 3	NW 5
29	86.3	85.9	87.5	86.6	3.8	6.8	1.1	3.2	7.7	1.1	90	57	85	77	0.8	4.3	1.0	2.0	10	8	1	NW 5	NNW 3	C 0
30	89.2	91.3	93.7	91.4	0.6	4.4	-0.5	1.0	5.0	-0.7	73	52	75	67	1.8	4.0	1.5	2.4	10	9 ⊼	4	NNE 1	N 5	NW 2
31																								
M	91.8	92.0	92.4	92.1	5.7	11.9	7.8	8.3	13.2	4.2	84	64	79	76	1.4	6.3	2.6	3.5	7.3	7.3	5.1	3.3	3.0	3.0

Chojnice H_s=172m H_t=177,2m h_w=12,5m Marzec - Mars 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘBIENIE GU h	POGODA
1	7	•	5	
2	6	0.0	pz.	*$^{14^{05}}$-16^{10},17^{10}-18^{30};19^{10}...23^{30};=5^{50}-24
3	5	0.0	pz.	*°7^{30}-9^{50} ⚥°11^{40}-12^{10} ⚥$^{0-1}$$12^{30}$-$13^{15}$ *°18^{30}-24;=1^{00}-24
4	5	1.1	5	*°0^{00}-3^{15},8^{40}-9^{35};10^{50}-12^{05},=0^{00}-3^{30} ≡$^{0-2}$$12^{25}$=-$19^{10}$
5	6	5.8	5	*°8^{05}-9^{40},15^{45}-20^{40} △°-24;=6^{10}-24
6	6	3.7	6	●°1^{00}-4^{05} *$^{0-1}$$11^{20}$ △°12^{40} *°16^{35};=16^{35}-20^{30}
7	7	0.0	8	⚥°15^{50}-18^{10}
8	7	•	9	=2^{30}-11^{30},22^{30}-23^{40};V°22^{45}-24
9	7	•	9	V°0^{00}-8^{30}
10	7	0.0	7	●°21^{55}-23^{15}
11	6	0.5	5	●°8^{40}-10^{30} ⚲°11^{15} ●°12^{40}-13^{10};=6^{15}-15^{40} ≡$^{0-2}$-24
12	5	9.4	4	⚲°5^{45}-10^{30} △ 10^{55}-12^{15} *$^{0-1}$$12^{25}$-24;≡$^{2-0}$$0^{00}$-$11^{40}$=-24
13	7	1.6	12	*°0^{00-10},15-3^{20} *$^{0-1}$$7^{15}$-$10^{50}$ ⚥°12^{40-55},13^{45}-18^{10};⚲10^{20}-16^{30}
14	7	•	14	
15	7	•	14	
16	7	•	10	=5^{30}-6^{30}
17	7	•	10	=3^{30}-7^{15}
18	7	0.0	8	⚥°12^{25-30},13^{35-40}
19	7	0.0	7	⚥°9^{00-05};18^{00-05};=6^{30}-8^{30}
20	7	•	6	=1^{00}-9^{30}
21	7	•	3	=6^{15}-12^{30}
22	7	•	2	=3^{30}-9^{30}
23	7	•	1	=3^{45}-8^{10}
24	7	•	1	=3^{20}-7^{15};⊔°0^{00}-7^{00}
25	7	•	1	⊔'0^{00}-8^{00}
26	7	•	pz.	
27	7	1.4	pz.	⊕7^{30}-17^{00}
28	5	0.9	3	*$^{0-1}$$5^{15}$...$11^{20}$ ⚥°13^{05}-14^{30} ●°15^{10} *°17^{30}-18^{20} *°18^{45};=;≡°8^{30}-24
29	6	1.0	5	≡°1^{00}-3^{40}=-13^{20},17^{10}-19^{30}
30	1	1.3	pz.	●°3^{40}-6^{15} ⚲ $^{0-2}$$10^{40}$ ●°18^{45}-19^{25};=3^{30}-7^{35} ≡$^{0-2}$-14^{30}=-22^{30} ≡°-24
31	7	2.9	pz.	●$^{0-1}$$3^{05}$-$8^{25}$ ●°9^{07}-13^{10};≡$^{0-1}$$0^{00}$-$11^{20}$=-$13^{15}$
Σ	—	29.6	—	UWAGI.

Kwiecień - Avril

1	7	1.4	•	*°9^{00}-10^{25} ⚥°12^{05-20} ⚹°12^{45-55},13^{45-49} ⚥°14^{40}-15^{05} ⚥°-15^{20} ⚹°-15^{38} ⚥°15^{50}-16^{05} 17^{05-20} ⚹°-17^{35} ⚥°21^{40}-22^{15};=a
2	7	1.5	•	⚥$^{0-1}$$12^{40}$...$19^{50}$;=$6^{30}$-$8^{10}$
3	7	0.3	•	⚥°1^{15-35} ●°4^{05}-8^{50};⚲9^{20}-17^{30}
4	7	0.7	•	⚥°16^{50}-17^{17} ⚥°17^{35}-18^{07} ●°20^{40}-21^{50}
5	6	6.6	•	●$^{0-1}$$6^{45}$-$14^{30}$;=$4^{30}$-$15^{30}$;$23^{15-30}$ ≡°-24
6	5	2.6	•	⚥°16^{45}-18^{05};≡$^{2-1}$$0^{00}$-$11^{40}$=-$14^{30}$
7	7	1.7	•	⚹°11^{55}-12^{03} ●°23^{45}-24;=4^{20}-7^{30}
8	6	0.8	•	●°0^{00-50},1^{40}-3^{35},7^{05}...17^{10},19^{05}...21^{30}-24;=1^{30}-17^{30},20^{40}-24
9	7	1.9	•	●°0^{00-50} ⚥$^{1-0}$$15^{15-40}$;(R)°$15^{05-30}$ SW-NE;⚲12^{30}-13^{20}
10	7	•	•	=3^{15}-8^{40};⊔'3^{00}-8^{00}
11	7	•	•	⊔°3^{00}-8^{00}
12	7	2.1	•	⚥°18^{45}-19^{01},19^{15}-21^{30} ●°-24;⊔°3^{00}-7^{00}
13	7	0.0	•	⚥°0^{00-15},13^{40}-14^{05};=0^{15}-2^{40} ≡°4^{45}=-8^{30};⊕6^{30}-7^{15} ⊠17^{45}-22^{50}
14	7	0.5	•	●°8^{40}-12^{15}
15	7	•	•	
16	7	0.0	•	⚥°23^{55}-24;=5^{10}-10^{20};⊕10^{30}-16^{30}
17	7	•	•	
18	7	•	•	=19^{20}-20^{30}
19	7	•	•	
20	7	0.0	•	⚥°15^{45-50},16^{45-48};=3^{30}-8^{30};△°2^{00}-9^{00}
21	7	•	•	=3^{30}-9^{15};△'na-a;⊠1^{00}-3^{30}
22	7	•	•	=2^{15-40} ≡$^{0-2}$$8^{50}$=-$9^{10}$;△°nn-24
23	8	•	•	=3^{10}-7^{40};△'0^{00}-a △°n-24
24	7	•	•	△°0^{00}-8,23-24
25	7	•	•	△°0^{00}-9
26	7	0.0	•	⚥°9^{20-35};(R)°9^{25-45} NW-E;△°0^{00}-9,20-24
27	7	0.6	•	⚥°7^{52}-8^{15};△°0^{00}-7^{00}
28	7	5.6	•	⚥°9^{45}-10^{10} ⚥°...13^{55} ⚹°12^{15-20} ⚥°17^{35}-18^{05};△°0^{00}-7
29	7	0.2	•	⚥°7^{50}-8^{15},14^{20-40},15^{55}-16^{15}
30	6	0.0	•	⚹°12^{55}-13^{02};⊔°2-5
31				
Σ	—	26.5	—	UWAGI.

Chojnice φ=53°42' λ=17°33' Maj-Mai 1962

Dzień	Ciśnienie P=900+ I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność względna U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie i pogoda N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	89.9	87.1	85.4	87.5	0.1	6.0	0.8	1.9	6.5	-2.9	88	53	92	78	0.8	4.5	0.5	1.9	10 *	10	6	WNW 1	NW 4	N 1
2	85.2	84.8	87.0	85.0	0.8	4.3	1.3	1.9	5.2	-1.1	92	69	85	82	0.5	2.6	1.0	1.4	10	10 ●	2	NW 2	NW 4	NE 1
3	86.7	86.8	85.4	86.3	2.0	5.4	4.0	3.8	7.9	-0.8	84	72	90	82	1.2	2.5	0.8	1.5	6	10	10	SSW 3	SW 5	SW 2
4	85.4	84.5	87.3	85.1	4.4	8.6	3.0	4.8	9.2	2.6	95	66	86	82	0.6	3.8	1.1	1.8	10	8 ●	5	NNE 2	NNW 7	N 2
5	89.9	91.8	94.9	92.2	2.0	8.7	6.0	5.7	10.0	0.2	87	50	64	67	0.9	5.6	3.4	3.3	10	8	3	NNE 2	N 2	C 0
6	98.1	97.4	95.1	96.9	5.8	12.2	9.7	9.4	14.0	1.5	82	39	59	60	1.7	8.6	4.9	5.1	0 ⊘	6 ⊘	10	C 0	SE 4	SE 3
7	91.2	91.7	92.5	91.8	8.0	15.4	13.6	12.6	16.3	6.8	95	85	89	89	0.7	2.6	1.8	1.7	10 ●=	10	8	SE 2	WSW 1	C 0
8	91.2	91.2	90.1	90.8	12.5	16.3	13.5	14.0	17.6	10.8	96	68	82	82	0.5	6.0	2.8	3.1	10	7	10 ●	NW 2	NW 4	C 0
9	91.6	92.3	90.6	91.5	11.0	14.1	12.6	12.6	16.4	8.2	89	73	79	80	1.5	4.4	3.1	3.0	10	10	5	NW 3	W 4	NE 1
10	86.7	87.0	88.9	87.5	9.8	14.6	10.0	11.1	17.3	8.2	92	78	91	87	0.9	3.6	1.1	1.9	10 ●	9	7	SE 3	S 2	C 0
11	90.0	89.9	91.0	90.3	8.6	13.6	9.6	10.4	14.5	6.0	94	61	87	81	0.6	6.2	1.6	2.8	3 ⊙	8 ⊙	8 (R)	W 1	SW 3	NE 1
12	92.5	92.6	94.9	93.3	9.6	15.1	9.3	10.8	15.7	6.6	86	51	89	75	1.8	8.5	1.3	3.9	5 ⊙	6	2	SE 2	S 4	NE 1
13	94.6	94.5	92.7	93.9	8.3	13.5	9.6	10.2	13.6	7.0	97	74	91	87	0.4	4.0	1.2	1.9	10	10	9	C 0	SE 5	W 2
14	88.0	83.4	78.9	83.4	7.6	9.7	7.1	7.9	10.1	6.2	96	97	96	96	0.4	0.3	0.5	0.4	10	10 ●	10 ●	NNW 2	N 5	NW 8
15	79.2	81.5	85.0	81.9	6.6	7.4	7.0	7.0	9.7	6.1	87	88	91	89	1.3	1.2	0.9	1.1	10 ●	10 ●	0	NW 12	WNW 12	NW 4
16	87.2	90.8	91.9	90.0	8.2	9.0	5.2	6.9	10.0	5.1	82	75	87	81	2.0	2.9	1.1	2.0	8 ⊙	10	4	NW 7	W 12	W 2
17	89.6	88.9	87.9	88.8	6.8	12.1	7.7	8.6	13.5	3.2	86	79	89	85	1.5	3.0	1.2	1.9	10	10	10	SW 4	SW 3	NNW 2
18	91.4	93.9	96.4	93.9	6.6	13.3	7.8	8.9	13.4	6.3	93	57	86	79	0.7	6.6	1.5	2.9	10	9	3	W 3	W 8	SW 3
19	93.2	91.8	86.7	91.2	9.8	18.2	15.0	14.3	18.4	5.5	82	40	71	64	2.2	12.5	4.8	6.5	0 ⊙	9	9	S 3	S 6	SE 4
20	87.1	89.2	91.8	89.4	9.6	12.8	9.1	10.2	15.3	8.9	92	74	89	85	1.0	3.9	1.3	2.1	10 ●	10	6	NW 4	W 5	WNW 1
21	94.8	94.4	93.1	94.1	8.8	14.2	10.7	11.1	16.6	5.3	88	48	80	72	1.4	8.4	2.6	4.1	7 ⊙	6 ⊙	6	NW 1	W 2	SSW 1
22	90.4	89.6	91.6	90.5	10.6	15.3	10.3	11.6	15.6	6.8	77	54	94	75	2.9	8.0	0.8	3.9	2 ⊙	9	9	S 4	S 7	SW 3
23	93.0	92.1	93.1	92.7	10.8	15.8	9.2	11.2	16.9	8.3	89	57	95	80	1.5	7.6	0.6	3.2	10	10	10 ●	SSW 5	SSW 12	S 3
24	95.4	94.9	94.2	94.8	9.2	14.5	10.8	11.3	15.7	6.3	76	48	73	66	2.7	8.6	3.6	5.0	2 ⊙	9	10	SW 5	SSW 7	S 2
25	93.6	93.7	94.7	94.0	10.0	11.0	9.0	9.8	15.4	6.1	78	85	95	85	2.7	2.3	0.7	1.9	2 ⊙	9 ●	10	C 0	SE 3	N 2
26	93.3	92.2	90.3	92.0	8.0	10.8	8.7	9.0	12.4	6.3	92	91	97	93	0.9	1.2	0.3	0.8	10	10 ●	10 ●	NE 3	NE 3	N 1
27	92.3	94.2	96.1	94.2	10.1	12.5	10.0	10.6	13.4	8.6	92	73	84	83	1.0	3.9	1.9	2.3	10	10	9	S 4	SW 3	W 1
28	96.9	95.7	92.3	95.0	10.2	15.3	11.9	12.3	17.1	7.6	82	61	89	77	2.2	6.9	1.5	3.5	10	9	10 ●	W 2	SW 2	N 1
29	91.6	93.9	94.7	93.4	11.2	12.6	8.0	10.0	13.2	7.8	89	72	93	85	1.5	4.1	0.7	2.1	9	10	6	SW 5	SW 4	NW 1
30	94.8	93.6	93.9	94.8	9.6	13.0	7.6	10.0	13.2	5.4	88	64	86	79	1.5	6.0	1.4	3.0	0 ⊙	8	9	WSW 4	SW 6	WNW 2
31	93.6	90.4	88.7	90.9	8.7	10.6	6.7	8.2	11.3	5.7	84	79	87	83	1.8	2.8	1.3	2.0	2	10	1	SW 3	SSE 5	WNW 1
M	90.9	90.8	90.9	90.9	7.9	12.2	8.5	9.3	13.5	5.4	88	67	86	80	1.3	4.9	1.7	2.6	7.3	9.0	7.0	3.1	3.0	1.8

Czerwiec-Juin

1	90.5	94.0	95.0	93.2	5.0	11.5	7.8	8.0	12.9	3.7	90	62	78	77	0.8	5.2	2.4	2.8	10 ●	8	6	SW 7	NW 9	N 1
2	95.0	97.0	100.6	97.5	5.6	10.4	6.8	7.4	12.3	5.4	97	64	88	83	0.3	4.5	1.2	2.0	9	9	3	NE 1	WNW 5	C 0
3	102.8	103.6	104.7	103.7	5.2	11.1	5.6	6.9	12.5	2.4	97	59	92	83	0.2	5.4	0.7	2.1	5 ⊙	8	6	NW 3	NNE 3	N 1
4	106.0	104.9	105.6	105.5	4.8	14.2	9.0	9.2	15.2	2.2	84	49	63	65	1.4	8.2	4.2	4.6	10 ●	6 ⊙	6	N 4	N 8	NNW 6
5	105.3	105.5	107.4	106.1	8.4	13.1	6.6	8.7	13.9	5.9	62	32	64	53	4.1	10.2	3.5	5.9	7 ⊙	7 ⊙	3	NNW 8	N 10	N 7
6	108.2	108.7	109.0	108.6	7.8	13.5	8.3	9.5	13.8	3.8	55	31	54	47	4.8	10.7	5.0	6.8	5 ⊙	1 ⊙	2	NNE 8	NNE 8	NNE 6
7	109.9	109.3	109.0	109.5	9.5	17.2	10.6	12.0	18.2	4.4	69	27	57	51	3.7	14.3	5.5	7.8	7	1	0	N 2	NE 5	NE 1
8	108.6	106.4	101.9	105.6	10.3	19.3	12.6	13.7	20.9	4.8	60	41	65	55	5.0	13.3	5.2	7.8	0 ⊙	3 ⊙	4	NW 3	WSW 6	WNW 2
9	96.9	96.4	94.7	96.0	12.5	13.0	12.2	13.0	17.6	8.5	82	71	83	79	2.6	4.8	2.4	3.3	10	9	7	NW 4	W 6	C 0
10	93.5	91.3	89.5	91.4	12.3	19.2	14.8	15.3	20.6	6.6	69	44	70	61	4.5	12.5	5.0	7.3	3 ⊙	6	8	S 2	SW 4	W 3
11	87.0	84.8	86.8	86.2	11.8	16.3	9.2	11.6	17.1	8.6	90	60	77	76	1.3	7.4	2.6	3.8	10	5	10	SW 3	WSW 9	W 2
12	88.8	91.4	93.5	91.2	9.6	10.1	8.6	9.2	15.2	7.0	92	86	80	86	1.0	1.8	2.3	1.7	10	10 ●	0	W 6	NW 1	WNW 1
13	93.6	93.9	93.1	93.5	11.5	16.4	13.8	13.9	18.9	5.0	73	53	69	68	2.8	8.4	4.9	5.4	1 ⊙	6 ⊙	5	NW 4	SW 4	S 2
14	93.6	92.2	93.7	93.2	13.6	22.0	16.1	17.0	23.4	11.0	72	44	66	61	4.4	14.7	6.1	8.4	10	8 ⊙	10	SE 2	SSE 5	NW 2
15	97.5	98.1	99.0	98.2	15.1	24.7	19.0	19.4	26.3	10.1	78	47	75	67	3.9	16.6	5.6	8.7	9	4 ⊙	10	NW 1	SW 3	W 6
16	98.6	96.8	96.7	97.4	19.6	26.1	17.3	20.2	27.2	13.9	84	54	94	77	3.6	15.5	1.2	6.8	2 ⊙	6	10 o (R)	SE 1	SSE 2	NW 3
17	99.4	101.3	101.2	100.6	14.6	15.3	11.3	13.2	18.3	11.1	89	81	76	82	1.8	3.4	3.3	2.8	10	10	8	NW 6	NW 6	NW 2
18	100.7	99.7	97.6	99.3	12.5	20.0	16.2	16.2	21.9	7.4	80	49	61	63	2.9	12.0	7.2	7.4	0 ⊙	1 ⊙	4	NW 1	SSW 1	SSE 1
19	95.6	93.2	88.8	92.3	16.5	24.3	20.6	20.6	25.4	11.7	76	53	63	64	4.6	14.4	8.9	9.3	10	10 ⊙	10 (R)	SE 3	SSE 5	SE 3
20	94.0	93.1	93.4	94.8	14.3	19.9	15.6	16.4	21.1	13.3	90	54	77	74	1.6	10.6	4.1	5.4	9 ⊙	7 ⊙	10	W 4	SW 5	WSW 2
21	97.1	98.0	99.4	98.2	13.3	16.4	15.4	15.7	20.2	9.4	76	79	84	80	4.3	3.8	2.8	3.6	9	10	2	S 3	W 8	NW 3
22	101.4	100.7	99.4	100.3	15.8	21.7	19.3	19.1	23.2	10.5	79	65	76	73	3.7	9.2	3.5	6.1	5	8	10	SW 2	SW 5	SW 1
23	98.8	99.2	98.8	98.9	17.1	18.7	15.2	16.6	20.2	15.0	90	85	94	90	2.0	3.4	1.0	2.1	10 (R)	10	8	NW 3	NW 3	C 0
24	97.3	95.3	92.0	94.9	14.4	20.6	19.3	18.4	22.8	11.2	97	57	73	76	0.6	10.3	6.0	5.6	2 ⊙	9	10	W 1	SW 2	W 1
25	91.8	93.8	93.5	93.7	13.7	13.9	10.2	12.0	19.3	10.1	67	78	80	73	5.2	3.6	2.5	3.8	1 ⊙	9	2	SW 10	SW 10	W 3
26	94.6	93.7	90.8	93.0	10.0	14.7	11.6	12.0	16.0	5.7	79	61	78	73	2.5	6.5	2.9	4.0	4 ⊙	8	4	W 6	W 4	SW 1
27	86.9	87.4	88.2	87.5	10.2	10.1	9.6	9.9	13.4	8.8	93	88	92	91	0.8	1.3	1.0	1.1	10	10 ●	6	SW 4	SW 7	W 3
28	87.6	86.1	83.4	85.7	8.8	8.3	8.6	8.6	9.6	7.9	84	93	93	90	1.8	0.8	0.8	1.1	9	10 ●	10	SW 7	SW 8	SW 3
29	84.0	83.4	87.1	83.3	10.7	12.3	11.4	11.3	13.7	7.3	90	81	94	88	1.3	2.7	0.9	1.6	9	10 ●	10 ●	W 5	WNW 7	W 7
30	89.1	90.9	93.6	91.2	11.9	15.4	12.0	12.8	16.9	10.6	94	71	79	81	0.8	3.1	3.0	3.0	10	8	6	NW 3	NW 7	WNW 3
31																								
M	96.5	96.5	96.4	96.5	11.6	16.4	12.5	13.2	18.3	8.2	81	61	76	73	2.6	8.0	3.6	4.7	6.9	7.2	6.3	3.9	3.5	2.7

Chojnice $H_s = 172m$ $H_k = 177{,}2m$ $h_w = 12{,}5m$ Maj - Mai 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	0.0	•	$\overset{*}{\bullet}{}^{\circ}6^{35-50}\overset{\bullet}{\bullet}{}^{\circ}14^{57-15^{02}}\overset{\bullet}{\bullet}{}^{\circ}15^{15}\overset{\bullet}{\bullet}{}^{\circ}16^{03-18}\overset{\bullet}{\bullet}{}^{\circ}18^{50-19^{04}};\sqcup{}^{\circ}3\text{-}5$
2	7	0.0	•	$\overset{\bullet}{\bullet}{}^{\circ}12^{50-13^{05}}, 23^{55-24}; = 2^{10-4^{55}} \equiv {}^{\circ}5^{45} = -6^{05}; \sqcup^{1-2} na$
3	7	1.2	•	$\overset{\bullet}{\bullet}{}^{\circ}0^{00}\ldots 1^{15}, 10^{15}\ldots 16^{30} \blacktriangle {}^{\circ}16^{30-32}; \sqcup^{\circ} na$
4	7	0.1	•	$\overset{\bullet}{\bullet}{}^{\circ}3^{40}\text{-}5^{20}; 8^{40-50}; 12^{38}\text{-}13^{10}; = 4^{30}\text{-}7^{30}$
5	7	•	•	$= 19^{20}\text{-}24$
6	7	2.3	•	$= 0^{00}\text{-}7^{30}; \triangle^{2-1} na\text{-}a$
7	6	5.9	•	$\bullet{}^{\circ}2^{35}\text{-}7^{55}\overset{\circ}{\bullet}{}^{-15}\overset{\bullet}{\bullet}{}^{1-0}12^{55}\text{-}13^{10}\overset{\bullet}{\bullet}{}^{\circ}22^{46}\text{-}23^{35}; =, \equiv {}^{\circ}3^{30}\text{-}13^{02} = n\text{-}24$
8	7	0.9	•	$\bullet{}^{\circ}1^{20}\text{-}2^{40}, 20^{35}\text{-}22^{15}, 23^{20}\text{-}24; = 0^{00}\text{-}8^{30}$
9	7	0.2	•	$\bullet{}^{\circ}0^{00}\text{-}2^{10}$
10	7	7.9	•	$\overset{\bullet}{\bullet}{}^{\circ}6^{40}\text{-}8^{10}\bullet{}^{0-1}\text{-}11^{07}\overset{\bullet}{\bullet}{}^{\circ}15^{25-42}\overset{\bullet}{\bullet}{}^{1-0}19^{12}\text{-}20^{15}; \mathrm{R}^{\circ}19^{50}\text{-}20^{20}\,NW\text{-}E; = 1^{00}\text{-}11^{30}$
11	7	0.3	•	$\overset{\bullet}{\bullet}{}^{\circ}14^{36}\text{-}15^{20}; (\mathrm{R})^{\circ}14^{15}\text{-}15^{30}\,SW\text{-}E, 19^{45}\text{-}21^{40}\,SW\text{-}E; = 3^{40}\text{-}5^{50}$
12	7	4.1	•	$\overset{\bullet}{\bullet}{}^{\circ}15^{35}\text{-}16^{15}\overset{\bullet}{\bullet}{}^{0-1}18^{50}\text{-}19^{45}; \mathrm{R}^{\circ}10^{50}\text{-}11^{25}\,SW\text{-}S, 15^{40}\text{-}16^{10}\,SW\text{-}NE, 17^{45}\text{-}20^{10}; = na, nn \equiv {}^{\circ}nn; \triangle^{2-1} na\text{-}a$
13	7	1.6	•	$\overset{\bullet}{\bullet}{}^{1-0}2^{45}\text{-}4^{10}\bullet{}^{0}\text{-}5^{40}\overset{\bullet}{\bullet}{}^{\circ}7^{40}\text{-}8^{10}, 8^{30}\text{-}11^{40}, 13^{35}\text{-}15^{15}; \equiv {}^{0-1}0^{00}\text{-}2^{40} = -11^{50}$
14	6	18.8	•	$\bullet{}^{0-1}8^{52}\text{-}23^{40}; \gg 22^{15}\text{-}24; = 2^{30}\text{-}15^{00}; \triangle{}^{0}3\text{-}8$
15	6	0.1	•	$\bullet{}^{0-1}0^{20}\text{-}7^{40}\bullet{}^{0}8^{15}\text{-}10^{35}, 11^{45}\text{-}13^{10}; \gg 0^{00}\ldots 18^{20}$
16	7	0.0	•	$\gg 10^{30}\text{-}15^{30}; = 3^{30}\text{-}5^{40}$
17	6	6.3	•	$\bullet{}^{\circ}4^{55}\text{-}5^{04}\overset{\bullet}{\bullet}{}^{\circ}6^{55}\ldots 8^{05}\overset{\bullet}{\bullet}{}^{0-1}15^{45}\text{-}16^{25}\bullet{}^{2}\text{-}16^{30}\overset{\bullet}{\bullet}{}^{1-2}18^{20}\overset{\bullet}{\bullet}{}^{\circ}18^{45}\text{-}19^{10}; \mathrm{R}^{15}16^{05-35}\,SW\text{-}NE;$
18	7	0.8	•	$\overset{\bullet}{\bullet}{}^{0}11^{05-10}, 11^{35-42}, 13^{45-48}; = 0^{00}\text{-}8^{30}$
19	7	3.2	•	$= 1^{00}\text{-}6^{30}; \triangle^{2-0} na\text{-}9$
20	7	1.3	•	$\bullet{}^{\circ}3^{35}\text{-}5^{20}\overset{\bullet}{\bullet}{}^{0-1}6^{18}\text{-}7^{20}\overset{\bullet}{\bullet}{}^{\circ}7^{30}\text{-}9^{15}; = 9^{15}\text{-}10^{30}; \triangle{}^{\circ}20\text{-}24$
21	7	•	•	$= 3^{30}\text{-}6^{15}; \triangle^{0-1} 0^{00}\text{-}9$
22	7	0.2	•	$\overset{\bullet}{\bullet}{}^{\circ}21^{35}\text{-}23^{10}; = 1^{00}\text{-}7^{30}; 17^{10}\text{-}23^{30}; \triangle^{0-1} 0^{00}\text{-}8$
23	7	1.4	•	$\overset{\bullet}{\bullet}{}^{\circ}14^{43-47}; 16^{45}\text{-}17^{02}, 18^{55}\text{-}21^{15}, 22^{40}\text{-}23^{30}; \gg 10^{30}\,15^{20}; = na\text{-}a, n\text{-}24; \triangle^{0-1} na\text{-}a$
24	7	•	•	$= 1^{00}\text{-}7^{15}; \triangle{}^{\circ}22\text{-}24$
25	6	9.5	•	$\overset{\bullet}{\bullet}{}^{\circ}11^{20}\ldots 13^{05}, 14^{57}\text{-}18^{00}; = 19^{30}\text{-}24; \triangle^{1-0} 0^{00}\text{-}9$
26	6	9.1	•	$\overset{\bullet}{\bullet}{}^{\circ}9^{20-30}, 10^{40}\ldots 16^{30}\bullet{}^{\circ}\text{-}23^{15}\bullet{}^{2}\text{-}24; = 0^{00}\text{-}13^{40}, 15^{30}\text{-}24$
27	7	•	•	$\overset{\bullet}{\bullet}{}^{2-1} 0^{00}\text{-}3^{40}; = 0^{00}\text{-}7^{20}$
28	7	11.6	•	$\overset{\bullet}{\bullet}{}^{0-1} 20^{50}\text{-}23^{35}$
29	7	0.2	•	$\overset{\bullet}{\bullet}{}^{\circ}5^{45}\text{-}6^{20}, 18^{35}\text{-}19^{10}; = 4^{30}\text{-}8^{30}$
30	7	0.1	•	$\overset{\bullet}{\bullet}{}^{1}12^{52}\text{-}13^{03}\overset{\bullet}{\bullet}{}^{1-0}14^{10-57}; = 3^{10}\text{-}7^{15}; \triangle^{0-1} na\text{-}a$
31	7	2.3	•	$\overset{\bullet}{\bullet}{}^{\circ}12^{40}\text{-}13^{45}, 14^{42}\text{-}16^{10}, 19^{30-45}; \mathrm{R}^{\circ}15^{55}\text{-}16^{25}\,SE\text{-}NE; \triangle^{1-2} na\text{-}10$
Σ	—	89.4	—	UWAGI.

Czerwiec - Juin

1	7	3.7	•	$\overset{\bullet}{\bullet}{}^{\circ}7^{20}\text{-}8^{15}; \gg 12^{30}\text{-}13^{45}$
2	7	0.7	•	$\overset{\bullet}{\bullet}{}^{\circ}4^{55}\text{-}7^{20}\overset{\bullet}{\bullet}{}^{1}10^{10-25}\overset{\bullet}{\bullet}{}^{\circ}19^{35}\text{-}20^{07}; \triangle{}^{1} nn$
3	7	1.3	•	$\overset{\bullet}{\bullet}{}^{0-1}18^{20}\text{-}19^{12}, 19^{50}\text{-}20^{05}; \mathrm{R}^{\circ}17^{30}\text{-}18^{15}\,NE\text{-}N; = 4^{45}\text{-}5^{50} \equiv {}^{2-0}\text{-}7^{30} = -8^{20}; \triangle{}^{1} 0^{00}\text{-}8^{00}; \frown 18^{15}\text{-}19^{15}$
4	7	1.3	•	$\overset{\bullet}{\bullet}{}^{\circ}7^{40}\text{-}9^{20}$
5	8	•	•	$\gg 9^{20}\text{-}11^{30}, 13^{10}\text{-}14^{40}; \triangle{}^{\circ}0^{00}\text{-}8^{00}$
6	8	•	•	$\gg 16^{10}\text{-}17^{40}$
7	7	•	•	
8	8	•	•	$\triangle^{0-1} 2\text{-}8\ \triangle{}^{\circ}21\text{-}24$
9	7	•	•	$\triangle{}^{\circ}0\text{-}8, 21\text{-}24$
10	7	0.3	•	$\triangle^{0-1} 0^{00}\text{-}10$
11	7	0.1	•	$\overset{\bullet}{\bullet}{}^{\circ}6^{45-50}\overset{\bullet}{\bullet}{}^{0-2}10^{53}\ldots 12^{04}\overset{\bullet}{\bullet}{}^{1}16^{03\ldots 25}; \mathrm{R}^{\circ}6^{50}\text{-}7^{30}\,E\text{-}W, 11^{20}\text{-}12^{10}\,N\text{-}NE; \gg n$
12	6	7.7	•	$\overset{\bullet}{\bullet}{}^{\circ}5^{50}\text{-}6^{40}, 12^{35}\ldots 16^{12}, 18^{30-37}$
13	7	•	•	$\triangle^{0-1} na\text{-}9$
14	7	•	•	$\triangle^{0-1} na\text{-}10$
15	7	0.0	•	$\overset{\bullet}{\bullet}{}^{\circ}22^{50}\text{-}23^{20}; = 3^{30}\text{-}10^{30}; \triangle^{0-1} 0^{00}\text{-}8$
16	7	14.9	•	$\overset{\bullet}{\bullet}{}^{\circ}17^{15}\text{-}18^{05}\overset{\bullet}{\bullet}{}^{0-1}19^{15}\text{-}23^{15}; \mathrm{R}^{\circ}16^{10}\text{-}18^{15}\,SW\text{-}E, 19^{05}\text{-}22^{45}\,SW\text{-}E; = 4^{20}\text{-}8^{30}$
17	6	•	•	$= 9^{20}\text{-}15^{40}$
18	7	•	•	$\triangle^{0-1} 0^{00}\text{-}9$
19	7	3.4	•	$\overset{\bullet}{\bullet}{}^{1}22^{35-45}\overset{\bullet}{\bullet}{}^{2-0}23^{04-35}; \mathrm{R}^{\circ}21^{30}\text{-}23^{45}\,SW; \triangle^{0-1} 2\text{-}9$
20	7	•	•	$\overset{\bullet}{\bullet}{}^{\circ}3^{15}\text{-}4^{20}; \triangle^{0-2} nn$
21	7	•	•	$\triangle^{2-0} na\text{-}a$
22	7	•	•	$\triangle^{2-0} na\text{-}a$
23	7	1.5	•	$\overset{\bullet}{\bullet}{}^{\circ}9^{10}\text{-}10^{35}\overset{\bullet}{\bullet}{}^{0-1}17^{10}\text{-}19^{35}; \mathrm{R}^{\circ}7^{45}\text{-}8^{10}\,NW\text{-}E; = na\text{-}a, nn \equiv {}^{\circ}23^{50}\text{-}24$
24	7	•	•	$\equiv {}^{0-1}0^{00}\text{-}6^{45} = -7^{20}; \triangle{}^{\circ} nn$
25	7	0.3	•	$\overset{\bullet}{\bullet}{}^{\circ}14^{15-40}, 16^{41-45}\,20^{02-07}; \gg 7^{15}\text{-}16^{30}; \triangle{}^{\circ}0^{00}\text{-}9$
26	7	7.2	•	
27	7	5.6	•	$\overset{\bullet}{\bullet}{}^{\circ}3^{06}\text{-}4^{30}\bullet{}^{\circ}6^{15}\overset{\bullet}{\bullet}{}^{0-1}11^{51}\ldots 17^{15}\bullet{}^{\circ}\text{-}20^{25}; = 3^{00}\text{-}7^{30}$
28	6	3.5	•	$\overset{\bullet}{\bullet}{}^{\circ}4^{10-25}, 10^{55}\ldots 15^{15}\bullet{}^{\circ}\text{-}16^{30}\bullet{}^{\circ}\text{-}18^{20}, 19^{25-50}\overset{\bullet}{\bullet}{}^{\circ}23^{45}\text{-}24; = 16^{30}\text{-}20^{40}$
29	7	8.8	•	$\overset{\bullet}{\bullet}{}^{0-2}0^{00}\ldots 22^{10}$
30	7	0.0	•	$\overset{\bullet}{\bullet}{}^{\circ}0^{40}\text{-}1^{30}, 2^{40}\text{-}4^{15}\bullet{}^{\circ}4^{15}\text{-}5^{45}\overset{\bullet}{\bullet}{}^{\circ}7^{30-45}, 10^{35-50}; = 7^{30}\text{-}8^{30}; \triangle^{\circ} nn$
31		•		
Σ	—	60.3	—	UWAGI.

Chojnice φ = 53°42' λ = 17°33' Lipiec - Juillet 1962

Dzień	Ciśnienie P = 900 + I	II	III	Dzień	Temperatura T I	II	III	Dzień	Max	Min	Wilgotność względna U I	II	III	Dzień	Niedosyt wilgotności Δ I	II	III	Dzień	Zachmurzenie N w I	II	III	Kierunek i prędkość wiatru D v I	II	III
1	95.7	94.0	95.0	95.6	10.9	12.5	10.2	10.9	14.1	7.7	80	74	91	82	2.6	3.7	1.1	2.5	2 ⊙	10	8	WNW 4	WSW 5	SW 2
2	91.1	90.4	85.5	89.0	11.8	11.8	11.6	11.7	13.7	6.9	95	78	85	85	1.0	3.0	2.3	2.1	10	10	10 ●	W 3	SW 4	SW 5
3	79.4	78.0	77.2	78.2	9.4	12.4	8.2	9.6	13.8	8.1	95	78	92	88	0.8	3.2	0.9	1.6	10 ●	9	8	SW 3	SW 8	NW 1
4	74.7	74.1	77.8	75.5	7.5	8.6	8.9	8.5	10.9	6.6	94	96	94	95	0.6	0.5	0.6	0.6	10 ●	10 ●	5	SE 5	S 5	SW 5
5	81.5	83.2	86.5	85.7	9.3	14.8	10.4	11.2	16.0	5.9	91	66	97	85	1.1	5.7	0.3	2.4	10	7	10 ●	SW 5	SW 9	WSW 1
6	89.0	90.8	92.4	90.7	11.0	14.9	10.4	11.7	16.6	8.1	91	67	85	81	1.1	5.5	1.9	2.8	9	9	6	SW 6	WSW 6	WSW 1
7	92.3	92.5	94.3	93.0	11.7	14.3	10.5	11.8	15.5	7.7	84	76	90	83	2.1	3.9	1.3	2.4	9	9	10	SW 5	SW 5	W 1
8	95.6	97.0	98.7	97.1	11.1	14.9	12.5	12.6	16.3	8.1	91	68	89	83	1.1	5.3	1.5	2.6	9	9	9	SW 2	NW 1	NNW 1
9	100.1	99.7	97.9	99.2	9.5	17.0	13.2	13.2	19.4	8.5	97	65	86	83	0.3	6.9	2.1	3.1	10	7 ⊙	0	NW 2	NW 2	W 1
10	95.6	94.3	92.6	94.2	13.1	20.5	14.4	15.6	21.6	7.3	88	52	79	73	1.8	11.6	3.4	5.6	0 ⊙	5 ⊙	0	WNW 3	NW 5	NW 3
11	91.1	88.8	87.6	89.2	15.2	22.3	16.6	17.7	23.2	10.4	88	54	86	76	2.1	12.3	2.7	5.7	0 ⊙	9	10	NW 1	WNW 3	C 0
12	86.3	85.9	85.5	85.9	14.7	20.3	13.3	15.4	21.1	12.7	89	57	95	80	1.8	10.2	0.7	4.2	10	9	4	NW 2	WSW 10	SW 1
13	83.8	84.0	86.1	84.6	13.4	16.1	13.4	14.1	17.2	12.2	91	76	96	88	1.4	4.4	0.6	2.1	10	9	10	WSW 3	W 7	N 1
14	86.2	85.4	86.3	86.0	12.4	18.8	12.9	14.2	19.3	10.8	94	67	95	85	0.9	7.1	0.7	2.9	10	7 ⊙	6	WNW 3	W 2	W 1
15	86.0	86.1	86.8	86.3	12.2	17.8	15.0	15.0	19.6	9.9	98	74	91	88	0.3	5.4	1.5	2.4	2 ⊙	8	3	N 1	NW 1	C 0
16	88.1	89.0	91.0	89.4	13.1	19.3	13.7	15.0	21.7	10.4	95	62	82	80	0.7	8.6	2.9	4.1	8	6 ⊙	0	NE 2	NE 3	NE 2
17	93.9	94.4	96.1	94.8	14.1	21.6	14.6	16.2	21.7	7.9	85	50	76	70	2.4	12.9	4.0	6.4	0 ⊙	6	1	NE 1	NE 1	E 1
18	97.1	96.2	96.6	96.6	13.7	21.5	14.9	16.2	22.3	7.8	86	52	81	73	2.2	12.2	3.3	5.9	0	8 ⊙	2	NE 1	NNE 3	NE 1
19	97.2	97.0	97.2	97.1	13.8	22.1	16.2	17.1	24.0	9.1	85	53	81	73	2.3	12.5	3.4	6.1	4 ⊙	5 ⊙	1	NW 3	NW 4	E 1
20	96.7	95.5	95.8	96.0	16.3	23.6	17.4	18.7	23.7	11.2	76	53	89	73	4.3	13.8	2.3	6.8	9 ⊙	8 ⊙	10	SSE 2	SW 5	C 0
21	96.0	93.0	90.8	93.3	17.3	25.0	21.8	21.5	26.3	12.0	90	55	71	72	2.0	14.3	7.7	8.0	0 ⊙	7 ⊙	10	SSW 1	S 3	SSE 1
22	94.2	93.6	95.8	94.5	19.1	23.1	15.8	18.4	23.7	15.7	88	69	91	83	2.8	8.6	1.5	4.3	10	6	5	WNW 1	SE 5	NNW 1
23	98.0	98.4	99.5	98.6	15.8	21.3	13.0	15.8	21.6	11.6	93	47	88	76	1.3	13.5	1.8	5.5	6 ⊙	7	1	W 1	WSW 6	W 1
24	100.9	101.5	102.1	101.5	12.9	15.5	9.7	12.0	17.1	9.5	80	67	89	79	2.9	5.8	1.2	3.3	3 ⊙	9	0	W 4	W 5	C 0
25	103.1	102.2	99.8	101.7	12.9	17.6	15.1	15.2	19.9	6.3	88	58	83	76	1.8	8.4	3.0	4.4	0 ⊙	8 ⊙	8	W 1	WNW 5	SE 1
26	96.9	95.1	93.3	95.1	16.2	26.5	16.2	18.8	26.7	11.4	76	55	97	76	4.4	15.7	0.6	6.9	2 ⊙	8	10 ●	ESE 1	SE 2	NE 2
27	92.4	92.0	92.1	92.2	17.1	21.0	12.0	15.5	21.7	11.9	96	70	93	86	0.8	7.5	1.0	3.1	10	8	10 ●	W 1	WSW 7	NW 8
28	96.4	97.4	99.1	97.6	13.2	16.8	10.2	12.6	18.4	10.2	87	75	82	81	2.0	4.8	2.2	3.0	9	9 ●	0	NW 5	W 1	C 0
29	99.6	99.8	99.9	99.8	11.6	13.6	12.4	12.5	19.2	7.4	98	86	81	88	0.3	2.2	2.7	1.7	4 ⊙	10 ●	2	WSW 2	NW 3	C 0
30	100.9	100.2	99.9	100.3	13.2	19.0	13.0	14.6	20.2	7.1	93	52	83	76	1.1	10.5	2.6	4.7	6 ⊙	7	1	C 0	WSW 1	E 1
31	99.7	99.2	96.8	98.6	13.8	20.1	15.2	16.1	21.1	11.7	84	56	82	74	2.5	10.3	3.2	5.3	6	8 ⊙	6	S 1	S 3	SW 1
M	92.8	92.5	92.7	92.7	13.1	18.2	13.3	14.5	19.6	9.4	89	65	87	80	1.7	8.1	2.1	4.0	6.1	8.0	5.4	2.4	4.2	1.4

Sierpień - Août

1	95.3	94.9	94.8	95.0	14.4	17.6	12.2	14.1	19.4	12.0	90	69	94	84	1.6	6.2	0.9	2.9	6 ⊙	8	2	WNW 4	W 8	W 2
2	94.4	94.3	94.0	94.2	13.6	17.7	14.3	15.0	19.2	11.5	89	63	87	80	1.8	7.4	2.2	3.8	9	9	9	W 5	WNW 4	C 0
3	94.1	94.3	94.5	94.3	15.4	20.1	16.2	17.0	21.6	12.6	84	67	81	77	2.8	7.8	3.4	4.7	4 ⊙	9	10	C 0	WNW 1	C 0
4	93.7	92.4	93.9	93.3	14.8	21.6	17.2	17.7	23.4	11.7	80	73	93	82	3.3	7.0	1.4	3.9	9	10	9	E 2	S 1	NW 3
5	93.7	90.2	88.1	90.7	15.2	18.4	13.6	15.2	20.4	12.0	99	89	95	94	0.2	2.3	0.7	1.1	8	10	7	NW 1	SE 1	C 0
6	89.9	90.7	90.1	90.2	13.8	19.2	16.0	16.2	20.1	13.4	97	64	80	80	0.6	7.9	3.6	4.0	9	8	6	W 1	SW 3	C 0
7	86.7	82.5	82.8	91.0	14.5	18.9	16.3	16.5	19.3	11.2	90	95	91	92	1.6	1.0	1.7	1.4	10	10 ●	9	E 1	E 3	WSW 8
8	87.7	91.1	94.9	91.2	13.1	17.0	11.0	13.0	18.6	10.9	78	54	84	72	3.3	9.0	2.1	4.8	0 ⊙	7 ⊙	0	SW 9	SSW 8	WSW 2
9	100.3	101.6	102.2	101.4	10.0	15.2	11.6	12.1	17.0	7.5	93	64	84	80	0.8	6.2	2.1	3.0	8 ⊙	9	2	WSW 5	W 5	C 0
10	100.5	96.8	95.2	96.8	12.0	19.4	15.0	15.4	20.4	7.6	83	57	85	75	2.3	9.7	2.5	4.8	4 ⊙	9	10	S 2	S 5	SW 1
11	92.8	92.9	93.7	93.1	13.1	19.3	15.6	15.9	20.6	12.0	85	61	84	77	2.3	8.8	2.8	4.6	10	8	8	WSW 5	SW 6	C 0
12	95.3	95.2	95.3	95.3	16.4	25.3	19.6	20.2	26.1	11.6	87	56	79	74	2.5	14.1	4.7	7.1	0 ⊙	4 ⊙	3	SW 3	SW 6	N 3
13	97.8	98.0	99.4	98.4	15.6	21.4	13.2	15.8	22.9	12.6	94	70	67	77	1.1	7.8	5.0	4.6	1 ⊙	9 ⊙	3	NW 1	NW 3	N 1
14	99.8	99.0	97.6	98.8	11.0	18.6	11.6	13.2	20.1	7.5	91	49	78	73	1.1	10.9	2.9	5.0	2 ⊙	5 ⊙	4	NW 1	NW 1	N 1
15	94.3	89.6	86.7	90.3	11.3	14.3	15.0	13.9	16.6	9.0	90	92	97	93	1.3	1.3	0.3	1.0	10	10	10	E 3	NE 3	SE 1
16	87.5	89.1	91.0	89.2	15.9	20.1	16.1	17.0	23.1	12.6	98	73	89	87	0.4	6.0	1.9	2.8	10	7 ⊙	9	W 2	WSW 4	SW 1
17	92.4	92.3	89.9	91.5	15.0	21.8	17.5	18.0	22.9	13.2	96	54	73	74	0.7	11.9	5.5	6.0	8 ⊙	6	10	C 0	W 1	ESE 2
18	86.7	88.9	91.1	88.9	15.0	17.6	12.0	14.2	18.4	11.7	96	68	91	85	0.7	6.4	1.2	2.8	10 ●	8	10 ●	S 3	SW 7	W 5
19	90.7	91.6	93.1	91.8	11.5	17.0	13.5	13.9	17.5	9.9	95	69	88	84	0.7	6.0	1.8	2.8	10 ●	9	9	W 6	WNW 4	WNW 4
20	93.8	93.5	96.1	95.1	13.6	18.5	14.5	15.3	20.4	12.9	95	80	94	90	0.7	4.3	0.9	2.0	10 ●	9	10	NW 4	NW 3	N 2
21	95.0	94.4	92.6	94.0	13.2	16.2	15.2	15.0	18.9	12.2	90	77	86	84	1.6	4.2	2.5	2.8	10	10	10	C 0	SE 1	SE 2
22	92.4	93.7	92.9	93.0	13.7	18.4	14.4	15.2	20.1	13.2	97	65	89	84	0.6	7.4	1.8	3.3	10 ●	5	10	W 3	WSW 5	SSW 1
23	91.3	92.9	93.7	92.6	11.2	15.2	10.8	12.0	15.5	10.4	92	70	97	86	1.0	5.1	0.4	2.2	9 ⊙	9	8	SW 5	W 9	W 2
24	87.4	82.9	83.9	84.7	11.0	15.2	13.2	13.2	16.3	8.7	94	93	95	94	0.8	1.2	0.7	0.9	10 ●	10 ●	10	S 3	SW 7	W 5
25	87.3	88.3	91.5	89.0	11.8	13.8	10.7	11.8	16.6	10.7	93	91	94	93	1.0	1.5	0.9	1.1	9	9 ●	3	SW 7	WSW 7	WSW 7
26	94.1	96.5	96.9	95.8	10.8	15.8	10.6	12.0	17.1	9.8	87	62	91	80	1.7	6.7	1.2	3.2	10	8	0	WSW 8	W 7	S 1
27	90.7	87.3	89.2	89.1	10.9	19.8	13.4	14.4	20.2	8.7	87	62	77	75	1.6	8.7	3.5	4.6	9	10	4	S 3	SSW 7	WSW 4
28	92.1	93.5	93.3	93.6	11.4	15.3	10.8	12.1	16.5	10.5	75	54	92	74	3.3	8.0	1.0	4.2	10	6 ⊙	5	W 14	SW 10	SW 5
29	93.9	93.6	94.5	94.0	11.3	12.3	10.7	11.3	14.4	9.1	93	93	92	93	1.0	0.7	1.0	0.9	9	10 ●	2	SW 5	SW 3	W 1
30	96.7	98.3	96.4	97.2	10.8	14.0	10.1	11.2	13.9	9.4	90	68	91	83	1.4	5.1	1.2	2.6	9 ⊙	10 ●	8	NW 6	NW 9	W 3
31	89.3	89.3	93.1	90.6	10.0	11.3	10.3	10.3	13.4	9.2	96	88	92	92	0.3	1.7	0.9	1.0	9	10	5	W 4	W 7	NW 3
M	92.8	92.6	93.0	92.8	12.9	17.6	13.6	14.4	19.1	10.8	90	71	87	83	1.4	6.2	2.0	3.2	7.8	8.4	6.6	3.7	4.6	2.3

Chojnice $H_s = 172m$ $H_b = 177,2m$ $h_w = 12,5m$ Liniec - Juillet 1962

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚCIEŃ GŁ.	POGODA
1	7	.	.	$\triangle^{1}0^{00}-9$
2	7	3.5	.	$\bullet^{0}20^{45}-24; =0^{00}-2^{40} \equiv^{0}4^{50} = -7^{30}$
3	7	4.4	.	$\bullet^{0}0^{00-35}, 2^{35}-3^{45} \Downarrow^{0-1} 7^{25} \ldots 11^{50} \bullet^{0} 12^{05-10} \Downarrow^{0} 13^{08} \ldots 21^{20}$
4	6	10.1	.	$\Downarrow^{00} 6^{45}-10^{00} \bullet^{1-0} 13^{40} \bullet^{0} -15^{15} \bullet^{0} 15^{40}-16^{25} \Downarrow^{0} 17^{45}-18^{15}, 18^{50}-19^{35}$
5	7	4.8	.	$\Downarrow^{0} 15^{35}-16^{22} \Downarrow^{1-0} 17^{08-40} \Downarrow^{0} 21^{40}-22^{52}; = 1^{30-45} \equiv^{0} -2^{50} = -6^{30}$
6	7	0.0	.	$\Downarrow^{0} 14^{52}-15^{05}; \gg 11^{20}-12^{30}; = 6^{10}-8^{30}$
7	7	1.1	.	$\Downarrow^{0} 9^{50}-10^{15}, 13^{15} \ldots 16^{45}; = 4^{30}-8^{30}; \triangle^{0} 5-9$
8	7	.	.	$\triangle^{0-1} 0^{00}-9 \triangle^{1} 21-24$
9	7	.	.	$= 4^{20}-7^{15} \equiv^{0} -7^{45} = -8^{40}; \triangle^{0-2} 0^{00}-8 \triangle^{0} 22-24$
10	7	.	.	$= 2^{15}-3^{50} \equiv^{0} -4^{45} = -5^{10}; \triangle^{2-0} 0^{00}-10 \triangle^{0} 21-24$
11	7	0.4	.	$\Downarrow^{0} 21^{25-42}; = 3^{30}-6^{40}; \triangle^{1-2} na-8$
12	7	2.6	.	$\Downarrow^{0} 17^{50}-18^{10}, 19^{45-25}; R^{0} 17^{45}-18^{15} W-NE; = 22^{15}-24$
13	7	5.5	.	$\Downarrow^{0} 2^{30}-4^{45} \Downarrow^{0-1} 16^{20} \ldots 20^{25}; = 0^{00}-10^{40}, 17^{00}-24$
14	7	13.3	.	$\Downarrow^{0-1} 11^{44} \ldots 20^{40}; = 0^{00}-9^{40}, 20^{40}-24; \triangle^{0-1} na-8$
15	7	.	.	$= 0^{00}-5^{50} \equiv^{1} -7^{30} = -7^{50}; \triangle^{1} 22-24$
16	7	.	.	$= 3^{50}-7^{30}; \triangle^{1} 0^{00}-9 \triangle^{0-1} 20-24$
17	7	.	.	$= 3^{30}-5^{40} \equiv^{0} -6^{30} = -7^{15}; \triangle^{2-0} 0^{00}-8 \triangle^{0} 22-24$
18	8	.	.	$= 5^{40}-7^{15}; \triangle^{2-0} 0^{00}-10 \triangle^{0} 20-24$
19	8	.	.	$\triangle^{0-2} 0^{00}-11 \triangle^{0} 21-24$
20	7	1.1	.	$\Downarrow^{0} 15^{53}-16^{35}; = 4^{40}-6^{10}, 15^{30}-24; \triangle^{0-1} 0^{00}-9, 18-24$
21	7	0.0	.	$\Downarrow^{0} 20^{15-21}; = 0^{00}-8^{15}; \triangle^{1-0} 0^{00}-9 \triangle^{0} 22-24$
22	8	0.4	.	$\Downarrow^{0} 20^{20-55}; = 4^{30}-7^{15}; \triangle^{1-0} 0^{00}-9$
23	7	0.0	.	$\Downarrow^{0} 20^{10-16}$
24	7	0.0	.	$\Downarrow^{0} 16^{10-15}; \triangle^{1-0} na-10 \triangle^{1} 21-24$
25	7	.	.	$\triangle^{2-1} 0^{00}-10$
26	8	24.1	.	$\Downarrow^{0-2} 16^{20} \ldots 22^{30}; R^{0} 19^{10-20^{15}} SW-NE R^{0} 20^{50}-22^{40} NE; = 7^{20}-8^{15}, 17^{10}-24; \triangle^{0} na-10$
27	6	0.1	.	$\Downarrow^{0} 19^{48}-20^{40}, 21^{35}-22^{19}; = 0^{00}-1^{50} \equiv^{0-2} -6^{55} = -15^{30}$
28	7	2.5	.	$\Downarrow^{0-1} 10^{42} \ldots 13^{55}; \triangle^{0-2} na-10 \triangle^{0} 22-24$
29	6	3.0	.	$\Downarrow^{0} 12^{40} \ldots 17^{05}; = 4^{50}-6^{30}, 7^{15}-8^{30}; \triangle^{2-0} 0^{00}-12$
30	7	.	.	$\triangle^{2-0} na-10 \triangle^{0-1} 21-24$
31	7	1.1	.	$\Downarrow^{0} 11^{45}-12^{05}; \triangle^{1-0} 0^{00}-9$
Σ	—	78.0	—	UWAGI

Sierpień - Août

1	7	0.0	.	$\Downarrow^{0} 4^{50}-5^{25}, 8^{55}-9^{08}, 19^{26-40}; = 4^{30}-11^{10}; \triangle^{1} 21-24$
2	7	.	.	$= 4^{20}-7^{40}; \triangle^{2-0} 0^{00}-9 \triangle^{0} 21-24$
3	7	.	.	$= 2^{30}-7^{10}; \triangle^{2-0} 0^{00}-9 \triangle^{0} 21-24$
4	7	18.5	.	$\Downarrow^{0} 11^{55}-12^{03} \Downarrow^{0-2} 17^{10-25} \blacktriangle^{0} 17^{17-20}; R^{0} 16^{45}-18^{30} W-E; = 19^{20}-24$
5	7	4.4	.	$\Downarrow^{0-2} 10^{55}-12^{25} \Downarrow^{1-0} 16^{20}-17^{20}; R^{0} 16^{25}-17^{50} NW-SE; = 0^{00}-3^{50} \equiv^{0-1} -6^{45} = \ldots 24$
6	7	.	.	$= 3^{30}-10^{30}$
7	6	17.2	.	$\Downarrow^{0} 11^{35}-13^{05} \bullet^{0-1} -15^{10} \Downarrow^{0-2} 15^{15}-19^{40} \Downarrow^{0-1} 19^{50}-21^{05}; R^{0} 15^{20-55} SW-SE, R^{1} 16^{30}-17^{45} S-NE; = a-nn$
8	7	.	.	$\triangle^{0} 21-24$
9	7	0.0	.	$\Downarrow^{0} 14^{10-22}; = 5^{10}-8^{30}; \triangle^{0-2} 0^{00}-10 \triangle^{1} 20-24$
10	7	0.0	.	$\Downarrow^{0} 19^{56} \ldots 21^{48}; = 6^{20}-7^{30}; \triangle^{2-0} 0^{00}-10$
11	7	.	.	$\triangle^{0-1} 20-24$
12	7	.	.	$= 4^{30}-7^{50}; \triangle^{2-0} 0^{00}-9$
13	7	.	.	$= 4^{30}-7^{15}; \triangle^{2-0} 0^{00}-10 \triangle^{1-2} 21-24$
14	8	0.0	.	$\triangle^{2-0} 0^{00}-10 \triangle^{0} 22-24$
15	7	2.1	.	$\Downarrow^{0} 7^{10-35}, 13^{05-35}, 19^{30}-20^{05}, 23^{40-50}; R^{0} 13^{10-45} W-E; = 22^{30}-24; \triangle^{1} 0^{00}-7$
16	7	0.0	.	$\Downarrow^{0} 20^{20-30}; = 0^{00}-5^{30} \equiv^{0} -7^{00} = -11^{40}; \triangle^{1} 4-9$
17	7	0.0	.	$\Downarrow^{0} 18^{46} \ldots 21^{05}; = 6^{20}-8^{30}; \triangle^{1} 0^{00}-9 \triangle^{0} 21-24$
18	7	7.8	.	$\Downarrow^{0} 7^{45}-9^{30} \bullet^{0} -10^{25} \Downarrow^{0} 16^{45}-17^{05}, 21^{45}-22^{05}; = 2^{00}-5^{15} \equiv^{0} -5^{54} = -10^{30}; \triangle^{1-2} 0^{00}-5$
19	7	2.2	.	$\Downarrow^{0} 14^{30-45}, 15^{35-45}, 16^{04-25}; = 5^{30}-9^{30}; \triangle^{1} na$
20	7	0.5	.	$\Downarrow^{0} 1^{30}-2^{20} \bullet^{0} 7^{56}-9^{25} \Downarrow^{0} 11^{45}-12^{15}; = 22^{20}-24$
21	7	4.2	.	$= 0^{00}-9^{20}, 19^{30}-24; \triangle^{0-1} 0^{00}-10$
22	7	7.0	.	$\Downarrow^{0} 3^{45}-5^{55} \bullet^{0-2} 6^{40}-8^{45}; = 0^{00}-10^{30}$
23	7	7.7	.	$\Downarrow^{0-2} 2^{30}-4^{40} \Downarrow^{0} 14^{35} \ldots 21^{35}$
24	6	24.5	.	$\Downarrow^{0} 4^{45}-6^{20} \bullet^{0-1} 12^{25} \bullet^{0} 13^{45}-15^{10} \bullet^{0-2} 17^{50}-20^{02}; = na-n,n$
25	7	3.3	.	$\Downarrow^{0-1} 9^{54} \ldots 21^{10}$
26	7	0.2	.	$\Downarrow^{0} 15^{54}-16^{35}; \triangle^{1} 20-24$
27	7	0.0	.	$\Downarrow^{0} 15^{07-10}; = 4^{40}-7^{15}$
28	7	0.0	.	$\Downarrow^{0} 11^{40-45}, 19^{45-50}; \gg 5^{15}-20^{30}$
29	6	0.7	.	$\Downarrow^{0} 10^{10} \ldots 15^{25}, 18^{45}-19^{15}; = 5^{30}-15^{40}; \triangle^{1-2} 0^{00}-10$
30	7	4.5	.	$\Downarrow^{0} 23^{06}-24; \triangle^{2-0} na-10$
31	6	1.4	.	$\Downarrow^{0} 0^{00-20} \Downarrow^{0-1} 6^{30}-7^{20} \Downarrow^{0} 9^{35} \ldots 14^{35}$
Σ	—	106.0	—	UWAGI

Chojnice φ=53°42' λ=17°33' Wrzesień - Septembre 1962

Dni	Ciśnienie P−900 I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność wzgl. U I	II	III	Dies	Niedosyt wilgotności f I	II	III	Dies	Zachmurzenie i pogoda N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	96.0	98.6	101.0	98.8	10.1	17.1	9.4	11.5	17.7	8.0	96	55	91	80	0.5	9.2	1.1	3.6	9 ⊙	6 ⊙	0	WNW 2	WNW 7	C 0
2	101.3	101.0	99.5	100.6	9.2	17.5	10.3	11.8	18.8	5.6	97	58	88	81	0.3	8.4	1.4	3.4	10	10	0	SW 3	WSW 5	W 1
3	98.5	98.3	96.2	97.7	10.4	21.5	15.6	15.8	22.5	8.1	95	52	75	73	0.8	12.4	4.4	5.9	6 ⊙	7 ⊙	0	SW 1	W 1	SE 1
4	91.8	88.5	86.4	88.9	13.0	24.8	17.7	18.3	25.6	11.1	77	49	88	71	3.5	15.9	2.4	7.3	5 ⊙	0 ⊙	9	SE 2	SW 4	W 1
5	80.6	82.5	82.7	81.9	15.5	18.1	13.3	15.0	19.7	10.9	91	71	79	80	1.5	6.0	3.2	3.6	10 ⊼	10	8 ●	SW 3	SW 7	SW 5
6	82.0	84.0	80.5	82.2	12.0	17.0	13.1	13.8	17.7	9.7	88	63	85	79	1.7	7.2	2.3	3.7	9	9 ⊙	10	SW 8	WSW 8	S 1
7	73.0	73.7	80.3	75.7	15.0	12.8	10.6	12.2	17.4	9.7	89	91	92	91	1.8	1.4	1.0	1.4	10	8 ⊙	6	SW 8	SW 8	WSW 4
8	85.4	86.5	88.2	86.7	7.6	13.7	9.3	10.0	14.7	6.3	93	56	89	79	0.7	6.9	1.3	3.0	6 ⊙	6 ⊙	0	SW 7	SW 9	SW 2
9	95.1	98.5	99.8	97.8	10.0	14.2	9.5	10.8	14.5	8.1	92	65	89	82	1.0	5.6	1.3	2.6	9	9	9	W 7	WNW 7	SW 3
10	96.9	94.0	92.5	94.5	9.1	19.3	13.1	13.6	20.5	7.6	87	49	74	70	1.6	11.4	4.0	5.7	7 ⊙	0 ⊙	2	SSW 2	SSW 9	SSW 4
11	88.7	87.4	94.3	90.1	13.2	15.7	11.1	12.8	15.9	10.1	84	96	89	90	2.5	0.7	1.5	1.6	10	10	0	SW 2	SW 6	WNW 3
12	89.4	82.8	80.5	84.2	12.0	20.5	16.0	16.1	21.8	7.6	98	71	75	81	0.3	6.9	4.5	3.9	9	10	10	S 4	SW 8	W 12
13	91.6	94.3	97.0	94.3	9.6	14.8	9.3	10.8	16.0	7.6	89	53	88	77	1.3	7.9	1.4	3.5	1 ⊙	4 ⊙	2	WSW 4	WNW 9	W 3
14	99.5	101.4	101.7	100.9	8.8	12.3	8.4	9.5	12.7	8.1	81	66	89	79	2.1	4.8	1.2	2.7	8	10	9	W 5	W 8	WNW 2
15	99.7	97.9	95.1	96.9	7.1	12.4	9.5	9.6	14.4	5.6	97	67	83	82	0.3	4.8	2.1	2.4	10	10	4	W 2	SE 3	E 3
16	88.3	87.0	88.9	88.1	7.3	17.3	13.8	13.0	18.3	6.3	93	73	98	88	0.7	5.2	0.4	2.1	1 ⊙	10	10 ●	SE 1	SW 2	SW 1
17	90.0	91.6	91.4	91.0	9.5	13.1	9.9	10.6	13.9	8.6	97	73	84	85	0.3	4.1	1.9	2.1	10	10	6	W 1	WNW 1	C 0
18	90.9	90.0	87.8	89.6	4.9	13.2	8.4	8.7	13.3	4.6	95	68	83	82	0.5	4.8	1.8	2.4	9	10	10 ●	C 0	C 0	NE 1
19	86.7	89.7	92.7	89.7	7.4	8.3	6.8	7.3	9.4	6.6	88	86	94	89	1.2	1.6	0.6	1.1	10 ●	10	5	W 3	W 4	WSW 3
20	93.5	94.2	94.3	94.1	7.4	10.3	7.5	8.2	12.2	6.3	97	83	89	90	0.3	2.1	1.2	1.2	10	10	10	W 5	WNW 5	W 2
21	94.6	94.7	95.7	95.0	9.0	11.0	7.0	8.5	11.4	6.6	95	84	94	91	0.7	2.1	0.6	1.1	10	10	10 ●	W 6	W 6	NW 2
22	97.2	98.4	99.1	98.2	7.1	11.8	7.0	8.2	11.9	5.4	93	67	91	84	0.8	4.5	0.9	1.1	2	10	10	NW 1	NW 3	NW 2
23	95.1	92.6	95.0	94.2	8.8	9.8	7.1	8.2	11.2	5.8	96	92	94	93	0.4	0.9	0.6	0.6	10	9	0	W 2	WNW 5	NW 1
24	99.7	102.4	105.9	102.7	7.1	13.7	7.6	9.0	14.4	3.8	97	63	93	84	0.3	5.9	0.7	2.3	10	6	0	C 0	NE 2	C 0
25	108.2	109.2	107.9	108.4	5.3	14.6	8.6	9.3	15.3	4.6	98	60	84	81	0.1	6.7	1.9	2.9	0 ≡ ⊙	2 ⊙	0	E 1	SSE 1	E 2
26	106.1	104.7	102.5	104.4	6.1	15.7	9.3	10.1	15.7	5.6	94	55	79	76	0.6	7.9	2.5	3.7	0 ⊙	2 ⊙	0	E 3	SE 7	E 5
27	101.0	98.6	97.2	98.9	5.3	15.4	10.0	10.2	15.5	4.6	92	55	89	79	0.7	7.9	1.3	3.3	0 ⊙	5 ⊙	6	E 3	SE 5	E 3
28	95.5	94.9	94.4	94.9	9.5	12.3	11.5	11.2	12.3	9.2	99	88	95	94	0.2	1.7	0.7	0.9	10 ≡	10	10	ENE 2	E 3	C 0
29	93.5	93.7	94.9	94.0	10.2	12.0	11.7	11.4	12.7	9.9	97	93	95	95	0.3	1.0	0.6	0.6	10 ≡	10	10	NE 2	C 0	C 0
30	97.0	97.9	99.1	98.0	9.1	17.0	12.1	12.6	18.1	8.9	99	72	91	87	0.2	5.4	1.2	2.3	10 ≡	2	0	C 0	SE 1	C 0
31																								
M	93.6	93.6	94.0	93.7	9.2	14.9	10.5	11.3	15.8	7.4	93	69	88	83	0.9	5.7	1.7	2.8	7.4	7.5	5.2	3.0	4.8	2.2

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1	100.2	101.4	102.9	101.5	9.4	17.9	14.6	14.1	19.6	9.1	89	67	87	81	1.3	6.7	2.2	3.4	7 ⊙	9	10	ESE 1	SSE 5	ESE 1
2	104.4	104.8	104.5	104.6	11.8	19.4	13.6	14.6	20.3	11.7	96	64	87	82	0.5	8.0	2.0	3.5	10	3 ⊙	0	SE 3	SE 4	SE 3
3	103.7	103.1	102.9	103.2	14.5	19.8	13.8	14.3	20.7	9.9	92	61	86	80	1.0	9.1	2.2	4.1	9	8 ⊙	4	SE 2	SE 6	SE 4
4	102.1	101.7	101.6	101.8	9.8	18.3	15.2	14.6	18.6	9.6	97	70	87	85	0.3	6.2	2.3	2.9	8	10	8	SE 3	SE 2	WSW 1
5	101.8	102.3	103.1	102.4	12.1	15.2	12.8	13.2	15.3	11.6	99	94	98	97	0.1	1.0	0.4	0.5	10 ≡	10	10	C 0	C 0	NW 1
6	104.6	107.3	110.0	107.3	12.0	12.6	11.4	11.8	12.8	11.2	98	95	93	95	0.3	0.7	1.0	0.7	10 ≡	10	10	N 2	N 1	N 1
7	112.3	113.8	114.8	113.6	8.6	12.5	8.0	9.3	14.0	7.7	92	71	94	86	1.0	4.2	0.6	1.6	7	8	6	C 0	WNW 3	C 0
8	115.2	115.2	114.1	114.8	3.4	14.7	10.3	9.7	16.0	3.3	97	77	94	89	0.3	3.8	0.8	1.6	3 ≡	8 ⊙	0	C 0	C 0	C 0
9	113.0	111.8	109.6	111.3	4.3	17.2	10.3	10.5	17.9	3.9	97	69	96	87	0.3	6.0	0.5	2.3	10 ≡	2 ⊙	0	C 0	SSW 1	C 0
10	107.6	106.4	103.6	106.9	5.8	9.0	7.0	7.2	12.5	5.4	97	93	96	95	0.3	0.8	0.4	0.5	10 ≡	9	0	SE 1	SE 1	C 0
11	100.3	98.5	96.0	98.3	2.1	8.8	8.3	6.9	11.9	1.6	100	93	96	96	0.0	0.8	0.5	0.4	10 ≡	10	10	SSE 1	S 1	C 0
12	96.6	98.8	101.1	98.8	6.8	10.2	7.5	8.0	11.7	5.3	94	81	90	88	0.6	2.4	1.1	1.4	10	9	6	C 0	N 2	NE 2
13	101.8	99.9	95.3	99.0	2.2	12.0	6.4	6.8	12.9	2.0	95	53	92	80	0.4	6.6	0.7	2.6	6	0 ⊙	0	C 0	SE 3	SE 1
14	90.1	91.0	94.9	92.0	4.7	9.7	7.4	7.3	10.6	2.3	97	84	91	91	0.2	1.9	0.9	1.0	10	8	10 ●	SW 1	W 7	N 5
15	102.0	104.6	105.6	104.1	1.2	8.5	1.4	3.1	8.7	1.1	89	49	85	74	0.8	5.7	1.0	2.5	1 ●	2 ⊙	0	N 1	NNW 1	C 0
16	102.3	100.6	99.8	101.0	2.1	9.9	7.6	6.8	10.6	-0.1	78	63	86	76	1.3	4.3	1.4	2.5	10	6 ⊙	10	SW 3	SW 8	WSW 1
17	99.9	101.0	100.4	100.4	8.4	9.4	8.8	8.8	10.2	6.6	94	89	97	93	0.6	1.3	0.3	0.7	10	10	10	W 4	W 4	W 3
18	97.0	94.1	87.0	92.7	10.1	10.7	11.8	11.1	11.8	8.6	87	90	80	86	1.6	1.3	2.8	1.9	10	10	10	W 7	SW 10	W 12
19	89.2	91.2	90.5	90.3	9.3	12.3	9.0	9.9	12.7	8.6	91	60	84	78	1.1	5.8	1.9	2.9	9	8	10	W 5	NW 8	NW 9
20	96.6	101.0	106.5	101.4	5.4	10.4	2.4	5.2	11.1	2.3	95	51	86	77	0.5	6.2	1.1	2.6	0 ⊙	4 ⊙	0	NW 2	NW 5	C 0
21	107.5	107.1	107.0	107.2	1.3	10.5	8.3	7.1	10.5	-0.1	89	76	96	87	0.8	3.0	0.5	1.4	0 ⊙	8	10 ●	SW 2	W 7	W 3
22	106.8	106.9	105.6	106.8	7.7	8.8	7.7	8.0	9.3	7.1	94	81	83	86	0.6	2.1	1.8	1.3	10	10	10	W 1	W 4	WNW 4
23	103.7	103.2	101.7	102.9	6.9	9.2	6.0	7.0	9.4	5.9	96	84	89	90	0.4	1.8	1.1	1.1	10	10	10	WSW 3	W 2	SW 4
24	97.8	98.6	100.1	98.8	2.0	6.0	4.9	4.4	6.6	1.4	96	94	97	96	0.3	0.6	0.3	0.4	10 ≡	10	10 ≡	SW 2	W 4	SW 4
25	98.4	96.9	95.8	97.0	4.1	9.3	8.3	7.3	10.4	4.1	98	84	74	85	0.2	1.9	2.9	1.7	10 ≡	10	0	SW 3	SSW 4	S 4
26	93.3	91.4	88.6	91.2	2.6	10.7	8.3	7.3	11.3	2.0	96	68	86	83	0.3	4.2	1.6	2.0	0	0	0	SSE 1	S 3	S 4
27	87.9	93.3	96.7	92.6	6.1	8.1	0.8	4.0	9.2	0.8	94	71	83	83	0.6	3.1	1.0	1.6	10 ●	8	0	NW 5	NW 4	C 0
28	90.8	87.9	87.9	88.9	2.2	5.3	4.6	4.2	5.7	0.1	98	71	79	83	0.2	2.6	1.8	1.3	10 ● ≡	9	10	S 1	SW 6	SW 1
29	89.6	91.4	94.5	91.8	2.8	7.0	1.7	3.3	7.3	1.7	93	81	98	91	0.6	1.9	0.1	0.9	10	10	0	SW 1	SW 1	C 0
30	94.6	93.4	89.6	92.3	2.3	4.4	3.0	3.2	4.8	0.3	100	98	93	97	0.0	0.2	0.6	0.3	10 ≡	10 ≡	0	SW 2	S 2	SSE 3
31	87.4	88.1	89.3	88.3	2.3	7.1	4.3	4.6	7.3	0.3	96	74	87	86	0.3	2.6	1.1	1.3	10 ≡	10	10	S 1	S 3	C 0
M	100.0	100.2	100.0	100.1	5.8	11.1	7.9	8.2	12.0	4.7	94	76	89	86	0.5	3.3	1.2	1.7	8.1	7.7	5.6	1.3	3.6	2.3

Chojnice $H_s = 172m$ $H_a = 177{,}2m$ $h_w = 12{,}5m$ Wrzesień - Septembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ SNIEGU h	POGODA
1	7	•	•	$=4^{30}-7^{40}$; $\triangle^{1-2}21-24$
2	7	•	•	$=4^{30}-10^{30}$; $\triangle^{2-0}0^{00}-11$
3	7	•	•	$=4^{30}-10^{30}19^{20}-22^{10}$; $\triangle^{1}0^{00}-10^{00}$
4	7	0.0	•	$=5^{20}-10^{40}19^{40}-24$; $\triangle^{1}$na-8,20-24
5	7	0.1	•	$\Downarrow^{0}7^{42}...10^{05}18^{53}-19^{05}21^{40-50}$; R $7^{50}-8^{15}$ SW-NW; $=0^{00}-10^{15}$; $\triangle^{1}0^{00}-7$
6	7	2.8	•	$=19^{10}-21^{15}$
7	7	1.4	•	$\bullet^{0}0^{05}-1^{40}\bullet^{0-1}2^{15}-5^{20}\Downarrow^{0-1}10^{15}...19^{59}$; R $^{0}13^{20-45}$ W-E
8	7	0.0	•	$\triangle^{2-1}0^{00}-10$
9	7	0.0	•	$\Downarrow^{00}7^{33-45}$; $9^{53}-10^{15}$
10	7	0.0	•	$\succ 14^{15}-16^{30}$; $\triangle^{1}0-8$
11	6	4.7	•	$\Downarrow^{0}7^{25}...10^{10}\bullet^{0-1}-12^{39}\Downarrow^{0}18^{52-57}$; $=7^{30}-14^{15}$
12	7	8.7	•	$\Downarrow^{0}8^{55}-10^{05}\Downarrow^{0-2}16^{45}...18^{35}\Downarrow^{1-0}22^{40}-23^{20}$; R $^{2}17^{05-25}$ W-E $\Rightarrow 18^{00}-24$; $=6^{10}-10^{15}$; $\frown 17^{25-30}$; 18^{35-36}
13	7	0.0	•	$\Rightarrow 0^{00}-3^{30}$
14	7	0.2	•	$\Downarrow^{0}1^{10-25}$; $9^{50}-10^{10}$; $\triangle^{0}22-24$
15	7	•	•	$=4^{10}-6^{45}\equiv^{0}7^{30}=-8^{15}$; $\triangle^{1-2}0^{00}-12\ \triangle^{0}20-24$
16	7	7.8	•	$\Downarrow^{0}13^{25}-17^{35}\bullet^{0}18^{02}-22^{45}\bullet^{0-1}23^{05}-24$; $=6^{30}-10^{10}$; $15^{10}-24$; $\triangle^{1-0}0-11$
17	7	•	•	$\bullet^{1-0}0^{00}-4^{25}$; $=0^{00}-9^{15}$; $\triangle^{0}20-24$
18	7	13.3	•	$\Downarrow^{0}14^{58}-15^{15}$; $16^{07}-17^{10}\bullet^{0}20^{50}-24$; $=3^{10-45}=8^{05-25}$; $\triangle^{1-2}0^{00}-11$
19	7	15.9	•	$\bullet^{0-1}0^{00}-3^{40}\bullet^{0}4^{10}-13^{30}$; $14^{20-30}\Downarrow^{0}16^{40}-18^{05}$
20	7	7.7		$\Downarrow^{0-2}12^{43}...14^{15}\blacktriangle^{0}14^{06-09}$; 16^{45-55}; $20^{55}-21^{15}$; $23^{55}-24$; R $^{0}12^{30}-13^{05}$ NW-SE; $\equiv^{0}1^{45}-5^{40}=-10^{20}$
21	7	2.9	•	$\Downarrow^{0-1}0^{00}-1^{15}\Downarrow^{0}1^{40}-2^{20}\Downarrow^{0-1}14^{03-25}\Downarrow^{0}21^{50}-22^{30}$; $22^{45}-23^{15}$; $=3^{30}-8^{30}$
22	7	2.0	•	$\Downarrow^{0}21^{52-54}$; 22^{45}; 23^{05}
23	7	6.8	•	$\Downarrow^{0-1}7^{12}...17^{10}$; $=5^{15}-13^{40}$
24	7	•	•	$=0^{30}-1^{30}\equiv^{0}4^{20}\equiv^{0}4^{40}=-10^{15}$
25	7	•	•	$=4^{20}-6^{35}\equiv^{0}7^{10}\equiv^{0}9^{55}=-12^{15}$; $\triangle^{1-2}20-24$
26	7	•	•	$=5^{30}-9^{40}$; $\triangle^{2-1}0^{00}-11\ \triangle^{1}20-24$
27	7	0.1	•	$\triangle^{2-1}0^{00}-11$
28	6	0.1	•	$\bullet^{0}4^{05}-7^{35}\bullet^{1-0}8^{10}-9^{15}$; $15^{30}-17^{15}$; $=4^{10}-7^{15}\equiv^{1-0}8^{50}=-24$
29	6	0.9	•	$\bullet^{1}0^{30}-1^{25}\bullet^{2-1}5^{40}-7^{20}\bullet^{1}8^{25}-11^{30}\bullet^{2}19^{45}-21^{10}$; $=0^{00}-6^{40}\equiv^{0-1}-10^{45}=-24$
30	6	•	•	$=0^{00-40}\equiv^{0-1}-3^{45}=-5^{50}\equiv^{0-2}-9^{55}=-24$
31				
Σ	—	75.4	—	UWAGI

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1	6	•	•	$=0^{00}-24$
2	6	•	•	$=0^{00}-15^{20}16^{40}-24$; $\triangle^{1}0^{00}-9$,20-24
3	7	•	•	$=0^{00}-10^{30}$; $\triangle^{1-0}0^{00}-11$
4	6	0.0	•	$\Downarrow^{0}15^{50}-16^{15}$; $=4^{10}-24$
5	5	22.7	•	$\bullet^{0}7^{15-40}$; $8^{30}...12^{10}\bullet^{1-0}17^{15}-19^{35}$; $=0^{00}-6^{20}\equiv^{0}-6^{40}\equiv^{0}-7^{50}=-22^{30}\equiv^{0}-24$
6	6	0.0	•	$\bullet^{0}3^{05}-4^{15}\bullet^{0}17^{50}-18^{35}$; $\equiv^{0}0^{00}-7^{50}=-21^{30}$
7	7	•	•	$=5^{15}-9^{40}$; $20^{30}-24$
8	6	•	•	$=1^{00}-5^{30}\equiv^{0}7^{50}=-24$; $\triangle^{2}1-9\ \triangle^{1}20-24$
9	6	•	•	$=0^{00}-2^{50}\equiv^{1-0}-9^{55}=-24$; $\triangle^{2}0^{00}-10\ \triangle^{0-2}17-24$
10	6	•	•	$=0^{00}-1^{50}\equiv^{0-2}-12^{30}=-24$; $\triangle^{2-1}0^{00}-13\ \triangle^{1}18-24$
11	6	•	•	$=0^{00}-1^{30}\equiv^{0-2}-10^{50}=-21^{30}$; $\triangle^{2-0}0^{00}-14\ \triangle^{0-2}19-24$
12	7	•	•	$=0^{00}-1^{30}5^{10}-9^{30}$; $\triangle^{2-0}0^{00}-12\ \triangle^{1}22-24$
13	7	•	•	$=21^{30}-24$; $\triangle^{2-0}0-11\ \triangle^{1}20-24$
14	6	3.3	•	$\bullet^{0}10^{52}-11^{25}\Downarrow^{0}15^{48-54}$; $16^{35}-19^{40}$; $20^{15}-22^{10}$; $=0^{00}-13^{40}$; $\triangle^{2}0^{00}-8$
15	7	•	•	$\sqcup^{0}0^{00}-6$, 21-24
16	7	0.0	•	$\sqcup^{0}0^{00}-5$
17	7	0.0	•	$\bullet^{0}3^{55}-4^{20}$; $9^{30}-12^{40}$; $=1^{15}-3^{50}\equiv^{0}4^{45}=-8^{30}$; $20^{30}-24$
18	6	0.6	•	$\bullet^{1}0^{05}-2^{10}$; $7^{40}-9^{20}\bullet^{0}14^{15}-16^{25}\bullet^{1-2}23^{15}-24$; $\Rightarrow 12^{30}-24$; $=0^{00}-3^{30}$; $7^{30}-24$
19	7	0.0	•	$\bullet^{2}0^{00-20}\bullet^{0}-1^{20}\Downarrow^{0}5^{35}-6^{10}$; 20^{40-46}; $21^{40}-22^{10}$; $\Rightarrow 0^{00}-2^{15}$; $=0^{00}-7^{30}$
20	7	•	•	$\sqcup^{0}21-24$; $\triangle^{2-0}$na-10
21	7	0.0	•	$\bullet^{0-2}15^{30}-23^{15}$; $=15^{40}-24$; $\sqcup^{2-1}0^{00}-8$
22	7	0.0	•	$=0^{00}-7^{30}$
23	7	•	•	$\bullet^{0}3^{50}-4^{40}$ 5^{35}; $=3^{20}-10^{20}16^{30}-17^{40}$
24	5	•	•	$=1^{10}-2^{50}\equiv^{0-1}-10^{50}=-20^{45}\equiv^{0-1}-24$; $\triangle^{1}20-24$
25	6	•	•	$\equiv^{1-2}0^{00}-10^{55}=-17^{40}$; $\triangle^{2}0^{00}-10$
26	6	1.0	•	$=1^{30}-7^{35}\equiv^{0-2}-10^{45}=-24$; $\sqcup^{1}5-7$
27	7	0.8	•	$\Downarrow^{0}5^{50}-6^{00}$; $6^{25}-7^{15}$; $7^{23}-8^{02}$; $=0^{00}-8^{30}$
28	7	0.0	•	$\Downarrow^{0}4^{55}-5^{05}\bullet^{0}6^{43}-8^{40}$; $=5^{30}-6^{45}\equiv^{0}7^{30}=-9^{30}$
29	6	•	•	$=6^{10}-22^{30}\equiv^{0}23^{40}=-24$; $\sqcup^{0}20-24$
30	2	•	•	$=0^{00}-5^{45}\equiv^{0-2}12^{55}=-20^{20}$; $\sqcup^{0}0^{00}-5$
31	6	2.8	•	$=2^{10}-4^{15}\equiv^{0}7^{35}=-14^{15}$; $15^{40}-24$
Σ	—	31.2	—	UWAGI

Chojnice φ=53°42' λ=17°33' Listopad - Novembre 1962

Dni	Ciśnienie P— 900 + I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność wzgl. U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie i pogoda N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	89.4	88.2	88.7	88.8	3.7	5.1	6.1	5.2	6.3	3.3	97	97	97	97	0.3	0.3	0.3	0.3	10 ●	10 ●	10 ●	C 0	N 4	N 5
2	89.0	90.3	95.7	91.0	7.8	8.8	7.2	7.8	9.1	6.1	97	97	97	97	0.3	0.3	0.3	0.3	10 ,	10 ≡	10 ≡	N 1	C 0	S 2
3	95.4	95.4	95.5	95.4	6.3	7.8	7.5	7.3	8.0	6.1	98	86	96	93	0.1	1.5	0.5	0.7	10 ≡	10	10	SE 1	S 2	E 1
4	94.8	94.4	94.3	94.5	7.2	10.2	9.1	8.9	11.5	6.4	94	78	95	89	0.6	2.7	0.7	1.3	10	8	10	SSE 3	SE 2	ESE 3
5	92.8	92.0	91.7	92.2	9.3	11.8	8.7	9.6	11.9	8.5	91	81	93	88	1.1	2.6	0.7	1.5	10	4	2	SE 5	ESE 9	ESE 9
6	91.0	90.7	92.1	91.3	3.2	8.7	7.7	6.8	8.9	3.0	84	58	64	69	1.2	4.7	3.8	3.2	0 ⊙	4 ⊙	10	E 7	E 7	ESE 8
7	95.3	98.2	99.1	97.5	4.4	8.8	5.6	6.1	9.4	4.2	76	72	78	75	2.1	3.2	2.0	2.4	8	8	6	E 5	SE 4	E 4
8	97.7	95.9	95.8	96.5	2.6	9.8	5.0	5.6	10.2	2.5	86	67	86	83	1.1	4.0	1.2	2.1	1	0 ⊙	0	E 4	E 3	E 3
9	95.9	96.9	99.4	97.4	3.2	6.9	5.1	5.1	7.2	2.8	88	78	84	83	0.9	2.2	1.4	1.5	1	4	10	E 3	ENE 5	E 6
10	100.7	102.2	104.2	102.4	2.6	1.1	0.3	1.1	5.1	0.3	86	83	72	80	1.1	1.1	1.7	1.3	10	10	10	ENE 8	NE 6	NE 5
11	103.9	102.6	100.9	102.5	-0.5	0.2	0.4	0.1	0.5	-0.8	86	90	94	90	0.9	0.6	0.4	0.6	10	10 ✳	10 ✳	NE 5	NE 5	E 5
12	99.8	99.4	98.0	99.1	1.0	1.1	-0.1	0.5	1.2	-0.1	96	96	94	95	0.3	0.2	0.4	0.3	10	10 ●	10	E 6	ENE 4	ENE 2
13	97.4	98.6	99.4	98.5	0.3	2.2	2.3	1.8	2.6	-0.1	98	93	96	96	0.1	0.6	0.3	0.3	10 ≡	10	10	ESE 1	SSW 1	S 1
14	98.7	98.0	95.9	97.5	2.1	3.8	3.0	3.0	4.0	2.0	96	98	98	97	0.3	0.1	0.2	0.2	10 ≡	10 ≡	10 ≡	E 1	C 0	C 0
15	89.6	84.9	81.8	85.4	3.6	4.8	1.4	2.8	5.3	1.4	97	92	87	92	0.3	0.7	0.9	0.6	10 , ≡	9	10	SW 3	SSW 5	SW 3
16	83.6	85.9	88.5	86.0	1.3	3.0	-0.5	0.8	3.7	-0.6	92	74	86	84	0.5	2.0	0.9	1.1	10	6 ⊙	0	WSW 3	W 8	W 4
17	90.8	91.9	91.1	91.3	-1.3	-1.0	-1.6	-1.4	-0.5	-1.7	86	85	86	86	0.8	0.9	0.7	0.8	10	10	8	W 3	SSW 2	SE 2
18	86.3	84.4	81.8	84.2	-1.6	0.3	0.9	0.1	1.0	-2.8	86	79	85	83	0.7	1.3	1.0	1.0	10	10	10	E 7	E 6	E 4
19	76.0	79.4	84.7	80.0	0.3	1.1	0.6	0.6	1.6	0.3	98	98	94	97	0.1	0.1	0.4	0.2	10 ✳	10	10	ESE 3	SSW 3	S 2
20	85.1	86.0	85.9	85.7	0.2	1.6	0.5	0.7	1.8	-0.1	98	96	96	97	0.1	0.3	0.2	0.2	10	10 , ≡	10 ≡	SW 1	C 0	W 3
21	87.9	89.7	90.9	89.5	-0.7	0.6	-0.5	-0.3	1.3	-1.0	91	86	88	88	0.5	0.9	0.7	0.7	10	9	10	SW 5	S 3	C 0
22	90.1	91.0	93.2	91.4	-2.1	-0.4	0.0	-0.6	0.0	-2.1	87	86	98	90	0.6	0.8	0.1	0.5	10	10 ✳	10 ✳	NE 3	NE 2	ESE 2
23	95.5	97.3	101.6	98.1	-2.2	-0.4	-1.5	-1.4	0.2	-2.9	83	92	90	88	0.9	0.5	0.5	0.6	5	10 ✳	10	S 3	SW 4	WSW 2
24	105.5	107.0	109.2	107.2	-2.7	-0.6	-0.5	-1.1	0.0	-5.7	89	95	94	93	0.6	0.3	0.4	0.4	10	10 ≡	10	SW 2	W 2	W 1
25	109.3	107.8	106.8	108.0	-2.5	-1.1	-0.6	-1.2	-0.5	-2.7	93	87	93	91	0.4	0.8	0.4	0.5	10 ≡	10	10	WSW 4	SSW 4	SW 3
26	109.4	110.8	111.0	110.4	0.1	0.8	0.9	0.7	1.1	-0.8	98	98	96	97	0.2	0.2	0.2	0.2	10 ≡	10 ≡	10	C 0	WSW 1	SW 3
27	109.1	108.6	105.6	107.8	2.0	3.4	3.4	3.0	3.5	0.9	98	98	100	99	0.2	0.1	0.0	0.1	10 ≡	10 ≡	10 ≡	W 2	SW 3	SW 3
28	101.1	100.0	100.7	100.6	2.9	4.5	4.6	4.2	4.6	2.6	93	90	93	92	0.5	0.8	0.6	0.6	10	10	10	SW 4	W 7	W 4
29	100.0	97.5	91.4	96.3	3.0	4.8	5.2	4.6	6.0	2.5	93	95	90	93	0.6	0.4	0.8	0.6	10	10	10 ●	W 2	SW 5	W 9
30	89.1	91.2	99.3	93.2	4.2	3.3	0.8	2.3	5.4	0.8	87	93	94	91	1.0	0.5	0.4	0.6	7	10	10 ✳	W 7	NNW 5	NE 4
31																								
M	95.0	95.2	95.7	95.3	1.9	3.7	2.7	2.8	4.3	1.1	91	87	90	89	0.6	1.2	0.7	0.8	8.7	8.7	8.9	3.4	3.7	3.4

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Dni	Ciśnienie I	II	III	Dies	Temperatura I	II	III	Dies	Max	Min	U I	II	III	Dies	Δ I	II	III	Dies	N,w I	II	III	D,v I	II	III
1	110.0	113.7	118.4	114.0	-1.0	0.0	-3.0	-1.8	0.8	-3.1	87	80	84	84	0.8	1.2	0.8	0.9	8	2 ⊙	0	NNW 2	N 7	C 0
2	119.7	120.3	118.5	119.5	-4.3	-0.7	-4.1	-3.3	-0.7	-4.8	89	85	89	88	0.5	0.9	0.5	0.6	0	9	1	C 0	W 6	W 5
3	115.4	113.7	108.9	112.7	-6.1	-3.1	-4.4	-4.5	-2.5	-6.5	89	86	84	86	0.4	0.7	0.7	0.6	9	9	0	W 5	SW 4	WSW 2
4	103.9	102.6	100.2	102.2	-2.5	2.4	0.2	0.1	3.6	-5.1	89	63	66	73	0.6	2.7	2.1	1.8	7	2 ⊙	6	SW 2	W 5	WNW 4
5	101.2	105.4	107.8	104.8	1.9	2.6	1.6	1.9	2.8	-0.9	93	96	98	96	0.5	0.3	0.2	0.3	10	10 ,	10 ≡	NW 1	NNW 1	C 0
6	107.2	106.8	106.0	106.7	-0.2	-0.1	-0.2	-0.2	1.6	-0.5	94	98	98	97	0.4	0.2	0.1	0.2	10 ≡	10 ≡	10 ≡	W 4	W 6	W 5
7	104.2	104.2	105.6	104.7	-2.9	0.0	-2.7	-2.1	1.3	-3.4	95	92	86	91	0.2	0.5	0.7	0.5	10 ≡	0 ⊙	0	W 3	W 1	C 0
8	107.4	107.0	102.3	105.6	-6.1	-4.5	-4.3	-4.8	-2.7	-6.6	92	91	91	91	0.3	0.4	0.4	0.4	10 ≡	10 ≡	0 ≡	SE 1	S 2	S 2
9	88.8	82.1	72.3	81.1	-0.5	0.7	0.3	0.2	0.9	-4.4	78	88	96	87	1.3	0.7	0.2	0.7	9	10	10 ✳	SW 6	SW 10	SW 12
10	72.4	73.4	77.4	74.4	1.3	2.6	2.8	2.4	2.9	0.3	91	93	91	92	0.6	0.6	0.7	0.6	10 ●	10 ●	10	WSW 14	SW 10	WNW 4
11	80.3	80.6	75.6	78.8	1.5	2.4	0.8	1.4	2.9	0.8	91	86	96	91	0.6	1.1	0.3	0.7	9	10	10 ●	W 6	W 6	SW 7
12	69.0	67.9	69.5	68.8	2.6	3.2	3.8	3.4	4.4	0.8	95	91	92	93	0.4	0.7	0.7	0.6	10	10	10 ●	SW 8	SSW 6	SSW 10
13	74.2	74.9	77.2	75.4	1.2	0.5	-0.4	0.2	3.8	-0.6	96	96	96	96	0.3	0.2	0.2	0.2	8	10 ✳	10 ≡	SSE 2	E 1	C 0
14	79.9	81.6	80.8	80.8	-1.6	0.2	-1.6	-1.2	0.2	-2.9	94	96	92	94	0.3	0.3	0.4	0.3	10 ≡	10	7	WNW 1	WSW 3	W 2
15	66.9	59.2	58.6	61.6	-1.3	0.1	0.4	-0.1	1.0	-3.9	93	98	96	96	0.4	0.2	0.3	0.3	10 ✳	10	10 ● ✳	S 9	SW 7	WSW 7
16	51.6	52.5	60.0	54.7	0.0	0.3	-0.4	-0.1	1.0	-0.5	98	92	92	94	0.1	0.5	0.5	0.4	10 ✳	10 ✳	10	SE 3	NE 2	NE 2
17	68.6	71.9	76.0	72.2	-0.3	0.3	-3.1	-1.6	0.3	-3.9	92	96	86	91	0.5	0.2	0.7	0.5	10	10	0	NW 1	NW 1	C 0
18	76.9	78.1	80.4	78.5	-3.3	-2.8	-4.8	-3.9	-2.0	-5.2	95	91	91	92	0.3	0.5	0.4	0.4	10	10	10	C 0	C 0	NE 2
19	83.3	86.7	93.5	87.8	-5.2	-8.4	-7.2	-7.0	-4.1	-9.2	90	86	90	89	0.4	0.4	0.3	0.4	10	10	10	C 0	NE 3	NE 2
20	99.1	101.5	102.5	101.0	-6.6	-7.3	-10.1	-8.5	-6.3	-10.5	88	85	84	86	0.4	0.3	0.4	0.4	10	9 ✳	10	C 0	NE 2	E 2
21	99.1	99.1	102.7	100.3	-18.3	-14.5	-16.9	-16.6	-10.1	-18.7	78	78	80	79	0.3	0.4	0.3	0.3	0	2	0	E 2	E 4	ENE 2
22	110.0	115.5	120.9	115.5	-17.9	-12.0	-15.9	-15.4	-11.8	-19.1	79	85	76	80	0.3	0.4	0.4	0.4	0	0	0	NE 2	NE 2	NNE 1
23	123.0	125.4	126.7	125.0	-14.7	-9.9	-12.9	-12.6	-9.6	-18.0	82	71	69	74	0.3	0.8	0.7	0.6	0	0 ⊙	0	ENE 1	NE 1	NE 3
24	124.6	123.5	120.6	122.9	-14.1	-6.4	-7.8	-9.0	-5.9	-18.0	75	75	84	78	0.5	0.9	0.5	0.6	0	10	7	C 0	E 1	C 0
25	115.2	111.4	104.3	110.3	-7.0	-5.3	-6.5	-6.3	-5.0	-9.3	85	87	83	85	0.5	0.5	0.6	0.5	10	10 ✳	10	NE 1	C 0	SE 3
26	96.8	93.0	90.2	93.3	-10.1	-12.2	-10.5	-10.8	-6.5	-12.5	84	81	87	84	0.4	0.4	0.4	0.4	10 ✳	8	10	S 3	SSW 1	SW 6
27	88.2	88.1	89.0	88.4	-12.6	-10.7	-9.7	-10.7	-8.9	-12.9	85	87	85	86	0.4	0.4	0.4	0.4	8	3 ⊙	10 ✳	S 2	SSW 1	S 2
28	88.5	89.3	91.2	89.7	-8.3	-6.6	-6.1	-6.8	-6.1	-9.9	83	88	84	85	0.5	0.4	0.6	0.5	10 ✳	10	10	SSW 1	SW 3	SW 3
29	89.4	87.3	86.6	87.8	-6.3	-7.3	-10.1	-8.4	-5.4	-10.3	86	82	87	85	0.5	0.6	0.4	0.5	10 ✳	10 ✳	0	SE 2	E 2	C 0
30	89.2	92.1	95.3	92.2	-7.8	-6.4	-8.7	-7.9	-6.1	-11.9	81	91	89	87	0.6	0.3	0.4	0.4	10	3 ⊙	0	C 0	N 1	NE 1
31	98.8	101.3	103.1	101.1	-10.4	-9.4	-14.1	-12.0	-7.4	-14.6	84	82	83	83	0.4	0.3	0.3	0.4	0	7	0	NE 2	NE 1	NE 3
M	93.6	93.9	94.3	93.9	-5.2	-5.6	-5.0	-4.7	-2.4	-7.3	88	87	87	87	0.5	0.6	0.5	0.5	7.7	7.5	5.8	2.7	3.2	3.0

Chojnice $H_s = 172m$ $H_t = 177{,}2m$ $h_w = 12{,}5m$ Listopad - Novembre 1962

DNI	WIDZIALNOŚĆ v	OPAD R	GRUB. ŚNIEGU h	POGODA
1	6	22.1	•	•0-1 3^46-13^30; 16^58-21^25 •22^40-23^20; =0^00-21^40
2	3	0.9	•	•0^15-3^15 •6^40-7^45 8^05-20 9^40-10^30 •16^06-19^10; =4^20-8^40 ≡°-24
3	6	0.0	•	•17^50-18^45; ≡°0^00-7^50 =-24
4	6	•	•	=0^00-24; △°na-10
5	6	•	•	=0^00-17^30
6	7	•	•	»19^30-20^40
7	7	•	•	
8	7	•	•	=13^15-17^40
9	6	•	•	=6^15-17^20
10	7	0.0	•	=6^20-8^30
11	5	2.6	•	*°5^30-6^15 *0-1 7^10-11^50 *°-12^30 *°-22^40
12	6	1.8	pł.	•°7^10-40 •°-8^30 •1-2-10^45 •°-13^20 ‡°-14^30 ‡°-17^45; 18^30-19^20 •0-1 21^40-24; =7^10-24
13	6	•	•	•1-0 0^00-2^20; =0^00-2^45 ≡0-1-8^50 =-24
14	2	0.3	•	•14^40-16^10; 21^30-23^50; =0^00-5^50 ≡0-2-24; △'0^00-8
15	5	0.0	•	•0-1 5^06-8^10; ≡2-0 0^00-10^45 =-24
16	7	0.0	•	‡°15^53-16^02, 17^40-43; 19^50-53; =0^00-9^30
17	7	•	•	⊔'22-24
18	6	3.7	•	‡°21^40-22^10 *°-24; =9^10-17^30; ⊔'0^00-10
19	6	0.3	5	*°0^00...1^45, 3^50-7^20, 8^50-9^15; =3^30-8^40 ≡0-1-11^45 =-12^20 ≡°-12^45 =-24
20	3	0.3	1	•11^45-14^20; =0^00-7^50 ≡0-1-21^40 =-24; ⊔°0^00-8
21	6	•	pł.	=0^00-4^15 6^30-24
22	6	3.1	pł.	*°9^50-11^40, 12^45-13^10, 13^30-14^15 △°14^30-16^20 *°-21^45; =0^00-22^45 ≡-24
23	5	0.5	2	*°2^15-3^45, 9^10-13^40; ≡°-3^40 =-24
24	3	•	3	≡'0^40-6^30 =12^40 ≡°-13^45 =-24
25	6	•	2	=0^00-6^40 ≡°-7^50 ≡-24
26	1	•	2	=0^00-3^50 ≡0-2-13^40 =-24
27	2	0.0	pł.	•°17^45-18^10; =0^00-1^30 ≡0-1-24
28	7	0.5	•	•°13^50-17^45; ≡1-0 0^00-5^55 =-12^20; 13^30-21^20
29	5	2.3	•	•°5^45-6^35, 9^48-10^20 •2-12^45 •°13^30-14^50, 17^52-19^15 •°-23^35 •1-24; =9^20-24
30	7	2.3	•	•1-0 0^00-2^35 ‡ 7^48-9^35, 11^25-40, 16^15-35, 17^40-18^20 ‡°-22^15
31				
Σ	—	40.7	—	UWAGI

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1	7	•	•	⊔1-2 0^00-24
2	7	•	•	⊔2 0^00-24
3	6	•	•	=7^15-17^40; ⊔2 0^00-24 v°8^30-14^00
4	6	•	•	=7^30-22^10; ⊔2 0^00-10
5	5	0.3	•	•°9^50-14^40; =2^20-19^50 ≡0-1-24; △'19^00-24
6	2	0.0	•	•°1^15-6^10, 18^05-20^15; ≡0-1 0^00-24
7	7	•	•	≡'0^00-8^55 =-11^20, 13^35-24; v°5^50-10^00
8	3	•	•	=0^00-1^50 ≡0-2-17^30 ≡°-24; v'1^40-24
9	6	1.3	•	*°13^10...14^15, 19^45-24; ≡°0^00-5^40 =-24; » 9^20-13^30, 15^10-24; v°0^00-7^00
10	7	1.7	•	*°0^00-20 *°-1^25 •°5^40-7^15 *1-0 9^15 10^17-13^15 13^35-14^45; » 0^00-10^30, 12^40-14^10; =0^00-1^40
11	7	4.5	•	•°13^40-18^15 20^45-21^35, 22^40-24; =21^30-24
12	6	0.6	•	•°0^00-6^15, 7^35-9^20 15^05...16^25 19^20-22^10; » 20^10-22^30; =0^00-17^20
13	4	5.5	•	•°9^40-11^30 ‡°12^10 ‡0-1-14^15 *°-17^30 =0^00-15^40 ≡0-2-24
14	6	1.0	2	*1-0 9^10-10^20; ≡2-0 0^00-11^55 =-17^30
15	7	2.7	5	*0-1 5^35-12^10 *° 20^10-21^20; » 8^15-9^30
16	6	0.9	5	*°5^20-12^15 ‡°12^30...19^35; =1^30-20^30
17	6	0.0	6	‡° 2^55-3^50 *°9^45-11^35; =6^30-19^10 19^15-20^20 22^30-23^50 ≡°-24; v°23^50-24
18	6	1.0	6	*°6^05-13^45-15^15...17^35, 18^30-19^40; ≡1-0 0^00-4^45 =-21^20; v°0^00-24
19	7	•	7	*°1^40-2^20; =2^00-10^30; v°0^00-17^00
20	7	0.0	6	*°10^50...13^25; =15^10-16^40, 18^20-22^30
21	7	•	6	=7^20-9^10; v°1^30-24
22	7	•	6	v°0^00-18^00
23	7	•	5	
24	7	0.1	5	‡°8^55-12^20
25	6	0.2	5	*°9^05-15^40
26	7	0.2	6	*°6^45-12^15, 14^30-19^40
27	6	0.2	7	*°8^42-45 8^54-9^03, 17^45-23^35; =7^20-23^30
28	5	1.0	8	*°5^55-11^15...12^20; =5^15-24
29	5	1.0	9	*°5^05-13^40; =0^00-24
30	7	•	10	=0^00-2^30, 18^30-23^30; v°18^00-24
31	6	•	10	=7^30-17^40; v°0^00-15^30
Σ	—	22.2	—	UWAGI.

Szczecin - Dąbie φ = 53°24' λ = 14°37' Styczeń - Janvier 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Mag	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	96.3	102.6	106.0	101.6	3.6	3.1	1.6	2.5	5.6	1.3	70	78	81	76	2.4	1.7	1.3	1.8	10	10	8	SW 10	WSW10	WSW 7
2	109.8	113.2	118.1	113.7	0.4	0.1	-3.1	-1.4	1.6	-3.2	78	70	84	77	1.4	1.9	0.8	1.4	10	9	0	W 4	NW 4	WNW 3
3	118.4	120.9	123.9	121.1	0.2	1.6	1.4	1.2	1.8	-5.2	92	98	96	95	0.5	0.2	0.3	0.3	10 ◐	10 ◐	10	WSW 5	W 2	C 0
4	124.9	125.4	125.3	125.2	-0.3	-0.6	-0.4	-0.4	1.4	-1.0	98	98	96	97	0.2	0.1	0.2	0.2	10	10 ◐	10	SW 4	WSW 3	W 2
5	122.1	119.8	115.9	119.3	-0.6	-2.0	-2.6	-2.0	-0.3	-3.2	97	98	95	97	0.2	0.1	0.2	0.2	10 ●	10	10	WSW 4	WSW 4	WSW 5
6	110.8	108.4	110.2	109.8	-0.8	0.6	2.4	1.2	2.6	-2.9	97	96	95	96	0.2	0.3	0.4	0.3	10 ●	10 *	10	WSW 6	WSW 5	W 5
7	117.5	122.7	123.2	121.1	0.8	1.4	1.0	1.0	3.3	0.0	92	89	94	92	0.5	0.8	0.4	0.6	0	9	4	WNW 4	WNW 3	W 2
8	122.3	123.0	121.4	122.2	2.2	2.7	2.5	2.5	3.0	0.8	96	98	95	96	0.3	0.1	0.4	0.3	10	10 ◐	10	SW 4	SW 3	SW 2
9	113.6	109.4	109.3	110.8	2.4	4.8	3.6	3.6	4.8	0.5	91	71	90	84	0.7	2.5	0.8	1.3	4	8	10 ●	SW 5	SW 8	SW 4
10	103.7	100.3	96.4	100.1	2.2	2.8	3.3	2.9	3.6	1.5	89	70	73	77	0.8	2.2	2.1	1.7	10	9	10 ●	SW 4	SSW 6	SW 11
11	97.7	92.1	91.1	93.6	2.8	6.1	7.6	6.0	8.0	2.3	86	80	75	80	1.1	1.8	2.6	1.8	2	10 ●	1	SW 7	SSW10	SSW 9
12	98.7	97.1	86.1	94.0	4.9	6.5	4.0	4.8	7.9	3.1	76	68	87	77	2.1	3.1	1.1	2.1	1	4	10 ●	SW 5	SW 6	SSW 9
13	82.5	84.3	89.2	85.3	4.0	5.3	3.8	4.2	5.6	2.9	83	56	64	68	1.3	3.9	2.9	2.7	9	9	4	SW 6	WSW 8	SW 7
14	93.9	96.3	99.2	96.5	3.2	4.4	3.0	3.4	4.7	2.0	79	69	90	79	1.6	2.6	0.8	1.7	10	9	10	SW 6	SW 6	WSW 5
15	106.2	110.6	115.0	110.6	3.2	4.2	3.6	3.6	4.2	2.7	90	84	86	87	0.8	1.3	1.1	1.1	10	9	10	WSW 4	WSW 6	WSW 3
16	115.0	112.5	109.1	112.2	0.4	3.6	4.0	3.0	4.7	-0.6	84	67	59	70	1.0	2.6	3.3	2.3	3	9	10	SW 6	WSW 7	SW 7
17	108.7	110.3	110.3	109.8	3.1	5.1	4.4	4.2	6.0	2.2	88	75	80	81	0.9	2.2	1.7	1.6	10 ●	9	9	SW 8	SW 6	SW 7
18	108.1	108.1	110.3	108.8	3.2	5.1	4.7	4.4	6.0	2.7	76	70	84	77	1.9	2.6	1.3	1.9	8	9	1	SW 7	SW 8	SW 5
19	112.6	110.6	102.5	108.6	2.6	5.3	5.5	4.7	6.4	2.0	96	84	88	89	0.3	1.4	1.1	0.9	3	9	10	SW 4	SW 4	SW 7
20	107.2	113.6	118.4	113.1	5.7	5.9	3.4	4.6	6.8	3.3	73	73	86	77	2.6	2.5	1.1	2.1	9	10	7	W 8	WSW 7	WSW 4
21	115.9	114.4	111.2	113.8	5.7	7.5	7.8	7.2	8.4	2.4	95	97	95	95	0.5	0.3	0.8	0.5	10	10 ●	10	SW 5	WSW 1	WSW 6
22	102.0	95.6	101.9	99.8	8.0	7.9	5.1	6.5	8.8	3.8	84	83	72	80	1.6	1.7	2.5	1.9	10	10 ●	9	SW 8	SW 8	WSW 7
23	105.8	106.9	110.7	107.8	3.6	5.1	3.8	4.1	5.6	2.8	76	67	87	77	1.9	2.9	1.1	2.0	9	9	9	WSW 7	WSW 8	WSW 7
24	112.2	111.5	108.4	110.7	2.2	4.2	3.0	3.1	4.7	1.2	86	85	91	87	1.1	1.2	0.7	1.0	6	10	10 ●	WSW 4	WSW 5	SW 4
25	102.6	102.6	109.3	104.8	3.4	8.2	2.9	4.4	8.4	1.8	97	92	95	95	0.3	0.9	0.4	0.5	10	9	10	S 3	SW 4	N 3
26	117.9	117.8	111.9	115.9	1.5	1.1	2.0	1.6	3.1	0.0	94	98	93	95	0.4	0.1	0.6	0.4	6 ≡	10	10 ●	C 0	W 3	SW 1
27	114.3	115.7	114.4	114.8	4.3	5.7	4.6	4.8	6.1	1.5	82	70	79	77	1.5	2.8	1.8	2.0	10	7	9	NW 3	NW 6	NW 7
28	115.8	119.6	124.1	119.8	1.3	-2.4	-2.4	-1.5	4.8	-3.6	83	89	87	86	1.1	0.5	0.7	0.8	9	9 *	7	N 6	N 8	N 8
29	128.6	131.6	134.8	131.7	-3.6	-1.3	-3.8	-3.1	-0.9	-4.1	90	80	85	85	0.5	1.1	0.7	0.8	1	9	4	N 4	NE 4	NE 1
30	137.4	139.6	140.8	139.3	-6.2	-5.4	-10.2	-8.0	-3.8	-12.6	81	72	87	80	0.7	1.1	0.4	0.7	10	0	0	ENE 3	E 1	C 0
31	137.8	136.2	131.2	135.1	-15.0	-5.4	-7.9	-9.0	-4.9	-15.4	91	75	84	83	0.2	1.0	0.5	0.6	0	0	0	C 0	WSW 1	C 0
M	111.6	112.0	112.2	111.9	1.6	2.9	1.9	2.1	4.1	-0.4	87	81	86	85	1.0	1.5	1.1	1.2	7.4	8.5	7.5	5.0	5.3	4.8

Luty - Février

1	120.8	114.9	113.2	116.3	-12.8	-5.4	-8.4	-8.8	-4.5	-14.3	85	70	80	78	0.4	1.2	0.6	0.7	0	0	0	C 0	SSE 2	SW 3
2	113.1	114.5	118.6	115.4	-4.2	-1.4	-0.2	-1.5	-0.2	-9.5	91	92	100	94	0.4	0.4	0.0	0.3	10	10	10 ≡	SW 4	WSW 4	WSW 2
3	123.1	124.2	121.9	123.1	0.6	1.2	-0.7	0.1	1.3	-0.8	96	79	90	88	0.3	1.4	0.6	0.8	10	9	4	WSW 2	WSW 3	WSW 4
4	112.3	115.7	117.6	115.2	-0.7	4.3	0.9	1.4	4.7	-1.4	95	77	90	87	0.3	1.9	0.6	0.9	10	3	4	WSW 7	W 6	WSW 3
5	106.4	97.3	103.0	102.2	0.1	1.6	3.0	1.9	4.6	-0.5	98	100	88	95	0.2	0.0	0.9	0.4	10 *	10 ●	10 ●	SW 8	SW 8	W 7
6	112.4	116.0	117.7	115.4	3.3	5.7	2.2	3.4	6.1	1.7	79	74	89	81	1.5	2.4	0.8	1.6	6	6	0	NW 7	WNW 6	SW 4
7	112.8	110.5	106.7	110.0	3.4	5.2	6.1	5.2	6.6	1.8	97	92	85	91	0.3	0.7	1.4	0.8	10 ●	10	10	SW 4	SW 5	SW 5
8	105.4	108.3	111.6	108.4	4.0	7.5	5.1	5.4	8.1	3.1	92	80	90	87	0.6	2.1	0.9	1.2	10	7	10	SW 4	WSW 4	W 2
9	119.2	125.0	129.7	124.6	1.7	5.0	0.6	2.0	5.4	-0.6	87	63	78	76	0.9	3.3	1.4	1.9	10	6	0	NW 3	NNW 3	C 0
10	129.3	127.1	124.6	127.0	0.8	4.2	3.8	3.2	4.7	-1.4	88	74	90	84	0.8	2.1	0.8	1.2	10	10	10	WSW 4	WSW 5	SW 4
11	118.7	122.3	123.4	121.5	4.0	5.0	2.2	3.4	5.6	1.8	95	66	77	79	0.4	3.0	1.7	1.7	10 ●	9	0	SW 6	WNW 7	WSW 6
12	97.9	83.4	79.0	86.8	0.5	7.3	3.8	3.8	7.7	-0.1	100	84	78	87	0.0	1.6	1.7	1.1	10 *	10 ●	8	SW 11	WSW14	W 12
13	82.2	83.3	85.6	83.7	1.8	4.8	-0.4	1.4	5.4	-0.6	78	49	92	73	1.6	4.4	0.5	2.2	6	4	4	W 8	NW 4	WSW 3
14	90.0	95.3	105.0	96.8	-1.8	0.6	-1.4	-1.0	1.2	-2.4	94	72	86	84	0.3	1.8	0.8	1.0	2	4	8	W 3	N 7	N 6
15	114.6	119.1	118.3	117.3	-2.6	-2.1	-4.1	-3.2	-1.2	-4.4	85	66	68	73	0.8	1.7	1.4	1.3	7	7	9	N 6	N 5	WSW 5
16	94.2	84.9	82.0	87.0	1.2	5.0	3.2	3.2	5.8	-4.2	94	92	73	86	0.4	0.7	2.1	1.1	10 ● *	10 ●	9	SW 9	WSW 9	W 12
17	84.0	92.0	102.5	92.8	4.0	4.4	3.4	3.8	4.8	0.8	70	65	53	63	2.4	3.0	3.6	3.0	10	10 *	9	WNW12	NW 14	NNW14
18	113.4	118.8	121.3	117.8	0.6	3.2	1.4	1.6	3.6	0.3	61	50	69	60	2.5	3.9	2.2	2.9	1	3	9	NNW 8	NNW 9	NW 2
19	116.2	116.7	118.2	117.0	3.6	5.7	5.5	5.1	6.4	0.0	95	94	84	91	0.4	0.6	1.4	0.8	10 ●	10 ●	10	W 2	NW 5	W 4
20	117.8	117.4	120.5	118.6	3.8	6.3	4.3	4.7	7.5	3.6	87	85	79	84	1.1	1.4	1.8	1.4	4	10 ◐	0	W 5	WNW 6	NW 7
21	129.9	130.4	134.7	130.3	1.6	0.4	0.2	0.6	4.4	-0.7	69	77	73	73	2.2	1.4	1.7	1.8	7	9	10 *	N 7	NNE 7	NNE 7
22	136.0	136.9	139.0	137.3	-0.6	-0.6	-1.8	-1.2	0.2	-2.7	74	70	73	72	1.5	1.8	1.4	1.6	10 *	8	9	NE 6	NE 6	NE 5
23	138.4	135.7	131.5	135.2	-0.7	1.2	-0.1	0.1	1.4	-2.8	83	68	82	78	1.0	2.2	1.1	1.4	9	9	6	NNE 3	NNE 5	N 5
24	125.2	123.6	125.0	124.6	1.0	0.6	-3.2	-1.2	1.5	-3.5	79	70	66	72	1.4	1.9	1.6	1.6	10	9	6	NNE 7	NE 6	ENE 9
25	125.1	125.4	126.1	125.5	-5.2	-4.3	-4.3	-4.5	-3.2	-5.6	80	68	75	74	0.8	1.4	1.1	1.1	6	10 *	10	E 6	E 7	E 6
26	124.4	123.6	122.5	123.5	-5.6	-1.1	-1.2	-1.8	-0.6	-4.9	90	73	70	78	0.5	1.6	1.7	1.3	10 *	10 *	10	ENE 5	E 5	E 4
27	121.4	120.2	119.2	120.3	-2.0	-0.8	-1.2	-1.3	-0.3	-2.4	81	77	72	77	1.0	1.3	1.6	1.3	10	10	10	ENE 6	E 6	ENE 5
28	115.8	114.2	113.1	114.4	-5.6	0.4	-2.3	-2.0	1.6	-5.8	87	66	87	80	0.6	2.1	0.7	1.1	10	8	3	ENE 4	E 4	NE 2
29																								
30																								
31																								
M	114.1	114.2	115.4	114.6	-0.1	2.3	0.6	0.8	3.2	-1.9	86	75	80	80	0.9	1.8	1.3	1.3	8.1	7.9	6.7	5.6	6.1	5.3

Szczecin-Dąbie $H_s = 1m$. $H_k = 6,9m$ $h_w = 20m$ Styczeń - Janvier 1962

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	0.1	.	♈°7^{16}..8^{38}, 11^{05-10}, ≫5^{10}-14^{30}
2	8	0.0	.	
3	5	0.3	.	⚲°6^{50}-10^{40} ♀°-14^{40}. = 14^{40}-24, ~7^{10}-11^{30}
4	4	0.0	.	♦°8^{01}-9^{10}..14^{20} ⚲°18^{45}-24, = 0^{00}-24, ~18^{50}-24
5	6	0.3	.	⚲°0^{00}-3^{40}, 6^{20}..11^{40}..12^{10} △°22^{10}-23^{15} ↔ -24, = 0^{00}-24, ~0^{00}-24
6	4	4.7	.	→ 0^{00}-1^{20} △°5^{40}-6^{50} ♈°7^{35}, 8^{10}-9^{30} ♐°-12^{40} ✱°-14^{35} ✱°-15^{30} ♐°-17^{00}, = 0^{00}-22^{30} ~ 0^{00}-12^{40}
7	7	1.6	.	♦°22^{50}..24
8	5	0.0	.	♦°0^{00}-2^{50} ♀°-4^{40}, 7^{10}..9^{05} 11^{45}..14^{40}, = 4^{40}-24
9	7	0.1	.	♦°17^{15}..21^{40}, = 0^{00}-11^{15}, 21^{40}-24
10	7	0.1	.	♦°4^{50}-6^{05}, 20^{35}..23^{15}-24, ≫16^{10}-23^{10}, = 0^{00}-7^{30}
11	7	0.2	.	♦°0^{00}-0^{40}, 1^{45} 10^{40}..14^{30}-15^{35}, ≫12^{30}-18^{40}, = 4^{15}-8^{10}
12	8	1.8	.	♦°18^{50}-21^{40}..22^{15}
13	8	.	.	♦°2^{40}-3^{20}
14	7	0.0	.	
15	7	0.0	.	♦°3^{45}..4^{25} ♈°6^{04-07}, 7^{09-13}
16	7	3.4	.	
17	6	0.0	.	♦°1^{00}-9^{15}, = 9^{15}-24
18	7	0.0	.	♦°0^{40}-2^{20}, 14^{42}..17^{25}, = 0^{00}-8^{30} ∞ 11^{30}-14^{45}, 16^{15}-24
19	6	0.8	.	♦°18^{30}..20^{45}, = 0^{00}-16^{30}
20	8	0.0	.	♈°8^{05-25}, ♋ 20^{50}-22^{50}
21	5	3.8	.	♦°2^{50}..3^{20} 4^{10}-6^{40}, 12^{20}-15^{40} 19^{15}-20^{35} 23^{50}..24, = 3^{20}-24
22	7	1.1	.	♦°0^{00}..1^{45}, 9^{35}-12^{30}..13^{15} ♈°15^{02-20}, 16^{20-27}, 22^{55}-23^{10}, ≫13^{20}-19^{15}, = 0^{00}-7^{15}
23	8	0.8	.	♈°13^{45}..16^{16}, 21^{28}..23^{08}
24	7	2.0	.	♦°18^{10}-21^{40}..24
25	7	3.3	.	♦°0^{00}..2^{50}-5^{40} ♦°-7^{50}..8^{50} ♈°12^{20}..15^{10}-17^{40} = 5^{40}-9^{40} 19^{30}-24
26	3	1.4	.	♦°16^{40}..17^{10}-22^{20}..23^{35}-24, = 0^{00}-9^{15} = °-13^{07} = -13^{40}, 16^{20}-24
27	7	1.6	.	♦°0^{00}-1^{40} ♈°14^{03-38} 15^{07-15}, = 0^{00}-7^{30}
28	8	0.3	.	♈°4^{40}-6^{20} ✱°-9^{49}..16^{04} ♈°18^{32}..24
29	8	0.0	1	♈°-0^{00}..10^{03} ✱ 10^{12-54}
30	8	.	2	= 17^{10}-24
31	7	.	2	= 0^{00}-9^{30}
Σ	—	27.7	—	UWAGI

Luty - Février

1	6	0.0	2	= 9^{30}-13^{30} ∞ -19^{30}
2	4	.	2	✱°0^{40}-3^{30}, 4^{30}-5^{30}, = 4^{30}-19^{28} = °-20^{15} = °-22^{45} = -24
3	7	0.3	2	= 0^{00}-9^{30}
4	7	0.0	2	✱°4^{15}..5^{30}-6^{20}..7^{00}, = 7^{00}-11^{35}
5	6	3.7	1	✱°-6^{40}-8^{05}..10^{10}-11^{15} ✱°-12^{10} ♐°-14^{40}, 18^{10}..24, = 3^{15}-13^{20}
6	8	0.8	.	♦°0^{00}..40
7	6	0.0	.	♦°0^{45}..2^{30}-4^{25} 6^{48}-7^{35}, 14^{05}..17^{15}, = 4^{25}-24
8	7	0.1	.	♈°14^{45}-15^{00}, = 0^{00}-12^{35} 17^{10}-24
9	8	.	.	= 0^{00}-8^{15}
10	7	2.0	.	♦°14^{15}-15^{20}, 16^{10}-17^{30}..18^{10}, = 15^{20}-24
11	8	2.1	.	♦°0^{50}..2^{45}, 4^{40}..5^{50} ♦°-7^{45} ♈°9^{02-15}, 10^{35-37}, = 0^{00}-7^{45}
12	8	12.7	2	✱°3^{30}-8^{40} ✱°-9^{20} ♐°-12^{10}..14^{00} ♐°-15^{50} ✱°-16^{25} ♈°18^{44-53}, 19^{39-55}, ☾15^{13}, ≫6^{15}-24
13	8	0.0	.	♈°6^{22-26} ♈°8^{25-42}, ≫0^{00}-4^{30}
14	8	0.5	.	♈°7^{45}-8^{20}, 14^{43}..16^{13}, 22^{10-18}, 23^{02-20}
15	8	2.4	1	♈°0^{55}-2^{10} ✱°..3^{20} 7^{13}-8^{20} ♈°8^{28}-9^{10} 9^{25}-11^{20}, ⊕14^{30}-17^{00} ♋ 19^{30}-22^{30}
16	5	4.5	4	✱°-0^{40}-6^{20} ✱°-7^{15} ♐°-13^{40} ✱°-14^{30} ♈°-16^{03-25}, ≫17^{50}-24
17	8	2.3	.	♦°0^{10}..2^{40} ♈°7^{40-50}, 11^{52-55} ♈°-12^{06}..56 ♈°-17^{40}, ≫0^{00}-24
18	8	8.0	.	✱°22^{35}-23^{30}..24, ≫0^{00}-1^{20} 10^{20}-12^{05}
19	6	1.9	.	✱°0^{00}..0^{25}-2^{17} ✱°-3^{00} ♐°-17^{15} 23^{40}..24
20	5	0.0	.	♦°0^{00}..2^{15} ♐°12^{45}-13^{30}..14^{35}
21	8	0.0	.	♈°12^{45}..15^{10} ✱°-16^{40}, 20^{45}..24
22	8	0.0	.	✱°-0^{00} 9^{50} ♈°-..17^{16}
23	8	0.0	.	✱°0^{35}..1^{50} ♈°-11^{16} ♈ 13^{40-48} ♈ 15^{05-10}, 15^{50}-16^{00}
24	8	0.0	.	♈°-9^{40}..16^{35} ♈°23^{50}-24
25	7	0.0	.	♈°0^{00-10} 7^{10}-8^{00} ✱°8^{00}..15^{15}
26	7	0.0	.	✱°5^{40}-13^{10}, 23^{40}..24
27	7	0.0	.	✱°0^{00}..4^{35}, 22^{05}..24, = 2^{10}-6^{25}
28	7	.	.	✱°0^{00}..5^{40}
29				
30				
31				
Σ	—	43.5	—	UWAGI

Szczecin-Dąbie φ = 53°24' λ = 14°37' Marzec-Mars 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	112.1	111.5	109.1	110.8	-5.0	-5.3	-5.0	-5.6	-1.5	-6.1	85	79	79	81	0.6	1.0	1.0	0.9	10	9	10	ENE 1	NNE 2	C 0
2	104.3	103.4	102.7	103.5	-4.0	-0.8	-1.1	-1.8	-0.3	-5.4	91	69	75	78	0.4	1.8	1.4	1.2	10	9	10	C 0	SW 2	C 0
3	101.6	101.7	100.9	101.4	-1.2	2.7	-1.8	-0.5	3.6	-2.4	91	63	87	80	0.5	2.7	0.8	1.3	10	4	10	SW 4	SW 4	C 0
4	97.8	96.4	96.3	96.8	-1.2	1.2	-0.3	-0.2	1.4	-2.0	95	85	86	89	0.3	1.1	0.9	0.8	10 *	10	10	C 0	NNE 2	NE 4
5	98.1	97.7	97.8	97.9	-0.2	-0.4	-2.3	-1.3	0.1	-2.6	80	88	96	88	1.2	0.7	0.3	0.7	10 *	10 *	10 *	NE 4	ENE 5	ENE 4
6	100.4	107.9	115.8	108.0	-0.8	0.2	-3.0	-1.6	0.3	-3.5	95	75	79	83	0.3	1.5	1.0	0.9	10 *	9	9	NNE 7	N 6	NW 3
7	120.7	122.8	125.5	123.0	-4.0	2.0	-1.7	-1.4	3.1	-7.1	87	69	88	81	0.6	2.2	0.7	1.2	9	2	0	WSW 2	WNW 3	W 1
8	126.4	127.4	126.0	126.6	-5.1	3.8	-3.4	-2.0	4.4	-5.4	93	60	88	80	0.3	3.2	0.6	1.4	0	1	0	W 3	WSW 1	C 0
9	122.4	118.5	112.5	117.8	-3.0	2.6	1.8	0.8	3.2	-6.2	79	62	68	70	1.0	2.9	2.3	2.1	7	8	9	ESE 9	SE 12	SE 8
10	108.1	107.2	105.3	106.9	0.8	4.8	3.3	3.0	4.8	0.1	78	56	79	71	1.4	3.8	1.5	2.2	9	9	10	S 6	SSW 5	S 3
11	103.1	103.8	102.7	103.2	3.4	5.0	3.8	4.0	6.4	2.8	86	90	97	91	1.1	0.8	0.3	0.7	10	10 ●,	10 ≡	SW 2	WSW 2	C 0
12	99.3	98.3	103.2	100.3	1.1	0.2	-2.3	-0.8	4.1	-2.8	100	98	91	96	0.0	0.1	0.5	0.2	10 ●	10 *	10 *	NW 3	NNE 4	N 8
13	108.0	110.5	112.9	110.5	-5.0	-2.1	-4.8	-4.2	-1.4	-5.6	88	62	66	72	0.5	2.0	1.4	1.3	9 *	6	1	WNW 4	NNW 4	WNW 3
14	116.7	117.6	115.7	116.7	-7.0	-0.8	-1.3	-2.6	0.1	-7.5	88	63	62	71	0.4	2.1	2.1	1.5	0	9	10	NW 2	SW 6	S 7
15	114.7	115.8	119.5	116.7	-2.2	2.2	-1.1	-0.6	2.4	-3.0	76	60	97	78	1.2	2.9	0.2	1.4	9	6	10 *	SW 4	SW 3	C 0
16	124.8	125.9	126.0	125.6	-6.8	0.1	-1.4	-2.4	0.9	-10.1	91	77	86	85	0.3	1.5	0.8	0.9	7	6	9	SE 2	NE 1	NNE 2
17	123.0	121.2	121.7	122.0	-0.8	2.0	-0.8	-0.1	2.3	-2.2	93	71	90	85	0.4	2.1	0.6	1.0	10	10	10	N 1	N 4	N 4
18	120.7	121.0	120.7	120.8	-3.7	3.4	-1.9	-1.0	3.6	-4.1	94	45	75	71	0.3	4.3	1.3	2.0	2	4	0	W 2	N 4	C 0
19	120.0	119.6	118.8	119.5	-4.9	2.0	-0.9	-1.2	2.8	-7.2	88	58	81	76	0.5	3.0	1.1	1.5	3	7 *	7	C 0	W 1	C 0
20	117.0	116.4	115.3	116.2	-0.4	3.8	2.4	2.0	4.6	-1.9	72	48	48	56	1.6	4.2	3.8	3.2	7	8	10	SW 4	SW 7	S 4
21	115.1	114.2	113.4	114.2	-1.8	5.3	-1.6	0.1	5.5	-2.1	89	47	78	71	0.6	4.7	1.2	2.2	7	1	0	ESE 2	SSE 3	SE 2
22	112.2	111.4	109.9	111.2	-4.6	3.5	-1.6	-1.1	4.7	-6.2	91	46	74	70	0.4	4.2	1.4	2.0	1	0	0	SE 2	C 0	SE 1
23	109.8	110.8	112.6	111.1	-5.4	4.6	-1.0	-0.7	5.1	-6.7	85	44	81	70	0.6	4.8	1.1	2.2	2	2	0	C 0	NE 3	NE 2
24	116.2	117.5	119.8	117.8	-5.6	2.7	-1.7	-1.6	3.6	-6.8	92	47	80	73	0.3	3.9	1.1	1.8	1	3	2	C 0	NE 2	NNE 1
25	120.6	120.2	118.4	119.7	-3.7	4.0	-0.2	0.0	5.4	-6.6	94	55	76	75	0.3	3.7	1.4	1.8	0	4	9	C 0	W 4	W 1
26	115.2	112.1	108.0	111.8	-3.8	7.1	2.2	1.9	7.7	-4.7	90	40	54	61	0.4	6.0	3.3	3.2	0	3	0	C 0	S 7	S 6
27	103.0	101.3	99.2	101.2	-0.8	5.3	1.0	1.6	6.6	-1.4	55	44	85	61	2.7	5.0	1.0	2.9	6	7	10	SE 5	SE 7	SSE 8
28	97.5	100.3	106.1	101.3	2.2	3.6	1.1	2.0	3.7	0.2	95	90	83	89	0.4	0.8	1.1	0.8	10 ●	10	10	SW 3	WNW 3	NW 2
29	105.9	102.3	95.6	101.3	-0.6	5.7	5.0	3.8	7.0	-1.4	96	67	72	78	0.2	3.1	2.4	1.9	9	6	10	C 0	SE 4	SE 4
30	90.4	90.6	86.5	89.2	6.7	13.0	11.4	10.6	13.7	3.5	94	64	72	77	0.6	5.4	3.8	3.3	10	9	9	SW 5	WSW 4	S 3
31	80.5	89.0	94.4	88.0	10.0	8.9	5.2	7.3	11.6	4.2	95	58	69	74	0.7	4.8	2.7	2.7	10 ●	8	4	SW 4	WNW 7	SW 1
M	109.9	110.1	110.1	110.0	-1.9	3.0	0.0	0.3	3.9	-5.6	88	64	79	77	0.6	2.9	1.4	1.6	6.7	6.5	6.7	2.6	3.9	2.6

Kwiecień-Avril

1	100.6	102.4	104.2	102.4	2.8	6.0	2.2	3.3	9.5	0.8	89	66	86	80	0.8	3.3	1.1	1.7	9	6	0	SW 4	W 7	WSW 6
2	103.3	105.3	108.5	105.7	2.4	7.5	4.6	4.8	8.5	1.4	93	63	76	77	0.6	3.9	2.1	2.2	7	9	0	SW 6	W 7	WSW 5
3	104.5	100.7	96.9	100.7	6.7	13.9	13.0	11.6	15.4	4.2	82	41	46	56	1.7	9.4	8.1	6.4	10	2	0	SW 7	WSW 9	SW 6
4	94.6	94.5	91.6	93.6	9.5	11.9	5.5	8.1	13.5	5.5	71	59	91	74	3.4	5.7	0.8	3.3	10	10	8	SW 5	SSW 3	SW 2
5	86.6	85.1	87.6	86.4	2.3	12.9	6.5	7.0	13.6	0.4	98	39	96	78	0.1	9.1	0.5	3.2	0 ≡	6	4	SE 3	SSE 4	C 0
6	91.7	96.2	105.3	97.7	2.2	7.5	4.6	4.7	7.8	0.0	100	87	85	91	0.0	1.4	1.3	0.9	10 ≡	10	8	C 0	NW 1	NNW 3
7	110.7	109.3	103.3	107.8	2.6	7.8	4.7	5.0	9.9	1.3	84	50	87	74	1.2	5.4	1.1	2.6	7	8	10 ●	WNW 3	W 5	SW 7
8	100.1	100.1	99.4	99.9	8.3	9.9	8.6	8.8	11.8	4.0	96	81	90	89	0.5	2.4	1.1	1.3	10 ●	10	10 ●	SW 6	SW 7	SW 7
9	104.2	108.0	112.4	108.2	5.9	9.2	4.9	6.2	10.4	2.5	77	55	70	67	2.1	5.2	2.6	3.3	4	7	0	SW 7	WSW 7	SW 1
10	117.1	118.6	119.1	118.3	3.2	8.9	7.3	6.7	10.2	1.8	93	64	50	69	0.5	4.1	5.1	3.2	9	8	4	SW 4	W 4	SSW 4
11	121.6	120.3	118.5	120.1	4.0	12.4	9.4	8.8	13.7	1.7	85	43	51	60	1.2	8.2	5.7	5.0	0	5	1	SW 1	SW 6	SW 3
12	116.1	115.5	115.1	115.6	6.3	9.3	6.1	7.0	9.5	5.1	63	81	94	79	3.5	2.2	0.6	2.1	7	10 ●	9	SW 5	SW 4	C 0
13	115.3	114.7	114.1	114.7	3.4	7.8	4.6	5.1	8.7	2.4	86	55	92	78	1.1	4.8	0.7	2.2	10	7	9	W 3	W 4	C 0
14	116.5	121.1	126.1	121.2	3.2	7.1	3.9	4.5	8.9	2.0	97	69	87	84	0.3	3.2	1.1	1.5	9	10	10 ●	SW 2	NE 5	NE 7
15	127.2	125.6	124.9	125.9	4.1	7.9	6.7	6.4	8.2	3.4	85	75	82	81	1.2	2.6	1.7	1.8	9	10	10	ENE 5	ENE 5	ENE 4
16	122.2	118.0	118.4	119.5	7.5	16.9	7.3	9.8	19.1	6.5	87	51	94	77	1.4	9.4	0.6	3.8	10	9	10 ●	E 5	E 6	ENE 3
17	119.6	115.2	112.5	115.8	5.2	15.3	12.9	11.6	19.5	2.3	98	69	76	81	0.1	5.5	3.6	3.1	9	10	7	SE 2	SE 4	SE 5
18	111.1	110.0	109.9	110.3	10.8	20.1	15.7	14.6	20.6	8.7	82	50	81	71	2.3	11.6	3.0	5.6	9	9	9	SE 5	SE 4	SE 2
19	110.7	111.8	115.1	112.5	11.1	21.3	12.1	14.2	23.3	9.3	89	48	80	72	1.5	13.3	2.8	5.9	10	10	10	ESE 1	SW 3	C 0
20	119.1	119.4	116.9	118.5	5.1	7.6	7.6	7.0	12.1	4.8	98	87	93	93	0.2	1.3	0.7	0.7	10	10	9	NNW 2	N 3	N 1
21	116.6	118.9	120.3	118.6	6.8	15.1	10.5	10.7	17.5	5.4	100	71	91	87	0.0	5.0	1.1	2.0	10 ≡	6	4	NE 2	NE 3	NNE 3
22	119.8	117.6	116.5	118.0	5.5	22.6	17.9	16.0	26.1	4.6	100	54	66	73	0.0	12.7	7.1	6.6	10 ≡	4	3	NE 3	SE 4	SE 3
23	120.1	121.3	122.4	121.3	8.7	13.3	6.4	8.7	18.0	6.2	96	70	93	87	0.4	4.7	0.4	1.8	10	2	10	N 3	N 4	NNE 4
24	123.5	123.6	124.5	124.0	8.0	23.7	15.4	15.6	25.5	6.4	87	39	76	67	1.3	17.8	4.3	7.8	0	0	0	ENE 4	E 4	E 2
25	125.5	124.8	123.8	124.7	12.5	25.2	14.5	16.7	27.9	11.2	85	51	84	73	2.2	15.8	2.7	6.9	2	0	0	E 2	E 2	N 1
26	122.7	119.8	113.5	118.7	11.3	15.7	13.5	13.5	19.2	10.3	86	66	63	72	1.8	6.0	5.7	4.3	9	2	10	NW 3	NW 2	C 0
27	112.2	114.5	110.2	112.3	7.3	12.2	9.5	9.6	14.5	6.6	91	51	61	68	0.9	7.0	4.6	4.2	10 ●	6	3	NW 5	NNW 7	W 3
28	104.0	105.6	108.4	106.0	7.8	10.7	6.7	8.0	12.3	6.3	76	50	74	67	2.5	6.4	2.6	3.8	9	6	6	N 6	N 7	N 3
29	108.3	107.6	107.4	107.8	3.3	9.9	4.9	6.2	11.4	3.2	87	50	78	72	1.1	6.1	2.0	3.1	7	9	9 ●	WNW 4	N 7	NE 5
30	111.3	113.5	115.4	113.4	3.5	7.8	3.4	4.5	8.3	1.6	68	43	85	65	2.5	6.0	1.2	3.2	1	3	10 ●	NE 6	NNE 5	N 3
31																								
M	111.9	112.0	112.1	112.0	6.1	12.6	8.3	8.8	14.5	4.3	88	59	79	75	1.2	6.6	2.5	3.4	7.6	6.9	6.1	3.8	4.8	3.2

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU s	POGODA
1	7	0.0	•	△°0^05-10^15; =6^30-12^30; 17^30-24
2	7	0.2	•	=0^00-10^40
3	6	0.0	1	*°0^50...3^10-5^10; =5^10-24
4	6	0.4	•	*°3^35...6^05 *°-1-11^40; =0^00-24
5	6	9.2	•	*°6^15...9^40 △°-11^30 *°-1...12^10-24; =0^00-24
6	7	0.7	12	*°0^00-1^50; 5^45...6^30-12^05; =0^00-12^05
7	7	•	15	=18^50-24
8	7	•	11	=0^00-5^50; 18^15-24
9	8	•	6	⚡7^15-18^30; =0^00-5^20; ⊕8^05-10^20
10	8	0.0	4	•°15^05...17^40
11	5	1.3	pł.	•°7^10...10^40 •°11^42-13^40 •°18^50...19^35; =4^30-20^50 ≡°-1-24
12	5	10.0	•	•°4^45-11^05 *°-11^15 *°-1-20^40...24; =°0^00-4^45 =-10^10; 17^15-24
13	8	0.0	8	*°-1 0^00...4^10-6^15...7^20 ⚥° 7^40...15^42; =0^00-7^10
14	8	0.0	7	*°22^45-23^30...24
15	7	2.0	4	*°0^00...2^15 7^35-8^15 ⚥°-1 14^10-16^05 18^05...21^40 *°23^50...24
16	6	•	8	*°0^00...1^40; =1^40-6^30; 9^20-24; ⊖22^25-23^15
17	8	•	4	=0^00-8^20; ⊕12^45-16^15 ⊖18^30-24
18	8	•	4	=3^30-8^45 ≈°-9^30 =-10^30; 21^30-24; ⊖0^00-2^30
19	8	0.0	•	⚥°12^50...16^35; =0^00-1^30; ⌴°3^00-10^00
20	8	•	•	
21	7	•	•	=0^20-10^30 ∞-19^30 =-21^20
22	7	•	•	=4^45-6^30; ⌴°1^00-9^00
23	8	•	•	=1^00-9^50; ⌴°1^00-9^00
24	8	•	•	=3^50-8^50; 18^25-24; ⌴°1^00-9^00
25	7	•	•	=0^00-9^30 ∞-13^30; ⌴°1^00-8^00
26	7	•	•	
27	8	1.6	•	*'17^50-18^20 ⚥°20^35-20^40
28	6	0.4	•	•°1^29...3^30-5^45...8^35 *°14^40-15^40; =8^35-9^30; 12^20-24
29	7	1.8	•	•°21^35-24; =0^00-8^30
30	8	0.4	•	•°0^00-4^20; 22^25...23^10-24; =4^20-9^15
31	8	2.9	•	•°0^00-3^35...5^15; 6^40...7^12-10^15; =6^20-9^30
Σ	—	30.9	—	UWAGI

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1	8	1.9	•	⚥°7^25-28 9^35-40; 11^15-20 •▲'11^35-37 ⚥°-11^40 ⚥°18^25-35
2	8	2.3	•	⚥°5^35-36; 10^45-49 ⚥° 12^49-53 ⚥° 15^40-45; 17^15-20 •°23^40...24
3	8	•	•	•°0^00...2^30-5^40
4	8	1.7	•	⚥° 7^12-19 ⚥°-1 14^10...20^12; ∩17^42-18^04
5	8	2.1	•	⚥°14^25-30; 15^40-16^35; =4^30-5^45 ≈°-7^45 =-8^20 =-23^45 ≡°-24
6	6	0.0	•	•°19^40...20^20; ≡°-2 0^00-9^40 =-13^30
7	8	3.7	•	⚥°11^35-39 ⚥° 12^45...13^25 •°18^45-22^15; 23^30-24
8	7	0.7	•	•°0^00...11^15; 16^10...20^15-21^25; =2^50-11^15
9	8	1.0	•	•°8^45...10^40 ⚥° 17^15-20 ▲°-17^22
10	8	0.2	•	⚥°9^30-40; 9^45-10^05; 12^18-25
11	8	•	•	
12	6	1.3	•	•°9^05...15^20; 16^40...18^15-19^40; =9^20-24
13	8	0.0	•	⚥°13^45-47; 16^10-15; =0^00-6^20
14	8	0.1	•	⚥° 7^25-35 •°8^15...10^35; 20^45...22^40
15	8	0.0	•	•°14^25...15^15
16	7	12.6	•	⚥°-1 17^42-19^15 •°-20^15...22^20; ⚡16^15-18^15; ⊕10^30-14^30
17	7	•	•	=4^30-9^30
18	8	•	•	
19	8	•	•	=18^30-24; ⊕12^20-45
20	7	0.3	•	=0^00-12^30; 19^30-24; △°21^00-24
21	7	•	•	•°2^40-3^20; =0^00-6^50 ≡°-7^50 =-10^20; 19^30-24; △°19^00-24
22	7	•	•	=0^00-5^50 ≈°-8^40 =-9^30; △°-1 0^00-9^00 △°22^00-24
23	8	•	•	=5^30-10^15; 18^30-24; △°0^00-8^00
24	7	•	•	=0^00-6^40; 19^30-21^30; △°1^00-8^00; 22^00-24
25	7	•	•	=20^30-24; △°0^00-8^00; 20^00-24
26	6	0.3	•	•°21^30-22^20; =0^00-14^30; △°0^00-9^00
27	8	0.0	•	•°4^40-5^45; 6^35...7^20 8^40...9^25
28	8	•	•	⚥°2^40-48; △°21^00-24
29	8	0.7	•	⚥°7^33-39 ⚥ ▲°9^17-20 ⚥°9^42-49; 16^03-15; 20^50-21^05; 22^40-23^10; 23^45-24; △°0^00-7^35
30	8	0.1	•	⚥°0^00...1^45; 20^40...22^45
31				
Σ	—	29.0	—	UWAGI

Szczecin - Dąbie φ = 53°24' λ = 14°37' Maj - Mai 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	112.5	110.0	105.4	109.3	3.4	5.7	4.2	4.4	8.5	0.0	70	64	88	74	2.4	3.4	0.9	2.2	9	10	10 ●	NW 1	NW 5	S 2
2	105.7	106.1	107.8	106.5	2.0	8.5	1.8	3.5	9.2	0.8	98	47	74	73	0.2	5.9	1.8	2.6	9	9	0	C 0	NW 1	C 0
3	106.8	106.4	104.9	106.0	5.0	5.5	5.7	5.5	8.8	-0.5	84	88	91	88	1.4	1.1	0.9	1.1	9	10 ●	9 ●	WSW 2	W 5	WSW 4
4	105.3	106.8	108.2	106.8	6.3	10.1	5.6	6.9	10.7	5.4	88	48	80	72	1.1	6.5	1.8	3.1	2	6	7	N 1	NNE 3	C 0
5	110.3	111.9	114.4	112.2	4.2	9.9	5.3	6.2	11.4	0.4	88	57	75	73	0.9	5.2	2.2	2.8	6	9	0	C 0	C 0	C 0
6	116.5	115.0	111.3	114.3	6.5	14.4	13.2	11.8	17.0	-1.7	84	45	64	64	1.6	9.1	5.5	5.4	1	4	10 ●	C 0	S 7	SSE 6
7	110.7	111.6	111.6	111.3	14.4	18.5	15.3	15.9	20.6	11.3	93	66	89	83	1.1	7.2	1.9	3.4	9	9	9	WSW 2	W 4	WSW 3
8	111.8	111.5	110.4	111.2	12.0	17.8	12.3	13.6	18.3	11.4	99	64	93	85	0.2	7.4	1.0	2.9	10 ≡	10	10	W 2	W 2	NE 1
9	112.3	111.5	108.0	110.6	10.4	16.1	14.3	13.8	18.9	9.1	97	72	84	84	0.3	5.1	2.5	2.6	10	9	10 ●	SW 3	WSW 1	C 0
10	104.9	106.9	108.6	106.8	13.4	16.6	10.3	12.6	17.0	10.3	81	53	80	71	3.0	8.9	2.5	4.8	4	6	6	SW 4	W 8	NW 3
11	109.5	109.4	110.1	109.7	9.5	12.6	9.0	10.0	15.2	7.8	86	57	93	79	1.7	6.3	0.8	2.9	7	10 ●R	9	WSW 6	SW 4	SE 2
12	111.5	112.6	114.0	112.7	9.6	13.7	9.7	10.7	16.1	8.6	91	65	95	84	1.2	5.5	0.6	2.4	9	8	2	SW 2	WSW 3	C 0
13	114.8	115.1	114.5	114.8	9.6	13.1	9.1	10.2	15.0	7.7	99	74	87	87	0.2	4.0	1.6	1.9	10 ●	7	4	E 1	N 3	NE 2
14	110.0	107.7	107.1	108.3	8.3	8.0	8.7	8.4	9.7	7.5	92	93	92	92	1.0	0.7	0.9	0.9	10	10	10 ●	N 4	N 7	N 6
15	106.4	107.3	109.1	107.6	8.1	11.6	10.9	10.4	13.4	7.7	91	71	66	76	0.9	3.9	4.4	3.1	10 ●	10	9	NW 6	NNW 6	NW 3
16	111.4	113.1	111.7	112.1	8.9	10.7	9.9	9.8	12.5	8.0	73	49	64	62	3.0	6.6	4.3	4.6	9	9	10	NW 5	WNW 6	WSW 4
17	109.1	107.3	109.1	108.5	10.5	15.5	8.9	11.0	16.2	8.8	80	51	92	74	2.6	8.7	0.9	4.1	7	9	5	WSW 4	WSW 3	W 3
18	112.0	113.8	115.3	113.7	8.3	12.8	9.0	9.8	16.9	5.7	89	57	83	76	1.3	6.3	2.0	3.2	9	6	4	WSW 4	W 6	C 0
19	112.1	107.6	105.0	108.2	12.0	20.9	14.7	15.6	21.0	4.2	74	40	79	64	3.6	14.7	3.4	7.2	4	8	10	C 0	S 8	WSW 3
20	107.6	110.0	113.1	110.2	11.4	14.3	9.6	11.2	14.7	9.4	79	52	86	72	2.8	7.8	1.8	4.1	8	9	6	W 4	W 6	W 2
21	115.2	113.1	110.5	112.9	8.6	17.1	12.4	12.6	17.5	6.7	90	46	62	66	1.1	10.6	5.5	5.7	2	5	1	WSW 2	WSW 3	SSE 4
22	107.1	108.4	111.9	109.1	12.3	15.1	12.5	13.1	17.0	10.0	72	71	86	76	4.0	5.0	2.1	3.7	8	8	9	S 5	WSW 6	SW 3
23	111.0	110.7	112.9	111.5	12.3	15.0	11.4	12.5	15.7	11.0	79	70	72	74	3.0	5.0	3.8	3.9	9	10	9	SW 6	SW 8	WSW 2
24	115.2	114.0	113.6	114.3	9.5	14.2	9.3	10.6	16.4	6.6	73	48	89	70	3.3	8.4	1.3	4.3	1	7	7	WSW 5	SW 6	SW 1
25	113.7	113.7	114.4	113.9	8.9	14.3	8.4	10.0	16.3	6.1	89	48	90	76	1.2	8.4	1.0	3.5	4	8	4	W 1	W 1	SE 1
26	113.9	113.0	112.7	113.2	10.0	12.9	10.0	10.7	14.2	5.9	89	67	89	82	1.3	4.9	1.3	2.5	9	10 ●	10 ●	C 0	NE 4	NE 4
27	113.1	115.3	116.1	114.8	8.7	10.2	9.3	9.4	11.3	8.5	93	82	89	88	0.7	2.2	1.3	1.4	10	10	8	N 2	WNW 1	C 0
28	116.3	115.1	112.5	114.6	10.1	15.0	11.9	12.2	15.9	2.0	87	61	76	75	1.6	6.6	3.3	3.8	2	7	10	C 0	E 1	NE 2
29	112.8	114.2	114.5	113.8	9.1	12.3	10.3	10.5	14.6	8.3	95	80	92	89	0.7	2.9	0.9	1.5	10	10	6	W 2	SW 4	WSW 2
30	114.8	116.2	115.9	115.6	9.7	9.9	8.7	9.2	13.4	7.6	87	83	86	85	1.6	2.1	1.5	1.7	3	10	9	WSW 5	NW 5	W 1
31	112.9	108.6	109.1	110.2	8.9	13.7	7.6	9.4	15.0	5.6	79	64	79	74	2.4	5.7	2.2	3.4	8	9 ●	9 ●	SW 1	SW 8	WSW 4
M	111.2	111.1	111.1	111.1	9.1	13.1	9.7	10.4	14.8	6.5	86	62	83	77	1.7	6.0	2.1	3.3	7.0	8.5	7.2	2.6	4.4	2.2

Czerwiec - Juin

1	113.2	114.9	115.7	114.6	7.9	11.5	8.7	9.2	13.9	4.0	80	62	84	75	2.0	5.2	1.8	3.0	6	9	9	W 6	NW 3	C 0
2	116.8	118.8	121.8	119.1	7.7	11.5	7.3	8.4	13.0	4.0	75	62	81	73	2.6	5.2	1.9	3.9	4	8	2	W 4	NNW 4	WNW 2
3	124.7	126.0	127.7	126.1	8.9	10.9	7.3	8.6	12.9	5.0	82	65	83	77	2.0	4.6	1.7	2.8	9	8	6	N 2	N 5	N 3
4	127.5	127.8	128.4	127.9	9.9	14.5	9.4	10.8	16.7	2.7	71	46	73	63	3.6	8.9	3.2	5.2	1	9	4	C 0	N 4	W 2
5	129.2	129.6	131.4	130.1	10.7	15.0	8.3	10.6	16.5	4.2	87	47	60	65	1.7	9.0	4.5	5.1	6	8	1	N 3	NNE 7	NNE 6
6	132.3	132.4	132.2	132.3	10.8	14.7	9.5	11.1	15.0	6.7	60	42	63	55	5.3	9.6	4.5	6.5	1	1	0	NNE 5	NNE 8	NNE 4
7	131.9	130.9	129.6	130.8	11.1	18.8	11.9	13.4	19.5	4.6	64	48	65	59	4.8	11.3	4.9	7.0	4	4	1	NNE 3	NNE 5	NNE 3
8	129.9	127.3	123.4	126.9	11.9	21.1	14.7	15.6	23.0	2.1	72	38	71	60	3.9	15.4	4.8	8.0	0	0	2	C 0	W 3	C 0
9	118.9	117.5	115.0	117.1	14.1	18.7	13.3	14.8	19.4	9.3	70	55	81	69	4.8	9.7	3.0	5.8	1	2	0	WNW 3	NW 3	C 0
10	112.8	111.0	109.1	111.0	13.7	21.1	16.1	16.8	22.0	5.9	83	49	74	69	2.7	12.8	4.7	6.7	2	6	9	W 1	W 3	C 0
11	107.7	107.5	108.7	108.0	13.0	13.8	11.7	12.6	16.2	11.0	83	63	67	71	2.6	5.9	4.5	4.3	6	9	9	W 4	WNW 5	WNW 4
12	111.2	112.9	114.3	112.8	10.1	13.7	12.3	12.1	16.3	8.2	78	63	70	70	2.7	5.9	4.3	4.3	9	9	2	WNW 3	W 5	C 0
13	116.0	115.0	112.9	114.6	13.3	19.0	14.3	15.2	21.0	7.8	68	42	70	60	5.0	12.8	5.0	7.6	1	6	9	W 2	WSW 4	S 3
14	111.0	111.0	113.8	111.9	16.0	24.3	17.3	18.7	25.8	13.5	59	41	79	60	7.5	17.8	4.1	9.8	6	4	3	S 3	W 3	N 1
15	116.1	116.3	118.0	116.8	17.5	28.6	18.9	21.0	29.4	8.8	79	41	91	70	4.2	23.0	1.9	9.7	3	4	10(R)	W 2	WSW 3	SW 4
16	117.1	117.4	117.3	117.3	18.4	21.5	18.3	19.1	23.3	14.8	94	76	97	89	1.3	6.1	0.6	2.7	8	10	9	C 0	C 0	WNW 4
17	121.2	121.7	121.6	121.5	15.5	19.3	14.2	15.8	20.6	13.7	78	56	72	69	3.9	9.9	4.6	6.1	9	4	9	NW 4	NW 2	NE 2
18	121.1	118.5	115.6	118.4	14.8	21.3	17.9	18.0	23.2	5.5	70	48	68	62	5.0	13.3	6.5	8.3	0	4	9	NE 2	N 2	E 2
19	112.4	108.8	109.2	110.1	19.2	28.2	17.6	20.6	29.4	15.5	75	48	91	71	5.6	20.0	1.8	9.1	8	3	10 ●	SE 3	SSE 6	WNW 2
20	114.2	114.4	115.1	114.6	15.5	20.9	15.8	17.0	21.9	12.7	83	44	65	64	3.0	13.8	6.2	7.7	2	8	1	WSW 3	WSW 6	WSW 2
21	116.1	117.5	119.3	117.6	15.7	20.7	17.1	17.6	23.6	13.7	67	64	71	67	5.8	8.8	5.6	6.7	10	7	3	W 4	SW 6	NE 1
22	120.4	120.2	118.4	119.7	17.1	23.7	21.5	21.0	25.6	11.0	84	59	78	74	3.2	12.1	5.6	7.0	0	3	7	SW 5	WSW 4	C 0
23	119.2	119.1	118.0	118.8	16.9	19.2	18.2	18.1	21.6	16.6	94	79	90	88	1.2	4.6	2.1	2.6	10	10	4	C 0	WNW 1	W 2
24	117.0	113.5	113.4	114.6	15.7	22.9	17.5	18.4	25.2	13.0	86	51	70	69	2.4	13.6	6.1	7.4	2	6	3	C 0	WSW 5	W 1
25	113.5	116.0	117.4	115.6	13.3	15.7	12.2	13.4	17.9	12.0	65	63	64	64	5.3	6.6	5.1	5.7	9	8	8	SW 8	WNW 8	WNW 5
26	115.4	113.3	109.2	112.6	11.7	15.1	13.7	13.6	17.0	7.3	75	56	72	68	3.4	7.7	4.4	5.2	1	10 ●	9	WSW 4	W 4	C 0
27	107.1	109.0	110.1	108.7	9.7	11.9	12.4	11.6	15.9	8.7	95	76	79	83	0.6	3.3	3.0	2.3	10 ●	10	9	W 5	WNW 7	WNW 6
28	108.6	104.8	104.8	106.1	8.3	10.7	9.7	9.6	13.1	8.2	90	87	89	89	1.1	1.7	1.2	1.3	10 ●	10	9	WSW 6	WSW 7	W 4
29	107.4	109.6	111.4	109.5	12.0	15.7	12.8	13.3	17.0	8.6	88	64	70	74	1.7	6.4	4.4	4.2	10	9	8	NW 5	NW 7	WNW 5
30	112.0	114.0	114.6	113.5	11.1	14.8	13.1	13.0	15.2	10.2	94	74	79	82	0.8	4.3	3.1	2.7	10 ●	9	9	W 4	WNW 5	C 0
31																								
M	117.4	117.2	117.2	117.3	13.0	18.0	13.8	14.6	19.7	9.0	78	57	76	70	3.3	9.6	3.8	5.6	5.3	6.6	5.8	3.1	4.5	2.3

Szczecin-Dąbie $H_s = 1m$ $H_0 = 6{,}9m$ $h_w = 20m$ Maj - Mai 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	8	3.3	•	•°13^05...24,⊕6^30-11^30
2	8	2.2	•	•°0^00-1^40 ▽°13^10-20,14^10-52,=4^40-7^20
3	7	6.2	•	▽°2^35-40 2^55-3^05 •°-4^50 •°-1 11^01-16^39 ▽°17^15-35 •°19^50-21^05,⊕8^30-9^30
4	8	0.0	•	•°1^10...4^40 ▽°15^45-52; △°22^00-24
5	8	•	•	△°0^00-9^00,20^00-24
6	8	1.6	•	•°20^05...21^30-24;=1^30-7^15; △°0^00-3^00 ⌣°na
7	7	10.2	•	•°0^00-3^40 7^40-8^20...9^35 ▽°2 22^10-40;(R)22^05-R22^20-50 W-E;=3^40-10^30,np
8	7	4.1	•	•°16^40-18^15 ▽°19^47-20^50;=0^00-50 ≍°-2-1^20 ≍°-0 7^40=-8^20,n...np ≍°23^50-24
9	7	6.2	•	▽°20^55-21^05 22^25-48; ≍°0^00-1^50 =-3^50 ≡°-1-6^40=-11^20
10	8	0.0	•	•°-2 0^05-4^20...5^15 ▽°14^30-35;(R)19^00-20^50 W-E
11	7	6.5	•	▽°-0 12^40...24;(R)12^36-R12^55-13^15 SW-NE; △°1^00-8^00
12	7	1.4	•	▽°0^00-15 •°4^10...6^20,=3^30-8^30, △°21^00-24
13	7	3.9	•	•°5^05...7^10-11^10,=2^30-11^30; △°0^00-5^00 21^00-24
14	7	5.9	•	•°14^40-18^40,19^40...20^40 •°-24; △°0^00-9^00
15	7	0.0	•	•°0^00-4^30...8^15
16	8	0.0	•	▽°10^45-47
17	8	1.6	•	•°0^20...2^10 ▽°13^45-14^46,16^50-53,17^05-26,=2^10-7^30
18	8	0.5	•	▽°17^08-30;(R)12^15-45 SW-ESE;=1^30-5^40,23^30-24; ⌒17^15-30
19	8	5.4	•	•°15^30...19^20 23^35...24;=0^00-48 ≍°-2^40=-5^30,⊕8^45-10^30
20	8	0.6	•	•°0^00...05 •°-0-3^45 ▽°18^50-19^05
21	8	0.2	•	△°1^00-9^00
22	7	0.4	•	•°3^10...5^15,8^48...11^25 ▽°13^30-34,19^17-35,=20^30-24
23	7	0.0	•	▽°3^25-35,8^15-20 •°9^40...10^20,14^43-48,=0^00-7^30
24	8	0.8	•	▽°17^10-12 ▽°19^15-25, △°1^00-4^00
25	8	•	•	=3^30-5^50; △°21^00-24
26	7	7.2	•	•°-1 11^10...14^10,17^10 •°20^40-24;=2^30-5^30,18^30-24; △°0^00-8^00
27	8	0.0	•	•°0^00...7^20,10^20...11^20 ▽°16^45-48;=23^20-24
28	8	2.6	•	=0^00-45 ≍°-3^30 ≡-5^30 ≍°-6^40=-7^30
29	7	1.1	•	•°2^00...2^35-4^35 ▽°10^46-49,14^44-56,15^04-08,20^42-21^08
30	8	0.0	•	▽°12^26-42;=7^10-11^40
31	7	0.9	•	▽°13^58-14^12,16^50...17^18,21^28-32,21^55-22^05,R°14^15
Σ	—	72.8	—	UWAGI:

Czerwiec - Juin

1	8	0.5	•	▽°10^28-32 11^02-06 ▲°11^50-53 ▽°14^47-50 ▽°16^25-30 ▽°20^02-06
2	8	1.0	•	▽°13^46-48,16^48-52,17^12-21
3	8	0.5	•	▽°-0 3^38-52 •°9^08-55,9^40-52,14^10-35
4	8	•	•	△°22^00-24
5	8	•	•	≍°2^20-3^40=-4^30; △°0^00-9^00,⊕14^10-25
6	8	•	•	△°3^00-9^00
7	8	•	•	△°1^00-8^00
8	8	•	•	△°0^00-9^00,21^00-24
9	7	•	•	△°0^00-9^00,23^00-24
10	8	0.7	•	R°22^30-23^00 W-E;=1^30-4^30,23^50-24; △°0^00-9^00
11	8	0.6	•	▽°2^00-20 11^19-30,11^38-12^10,R°2^20-3^40 W-E;=0^00-1^50
12	8	0.0	•	▽°13^48-52
13	8	•	•	△°0^00-8^00
14	7	•	•	∞11^30-19^30; △°21^00-24
15	7	10.7	•	▽°15^35-48 ▽°-1 17^23-19^15 ▽°22^05-23^10;(R)17^05-R17^25-19^25 W-E;21^50-22^40 W-E;=1^38-8^30; △°0^00-9^00
16	7	1.7	•	•°9^50...10^10 ▽°-1 10^15-11^10 •°18^40-20^35,R°10^15-11^02 W-E;=1^10-2^15 ≍°-4^30 ≡-0-5^30=-13^30,17^30-23^30
17	8	•	•	=2^30-4^30; △°0^00-8^00,23^00-24
18	8	•	•	≍°2^20-3^15 =-5^35; △°0^00-9^00
19	7	7.8	•	▽°-1 19^05-20^05 ▽°21^35-22^25,23^54-24,R19^15-45 SW-NE
20	8	0.0	•	▽°0^00-08 0^32-37
21	7	•	•	▽°7^34-37; △°23^00-24
22	7	2.7	•	=7^15-9^30; △°0^00-9^00
23	7	0.0	•	▽°-0 2^45-3^25 ▽°4^45-5^15,13^42-48 •°14^05...45;=7^30-10^20; △°na,np
24	8	•	•	=1^30-6^40; △°-1 0^00-10^00
25	8	0.0	•	▽12^03-04 14^30-32 15^15-19,16^13-15
26	8	8.3	•	•°13^48...15^10 23^25...24
27	8	4.4	•	•°-1 0^00...0^30-1^07...2^48 ▽°6^42-7^24 •°-7^38 •°-13^20
28	7	6.9	•	•°5^45-9^05,10^10...11^30-13^30...15^15 ▽°-1 15^46...18^20 ▽°20^15-43,R°16^03-35 W-E
29	8	0.6	•	▽°7^07-20 8^05-08
30	7	0.0	•	•°1^50...8^10;=8^10-11^30
31				
Σ	—	46.4	—	UWAGI:

Szczecin-Dąbie φ=53°24' λ=14°37' Lipiec-Juillet 1962

DNI	CIŚNIENIE P=900+ I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	114.4	114.9	113.9	114.4	10.7	12.5	11.6	11.6	15.6	9.9	82	86	95	88	2.3	2.1	0.6	1.7	10	10	8	W 4	W 4	C 0
2	112.6	110.5	106.0	109.7	10.4	14.1	10.6	11.4	14.4	8.7	91	81	92	88	1.1	3.1	1.0	1.7	10	10 ●	10	W 4	W 5	WNW 1
3	100.3	97.8	96.2	98.1	10.9	13.1	9.1	10.6	14.3	9.0	81	67	89	79	2.4	5.0	1.3	2.9	8	9	6	W 5	W 7	SW 6
4	91.0	95.7	98.2	94.3	9.1	13.4	10.7	11.0	15.6	8.2	96	70	92	86	0.5	4.7	1.0	2.1	10 ●	9 ○	4	SW 6	NW 6	W 2
5	100.2	102.4	105.9	102.8	9.9	13.2	11.5	11.5	15.9	8.3	92	84	91	89	1.0	2.5	1.2	1.6	10	10 ○	9	W 6	WSW 5	SW 3
6	108.7	110.5	111.6	110.3	11.5	13.9	11.3	12.0	14.6	9.5	82	67	95	81	2.5	5.2	0.7	2.8	4	10	10 ●	SW 4	W 7	SW 4
7	112.1	112.5	114.6	113.1	11.7	16.5	11.4	12.8	17.7	10.9	91	69	95	85	1.1	5.9	0.7	2.6	10	9	10 ● R	SW 4	WSW 5	WSW 2
8	116.6	118.1	120.0	118.2	12.4	15.5	13.3	13.6	16.3	11.0	89	77	92	86	1.6	4.1	1.3	2.3	10	9	3	WNW 4	NW 2	NW 1
9	120.9	120.1	118.5	119.8	12.9	18.9	14.1	15.0	19.9	9.1	89	59	85	78	1.6	9.0	2.4	4.3	2	8	1	WNW 1	NE 1	NE 2
10	117.6	116.3	114.1	116.0	12.6	21.3	15.1	16.0	22.3	6.4	87	54	86	76	1.9	11.7	2.5	5.4	2	4	0	C 0	NE 2	C 0
11	111.4	108.5	107.3	109.1	14.9	21.6	14.9	16.6	22.6	7.5	84	43	92	73	2.7	14.8	1.3	6.3	6	10	8	W 3	SSE 3	C 0
12	107.0	106.0	104.3	105.8	15.7	17.2	16.0	16.2	21.0	12.7	90	75	79	81	1.7	4.9	3.8	3.5	8	9	9	W 3	SW 4	SW 3
13	103.9	105.3	107.5	105.6	15.9	17.1	14.0	14.8	19.4	13.2	91	69	94	85	1.5	6.0	0.9	2.8	10	7	6	SW 4	NW 6	W 3
14	106.0	106.3	106.4	106.2	13.9	16.9	14.0	14.7	17.2	12.9	93	71	98	87	1.1	5.5	0.4	2.3	10	9	3	C 0	W 2	C 0
15	105.4	104.8	105.5	105.2	14.3	19.2	15.5	16.1	20.7	11.0	94	62	88	81	0.9	8.5	2.1	3.8	9	9	9	C 0	C 0	C 0
16	107.2	108.2	110.4	108.6	14.1	18.7	15.1	15.8	22.4	9.6	91	69	92	84	1.5	6.7	1.4	3.2	6	7	9	E 2	NE 3	C 0
17	113.1	113.7	115.4	114.1	15.3	20.9	17.7	17.9	22.0	12.5	87	64	79	77	2.3	8.8	4.2	5.1	7	4	9	E 2	SE 3	C 0
18	116.4	116.2	116.8	116.5	14.7	22.1	17.5	18.0	23.2	14.2	80	49	89	73	3.3	13.5	2.2	6.3	9	6	9	SE 2	S 4	NE 1
19	117.8	116.9	115.7	116.8	15.2	22.3	17.5	18.1	24.5	9.6	84	48	77	70	2.8	13.9	4.6	7.1	0	2	6	C 0	ENE 2	SW 3
20	114.8	114.6	115.1	114.8	18.3	22.3	16.9	18.6	23.6	15.2	70	60	91	74	6.2	10.7	1.8	6.2	7	9	0	SW 4	W 3	C 0
21	113.6	109.8	110.0	111.1	17.7	24.1	18.9	19.9	26.1	11.8	89	64	95	83	2.2	10.8	1.0	4.7	2	10	6	SE 2	SE 5	SW 4
22	113.2	112.9	115.6	113.9	18.2	22.7	17.5	19.0	24.5	16.5	91	54	87	77	1.9	12.8	2.6	5.8	6	9	6	C 0	WSW 5	C 0
23	118.1	118.5	120.0	118.9	15.1	19.8	14.7	16.1	21.4	12.8	80	51	83	71	3.5	11.4	2.9	5.9	7	8	9	WSW 4	W 6	W 3
24	122.4	123.1	123.3	122.9	13.0	17.3	13.7	14.4	19.1	10.7	86	60	81	76	2.1	7.8	3.0	4.3	8	9	1	W 4	WNW 4	C 0
25	123.4	121.1	118.0	120.8	13.3	19.8	17.3	16.9	21.6	10.9	83	49	75	69	2.7	11.7	4.9	6.4	6	4	7	C 0	W 1	E 2
26	114.9	113.1	113.0	113.7	16.5	23.5	16.5	18.2	24.2	10.6	81	77	97	85	3.7	6.7	0.6	3.7	4	10	9	E 3	NE 1	C 0
27	112.7	112.2	117.7	114.2	16.6	18.9	13.3	15.5	20.0	13.2	96	69	92	86	0.8	6.7	1.3	2.9	10	9	4	WSW 4	W 8	NW 1
28	118.8	119.4	120.2	119.5	12.9	19.9	13.9	15.2	20.6	12.0	89	56	83	76	1.6	10.2	2.7	4.8	9	4	0	WNW 2	NE 5	W 1
29	120.3	119.9	120.2	120.1	12.3	19.9	15.1	15.6	20.4	8.8	88	52	85	75	1.7	11.2	2.6	5.2	1	3	8	W 2	NE 1	NNE 3
30	120.8	119.5	118.5	119.6	13.7	19.8	13.3	15.0	20.2	12.4	93	59	93	82	1.1	9.5	1.1	3.9	9	2	6	C 0	SE 4	C 0
31	118.9	118.1	116.0	117.7	14.7	22.1	17.9	18.2	23.5	11.0	90	53	77	73	1.6	12.5	4.6	6.2	0	3	9	SE 2	W 2	W 4
M	112.7	112.4	112.8	112.6	13.8	18.7	14.5	15.4	20.2	11.0	87	63	88	79	2.0	8.3	2.0	4.1	6.8	7.5	6.3	2.6	3.7	1.6

Sierpień-Août

1	116.3	116.4	115.8	116.2	15.1	20.6	16.2	17.0	22.0	13.1	86	53	85	75	2.5	11.4	2.7	5.5	6	6	6	NW 5	W 6	WNW 2
2	115.5	114.4	113.3	114.4	14.0	20.3	17.1	17.1	22.0	12.0	91	52	81	75	1.5	11.3	3.7	5.5	9	6	9	W 2	W 2	C 0
3	113.8	113.8	113.8	113.8	15.6	20.9	17.3	17.8	21.6	11.1	81	66	87	78	3.4	8.4	2.6	4.8	0	10	7	E 1	NNE 1	E 2
4	111.6	111.4	113.8	112.3	15.3	21.7	18.2	18.4	23.6	13.4	94	72	89	85	1.0	7.2	2.3	3.5	10	8	6	S 2	WSW 2	C 0
5	112.4	109.0	107.9	109.8	15.7	16.1	15.7	15.8	18.8	12.4	91	88	95	91	1.5	2.1	0.9	1.5	9	9	10 ●	SSE 3	SE 1	C 0
6	110.1	110.2	108.2	109.5	12.1	18.5	16.1	15.7	19.7	11.3	96	65	73	78	0.5	7.4	4.9	4.3	9	6	2	W 3	SW 2	S 2
7	103.2	100.8	103.6	102.5	14.9	18.3	13.9	15.2	18.7	11.4	91	95	91	92	1.5	1.0	1.5	1.3	10	10 ●	0	SE 4	SW 1	SW 5
8	106.2	110.1	115.6	110.6	13.9	17.6	12.0	13.9	19.0	12.0	69	51	86	69	4.9	9.8	2.0	5.6	10	7	1	SW 7	WSW 9	WSW 4
9	120.6	122.0	121.3	121.3	11.3	17.1	10.7	12.4	19.4	9.3	91	49	89	76	1.2	9.9	1.5	4.2	2	7	3	SW 4	W 4	SW 1
10	118.0	114.4	111.9	114.8	14.9	19.5	15.4	16.3	20.7	8.7	64	55	85	68	6.0	10.3	2.6	6.3	9	10	3	SW 5	SSW 6	SW 3
11	112.5	112.4	112.4	112.4	14.9	21.5	18.2	18.2	22.4	13.2	76	46	76	66	4.0	13.7	5.1	7.6	9	7	7	WSW 4	WSW 7	SW 2
12	113.0	113.0	115.3	113.8	18.7	27.4	18.2	20.6	28.4	16.3	78	52	85	72	4.8	17.7	3.1	8.5	0	1	2	SW 5	SW 5	C 0
13	118.2	118.9	119.8	119.0	16.7	20.0	15.3	16.8	21.0	13.2	89	73	77	80	2.2	6.4	4.1	4.2	10	9	9	C 0	NNE 4	NNE 4
14	120.3	119.6	117.9	119.3	14.0	19.3	12.7	14.7	20.0	8.2	85	66	86	79	2.3	7.6	2.1	4.0	8	5	2	C 0	N 3	N 3
15	111.5	106.5	105.8	107.9	12.9	18.9	17.3	16.6	20.2	10.0	88	83	96	89	1.8	5.7	0.8	2.1	9	9	10	ESE 5	S 5	C 0
16	107.4	108.6	110.0	108.7	16.3	21.8	17.7	18.4	22.9	15.0	92	61	86	80	1.5	10.1	2.8	4.8	9	8	6	WSW 4	W 4	WSW 1
17	111.5	110.6	106.9	109.7	15.4	21.9	19.5	19.1	22.9	13.8	82	52	69	68	3.2	12.6	7.1	7.6	9	8	9	SW 2	S 5	S 5
18	106.1	109.3	111.5	109.0	14.3	16.1	12.5	13.8	19.5	12.5	93	79	89	87	1.1	3.8	1.5	2.1	9	10	6	SW 5	WSW 6	SW 4
19	111.4	113.1	115.9	113.5	12.2	16.3	14.8	14.5	20.2	11.4	96	85	92	91	0.5	2.7	1.3	1.5	10 ●	5	9	W 4	NW 5	NW 3
20	116.9	117.8	117.1	117.3	14.8	15.6	15.4	15.3	16.7	13.7	94	92	93	93	0.9	1.3	1.1	1.1	10	10	10	NNW 2	NNW 3	NNE 1
21	113.9	112.1	111.8	112.6	14.5	18.7	15.9	16.2	21.2	13.8	98	81	98	92	0.4	4.2	0.4	1.7	10	9	10 ●	NE 1	SE 3	NW 1
22	114.1	114.1	111.1	113.1	13.7	18.1	15.2	15.6	19.2	12.8	94	73	91	86	0.9	5.6	1.5	2.7	8	9	10	W 1	WSW 5	SW 3
23	111.8	113.6	113.7	113.0	11.8	17.0	14.0	14.2	17.4	11.0	96	73	83	83	0.5	5.6	2.7	2.9	10	9	9	WSW 4	W 6	SW 3
24	103.2	101.9	105.1	105.4	13.3	17.4	14.6	15.0	18.6	12.5	96	90	95	94	0.6	2.1	0.7	1.1	10 ●	10	9	SW 7	SW 7	SW 5
25	107.6	108.7	112.7	109.7	13.0	17.2	12.5	13.8	17.5	11.7	89	68	86	81	1.6	6.4	2.1	3.4	8	9	6	WSW 7	WSW 8	WSW 5
26	115.5	117.4	115.5	116.1	12.0	16.2	13.2	13.6	19.0	10.4	84	65	92	80	2.2	6.5	1.3	3.3	6	7	0	WSW 5	W 6	SW 3
27	107.0	105.8	111.0	107.9	13.3	20.4	13.4	15.1	21.1	11.8	71	55	83	70	4.5	10.9	2.7	6.0	6	8	9	SW 5	WSW 8	W 7
28	114.2	115.9	116.6	115.6	11.8	12.4	11.8	12.0	16.6	11.2	85	81	89	85	2.0	2.7	1.5	2.1	9	9	0	WSW 6	WSW 5	SW 5
29	114.2	114.0	117.1	115.1	12.8	13.9	12.4	12.9	15.6	11.5	96	95	92	94	0.5	0.7	1.2	0.8	10 ●	10	6	WSW 3	SW 2	W 4
30	119.9	120.4	116.6	119.0	10.6	15.8	13.6	13.4	17.2	9.6	94	64	79	79	0.8	6.4	3.4	3.5	6	8	9	W 5	WNW 4	WSW 4
31	112.2	113.2	116.0	113.8	12.4	15.7	12.2	13.1	16.2	12.0	77	59	89	75	3.4	7.2	1.5	4.0	9	6	10	W 6	NW 7	NW 5
M	112.6	112.6	113.1	112.8	13.9	18.5	14.9	15.6	20.0	11.9	87	69	87	81	2.1	7.0	2.3	3.8	8.0	7.9	6.3	3.8	4.5	2.8

Szczecin-Dąbie $H_s = 1m$ $H_k = 6{,}9m$ $h_w = 20m$ Lipiec - Juillet 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	5.2	•	⚥°$8^{45-}9^{10}$,$11^{53-}12^{05}$,12^{35-40},15^{42-50}⚥'$17^{10-}18^{05}$
2	8	6.7	•	⚥°13^{05}...16^{55},•$^{0-1}17^{05}$...$19^{00-}21^{20}$,$22^{42-}24$
3	8	9.9	•	•°$0^{00-}1^{25}$ 3^{10-52}⚥°9^{22-35} 14^{37-45}⚥'16^{12-25}⚥°16^{31-40} 23^{10-18}
4	8	0.6	•	⚥°$0^{54-}1^{05}$,•°$1^{10-}8^{20}$⚥°12^{45-48} 13^{03-09} $13^{56-}14^{02}$,15^{32-37},⌓°nn
5	8	6.1	•	⚥°$13^{33-}14^{06}$,•°14^{15}...15^{15}⚥$^{0-1}15^{39}$...24,=$3^{30-}8^{30}$,⌓°$0^{00-}7^{00}$
6	9	0.2	•	⚥°0^{00-10},•°$20^{05-}22^{10}$,=$22^{10-}24$
7	8	8.4	•	•°$4^{40-}5^{40}$⚥$^{0-1}16^{48}$...22^{55},[R]°17^{05-30}NW-SE,([R])°21^{30-}[R]$21^{50-}22^{35}$NW-SE;=na...
8	8	1.6	•	⚥'0^{27-40}⚥$^{0-1}13^{18}$...17^{47},=nn
9	7	•	•	=0^{00-40}=°-4^{50}=-8^{40},⌓°nn
10	8	•	•	=°6^{35-50}=-9^{40},$22^{40-}24$,⌓°$0^{00-}9^{00}$,$21^{00-}24$
11	8	3.4	•	•$^{0-1}17^{52-}18^{46}$,=$0^{00-}2^{00}$=°-2^{50}=-7^{10},$23^{30-}24$,⌓°$0^{00-}8^{00}$
12	7	1.0	•	⚥°12^{25-30},=$0^{00-}8^{15}$,⊕8^{25-45}
13	8	5.2	•	•°$8^{20-}10^{10}$⚥$^{1-0}16^{38}$...20^{55},[R]°$16^{35-}17^{30}$W-E;=$1^{15-}10^{20}$
14	7	15.4	•	⚥°$14^{34-}15^{40}$⚥°$17^{10-}18^{14}$⚥$^{0-2}18^{55-}19^{44}$,=$3^{30-}9^{30}$=$21^{25-}24$
15	7	•	•	=$0^{00-}1^{55}$=°3^{50}=-9^{30}
16	8	2.4	•	⚥$^{0-1}12^{02-40}$⚥°$13^{20-}20^{10}$,([R])$17^{05-}18^{05}$E-W;=$4^{30-}6^{20}$=°-6^{55}=-7^{45},⌓°$2^{00-}10^{00}$
17	8	•	•	=$2^{50-}4^{45}$
18	8	0.8	•	⚥°$16^{40-}17^{46}$,([R])$17^{50-}18^{20}$SSE-SW;⌓°$1^{00-}9^{00}$
19	8	•	•	⌓°$21^{00-}24$
20	6	•	•	=$3^{50-}7^{50}$∞-21^{20}=-24=$21^{45-}24$,⌓°$0^{00-}9^{00}$
21	7	9.0	•	⚥$^{0-1}19^{19-}20^{23}$[R]$19^{22-}20^{27}$SW-NE;=$0^{00-}8^{30}$=$0^{00-}6^{15}$∞$8^{30-}17^{30}$=nn
22	8	1.7	•	⚥°$1^{45-}2^{50}$⚥'13^{44-56}⚥°$16^{42-}17^{02}$,([R])14^{15-20}W-E([R])16^{35-}[R]$16^{50-}17^{15}$W-E;=na=°-5^{45}=$-$a ⌓°nn
23	8	•	•	⌓°$0^{00-}9^{00}$
24	8	•	•	⌓°$0^{00-}9^{00}$,nh
25	8	•	•	⌓°$0^{00-}10^{00}$ $22^{00-}24$
26	7	8.0	•	•°14^{10}...^{45}⚥$^{0-1}16^{35-}17^{40}$,$18^{48-}19^{40}$,[R]°$16^{20-}17^{20}$SW-NE;=$20^{30-}24$;⌓°$0^{00-}9^{00}$
27	7	•	•	=$0^{00-}4^{45}$=$^{0-1}6^{45}$=-10^{20},⌓°$21^{00-}24$
28	8	•	•	⌓°$0^{00-}10^{00}$ $21^{00-}24$
29	8	0.0	•	=$5^{30-}6^{40}$,⌓°$0^{00-}9^{00}$ $23^{00-}24$
30	8	4.6	•	⚥°4^{37-40},8^{33}...9^{07}⚥$^{0-1}15^{15-}16^{15}$⚥°$19^{28-}20^{25}$,⌓°$0^{00-}4^{00}$,⌒20^{05-25}
31	8	0.5	•	⚥°19^{30-33},=$1^{30-}8^{30}$
Σ	—	90.7	—	UWAGI

Sierpień - Août

1	8	0.6	•	•°2^{00-50}⚥$^{1-0}18^{20-35}$⚥°19^{15-18},⌓°$0^{00-}10$,$23^{00-}24$
2	8	•	•	⌓°$0^{00-}10^{00}$,$23^{00-}24$
3	8	•	•	=$0^{15-}6^{30}$,⌓°$0^{00-}10^{00}$,$21^{00-}24$
4	6	0.1	•	•°9^{05}...10^{45},=$3^{30-}12^{30}$,nn;⌓$^{0-1}0^{00-}9^{00}$⌓°nn
5	7	2.0	•	•$^{0-1}11^{02-}13^{20}$⚥°14^{10-45},•°19^{40}...22^{20},=$0^{00-}3^{45}$=°6^{50}=-13^{30},⌓°$0^{00-}11^{00}$
6	7	•	•	=$3^{30-}10^{30}$,⌓°$21^{00-}24$
7	5	12.4	•	⚥°$9^{15-}11^{00}$,•$^{0-1}16^{05}$...17^{10},•°18^{25},[R]°9^{30-35}SSW-NNE;=$1^{30-}18^{30}$,⌓°$0^{00-}9^{00}$
8	8	0.0	•	⚥°19^{30-33} 20^{45-48}
9	8	•	•	⌓°$21^{00-}24$
10	7	0.2	•	•°17^{35}...18^{45}⚥°20^{15-18}⚥'20^{47-55},⌓°$0^{00-}9^{00}$
11	7	•	•	
12	7	•	•	=$19^{30-}20^{30}$,⌓°$22^{00-}24$
13	8	•	•	=$3^{30-}7^{30}$,⌓°$0^{00-}9^{00}$
14	8	•	•	∠$2^{25-}3^{05}$,=$4^{15-}6^{25}$=-7^{40},⌓°$1^{00-}10^{00}$,$22^{00-}24$
15	7	3.4	•	⚥°$10^{20-}11^{08}$,([R])$10^{35-}11^{10}$SSW-NE;=$15^{30-}24$,⌓°$0^{00-}8^{00}$,$22^{00-}24$
16	8	•	•	=$0^{00-}9^{30}$,⌓°$0^{00-}11^{00}$,$23^{00-}24$
17	8	6.6	•	⌓°$0^{00-}10^{00}$
18	8	0.0	•	⚥$^{1-0}3^{45-}5^{05}$⚥°11^{43}...13^{04},17^{40-43},18^{35-40}
19	8	3.1	•	•°$7^{05-}10^{25}$,•$^{0-1}12^{08-}13^{15}$⚥°19^{07-26}
20	7	0.0	•	•°$2^{10-}3^{25}$ 5^{42} 6^{40},•°10^{30}...$11^{30-}12^{40}$,=$4^{15-}7^{40}$
21	7	9.4	•	•°$20^{05-}24$;=$1^{30-}9^{30}$
22	7	4.7	•	•°$0^{00-}2^{20}$,$20^{30-}21^{40}$ $23^{15-}24$;=$2^{20-}10^{50}$
23	8	5.7	•	•°$0^{00-}1^{35}$,•$^{0-1}6^{40}$...9^{05}⚥°12^{20-28} 13^{01-06}
24	7	11.2	•	•°$3^{15-}9^{10}$,11^{40}...13^{20},•$^{1}16^{07-}17^{02}$,•°17^{40};=$9^{10-}10^{30}$
25	8	3.8	•	⚥°$12^{25-}19^{57}$,[R]14^{43-58}W-E,$15^{47-}16^{10}$NW-SE
26	8	•	•	⌓°$20^{00-}24$
27	8	0.5	•	⚥°11^{07-20}⚥'20^{30-40}⚥°21^{05-15},⌓°$0^{00-}9^{00}$
28	8	3.4	•	⚥'10^{38-48}⚥°10^{48}...14^{53}
29	7	3.9	•	•°6^{05-40} $7^{15-}12^{35}$,$15^{10-}16^{05}$,=$5^{15-}12^{35}$
30	8	•	•	⌓°$2^{00-}9^{00}$
31	8	0.5	•	•°19^{40}...20^{00},$22^{05-}23^{35}$
Σ	—	71.5	—	UWAGI.

Szczecin - Dąbie φ = 53°24' λ = 14°37' Wrzesień - Septembre 1962

Dni	Ciśnienie P − 900 + I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność względna U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie i pogoda N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	119.2	121.4	122.1	120.9	10.7	18.6	11.8	13.2	19.1	9.6	99	60	91	85	0.2	8.5	1.1	3.3	10	6	1	NW 1	NW 4	W 3
2	121.9	121.1	118.7	120.6	9.4	18.3	12.0	12.9	20.4	8.8	95	57	91	81	0.6	9.0	1.2	3.6	4	2	2	SW 3	WSW 4	C 0
3	118.0	117.0	113.1	116.0	9.9	25.1	15.3	15.9	24.4	6.4	97	49	81	76	0.3	14.3	3.4	6.0	6	0	0	C 0	C 0	SE 5
4	108.2	107.4	105.7	106.4	14.0	24.8	17.5	18.4	25.5	12.4	85	57	90	77	2.3	13.5	2.0	5.9	4	6	9	C 0	WSW 4	C 0
5	99.5	101.8	101.9	101.1	15.9	17.7	12.4	14.6	19.0	11.9	95	71	89	85	1.0	5.9	1.6	2.8	9	6	6	SW 5	WSW 7	SW 4
6	102.3	103.7	97.7	101.2	13.2	16.9	15.0	15.0	18.7	11.9	87	66	90	81	2.0	6.4	1.6	3.3	9	7	10 ●	WSW 9	WSW 7	SW 5
7	91.8	94.4	102.5	96.2	15.3	15.3	11.0	13.2	17.0	11.0	84	77	79	80	2.8	4.1	2.7	3.2	9	6	0	WSW 7	W 6	WSW 5
8	105.9	106.8	109.3	107.3	8.8	15.2	11.0	11.0	15.6	7.9	88	69	94	84	1.4	4.7	0.8	2.3	2	10 ●	9	WSW 5	WSW 7	W 4
9	117.3	120.2	119.2	118.9	10.5	14.2	11.8	12.1	15.7	8.6	94	69	82	82	0.8	5.0	2.5	2.8	6	10	9	WNW 5	W 3	SW 3
10	115.1	112.7	111.0	112.9	10.7	19.9	13.7	14.5	21.6	10.1	78	53	86	72	2.9	10.8	2.2	5.3	1	1	8	SW 6	SW 6	SW 1
11	107.7	109.8	115.1	110.9	14.6	19.3	12.7	14.8	20.0	12.6	92	71	91	85	1.3	6.4	1.4	3.0	10 ●	7	4	SW 5	W 8	WNW 3
12	106.8	101.3	104.3	104.1	15.0	22.2	13.6	16.1	23.3	11.9	90	69	85	81	1.6	8.4	2.3	4.1	10	4	10	SW 7	SW 8	WNW 6
13	114.3	116.7	120.6	117.2	10.2	15.3	10.5	11.6	17.0	9.2	91	61	84	79	1.1	6.9	2.1	3.4	2	7	0	W 4	WNW 7	NW 3
14	122.5	124.0	122.4	123.0	10.5	13.0	9.6	10.7	13.7	9.2	82	69	91	81	2.3	4.6	1.2	2.7	6	10	6	W 3	W 5	C 0
15	119.0	114.9	109.3	114.4	5.0	14.4	10.0	9.8	17.0	3.1	97	69	87	84	0.3	5.1	1.6	2.3	8	9	2	C 0	SE 7	SE 4
16	106.5	105.9	108.2	106.9	7.4	16.7	14.0	13.0	17.4	5.2	99	79	88	89	0.2	4.1	2.0	2.1	2	10	10	C 0	SW 6	W 2
17	110.8	111.0	110.9	110.9	8.5	14.9	11.8	11.8	16.4	8.3	92	51	75	73	0.9	8.2	3.4	4.2	9	6	6	W 1	WSW 5	SW 4
18	110.3	109.7	109.1	109.7	5.4	14.9	9.4	9.8	15.3	4.6	98	63	95	85	0.2	6.2	0.8	2.4	6	10	10	C 0	ESE 2	C 0
19	109.8	111.6	113.9	111.8	8.8	10.4	9.1	9.4	11.4	7.5	93	93	93	93	0.8	0.8	0.8	0.8	10 ●R	10 ●	0	SE 5	WSW 4	W 3
20	115.1	115.9	117.1	116.0	6.9	14.0	8.4	9.4	14.6	6.6	97	68	89	85	0.3	5.1	1.2	2.2	9	9	4	W 2	W 6	WNW 3
21	117.9	117.5	118.1	117.8	8.5	11.6	9.7	9.9	12.3	7.7	96	87	86	90	0.5	1.8	1.7	1.3	9	10	3	W 4	W 4	W 3
22	120.4	120.9	120.7	120.7	8.5	14.2	10.6	11.0	14.5	7.9	99	75	94	89	0.2	4.1	0.8	1.7	10 ≡	9	9	C 0	NNW 4	WNW 2
23	117.7	115.4	117.4	116.8	9.6	11.2	9.0	9.7	14.3	8.9	96	82	88	89	0.5	2.5	1.4	1.5	10 ●	8	0	WNW 5	NW 4	NW 3
24	121.2	123.5	125.6	123.4	7.0	14.4	8.4	9.6	15.3	6.0	98	71	97	89	0.1	4.8	0.3	1.7	3 ≡	5	0	W 2	NNE 1	C 0
25	127.2	127.6	125.1	126.6	3.8	14.0	7.8	8.4	14.1	2.0	98	70	90	86	0.1	4.8	1.1	2.0	0 ≡	8	0	C 0	SE 6	C 0
26	122.1	120.7	118.7	120.3	7.0	17.9	11.0	11.7	18.1	4.2	96	46	75	72	0.4	11.2	3.2	4.9	4	0	0	SE 8	SE 12	SE 6
27	117.3	116.3	115.1	116.2	7.0	16.6	8.4	10.1	16.8	6.5	90	51	93	78	1.0	9.2	0.7	3.6	0	2	0	SE 5	SE 9	C 0
28	114.5	113.2	113.1	113.6	10.8	13.6	7.2	9.7	14.3	6.4	92	72	97	87	1.0	4.4	0.3	1.9	10	9	0	C 0	SE 3	C 0
29	112.6	112.6	113.6	112.9	8.7	14.3	11.2	11.4	16.6	3.7	100	84	96	93	0.0	2.5	0.5	1.0	10 ≡	10	0	C 0	SE 3	ESE 3
30	115.7	117.3	116.5	116.5	10.2	13.3	11.8	11.8	14.2	8.2	100	90	97	62	0.0	1.6	0.3	0.6	10 ≡	9	0	C 0	C 0	SE 3
31																								
M	113.6	113.7	113.8	113.7	9.7	15.9	11.2	12.0	17.1	7.9	93	68	89	83	0.9	6.2	1.5	2.9	6.6	6.9	3.9	3.1	3.1	2.6

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1	117.2	119.3	121.3	119.3	12.6	17.1	14.2	14.5	17.6	11.6	87	77	98	87	1.9	4.5	0.4	2.3	8	10	10	C 0	C 0	C 0
2	122.3	122.1	121.4	121.9	8.2	21.7	14.7	14.8	22.9	7.8	100	66	89	85	0.0	8.9	1.8	3.6	10 ≡	0	0	C 0	SE 4	SE 3
3	120.5	120.3	120.1	120.3	11.6	22.1	14.6	15.7	23.0	10.9	98	60	88	82	0.3	10.7	2.0	4.3	2	5	0	SE 2	S 4	SE 3
4	120.2	120.3	121.8	120.8	10.0	17.0	14.1	13.8	17.7	8.9	100	89	99	96	0.0	2.2	0.2	0.8	5 ≡	9	8	SE 1	SE 3	C 0
5	121.7	123.0	124.9	123.2	13.6	13.6	12.0	12.8	14.6	12.0	98	98	90	95	0.4	0.4	1.3	0.7	6	10 ●	10	C 0	WNW 3	NNW 3
6	126.5	128.6	131.4	128.8	10.2	15.0	9.4	11.0	15.7	8.9	96	75	95	89	0.4	4.1	0.6	1.7	4	4	0	WNW 2	NNE 4	C 0
7	133.0	134.0	134.4	133.8	7.2	13.6	6.8	8.6	13.6	6.4	99	76	99	91	0.2	3.7	0.2	1.4	9	9	2	NE 2	SE 2	C 0
8	134.9	134.7	133.2	134.3	4.0	12.6	10.3	9.3	15.5	2.3	100	95	96	97	0.0	0.7	0.5	0.4	0 ≡	9	8	C 0	SE 3	SE 3
9	131.9	130.5	128.3	130.2	8.5	16.7	8.7	10.6	17.7	8.2	100	74	94	89	0.0	5.0	0.6	1.9	10 ≡	0	0 ≡	SE 2	SE 5	C 0
10	126.1	124.6	122.2	124.3	8.2	14.0	7.3	9.2	15.4	4.6	100	82	97	93	0.0	2.9	0.3	1.1	10 ≡	0	0	SE 4	SE 4	C 0
11	119.8	118.8	117.2	118.6	4.4	6.2	6.8	6.0	10.6	3.3	98	92	96	95	0.2	0.7	0.5	0.5	10 ≡	9	10	C 0	C 0	N 2
12	117.7	119.9	121.4	119.7	8.6	10.3	7.0	8.2	11.4	5.1	96	78	94	89	0.5	2.7	0.6	1.3	10	10	2	NE 5	C 0	C 0
13	121.0	119.3	114.5	118.3	0.6	12.3	3.3	4.9	13.4	-0.4	100	67	97	88	0.0	4.7	0.2	1.6	10 ≡	1	0	C 0	SE 6	C 0
14	112.0	113.3	116.8	114.0	7.0	11.0	8.4	8.7	13.0	0.8	96	79	79	85	0.4	2.7	2.2	1.8	9	10	9	W 2	W 4	NNW 2
15	123.2	125.7	125.3	124.8	-0.6	11.0	1.6	3.4	12.4	-1.1	100	50	91	80	0.0	6.6	0.7	2.4	3 ≡	6	6	C 0	C 0	C 0
16	122.5	120.6	120.6	121.2	5.4	9.6	9.4	8.4	10.0	1.2	80	91	96	89	1.8	1.2	0.5	1.2	10	10	10	SW 3	WSW 4	W 4
17	121.1	122.2	122.1	121.8	9.2	12.5	11.7	11.3	13.5	8.6	93	88	90	90	0.8	1.7	1.3	1.3	9	10	10	W 3	W 2	W 3
18	119.4	116.8	109.9	115.4	11.2	12.4	13.0	12.4	13.1	10.8	89	85	74	83	1.5	2.2	4.0	2.6	10	10	10	W 3	W 7	W 7
19	112.7	114.5	114.2	113.8	8.8	12.6	11.0	10.8	13.4	8.7	85	61	74	73	1.7	5.7	3.4	3.6	8	4	9	NW 4	NW 6	WNW 5
20	119.3	123.8	128.0	123.7	6.5	12.8	1.8	5.7	13.6	1.4	94	71	94	86	0.6	4.3	0.4	1.8	0	7	0	W 3	NW 3	C 0
21	129.0	129.1	128.8	129.0	3.9	11.4	10.0	8.8	11.4	0.2	97	79	88	88	0.3	2.8	1.5	1.5	1	9	10	W 4	W 6	W 2
22	128.6	127.9	126.9	127.8	9.3	10.5	8.2	9.0	10.6	8.1	84	75	83	81	1.9	3.2	1.8	2.3	10	10	10	W 2	W 3	C 0
23	124.8	124.2	121.5	123.5	7.8	8.2	0.2	4.1	8.8	0.2	90	85	98	91	1.1	1.7	0.1	1.0	10	10	0 ≡	WSW 1	SW 2	C 0
24	119.5	120.3	120.4	120.1	2.7	5.6	7.3	5.7	8.1	-1.7	100	98	96	98	0.0	0.2	0.4	0.2	10 ≡	10 ≡	10	W 3	W 4	W 4
25	117.9	116.2	113.9	116.0	4.4	10.4	11.2	9.3	11.8	3.1	100	83	72	85	0.0	2.1	3.7	1.9	10 ≡	9	0	C 0	SSW 2	SW 5
26	111.3	109.4	106.0	108.9	6.4	13.9	13.6	11.9	15.0	5.7	84	70	64	73	1.6	4.7	5.7	4.0	3	9	0	SW 5	SW 5	SW 6
27	111.2	115.3	116.1	114.2	4.0	8.4	2.4	4.3	13.6	2.1	92	69	96	86	0.6	3.4	0.3	1.4	7	9	6	NW 3	WNW 4	C 0
28	109.4	107.2	107.1	107.9	2.6	5.6	5.0	4.6	6.9	2.2	81	67	83	77	1.5	2.9	1.3	2.0	9	9	4	SW 3	WSW 5	SW 2
29	109.2	111.7	114.3	111.7	3.7	8.8	5.6	5.9	9.6	3.3	90	67	86	81	0.8	3.7	1.3	1.9	9	9	6	SW 5	W 4	SW 4
30	114.3	111.7	106.0	110.7	2.0	8.3	6.5	5.8	8.8	1.8	100	78	65	81	0.0	2.3	3.4	2.0	10 ≡	7	8	NE 1	SW 6	S 8
31	106.1	106.9	108.3	107.2	5.2	7.2	5.4	5.8	7.9	4.3	89	78	83	83	0.9	2.2	1.6	1.6	10	10	0	SW 4	S 3	S 3
M	120.1	120.4	120.0	120.2	6.7	12.0	8.4	8.9	13.2	4.8	94	78	89	87	0.6	3.4	1.4	1.8	7.5	7.5	5.1	2.2	3.3	2.2

Szczecin - Dąbie $H_s = 1m$ · $H_s = 6{,}9m$ - $h_w = 20m$ Wrzesień - Septembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘB. ŚNIEGU h	POGODA
1	8	•	•	$=5^{30}-6^{10}\equiv{}^{\circ}-6^{45}=-9^{40};\triangle{}^{\circ}21^{00}-24$
2	8	•	•	$=4^{30}-9^{30},21^{30}-23^{50}\equiv{}^{\circ}-24;\triangle{}^{\circ}0^{00}-11^{00},nn;\oplus 10^{30}-12^{30}$
3	7	•	•	$\equiv{}^{\circ}0^{00}-7^{45}=-12^{30},19^{30}-24;\triangle{}^{\circ}0^{00}-9^{00},22^{00}-24$
4	7	22.2	•	$\overset{\bullet}{\nabla}{}^{\circ}22^{15}\ldots 24;(\overline{\nabla})23^{30}-24;=0^{00}-5^{30},7^{30}-8^{30};\triangle{}^{\circ}0^{00}-10^{00}$
5	8	4.3	•	$\overset{\bullet}{\nabla}{}^{0-1}0^{00}-3^{30}\overset{\bullet}{\nabla}{}^{\circ}3^{50}-4^{20},10^{30-32}\overset{\bullet}{\nabla}{}'18^{40}-19^{05};\overline{\nabla}{}^{\circ}0^{00}-2^{40}W-E\,\overline{\nabla}{}^{\circ}14^{55}-15^{20}SW-NE\,\overline{\nabla}{}^{\circ}18^{40}-19^{15}SW-NE$
6	8	2.7	•	$\overset{\bullet}{=}{}^{\circ}19^{45}-24$
7	8	1.7	•	$\bullet{}^{\circ}0^{00}-1^{30}\ldots 2^{45}\overset{\bullet}{\nabla}{}^{0-1}8^{23}\ldots 12^{57}\overset{\bullet}{\nabla}{}^{\circ}16^{24-42};\overline{\nabla}{}^{\circ}11^{05-20}W-E;\gg 12^{44-55}$
8	8	3.1	•	$\overset{\bullet}{\nabla}{}^{\circ}13^{05}-14^{02},16^{20-35}\overset{\bullet}{\nabla}{}^{0-1}17^{30-40}\overset{\bullet}{\nabla}{}^{\circ}19^{15-55}$
9	8	0.9	•	$\overset{\bullet}{\nabla}{}'10^{55}-11^{07}$
10	8	1.4	•	
11	7	1.4	•	$\bullet{}^{\circ}6^{18}-9^{20},11^{15}\ldots 12^{05};=9^{20}-13^{10};\triangle{}^{\circ}21^{00}-24$
12	8	1.8	•	$\bullet 6^{20}\ldots 7^{40}\overset{\bullet}{\nabla}{}^{\circ}9^{15-18},11^{15-30},14^{57-58},15^{04-15},20^{20}\ldots 21^{48};\triangle{}^{\circ}0^{00}-6^{00}$
13	8	•	•	
14	8	•	•	$\triangle{}^{\circ}2^{00}-10^{00},21^{00}-24$
15	8	•	•	$=2^{30}-4^{30}5^{30}-7^{40};\triangle{}^{\circ}0^{00}-11^{00},22^{00}-24$
16	6	2.2	•	$\bullet{}^{\circ}14^{57}-15^{45}\ldots 16^{10};=2^{10}-5^{30}=-24;\triangle{}^{\circ}0^{00}-12^{00}$
17	8	•	•	$=0^{00}-15;\triangle{}^{\circ}21^{00}-24;\backsim 2^{25}-4^{30}$
18	7	2.0	•	$\overset{\bullet}{\nabla}{}^{\circ}19^{18}-20^{05};=3^{30}-6^{30}=-8^{20}\equiv{}'-8^{45}=-11^{45};\triangle{}^{\circ}0^{00}-10^{00}$
19	6	8.4	•	$\overset{\bullet}{\nabla}{}^{\circ}1^{50}-2^{45}3^{10-55}7^{43}-9^{10}\bullet{}^{\circ}9^{40}\ldots 10^{35}-11^{35}\bullet{}^{0-1}12^{23}-14^{45}\overset{\bullet}{\nabla}{}^{\circ}17^{36}-18^{08};\overline{\nabla}{}^{\circ}7^{55}-8^{45}NE-SW;=na-a,nn$
20	8	0.7	•	$\overset{\bullet}{\nabla}{}'12^{20-26}\overset{\bullet}{\nabla}{}^{\circ}18^{50-52};=0^{00}-10^{30}$
21	8	0.3	•	$\overset{\bullet}{\nabla}{}^{\circ}10^{20-27}\bullet{}^{\circ}11^{25}\ldots 12^{40}\overset{\bullet}{\nabla}{}^{\circ}12^{50}-13^{02}$
22	7	0.8	•	$\overset{\bullet}{\nabla}{}^{\circ}17^{05-15};=4^{30}-6^{10}\equiv{}^{\circ}-9^{30}=-10^{05}$
23	7	3.6	•	$\bullet{}^{\circ}6^{45}\ldots 7^{20}-11^{20}\overset{\bullet}{\nabla}{}^{\circ}13^{22-56},14^{03-07},20^{12-15}$
24	8	•	•	$=5^{40}-6^{35}\equiv{}^{\circ}-7^{25}\equiv{}^{\circ}-8^{45}=-10^{35},22^{30}-24;\triangle{}'nn$
25	8	•	•	$=0^{00}-3^{45}\equiv{}^{\circ}5^{45}=-6^{15}=-7^{45}=6^{30}-7^{45}\equiv{}^{0-1}-9^{30}\equiv{}'-10^{30}=-12^{10}=-21^{30}=-24;\triangle{}^{1-2}0^{00}-12^{00}\triangle{}'nn$
26	7	•	•	$\gg 12^{30}-18^{30};=0^{00}-4^{30};\triangle{}^{\circ}0^{00}-11^{00}$
27	7	•	•	$=19^{30}-24;\triangle{}^{0-1}20^{00}-24$
28	7	•	•	$=0^{00}-11^{45},18^{30}-23^{45}\equiv{}^{\circ}-24;\triangle{}^{1-0}0^{00}-12^{00}$
29	7	•	•	$\equiv{}^{\circ}0^{00-30}\equiv{}^{0-2}-9^{35}=-12^{10},18^{45}-24$
30	5	•	•	$=0^{00-30}\equiv{}^{1-0}-11^{20}=-24;\triangle{}^{\circ}22^{00}-24$
31				
Σ	—	57.5	—	UWAGI.

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1	6	0.1	•	$\bullet{}^{\circ}13^{03}\ldots 14^{20}18^{15-25};=0^{00}-22^{50}\equiv{}'-24;\triangle{}^{\circ}0^{00}-10^{00}$
2	6	•	•	$\equiv{}^{1-2}0^{00}-4^{30}\equiv{}^{2-1}-7^{46}\equiv{}^{\circ}-8^{30}=-12^{30}\infty-16^{30}=-24$
3	7	•	•	$=0^{00}-10^{30},17^{40}-18^{30},21^{30}-23^{40}\equiv{}^{\circ}-24$
4	6	3.2	•	$\bullet{}^{\circ}11^{40-52},15^{15-20}17^{10}-20^{15},\overline{\nabla}{}^{\circ}18^{15}-19^{30}SW-NE;\equiv{}^{0-1}0^{00}-7^{35}=-21^{50}\equiv{}^{0-1}-24$
5	5	1.0	•	$\bullet\bullet{}^{\circ}9^{10}-11^{30}\bullet{}^{\circ}-13^{45},16^{05}-17^{40}\bullet{}^{\circ}19^{05}-20^{40};\equiv{}^{0-1}0^{00}-6^{45}=-24$
6	7	•	•	$=0^{00}-8^{10}\equiv{}^{\circ}-8^{45}=-9^{40}17^{30}-24$
7	7	•	•	$=0^{00}-9^{45}=5^{25}-7^{35}=18^{30}-23^{30}\equiv{}^{\circ}-24$
8	6	•	•	$\equiv{}^{\circ}0^{00}-7^{25}=-7^{45}\equiv{}^{\circ}-8^{10}\equiv{}^{2-1}-11^{35}=-14^{30}16^{30}-24;\triangle{}^{\circ}20^{00}-24$
9	7	•	•	$=0^{00}-5^{40}\equiv{}^{0-1}-9^{15}=-12^{30}=18^{40}-20^{50}=19^{30}-20^{50}\equiv{}^{0-1}-24;\triangle{}^{\circ}0^{00}-11^{00},19^{00}-24$
10	7	•	•	$\equiv{}^{0-1}0^{00}-4^{50}\equiv{}^{\circ}-8^{40}=-12^{15}17^{15}-22^{40}\equiv{}^{\circ}23^{30}\equiv{}^{\circ}-24;\triangle{}^{\circ}0^{00}-11^{00}$
11	7	•	•	$\equiv{}^{1-0}0^{00}-7^{40}=-12^{20},17^{50}-24$
12	7	•	•	$=0^{00}-6^{50}=21^{30}-24;\triangle{}^{\circ}21^{00}-24$
13	7	•	•	$=0^{00}-3^{45}\equiv{}^{\circ}-6^{30}\equiv{}^{2-0}-10^{45}=-11^{40},17^{15}-22^{25}=17^{30}-22^{35}\equiv{}^{\circ}-24;\triangle{}^{\circ}0^{00}-12^{00}$
14	7	0.0	•	$\bullet{}^{\circ}15^{35-50};\equiv{}^{\circ}0^{00-30}\equiv{}^{1-0}-2^{25}=-12^{45}$
15	8	•	•	$=2^{40}-4^{20}\equiv{}^{\circ}-7^{40}=-9^{30};\smile{}^{\circ}6^{00}-a\triangle{}^{\circ}19^{00}-20^{00}\smile{}^{\circ}-22^{00}$
16	6	0.0	•	$\bullet{}^{\circ}8^{15}-9^{10}\bullet\bullet{}^{\circ}13^{25}\ldots 14^{05}\overset{\bullet}{\nabla}{}^{\circ}16^{10-15};=10^{20}-24$
17	7	0.0	•	$\bullet{}^{\circ}0^{00}-2^{50}3^{50}-5^{40}9^{22}-10^{05}\bullet{}^{\circ}11^{18}\ldots 12^{10};=0^{00}-6^{30},10^{05}-12^{45}$
18	6	0.1	•	$\bullet{}^{\circ}9^{10}\ldots 46\bullet{}^{\circ}22^{40}\ldots 24;=3^{30}-24$
19	8	•	•	$\bullet{}^{\circ}0^{00}-2^{15};=0^{00}-2^{30}$
20	8	•	•	$=19^{30}-24;\triangle{}^{\circ}2^{00}-11^{00}$
21	7	•	•	$=0^{00}-5^{30}\equiv{}^{\circ}7^{15}-8^{35}=-9^{30};\triangle{}^{\circ}na-a$
22	7	•	•	
23	7	0.0	•	$\bullet{}^{\circ}11^{35}\ldots 12^{20};=4^{30}-12^{30}16^{30}-20^{45}\equiv{}^{0-1}-24;\smile{}^{\circ}19^{00}-23^{00}$
24	3	•	•	$\equiv{}'0^{00}-1^{40}\equiv{}'-2^{45}\equiv{}^{\circ}-3^{20}\equiv{}^{1-0}-13^{40}=-24;\triangle{}^{\circ}0^{00}-24$
25	5	•	•	$\equiv{}^{0-2}0^{00}-9^{20}=-18^{30};\triangle{}'0^{00}-10^{00}$
26	6	4.0	•	$=6^{40}-7^{45}9^{05}-12^{30}\infty-18^{30}$
27	8	0.1	•	$\bullet{}^{\circ}2^{05}-5^{15}\overset{\bullet}{\nabla}{}^{\circ}14^{46-59};=18^{10-50}\equiv{}^{\circ}-20^{40}=-24;\triangle{}^{\circ}19^{00}-24$
28	7	•	•	$\triangle{}^{\circ}0^{00}-10^{00}$
29	7	•	•	$\triangle{}^{\circ}1^{00}-10^{00}$
30	7	0.1	•	$=3^{30}-4^{30}\equiv{}^{0-2}-9^{40}=-12^{30};\triangle{}^{\circ}3^{00}-10^{00}$
31	6	•	•	$\bullet{}^{\circ}0^{48}\ldots 2^{45};=5^{30}-24$
Σ	—	8.6	—	UWAGI.

Szczecin-Dąbie φ = 53°24' λ = 14°37' Listopad - Novembre 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	109.4	110.2	111.1	110.2	3.8	6.3	6.0	5.5	6.8	3.1	97	94	97	96	0.3	0.5	0.3	0.4	10	10	10 ●	C 0	C 0	C 0
2	110.6	111.4	112.6	111.5	6.4	9.0	8.2	8.0	9.1	5.9	95	93	97	95	0.4	0.8	0.3	0.5	10	10	10 ●	C 0	C 0	C 0
3	113.8	113.9	113.7	113.8	6.9	7.4	4.5	5.8	8.6	3.8	92	80	87	86	0.7	2.1	1.1	1.3	10	10	0	S 1	SSW 4	S 3
4	112.5	112.1	110.9	111.8	2.6	7.0	5.5	5.2	8.6	2.4	96	88	97	94	0.3	1.2	0.3	0.6	2	8	3	SE 4	SE 5	SE 6
5	108.8	106.6	106.2	107.2	6.6	12.4	9.4	9.4	12.9	5.0	90	73	89	84	1.0	3.9	1.3	2.1	10	8	0	SE 6	SE 8	SE 7
6	104.7	104.7	106.5	105.3	8.2	10.7	8.8	9.1	11.2	7.4	83	63	72	73	1.8	4.8	3.2	3.3	2	9	4	SE 8	SE 8	SE 9
7	110.7	114.4	116.0	113.7	6.7	10.8	7.1	7.9	11.6	6.5	88	79	93	87	1.2	2.8	0.8	1.6	6	9	0	SE 8	SE 7	E 2
8	114.0	111.2	111.4	112.2	4.8	13.0	8.5	8.7	14.2	4.0	97	70	82	83	0.3	4.5	2.0	2.3	0	0	0	ESE 3	SE 7	SE 5
9	111.8	112.7	116.8	113.8	5.6	9.5	5.9	6.7	10.2	5.2	88	71	79	79	1.1	3.4	2.0	2.2	4	8	9	E 4	ESE 5	E 6
10	119.6	121.6	124.8	122.0	4.8	5.4	2.6	3.8	6.6	2.4	79	72	67	73	1.8	2.5	2.5	2.3	10	10	10	ENE 7	E 9	ESE 8
11	124.2	122.6	119.7	122.2	1.8	1.9	2.0	1.9	2.8	1.5	76	89	89	85	1.7	0.8	0.8	1.1	10	10 ✳	10	ENE 5	E 6	E 5
12	118.1	118.3	118.1	118.2	2.8	3.7	1.7	2.5	3.9	1.7	95	93	94	94	0.4	0.6	0.4	0.5	10	10 ●	10 ●	E 4	SE 4	E 3
13	117.7	118.4	119.3	118.5	1.8	3.2	3.4	3.0	3.8	1.7	96	91	97	95	0.3	0.7	0.3	0.4	10	10	10	E 1	C 0	E 1
14	118.9	118.5	115.8	117.7	3.4	4.0	4.3	4.0	5.1	3.0	97	95	90	94	0.3	0.4	0.8	0.5	10	10	10	C 0	WSW 2	W 3
15	107.4	103.2	101.9	104.2	3.2	4.4	1.6	2.7	4.5	1.4	84	68	91	81	1.2	2.7	0.7	1.5	4	10	10	SW 7	SW 7	SW 4
16	105.5	107.8	110.7	108.0	2.3	3.8	0.0	1.5	5.1	-0.2	87	75	86	83	0.9	2.0	0.9	1.3	10	9	0	W 4	W 6	W 4
17	111.5	110.9	108.3	110.2	0.1	2.8	-0.7	0.4	2.8	-1.2	92	74	92	86	0.5	2.0	0.5	1.0	10	10	4	SW 3	S 4	SE 5
18	102.0	100.8	99.4	100.7	-1.1	3.4	-0.4	0.4	3.6	-1.7	87	70	92	83	0.7	2.4	0.5	1.2	10	4	4	SE 5	SE 9	E 6
19	96.1	99.8	103.7	99.9	0.2	0.6	1.2	0.8	2.9	-1.2	98	98	94	97	0.1	0.1	0.4	0.2	10 ● ✳	10 ✳	0	ESE 2	W 3	W 1
20	105.3	106.1	106.3	106.0	-1.3	0.1	1.1	0.2	1.3	-2.4	100	100	94	98	0.1	0.0	0.4	0.2	10 ≡	10 ≡	10	C 0	SW 1	SW 3
21	107.0	109.1	110.2	108.8	1.0	1.2	-1.9	-0.4	1.5	-4.2	92	75	98	88	0.5	1.7	0.1	0.8	10	9	10	WSW 3	SW 4	C 0
22	110.2	111.0	113.6	111.6	-0.6	-0.2	-0.7	-0.6	-0.2	-1.9	97	98	99	98	0.2	0.1	0.0	0.1	10 ✳	10 ✳	10	E 4	E 2	C 0
23	114.8	117.3	122.2	118.1	-0.8	-0.4	-1.2	-0.9	0.3	-1.6	97	94	100	97	0.2	0.3	0.0	0.2	10 ≡	10	10 ≡	C 0	C 0	C 0
24	126.2	128.6	130.1	128.3	-3.2	-2.2	-2.0	-2.4	-0.8	-3.8	97	98	94	96	0.1	0.1	0.4	0.2	0 ≡	10 ≡	10	C 0	C 0	C 0
25	129.1	127.8	127.6	128.2	-1.2	-0.2	0.4	-0.2	0.5	-2.0	93	86	92	90	0.4	0.8	0.5	0.6	9	10	10	SSW 3	SW 4	SW 3
26	130.9	132.3	132.7	132.0	1.8	3.0	2.6	2.5	3.1	0.4	98	95	96	96	0.2	0.4	0.3	0.3	10	10	10	C 0	W 2	W 4
27	131.2	129.7	126.8	129.2	3.4	6.4	3.0	4.0	6.9	2.4	98	98	100	99	0.1	0.1	0.0	0.1	10	9	10 ≡	W 3	W 1	C 0
28	124.1	123.2	123.3	123.5	3.8	7.0	5.8	5.6	7.2	2.4	97	85	95	92	0.3	1.4	0.4	0.7	10	10	10 ●	W 3	W 5	W 4
29	121.5	119.4	114.3	118.4	5.7	7.9	5.9	6.4	8.1	4.6	98	87	91	92	0.2	1.3	0.9	0.8	10 ●	10	10 ●	W 3	WSW 5	WSW 6
30	112.8	114.8	123.1	116.9	5.0	5.2	1.0	3.0	6.8	0.8	86	84	94	88	1.2	1.4	0.4	1.0	4	9	5	W 6	NW 6	N 5
31																								
M	114.4	114.6	115.2	114.7	2.8	4.9	3.1	3.5	5.6	1.5	92	85	91	89	0.6	1.5	0.8	1.0	8.0	9.1	7.0	3.2	4.1	3.4

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1	134.4	138.5	141.4	138.1	-0.8	2.1	-1.4	-0.4	2.8	-1.4	90	75	93	86	0.6	1.8	0.3	0.9	1	1	0	NNW 3	NW 4	NW 3
2	142.5	142.9	141.4	142.3	-4.2	-0.7	-4.4	-3.4	-0.4	-4.5	96	87	96	93	0.2	0.7	0.2	0.4	1	6	10	W 3	WSW 4	WSW 4
3	137.6	135.4	131.6	134.9	-5.4	-2.2	-4.0	-3.9	-1.6	-6.7	92	76	84	84	0.3	1.2	0.7	0.7	4	8	3	C 0	SW 1	SW 3
4	127.8	126.0	124.0	125.9	-2.0	1.0	-2.4	-1.4	1.0	-4.5	83	70	76	76	0.9	2.0	1.2	1.4	9	2	0	W 4	WSW 5	WSW 3
5	124.6	127.5	129.7	127.3	3.4	4.3	1.5	2.7	4.5	-2.7	91	87	96	91	0.7	1.1	0.3	0.7	10	10	10 ●	NNW 3	C 0	W 3
6	129.3	129.3	128.4	129.0	-0.2	-0.1	-1.0	-0.6	1.6	-1.0	98	100	97	98	0.1	0.0	0.2	0.1	10	10 ≡	10 ≡	W 4	C 0	W 3
7	126.4	126.5	127.7	126.9	-3.1	-1.0	-4.2	-3.1	-0.2	-4.2	97	93	94	95	0.1	0.4	0.3	0.3	10 ≡	0	0	W 1	W 1	C 0
8	128.0	127.4	120.5	125.3	-4.0	0.2	0.6	-0.6	1.4	-6.4	94	83	76	84	0.3	1.1	1.6	1.0	1	10	8	C 0	WSW 4	WSW 5
9	107.4	100.8	91.7	100.0	1.0	2.3	3.1	2.4	3.5	-0.3	75	82	91	83	1.7	1.3	0.6	1.2	10	10	10 ●	SSW 7	SW 7	W 7
10	93.5	94.1	100.5	96.0	3.8	4.3	3.9	4.0	5.6	2.4	92	87	85	88	0.7	1.1	1.2	1.0	10	9 ●	0	WNW 7	W 8	NW 7
11	102.8	101.1	93.2	99.0	3.4	3.3	3.4	3.4	4.1	2.5	93	93	91	92	0.5	0.5	0.7	0.6	10 ●	10 ●	10 ●	WNW 5	WSW 6	WSW 7
12	86.4	85.4	88.6	86.8	5.0	6.4	4.4	5.0	6.5	3.2	86	84	92	87	1.2	1.6	0.7	1.2	10	10 ●	9	W 8	WSW 8	SW 3
13	93.8	94.4	97.8	95.3	1.4	2.9	2.2	2.2	4.6	0.3	100	100	96	99	0.0	0.0	0.3	0.1	10 ≡	10 ≡	10	C 0	C 0	W 3
14	101.8	102.3	102.2	102.1	0.8	1.6	-0.8	0.2	2.2	-0.8	86	91	85	87	0.9	0.7	0.9	0.8	10	10	0	NW 2	W 4	W 4
15	80.9	80.9	79.5	80.4	0.6	3.3	2.6	2.3	3.6	-1.0	94	86	91	90	0.4	1.0	0.7	0.7	10 ● ✳	8	10	SW 9	WNW 6	W 5
16	67.5	69.8	82.4	73.2	0.7	3.2	1.2	1.6	3.5	0.4	96	98	98	97	0.2	0.2	0.2	0.2	10	10 ○	10	C 0	C 0	C 0
17	91.3	93.9	97.0	94.1	1.8	1.5	0.0	0.8	2.4	-0.1	93	94	94	94	0.6	0.4	0.4	0.5	10	10	3	N 5	NW 3	C 0
18	98.4	99.3	101.9	99.9	-4.3	-3.5	-3.9	-3.9	0.3	-5.6	98	97	89	95	0.1	0.1	0.5	0.2	0 ≡	10	10	C 0	C 0	C 0
19	103.8	107.3	114.6	108.6	-4.6	-3.6	-4.6	-4.4	-3.4	-5.4	88	90	84	87	0.5	0.3	0.7	0.6	10	10 ✳	10	S 1	SE 2	E 3
20	121.2	122.5	121.7	121.8	-5.2	-4.0	-5.8	-5.2	-3.8	-9.5	88	82	84	85	0.5	0.8	0.6	0.6	10	10	6	C 0	WSW 1	S 4
21	116.4	116.6	122.0	118.3	-5.3	-7.2	-13.1	-9.7	-4.8	-13.1	85	63	80	76	0.6	1.3	0.4	0.8	10	9	2	SSE 7	E 7	E 4
22	131.4	138.1	144.0	137.8	-15.2	-10.9	-11.0	-12.0	-9.7	-15.5	77	76	90	81	0.4	0.6	0.3	0.4	0	0	0	E 3	E 2	NE 1
23	145.6	146.4	147.5	146.5	-13.0	-7.8	-10.3	-10.4	-7.8	-15.6	92	70	84	82	0.2	1.0	0.4	0.5	0	0	0	C 0	E 5	E 1
24	147.7	144.8	141.6	144.7	-14.1	-4.4	-5.5	-7.4	-4.2	-17.3	87	79	85	84	0.3	0.9	0.6	0.6	0	9	6	C 0	SE 4	E 2
25	136.0	131.7	125.1	130.9	-9.6	-4.8	-5.4	-6.3	-4.7	-10.1	88	83	82	84	0.4	0.7	0.7	0.6	8	9	10	C 0	ESE 5	C 0
26	117.1	113.9	110.2	113.7	-7.0	-6.0	-7.0	-6.8	-5.4	-7.2	85	81	88	85	0.5	0.7	0.4	0.5	10	10	10	C 0	SW 3	SW 2
27	108.2	108.2	109.1	108.5	-9.0	-7.3	-6.1	-7.1	-6.1	-9.8	86	82	84	84	0.4	0.6	0.6	0.5	10	10 ✳	10	C 0	WSW 4	SW 2
28	108.6	109.9	110.3	109.6	-5.0	-3.8	-3.8	-4.1	-3.6	-6.2	93	80	82	85	0.3	0.9	0.8	0.7	10	10 ✳	10	SW 2	WSW 4	WSW 2
29	108.6	108.1	109.4	108.7	-6.1	-4.6	-7.9	-6.6	-3.6	-9.0	89	86	93	89	0.4	0.6	0.2	0.4	10 ✳	9 ✳	10	C 0	C 0	C 0
30	111.5	113.3	116.1	113.6	-7.1	-6.8	-5.0	-6.0	-5.0	-9.0	93	96	98	96	0.2	0.1	0.1	0.1	10	10 ≡	9	C 0	C 0	C 0
31	119.5	121.6	123.3	121.5	-6.2	-5.8	-11.3	-8.6	-4.4	-11.5	89	61	86	79	0.4	1.5	0.4	0.8	10	9	0	E 5	E 7	E 4
M	114.5	114.6	115.3	114.8	-3.5	-1.6	-3.1	-2.8	-0.7	-5.5	90	84	89	88	0.5	0.8	0.6	0.6	7.5	8.0	6.3	2.5	3.4	2.7

Szczecin-Dąbie $H_s = 1m$ $H_t = 6{,}9m$ $h_w = 20m$ Listopad - Novembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBSZNIEGU h	POGODA
1	5	0.6	•	•°7^10-10^30,19^40...20^30-22^15,°23^05-24;=0^00-24
2	5	0.0	•	°0^00-1^50,°15^55...17^50,°20^50...24;=0^00-24
3	7	•	•	°0^00...50;=0^00-12^30,°22^00-24
4	6	•	•	=3^30-23^45≡°-24;°0^00-12^00 20^00-24
5	7	•	•	≡°0^00-4^00≡°-5^40=-11^30∞-18^00;°0^00-12^00,nn
6	8	•	•	2^30-3^20,4^55-5^15,16^30-20^50;°0^00-10^00
7	8	•	•	=21^30-24;°5^00-9^00,20^00-24
8	7	•	•	=0^00-12^30∞-13^20=17^30-24;°0^00-11^00
9	7	•	•	=0^00-8^30∞-11^30;°5^00-12^00,17^00-24
10	7	•	•	°0^00-2^00
11	6	0.4	•	*°9^35...14^10*°16^50-17^10*°-17^45°-18^30...20^10
12	6	2.3	•	•°3^40...6^40,°8^45...11^15•°...13^00-21^30;=6^40-24
13	6	•	•	=0^00-24
14	5	•	•	=0^00-7^40≡^{0-1}-10^40=-11^25≡°-12^35=-24
15	7	0.0	•	•15^05...19^25,22^45...24;=0^00-11^30,14^30-24
16	8	•	•	•0^00...15;=0^00-6^30
17	7	•	•	=13^30-24;°1^00-10^00,20^00-24;⊕11^40-13^50
18	7	2.4	•	=0^00-6^00;°0^00-10^00;5^50-7^20
19	5	5.2	•	°1^40-3^50•°-5^40*°-7^20*^{0-1}-15^30...16^40;=13^10-21^45≡°-24
20	2	•	•	≡°0^00-5^30≡^{0-2}-17^40=-24
21	7	0.5	pż.	=0^00-10^30,15^30-24;°19^00-24
22	4	2.0	1	*5^10-17^40,18^50-19^40;=0^00-24;°0^00-5^00
23	6	0.0	5	=0^00-6^45≡°-9^10=-20^20≡'-22^45=-24
24	2	•	5	*°1^30 2^30=0^00-5^20≡°-7^30≡^{1-0}-17^40=-24
25	6	0.0	5	•16^40-19^20;=0^00-24
26	6	0.2	pż.	=0^00-24
27	5	•	•	°1^10-3^40;=0^00-7^20≡^{0-1}-9^45≡^{1-0}-11^15=-19^40≡^{0-1}-24
28	6	1.2	•	•16^10...23^05;≡'1^00-40=-24
29	7	2.2	•	°0^50...7^15-10^20,18^10...22^30-24;=0^00-11^30
30	8	4.1	•	•°0^00-1^30...2^40▽°11^06-20,13^15...14^40•°...18^10*^{1-0}-20^10
31				
Σ	—	21.1	—	UWAGI.

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1	7	•	•	
2	7	•	•	=13^30-24;^{1-0}1^00-24
3	6	•	•	=0^00-24;°0^00-24
4	6	•	•	=0^00-9^30∞-15^30=-24;°0^00-11^00
5	6	0.6	•	°18^15...21^00-24;=0^00-3^40≡°-5^35=-24
6	3	0.0	•	°0^00-6^10 9^10...11^35;=0^00-11^35≡^{0-1}24
7	4	•	•	≡°0^00-7^30≡°-8^10≡^{1-0}10^20=-24;°13^00-24
8	4	•	•	=0^00-24;°0^00-15^00
9	6	6.4	•	*^{0-1}10^10-11^15•15^50...24;=0^00-7^15,10^30-24
10	7	0.6	•	•°0^00-25,10^15...11^25▽°12^50...14^25;=0^00-25
11	6	7.4	•	•°5^10...8^10 11^20...14^30-16^40,20^25-24;=19^30-24
12	6	2.8	•	•°0^00-3^35 5^50...6^20,11^40...12^15-19^40-20^10;=0^00-7^30
13	3	0.7	•	•13^05-14^20;=3^30-6^10≡^{0-2}-13^50=-14^15≡^{0-1}-16^35=-24
14	7	3.6	•	▲°9^25-10^05*°-10^40▽°11^25...12^15▽°13^20...14^12▲°14^18-15^03;=0^00-7^30
15	7	4.1	2	*°0^40-6^10*°-8^10•°9^22-10^40,11^35...12^15
16	4	4.9	pż.	*°0^05-6^35•°7^20-10^10,11^15-15^40*°18^30;=7^30-10^10,12^18-13^15≡°-14^10=-15^40
17	6	1.3	•	•°11^18...12^05*°...12^36*°13^07...14^20;=7^30-24
18	5	•	•	≡^{0-1}0^50-8^45≡'-9^40=-22^30;°2^00-24
19	7	0.1	•	*°10^04-47,11^10...14^35;=-13^50-14^30;°0^00-10^00
20	7	•	•	=°8^30-9^30;°3^00-24
21	8	•	•	°0^00-24
22	7	•	•	°0^00-11^00,20^00-24
23	7	•	•	=9^30-10^30;°0^00-24
24	7	•	•	∞9^30-12^30;°0^00-24;⊕12^15-14^15
25	8	•	•	°0^00-14^00
26	7	0.0	•	°0^00-24
27	5	0.0	•	*'2^{25...30}*°11^05...16^35;=7^30-24;°0^00-11^00
28	5	0.4	•	*°0^10...3^40,8^35...9^00-13^25...14^30,22^45-24;=0^00-24
29	6	0.0	1	*°0^00-10^45,12^15-14^20;0^00-24
30	2	•	1	=0^00-7^45≡^{0-1}-14^50=-24;'1^00-9^50▽°-24
31	7	•	1	=0^00-5^30;▽°0^00-5^30
Σ	—	32.9	—	UWAGI.

Poznań - Ławica φ = 52°25' λ = 16°50' Styczeń - Janvier 1962

DNI	CIŚNIENIE P − 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	95.2	96.9	98.6	96.2	3.9	2.9	0.8	2.1	4.4	-0.5	61	71	81	71	3.2	2.2	1.5	2.2	4	9	9	W 8	WSW 12	WSW 7
2	99.7	102.1	107.4	103.1	-0.4	-0.8	-3.3	-2.0	1.3	-3.3	88	95	81	88	0.7	0.3	0.9	0.6	10	10 △	6	WSW 7	W 7	WNW 6
3	108.8	110.7	114.5	111.3	-4.7	0.0	0.0	-1.2	0.3	-6.6	83	94	98	92	0.7	0.4	0.1	0.4	10	10 ●	10 ●	WSW 6	W 5	C 0
4	116.1	115.7	115.4	115.7	-0.6	-0.7	-2.0	-1.3	0.1	-2.0	93	87	98	93	0.4	0.7	0.1	0.4	10	10	10 ●	SSW 2	SSW 3	W 5
5	112.9	111.2	107.0	110.4	-2.9	-3.0	-4.5	-3.7	-1.9	-5.6	93	93	86	91	0.3	0.4	0.6	0.4	10 ●	10	10	W 4	W 5	WSW 6
6	103.8	101.4	100.2	101.8	-2.9	-1.0	1.0	-0.5	1.2	-5.4	86	89	98	91	0.7	0.7	0.2	0.5	10	10	10	WSW 7	WSW 9	W 9
7	106.2	112.1	115.3	111.2	1.4	0.8	-2.4	-0.6	1.9	-2.6	89	88	96	91	0.8	0.8	0.2	0.6	9	9	2	WNW 9	NW 7	SW 1
8	113.7	114.4	113.2	113.8	0.0	1.0	1.1	0.8	1.6	-3.3	98	100	100	99	0.1	0.0	0.0	0.0	10 ●	10 ≡	10 ≡	SW 4	SW 2	SW 2
9	108.0	104.2	102.6	104.9	0.9	2.6	0.8	1.3	2.9	0.8	94	75	81	83	0.4	1.9	1.3	1.2	9	8	10	S 3	S 8	SSW 6
10	97.8	95.1	92.7	95.2	0.2	0.9	-0.2	0.2	1.4	-0.3	80	70	78	76	1.2	2.0	1.3	1.5	8	8	0	S 7	S 5	S 6
11	93.4	89.2	88.0	90.2	0.3	3.3	4.1	3.0	4.4	-0.4	86	78	82	82	0.8	1.7	1.5	1.3	2	10 ●	10	S 5	S 8	S 8
12	92.4	91.6	82.3	88.8	2.0	4.4	3.0	3.1	6.3	1.5	91	84	83	86	0.7	1.4	1.3	1.1	9	7	10	SW 4	SW 4	S 7
13	77.0	79.3	83.6	80.0	2.5	5.7	0.7	2.4	5.9	0.7	95	62	83	80	0.4	3.5	1.1	1.7	0	4 ⊙	3	SW 7	WSW 10	S 5
14	87.6	90.2	91.8	89.9	1.5	3.8	1.4	2.0	4.3	0.5	87	70	92	83	0.9	2.4	0.6	1.3	9	6 ⊙	10 ●	SW 5	SW 7	SW 6
15	98.4	102.4	107.2	102.7	2.2	3.2	2.2	2.4	3.4	1.4	89	83	80	84	0.8	1.3	1.5	1.2	10 ●	9 ●	9	SW 7	WSW 7	SW 4
16	109.2	107.5	103.8	106.8	-0.7	2.1	2.3	1.5	3.0	-1.2	89	77	75	80	0.6	1.7	1.8	1.4	4	10	10	SSW 6	S 5	S 8
17	102.0	103.3	104.4	103.2	2.6	3.5	1.3	2.2	4.0	1.1	75	71	83	76	1.9	2.2	1.1	1.7	10	9	9	SW 6	SSW 6	S 3
18	103.0	101.6	102.8	102.5	-0.5	3.0	1.8	1.5	3.5	-1.0	84	76	85	82	1.0	1.9	1.1	1.3	3	9	9	S 2	SW 7	SW 5
19	105.1	104.3	98.2	102.6	0.6	4.7	4.3	3.5	5.2	-0.2	92	81	84	86	0.5	1.6	1.4	1.2	8	0 ⊙	10 ●	SW 5	SW 5	SSW 8
20	100.9	105.3	110.3	105.5	4.0	5.2	4.4	4.5	6.9	3.5	80	73	80	78	1.6	2.3	1.7	1.9	8	9	10	SW 9	W 9	W 5
21	107.6	107.7	104.8	106.7	3.9	6.7	5.4	5.4	7.2	0.1	82	100	97	93	1.5	0.0	0.3	0.6	10 ●	10 ●	8	SW 5	SW 3	SW 4
22	97.2	92.0	96.4	95.2	6.6	8.6	4.7	6.2	9.3	3.8	88	74	73	78	1.1	2.9	2.3	2.1	9	10	4	S 6	SW 9	WSW 10
23	100.1	101.5	103.5	101.7	1.6	5.7	3.3	3.5	6.0	1.4	85	67	81	78	1.1	3.1	1.4	1.9	6	4 ⊙	10 ●	SW 8	SW 10	SW 8
24	104.7	104.2	101.3	103.4	1.0	2.7	2.0	1.9	3.4	0.4	87	93	96	92	0.9	0.5	0.3	0.6	0	10	10 ●	SW 6	SW 7	S 3
25	95.3	94.3	96.5	95.4	3.6	7.6	5.9	5.8	8.2	0.7	98	93	92	94	0.1	0.7	0.7	0.5	10 ●	10	10 ●	S 3	SW 5	W 7
26	106.9	108.1	103.7	106.2	0.8	3.0	0.6	1.2	6.0	-0.9	92	86	90	89	0.5	1.1	0.6	0.7	8	9	10 *	W 5	W 3	S 5
27	103.0	105.4	103.0	103.8	2.8	4.2	2.9	3.2	4.5	0.0	93	80	88	87	0.6	1.6	0.9	1.0	9	9	7	WNW 9	NW 10	W 10
28	103.2	104.7	108.8	105.6	0.9	-1.1	-3.9	-2.0	3.2	-4.3	87	69	85	80	0.9	1.8	0.7	1.1	7	9 *	8 *	NW 7	N 10	NW 8
29	114.3	118.3	122.5	118.4	-4.1	-4.1	-7.4	-5.8	-3.3	-7.5	84	73	62	73	0.7	1.2	1.3	1.1	9 *	9	0	N 8	NE 9	NE 6
30	125.4	127.8	129.5	127.6	-9.7	-6.9	-9.9	-9.1	-6.2	-11.0	72	64	78	71	0.8	1.3	0.6	0.9	4	0 ⊙	0	NE 5	NE 7	E 3
31	128.0	126.3	122.0	125.4	-13.0	-7.3	-10.8	-10.3	-6.6	-14.0	76	57	73	69	0.5	1.5	0.7	0.9	0	0	0	E 3	SE 3	E 2
M	103.7	104.2	104.2	104.0	0.1	2.0	0.3	0.7	3.0	-1.7	86	80	85	84	0.9	1.5	0.9	1.1	7.3	8.0	7.5	5.7	6.7	5.6

Luty - Février

1	111.5	105.7	104.9	107.4	-12.1	-8.1	-8.1	-9.1	-7.3	-12.5	93	69	75	79	0.2	1.0	0.8	0.7	0	9 * ⊙	0	SE 3	S 5	SW 2
2	105.0	106.4	109.6	107.0	-7.9	-2.3	-5.4	-4.2	-1.1	-11.6	78	72	81	77	0.7	1.5	0.9	1.0	9	8	10	SW 4	S 5	SW 1
3	113.8	115.6	115.0	114.8	-5.1	0.0	-1.3	-1.4	0.5	-5.7	88	96	89	91	0.6	0.2	0.6	0.5	10	10	10	C 0	SW 2	SW 1
4	106.5	106.6	109.1	107.4	-2.2	0.8	-2.0	-1.4	2.9	-5.6	79	88	91	86	1.1	0.8	0.5	0.8	10	10	0	SSW 9	W 7	SW 3
5	102.5	91.1	93.7	95.8	-2.1	-0.1	2.6	0.8	2.7	-4.0	89	98	82	90	0.5	0.2	1.3	0.7	9	10 *	10	S 3	S 8	W 9
6	101.3	105.4	108.8	105.2	2.6	3.7	1.8	2.5	4.6	1.1	72	65	85	74	2.1	2.8	1.1	2.0	9	8	4	W 10	WNW 10	W 7
7	106.2	104.1	100.8	103.7	0.4	4.0	2.5	2.4	4.1	-0.6	96	92	91	93	0.3	0.6	0.6	0.5	10	10	10	S 3	S 4	SSE 2
8	98.0	99.8	102.8	100.2	1.3	4.2	0.8	1.8	4.3	0.7	92	90	100	94	0.5	0.8	0.0	0.4	10	10	10 ≡	S 4	SW 3	S 3
9	108.8	114.0	119.9	114.2	0.7	1.6	-1.5	-0.2	3.5	-1.6	94	89	89	91	0.4	0.8	0.6	0.6	10	10	0	NW 6	NW 8	W 4
10	121.1	119.8	117.3	119.4	-1.5	1.6	1.4	0.7	2.7	-5.7	92	83	85	87	0.4	1.2	1.0	0.9	9	9	10	SW 3	SW 6	SW 5
11	110.6	111.8	115.0	112.5	1.3	1.8	1.5	1.5	4.0	0.7	81	85	78	81	1.3	1.1	1.5	1.3	10	10 ● *	0	SW 7	NW 13	W 7
12	97.0	81.6	72.9	83.8	0.6	3.4	2.3	2.2	5.8	-0.1	88	91	86	88	0.8	0.7	1.0	0.8	10 *	10 ●	10	SW 12	SW 12	W 10
13	74.1	74.0	76.0	74.7	2.6	2.6	0.2	1.4	4.4	-0.9	72	79	88	80	2.1	1.6	0.7	1.3	5	8 ⊙	5	W 9	W 5	W 4
14	81.2	83.4	91.3	85.3	-0.8	0.0	-2.1	-1.2	0.9	-2.2	91	77	83	84	0.3	1.4	0.9	0.9	9	8	9 *	WNW 4	NW 3	N 8
15	101.2	105.3	109.6	105.4	-4.5	-1.9	-5.7	-4.4	-1.3	-5.8	84	77	72	78	0.7	1.2	1.1	1.0	1	9 *	9	NW 7	NNW 9	W 4
16	90.9	80.7	76.8	82.8	-2.9	2.4	1.4	0.6	3.6	-6.3	95	96	89	93	0.2	0.3	0.8	0.4	10 *	10 ● *	10	SW 10	WSW 10	W 9
17	74.9	78.8	89.4	81.0	1.0	2.7	-0.5	0.7	3.2	-0.9	92	81	92	88	0.5	1.4	0.5	0.8	10 *	10 ● *	9 * △	W 12	WNW 15	NNW 15
18	99.6	105.3	111.3	105.4	-1.5	0.6	-0.3	-0.3	1.6	-3.6	74	73	70	72	1.5	1.8	1.8	1.7	6	9	9	NW 12	NW 13	W 6
19	106.1	106.3	107.9	106.8	-0.9	3.1	3.6	2.4	4.3	-1.6	97	95	90	94	0.2	0.4	0.8	0.5	10 *	10	10	SSW 4	W 8	W 8
20	107.8	106.4	107.9	107.4	2.6	6.6	3.4	4.0	7.7	2.5	82	75	85	81	1.3	2.4	1.2	1.6	10	8 ⊙	1	W 8	W 12	NW 9
21	112.8	116.0	120.3	116.4	-0.2	0.2	-0.7	-0.4	3.4	-0.9	72	76	64	71	1.7	1.3	2.1	1.8	4	10 *	9	NW 8	NNW 12	NNE 10
22	124.0	124.8	126.1	125.0	-5.0	-3.1	-3.1	-3.1	-0.7	-4.0	73	70	64	69	1.3	1.4	1.8	1.5	10	9	10	NE 9	E 7	NE 6
23	126.4	121.9	117.9	122.1	-4.7	0.4	-0.6	-1.4	1.1	-5.7	71	68	77	72	1.2	2.0	1.3	1.5	9	9	10	N 4	N 9	NE 9
24	112.9	111.5	112.1	112.2	-2.3	-3.8	-4.6	-3.8	-0.6	-5.0	85	80	81	82	0.8	0.9	0.8	0.8	10 *	10 *	10 *	NE 7	ENE 9	ENE 7
25	113.2	114.5	114.8	114.2	-6.4	-5.3	-4.3	-5.1	-4.2	-6.7	81	65	77	74	0.7	1.4	1.0	1.0	10 △	9 *	10 *	ENE 8	E 8	E 8
26	112.6	112.0	111.7	112.1	-2.9	-1.3	-2.0	-2.0	-1.1	-4.8	86	76	83	82	0.7	1.3	0.9	1.0	10 *	10 *	10	E 7	E 7	E 7
27	110.5	109.5	108.5	109.5	-2.9	-2.3	-2.6	-2.6	-2.0	-2.9	82	78	87	82	0.9	1.2	0.7	0.9	10	10	10 *	E 8	E 7	E 4
28	105.4	103.7	102.5	103.9	-4.5	-2.1	-2.9	-3.1	-1.4	-4.5	84	68	71	74	0.7	1.6	1.4	1.2	10	9	9	E 6	ENE 6	E 4
29																								
30																								
31																								
M	104.8	104.2	105.5	104.8	-1.9	0.3	-0.9	-0.8	1.6	-5.3	84	80	82	82	0.9	1.2	1.0	1.0	8.6	9.4	7.6	6.7	8.0	6.1

Poznań - Ławica H_s = 86m H_b = 92,1m h_w = 13m Styczeń - Janvier 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	0.0	3	•°0^00-1^15; ⤳6^15-16^10; = 0^00-1^45
2	6	0.1	3	•°5^40...6^30 ⁂°11^20-35 ⁂°-12^30 ♨-16^30; = 8^10-17^30
3	5	0.0	3	⁂°7^20-30 ⚲7^40-10^35, 11^45-24; = 7^30-24; ∼9^15-24
4	6	0.0	3	⚲0^00-3^35, 20^10-24; = 0^00-24; ∼0^00-24
5	5	0.0	3	⚲0^00-7^40 8^10-11^15; ∼0^00-24; = 0^00-24
6	4	1.2	3	⚲14^30-45 ♨14^50-15^10 ⁂°-17^15 •°-20^35; = 0^00-24; ∼0^00-24
7	7	0.0	pł.	•°1^35-2^40; = 0^00-7^10; ⌴'22^00-24; ∼0^00-4^00
8	2	0.2	pł.	•°6^20-12^40 16^30-20^27; = 4^15-8^15 ≡-8^45 ≡'-2 -12^50 ≡'-13^50 = -16^20 ≡'-2 -24; ⌴'0^00-8^00
9	6	•	pł.	≡°0^00-1^20 = -10^30 ∞-15^50 = -24
10	6	0.0	pł.	•°18^20...35; = 0^00-11^30 ∞-14^40 = -24
11	6	0.1	pł.	•°12^35-14^40 15^45-16^25, 17^35...18^40; ⤳11^15-12^30; = 0^00-24
12	6	5.5	pł.	•°21^40-24; = 0^00-21
13	7	0.0	•	•°0^00-4^20; ⤳12^10-15^20; = 0^00-4^30; ⌴°20^00-24
14	7	1.3	•	•°2^40...3^05 4^35...5^25 ⚲°-1 9^20-45 ⚲°12^05-15 •°16^40-24; = a,p-24; ⌴°0^00-9^00
15	6	0.2	•	•°0^00-2^25 3^45-8^30 •°9^20...10^30 11^45...12^10 •°12^45-13^20; = 0^00-24
16	6	0.2	•	= 0^00-10^00 ∞-12^30 = -24; ⌴°4^00-10^00
17	6	0.0	•	•°2^35-3^30...4^20 10^05-35; = 0^00-1^30 8^15-9^40 ∞-16^45 = -24
18	6	•	•	= 0^00-24; ⌴°4^00-9^00; ⌣ 0^30-3^35
19	6	0.9	•	•°20^17-21^35; = 0^00-24; ⌴°5^00-9^00
20	7	0.8	•	⚲'-0 1^30-2^05; ⤳1^05-2^20 7^04-9^40 12^56-16^35; = 0^00-1^25
21	4	1.7	•	•°4^40...5^20-7^40 •°-12^30...13^40 •, •°13^50-14^40 •°15^05-16^30 •°16^35-17^15 •°-18^20; = na-a ≡°8^30-11^20; = -24; ⊕ 22^40-23^40
22	7	0.0	•	•°13^02-40 ⚲°17^20-25; ⤳15^45-24; = 0^00-7^40; ⊕ 1^40-2^30
23	7	0.0	•	•°20^45...21^20 ⚲°23^15-25; ⤳0^00-3^10 11^10-13^36; ⌴°2^00-9^00
24	6	4.4	•	⁂°9^45...10^02 •°11^50...12^05 18^35-23^30 ⁂°-24; = 7^15-24
25	6	5.6	•	⁂°0^00-2^35 •°-5^40 •°-7^10 •°-1-12^50 •°16^06-17^35 •°19^35...23^25; = 0^00-24
26	6	2.0	•	•°19^20-40 ⁂°-1 19^45-24; = 0^00-14^30 16^45-24
27	7	0.7	•	'-0 0^00-1^45 ⁂°-3^40 •, •°-5^35 •°7^15...40 •°...9^50 ⚲°14^20-28, 16^32-17^40; ⤳8^50-14^50, 16^30-45, 17^20-23^05
28	7	0.4	•	⚲°8^05-40 ⚲°-1 12^50...24; ⤳8^40-19^30
29	7	0.0	2	⚲°0^00-3^20, 3^30-40 5^10-30, 6^35-9^16 ⚲'-9^40 ⚲°-12^45; ⤳0^30-3^20; = 9^40-11^15
30	7	0.0	2	⚲°0^45-1^30, 4^07-6^30; ∞16^30-19^40 = -24
31	5	•	1	= 0^00-12^40 ∞-21^30 = -24; ⌴'2^00-10^00
Σ	—	23.3	—	UWAGI:

Luty - Février

1	6	0.0	pł.	⁂°11^25-14^35, 17^50-18^26; = 0^00-9^40 ∞-20^50 = -24; ⌴'3^00-12^00
2	6	•	pł.	= 0^00-10^40 ∞-16^30 = -24
3	4	•	pł.	= 0^00-24
4	6	0.0	pł.	⁂°8^05-9^25 •°10^20-11^40; = 0^00-24; ⌴°2^00-15^00, 21^00-24
5	4	5.2	pł.	⁂°9^20...10^20-13^10 ⁂°-1 14^40 ⚲°16^40-17^10, 22^15-30; ⤳np; = 0^00-18^20; ⌴°-1 0^00-9^00
6	8	0.0	pł.	⚲°0^20-45 9^30-10^15; ⤳0^00-16^15
7	5	0.1	•	•°8^05-40; '-10^20; = 1^10-24; ⌴°0^00-7^00
8	5	0.6	•	•°8^40...9^40; = 0^00-16^10 ≡°-2 21^40 = -24
9	6	0.1	•	•°1^20...50 2^35-3^30 10^02-08 ⁂°-12^30; = 0^00-5^30 a-p; ⌴°20^00-24
10	6	0.7	•	⁂°16^50...17^15; = 6^35-24; ⌴°-1 0^00-10^00; ⌣ 19^40-20^20
11	4	2.9	•	♨0^42-50 •°1^30-45 •°-2^40 3^05...45 •, •, •°7^05-8^35 •°9^10-45 ⁂°; ⚲'-13^05 ⚲°14^02-15 ♨14^08-11; ⤳a-p; = 0^00-p; ⌴np
12	6	12.0	1	⁂'6^08-10^20 •°-16^15 17^15-18^05 ⚲-18^30 ⚲'-20^15 ⚲°21^45-22^45; ⤳6^05-24; = na-p; ⌴na
13	7	0.2	•	⚲°0^20-1^13 7^35-45 ⚲°11^02-35 2^50-22^05; ⤳0^00-5^10; ⌴°18^00-24
14	7	0.5	1	⚲°3^35...7^25 ⁂°...8^38 ⚲°♨10^20...17^45 ⚲°19^05-15 19^50-22^35; = p-np; ⌴°na
15	8	1.0	1	⁂°3^40-5^10 ⚲°-1 10^45 16^30; ⤳4^45-5^15 13^25-14^45; ⌣ 19^40-20^30 ⊕ 20^50-22^35
16	5	14.5	3	⁂°-1 3^15-10^20 •°-16^40 ⚲°-17^12 ⚲'18^33-19^01 ⚲'-19^45 ⚲°22^20-45; ⤳na-a; ⤳na-p; = na-p
17	6	2.4	pł.	⚲°-1 ⚲°-1 ⚲°-1 0^00...17^10 ♨'9^45-10^15 ♨°20^35-23^45 ⚲°-24; ⤳ 0^00-24
18	8	2.2	pł.	⚲°0^00-50 10^45-12^05 13^20-14^10; ⤳0^00-18^10; ⊕ 21^15-22^30
19	6	1.4	5	⁂°-1 1^30-7^30 ⚲°-7^35 •, •°-10^10 •°11^02-12^26 ⚲°15^30-16^06 •°16^30...23^27; ⤳a,p; = na-p, p-24
20	7	0.0	•	•°1^50-3^10 8^15-26, 14^45...15^40; ⤳0^20-2^30 8^50-19^45; = na
21	7	0.1	•	⚲°, ⁂°7^40...20^18 ⁂°22^40...23^25; ⤳8^45-23^30; ⌴°na-a
22	7	0.0	pł.	⁂°-1 0^15...9^30 ⚲°9^40...24; = 8^10-11^40, 16^40-18^15
23	7	0.0	pł.	⚲°0^00-30; ⤳11^20-35, 13^15-14^30
24	5	0.2	•	⁂°6^15...7^40-13^40, 14^15-20^20...24; ⤳p,np; = 7^30-24
25	6	0.4	1	⁂°0^00, 6^40 ♨-10^15 ⁂°-13^10 15^45-24; = 0^00-12^30 ∞-17^50 = -24
26	6	0.0	pł.	⁂°0^00-1^25, 2^40-10^10, 12^40-14^15, 15^20-16^10; = na, na-24
27	6	1.8	pł.	⁂°19^35-24; = 0^00-24
28	6	0.0	2	⁂°0^00...7^30; = 0^00-11^30 ∞-21^30 = -24
29				
30				
31				
Σ	—	46.3	—	UWAGI:

Poznań-Ławica φ=52°25' λ=16°50' Marzec-Mars 1962

DNI	CIŚNIENIE P=900+ I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	100.9	99.9	98.7	99.8	-5.3	-1.9	-4.3	-4.0	-1.6	-5.4	73	67	79	73	1.1	1.8	0.9	1.3	6	1 ⊙	4	E 4	NE 4	C 0
2	95.6	93.8	93.2	94.2	-4.6	-0.5	-1.1	-1.8	0.5	-6.6	81	64	77	74	0.8	2.1	1.3	1.4	10	9	10	W 1	SW 1	W 1
3	93.3	93.2	92.3	92.9	-2.2	1.2	-0.8	-0.6	1.9	-3.8	89	83	94	89	0.6	1.2	0.4	0.7	10 *	9	6	S 2	SW 4	S 1
4	87.5	85.5	85.1	86.0	-0.5	2.2	0.0	0.4	2.3	-1.2	92	89	98	93	0.5	0.8	0.1	0.5	10	10 ●	10 *	E 2	NE 4	NE 6
5	86.8	86.2	84.6	85.9	-0.5	0.1	0.3	0.0	0.4	-0.7	90	92	98	93	0.6	0.5	0.1	0.4	10 *	10 ●	10	NE 7	E 10	ENE 6
6	86.0	94.3	104.6	95.0	-2.1	-0.5	-5.5	-3.4	0.4	-5.6	96	90	85	90	0.2	0.6	0.6	0.5	10 *	10 *	0	NW 6	NNW 6	NW 5
7	110.8	112.6	115.4	112.9	-8.2	-0.1	-5.0	-3.6	1.4	-11.4	81	75	90	82	0.6	1.6	0.5	0.9	9	7 ⊙	2	NW 3	NW 6	NW 1
8	116.7	117.6	116.6	117.0	-10.8	1.4	-5.1	-4.9	3.5	-11.4	83	72	88	81	0.4	1.9	0.5	0.9	10 ═	0 ⊙	0	C 0	SW 2	SW 1
9	115.2	112.6	105.9	111.2	-5.1	1.8	0.3	-0.7	2.6	-6.8	88	67	69	75	0.5	2.3	1.9	1.6	4	5 ⊙	9	E 2	ESE 9	ESE 8
10	101.7	100.1	98.3	100.0	-1.8	3.8	1.8	1.4	3.8	-1.9	75	62	80	72	1.3	3.0	1.5	1.9	4 ⊙	10	10	SE 7	S 7	SE 2
11	95.6	95.2	93.6	94.8	2.2	8.1	4.2	4.7	10.3	1.5	82	67	88	79	1.3	3.6	0.9	1.9	9	2 ⊙	10	S 5	SW 4	S 1
12	89.8	87.1	85.9	87.6	1.7	5.5	-1.1	1.2	5.7	-1.1	98	84	97	93	0.1	1.4	0.2	0.6	10 ●═	10 ●	10 *	E 1	C 0	N 9
13	93.6	97.4	102.4	97.8	-3.7	-2.4	-7.0	-5.0	-0.9	-7.1	80	72	80	77	0.9	1.4	0.7	1.0	10 *	9 *	0	NW 10	NW 12	W 7
14	106.3	108.3	108.8	107.8	-8.0	-2.0	-5.9	-5.4	-0.9	-10.2	84	62	81	76	0.5	2.0	0.7	1.1	3 ⊙	4 ⊙	6	W 6	W 6	S 3
15	107.7	108.3	111.3	109.1	-5.5	0.8	-2.7	-2.5	0.9	-7.0	75	41	60	59	1.0	3.9	2.0	2.3	9	8	10	S 5	S 7	SE 3
16	114.0	114.9	114.1	114.3	-5.7	-2.0	-3.4	-3.6	-1.7	-7.6	74	56	63	64	1.0	2.3	1.8	1.7	10	9	10	NE 5	NE 7	N 6
17	109.9	107.4	108.1	108.5	-3.5	0.5	-1.3	-1.4	1.2	-5.0	83	74	72	76	0.8	1.6	1.6	1.3	10	9	8	N 8	N 10	N 8
18	108.7	109.4	109.8	109.3	-4.9	1.0	-1.7	-1.8	2.2	-5.7	88	71	84	81	0.5	1.9	0.9	1.1	5	6 ⊙	9	NW 5	N 6	N 3
19	109.9	110.2	109.3	109.8	-5.1	2.2	-0.3	-0.4	3.2	-5.3	86	71	72	76	0.7	2.1	1.7	1.5	8	7 ⊙	10	C 0	SW 2	SE 1
20	108.8	108.3	107.3	108.1	-2.5	1.6	-0.1	-0.3	3.5	-4.0	95	71	82	83	0.3	2.1	1.1	1.2	8 ⊙	7	9	S 2	SSE 1	SE 2
21	106.3	105.2	104.2	105.2	-1.7	2.7	-1.0	-0.2	3.2	-1.8	84	53	69	69	0.9	3.4	1.8	2.0	6	1 ⊙	0	SE 2	SE 7	E 5
22	101.8	100.7	99.6	100.7	-4.2	1.4	-1.7	-1.6	2.1	-4.6	84	52	69	68	0.7	3.3	1.7	1.9	0 ⊙	3 ⊙	0	NE 5	E 7	E 2
23	99.1	99.7	101.4	100.1	-4.2	1.0	-1.3	-1.4	2.8	-6.0	89	59	72	73	0.5	2.8	1.6	1.6	1 ⊙	6 ⊙	1	NE 5	NE 6	NE 4
24	104.3	106.8	109.3	106.8	-5.1	1.0	-1.9	-2.0	2.6	-6.5	85	57	79	74	0.6	2.9	1.1	1.5	6	3	1	N 3	N 6	C 0
25	110.7	110.4	108.8	110.0	-5.3	4.0	-1.9	-0.8	4.5	-4.9	90	39	78	69	0.5	4.9	1.2	2.2	2	3 ⊙	0	SE 1	W 3	C 0
26	106.5	104.5	101.5	104.2	-2.6	4.5	0.0	0.5	5.6	-3.6	86	45	56	62	0.7	4.6	2.7	2.7	3 ⊙	6 ⊙	0	SE 2	SE 6	SE 6
27	97.0	94.4	92.0	94.3	-2.6	3.4	0.9	0.6	3.6	-3.0	73	44	71	63	1.4	4.4	1.8	2.5	7 ⊙	6	10	SE 7	ESE 8	SE 8
28	89.9	91.1	95.4	92.1	1.5	5.5	1.4	2.4	7.5	-0.5	87	63	85	78	0.9	3.3	1.0	1.7	9 ●	7 ⊙	10	SW 5	W 9	NW 7
29	97.3	94.8	88.6	93.6	0.2	5.5	4.9	3.9	7.0	-0.2	80	65	73	73	1.2	3.1	2.4	2.2	9	6 ⊙	10	NW 5	S 2	SE 5
30	83.3	83.7	80.8	82.6	5.1	11.4	9.0	8.6	14.3	3.4	97	76	85	86	0.3	3.3	1.7	1.8	10	9	10	SW 4	SW 5	S 3
31	74.6	79.9	84.8	79.8	9.6	9.9	7.3	8.5	12.7	7.2	92	78	62	77	1.0	2.7	3.9	2.5	10	9 ⊙	10	SSW 8	W 12	NW 4
M	100.3	100.4	100.4	100.4	-2.6	2.3	-0.7	-0.4	3.4	-4.2	85	66	79	77	0.7	2.5	1.3	1.5	7.4	6.5	6.3	4.1	5.8	3.8

Kwiecień-Avril

1	91.2	94.7	96.6	94.2	2.2	6.5	3.4	3.9	7.6	1.2	95	62	81	79	0.4	3.7	1.5	1.9	10 ●	7	8	WSW 1	W 8	SW 7
2	96.7	97.6	101.6	98.6	2.0	8.0	3.4	4.2	8.5	0.6	96	63	76	78	0.3	3.9	1.9	2.0	10	9	0	SW 6	SW 8	SW 4
3	99.6	95.8	92.3	95.9	5.0	14.0	10.0	9.8	15.8	1.9	94	36	59	63	0.5	10.2	5.1	5.3	10 ●	5 ⊙	0	S 7	SW 12	S 6
4	88.4	87.9	84.2	86.8	5.8	12.7	7.7	8.5	14.0	5.4	76	56	89	74	2.2	6.5	1.2	3.3	9	9 ⊙	10 ●	S 5	SW 7	SW 5
5	77.3	76.0	78.6	77.3	6.9	12.0	5.0	7.2	12.7	5.0	94	65	86	82	0.5	4.9	1.2	2.2	10 ●	8	0	SE 2	NW 2	W 1
6	82.8	86.3	92.8	87.3	3.0	10.6	7.0	6.9	12.6	1.4	95	55	81	77	0.4	5.8	1.9	2.7	3 ⊙	8	10	SW 3	W 5	NNW 8
7	100.5	100.9	97.5	99.6	1.6	6.6	4.5	4.3	8.8	1.0	89	48	81	73	0.8	5.0	1.6	2.5	10	8	10 ●	NW 10	W 10	SW 6
8	93.9	94.5	93.6	94.0	6.9	10.5	10.0	9.4	11.6	3.9	91	71	66	76	0.8	3.7	4.2	2.9	10 ●	10	10	SW 8	SSW 10	SW 7
9	98.1	100.1	104.3	100.8	5.1	11.7	6.1	7.2	13.4	3.4	75	40	88	68	2.2	8.2	1.1	3.8	3 ⊙	9	9	SW 8	SW 6	SW 2
10	108.7	110.4	111.9	110.3	1.0	7.6	3.2	3.8	9.0	-0.2	98	60	84	81	0.2	4.2	1.2	1.9	1 ⊙	9	3	SW 1	W 5	S 1
11	113.1	111.8	110.9	111.9	1.4	12.2	8.0	7.4	13.1	0.0	94	40	84	73	0.4	8.5	1.6	3.5	2 ⊙	8	10	S 1	SE 1	C 0
12	109.3	106.8	105.5	107.2	4.4	15.7	9.2	9.6	15.9	1.9	87	37	80	68	1.1	11.2	2.3	4.9	2	3 ⊙	10	SW 1	SW 3	SW 3
13	104.5	104.5	104.0	104.3	6.7	7.3	4.7	5.8	9.5	4.3	97	74	73	81	0.3	2.6	2.3	1.7	10 ●	10	9	W 3	NE 3	N 1
14	106.0	109.4	113.8	109.7	3.7	5.4	3.6	4.1	5.9	2.3	93	75	93	87	0.6	2.3	0.5	1.1	10 ●	10 ●	10 ●●	NNE 3	NNE 7	NE 6
15	114.8	114.2	113.3	114.1	4.1	5.8	8.4	6.7	8.5	3.5	87	85	87	86	1.1	1.4	1.4	1.3	10	10	10	NE 7	NE 9	E 10
16	111.7	108.5	109.7	110.0	7.8	16.0	7.6	9.8	18.7	7.2	90	59	91	80	1.1	7.5	0.9	3.2	10	5 ⊙	8	E 9	E 12	NW 5
17	110.4	107.3	105.9	107.9	9.3	19.9	15.4	15.0	20.4	5.9	85	42	58	62	1.7	13.5	7.4	7.5	8	10	10	SE 4	SE 7	SE 5
18	103.4	102.0	101.7	102.4	12.6	21.6	16.0	16.6	23.3	11.6	63	39	60	54	5.4	15.9	7.4	9.6	9	10	10	SE 5	S 8	SE 3
19	102.5	103.7	104.9	103.7	12.5	23.4	16.0	17.0	24.6	10.4	71	39	76	62	4.2	17.7	4.4	8.8	9	9	9	SSE 2	SSW 2	C 0
20	107.6	107.6	106.5	107.2	11.8	19.6	16.0	15.8	22.4	10.8	88	57	84	76	1.6	9.8	2.9	4.8	6 ⊙	9 ⊙	4	NW 4	NW 4	NE 2
21	107.3	107.8	109.2	108.1	14.6	21.6	16.2	17.2	22.6	10.8	74	61	73	69	4.3	10.1	4.9	6.4	1 ⊙	7	9	S 2	SW 4	N 4
22	109.5	108.9	108.5	109.0	13.0	24.6	17.6	18.2	26.5	10.6	86	45	77	69	2.1	17.0	4.5	7.9	4 ⊙	5 ⊙	0	E 5	E 4	ENE 3
23	109.1	109.2	110.0	109.4	15.4	26.3	19.5	19.7	27.9	9.4	94	42	68	68	0.9	20.0	7.3	9.4	0 ⊙	1 ⊙	0	ESE 1	NW 2	NE 8
24	113.6	114.2	115.3	114.4	10.8	23.8	16.8	17.0	25.0	9.2	79	49	80	69	2.8	15.1	3.9	7.3	0 ⊙	1	0	E 6	E 4	E 5
25	116.6	116.2	114.4	115.7	14.6	25.4	19.1	19.6	27.1	10.5	78	46	61	62	3.6	17.4	8.7	9.9	5	3 ⊙	3	E 3	SE 3	SE 3
26	111.3	107.9	103.4	107.3	13.3	22.2	15.2	16.5	22.8	11.1	90	48	72	70	1.6	14.0	4.6	6.8	3 ⊙	3 ⊙	10 ●	NW 2	NW 7	NW 6
27	101.0	102.9	100.7	101.3	7.7	7.5	7.6	7.6	15.3	7.0	76	69	62	69	2.5	3.2	3.9	3.2	8 ⊙	9	4	NW 9	NW 10	W 5
28	92.4	93.6	96.9	94.3	6.4	9.1	4.0	5.9	10.9	3.7	76	55	90	74	2.3	5.3	0.8	2.8	9	8 ⊙	9 ●	NW 9	NW 10	N 5
29	98.3	97.0	97.3	97.5	4.6	6.7	0.8	3.2	10.0	0.7	82	74	94	83	1.5	2.6	0.4	1.5	8 ⊙	8 ⊙	4	NW 6	N 7	N 2
30	99.5	102.1	104.7	102.1	1.1	4.2	1.6	2.1	5.9	0.3	85	53	60	66	1.0	3.8	2.8	2.5	9 ⊙	9	6	NE 5	NNE 7	N 5
31																								
M	102.6	102.7	103.0	102.8	7.1	14.0	9.5	10.0	15.7	5.2	86	55	77	73	1.6	8.5	3.1	4.4	6.6	7.3	6.5	4.6	6.2	4.2

Poznań - Ławica $H_s = 86m$ $H_b = 92{,}1m$ $h_w = 13m$ Marzec - Mars 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	6	.	pł.	$=0^{00}-8^{30}\infty-16^{50}=-24$
2	6	0.0	pł.	$*^{\circ}13^{20-40};=0^{00}-10^{30}\infty-20^{40}=-24$
3	5	0.0	pł.	$*^{\circ}4^{40}-6^{10};6^{45}-9^{10};=0^{00}-24;\smile^{\circ}3^{00}-5^{00}$ np
4	5	0.8	pł.	$*^{\circ}7^{15}...8^{13}-10^{20}\bullet^{\circ}11^{40}-15^{26}*;\bullet^{\circ}-19^{40}*^{\circ}-24;=0^{00}-24;\smile^{\circ}0^{00}-7^{00}$
5	5	10.1	1	$*^{\circ}0^{00}-10^{20}\bullet^{\circ}10^{30}-14^{10}\ 21^{45}-22^{40}\bullet\bullet^{\circ}-24;=0^{00}-24$
6	5	1.1	2	$\bullet\bullet^{\circ};\bullet^{\circ\prime}0^{00}-3^{40}*'-5^{25}*^{\circ\prime}5^{30}-14^{15};15^{10}-18^{05};=0^{00}-20^{30}$
7	7	0.0	6	$*^{\circ}2^{40}-3^{10}\mathbf{v}^{\circ}16^{32}...17^{25};=np;\oplus^{\circ}12^{00}-14^{10}$
8	6	.	6	$=0^{00}-2^{10}=-4^{30}\equiv^{\circ}-6^{15}\equiv'-8^{10}\equiv^{\circ}-8^{50}=,\infty-22^{40}=-24;V'na-a$
9	7	.	5	$\gg 13^{45}-16^{40};18^{50}-20^{25};=0^{00}-1^{40}=-8^{40}\infty-11^{30};V'1^{30}-9^{00}$
10	7	0.1	3	$\bullet^{\circ}16^{10}-18^{40};=6^{15}-7^{30}\infty-11^{10};14^{15}-17^{20}=-24;\oplus 11^{30}-12^{40}$
11	6	0.4	2	$\bullet^{\circ}1^{10-30};=0^{00}-9^{30}\infty-17^{30}=-24$
12	5	6.6	pł.	$\bullet^{\circ}0^{25}...7^{20};9^{15}...10^{25};13^{25}-18^{35}*^{\circ};-24;\dagger np;\gg np;=,\equiv^{\circ}0^{00}-15^{40}\equiv^{\circ\prime};\equiv^{\circ}-18^{25}=-24$
13	7	0.9	(0)	$*^{\circ}0^{00}-4^{15};4^{40}-7^{40}\mathbf{v}^{\circ\prime}12^{35}...18^{00};\dagger 0^{00}-10^{30};\gg 0^{00}-15^{50};=0^{00}-8^{50}$
14	8	.	3	$=20^{20}-24$
15	6	.	2	$=0^{00}-1^{30};5^{30}-7^{30}\infty-24;\oplus 8^{30}-9^{20}\ \mathbf{v}\ 22^{15}-24$
16	6	.	2	$\infty 0^{00}-24;\mathbf{v}\ 0^{00}-1^{20}$
17	7	.	2	$\gg 9^{10}-18^{45};\infty 0^{00-50}=-9^{15};\oplus 9^{30}-10^{40}$
18	7	.	pł.	$\smile^{\circ}5^{00}-8^{00};\mathbf{v}\ 0^{40}-2^{30}$
19	7	.	pł.	$=7^{45}-9^{35}\infty-11^{10};\smile^{\circ}2^{00}-9^{00}$
20	7	.	pł.	$=5^{35}-8^{15}\ 17^{50}-24;\smile^{\circ}2^{00}-9^{00}$
21	6	.	pł.	$=,\infty 0^{00}-24$
22	6	.	pł.	$=,\infty 0^{00}-24;\smile^{\circ}1^{00}-9^{00};22^{00}-24$
23	6	.	pł.	$=,\infty 0^{00}-24;\smile^{\circ}0^{00}-9^{00}$
24	7	.	.	$=0^{00}-8^{30};18^{30}-24;\smile'1^{00}-8^{00}$
25	6	.	.	$=,\infty 0^{00}-24;\smile^{\circ}0^{00}-9^{00};20^{00}-24$
26	6	.	.	$=0^{00}-8^{30}\infty-24;\smile^{\circ\prime}0^{00}-9^{00}$
27	7	.	.	$\infty 0^{00}-8^{40};18^{10}-23^{30}=-24;\smile^{\circ}3^{00}-8^{00}$
28	7	0.3	.	$*^{\circ}2^{45}-3^{10}*\bullet^{\circ}-3^{30}\bullet^{\circ}4^{40}...10^{28}\mathbf{v}^{\circ}14^{10-25};15^{50}-16^{20};=,\infty 0^{00}-12^{20}=18^{45}-24$
29	6	2.1	.	$\bullet^{\circ}18^{40}...19^{25};22^{20}-24;=,\infty 0^{00}-24$
30	7	2.7	.	$\bullet^{\circ}0^{00}-4^{35}\bullet^{\circ}-5^{10}\mathbf{v}^{\circ}11^{45}-12^{10};14^{35-50}\bullet^{\circ}21^{05...15};22^{05}-24;=na-a,np$
31	7	1.5	.	$\bullet^{\circ}0^{00}-2^{10}\bullet\bullet^{\circ\prime}2^{20}-4^{30}\bullet^{\circ}...8^{35}\mathbf{v}^{\circ}9^{20}-11^{10};\gg 9^{10}-16^{30};=0^{00}-9^{40}$
Σ	—	26.6	—	UWAGI:

Kwiecień - Avril

1	7	5.1	.	$\bullet^{\circ\prime}5^{30}-7^{50}*^{\circ}-8^{40}\bullet^{\circ}-10^{27}\mathbf{v}^{\circ\prime}12^{20}...14^{17}\mathbf{v}^{\circ}21^{05-10}\mathbf{v}^{\circ}-22^{40};\gg 13^{04}-14^{03}=5^{20}-11^{30}$ np
2	7	1.2	.	$\mathbf{v}\ 13^{08-16}\mathbf{v}^{\circ}13^{21}...17^{05};\gg 13^{05}...15^{05};=0^{00}-9^{15}$
3	7	.	.	$\bullet^{\circ}0^{45}-2^{05}\bullet^{\circ}2^{10}-3^{40}\bullet^{\circ}-6^{35}...7^{05};\gg 11^{30}-17^{20};=3^{30}-8^{30}$
4	7	2.0	.	$\bullet^{\circ}18^{20}-24$
5	7	0.9	.	$\bullet^{\circ}0^{00-15}5^{15}...7^{30}-8^{40}\mathbf{v}^{\circ\prime}15^{20}...16^{35};=4^{40}-11^{30}$
6	6	.	.	$=,\infty 1^{30}-24$
7	8	1.6	.	$\mathbf{v}^{\circ}9^{45}...10^{20}\mathbf{v}^{\circ}11^{20-28}\bullet^{\circ}20^{20}-24;\gg 1^{20}-2^{30};5^{30}-14^{05};=na,np$
8	6	0.5	.	$\bullet^{\circ}0^{00}-2^{30}...4^{40}\bullet\bullet^{\circ}5^{40}-6^{30}\bullet^{\circ}6^{40}...7^{40}\bullet^{\circ}...8^{35};21^{10}-23^{35};\gg a-p;=0^{00}-10^{40}\infty-13^{45}$
9	8	0.0	.	$\mathbf{v}^{\circ}20^{20-35};\gg 15^{42}-16^{10};\frown^{\circ}3^{00}-8^{00}$
10	7	.	.	$=2^{15}-4^{30}=-5^{45}=-9^{20};19^{40}-24;\frown'2^{00}-3^{00}\smile'na-a\frown^{\circ}np$
11	7	.	.	$=0^{00}-7^{45};\frown^{\circ}0^{00}-2^{00}\smile^{\circ}3^{00}-7^{00}$
12	7	1.2	.	$\bullet^{\circ}23^{40}...24;=3^{40}-7^{20}\infty 18^{40}-20^{30}=-24;\frown^{\circ}na\smile^{\circ}-6^{00}\frown^{\circ}np$
13	7	3.3	.	$\bullet^{\circ}0^{00}...1^{10}-2^{35};3^{35}-10^{40}...11^{10}\mathbf{v}^{\circ}15^{02-06};=0^{00}-11^{45}$
14	7	0.3	.	$\bullet^{\circ}6^{32}...13^{35}\ 20^{10-40}\bullet\bullet^{\circ}-21^{35};\gg 15^{40}-16^{05};=6^{15}-8^{45}\ 19^{40}-22^{15}$
15	7	0.0	.	$\bullet^{\circ}4^{45}-5^{30}\ 7^{10}-8^{15};\gg 20^{30}-22^{20};=4^{50}-5^{45};19^{30}-24$
16	6	3.2	.	$\bullet^{\circ}17^{05...20}\mathbf{v}^{\circ}18^{40}-20^{16};\boxed{\mathrm{R}}^{\circ}19^{05-20-30}SW-NE;\gg na,a\ 8^{10}-17^{40};=,\infty 0^{00}-24$
17	7	.	.	$\gg 12^{15-35};13^{40}-15^{30};=,\infty 0^{00}-10^{40};\mathbf{v}\ 2^{45}-3^{50}$
18	7	.	.	$\frown^{\circ}20^{00}-24;\mathbf{v}\ 23^{45}-24$
19	7	.	.	$\infty 19^{30}-24;\frown^{\circ}0^{00}-3^{00};20^{00}-24;\mathbf{v}\ 0^{00}-3^{00}$
20	6	.	.	$\infty;=0^{00}-24;\frown^{\circ\prime}0^{00}-8^{00}\mathbf{v}\ 1^{00}-3^{40}$
21	6	.	.	$=,\infty 0^{00}-21^{25};\frown'0^{00}-9^{40};\oplus 12^{40}-13^{30}$
22	6	.	.	$=,\infty 1^{30}-24;\frown^{\circ}0^{00}-9^{00};20^{00}-24$
23	6	.	.	$=0^{00}-8^{45}\infty-13^{15};\frown^{\circ\prime}0^{00}-8^{00}$
24	7	.	.	$=,\infty 0^{00}-13^{15};\frown^{\circ\prime}0^{00}-8^{00}$
25	6	1.6	.	$=,\infty 2^{15}-13^{40};16^{30}-24;\frown^{\circ}3^{00}-7^{00};23^{00}-24$
26	6	0.1	.	$=,\infty 0^{00}-24;\frown^{\circ}0^{00}-8^{00}$
27	7	0.1	.	$\mathbf{v}^{\circ}5^{15-35}10^{33-35};20^{27}-21^{05};=,\infty 0^{00}-24;\frown^{\circ}2^{00}-6^{00}$
28	8	2.7	.	$\bullet^{\circ}3^{20}...4^{05}\bullet^{\circ}8^{12-45}\mathbf{v}^{\circ}21^{50}-22^{40};\gg 7^{30}-8^{40}\ 9^{50}-14^{15};=na$
29	8	5.5	.	$\mathbf{v}\ 1^{35-45};7^{10}...22^{05}\blacktriangle'9^{20-30}\mathbf{v}^{\circ}20^{20-35};\gg 7^{05-35};11^{30}...16^{10}$
30	8	0.2	pł.	$\mathbf{v}^{\circ}10^{06-20}15^{40-50};23^{30}-24;\gg 12^{12-20};17^{15-35}$
31				$\mathbf{v}^{\circ}0^{00-20}\mathbf{v}^{\circ\prime}-4^{05}\mathbf{v}\ 9^{45}-10^{05};=0^{10}-8^{15}$
Σ	—	29.5	—	UWAGI:

Poznań-Ławica φ=52°25' λ=16°50' Maj-Mai 1962

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	102.4	99.0	97.2	99.5	1.0	7.2	3.2	3.6	7.6	-3.0	81	38	91	70	1.3	6.4	0.7	2.8	10 ✳	10	10 ●	NW 5	NW 7	W 6
2	95.5	95.8	98.4	95.9	0.5	6.2	3.6	3.5	7.5	0.5	98	54	88	80	0.1	4.3	0.9	1.8	10 ✳	7	9	NE 2	N 7	W 2
3	99.0	98.4	96.8	98.1	2.8	6.7	4.9	4.8	7.7	-0.7	93	71	94	86	0.6	2.8	0.6	1.3	10	9 ●	9	SW 4	NW 5	SW 4
4	94.6	95.8	98.0	96.1	4.8	8.9	5.3	6.1	10.8	4.2	92	55	78	75	0.7	5.1	1.9	2.6	10	8 ⊙	8	W 7	NW 7	W 3
5	100.5	102.7	105.3	102.8	4.1	9.2	5.7	6.2	10.6	1.5	92	56	82	77	0.7	5.1	1.7	2.5	9	7	2	C 0	NE 3	C 0
6	107.8	107.3	105.0	106.7	6.9	15.0	11.4	11.2	16.2	1.5	85	46	62	64	1.4	9.2	5.2	5.3	0	7 ⊙	10	SE 1	SE 4	SE 3
7	102.3	103.0	103.5	102.9	10.6	18.8	13.5	14.1	20.6	8.8	100	63	94	86	0.0	8.1	0.9	3.0	10 ●	8	6	SW 3	W 6	SW 2
8	102.2	101.9	100.5	101.5	13.2	19.8	14.4	15.4	21.1	11.0	98	51	93	81	0.4	11.4	1.1	4.3	6 ◎	9	9	W 3	WNW 6	SW 3
9	103.8	102.7	99.9	102.1	9.9	18.1	14.9	14.4	19.8	9.6	97	58	77	77	0.3	8.8	3.8	4.3	9	8 ⊙	10	W 5	C 0	E 3
10	96.7	98.7	100.3	98.6	12.4	17.2	10.0	12.4	18.6	10.0	98	48	86	77	0.4	10.2	1.8	4.1	10 ●	6 ⊙	1	S 1	W 12	SW 3
11	101.3	100.8	101.3	101.1	9.5	12.4	9.6	10.3	15.9	5.5	87	63	83	78	1.6	5.3	2.1	3.0	3 ⊙	9	3	SW 2	W 5	S 4
12	103.1	103.5	103.9	103.5	8.8	16.6	14.6	13.6	18.0	5.2	88	44	75	69	1.4	10.6	4.1	5.4	0 ⊙	8	10	C 0	WSW 3	NE 2
13	104.2	105.0	103.9	104.4	10.4	11.8	8.9	10.0	14.7	8.9	95	78	89	87	0.6	3.0	1.2	1.6	10 ●	8 ⊙	4	S 2	NW 4	NW 2
14	97.6	93.2	92.4	94.4	7.1	7.9	6.9	7.2	9.0	6.1	94	94	94	94	0.6	0.6	0.5	0.6	10 ●	10 ●	10 ●	N 7	NW 8	NW 12
15	93.5	95.4	98.1	95.7	8.2	10.4	9.2	9.2	12.0	6.4	93	78	85	85	0.8	2.7	1.7	1.7	10	10	8	NW 12	NW 11	WNW 9
16	101.0	103.6	104.0	102.9	8.4	9.4	7.6	8.2	12.2	6.8	82	66	77	75	2.0	4.0	2.3	2.8	10	10	8	NW 10	W 8	W 3
17	101.6	100.0	100.6	100.9	8.5	16.6	10.5	11.5	17.3	4.7	80	57	80	72	2.3	8.2	2.6	4.4	10	9	8	SW 4	SW 6	W 3
18	105.2	105.5	107.4	105.4	7.8	12.7	9.5	9.9	15.8	3.1	93	64	87	81	0.8	5.4	1.6	2.6	4 ◎	6	9	NW 5	W 6	SE 1
19	105.2	100.2	96.7	100.7	11.0	21.0	17.2	16.6	22.4	5.5	80	40	72	64	2.6	14.9	5.4	7.6	2 ◎	6 ⊙	9	SE 2	S 7	W 5
20	99.2	101.7	103.5	101.5	9.8	12.6	8.8	10.0	17.3	8.7	93	60	80	78	0.8	5.8	2.3	3.0	10	10	5	W 6	W 6	NW 3
21	106.4	104.6	103.6	104.9	8.8	15.0	11.0	11.4	16.7	4.8	88	49	74	70	1.4	8.7	3.4	4.5	7	8	2	NW 1	SW 1	SE 1
22	100.6	101.1	103.9	101.9	10.4	12.2	11.3	11.3	15.7	6.3	74	86	91	84	3.3	2.0	1.2	2.8	10	10 ●	10	S 5	SW 4	W 2
23	105.4	103.8	104.5	104.6	12.4	17.6	11.5	13.2	19.0	8.1	79	53	89	74	3.0	9.5	1.5	4.7	7 ⊙	9	10 ●	SW 6	SW 8	NW 5
24	107.8	107.1	105.3	106.7	10.2	13.9	10.6	11.3	14.7	8.3	76	55	74	68	3.0	7.2	3.4	4.5	8	9	8	NW 5	W 5	S 2
25	104.1	104.1	104.3	104.2	9.8	14.6	10.2	11.2	15.2	6.4	81	55	91	76	2.3	7.5	1.1	3.6	9	4 ◎	10	N 4	NW 3	NE 2
26	102.7	101.2	100.4	101.4	9.4	11.6	10.0	10.2	12.3	8.7	96	79	96	90	0.5	2.8	0.5	1.3	10 ●	10 ●	10	E 3	NE 7	N 2
27	103.5	105.6	106.8	105.3	9.4	13.0	11.0	11.1	14.0	9.0	95	73	86	85	0.6	4.1	1.8	2.2	10 ●	10	9	NW 1	W 3	NNW 1
28	106.7	104.8	102.6	104.7	11.1	17.7	10.0	12.2	19.0	4.8	86	54	96	79	1.8	9.3	0.5	3.9	1 ◎	6 ⊙	9	ENE 2	E 3	WSW 4
29	104.2	105.6	105.8	105.2	10.2	13.6	11.2	11.6	15.9	7.8	88	65	82	78	1.4	5.5	2.5	3.1	9	9	9	W 6	SW 6	W 2
30	106.9	106.6	107.2	106.9	10.8	14.4	9.2	10.9	17.3	7.7	86	58	89	78	1.8	6.8	1.2	3.3	3	9	0	W 4	W 5	W 2
31	104.9	100.1	100.7	101.9	9.0	17.6	10.7	12.0	18.9	5.9	88	51	75	71	1.4	9.8	3.2	4.8	9	8 ⊙	4	C 0	SW 8	W 3
M	102.1	101.9	102.0	102.0	8.6	13.5	9.9	10.5	15.3	5.9	89	60	84	78	1.3	6.6	2.0	3.3	7.6	8.3	7.4	3.8	5.6	3.2

Czerwiec-Juin

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	104.4	106.1	105.0	105.2	7.1	13.0	10.2	10.1	14.8	5.2	66	50	86	67	3.5	7.5	1.7	4.2	6 ⊙	7 ◎	9	W 8	W 5	C 0
2	106.5	108.4	111.4	108.8	7.9	13.0	7.4	8.9	14.5	6.9	83	58	70	64	1.7	9.3	3.1	4.7	9	8	3	NW 5	WNW 8	NW 5
3	114.0	114.4	115.6	114.7	7.8	12.1	6.2	8.1	13.7	2.3	73	50	88	70	2.8	7.1	1.2	3.7	1 ⊙	8 ⊙	2	NW 3	NW 4	NNW 4
4	116.1	116.4	115.6	116.0	7.8	8.9	10.0	9.2	13.3	5.2	73	69	72	71	2.8	3.5	3.5	3.3	4 ⊙	9 ●	8	N 6	N 7	N 5
5	116.1	115.1	117.3	116.2	9.2	16.1	8.4	10.5	16.6	6.0	67	41	51	53	3.8	10.7	5.4	6.6	8	7	1	N 9	N 9	N 8
6	118.5	118.4	119.3	118.7	7.0	15.0	9.3	10.2	16.2	2.4	64	27	44	45	3.6	12.4	6.5	7.5	3 ⊙	4 ⊙	3	N 9	N 10	N 6
7	119.5	119.2	118.7	119.1	8.6	16.2	11.5	12.0	18.3	4.1	66	26	51	48	3.8	13.6	6.7	8.0	8	5 ⊙	1	N 7	N 8	NW 3
8	119.2	118.0	113.8	117.0	11.8	18.4	14.8	15.0	21.7	3.7	58	34	60	51	5.8	14.0	6.7	8.8	0 ⊙	1 ⊙	2	NE 1	NW 3	W 3
9	109.5	106.4	104.7	106.9	15.0	21.8	13.1	15.8	22.9	5.8	60	40	72	57	6.7	15.6	4.3	8.9	1 ⊙	4 ⊙	0	W 5	NW 7	N 2
10	103.8	102.0	99.8	101.9	13.4	21.3	16.9	17.1	22.6	5.5	69	37	71	59	4.8	16.0	5.5	8.8	1 ⊙	4 ⊙	9	SE 1	SW 2	NW 2
11	98.5	97.7	99.4	98.5	13.8	16.4	12.4	13.8	18.2	11.7	82	53	69	68	2.9	8.8	4.5	5.4	9	7	9	NW 1	W 8	WNW 5
12	102.0	103.7	105.1	103.6	10.8	12.0	12.4	11.9	15.4	9.0	64	66	72	67	4.6	4.8	4.0	4.5	8	10	8	NW 8	WNW 7	NW 2
13	107.0	106.9	105.6	106.5	13.0	19.7	14.1	15.2	20.7	5.1	65	37	62	55	5.3	14.3	6.1	8.6	0 ⊙	7 ⊙	7	NW 2	C 0	S 2
14	103.7	102.9	103.6	103.4	14.9	24.8	20.0	19.9	26.3	11.3	59	36	68	54	6.9	20.1	7.6	11.5	6 ⊙	2 ⊙	4	S 5	SW 7	C 0
15	108.3	108.8	108.2	108.4	18.5	27.7	22.2	22.6	29.9	11.3	63	36	63	54	7.8	23.8	9.9	13.8	6 ⊙	2 ⊙	4	N 1	SSW 2	SE 2
16	108.0	106.5	107.0	107.2	20.8	31.1	18.4	22.2	32.7	17.7	70	34	95	66	7.4	30.0	1.1	12.8	8	4 ⊙	10 ●	S 2	S 5	NW 2
17	111.4	111.8	111.2	111.5	16.9	20.1	15.5	17.0	22.3	14.4	79	62	75	72	4.0	9.0	4.4	5.8	1 ⊙	8	1	NW 7	NNW 7	NW 3
18	111.4	109.6	107.4	109.5	15.4	22.2	18.6	18.7	24.6	10.3	56	46	72	58	7.7	14.5	6.1	9.4	0 ⊙	2 ⊙	2	E 2	NW 3	E 1
19	105.2	103.0	99.5	102.6	18.2	26.0	22.1	22.1	27.3	15.0	69	49	76	65	6.4	17.2	6.4	10.0	4 ⊙	8 ⊙	9 (K)	SE 3	SSE 7	C 0
20	106.2	106.6	107.3	106.7	14.7	22.4	17.7	18.1	24.2	13.8	85	39	61	62	2.5	16.5	7.9	9.0	4 ⊙	6 ⊙	9	WNW 6	W 7	WSW 2
21	108.8	108.9	110.3	109.3	17.6	21.8	16.6	18.2	22.9	11.6	69	53	85	69	6.2	12.3	2.9	7.1	8	10	2	SW 3	W 9	SW 2
22	112.4	112.0	110.2	111.5	17.6	24.8	20.9	21.0	27.1	11.8	80	46	72	66	4.0	16.9	7.0	9.3	0 ⊙	7 ⊙	3	SW 2	W 5	S 2
23	109.2	109.3	108.8	109.1	19.9	25.8	19.7	21.3	27.1	15.9	76	51	75	67	5.5	16.2	5.7	9.1	4 ⊙	3 ⊙	10 ●	SW 2	N 6	N 3
24	108.4	105.8	103.3	105.8	17.9	24.3	21.4	21.2	27.5	13.9	83	47	59	63	3.4	16.0	10.4	9.9	3 ⊙	7 ⊙	2	SW 1	SW 7	W 4
25	106.0	108.0	108.9	107.6	16.4	18.2	13.3	15.4	21.4	13.3	52	39	58	50	8.9	12.8	6.3	9.4	1 ⊙	9 ⊙	3	W 9	WNW 12	W 6
26	108.0	104.6	100.9	104.3	12.2	18.6	14.2	14.8	20.3	5.8	64	39	78	60	5.1	13.0	3.6	7.2	3 ⊙	7 ⊙	10 ●	W 5	SW 9	N 4
27	100.0	100.9	101.9	100.9	10.8	13.4	12.4	12.2	16.2	9.7	86	64	67	72	1.8	5.5	4.8	4.0	9	9	9	W 6	SW 8	W 4
28	101.3	99.2	96.4	99.0	9.7	11.0	8.3	9.4	12.6	7.9	74	74	93	80	3.1	3.4	0.8	2.4	9	10 ●	8	W 9	WSW 8	W 6
29	97.9	100.0	101.6	99.8	9.9	14.4	12.4	12.3	15.3	7.2	87	64	77	76	1.6	6.0	3.4	3.7	10	9	9	W 8	W 12	W 9
30	102.2	104.2	105.6	104.0	9.5	12.6	12.4	11.7	14.7	8.9	91	84	83	86	1.1	2.4	2.4	2.0	10	10	9	W 9	W 9	W 5
31																								
M	108.1	107.8	107.4	107.8	13.1	18.8	14.4	15.2	20.7	9.1	71	48	71	63	4.5	12.4	5.0	7.3	4.8	6.5	5.5	4.8	6.7	3.4

Poznań - Ławica $H_s = 86m$ $H_t = 92{,}1m$ $h_w = 13m$ Maj - Mai 1962

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	5.8	•	♀°'-5^20-6^30 ✱°; ✱°-7^50 ♀°a, 15^33...20^45 •°-24; ≫12^32...13^35; = 6^15-9^15; 20^30-24, ⌓°na
2	7	1.8	pz•	•°0^00-6^10 ✱°'-6^40 ✱°'-8^25 •°-8^50 ♀°23^10-24, = 0^00-9^30
3	7	6.5	•	♀°0^00-1^15 7^03-32 •°7^40-9^45 10^10 ♀°11^26...15^15 •°-20^35 ♀°np; = na-a, p-24
4	7	0.0	•	♀°'-1^10...5^30 •°5^40-6^15 ♀°13^50-55; = 0^00-6^30
5	7	0.3	•	♀°9^20-11^05 13^45-15^08; = na-a; 19^40-24, ⌓'1^00-9^00 21^00-24
6	7	7.3	•	•°23^40...24; = 0^00-7^30 ∞19^30-23^40; ⌓'-2 0^00-9^00
7	7	1.3	•	•°0^00-7^50 ♀'16^25...50; =, ∞0^00-10^15 = 19^30-24
8	7	0.7	•	•°17^45-19^10 ♀°22^45-23^05; = 0^00-4^30 = -6^10 = -a, p-24; ⌓'-°na-a; ⊕ 15^45-16^10
9	6	3.7	•	=, ∞0^00-13^20, 15^35-24
10	7	0.1	•	♀°0^30...4^30 •°-8^15; ≫12^20-14^10; = 0^00-9^10; ⌓'np
11	7	0.0	•	♀°10^12-40, 13^02-07; = 3^15-8^30, 23^30-24; ⌓'na-a, hp
12	7	2.8	•	•°21^45-22^15 •°'-22^30-24; = 0^00-7^40 np; ⌓'na-a; ⊕ 11^45-13^15
13	7	0.1	•	•°0^00-1^40, 2^15...7^35 ♀°11^35-12^02; = 0^00-8^30, 23^15-24
14	6	16.7	•	•°6^45...8^20-24; ≫13^25-24; = 0^00-24; ⌓'2^00-6^45
15	7	0.0	•	•°0^00...22^40; ≫0^00-9^10, np; = 0^00-4^30, 17^45-24
16	7	0.0	•	♀°10^40-45, 12^20-25; ≫0^00...12^20; = 0^00-3^40
17	7	3.4	•	•°3^40...5^20; 7^30-40 ♀°14^25-55 ♀°15^40-16^05 ♀°20^15-25; ⚢°14^35-50 W-E; = na-11^30, np; ⌓'na
18	7	2.0	•	♀°'-8^05 14^05 ♀°19^45-20^20; ⚢°13^45-14^05 SW-SE; =, = 0^00-7^20 = np
19	7	0.9	•	= 0^00-7^40 ∞-9^30
20	7	0.0	•	♀°3^35-4^30 •°6^15, 10^05-15; ≫13^30-40, 2^35-3^30; = na-a, p-24; ⌓°na
21	7	•	•	= 0^00-3^40 = -5^10 = -8^25, 21^40-24, ⌓°1^00-9^00
22	6	0.3	•	•°11^50...13^09 ♀°16^03-10, 20^15-35; = na, a-p, np; ⌓°0^00-9^00
23	7	4.0	•	♀°16^07...17^05, 21^27-24; = 0^00-7^30, 19^40-24
24	7	0.0	•	♀°0^00-15; = 0^00-5^30 ∞19^30-21^15 = -24; ⊕ a-p, p
25	7	1.7	•	♀°6^08-40, 15^30...19^15; = 0^00-2^45 = -5^10 = -7^45, 20^30-24; ⌓°na
26	7	4.0	•	♀°na •°...10^30 ♀°12^17-13^10 •°'-17^35 •°...24; = 0^00-11^40, 13^15-24
27	7	0.2	•	•°0^00...40 •°6^45-8^20; = 0^00-8^40, 22^30-24
28	7	18.8	•	♀°-2 17^20-20^20 ▲'19^35-42 ⚢'19^15-19^25-20^12 SW-NE; =, ∞0^00-10^15, p-24; ⌓'2^00-9^00
29	7	0.0	•	♀°14^42-50; = 0^00-10^40 ∞18^30-20^30 = -24; ⌓°np; ⊕ p
30	6	0.4	•	♀°13^03...14^50, 17^40-50; = 0^00-10^00 ∞a, p-np = np; ⌓°na-a, np
31	6	0.5	•	♀°4^35-40 •°...7^10 ♀°'-15^12-35 ♀°16^40-17^02; =, ∞0^00-18^30; ⌓°na
Σ	—	83.3	—	UWAGI

Czerwiec - Juin

1	8	0.8	•	♀°16^13-17^05, 19^05-20; ≫4^13-30
2	8	0.0	•	•°4^55-7^35 ♀°12^33-40, 15^45-16^05
3	8	0.0	•	♀°16^10-17; ⌓°4^00-9^00
4	8	0.0	•	♀°13^50-14^20
5	8	•	•	⊕ 9^20-12^15
6	8	•	•	≫8^20-20^30
7	8	•	•	
8	8	•	•	
9	8	•	•	⌓°2^00-7^00
10	8	4.0	•	= 2^30-4^10 ≡'-°-5^40 = -7^40; ⌓'0^00-8^00
11	7	0.0	•	♀'3^03-56 ♀°4^25...5^07, 10^53...12^35; (⚢)2^35-⚢'3^03-26-(⚢)-3^50 NE ≫14^30-17^20; = na
12	8	0.0	•	♀°11^43-12^05, 12^30-40
13	8	•	•	= 3^30-6^15; ⌓'2^00-7^00
14	7	•	•	∞4^20-8^40, 20^30-22^45 = -24; ⊕ 11^15-13^15
15	6	•	•	= 0^00-7^30 ∞-24; ⌓°4^00-8^00
16	6	7.4	•	♀°'-18^15-22^35; (⚢)N 17^40-⚢'18^10-20^30-(⚢)21^10 E; ≫17^15-18^35; ∞ = 0^00-15^10 = 19^15-24
17	8	•	•	= 0^00-6^20, 22^30-24
18	8	•	•	= 0^00-5^10 ∞21^15-22^40 = -24
19	6	2.0	•	♀°21^20...24; (⚢)W 20^40-⚢°21^10-25-(⚢)22^15 E; ≫22^35-23^05; = ∞0^00-24
20	7	•	•	♀°0^00-30, 2^35-3^10; ≫2^30-40; = 0^00-7^30
21	7	0.0	•	♀°14^32-15^15; = 21^40-24
22	6	•	•	= 0^00-3^30 = -5^40 = -8^30 ∞-23^40 = -24; ⌓'3^00-10^00
23	6	2.0	•	♀°21^45-22^45; ⚢°22^15-45 W-E; = ∞0^00-24; ⌓°3^00-7^00
24	6	•	•	= 0^00-9^30 ∞-23^45
25	7	•	•	≫8^10-20, ⌓22^45-24
26	7	7.9	•	♀°20^15-25 •°21^20-24; = np, ⌓°na-a; ⌓0^00-3^00
27	7	0.4	•	•°0^00-4^15 ♀°14^02-15^05, 17^35-45; ≫14^20-35; = 0^00-8^30; ∩17^40-50
28	7	5.4	•	♀°10^03-15^10 •°15^20-17^35 ♀°'-17^40-20^15 ♀°22^45-24
29	7	4.2	•	♀°0^00-40, 9^38-43, 11^04-36, 14^45-15^15, 16^15-17^55; ≫10^30-16^30, 21^20-50
30	7	0.1	•	♀°4^05...8^40 •°9^15...10^35 ♀°14^40-50; = 9^20-13^20, 20^30-24
31				
Σ	—	34.2	—	UWAGI

Poznań - Ławica φ = 52°25' λ = 16°50' Lipiec - Juillet 1962

DNI	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N.w			KIERUNEK i PRĘDKOŚĆ WIATRU D.v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	106.1	106.5	105.2	105.9	11.2	12.3	10.9	11.3	14.3	10.1	83	71	86	80	2.3	4.2	1.8	2.8	7	10	9	W 3	W 6	SW 3
2	103.6	102.9	98.7	101.7	12.0	12.6	11.8	12.0	16.3	9.9	76	71	94	80	3.3	4.2	0.8	2.8	7 ⊙	10	10 ●	NW 2	W 6	SW 5
3	92.8	90.6	89.2	90.9	10.4	12.9	9.6	10.6	15.7	8.8	88	74	86	83	1.4	3.9	1.8	2.4	9	6	9 ●	W 8	W 8	SW 2
4	86.8	87.4	90.1	88.1	8.8	9.5	9.9	9.5	10.9	7.3	85	91	93	90	1.7	1.1	0.8	1.2	10 ●	10 ●	9	SW 8	SW 10	SW 5
5	93.4	95.3	98.4	95.7	11.7	14.8	12.4	12.8	16.7	8.7	82	70	77	76	2.5	5.0	3.4	3.6	9 ⊙	8	7	SW 5	SW 7	SW 3
6	101.7	102.6	103.9	102.7	10.8	16.7	12.8	13.3	18.0	7.3	90	62	81	78	1.4	7.2	2.8	3.8	9	8	8	SW 3	W 5	SW 2
7	104.7	104.9	105.9	105.2	11.8	14.9	11.9	12.6	15.6	9.4	82	65	81	76	2.5	5.9	2.6	3.7	9	10 ●	4	SW 6	WSW 7	W 4
8	107.3	109.0	110.2	108.8	11.7	15.5	12.9	13.2	16.5	9.2	93	65	93	84	1.0	6.2	1.1	2.8	10 ●	9	7	W 4	NW 7	NW 3
9	111.7	110.3	108.1	110.0	10.4	17.7	15.6	14.8	20.3	6.4	95	57	77	76	0.6	8.6	4.1	4.4	10	6	4	W 3	N 3	C 0
10	107.2	105.9	103.8	105.6	14.6	20.5	16.5	17.0	23.1	9.3	82	40	73	65	2.9	14.5	5.2	7.5	0	4 ⊙	1	C 0	NW 5	N 3
11	102.4	100.0	97.8	100.1	15.9	23.9	18.3	19.1	24.5	7.8	72	34	67	58	5.1	19.6	7.0	10.6	6	9	10 (R)	SW 2	SW 5	N 4
12	98.4	97.1	96.6	97.4	15.1	21.1	16.2	17.2	22.5	11.8	88	54	89	77	2.1	11.5	1.9	5.2	9	9 ●	9	W 6	W 5	SW 6
13	95.7	96.1	97.9	96.6	13.6	16.2	13.3	14.1	17.5	12.5	89	75	92	85	1.8	4.5	1.3	2.5	10 ●	9	9	SW 5	W 8	W 5
14	97.3	97.1	97.5	97.3	12.8	15.2	14.0	14.0	17.4	10.8	95	83	90	89	0.7	3.0	1.6	1.8	10 ●	10	9	SW 3	W 5	WNW 3
15	96.4	95.3	95.6	95.8	12.8	18.7	16.1	15.9	21.2	9.6	96	62	77	78	0.5	8.2	4.2	4.3	6	9	4	C 0	N 3	E 2
16	97.3	97.8	100.2	98.4	15.2	20.7	16.1	17.0	21.9	13.3	83	55	88	76	3.0	10.9	2.1	5.3	4	8 ⊙	7	NE 3	NE 4	N 2
17	103.2	103.8	105.3	104.1	15.4	21.4	17.3	17.8	22.9	10.9	78	48	70	65	3.9	13.2	5.8	7.6	2 ⊙	8 ⊙	4	E 4	NNE 5	E 1
18	106.8	105.9	106.1	106.3	14.0	21.4	16.6	17.2	22.6	10.2	80	37	76	64	3.2	15.9	4.6	7.9	8 ⊙	7	4	E 2	NE 8	N 1
19	107.5	107.2	107.2	107.3	14.9	23.0	17.2	18.1	24.7	8.8	75	37	67	60	4.1	17.6	6.5	9.4	5	3 ⊙	2	N 2	N 3	C 0
20	107.1	106.1	106.3	106.5	18.0	23.9	19.8	20.4	25.7	11.7	70	43	72	62	6.1	16.7	6.5	9.8	8 ⊙	9 ⊙	0	SE 1	WSW 6	C 0
21	106.0	102.4	101.1	103.2	18.6	28.6	22.8	23.2	30.4	12.6	82	37	67	62	3.9	24.5	9.2	12.5	1 ⊙	5 ⊙	4	E 2	S 7	S 4
22	105.3	104.9	106.6	105.6	19.0	26.3	19.8	21.2	27.9	18.2	94	45	72	70	1.3	18.7	6.5	8.8	8	7 ⊙	6	S 1	SSW 7	WSW 2
23	109.4	110.0	110.8	110.1	17.6	22.9	16.9	18.6	24.4	13.7	69	36	61	55	6.2	17.9	7.5	10.5	6 ⊙	7 ⊙	4	WNW 5	WNW 8	NW 8
24	114.0	113.6	113.9	113.8	13.4	19.0	13.5	14.8	20.5	11.1	80	44	66	63	3.2	12.3	5.3	6.9	9 ⊙	7	0	NW 6	WNW 10	NW 3
25	114.3	112.1	109.3	112.0	14.2	23.4	19.7	19.2	24.9	6.1	78	37	58	58	3.6	18.2	9.6	10.5	3	3 ⊙	8	C 0	S 2	E 1
26	106.4	104.2	102.6	104.4	17.7	31.7	21.9	23.3	33.0	14.6	72	33	78	61	5.7	31.3	5.8	14.3	4 ⊙	9 ⊙	3	SE 2	SW 6	SW 4
27	104.6	103.6	106.4	104.9	19.5	26.8	15.0	19.1	27.0	14.9	82	40	70	64	4.1	21.1	5.0	10.1	8 ⊙	7	3	W 5	W 8	NW 9
28	109.1	109.0	109.9	109.3	12.9	19.3	12.3	14.2	20.0	9.5	87	53	80	73	1.9	10.4	2.9	5.1	10	7 ⊙	0	WNW 6	WNW 7	NW 2
29	111.2	109.8	110.2	110.4	12.9	19.4	14.4	15.3	22.3	4.7	77	35	70	61	3.5	14.7	5.0	7.7	1 ⊙	6 ⊙	8	C 0	NW 4	C 0
30	111.3	110.3	109.4	110.3	15.2	20.4	15.8	16.3	22.3	8.2	79	42	61	61	3.2	14.0	6.9	8.0	8 ⊙	7	4	E 2	E 1	NE 1
31	110.1	109.1	107.8	109.0	15.6	24.1	16.5	18.2	25.5	10.7	69	33	82	61	5.5	20.0	3.5	9.7	1 ⊙	8	7	S 2	SW 4	S 1
M	104.2	103.6	103.6	103.8	14.1	19.8	15.4	16.2	21.5	10.3	82	53	77	71	3.0	12.4	4.3	6.6	6.7	7.6	5.6	3.3	5.8	2.9

Sierpień - Août

1	107.3	107.5	107.1	107.3	15.8	19.9	16.3	17.1	22.5	14.5	86	56	72	71	2.4	10.2	5.3	6.0	8	9	3	W 3	NW 7	NW 2
2	106.7	105.4	104.5	105.5	14.0	21.6	17.0	17.4	24.2	8.5	82	39	65	62	2.9	15.7	6.9	8.5	6 ⊙	5 ⊙	3	W 2	W 4	NE 1
3	105.8	105.9	104.3	104.0	17.0	25.3	19.4	20.3	26.4	12.9	74	38	68	60	5.1	20.0	7.2	10.8	4 ⊙	8 ⊙	9	C 0	N 2	NE 3
4	103.1	102.3	104.8	103.4	17.6	27.3	21.8	22.1	28.8	14.7	82	48	63	64	3.6	18.7	9.5	10.6	7	9 ⊙	10	S 2	SW 8	NW 3
5	103.8	99.6	98.8	100.7	17.9	27.2	18.4	20.5	28.8	15.5	85	46	84	72	3.0	19.3	3.3	8.5	9	9	9	C 0	S 6	NW 3
6	101.3	101.4	100.5	101.1	15.4	21.1	18.4	18.3	23.1	14.7	83	48	82	71	3.0	13.0	3.9	6.6	9	9	6	W 4	S 4	SW 1
7	95.0	90.5	96.5	94.0	19.6	23.3	15.3	18.4	23.5	14.9	80	79	76	78	4.5	6.0	4.3	4.9	9	10 ●	3	SE 2	C 0	W 7
8	101.6	104.5	107.2	104.4	15.2	19.0	13.4	15.2	24.4	11.8	70	42	73	62	5.1	12.7	4.2	7.3	0 ⊙	7 ⊙	2	SW 10	W 10	SW 3
9	112.8	113.4	113.2	113.1	11.6	17.9	12.6	13.7	21.0	7.9	85	47	74	69	1.9	10.8	3.7	5.5	0 ⊙	7 ⊙	0	SW 3	W 3	C 0
10	111.2	107.6	104.5	107.8	12.0	22.9	18.4	17.9	24.3	8.0	81	33	57	57	2.7	18.6	9.1	10.1	8	10	10	S 2	SSW 7	SW 2
11	105.6	105.0	105.5	105.4	14.7	23.2	17.2	18.1	24.9	12.8	81	42	74	66	3.1	16.3	5.1	8.2	9	6 ⊙	0	SW 5	SW 8	SW 2
12	106.4	105.8	105.2	105.8	17.6	28.5	20.8	21.9	29.8	12.4	76	35	73	63	4.7	25.1	5.6	11.8	0 ⊙	0 ⊙	1	SW 3	SW 2	C 0
13	107.2	107.6	108.2	107.7	18.7	27.0	19.6	21.2	27.9	15.0	77	47	71	65	5.0	18.9	6.7	10.2	2 ⊙	1 ⊙	8 (R)	NE 5	N 1	NE 8
14	109.8	109.8	107.5	109.0	13.2	16.0	15.8	15.2	19.8	12.4	82	74	73	76	2.8	4.7	4.8	4.1	10	10	9	NE 5	E 2	NE 2
15	102.8	98.9	97.7	99.8	13.8	20.3	18.1	17.6	24.5	10.9	85	81	88	85	2.3	4.6	2.5	3.1	10	7 ⊙	10	E 5	E 4	SW 3
16	99.1	100.4	101.7	100.4	16.7	24.2	17.4	18.9	25.3	14.2	91	52	79	74	1.8	14.5	4.2	6.8	3 ⊙	6 ⊙	4	SW 3	SW 7	SW 3
17	103.2	102.4	100.3	102.0	15.3	24.0	17.1	18.4	24.4	14.3	92	38	93	74	1.3	18.4	1.4	7.0	9 ●	9 ⊙	3	W 1	SW 2	SSE 3
18	98.3	101.8	103.6	101.2	15.2	14.2	13.5	14.1	18.1	13.3	99	90	77	89	0.2	1.6	3.5	1.8	10	10	6	SW 4	SW 7	W 6
19	103.3	104.6	105.4	104.4	12.0	12.4	14.4	13.3	14.9	11.6	94	93	89	92	0.8	1.0	1.8	1.2	10	10 ●	10	W 6	W 7	W 7
20	106.1	107.4	106.8	106.8	14.0	16.2	15.0	15.0	16.7	12.8	90	69	93	84	1.6	5.6	1.1	2.8	10	10	9	NW 7	NW 8	NW 3
21	105.0	103.5	102.3	103.6	14.8	20.6	16.2	17.0	22.1	13.4	92	60	83	78	1.3	9.7	3.1	4.7	9	9	2	C 0	SSE 3	SE 1
22	104.6	105.9	104.1	104.9	14.4	18.7	15.6	16.1	20.4	14.1	97	57	83	79	0.6	9.4	3.0	4.3	9	9	10	W 5	W 6	S 1
23	104.7	106.3	106.1	105.7	12.2	16.8	13.8	14.2	18.5	11.1	89	63	80	77	1.5	7.1	3.2	3.9	4 ⊙	9	10	WSW 6	W 8	SW 3
24	99.7	97.0	97.3	98.0	12.5	16.6	14.0	14.3	18.3	10.6	92	90	92	91	1.2	2.0	1.3	1.5	10 ●	10 ●	10 ●	S 5	SW 9	W 6
25	101.3	102.0	104.8	102.7	12.7	17.0	14.6	14.7	18.5	11.1	92	69	74	78	1.2	6.0	4.3	3.8	9	10	10	SW 5	SW 8	WSW 6
26	108.2	109.8	108.3	108.8	12.4	17.8	12.2	13.6	19.3	10.5	79	49	83	70	3.0	10.5	2.4	5.3	4	7	0	W 8	W 8	S 1
27	102.4	99.0	102.9	101.4	12.2	23.6	16.4	17.2	23.7	8.5	81	46	54	60	2.6	15.6	8.6	8.9	4 ⊙	9	4	S 2	SW 10	W 9
28	106.9	107.4	108.4	107.6	12.2	18.0	11.6	13.4	18.4	10.6	76	51	84	70	3.4	10.0	2.1	5.2	8	9	0	W 9	W 8	WSW 4
29	106.5	105.0	107.4	106.3	12.6	18.5	12.2	13.9	19.7	9.9	84	59	81	75	2.4	8.7	2.6	4.6	9	10	0	SW 3	W 8	W 5
30	110.0	111.2	109.2	110.1	11.3	16.7	10.8	12.4	17.4	10.0	84	47	84	72	2.2	10.1	2.2	4.8	9	9	2	W 8	W 9	SW 3
31	103.2	103.6	105.7	104.2	12.5	13.2	11.6	12.7	16.6	10.0	79	53	79	71	3.1	7.9	2.8	4.6	9	9	7	W 6	W 10	W 5
M	104.3	104.2	104.5	104.4	14.4	20.4	15.8	16.6	22.1	12.0	85	56	78	73	2.6	11.4	4.2	6.1	7.0	8.1	3.5	4.2	6.0	3.4

Poznań - Ławica $H_s = 86m$ $H_t = 92{,}1m$ $h_w = 13m$ Lipiec - Juillet 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	0.6	•	•10^{40}-11^{35} ▽°13^{15-30}; 20^{45}-21^{10}; = na, np
2	7	4.9	•	•$^{1-0}3^{05...35}$ •°$17^{50...18^{20}}$; 20^{50}-24; = 0^{00}-9^{30} 20^{30}-24; ⌓$^{1-0}$na
3	8	5.1	•	•na, a ▽$^{1}9^{05-07}$ ▲°-9^{09} ▽$^{0-1}$...14^{40} ▽° 21^{10}-22^{15}; = 0^{00}-7^{20}
4	6	2.4	↓	▽°4^{05}-5^{10} •$^{0-1}5^{20}$...16^{10} ▽° 8^{20}-9^{05}; 16^{20}-19^{10}; ≫10^{15}-14^{20}; = na-a, p, np
5	7	0.0	•	▽°19^{40-45}; = 0^{00}-9^{15}
6	7	1.4	•	▽$^{0-1}12^{01}$...17^{25} ▽° 22^{30-47}; = na-a ∞ a = np; ⌓$^{0-1}$na-a
7	7	0.7	•	•$^{3^{50}}$...4^{20}; 6^{35}...7^{45} ▽° 8^{20}-9^{45}; 11^{40}-15^{35}; = 0^{00}-13^{30}; np; ⌓°np
8	7	2.7	•	▽° 1^{10}-4^{10}; 5^{50}-6^{15} •° 7^{45}...8^{40} ▽° 9^{05-15}; p...; = 0^{00}-10^{00}; np; ⌓°na
9	7	•	•	= na ≡ 4^{50}-7^{10} = -10^{30}; np; ⌓° 23^{00}-24
10	8	•	•	= 0^{00}-7^{45}; ⌓$^{0-1}$ 0^{00}-10^{00}
11	7	0.0	•	▽° 12^{35}-13^{05}; (R) 21^{15}-22^{25} W-SE; = 3^{30}-7^{40} ∞ -9^{30} a -np = np; ⌓$^{0-2}$na-a, np
12	7	1.0	•	▽° 12^{48}-13^{02} ▽$^{0-1}$ 13^{52}-14^{35} ▽° 15^{20-30}; R $14^{04-10-35}$ NW-NE; = na-a, np; ⌓$^{\pm}$na-a
13	7	3.7	•	▽$^{0-1}$ 2^{20}...4^{20} •° 7^{45}...9^{10} ▽$^{0-1}$...24; R' 14^{40}-15^{10} SW-E; = 0^{00}-13^{45}; 21^{30}-24
14	7	0.4	•	▽° 0^{00-05} •° 6^{40}...12^{10} ▽° 15^{05-15}; = 0^{00}-12^{30}; 20^{35}-24; ⌓°p-np
15	7	•	•	= na = na = $^{0-1}4^{45}$-7^{30} = -8^{40}; 21^{15}-24; ⌓$^{1-0}$ 0^{00}-10^{00}
16	7	0.1	•	▽° 18^{10-45}; = 0^{00}-7^{30}; 21^{40}-24
17	7	•	•	= 0^{00}-9^{20} ∞ -15^{15}; 21^{30}-23^{40} = -24; ⌓°na-a, np
18	8	•	•	= 0^{00}-8^{30}; 21^{30}-24; ⌓° 0^{00}-10^{00}; ⊕ 9^{50}-13^{15}; 16^{40}-19^{20}
19	8	•	•	= 0^{00}-7^{10}; ⌓° 4^{00}-8^{00}
20	7	•	•	= 0^{40}-7^{15} ∞ -22^{30} = -24; ⌓° 2^{00}-7^{00}
21	7	1.7	•	= na ≡ $^{0-1}4^{25}$-6^{45} = -8^{30} ∞ -12^{40}; 21^{15}-24; ⌓°na
22	7	•	•	▽° 0^{35}...6^{50}; (R)° SW 0^{20}-R° 0^{35}-(R) 1^{15} E; ∞ 0^{00-30} = -7^{40}; ⌒ 5^{40}-6^{05}
23	7	•	•	= 2^{15}-7^{30}
24	8	•	•	≫13^{30}-15^{20}; = 4^{35}-8^{15}; ⌓° 4^{00}-8^{00}
25	7	•	•	= 2^{30}-4^{10} = -5^{45} = -8^{30} ∞ 21^{30}-24; ⌓°na-a
26	6	0.1	•	▽° 20^{23}-21^{15}; 22^{40}-23^{05}; (R)° 19^{55}-20^{50} NW-E (R)° S 23^{10}-R° 23^{40}-23^{55}-(R)° 24; = na-a ∞ -p = -24
27	7	•	•	= 0^{00}-8^{30} ∞ -12^{15}; ⌓° 3^{00}-9^{00}
28	7	0.0	•	▽° 14^{35}...16^{20}; 19^{16-20}; ≫ 14^{50-57}; =, = na = -7^{45}
29	8	•	•	= 2^{20}-5^{10} = -6^{10}; ⌓° 0^{00}-10^{00}
30	8	•	•	= 4^{35}-8^{30} ∞ -9^{10}; 21^{30}-24; ⌓° 2^{00}-8^{00}
31	7	0.5	•	▽° 16^{27}...20^{45} •° 23^{45}-24; ∞ 0^{00}-1^{15} = -7^{05}; 21^{15}-24
Σ	—	25.3	—	UWAGI:

Sierpień - Août

1	6	•	•	•° 0^{00-40}; 2^{40}...3^{10}; 6^{45}-7^{05}; = 0^{00}-10^{30} ∞ -15^{30}
2	8	•	•	= 2^{40}-8^{45} ∞ 21^{30}-23^{30} = -24; ⌓° 2^{00}-9^{00}
3	7	•	•	= 0^{00}-7^{40} ∞ -10^{30}; 20^{40}-22^{30} = -24
4	6	•	•	≫15^{35}-18^{40}; = 0^{00}-9^{50} ∞ -24
5	6	3.0	•	▽° 18^{20-30} ▽$^{1-0}$ 22^{15}-23^{40}; (R) SW 22^{10}-R° 22^{22}-(R) 23^{15} NE; ≫14^{40}-15^{35}; ∞; = 0^{00}-18^{15}; p-24 ⊕ a, p
6	7	•	•	▽° 3^{45}-4^{05}; = 0^{00}-7^{15}; 21^{30}-24
7	6	8.3	•	•° 9^{40}...14^{25} ▽° 15^{35}-18^{15}; 19^{10}-21^{20}; ≫14^{35}-15^{50}; 20^{50}-21^{35}; = 0^{00}-21^{10} ⌓° 2^{00}-8^{00}
8	7	•	•	≫7^{05}-15^{10}; = 0^{20}-5^{40} 22^{30}-24
9	7	•	•	= 0^{00}-2^{30}; ⌓° 23^{00}-24
10	7	•	•	= 0^{15}-9^{25} ∞ -24; ⌓° 0^{00}-9^{00}
11	7	•	•	∞ = 0^{00}-13^{20}; 20^{30}-24
12	7	•	•	= 0^{00}-8^{30} ∞ -10^{15} = 23^{30}-24
13	7	7.4	•	▽° 22^{05}-23^{10}; (R)° W SW 21^{40}-R° 21^{45}-24; = 0^{00}-8^{35} ∞ -22^{20}; ⌓° 2^{00}-7^{00}
14	7	•	•	▽$^{0-2}$ 0^{10}-1^{15}; 3^{40}-5^{05}; 6^{14-35}; R° 0^{00-20}-(R)° 1^{10} E; (R)° W 3^{20}-R° 3^{35}-5^{10}-(R)° 5^{15} E; = na
15	6	4.0	•	▽° 10^{15}-11^{20} •° 12^{10}-13^{20} ▽$^{0-2}$ 17^{50}-20^{10}; (R)° SW 18^{45}-R° 19^{05-50}-(R)° 20^{35} SE; = 5^{30}-14^{40}; 17^{45}-24; ⌓°na-a
16	7	0.0	•	= na, a ∞ a = 21^{30}-24
17	6	6.4	•	•° 7^{30}...8^{02}; 17^{20}-18^{20}; $19^{02...30}$; = 0^{00}-10^{10} ∞ 12^{20}-14^{30} = 19^{10}-24; ⌓°na
18	7	5.3	•	▽$^{1-0}$ 6^{05}...16^{10}; = 0^{00}-8^{45} 20^{40}-24; ⊕ 0^{15-40}
19	6	0.6	•	▽$^{0-1}$; •° 6^{32}...12^{40}; •° 13^{15}-14^{30}...16^{15}; = na-a, p, np
20	7	0.0	•	•° 12^{45}...13^{15} ▽° 14^{35}-15^{45}; = 0^{00}-8^{30} 21^{20}-24
21	7	4.4	•	•° 23^{40}-24; = 0^{00}-10^{45} ∞ -12^{30} = 20^{20}-24; ⌓' 21^{00}-23^{40}
22	8	1.7	•	•° 0^{00}-3^{40}; •° -5^{20} •$^{0-1}$ 6^{15}-7^{40} ▽° 13^{40}-16^{40}; = 0^{00}-10^{10}; 20^{15}-24; ⌓°np
23	7	2.0	•	•° 0^{45}...2^{20} ▽° 2^{35}-3^{35}; (R)° NW 2^{50}-R° 3^{05}-(R)° 3^{40} NE; ≫11^{20}-13^{20}; = 0^{00}-7^{10}; p-24; ⌓°na
24	6	11.4	•	•° 4^{40}-11^{40}; 12^{20}-15^{45}; 16^{45}; 17^{20} •$^{1-0}$-21^{20} ▽$^{1-0}$-22^{17}; 22^{50}-23^{05}; ≫a, p; = 0^{00}-24
25	7	4.9	•	▽$^{1-2}$ $16^{23...48}$; = ∞ 0^{00}-13^{15}; ⊕ 11^{15}-14^{10}
26	7	•	•	= 4^{30}-7^{15}; 22^{30}-24; ⌓' np
27	7	•	•	≫13^{15}-14^{15}; 16^{40}-17^{30}; = 0^{00}-8^{30} ∞ -9^{45}; ⌓' 0^{00}-10^{00}
28	7	0.0	•	▽° 16^{02}...18^{38}; ≫15^{10}-17^{20}; = 21^{30}-24
29	6	0.1	•	•° 4^{40}...5^{30}; $11^{15...25}$ ▽° 15^{15-20}; 16^{35}-17^{40}; = 0^{00}-10^{30} ∞ -18^{00} = -24; ⌓°na
30	7	•	•	≫14^{40-50}; = 0^{00}-5^{25}; ⌓' 21^{00}-24
31	7	0.0	•	▽° 18^{15-27}; ≫9^{20}-16^{50}; = 6^{30}-9^{15}; ⌓' 0^{00}-8^{00}
Σ	—	59.5	—	UWAGI:

Poznań-Ławica φ=52°25' λ=16°50' Wrzesień-Septembre 1962

DNI	CIŚNIENIE P=900 I				TEMPERATURA T I						WILGOTNOŚĆ WZGL. U I				NIEDOSYT WILGOTNOŚCI f I				ZACHMURZENIE I POGODA N.w I			KIERUNEK I PRĘDKOŚĆ WIATRU D.v I		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	109.2	110.9	112.5	110.9	10.6	16.5	9.4	11.5	17.8	7.5	91	57	91	80	1.2	8.2	1.1	3.5	10	8 ●	0	NW 6	NW 6	C 0
2	113.5	112.7	110.5	112.2	7.5	18.7	11.7	12.4	20.8	4.3	100	50	84	78	0.0	10.8	2.1	4.3	0 ≡	10 ⊙	0	SW 1	SW 4	SW 1
3	109.5	108.6	105.7	107.9	9.2	25.9	17.2	16.9	25.5	6.6	96	37	59	64	0.4	18.7	8.0	9.0	2 ⊙	1 ⊙	0	C 0	S 1	SE 2
4	101.7	99.1	95.6	98.8	12.8	28.6	19.8	20.2	29.7	11.3	79	37	71	62	3.1	24.8	6.7	11.5	1 ⊙	1 ⊙	0	SE 2	SW 5	NE 3
5	93.3	95.1	95.5	94.6	17.2	19.7	14.2	16.3	21.6	13.7	87	53	73	71	2.6	10.7	4.4	5.9	9	9	3	SW 5	SW 8	SW 4
6	96.0	96.0	91.6	94.5	12.9	19.3	15.8	16.0	20.9	11.5	80	48	79	69	2.9	11.7	3.7	6.1	6 ⊙	8	10	SW 5	W 8	S 5
7	86.4	87.1	93.9	89.1	16.4	16.2	13.0	14.6	18.2	12.6	79	77	84	80	3.8	4.2	2.5	3.5	10	9 ●▲	10	SW 6	W 10	W 7
8	98.5	99.0	100.9	99.5	8.4	17.1	9.7	11.2	17.6	6.9	93	49	96	79	0.7	9.9	0.4	3.7	2 ⊙	6 ⊙	3	SW 5	W 5	SW 3
9	108.7	111.3	111.8	110.6	10.1	13.6	9.4	10.6	15.2	9.4	86	65	93	81	1.8	5.5	0.8	2.7	9	9	5	W 8	NW 7	SW 1
10	108.9	106.1	103.6	106.2	7.8	21.4	13.0	13.8	22.7	6.8	93	35	77	68	0.8	16.5	3.5	6.9	3	0 ⊙	4	SSE 2	SW 8	SW 2
11	101.4	100.9	106.7	103.0	14.0	18.9	14.1	15.3	20.0	10.2	75	78	91	81	4.1	4.7	1.5	3.4	10	8 ⊙	2	SW 5	W 11	W 4
12	102.6	96.1	94.7	97.8	14.1	23.5	19.4	19.1	25.6	11.0	87	59	54	67	2.2	11.8	10.5	8.2	10	7 ⊙	1	SW 6	SW 10	W 8
13	105.3	107.0	110.4	107.6	10.0	15.4	10.2	11.4	19.5	9.0	89	45	78	71	1.3	9.7	2.7	4.6	9	5	0	W 4	W 10	W 5
14	113.3	114.6	113.5	113.8	8.3	12.9	8.9	9.8	14.4	7.0	86	62	85	78	1.6	5.7	1.7	3.0	9	9	9	W 5	W 8	W 2
15	110.9	107.1	102.0	106.7	4.6	16.9	12.8	11.8	18.6	3.4	95	46	68	70	0.4	10.4	4.7	5.2	6 ⊙	4	0	C 0	SSE 5	ESE 3
16	99.0	98.5	99.6	99.0	11.0	19.9	14.4	14.9	21.4	7.9	84	67	93	81	2.1	7.5	1.1	3.6	7 ●	9	10	S 3	SW 4	NW 3
17	101.2	102.3	102.1	101.9	11.0	13.4	10.5	11.4	14.5	10.5	92	67	92	84	1.0	5.2	1.0	2.4	10	10	10	N 4	C 0	C 0
18	100.9	99.5	98.8	99.7	7.9	12.8	7.8	9.1	13.1	6.0	96	67	96	86	0.4	4.9	0.5	1.9	9	10	10 ●	N 2	E 4	N 3
19	99.8	102.2	104.9	102.3	7.0	11.2	8.0	8.6	12.0	6.8	98	74	96	89	0.1	3.4	0.4	1.3	10 ●	10	9	SW 5	NW 4	SW 2
20	106.2	106.5	107.6	106.8	5.8	13.3	9.4	9.5	14.8	5.4	98	68	84	83	0.1	5.0	1.9	2.3	4	7 ⊙	10	SW 2	W 7	SW 2
21	108.0	107.8	107.4	107.7	7.7	12.1	9.8	9.8	13.2	5.9	90	69	88	82	1.0	4.3	1.4	2.2	8	9 ●	10	W 5	WNW 8	W 6
22	109.1	110.3	111.3	110.2	8.4	12.4	7.1	8.8	14.6	6.7	96	71	93	87	0.4	4.2	0.8	1.8	8	9 ●	3	NW 5	NW 8	NW 1
23	108.1	106.1	107.2	107.1	8.9	9.6	6.8	8.0	12.3	6.4	93	97	96	95	0.8	0.4	0.5	0.6	9	10	1	W 5	W 4	W 3
24	111.0	113.8	116.2	113.7	7.0	9.6	8.6	8.4	12.9	3.7	98	96	96	97	0.1	0.5	0.5	0.4	10	10	9	W 2	NW 4	SW 1
25	118.6	118.8	116.7	118.0	4.7	13.6	9.8	9.5	15.0	4.6	98	69	81	83	0.1	4.9	2.3	2.4	10 ≡	6 ⊙	0	C 0	SE 5	E 4
26	114.4	112.4	111.2	112.7	8.0	17.1	11.6	12.1	17.6	5.7	85	46	68	66	1.5	10.6	4.3	5.5	0 ⊙	0 ⊙	0	SE 5	SE 5	E 6
27	109.2	107.4	105.7	107.4	7.0	16.5	12.6	12.2	16.6	5.7	87	54	79	73	1.3	8.7	3.1	4.4	0	7	10	E 5	SE 5	E 3
28	104.8	104.3	103.9	104.3	8.4	14.8	11.9	11.8	14.9	7.7	96	66	89	84	0.4	5.7	1.5	2.5	9 ≡	8 ⊙	10	ESE 2	SE 2	E 2
29	103.2	103.5	105.2	104.0	11.7	15.2	11.8	12.6	16.6	11.5	96	74	91	87	0.5	4.4	1.1	2.0	10 ● ≡	9	4	C 0	C 0	SE 1
30	107.5	108.1	109.0	108.2	8.5	19.4	11.6	12.8	19.9	7.1	99	64	93	85	0.2	8.2	1.0	3.1	9 ≡	0 ⊙	0	SE 1	SE 1	SE 2
31																								
M	105.3	105.1	105.2	105.2	9.6	16.4	11.7	12.4	17.9	7.8	91	62	84	79	1.2	8.0	2.5	3.9	7.0	6.9	4.8	3.5	5.6	3.0

Październik-Octobre

1	110.5	111.0	112.1	111.1	9.7	22.1	16.0	16.0	22.5	8.9	95	51	80	75	0.8	13.1	3.6	5.8	5	9 ⊙	9	SE 1	SE 5	SE 1
2	114.5	114.2	114.1	114.2	11.3	21.5	14.8	15.6	22.2	11.1	95	58	80	78	0.7	10.6	3.3	4.9	0 ⊙	1 ⊙	0	SE 2	SE 5	SE 3
3	113.1	112.6	112.5	112.7	10.2	21.7	15.5	15.7	23.1	10.0	96	61	81	79	0.4	10.2	3.4	4.7	3 ⊙	4 ⊙	0	SE 1	SE 5	SE 3
4	112.2	112.3	112.0	112.2	10.8	20.0	14.8	15.1	20.9	10.5	94	68	93	85	0.9	7.6	1.1	3.2	5	9 ⊙	10	SE 2	WSW 1	NW 2
5	112.4	113.4	114.1	113.3	13.9	15.2	14.1	14.3	17.0	13.0	99	83	93	92	0.2	3.0	1.1	1.4	9 ≡	10	10 ●	W 2	WNW 4	NW 2
6	114.8	117.0	120.1	117.3	12.2	13.5	12.0	12.4	14.6	12.0	95	92	95	94	0.7	1.3	0.7	0.9	10 ●	10	4	NW 5	N 6	N 5
7	122.1	123.7	124.6	123.5	11.7	13.7	9.7	11.2	14.0	9.5	91	80	92	88	1.1	3.2	0.9	1.7	9	10	0	NE 2	NE 4	NE 4
8	125.1	125.8	124.2	125.0	9.4	11.5	8.5	9.5	12.8	7.6	99	93	100	97	0.2	1.0	0.0	0.4	10 ≡	10	0 ≡	E 3	SE 2	E 2
9	122.7	121.8	119.9	121.5	6.6	16.3	8.9	10.2	16.7	6.1	98	72	99	90	0.1	5.3	0.2	1.9	10 ≡	0 ⊙	10 ≡	C 0	SE 5	ESE 1
10	117.1	116.5	114.0	115.9	5.9	7.9	2.6	4.8	9.0	2.5	100	93	96	96	0.0	0.7	0.3	0.3	10 ≡	10	0 ≡	E 5	SE 3	C 0
11	110.8	109.1	106.8	108.9	2.4	5.9	4.9	4.5	6.3	2.0	100	98	97	98	0.0	0.2	0.3	0.2	10 ≡	10 ≡	10 ≡	C 0	S 1	NW 1
12	107.9	109.5	111.2	109.5	5.6	8.4	3.4	5.2	9.6	3.1	86	83	98	89	1.3	1.8	0.1	1.1	9	10	0 ≡	N 2	N 2	C 0
13	111.6	110.0	105.6	109.1	2.4	12.8	7.1	7.4	13.4	1.0	100	57	87	81	0.0	6.3	1.3	2.5	10 ≡	1 ⊙	0	E 1	SE 5	SE 1
14	102.1	103.7	106.9	104.2	6.4	9.6	8.5	8.2	10.0	2.6	98	77	92	89	0.1	2.8	0.9	1.3	10 ≡	10	10	W 4	NW 7	W 5
15	112.7	115.2	116.7	114.9	4.2	10.4	0.8	4.0	11.7	0.8	88	44	90	74	0.9	7.0	0.7	2.9	2 ⊙	4 ⊙	1	N 2	C 0	C 0
16	114.5	112.5	111.7	112.9	0.2	10.2	8.0	6.6	12.0	-1.1	92	60	83	78	0.5	4.9	1.8	2.4	9	9 ⊙	10	ESE 1	SW 4	SW 2
17	112.5	113.5	113.2	113.1	8.4	10.7	10.5	10.0	11.3	7.4	93	87	96	92	0.7	1.7	0.5	1.0	10	10	10 ●	W 2	W 5	W 5
18	110.9	108.8	101.8	107.2	11.0	11.8	11.6	11.5	12.3	10.2	87	84	79	83	1.6	2.1	2.8	2.2	10	10	0	W 5	W 8	SW 5
19	102.5	104.2	104.0	103.6	9.5	12.6	9.9	10.5	12.8	8.9	86	63	72	74	1.7	5.4	3.4	3.5	7 ⊙	8 ⊙	9	NW 7	W 9	W 7
20	108.5	112.3	117.8	112.9	7.2	12.3	3.1	6.4	13.0	2.6	93	58	83	78	0.8	6.1	1.3	2.7	3 ⊙	7 ⊙	0	NW 4	NW 8	NW 3
21	120.2	120.0	119.2	119.8	-0.9	13.4	6.6	6.4	14.0	-1.8	95	43	83	74	0.3	8.8	1.4	3.5	0 ⊙	0 ⊙	0	SW 2	W 7	W 2
22	119.1	118.8	117.3	118.4	7.2	9.1	1.7	4.9	9.5	1.7	99	85	98	94	0.2	1.8	0.1	0.7	10 ●	10	0 ≡	SW 5	W 3	W 1
23	115.7	115.3	112.9	114.6	4.4	8.6	2.7	4.6	10.4	-0.1	98	72	100	90	0.2	3.2	0.0	1.1	10	6	0	C 0	WNW 2	S 1
24	110.0	111.1	111.8	111.0	-0.1	5.2	4.7	3.6	9.3	-1.9	98	83	95	92	0.2	1.5	0.4	0.7	0 ≡	3 ⊙	10	SW 3	NW 6	SSW 3
25	110.1	108.7	107.5	108.8	6.0	14.0	6.0	8.0	14.4	4.6	89	50	83	74	1.1	8.0	1.6	3.6	9	3 ⊙	0	S 2	S 8	S 3
26	105.0	103.0	101.1	103.0	0.6	13.4	7.0	7.0	13.8	0.6	100	57	87	81	0.0	6.6	1.3	2.6	0 ≡	0 ⊙	0	S 1	SW 5	S 2
27	99.3	105.5	107.1	104.0	5.4	6.0	0.8	3.2	7.4	0.4	84	77	96	86	1.4	2.2	0.3	1.3	8	8	8	SW 4	NW 3	C 0
28	102.1	100.1	99.2	100.5	3.6	6.7	4.8	5.0	7.7	0.8	98	68	90	85	0.1	3.1	0.8	1.3	10	9 ⊙	10	C 0	SW 6	SW 2
29	100.6	102.7	106.3	103.2	4.4	7.4	1.2	3.6	8.5	1.2	97	79	100	92	0.3	2.2	0.0	0.8	10	10 ●	0	SW 1	W 2	W 2
30	106.8	104.7	100.6	104.0	0.0	9.6	2.7	3.8	10.0	-0.9	98	68	93	86	0.1	3.9	0.3	1.3	2	5 ⊙	0	SW 3	S 7	S 2
31	98.4	98.7	99.6	98.9	1.7	8.8	4.4	4.8	9.3	1.1	96	64	87	82	0.3	4.0	1.1	1.8	8	9	10	S 3	SW 2	C 0
M	111.1	111.3	111.2	111.3	6.2	11.9	7.3	8.2	12.9	4.3	95	71	90	85	0.5	4.3	1.1	2.0	7.0	6.9	4.2	2.3	4.5	2.2

Poznań - Ławica H_s=86m H_t=92,1m h_w=13m Wrzesień - Septembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ SNIEGU h	POGODA
1	8	0.2	•	⚥°2^15-25 13^37 16^15, =5^20-6^40 ≡°'-7^10 =-8^15 21^15-24, ⌓'p-24
2	7	•	•	=0^00-5^10 =-5^45 ≡°'-8^05 =-10^40 ∞p =-24; ⌓°'na-a,p-np
3	7	•	•	=0^00-8^30 ∞-10^45 19^40-24; ⌓'0^00-a,np
4	6	•	•	∞, =0^00-24; ⌓°na-a
5	7	0.2	•	⚥'19^15-30, ≫19^15-30, =0^00-8^30
6	8	0.2	•	⚥°3^15-20 •°18^45 20^40 23^10 24; =21^30-24; ⊕13^40-15^15
7	5	9.5	•	•°0^00 2^30, 4^45 7^10 9^02-10^50 ⚥'°13^35 16^13 ⚥°20^45-21^30, ⚠'13^45-14^10-14^15 W-E ≫12^20-16^10, =na
8	7	3.2	•	⚥°17^33-18^03 ⚥'°20^24-21^20, (⚠)°17^28-35 NW-NE; ≫10^05-20, =19^40-24, ∩p
9	8	0.1	•	⚥°11^05-45 13^15-20, =na,p-24, ⌓°21^00-24
10	7	•	•	=0^00-8^30; ⌓°'na-a ⌓'p-24
11	6	8.4	•	•°'8^05-12^45 ⚥°2 15^10-35 ⚥°16^50-17^02 20^12-27, ≫p, =na,p-24; ⌓'na-a
12	7	2.0	•	⚥°18^50-19^06; ⚠°18^45-18^50-19^10 W-SW; ≫12^15-14^40 ⚟ 23^15-24; =na-a
13	8	0.0	•	⚥°0^40-50 19^15-30, ⚟ 0^00 15 ≫12^15-17^15
14	8	•	•	=3^30-6^15, ⌓°21^00-24
15	6	•	•	=1^30-9^30 ∞-22^40 =-24; ⌓°'0^00-a
16	6	7.0	•	•°10^20-11^20 21^05-24, =0^00-9^30 ∞-17^30 =-24
17	7	•	•	•°0^00-3^30, =0^00-11^30 19^45-24, ⌓'21^00-24
18	7	20.9	•	•°14^40 15^10-24, =0^00-12^30 15^40-24, ⌓°'0^00-13^00; ⊕10^20-45
19	7	3.7	•	•°0^00-11^27 ⚥°12^15-45 15^23-16^20 •°19^45 20^15-21^45, =0^00-a,p-24
20	6	0.1	•	•°9^26 10^10 ⚥°14^45-15^04 20^17-30, ≫17^02-15, =0^00-a ∞-p=p-24
21	7	2.8	•	⚥°'14^40 19^30, ≫a, =0^00-a,np, ⌓'na-a, ⊎5^25-50
22	7	0.1	•	⚥°2^45-3^05 ⚥'°6^27-7^20 ⚥°13^50-14^15, =0^00-11^15 21^45-24, ⌓'np; ∩ na,a
23	6	5.4	•	•°9^15 9^45-14^26 ⚥°16^40 17^20 19^30-40, =0^00-14^30, np, ⌓'0^00-9^15
24	6	1.9	•	⚥'9^10-15 •°-10^35, =na ≡°-7^40 =-p,p-24
25	6	•	•	=0^00-2^15 ≡°-2-5^30 ≡-11^20 =-13^30 ∞-16^30 =19^15-24
26	7	•	•	=0^00-9^30 ∞-11^30 19^30-24, ⌓°'2^00-10^00
27	7	•	•	∞, =0^00-11^15, 18^30-24, ⌓'5^00-11^00
28	6	0.1	•	=0^00-7^40 ≡°-8^10 ≡'-8^40 =-13^30 ∞-19^00 =-24; ⌓°na-a,np
29	6	0.0	•	⚥°0^40 2^00-3^20 5^40-9^10, =0^00-6^40 ≡°-9^15 =∞-24; ⌓°na,p-np
30	5	•	•	=0^00-3^20 ≡°-2-6^10 ≡°-7^05 ∞, =-24; ⌓°na-a ⌓°'p-24
31				
Σ	–	65.8	–	UWAGI

Październik - Octobre

1	6	•	•	=0^00-9^40 ∞-17^30 =-24, ⌓'0^00-11^00 ⌓°'18^00-24
2	6	•	•	=∞0^00-24; ⌓'0^00-11^00
3	6	•	•	=∞0^00-24; ⌓'1^00-10^00, 23^00-24; ⊕15^45-16^05
4	6	6.6	•	(⚠)°22^20-45 W-S, =∞0^00-24; ⌓'0^00-11^00 ⌓°'22^00-24
5	6	5.3	•	⚥°'°4^30-6^35 •°20^35 21^10 ⚥°-21^50; (⚠)°1^22-2^35 W-S ⚠°4^10-50 NW-N; =na ≡°'-a =-p ∞p =-24; ⌓'na
6	6	0.6	•	⚥°2^30-5^35 •°-8^10 11^17-35, =0^00-3^15 ≡°-4^40 =-24
7	6	•	•	=0^00-24; ⌓°'p-24
8	5	•	•	=na ≡°3^30-4^20 ≡°-2-10^02 =, ≡°-24; ⌓'na
9	6	•	•	=0^00-2^10 ≡°', ≡'-2 2^10-9^50 =∞-20^05 ≡°-21^35 ≡'-24; ⌓°p
10	5	•	•	≡°-2 0^00-10^05 =-20^07 ≡°-2-22^50 ≡2-24, ⌓°17^00-20^00
11	3	0.0	•	≡2-°0^00-12^30 ≡°-16^40 ≡°-2-24
12	6	•	•	⚥°4^40-5^30, ≡°0^00-40 ≡°-2^20 =-20^20 ≡°'-24; ⌓°p
13	6	0.0	•	≡°-2 ≡2 0^00-9^30 =∞-24, ⌓°'p-24
14	6	1.2	•	⚥3^40-4^40 •°18^40-19^45 21^03 22^20, =0^00-2^45 ≡°', ≡°'-8^05 =-24; ⌓°na
15	8	•	•	•°3^07 4^40, =0^00-5^30, 20^45-24, ⌴°np
16	7	•	•	=0^00-10^40 ∞-17^20 =-24; ⌴°'0^00-8^00, ⚥°5^15-6^30
17	6	0.1	•	•°11^35-12^10 16^15 17^15-18^15 ⚥°20^03-20 •°-21^15, =0^00-24; ⌓°na-a
18	6	0.6	•	=0^00-24
19	8	0.2	•	⚥°'1^40-3^20 •°-4^10 ⚥°22^33-23^45, ≫14^10-15^15, =0^00-7^15
20	7	•	•	⚥°4^42-50 5^10-45, ⌓°22^00-24
21	8	0.0	•	=22^20-24, ⌓°na ⌴°'-9^00 ⌓°19^00-24
22	6	0.0	•	⚥°5^05-7^10, 8^40-9^35, =0^00-19^30 ≡°-2-24; ⌓'0^00-5^00
23	6	•	•	≡°-1 0^00-2^10 =∞-21^40 ≡°'-24; ⌓°19^00-21^00 ⌴°23^00-24
24	5	•	•	≡°'0^00-8^45 =∞-24; ⌴°'0^00-9^00 ⌓°18^00-24
25	6	•	•	=0^00-11^30 ∞-17^30 =-24; ⌓°0^00-11^00, 20^00-24
26	6	•	•	=0^00-4^20 ≡°-2-8^40 =∞-24, ⌓'na ⌴°-a ⌓°np
27	8	1.5	•	•°7^20 7^40-8^05 ⚥°8^10-9^05 •°22^35-23^15 ≫9^24-40, =na-a,p-24; ⌓°na-a,p-np
28	6	0.2	•	•°1^40-6^15 7^35-8^40, =0^00-11^45 ∞-13^50 =-24, ⌓°p-24
29	6	0.0	•	•°4^40 5^30 7^15 25 10^40 13^10, =0^00-24; ⌓°0^00-4 ⌴°np
30	6	•	•	=∞0^00-24; ⌴°0^00-8^00 ⌓°'p-24
31	6	5.4	•	•°23^45 24, =0^00-3^35 ≡'-4^50 =∞-24; ⌓'na ⌓°p-np
Σ	–	21.7	–	UWAGI

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Poznań - Ławica φ = 52°25' λ = 16°50' Listopad - Novembre 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	98.8	98.5	99.2	98.8	4.6	5.6	5.6	5.4	5.8	4.0	95	95	95	95	0.4	0.4	0.4	0.4	10 ●	10 ●	10 ●	N 4	N 6	N 5
2	100.1	101.8	104.8	102.2	6.4	7.4	6.9	6.9	7.7	5.4	98	97	96	97	0.1	0.3	0.4	0.3	10 ═ ⚲	10	10	C 0	SW 4	S 2
3	105.3	105.1	104.8	105.1	6.2	8.4	8.2	7.8	8.7	6.1	95	83	94	91	0.5	1.8	0.6	1.0	10	9	10	C 0	S 1	C 0
4	104.9	104.0	102.9	103.9	5.2	11.5	9.2	8.8	12.4	4.8	100	75	89	88	0.0	3.5	1.2	1.6	10 ═	4	3	SE 4	SE 5	SE 5
5	101.3	99.5	99.5	100.1	6.6	14.2	10.3	10.4	14.7	6.3	93	62	85	80	0.7	6.1	1.9	2.9	1	2 ⊙	0	SE 7	ESE 8	ESE 8
6	98.2	98.0	99.6	98.6	5.2	9.2	9.2	8.2	10.4	5.2	83	66	67	72	1.5	3.9	3.8	3.1	2 ⊙	9	6	ESE 7	E 5	ESE 9
7	102.9	106.3	107.2	105.5	7.8	12.6	9.4	9.8	12.9	7.7	80	69	85	78	2.1	4.6	1.7	2.8	6	8	9	SE 5	SE 6	SE 3
8	105.5	103.0	102.6	103.7	6.6	14.4	10.2	10.4	15.6	6.4	90	63	78	77	1.0	6.1	2.7	3.3	0	0 ⊙	1	SE 5	ESE 9	ESE 7
9	102.7	103.6	106.0	104.1	5.0	7.8	4.6	5.5	10.3	4.6	86	76	81	81	1.2	2.5	1.7	1.8	7	7 ⊙	8	E 7	E 8	E 12
10	107.7	109.1	111.8	109.5	4.4	3.8	2.6	3.4	6.0	2.6	82	77	75	78	1.5	1.9	1.9	1.8	10	10	10	ENE 12	E 12	E 9
11	111.9	110.1	108.8	110.3	0.4	1.1	2.0	1.4	2.6	0.4	90	92	96	93	0.6	0.5	0.3	0.5	10 ✱	10	10 ●	E 8	E 8	E 6
12	107.7	107.4	107.5	107.5	3.0	3.0	1.0	2.0	3.3	0.5	96	93	100	96	0.3	0.6	0.0	0.3	10 ⚲	10 ●	10 ● ⚲	E 6	E 5	E 2
13	108.3	109.0	109.2	108.8	2.1	4.0	4.2	3.6	5.0	1.0	98	93	95	95	0.1	0.5	0.4	0.3	10 ═	10 ═	10 ═ ● ⚲	C 0	C 0	E 3
14	108.8	108.2	107.1	108.0	3.4	4.7	4.6	4.3	5.2	3.1	98	97	98	98	0.1	0.2	0.2	0.2	10	10	10	E 2	N 3	C 0
15	101.3	96.8	94.1	97.4	4.2	5.2	3.4	4.0	5.7	3.4	98	90	75	88	0.1	0.8	2.0	1.0	10	10	10	S 4	S 5	W 5
16	96.5	98.9	101.7	99.0	1.1	3.2	-0.3	0.9	4.1	-0.3	87	84	90	87	0.9	1.2	0.6	0.9	2	9 ●	0	W 7	W 5	W 6
17	103.3	103.0	100.0	102.1	-0.2	1.4	0.0	0.3	1.8	-1.9	86	79	84	83	0.8	1.4	1.0	1.1	10	10	0	W 1	S 2	ESE 7
18	93.9	92.1	89.7	91.9	0.3	2.9	3.0	2.3	3.1	-0.7	85	74	93	84	0.9	1.9	0.6	1.1	10	1 ⊙	10 ● ✱	ESE 5	SE 7	SE 4
19	86.3	92.2	95.3	91.3	3.3	4.0	2.3	3.0	4.7	1.0	97	83	93	91	0.2	1.3	0.5	0.7	10	7 ⊙	10	S 2	SW 7	SE 1
20	95.9	96.9	98.1	97.0	1.7	2.7	1.4	1.8	3.0	0.9	98	95	91	95	0.1	0.4	0.7	0.4	10	10 ●	10	C 0	NW 4	W 5
21	100.0	100.6	100.1	100.2	-2.0	2.6	-1.2	-0.4	2.9	-2.6	93	74	99	89	0.4	2.0	0.1	0.8	0	0 ⊙	10 ═	SW 2	SW 1	E 2
22	98.5	100.3	104.1	101.0	0.0	0.9	1.2	0.8	1.3	-1.8	88	94	92	95	0.7	0.4	0.5	0.5	10	10	10	E 6	E 3	S 3
23	107.5	109.8	113.3	110.2	0.0	0.0	0.0	0.0	1.3	-0.6	88	86	82	85	0.7	0.8	1.1	0.9	10 ✱	10	10	SW 6	SW 4	SW 2
24	116.9	118.8	120.7	118.8	-0.5	0.2	-0.1	-0.1	0.7	-0.5	92	85	96	91	0.5	1.0	0.3	0.6	10	10	10	W 2	C 0	C 0
25	121.1	120.6	118.7	120.1	-0.5	-0.1	0.4	0.0	0.4	-1.0	80	78	86	81	1.2	1.3	0.9	1.1	10	10	10	S 2	SW 5	S 3
26	120.8	122.4	123.6	122.3	0.6	2.2	2.4	1.9	3.0	0.1	98	98	91	96	0.1	0.2	0.7	0.3	10 ═	10 ═	10	C 0	NW 2	W 1
27	121.3	120.4	117.9	119.9	2.9	3.9	4.1	3.8	4.4	2.2	98	95	97	97	0.1	0.4	0.3	0.3	10	10 ⚲	10 ⚲ ═	W 2	SW 1	SW 1
28	114.3	114.0	114.0	114.1	2.9	4.8	4.4	4.1	5.2	2.6	98	92	97	96	0.1	0.7	0.3	0.4	10 ═	9	10 ⚲	SW 2	W 6	W 5
29	112.9	110.8	107.1	110.3	4.9	6.0	5.9	5.7	7.4	4.4	94	95	89	93	0.6	0.5	1.0	0.7	10	10 ⚲	10	WNW 3	W 5	WSW 9
30	103.7	104.1	109.7	105.8	5.0	5.0	2.2	3.6	6.1	2.2	90	87	93	90	0.8	1.1	0.6	0.8	9	8	10 ●	W 6	W 8	N 6
31																								
M	105.3	105.5	106.0	105.6	3.0	5.1	3.9	4.0	5.9	2.2	92	84	89	88	0.6	1.6	0.9	1.0	8.2	8.1	8.2	3.9	4.8	4.4

Grudzień - Décembre

1	121.9	126.3	130.4	126.2	-0.9	1.4	-0.8	-0.3	2.4	-1.8	89	70	87	82	0.6	2.1	0.7	1.1	2	4 ⊙	8	N 7	NW 7	NW 5
2	132.7	133.9	132.5	133.0	-4.3	-2.7	-2.6	-3.0	-0.8	-5.7	94	93	87	91	0.3	0.3	0.7	0.4	10 ═	10 ═	10	SW 2	W 4	SW 3
3	128.8	126.4	122.4	125.9	-4.1	-0.4	-4.9	-3.6	0.3	-5.0	91	76	93	87	0.4	1.4	0.3	0.7	10	2 ⊙	1	WSW 1	SW 2	SW 2
4	118.3	116.7	114.4	116.5	-2.9	1.4	-1.9	-1.3	1.9	-6.0	77	70	67	71	1.1	2.1	1.8	1.7	9	2 ⊙	1	W 3	W 7	W 6
5	114.3	116.8	120.1	117.1	-0.1	1.1	1.1	0.8	1.5	-3.8	98	96	98	97	0.2	0.2	0.1	0.2	10 ⚲ ═	10 ═	10 ⚲	W 3	W 4	C 0
6	120.3	119.7	119.0	119.7	-0.2	-0.9	-1.7	-1.1	1.2	-1.8	94	94	96	95	0.4	0.3	0.2	0.3	10 ⚲	10 ⚲ ═	10 ═	WSW 3	SW 4	C 0
7	116.8	116.6	118.2	117.2	-1.9	-0.2	-6.3	-3.7	0.0	-6.3	96	98	97	97	0.2	0.1	0.1	0.1	10 ═	0 ⊙	0 ═	C 0	WSW 2	C 0
8	119.4	119.4	114.9	117.9	-8.0	-0.9	-4.3	-4.4	-0.7	-8.3	96	95	89	93	0.1	0.3	0.5	0.3	0 ═	9 ⊙ ═	8	C 0	WSW 1	WSW 1
9	102.7	95.9	87.0	95.2	-1.5	2.0	2.4	1.3	2.4	-4.9	88	73	89	83	0.7	2.0	0.8	1.2	9	10	10	S 3	SW 8	SW 9
10	87.8	88.2	90.9	89.0	2.4	3.9	3.2	3.2	4.5	2.3	84	78	95	86	1.2	1.8	0.4	1.1	10	10	9	SW 8	SW 8	W 6
11	93.8	93.9	88.7	92.1	3.0	3.4	2.3	2.8	3.9	2.3	95	90	93	93	0.4	0.8	0.5	0.6	10 ●	10	10 ●	W 6	WSW 7	SW 8
12	81.8	79.8	82.0	81.2	2.9	6.2	3.4	4.0	6.5	2.2	93	73	76	81	0.5	2.6	1.9	1.7	10 ●	10	10	SSW 8	S 9	SW 8
13	84.6	84.5	88.3	85.8	1.0	1.0	0.6	0.8	3.4	0.6	90	96	100	95	0.7	0.3	0.0	0.3	10 ●	10 ✱	10 ═	SE 1	SE 1	NW 1
14	92.0	93.9	94.7	93.5	0.8	1.6	0.2	0.7	2.0	0.2	100	80	82	87	0.0	1.4	1.1	0.8	10 ═	6	10	NW 4	W 5	W 7
15	79.0	71.7	72.8	74.5	-0.4	0.3	1.5	0.7	1.7	-1.5	94	98	92	95	0.3	0.1	0.5	0.3	10 ✱	10 ✱	9	S 8	W 5	WSW 6
16	56.9	61.3	68.7	62.3	0.3	3.0	0.4	1.0	3.1	0.2	98	93	94	95	0.1	0.6	0.4	0.4	10	10 ●	10 ✱	SSE 2	W 5	NNE 5
17	80.1	83.1	86.6	83.3	0.2	1.0	0.3	0.4	1.1	-0.1	94	98	94	95	0.4	0.2	0.3	0.3	10 ✱	10	10	W 2	NW 6	NW 2
18	87.6	88.7	91.1	89.1	-2.1	-4.3	-4.2	-3.7	0.4	-4.8	89	94	91	91	0.6	0.3	0.4	0.4	10	10 ⚲ ═	9	N 2	NNE 1	NNW 1
19	93.9	96.4	103.3	97.9	-4.9	-4.0	-5.1	-4.8	-3.9	-6.3	88	82	83	84	0.5	0.8	0.7	0.7	10 ✱	10 ✱	10 ✱	C 0	NE 3	NE 3
20	110.3	112.5	112.8	111.9	-6.5	-5.5	-5.9	-6.0	-5.1	-9.9	83	77	76	79	0.6	0.9	0.9	0.8	10	9	10	N 2	N 2	E 1
21	108.5	107.1	111.3	109.0	-11.5	-11.6	-15.4	-13.5	-5.9	-15.5	75	75	77	76	0.6	0.6	0.4	0.5	2	2	0	E 4	E 6	E 8
22	120.3	125.9	130.7	125.6	-17.5	-14.9	-14.6	-15.4	-14.6	-19.4	79	69	74	74	0.3	0.6	0.5	0.5	0	0	0	E 5	N 6	NE 5
23	132.2	134.4	135.4	134.0	-14.4	-11.4	-11.1	-12.0	-10.5	-17.0	61	65	62	63	0.8	0.9	1.0	0.9	0	6 ⊙	0	NE 7	E 5	E 7
24	134.6	132.8	130.2	132.5	-11.3	-5.9	-6.6	-7.6	-5.7	-14.6	69	64	75	69	0.8	1.4	0.9	1.0	6	6	9	E 5	ENE 9	E 6
25	125.2	121.3	115.4	120.6	-8.5	-6.3	-9.3	-8.4	-6.2	-10.0	80	70	79	76	0.6	1.1	0.6	0.8	8	9	3	E 6	SE 3	E 3
26	108.0	104.5	101.8	104.8	-9.7	-8.4	-10.3	-9.7	-8.3	-12.6	78	74	84	79	0.6	0.8	0.4	0.6	10 ✱	8 ⊙ ✱	6 ✱	SE 2	SW 2	S 1
27	100.0	99.6	100.6	100.1	-8.3	-7.8	-8.4	-8.2	-7.8	-11.5	69	73	74	72	1.0	0.9	0.8	0.9	10	7 ✱	10	SW 3	SW 2	S 3
28	100.5	101.8	102.2	101.5	-6.6	-4.7	-4.8	-5.2	-4.1	-8.7	78	83	81	81	0.8	0.7	0.8	0.8	10	10	10	SW 4	SW 3	S 2
29	98.8	97.3	98.1	98.1	-8.7	-8.2	-8.1	-8.3	-4.7	-11.0	77	73	81	78	0.7	0.8	0.6	0.7	10	6	9	E 3	C 0	NW 2
30	100.7	102.2	105.0	102.6	-7.1	-7.0	-7.8	-7.4	-7.0	-12.9	82	85	78	82	0.6	0.5	0.7	0.6	10	10	10	C 0	NE 3	E 3
31	107.8	110.2	112.0	110.0	-8.4	-8.1	-10.8	-9.5	-6.9	-10.9	77	69	73	73	0.7	1.0	0.7	0.8	10	10	0	E 8	E 8	E 6
M	105.1	105.3	105.9	105.4	-4.5	-2.8	-4.2	-3.9	-1.8	-6.5	86	81	84	84	0.5	0.9	0.6	0.7	8.3	7.6	7.2	3.6	4.3	3.9

Poznań - Ławica $H_s = 86m$ $H_t = 92{,}1m$ $h_w = 13m$ Listopad - Novembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	5	35.5	•	•°00...0^30-2^18...4^30-24;=0^00-24
2	6	0.6	•	•°00-1^30•,•,•°-8^05•,•°8^35-9^10,°-1 9^40-12^15;=,≡°0^00-24
3	5	•	•	=0^00-24;⌒°22-24
4	6	•	•	=0^00-20≡°-0^45≡°-1^35=-4^45≡°-1-8^40=-13^30∞-15^30=-24;⌒°n-24
5	6	•	•	»13^10-16^20;=,∞0^00-24;⌒°-1 0^00-13⌒°np;ω 21^30-22^45
6	6	•	•	»21^35-22^45;=,∞0^00-24;⌒°-1 0^00-8
7	6	•	•	∞,=0^00-24;⌒°1-9,21-24
8	6	•	•	=0^00-10^30∞-16^45=-24;⌒°-1 0^00-9^00
9	6	•	•	»13^35-14^10,15^15-24;=∞0^00-24;⌒°3^00-10^00
10	6	0.2	•	*°22^15...23^45;»0^00...19^30;=0^00-24
11	6	1.3	•	*°0^45...1^15*°-12^05•°14^40-15^50*°-19^45•°-22^10;=0^00-24
12	6	3.8	•	•,•,•°5^40-16^32*°-1-17^25*,*°-20^30•,•,•°-24;=0^00-22^20≡°-24
13	5	•	•	•°0^00-35;≡°0^00-1^45=-24
14	3	0.4	•	•°19^10-20^30•,•°-24;=0^00-2^40≡°-3^20≡°-1 2^20≡°-13^45≡°-1-24
15	5	•	•	•,•°0^00-4^15,°-4^27;≡'0^00-1^50=-24
16	7	0.1	•	*°11^25-35*°-12^05*°...13^15*'-13^40;=0^00-7^15;⌣°20^00-24
17	6	•	•	=1^30-24;⌣°-1 0^00-10⌣°20-24
18	6	6.4	•	*°19^03-24;=,∞0^00-24;⌣°0^00-9^00
19	5	0.9	•	*°0^00-1^30•°-6^40,23^40-24;=0^00-24
20	5	2.2	•	•°0^00-1^10,3^20...5^15 8^35-14^20;=0^00-24
21	6	•	•	=∞0^00-20^35≡°-1-8-22^50≡°-24;⌣°-1 na-13⌣°17-24
22	4	0.3	•	*°8^01-10^27,°21^40-22^35*°-24;≡°0^00-45=-24;⌣°0^00-8
23	5	0.3	•	*°0^00-1^20,5^35-7^40,8^45-11^10,12^05-25;=0^00-24
24	6	•	•	=0^00-24
25	6	•	•	=0^00-24
26	2	0.0	•	=0^00-3^20≡°-1-10^45=-11^15≡°-11^45≡'-13^10=-24
27	4	0.2	•	•°4^45...23^35;=0^00-7^45≡°-8^10=-18^45≡°-19^38≡°-1-24
28	5	0.6	•	•°3^10...5^25,12^05-45•°-1 17^20-23^45;≡°0^00-45=-6^40≡°-8^35=-24
29	4	1.9		•,•°-1 0^50-5^15,7^40-11^40,12^40-16^30•°16^40-17^05•°18^33...19^35,23^35...24;»22^15-23^20;=0^00-9^20≡°-9^50=-24
30	7	0.9	•	•,•°0^00...1^15-5^40*°9^35...23^20;»0^50-2^30;=0^00-9^15,∩11^35-45
31				
Σ	—	33.6	—	UWAGI:

Grudzień - Décembre

1	8	•	•	⌣'0^00-10
2	3	•	•	≡°-1 5^15-11^20≡°-14^15=-24;⌣°0^00-24
3	6	•	•	=0^00-24⌣°-1 0^00-11^00,17^00-24
4	6	0.1	•	=,∞0^00-24⌣'0^00-12⌣°20-24
5	3	0.0	•	•,3^45-7^35,14^20-17^30,18^20-24;=,∞0^00-5^35≡°-1-13^30=-15^20≡°-17^15=-24;⌣°0^00-8
6	3	0.0	•	•,°0^00-8^05 9^15...15^10;=0^00-9^20≡°-1-24
7	4	•	•	≡²0^00-8^50≡²-0-10^40=-15^15≡°-2-24;v1-2 6^00-24
8	3	•	•	≡°-1 0^00-7^20≡²-8^40≡1-°-18^15=-24;v² 0^00-24⌣°18-24;ω17^00-24ω 23^35-24
9	6	2.7	•	*°-1 14^10-15^20*18^40-19^40*°-20^35*°22^40-23^15;»21^20-24;=0^00-11^30∞-14^30=-23^15;v² 0^00-11^00⌣°-1 0^00-10^00;ω 0^00-2^28ω 0^00-3^15
10	7	1.0	•	*°0^30-2^07 14^20-15^15•°16^15...20^20;»0^00-30;=13^15-21^30
11	6	5.2	•	•°4^35...12^40,14^45...16^10,16^15-21^35,22^40...24;=6^15-24
12	7	0.3	•	•°0^00...1^35 3^20-8^15 15^10-16^20...17^35;=0^00-8^30
13	4	3.2	•	•°6^50...7^10•'7^15-10^25*°-11^15*'-11^40*°-14^35;≡°-1;=7^05-24
14	7	2.2	•	•,•°8^10-9^10*°-9^35*°-10^15;=0^00-2^10≡°-1;≡²-1 2^10-9^50=-11^45,14^15-24
15	4	8.3	1	*°13^20-35•°14^45...15^35;»7^40-11^15;=0^00-24;ω 3^05-35
16	5	7.3	7	*°2^05-5^35*°-6^30 7^35-9^15•°10^50-14^45 15^10-19^20*°-24;=0^00-24
17	6	0.7	3	*°0^00-2^40*°5^35-9^15,°-9^50•°14^15...35;=0^00-9^15≡°-9^45=-24
18	3	0.0	2	•,*°1^40-2^25,°9^45-13^25;=0^00-8^25≡°-1-13^25=-24
19	6	0.1	2	*°2^10-3^40 5^40-6^15 6^50...7^20 9^32...18^40,20^20...24;=0^00-24
20	6	0.0	3	*°0^00...1^30-4^25,22^20...40,23^50...24;=0^00-24
21	5	•	3	*°0^00...3^10-5^35;=∞0^00-24
22	6	0.0	3	*°10^40-11^30;=∞0^00-24
23	6	•	3	∞0^00-24;⊕10^30-12^15
24	6	0.0	3	*°8^05-9^45;∞0^00-21^30=-24;⌣°1-10
25	6	0.0	2	=,∞0^00-24;⌣°2-13^00
26	7	0.0	2	*°4^40-7^40,23^50-24;=15^30-24
27	6	0.1	2	*°0^00-20 1^40-3^35 8^20...11^40-13^10 17^10-19^25,20^35...23^45;=,∞0^00-24
28	5	0.2	3	*°2^35-5^25 9^15-13^26;=0^00-24
29	4	•	3	*°1^36-2^40;=,∞0^00-24
30	4	•	3	=0^00-9^45≡°-10^40=-24
31	6	•	3	=0^00-2^30=,∞7^10-24;⊕10^20-12^15
Σ	—	31.4	—	UWAGI:

Warszawa - Bielany φ = 52°17' λ = 20°58' Styczeń - Janvier 1962

DNI	CIŚNIENIE P-900 I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI I	II	III	Dies	ZACHMURZENIE - POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	92.6	96.5	97.0	95.4	3.5	3.0	1.4	2.3	4.5	-2.2	85	67	70	74	1.2	2.5	2.1	1.9	9	10	10	SW 3	SW 4	W 5
2	96.4	97.6	101.3	98.4	-1.4	-0.2	-1.3	-1.0	1.4	-1.7	83	86	76	82	0.9	0.8	1.3	1.0	9	10	10	WSW 3	W 3	NW 3
3	104.2	106.0	111.5	107.2	-5.5	-3.1	-0.6	-2.4	-0.4	-6.0	85	95	94	91	0.6	0.3	0.3	0.4	9	10 *	10	W 6	W 4	W 2
4	114.7	113.7	111.9	113.4	-1.0	-0.1	-1.4	-1.0	0.2	-1.4	92	76	86	85	0.5	1.5	0.8	0.9	10	10	10	W 1	W 3	W 3
5	110.4	109.7	104.4	108.2	-2.6	-2.6	-4.2	-3.4	-1.1	-4.2	95	95	87	92	0.2	0.2	0.6	0.3	10 ●	10	0	W 2	W 2	SW 5
6	100.6	99.5	95.6	98.6	-4.9	-3.8	-0.3	-2.3	-0.1	-5.4	93	85	92	90	0.3	0.7	0.5	0.5	10	10	10	W 5	W 5	WSW 6
7	99.9	105.6	112.4	106.0	1.3	1.8	0.6	1.1	2.1	-0.3	91	82	84	86	0.6	1.3	1.0	1.0	10	10	9	W 3	NW 5	W 1
8	114.3	113.8	113.1	113.7	-1.3	1.3	1.0	0.5	1.4	-3.0	82	68	94	81	1.0	2.1	0.4	1.2	8	10	10	C 0	S 2	SW 2
9	110.4	108.6	104.9	108.0	1.4	2.8	-2.5	-0.2	2.9	-2.6	87	70	76	78	0.9	2.2	1.2	1.4	10	8	0	SW 2	SSW 3	SSE 4
10	101.9	99.8	96.3	99.3	-2.9	-1.8	-1.0	-1.7	-0.9	-3.5	71	63	79	71	1.4	2.0	1.2	1.5	9	9	9	S 3	S 5	SSE 4
11	96.2	94.7	91.6	94.2	1.1	3.7	3.6	3.0	4.3	-1.3	85	65	75	75	1.0	2.8	2.0	1.9	0	5	10 ●	SSW 3	S 7	SSE 8
12	93.3	93.2	88.6	91.7	4.3	3.3	2.0	2.9	4.6	2.0	84	95	94	91	1.4	0.4	0.4	0.7	10 ●	10 ●	3	SSE 3	SSW 3	SSE 4
13	78.6	80.5	84.6	81.2	3.2	5.2	2.9	3.6	5.3	1.7	84	75	77	79	1.2	2.2	1.7	1.7	10 *	2	2	SSW 5	SW 6	SSW 4
14	87.3	89.6	92.5	89.8	1.8	3.6	2.0	2.4	3.8	0.5	83	75	75	78	1.2	2.0	1.8	1.7	9	6	9	S 4	WSW 5	SW 3
15	95.9	100.3	104.7	100.3	2.2	2.5	1.7	2.0	2.6	1.5	96	89	87	91	0.3	0.8	0.9	0.7	10 ●	10	9	WSW 7	WSW 6	SW 4
16	108.4	109.5	106.3	108.1	0.4	3.7	1.4	1.7	4.1	0.0	84	65	65	71	1.0	2.8	2.4	2.1	10	7 ⊙	8	WSW 3	SW 3	S 5
17	104.0	104.0	105.7	104.6	2.6	3.5	1.6	2.3	3.6	1.1	60	53	65	59	3.0	3.6	2.4	3.0	10	10	8	SW 6	SW 6	SSW 2
18	103.5	102.6	102.1	102.7	-1.4	2.8	1.4	1.0	3.5	-1.4	92	65	81	79	0.4	2.6	1.3	1.4	6	8 ⊙	8	SSW 3	SSW 2	SSW 2
19	104.3	104.7	101.3	103.4	2.8	3.5	2.1	2.6	4.0	1.3	81	80	89	83	1.5	1.5	0.8	1.3	10	10 ●	7	SW 3	WSW 4	SSW 2
20	99.1	100.0	105.7	101.6	3.2	5.3	3.8	4.0	5.9	2.0	79	68	77	75	1.6	2.9	1.9	2.1	1	9	8	WSW 7	W 8	W 7
21	106.1	105.9	104.6	105.5	2.4	4.6	5.1	4.3	5.1	1.9	77	93	98	89	1.7	0.6	0.2	0.8	9	10 ●	10 ●	SW 5	W 6	SW 2
22	100.0	95.2	95.1	96.8	6.0	8.3	6.3	6.7	8.9	5.0	86	73	63	74	1.3	3.0	3.5	2.6	10	9 ⊙	8	SSW 2	SW 3	WSW 6
23	99.7	101.5	103.1	101.4	2.5	5.3	2.5	3.2	6.4	2.3	72	59	70	67	2.1	3.7	2.2	2.7	1	1 ⊙	0	SW 4	SW 6	SW 6
24	104.1	104.7	103.5	104.1	2.2	3.9	1.6	2.3	4.1	1.4	80	67	89	79	1.5	2.7	0.8	1.7	9	3 ⊙	10	SW 3	SW 6	SW 2
25	98.6	95.0	93.8	95.1	1.4	1.7	5.3	3.4	5.7	1.2	92	98	100	97	0.6	0.1	0.0	0.2	9	10 * ●	10 ●	SE 3	SE 2	W 2
26	100.1	105.1	104.1	103.1	0.1	-0.1	-0.3	-0.2	5.4	-0.5	92	84	92	89	0.5	1.0	0.5	0.7	9	10 *	9	N 3	NW 6	C 0
27	100.8	98.7	98.3	99.3	-0.2	0.1	0.7	0.3	1.4	-0.5	86	90	96	91	0.8	0.6	0.2	0.5	10	10 *	10 *	SW 2	SW 3	W 4
28	97.5	95.0	100.8	97.8	0.1	-0.9	-6.0	-3.2	0.8	-6.0	88	73	81	81	0.8	1.5	0.7	1.0	9	10	9 *	W 3	W 6	WNW 8
29	107.9	113.5	118.3	113.2	-8.3	-7.2	-9.3	-8.5	-5.8	-9.5	80	71	82	78	0.6	1.0	0.5	0.7	10 *	9 *	10 *	NNE 8	NNE 10	NE 5
30	122.9	126.1	127.7	125.6	-9.4	-10.0	-13.9	-11.8	-8.7	-13.9	85	68	83	79	0.4	0.9	0.3	0.5	9	0	0	ENE 5	NE 5	NE 2
31	127.0	125.5	122.0	124.8	-17.7	-11.7	-13.5	-14.1	-10.8	-18.0	90	78	84	84	0.2	0.5	0.4	0.4	1	0	0	NE 1	ESE 3	E 1
M	102.6	103.1	103.3	103.0	-0.5	0.9	-0.2	0.0	2.1	-1.9	85	76	83	81	1.0	1.6	1.1	1.2	8.3	7.9	7.3	3.6	4.6	3.7

Luty - Fevrier

DNI	CIŚNIENIE P-900 I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI I	II	III	Dies	ZACHMURZENIE - POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	112.6	107.5	106.3	108.8	-13.2	-8.6	-7.4	-9.2	-7.1	-15.2	84	71	82	79	0.4	0.9	0.6	0.6	1	10	0	E 4	SE 5	SE 4
2	105.5	107.0	109.5	107.3	-7.6	-3.8	-6.3	-6.0	-2.5	-8.7	82	78	86	82	0.6	1.0	0.5	0.7	9	6	0	SE 2	S 1	C 0
3	112.5	113.5	113.3	113.1	-10.5	-4.0	-4.5	-5.9	-1.7	-10.8	94	91	84	90	0.2	0.4	0.7	0.4	10 ≡	0 ≡	0	C 0	C 0	C 0
4	109.3	105.4	106.6	107.1	-7.1	-1.4	-0.5	-2.4	-0.5	-8.9	85	70	90	82	0.5	1.7	0.6	0.9	4	10	9	C 0	WSW 5	WSW 4
5	105.0	97.5	89.3	97.3	-2.7	1.6	0.8	0.1	2.0	-3.3	95	74	98	89	0.2	1.8	0.2	0.7	10 ≡	10	10	SW 3	S 7	WSW 5
6	93.1	97.3	103.9	98.1	0.6	1.1	1.4	1.1	2.0	0.5	98	92	76	89	0.1	0.5	1.7	0.8	10 * ●	10 * ●	9	W 8	W 8	WNW 6
7	106.5	106.7	103.8	105.7	0.4	2.3	0.2	0.8	2.7	-0.3	76	70	82	76	1.5	2.2	1.1	1.6	9	9	0	W 2	S 3	SE 4
8	100.8	100.8	102.1	101.2	-2.2	1.1	0.7	0.1	1.6	-2.3	79	75	96	83	1.1	1.6	0.2	1.0	9	10	10 * ●	SE 6	SE 6	S 2
9	104.9	109.8	115.4	110.0	1.8	1.6	0.8	1.2	2.1	0.7	98	96	86	93	0.2	0.3	0.9	0.5	10 ●	10 ●	9	SSW 1	WNW 3	W 3
10	119.1	119.1	116.9	118.4	-1.4	2.0	1.7	1.0	3.1	-1.5	97	75	80	84	0.2	1.8	1.4	1.1	9	3 ⊙	9	WNW 2	SW 2	SW 2
11	110.7	107.5	110.6	109.6	1.4	1.3	0.8	1.1	3.1	0.5	76	91	92	86	1.7	0.6	0.5	0.9	10	10 * ●	1	SW 5	W 7	WSW 6
12	102.2	84.7	71.5	86.1	0.5	0.0	1.7	1.0	5.4	-0.7	74	96	92	87	1.6	0.2	0.5	0.8	3	10	10 ●	SW 7	WSW 9	W 6
13	70.4	71.1	75.3	72.3	2.2	3.0	-0.8	0.9	3.4	-0.9	63	74	83	73	2.7	2.0	1.0	1.9	5	9	0	W 12	W 6	SW 3
14	78.6	81.0	85.1	81.6	-1.0	-0.3	-1.1	-0.9	0.5	-2.0	95	80	79	85	0.3	1.2	1.2	0.9	10	10	6	SW 3	NW 2	NW 3
15	92.0	95.7	102.9	96.9	-4.2	-1.7	-5.5	-3.2	-0.6	-4.2	68	55	81	68	1.4	2.4	0.9	1.6	4	8 ⊙	9	NW 5	NW 10	NW 8
16	96.4	82.7	73.3	84.1	-6.4	-2.6	1.9	-1.3	2.4	-6.8	75	93	84	84	0.9	0.3	1.2	0.8	8	10 *	9	SSW 2	SW 5	SW 6
17	67.9	71.1	80.6	73.2	1.1	2.1	-1.7	0.0	2.9	-1.7	89	80	65	78	0.7	1.4	1.9	1.3	10 *	9 ⊙	9	W 7	W 6	NW 9
18	89.3	94.8	103.5	95.9	-5.7	-2.1	-5.5	-3.2	-1.6	-4.0	73	66	72	70	1.2	1.7	1.3	1.4	10	10	9	NW 9	NW 9	NW 5
19	104.8	104.4	103.4	104.2	-4.3	-0.8	-0.3	-1.4	-0.3	-5.1	82	73	94	83	0.8	1.6	0.4	0.9	8	10	10 *	W 1	WSW 3	WSW 2
20	103.0	102.0	100.2	101.7	2.5	2.6	3.3	2.9	3.7	-0.4	93	86	86	88	0.5	1.1	1.0	0.9	10 ●	10	10	W 3	W 6	W 8
21	103.8	106.4	114.2	108.1	-1.1	-0.7	-3.9	-2.4	3.4	-4.0	91	77	75	81	0.5	1.3	1.1	1.0	10 *	10 *	10 *	NW 8	N 5	N 6
22	120.2	121.3	121.9	121.1	-4.6	-3.9	-6.2	-5.2	-3.6	-6.4	81	75	73	76	0.8	1.1	1.0	1.0	10 *	10 *	10	NE 5	NNE 4	NNE 6
23	119.3	116.3	114.1	116.6	-7.1	-4.9	-5.1	-5.6	-4.2	-9.5	80	69	75	75	0.7	1.3	1.0	1.0	10	10	10 *	NW 6	NNW 5	NNW 5
24	109.6	108.5	110.9	109.7	-6.5	-4.4	-7.3	-6.4	-4.2	-7.5	83	77	79	80	0.6	1.0	0.7	0.8	10 *	10	6 *	NE 5	NE 6	NNE 4
25	113.9	114.9	114.4	114.4	-8.4	-4.9	-4.1	-5.4	-3.8	-8.8	83	71	87	80	0.5	1.2	0.6	0.8	5	10	9 *	ENE 4	E 4	ENE 6
26	111.8	112.0	112.3	112.0	-3.4	-1.9	-3.2	-2.9	-1.6	-4.3	94	79	81	85	0.3	1.1	0.9	0.8	10 *	10	10	ENE 7	ENE 8	E 4
27	110.8	110.1	108.6	109.8	-4.6	-2.3	-5.1	-4.3	-2.1	-5.2	88	78	85	84	0.5	1.2	0.6	0.8	10	10	10	ENE 5	E 8	ESE 5
28	105.3	103.7	101.1	103.4	-8.3	-5.9	-6.0	-6.6	-4.9	-8.6	86	76	84	82	0.4	0.9	0.6	0.6	8 ⊙	2 ⊙	10	E 3	E 3	E 2
29																								
30																								
31																								
M	102.8	101.9	102.5	102.4	-3.5	-1.3	-2.0	-2.2	0.0	-4.6	84	78	83	82	0.8	1.2	0.9	1.0	8.3	8.8	7.3	4.5	5.2	4.4

Warszawa-Bielany H_s=98m H_b=104,7m h_w=16m Styczeń - Janvier 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	7	•	4	
2	6	0.0	4	•a*p; =a-p
3	4	0.6	4	*10^05-p
4	6	•	5	=n-p
5	6	0.0	5	•na; =n-n
6	5	1.1	5	Δ*p*p; =na-p; ~p
7	8	•	4	=na
8	6	•	3	=n-n
9	6	•	3	=n-p
10	7	•	2	=n-a
11	5	0.6	pł.	•p; =p
12	5	5.3	pł.	•n...p; =n-n
13	8	1.4	•	≢na-7^55
14	7	0.0	•	⊔'n-a ⊔p-n
15	6	0.0	•	•na-7^50; =a
16	8	•	•	
17	8	•	•	
18	7	•	•	⊔na
19	6	0.1	•	•11^35-13^20; =a-p
20	8	•	•	
21	5	1.9	•	•a-19^20•-20^45•-n; =a-16^15≡-19^20=-n
22	6	0.0	•	•p; =a-p
23	7	•	•	
24	6	0.1	•	*na ≢a; ∞a-p
25	4	6.7	•	*,*a •p-n
26	5	0.0	1	*n,a...p; Vp-n
27	4	3.1	pł.	*6^25...n; Vn-a
28	7	0.7	1	*a...n
29	7	0.1	2	*n...p
30	8	•	2	
31	6	•	2	=n-n; ⊔n-a, p-n
Σ	—	21.7	—	UWAGI.

Luty - Février

1	6	0.0	2	*13^10-15^15; =n-a =a-p =p-n; ⊔n-a
2	6	0.0	2	*a; =n-p; ⊔n-a, p-n
3	5	•	2	≡^2-0 n-p ≡a-p =p-n; Vn-a
4	5	0.0	2	*13^15-p; = n-n; Vn-a
5	6	3.4	2	*14^40-18^30; ≡na-9^20=a-p
6	6	1.2	4	**na-p; =na
7	8	•	2	
8	6	4.7	2	**16^10-np; =a-np
9	6	0.1	1	•na-10^35•-13^10; =na-a ≡10^20-11^45
10	7	•	pł.	=a
11	6	1.4	pł.	**11^20-p; =na-a
12	1	7.3	pł.	+,*,•a*,≢,•,p...n; por. wiatru ponad 10 m/s a-p
13	7	•	pł.	≫n-a
14	7	0.0	pł.	Δn-a *a,p; =n-a; ⊔n-a; ω p-n
15	8	0.0	•	*16^45-p; ≫a-p (por. ponad 15 m/s)
16	2	4.9	•	*'a-n; ⊔n-a
17	7	1.1	5	*n-a*^2 13^00-p; (K) 13^40 W-E
18	8	0.0	3	*p
19	7	2.3	2	*p-n
20	7	0.9	pł.	•'n•n-a; =n-a, p-n
21	6	0.4	1	*^0-1 n-n
22	6	0.0	2	*n...p
23	7	0.2	1	*a...n
24	6	0.2	3	*n...n; =a-p
25	6	1.8	3	*^0-1 p-n; =n-p
26	7	0.0	6	*na-9^20; =na
27	6	•	5	=na
28	6	•	5	=na
29				
30				
31				
Σ	—	29.9	—	UWAGI.

Warszawa - Bielany φ = 52°17' λ = 20°58' Marzec - Mars 1962

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIER. i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	98.4	98.3	97.2	98.0	-6.4	-4.5	-5.5	-5.5	-3.9	-6.8	91	88	82	87	0.3	0.5	0.7	0.5	10	10	9	NE 2	NE 3	NE 4
2	94.5	93.2	92.2	93.3	-5.8	-5.3	-5.6	-4.1	-2.4	-6.5	89	85	85	86	0.4	0.8	0.7	0.6	10	10 △	10	C 0	C 0	C 0
3	93.4	93.8	93.1	95.4	-4.5	1.2	0.7	-0.5	1.6	-5.6	96	61	77	78	0.2	2.7	1.5	1.5	10 *	8 ⊙	10 *	NW 2	SSW 2	SSE 3
4	88.4	84.7	82.7	85.3	0.3	4.3	1.7	2.0	4.6	-0.1	92	71	98	87	0.5	2.4	0.1	1.0	10	10	10 ●	ESE 2	SE 1	C 0
5	85.0	87.0	84.4	85.5	0.5	1.1	1.3	1.0	2.2	0.5	100	94	100	98	0.0	0.4	0.0	0.1	10	10 ●	10 ●	NE 4	ENE 5	ENE 3
6	77.8	85.7	97.2	86.9	6.2	0.5	-0.1	1.6	6.5	-0.2	97	81	80	86	0.3	1.1	1.2	0.9	10 ●	10	10	SE 3	W 6	NW 7
7	105.8	108.6	111.9	108.7	-2.2	-1.4	-2.2	-2.0	0.1	-2.5	76	62	72	70	1.2	2.1	1.5	1.6	9 *	8 ⊙	0	NW 3	NW 7	NW 2
8	114.3	114.9	113.3	114.2	-4.1	0.1	-0.3	-1.2	1.3	-4.9	82	67	78	76	0.8	2.1	1.3	1.4	3 ⊙	9	1	C 0	W 3	WNW 4
9	115.5	117.1	113.7	115.4	-5.1	-1.6	-1.9	-2.6	-0.1	-5.4	88	65	65	73	0.5	1.9	1.9	1.4	9	3 ⊙	1	NE 3	ESE 5	SE 5
10	106.7	104.3	100.5	103.8	-3.3	1.9	1.5	0.4	3.4	-3.7	68	46	63	59	1.6	3.8	2.5	2.6	8	8	10	SE 10	SE 7	SE 6
11	97.1	95.3	93.9	95.4	1.9	8.4	5.9	5.5	9.8	1.5	78	61	76	72	1.5	4.3	2.3	2.7	9	6 ⊙	9 ●	S 2	S 3	S 2
12	90.1	87.0	81.7	86.3	1.5	3.0	0.6	1.4	6.1	0.5	96	96	98	97	0.3	0.3	0.1	0.2	10 ●	10	10 *	C 0	ESE 2	C 0
13	81.1	86.4	95.2	87.6	-3.5	-4.2	-4.8	-4.3	0.6	-4.9	90	84	74	83	0.5	0.7	1.1	1.1	10 *	10 *	3	NW 9	NW 9	NW 6
14	101.5	104.7	108.4	104.9	-7.9	-3.1	-5.4	-5.4	-2.5	-8.1	84	57	90	77	0.5	2.1	0.4	1.0	2	8	2 *	WSW 4	WNW 5	WSW 2
15	109.2	109.5	110.9	109.9	-8.3	-2.6	-4.7	-5.1	-2.4	-9.5	86	50	74	70	0.4	2.5	1.1	1.3	8	10	10	C 0	E 3	NE 3
16	110.3	108.9	106.4	108.5	-5.7	-4.8	-5.1	-5.2	-4.1	-6.0	77	52	51	60	0.9	2.0	2.0	1.6	10	10	10	NNE 5	N 7	N 4
17	100.2	98.9	98.8	99.3	-6.7	-4.8	-2.8	-4.3	-2.3	-7.2	91	88	56	78	0.3	0.5	2.2	1.0	10 *	10 *	10 *	N 8	N 6	NNW 5
18	100.9	103.8	106.0	103.6	-6.6	0.5	-2.3	-2.7	1.4	-7.1	64	57	68	63	1.3	2.7	1.7	1.9	2	2	1	NNW 7	NNW 7	NNW 3
19	108.0	108.8	109.2	108.7	-4.5	-0.5	-2.6	-2.6	0.1	-6.5	84	47	59	63	0.7	3.1	2.1	2.0	9 *	8	8	WNW 2	NNW 1	C 0
20	109.5	109.7	109.2	109.5	-6.7	0.2	-2.1	-2.7	1.1	-7.1	86	51	60	66	0.5	3.0	2.1	1.9	3	2	0	SW 1	SSW 2	SSE 2
21	108.0	106.6	104.5	106.4	-8.0	-1.2	-4.3	-4.4	0.5	-8.5	87	51	75	71	0.4	2.8	1.1	1.4	5	2	1	C 0	SE 4	NE 2
22	101.3	99.4	97.9	99.5	-8.3	-1.7	-2.5	-3.8	-1.3	-8.6	86	69	82	79	0.4	1.7	0.9	1.0	9	9 *	10	NE 3	NE 4	E 3
23	95.9	96.8	97.3	96.7	-2.9	-0.5	-0.6	-1.2	-0.4	-5.0	88	82	97	89	0.5	1.1	0.2	0.6	10 *	10	10 *	NNW 2	NNE 2	N 3
24	99.4	102.4	106.9	102.9	-1.9	-0.2	-1.3	-1.2	0.6	-2.0	96	74	70	80	0.2	1.5	1.7	1.1	10 *	9 *	9	N 2	N 2	NW 2
25	109.9	110.2	108.7	109.6	-6.2	0.5	-2.4	-2.6	2.7	-7.5	89	59	76	75	0.4	2.5	1.2	1.4	1	1	0	C 0	NNE 1	C 0
26	107.4	106.3	104.1	105.9	-6.9	0.1	-3.4	-3.4	0.9	-7.5	91	54	71	72	0.3	2.9	1.4	1.5	0	0	0	C 0	SE 5	SE 1
27	100.7	98.7	95.4	98.3	-7.4	-0.5	-1.8	-2.9	0.4	-8.1	79	45	55	60	0.7	3.2	2.4	2.1	3 ⊙	3 ⊙	6	SE 1	ESE 8	SE 6
28	92.0	91.5	92.5	92.0	-4.2	2.0	2.4	0.6	3.5	-4.5	82	66	82	77	0.8	2.5	1.3	1.5	8	9	9	SE 3	SE 3	S 2
29	94.3	94.6	93.6	94.2	0.3	1.5	-0.2	0.4	2.7	-0.3	90	78	78	82	0.6	1.5	1.3	1.1	10	10	0	W 3	W 3	SE 4
30	86.4	85.8	84.3	85.5	1.6	6.2	5.8	4.8	9.5	-0.5	98	83	88	90	0.2	1.6	1.1	1.0	10 ●	9	8	ESE 5	ESE 4	S 4
31	78.7	78.2	83.2	80.0	5.8	11.1	6.7	7.6	12.7	4.0	97	80	88	88	0.3	2.6	1.2	1.4	10 ●	10	8	SSE 7	SSW 3	C 0
M	98.8	99.1	99.2	99.0	-3.5	0.2	-1.1	-1.4	1.7	-4.4	87	68	76	77	0.6	2.0	1.3	1.3	7.7	7.5	6.3	3.0	4.0	2.8

Kwiecień - Avril

1	90.9	92.2	95.6	92.9	1.5	5.8	2.2	2.9	7.0	1.0	96	80	86	87	0.3	1.8	1.1	1.1	10	10 ●	0	C 0	W 7	SW 5
2	96.6	96.7	99.8	97.7	1.7	6.6	2.7	3.4	9.1	1.5	90	69	93	84	0.6	2.9	0.5	1.3	10	10 ●	0	WNW 2	W 5	WSW 4
3	100.9	100.2	96.1	99.1	2.8	9.9	9.1	7.7	12.6	1.8	79	61	60	67	1.6	4.8	4.7	3.7	10 ●	9 ⊙	2	SSW 6	S 7	S 5
4	92.3	89.3	85.7	89.1	5.6	14.2	10.6	10.2	15.6	4.4	64	39	61	55	3.3	9.9	5.0	6.1	3 ⊙	9 ⊙	2	SE 6	SSE 6	SSE 4
5	77.5	76.7	77.5	77.2	8.4	10.6	7.6	8.6	13.4	7.6	68	75	96	80	3.6	3.2	0.4	2.4	10	10 ●	10 ●	ESE 6	S 4	S 1
6	81.5	84.1	87.6	84.4	5.6	12.3	8.5	8.7	12.9	5.5	86	54	86	75	1.3	6.5	1.5	3.1	8	7 ⊙	8	SW 1	ENE 3	NE 2
7	91.5	93.8	96.4	93.9	3.7	5.5	2.8	3.7	8.7	2.8	85	55	74	71	1.2	4.1	2.0	2.4	10	9	0	N 7	NW 10	W 3
8	93.7	94.6	95.8	94.7	3.5	7.5	9.3	7.4	10.7	1.5	88	86	76	83	0.9	1.5	2.8	1.7	10 ●	10	8	SW 4	SW 5	S 3
9	97.2	100.4	102.8	100.1	7.6	12.2	9.0	9.4	13.1	7.2	82	48	68	66	1.9	7.4	3.7	4.3	9	8 ⊙	8	S 3	WSW 4	C 0
10	105.7	107.9	109.6	107.7	4.6	11.4	8.4	8.2	12.7	4.3	85	52	60	66	1.3	6.5	4.4	4.1	2 ⊙	8	8	SW 1	N 3	NW 2
11	110.5	110.2	108.4	109.7	6.0	9.9	8.7	8.3	11.8	6.0	76	63	77	72	2.3	4.5	2.5	3.1	10	9	2	N 4	N 5	N 2
12	106.9	106.0	104.0	105.6	5.9	12.9	9.8	9.6	15.9	4.7	94	65	81	80	0.6	5.3	2.3	2.7	6 ⊙	4 ⊙	4	N 1	WNW 2	C 0
13	102.3	101.1	99.2	100.9	8.4	11.8	7.8	9.0	12.5	7.5	86	66	97	83	1.5	4.7	0.3	2.2	8	10	10 ○	W 3	NE 4	NNW 2
14	99.0	103.3	109.1	103.8	4.9	6.6	7.4	6.6	8.1	4.7	94	85	90	90	0.6	1.4	1.0	1.0	10 ●	10	10	N 5	N 4	N 3
15	111.6	111.4	111.7	111.6	5.7	10.9	9.1	8.7	12.4	5.7	98	80	89	89	0.2	2.6	1.3	1.4	10	10	4	NNE 6	NE 7	NE 5
16	113.0	111.6	112.1	112.2	8.3	17.3	14.5	13.6	19.1	8.0	90	55	79	75	1.1	8.9	3.4	4.5	9 ⊙	4 ⊙	9	E 5	E 8	ESE 6
17	113.3	112.3	111.3	112.3	13.1	22.0	16.3	16.9	23.1	10.4	66	30	52	49	5.1	18.4	8.9	10.8	1 ⊙	7 ⊙	9	SE 5	SE 10	SE 6
18	108.0	106.5	105.0	106.5	12.4	20.3	17.3	16.8	20.9	12.2	80	42	50	57	2.9	13.7	9.9	8.8	10	9 ⊙	9	SE 7	S 9	SE 6
19	105.0	104.9	104.2	104.7	13.8	23.4	18.8	18.7	24.4	11.7	64	31	53	49	5.7	19.7	10.3	11.9	9 ⊙	9 ⊙	6	SSE 1	SW 2	C 0
20	105.6	106.1	106.1	105.9	14.9	24.7	18.9	19.4	25.9	12.0	67	37	65	56	5.5	19.6	7.7	10.9	10 ⊙	10 ⊙	9	SW 2	C 0	C 0
21	107.4	107.7	107.6	107.6	17.3	25.7	20.5	21.0	26.9	13.5	57	29	54	47	8.5	23.3	11.0	14.3	8 ⊙	1 ⊙	0	S 1	SW 2	C 0
22	108.2	107.9	107.9	108.0	16.2	26.8	19.2	20.4	27.6	14.0	74	26	52	51	4.7	26.2	10.5	13.8	6 ⊙	4 ⊙	0	C 0	SE 1	C 0
23	108.7	108.7	109.2	108.9	17.1	26.7	19.5	20.7	27.8	12.5	53	32	61	49	9.2	23.9	8.9	14.0	7	2	3	SE 1	C 0	C 0
24	112.2	113.5	114.4	113.4	15.0	20.2	16.9	17.2	23.9	12.7	88	69	68	75	2.0	7.3	6.1	5.1	0	7	0	N 2	N 4	N 3
25	116.9	116.1	114.7	115.9	11.7	21.2	15.3	15.9	21.9	9.4	71	38	48	52	3.9	15.7	9.0	9.5	7	0	0	NE 4	ENE 3	ESE 2
26	111.7	108.1	101.8	107.2	13.3	22.9	14.3	16.2	23.6	11.1	48	34	83	55	8.0	18.4	2.7	9.7	0	3	3	S 3	S 1	SE 2
27	95.9	95.6	96.8	96.1	9.9	10.7	6.8	8.6	14.9	6.8	96	81	82	86	0.5	2.5	1.8	1.6	9	8	8	NE 3	WNW 3	WNW 5
28	89.5	88.7	91.6	89.9	6.1	8.5	5.3	6.3	10.1	4.9	85	70	80	78	1.4	3.3	1.8	2.2	10 ●	8	7	WNW 4	NNE 4	NW 5
29	92.7	93.7	95.0	93.8	4.8	8.7	4.8	5.8	9.4	2.9	84	48	71	68	1.4	5.8	2.5	3.2	10 ●	8	4	WNW 5	NNW 4	NW 2
30	95.9	97.9	100.8	98.2	0.9	5.3	2.7	2.9	6.4	0.2	96	51	65	71	0.2	4.3	2.6	2.4	10	10	3	NE 2	WNW 5	NW 2
31																								
M	101.4	101.6	101.9	101.6	8.4	14.4	10.8	11.1	16.1	7.0	80	55	72	69	2.7	9.3	4.4	5.5	7.7	7.4	4.9	3.3	4.4	2.7

Warszawa-Bielany H_s=98m H_b=104,7m h_w=16m Marzec-Mars 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚNIEGU h	POGODA
1	5	•	4	=na-p
2	5	0.1	4	△°a-p; =na-n
3	6	0.2	3	*°na-7^40, p-n, =n-n
4	5	5.0	3	•°p-n; =n-n
5	5	9.2	pł.	•°a •°p-n
6	6	4.3	•	•'n-a ▽°a
7	7	0.0	•	▽°6^30-40
8	7	•	•	⊔°, =n-a
9	7	•	•	⊔'n-a
10	7	•	•	⚡-a na-a, ∞n-p
11	6	0.3	•	▽°p; =n-n
12	4	9.0	•	•°na-p ▽°p-n; =n-n
13	5	0.8	8	*°-1 n-a ▽°-1 a-16^10, =n-a
14	8	0.2	4	▽°a-p, 20^30-40
15	7	•	3	=n-a
16	7	1.9	2	
17	4	1.3	8	*'n-p, p...n; ⚡n-13^00
18	8	0.0	5	
19	8	0.0	3	*°na, =n-a ∞p-n, ⊔°n-a
20	7	•	2	=n-a, ⊔°n-a
21	6	•	2	=n-a, ⊔°n-a
22	6	0.0	pł.	*°12^32-40, 16^15-50, =n-n; ⊔°n-a
23	6	3.6	pł.	*°na, p-n, =n-n
24	6	0.0	5	*°n-p; =n-p
25	7	•	3	=n-a, ⊔°n-a, p-n
26	6	•	3	=n-n; ⊔'n-a
27	6	•	3	=n-a ∞a-p
28	6	0.0	3	▽°10^25, =n-n
29	6	0.2	pł.	▽°7^40, =n-n
30	6	0.4	pł.	•°na-a; =na-p
31	6	9.0	•	•°na-a •'np; =na-p
Σ	—	45.5	—	UWAGI

Kwiecień-Avril

1	6	0.3	•	•°12^30-50 ▽°p; =na-a
2	7	2.4	•	•°12^35-45 ▽°17^05-18^00
3	7	0.1	•	•°6^25-7^45; =na
4	8	0.0	•	=na
5	6	6.5	•	▽°na •°7^25-50, 9^10-35, 12^00-20^45; =a-p
6	7	0.0	•	•°17^30-19^00; =na
7	9	0.0	•	▽a-p
8	6	0.0	•	•°6^00-9^30, 17^10-19^55; =na-a
9	8	0.1	•	•°15^55-16^30; =na
10	8	•	•	=na; ⌓°na
11	7	•	•	
12	6	0.2	•	•°11^05-30; =na; ⌓°na, np
13	6	10.2	•	•°16^05-n; =na, ⌓°na
14	7	0.1	•	•°na-9^15
15	7	•	•	=na, ⌓°na
16	7	0.0	•	▽'20^19-21, =n-a ∞a-p
17	7	•	•	∞a-p, ⌓'n-a
18	7	•	•	∞n-a; ⚲p-n
19	7	•	•	=n-a ∞a-p =p-n; ⌓p-n; ⚲p-n
20	6	•	•	=n-a ∞a-p =p-n; ⌓°n-a ⌓²p-n; ⊕a
21	7	•	•	=n-a ∞a-p, ⌓'n-a ⌓°p-n
22	7	•	•	=n-a ∞a-p; ⌓'n-a ⌓°p-n
23	7	•	•	⌓°n-a ⌓°-1 p-n
24	6	•	•	=n-a ∞a-p, ⌓°n-a
25	8	•	•	⌓°n-a ⌓'p-n
26	7	12.2	•	▽°-3 p,n; R'15^30, n, ⌓°n-a
27	8	0.2	•	▽°-1 n-a ▽°a,p; R°na; =n-a
28	8	6.4	•	▽°n-p ▲16^06-12, 17^57-18^01
29	8	7.3	•	▽°n-a ▲°10^20-24, 15^16-18, 16^02-03
30	7	0.0	2	*n*°n-a
31				
Σ	—	46.0	—	UWAGI

Warszawa-Bielany φ=52°17' λ=20°58' Maj-Mai 1962

DNI	CIŚNIENIE P+900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	99.2	96.5	94.6	96.8	-0.5	3.8	2.6	2.1	4.3	-2.0	86	56	95	79	0.9	3.5	0.4	1.6	9	9	10 ●	NW 4	WNW 6	W 5
2	92.8	93.6	96.1	94.2	2.4	6.2	4.2	4.2	8.1	1.0	89	80	90	86	0.8	1.9	0.8	1.2	9	8	8	WSW 3	WSW 4	SW 2
3	98.1	98.0	96.7	97.6	3.7	8.6	5.6	5.9	10.6	1.9	90	59	91	80	0.8	4.6	0.9	2.1	0	6	9	SW 1	WSW 4	C 0
4	91.7	91.9	95.3	93.0	5.3	7.4	4.5	5.4	9.7	4.1	91	68	89	83	0.8	3.3	0.9	1.7	10	8	3	WSW 3	NW 1	WSW 3
5	99.7	101.6	104.5	101.9	1.9	8.5	5.9	5.6	9.5	0.7	93	66	88	82	0.5	3.7	1.2	1.8	10	8	4	C 0	WNW 1	C 0
6	108.6	108.4	107.5	108.2	4.0	12.9	9.1	8.8	13.9	-0.1	93	34	65	64	0.5	9.9	4.1	4.8	0	5	2	C 0	SW 2	C 0
7	104.8	104.1	103.2	104.0	9.1	13.1	10.7	10.9	13.4	5.3	76	57	95	76	2.8	6.6	0.7	3.4	9 ⊙	10 ●	10	S 1	SSE 4	C 0
8	102.0	100.2	99.0	100.4	10.7	19.7	16.5	15.8	20.9	9.7	97	66	84	82	0.4	7.7	3.1	3.7	10 ●	8 ⊙	10	C 0	NW 2	C 0
9	99.2	101.5	100.6	100.4	12.7	16.5	13.1	13.8	18.6	12.7	93	64	82	80	1.1	6.8	2.8	3.6	10 ●	9	2	NW 2	N 2	C 0
10	97.7	97.8	98.9	98.1	11.4	14.2	11.7	12.2	16.4	9.4	89	88	91	89	1.5	2.0	1.1	1.5	10	10	9	SE 3	W 3	SW 2
11	99.6	100.3	99.8	99.9	9.5	16.1	11.1	12.0	17.1	8.5	89	55	78	74	1.3	8.2	2.9	4.1	9	9 ⊙	2	W 3	SW 4	WSW 2
12	102.2	103.3	103.7	103.1	9.1	16.9	12.7	12.8	18.6	7.0	89	46	72	69	1.3	10.4	4.1	5.3	0 ⊙	3 ⊙	1	C 0	NW 1	SW 2
13	105.0	103.5	102.8	103.8	11.7	19.9	13.3	14.6	20.2	7.7	83	40	81	68	2.3	13.9	3.0	6.4	9 ⊙	7 ⊙	8	NNE 1	SE 3	SE 3
14	96.0	88.2	80.2	88.1	11.3	15.7	12.1	12.8	17.4	10.4	95	88	96	93	0.7	2.1	0.5	1.1	10 ●	9	10 ●	E 1	ESE 3	W 4
15	80.2	84.3	89.1	84.5	8.7	8.6	8.3	8.5	12.1	8.0	94	92	90	92	0.6	1.0	1.1	0.9	10 ●	10 ●	10 ●	W 8	WNW 7	WNW 7
16	92.9	96.7	101.7	97.1	8.1	11.9	8.8	9.4	12.0	7.3	89	69	78	79	1.2	4.3	2.4	2.6	10	10	10	W 8	W 8	W 5
17	102.1	100.8	99.2	100.7	8.1	13.9	12.1	11.6	15.8	6.9	72	56	86	71	3.0	7.1	2.0	4.0	4	9	10 ●	SW 6	WSW 5	SW 4
18	100.9	103.1	107.0	103.7	9.4	13.9	9.8	10.7	15.1	8.7	82	51	81	71	2.2	7.8	2.3	4.1	8	8 ●	1	WSW 3	WNW 7	C 0
19	107.6	105.3	100.5	104.5	10.4	17.9	15.9	15.0	19.4	7.0	85	44	60	63	1.9	11.5	7.2	6.9	0	2	5	WSW 1	SSE 5	SSE 6
20	95.7	99.1	101.5	98.8	15.0	13.1	9.5	11.8	16.1	9.5	74	88	96	86	4.3	1.8	0.5	2.2	10 ●	10 ●	10 ●	S 2	W 2	WNW 2
21	103.0	103.2	102.0	102.7	10.4	14.6	11.7	12.1	15.5	9.0	90	51	85	75	1.3	8.1	2.0	3.8	9 ⊙	8 ⊙	10 ●	NW 3	NNW 4	C 0
22	101.5	102.5	102.5	102.2	9.3	13.0	13.4	12.3	15.2	8.5	95	65	72	77	0.6	5.3	4.4	3.4	10 ●	5 ⊙	6	C 0	ESE 3	S 3
23	105.7	104.7	103.3	104.6	12.4	18.3	15.9	15.6	19.7	9.8	81	50	66	66	2.7	10.4	6.1	6.4	6 ⊙	8 ⊙	9	WSW 3	SSW 5	SW 2
24	104.8	106.4	104.9	105.4	12.3	15.5	11.8	12.8	16.1	11.8	88	53	76	72	1.7	8.2	3.3	4.4	10 ●	10	10	NW 1	WNW 4	WNW 3
25	102.6	103.4	102.9	103.0	9.0	10.7	11.3	10.6	12.5	8.4	95	91	83	90	0.7	1.2	2.3	1.4	10 ●	10 ●	9	N 3	N 2	C 0
26	99.8	99.2	99.5	99.5	10.0	13.1	13.6	12.6	15.2	9.9	97	92	98	96	0.3	1.3	0.4	0.7	10 ●	10 ●	10 ●	NNE 4	NE 3	C 0
27	102.7	104.5	104.8	104.0	11.9	14.4	13.8	13.5	16.0	11.5	85	72	88	82	2.0	4.6	2.0	2.9	10	9 ⊙	10 ●	WNW 2	C 0	WNW 1
28	105.2	104.1	101.0	105.4	13.1	18.0	15.5	15.5	19.4	11.6	83	62	90	78	2.6	7.8	1.7	4.0	10	9 ⊙	7	W 1	C 0	NE 1
29	103.5	104.9	104.5	104.3	11.9	17.5	13.8	14.2	19.1	11.4	84	53	71	69	2.1	9.5	4.6	5.4	9	8 ⊙	2	W 3	W 5	W 1
30	105.2	106.2	105.8	105.7	11.2	13.9	11.9	12.2	15.5	11.0	88	69	83	80	1.7	4.9	2.3	3.0	10 ●	10	10	W 1	W 5	C 0
31	105.1	101.7	98.1	101.6	11.9	18.9	16.5	16.0	19.9	10.4	81	45	57	61	2.6	12.0	8.2	7.6	7 ⊙	1 ⊙	7	SW 1	SW 4	NW 3
M	100.5	100.6	100.4	100.5	9.2	13.8	11.2	11.4	15.3	7.6	88	64	82	78	1.5	6.2	2.6	3.4	8.0	7.9	7.2	2.3	3.5	2.0

Czerwiec-Juin

1	100.9	104.9	104.0	103.3	8.9	10.1	9.7	9.6	16.5	8.3	63	65	73	67	4.2	4.4	3.2	3.9	10	10	10	W 7	W 4	W 1
2	104.9	106.4	108.4	106.6	6.3	10.4	8.9	8.6	13.1	6.2	94	74	89	86	0.5	3.3	1.2	1.7	10 ●	8 ⊙	9	C 0	C 0	NW 2
3	110.2	111.1	111.7	111.0	9.1	12.8	9.8	10.4	13.9	7.7	88	50	81	73	1.4	7.4	2.3	3.7	8 ⊙	9	9	NW 1	NE 3	NW 2
4	110.7	109.1	108.8	109.5	8.1	9.8	8.6	8.8	10.3	8.0	94	93	88	92	0.6	0.8	1.4	0.9	10 ●	10 ●	10 ●	NNW 3	N 6	NNW 4
5	106.7	107.9	109.3	108.0	6.8	9.0	9.9	8.9	10.2	6.4	90	88	60	79	1.0	1.4	4.9	2.4	10 ●	10 ●	10	NNW 5	N 7	NNW 6
6	109.5	111.0	112.9	111.1	6.7	12.5	8.5	9.0	13.0	6.5	60	30	57	49	4.0	10.2	4.7	6.3	10	8	10	NNW 6	NNW 8	NE 2
7	114.5	115.5	114.6	114.9	7.5	13.1	12.3	11.3	16.1	5.2	69	33	55	52	3.2	10.1	6.4	6.6	10	8	6	NE 4	ENE 7	N 1
8	115.8	115.3	112.8	114.6	10.7	18.6	15.6	15.1	20.2	7.0	76	39	64	60	3.1	13.0	6.4	7.5	8	7	5	N 1	NW 1	W 2
9	106.9	103.4	101.4	103.9	14.0	21.1	16.5	17.0	21.9	10.7	71	42	69	61	4.6	14.5	5.9	8.3	8	8	3	WSW 3	W 5	NW 2
10	102.5	101.3	99.8	101.2	11.0	17.6	14.8	14.6	18.8	7.1	74	38	59	57	3.4	12.5	6.9	7.6	0	1	1	NNE 3	NE 2	C 0
11	96.6	95.6	95.4	95.9	15.3	18.1	14.6	15.6	20.1	12.3	60	59	68	62	7.0	8.4	5.3	6.9	8 ⊙	9 ⊙	4	S 2	SW 4	W 4
12	98.4	99.3	101.5	99.7	11.5	15.8	10.8	12.2	16.2	9.8	82	57	86	75	2.5	7.8	1.8	4.0	9	9	6	WNW 4	W 6	W 4
13	104.4	105.4	105.3	105.0	12.6	14.4	13.6	13.6	18.6	9.5	65	54	68	62	5.2	7.6	5.0	5.9	1 ⊙	9	7	NW 2	WNW 2	NW 1
14	105.7	104.2	103.4	104.4	14.8	21.3	17.7	17.9	22.7	10.4	63	38	64	55	6.2	15.7	7.2	9.7	9	8 ⊙	2	WNW 2	SSE 4	C 0
15	105.1	107.5	108.1	106.9	18.4	24.9	20.2	20.9	26.1	16.3	68	37	61	55	6.8	19.8	9.3	12.0	3 ⊙	3 ⊙	2	WNW 2	NW 5	N 1
16	108.5	108.0	105.4	107.3	20.9	28.5	25.0	24.8	29.5	17.4	56	34	46	45	10.8	25.6	17.1	17.8	3 ⊙	4 ⊙	2	SW 3	SSE 1	SSE 4
17	106.6	108.2	109.2	108.0	18.7	22.5	16.8	18.7	25.1	16.7	92	60	71	74	1.7	11.0	5.5	6.1	8	6 ⊙	1	NW 2	NW 4	NW 1
18	110.0	109.5	107.7	109.1	15.1	20.5	17.5	17.6	25.1	13.0	64	43	67	58	6.2	13.7	6.6	8.8	8	2 ⊙	1	NNE 3	E 5	C 0
19	106.9	104.9	101.7	104.5	18.6	24.9	21.7	21.7	26.3	12.7	61	34	60	52	8.3	20.8	10.4	13.2	1 ⊙	2 ⊙	3	C 0	E 5	SE 2
20	101.5	104.5	106.1	104.0	18.7	19.5	18.8	19.0	22.2	17.0	90	67	58	72	2.1	7.5	9.2	6.3	8 ⊙	8 ⊙	6	W 3	NW 5	C 0
21	108.1	108.1	108.3	108.2	18.4	23.6	19.9	20.4	24.7	14.9	60	47	64	57	8.5	15.4	8.3	10.7	6 ⊙	9 ⊙	9	C 0	W 5	NW 1
22	111.0	111.0	110.1	110.7	17.7	24.6	21.7	21.4	26.2	15.2	78	46	66	63	4.4	16.8	8.9	10.0	1 ⊙	4 ⊙	1	W 2	SW 4	C 0
23	109.2	107.4	105.9	107.5	21.4	28.2	21.1	23.0	29.5	17.2	63	40	73	59	9.4	22.9	6.6	13.0	0 ⊙	3 ⊙	8	WSW 2	SW 4	NNE 2
24	107.2	106.2	102.7	105.4	15.8	22.7	22.3	20.8	23.8	14.7	95	52	60	69	0.9	13.4	10.7	8.3	9	8 ⊙	9	C 0	WSW 4	SE 3
25	102.2	103.6	106.0	103.9	17.1	20.9	14.9	17.0	22.4	14.9	71	40	58	56	5.6	14.7	7.0	9.1	9 ●	4	2	NW 3	W 9	WNW 5
26	106.0	104.6	101.8	104.1	12.5	17.1	15.4	15.1	19.3	10.1	64	42	62	56	5.2	11.2	6.7	7.7	2	6	5	W 5	WSW 6	C 0
27	98.7	99.4	100.1	99.4	14.7	16.1	12.7	14.0	17.7	12.7	65	51	68	61	5.8	9.1	4.7	6.5	9	7	3	SW 3	W 5	W 3
28	99.1	98.9	96.6	98.2	10.5	12.9	9.6	10.6	14.9	8.2	82	52	86	73	2.3	7.1	1.8	3.7	9	9	10	W 4	WSW 7	WSW 4
29	94.7	95.4	96.8	95.6	9.0	13.2	11.3	11.2	14.7	8.3	93	82	96	90	0.8	2.8	0.5	1.4	10 ●	9 ●	10 ●	WSW 3	WSW 7	W 6
30	96.5	99.1	101.0	98.9	11.2	15.5	12.6	13.0	16.1	10.3	94	58	95	82	0.8	7.4	0.7	3.0	9	9	3	W 4	W 3	WSW 4
31																								
M	105.3	105.6	105.2	105.4	15.4	18.0	15.1	15.4	19.8	11.2	75	52	69	65	4.2	11.2	5.9	7.1	6.9	6.9	5.6	2.8	4.4	2.2

Warszawa-Bielany H_s=98m H_b=104,7m h_w=16m

Maj - Mai 1962

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	2.8	•	$\overset{*}{\bullet}{}^{\circ}a, p \bullet{}^{\circ}p\text{-}n, \smile{}^{\circ}n\text{-}a$
2	7	8.3	•	$\overset{\bullet\bullet}{\bullet}n\text{-}a \triangle{}^{1} \bullet 11^{38}\text{-}12^{06} \overset{*}{\triangle}{}^{2} \triangle{}^{0} \bullet 15^{55}\text{-}16^{10} \bullet{}^{1}\text{-}p; = n\text{-}a$
3	8	3.2	•	$\overset{\bullet\bullet}{\bullet}a \overset{\bullet}{\bullet}{}^{1} p$
4	7	0.8	•	$\bullet{}^{\circ}na \overset{\bullet}{\bullet}{}^{\circ} 15^{00\text{-}15}, 17^{15\text{-}20}$
5	6	0.9	•	$\overset{\bullet}{\bullet} 15^{00\text{-}22}; = n\text{-}a \bullet\bullet a\text{-}p; \triangle{}^{2} n\text{-}a, p\text{-}n$
6	7	•	•	$= n\text{-}a; \triangle{}^{\circ} n\text{-}a$
7	6	0.4	•	$\overset{\bullet\bullet}{\bullet} 12^{19}\text{-}p; = n\text{-}n; \triangle{}^{1} n\text{-}a, p\text{-}n$
8	7	1.9	•	$\bullet{}^{\circ} n\text{-}6^{50} \overset{\bullet}{\bullet}{}^{\circ} a; = n\text{-}a \bullet\bullet a\text{-}p = p\text{-}n; \triangle{}^{1} p\text{-}n$
9	7	0.0	•	$\overset{\bullet}{\bullet}{}^{\circ} n\text{-}a$
10	6	3.2	•	$\overset{\bullet}{\bullet}{}^{2} 12^{12} \bullet{}^{0\text{-}1} 14^{00}\text{-}p; = n\text{-}p; \triangle{}^{\circ} n\text{-}a$
11	7	•	•	$= n\text{-}a; \triangle{}^{\circ} n\text{-}a \triangle{}^{2} p\text{-}n$
12	7	•	•	$= n\text{-}a; \triangle{}^{2} n\text{-}a \triangle{}^{1} p\text{-}n$
13	8	1.1	•	$= n\text{-}a; \triangle{}^{1} n\text{-}a$
14	7	68.5	•	$\bullet{}^{1} n\text{-}a, \overset{\bullet}{\bullet}{}^{2} 15^{27}\text{-}17^{30} \bullet{}^{2} 17^{35}\text{-}n; (R)^{\circ} 15^{37}\text{-}17^{10}$
15	6	40.1	•	$\bullet{}^{1} n\text{-}n$
16	7	3.4	•	$\bullet{}^{\circ} n, a; = n\text{-}a$
17	7	2.9	•	$\overset{\bullet}{\bullet}{}^{1} 16^{25\text{-}30} \overset{\bullet}{\bullet}{}^{\circ} 20^{10\text{-}39}; (R) 19^{48}\text{-}20^{00}; = n\text{-}a$
18	7	0.5	•	$\overset{\bullet}{\bullet}{}^{\circ} 12^{15\text{-}17}, 12^{30\text{-}37}; (R) 12^{05\text{-}15}, \triangle{}^{2} p\text{-}n$
19	7	0.0	•	$= n\text{-}a; \triangle{}^{2} n\text{-}a$
20	6	16.5	•	$\bullet{}^{\circ} n\text{-}a, 11^{55}\text{-}20^{45}$
21	8	8.6	•	$\bullet{}^{\circ} 18^{05}\text{-}np$
22	8	0.1	•	$\bullet{}^{\circ} na\text{-}8^{45}; 18^{35}\text{-}19^{00}; = na$
23	7	0.2	•	$\bullet{}^{\circ} 18^{05\text{-}20}; = na\text{-}a, \triangle{}^{1} na$
24	7	8.2	•	$\bullet{}^{\circ} na\text{-}a, 17^{05}\text{-}19^{10}; \triangle{}^{\circ} np$
25	7	13.0	•	$\bullet{}^{\circ} na\text{-}15^{00}, np$
26	7	6.2	•	$\bullet{}^{\circ} na\text{-}np; = na, np$
27	8	0.6	•	$\bullet{}^{\circ} a\ 21^{30\text{-}45}, np$
28	6	0.2	•	$\overset{\bullet}{\bullet}{}^{1} 23^{20}; (R) 23^{20\text{-}50}; = n\text{-}n; \triangle{}^{\circ} n\text{-}a$
29	7	3.7	•	$= n\text{-}a \bullet\bullet a\text{-}p; \triangle{}^{\circ} n\text{-}a, p\text{-}n$
30	6	2.4	•	$\bullet{}^{\circ} na \bullet{}^{1} 8^{34\text{-}50} \bullet{}^{2} 16^{05\text{-}20}, \bullet{}^{\circ} 20^{55}\text{-}21^{07}; (R) 16^{10}\text{-}17^{00}$
31	6	1.3	•	$\overset{\bullet}{\bullet}{}^{1} np; = n\text{-}a \bullet\bullet a\text{-}p; \triangle n\text{-}a$
Σ	—	199.0	—	UWAGI

Czerwiec - Juin

1	9	1.0	•	$\triangle{}^{\circ} p\text{-}n$
2	8	2.2	•	$\bullet{}^{\circ} na\text{-}a \overset{\bullet}{\bullet}{}^{1} p$
3	8	3.4	•	$\bullet{}^{0\text{-}1} 13^{36\text{-}40} \bullet{}^{\circ} 21^{40}\text{-}n, \triangle{}^{2} n\text{-}a$
4	6	25.8	•	$\bullet{}^{0\text{-}2} n\text{-}n$
5	7	4.4	•	$\bullet{}^{\circ} n\text{-}p$
6	7	0.0	•	$\bullet\ np$
7	8	•	•	$\triangle{}^{\circ} p\text{-}n$
8	8	•	•	
9	8	•	•	$\oplus\ a\text{-}p$
10	8	•	•	$\triangle p\text{-}n$
11	8	0.8	•	$\bullet{}^{\circ} 10^{55}\ 11^{05} \overset{\bullet}{\bullet}{}^{\circ} 16^{20\text{-}40}$
12	8	•	•	$\triangle{}^{\circ} na$
13	8	0.0	•	$\bullet{}^{\circ} 11^{50}\text{-}12^{00}; \triangle{}^{\circ} np$
14	8	•	•	$= na, np; \triangle{}^{\circ} na, np$
15	7	•	•	$= na, \triangle{}^{\circ} na, np$
16	7	4.6	•	$= na \bullet\bullet p; \triangle{}^{1} na\text{-}a$
17	7	•	•	$\bullet{}^{2} (R) na; = n\text{-}a, \triangle{}^{\circ} p\text{-}n$
18	7	•	•	$\triangle{}^{\circ} p\text{-}n$
19	7	2.1	•	$\bullet\bullet n\text{-}a$
20	8	•	•	$\bullet{}^{1} (R) na; = n\text{-}a, p\text{-}n, \triangle{}^{2} p\text{-}n$
21	7	•	•	$\bullet\bullet a\text{-}p$
22	7	•	•	$= n\text{-}a \bullet\bullet p\text{-}n, \triangle n\text{-}a$
23	7	4.9	•	$\bullet{}^{1} 23^{15}\text{-}n; (R) 22^{30}\text{-}n; = n\text{-}a \bullet\bullet a\text{-}p$
24	7	0.0	•	$= n\text{-}a$
25	8	0.0	•	$\bullet{}^{\circ} na, a$
26	8	•	•	$\triangle{}^{\circ} p\text{-}n$
27	7	0.0	•	$\bullet{}^{\circ} 8^{15\text{-}40}$
28	8	1.2	•	$\bullet{}^{\circ} a, p$
29	6	25.4	•	$\bullet{}^{0\text{-}2} n\text{-}n; R\ 13^{40\text{-}45}\ W\text{-}E$
30	8	5.0	•	$\overset{\bullet}{\bullet}{}^{1} p$
31				
Σ	—	80.8	—	UWAGI

Warszawa - Bielany φ = 52°17' λ = 20°58' Lipiec - Juillet 1962

DNI	CIŚNIENIE P+900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	103.0	104.0	103.5	103.5	11.5	15.3	12.6	13.0	17.4	10.4	90	70	74	78	1.4	5.3	3.7	3.5	8	10	10	W 3	W 6	W 2
2	102.0	100.6	98.1	100.2	12.2	15.0	13.2	13.4	17.9	10.1	74	66	73	71	3.7	5.7	4.2	4.5	1 ⊙	9	10	WSW 4	W 4	W 3
3	91.3	89.7	88.6	89.9	10.9	12.3	10.4	11.0	14.9	10.3	95	80	82	86	0.6	2.9	2.2	1.9	10 ●	10 ●	3	SSW 5	W 6	WSW 3
4	88.6	89.8	90.8	89.7	9.4	13.8	11.7	11.6	15.3	8.7	88	54	69	70	1.4	7.4	4.2	4.3	9 ⊙	7 ⊙	7	SW 4	SW 6	SW 2
5	93.9	95.8	97.6	95.8	10.7	15.3	14.1	13.6	16.8	9.5	78	59	70	69	2.9	7.2	4.8	5.0	10	10	8	SSW 1	SW 4	SW 1
6	101.7	102.4	103.4	102.5	12.5	18.6	14.2	14.9	19.6	10.9	78	50	69	66	3.2	10.7	5.0	6.3	8 ⊙	8 ⊙	4	SW 4	SW 6	SSW 1
7	104.4	104.1	104.3	104.3	12.6	18.0	14.6	15.0	19.1	10.5	78	50	70	66	3.2	10.3	5.0	6.2	9	7	9	WSW 3	WSW 3	W 1
8	105.2	105.6	106.5	105.8	11.7	16.5	14.3	14.2	18.8	10.7	90	57	73	73	1.3	8.2	4.5	4.7	9	8	3	W 2	NNW 4	WNW 2
9	108.0	107.5	105.9	107.1	12.9	18.6	15.2	15.5	19.9	9.9	85	52	70	69	2.3	10.3	5.1	5.9	2 ⊙	2 ⊙	0	C 0	N 3	NW 2
10	104.0	101.8	100.4	102.1	11.9	20.7	14.3	15.3	21.6	10.2	91	47	83	74	1.2	13.0	2.7	5.6	8 ⊙	4 ⊙	8	W 3	W 5	W 3
11	99.4	98.4	96.3	98.0	15.4	21.5	19.5	19.0	23.9	12.7	82	53	68	68	3.2	12.0	7.3	7.5	1 ⊙	4 ⊙	9	W 3	W 5	C 0
12	94.9	95.5	95.4	95.3	16.3	18.6	16.5	17.0	21.4	14.7	83	81	81	82	3.1	4.1	3.7	3.6	0 ⊙	9	5	W 1	C 0	W 1
13	94.6	94.5	94.7	94.6	14.5	17.4	13.2	14.6	17.6	13.2	87	70	86	81	2.2	6.1	2.1	3.5	7 ⊙	9	4	W 2	WSW 4	WSW 1
14	94.4	95.2	94.8	94.8	13.6	16.9	14.4	14.8	18.4	13.0	94	66	87	82	0.9	6.4	2.2	3.2	9	5 ⊙	3	W 5	W 3	W 1
15	95.4	94.9	94.6	95.0	12.5	18.2	16.2	15.8	20.8	11.7	94	65	80	80	0.9	7.3	3.6	3.9	10	9 ⊙	3	C 0	C 0	C 0
16	95.5	96.9	98.3	96.9	13.7	18.4	16.0	16.0	21.4	13.5	98	76	88	87	0.4	5.1	2.1	2.5	10 ●	8	2	C 0	ENE 3	C 0
17	101.4	102.2	102.8	102.1	14.2	19.7	17.5	17.2	21.4	11.5	82	58	70	70	2.9	9.6	6.1	6.2	6	4	8	NE 1	NE 4	N 1
18	103.9	102.8	102.0	102.9	14.8	20.7	18.7	18.2	22.1	11.6	83	54	67	68	2.9	11.1	7.1	7.0	3	7	10	N 1	N 3	N 2
19	101.5	102.2	103.9	102.5	16.1	22.3	18.5	18.8	23.9	15.0	80	54	68	67	3.6	12.3	6.8	7.6	10	9	4	NNW 4	N 4	NNW 2
20	106.1	105.9	105.4	105.8	17.3	24.3	19.3	20.0	25.2	13.2	77	40	73	63	4.5	18.2	6.0	9.6	1	3	1	C 0	N 1	C 0
21	106.1	104.6	103.6	104.8	19.4	27.6	23.4	23.4	28.5	16.9	70	36	55	54	6.8	23.7	13.1	14.5	5	4	3	C 0	S 3	S 2
22	104.2	104.4	105.0	104.5	18.9	24.3	20.7	21.2	25.3	18.2	72	74	84	77	6.1	7.9	4.0	6.0	10	9 ●	8	C 0	SSE 1	C 0
23	105.7	106.5	108.5	106.9	18.6	22.4	19.4	20.0	24.4	18.4	87	69	64	73	2.7	8.5	8.2	6.5	9	8	9	SW 3	NW 4	WNW 1
24	110.0	110.4	111.0	110.5	15.5	18.8	15.6	16.4	20.7	13.9	78	56	60	65	3.9	9.5	7.1	6.8	2 ⊙	6 ⊙	1	W 3	W 5	WNW 2
25	112.9	112.0	110.5	111.8	13.7	20.4	16.6	16.8	21.8	10.4	78	44	69	64	3.5	13.5	5.9	7.6	1 ⊙	3 ⊙	2	W 2	W 2	C 0
26	107.8	105.7	102.8	105.4	17.4	28.6	26.0	24.5	30.3	14.2	65	42	57	55	7.0	22.6	14.3	14.6	1 ⊙	3 ⊙	9 ●R	S 2	SSE 4	SSE 1
27	102.3	102.6	101.3	102.1	21.5	26.5	19.5	21.8	27.9	19.5	74	51	71	65	6.7	17.1	6.7	10.2	6 ⊙	10	2	WSW 2	WSW 6	SW 4
28	104.2	104.9	106.1	105.1	14.0	19.5	12.6	14.7	19.7	12.6	76	48	79	68	3.9	11.8	3.1	6.3	7	6 ⊙	2	W 6	W 6	WNW 2
29	107.9	107.6	107.7	107.7	12.3	19.2	14.4	15.1	21.8	9.5	85	45	74	68	2.2	12.2	4.3	6.2	0 ⊙	6 ⊙	4	WNW 1	NW 4	N 1
30	110.1	110.0	109.2	109.8	13.7	19.0	15.0	15.7	21.1	10.3	81	47	64	64	3.0	11.6	6.0	6.9	6 ⊙	8 ⊙	2	C 0	C 0	C 0
31	110.3	109.4	108.0	109.2	16.8	21.5	19.1	19.1	24.1	9.4	53	34	51	46	8.9	16.8	10.9	12.2	2 ⊙	5 ⊙	6	E 2	WSW 2	C 0
M	102.3	102.2	102.0	102.2	14.4	19.7	16.3	16.7	21.4	12.4	81	56	72	70	3.2	10.6	5.5	6.4	5.8	6.8	5.1	2.2	3.6	1.3

Sierpień - Août

1	105.3	104.8	104.6	104.9	15.6	19.1	15.7	16.5	21.2	14.7	72	76	75	74	5.0	5.4	4.4	4.9	9	9	1	SW 1	W 1	WNW 1
2	104.3	104.5	103.9	104.2	15.1	19.8	15.7	16.6	21.9	13.5	82	53	69	68	3.2	10.8	5.5	6.5	2 ⊙	9 ⊙	2	W 3	WSW 5	C 0
3	103.3	102.8	103.7	103.3	16.5	23.4	18.2	19.1	24.6	13.5	75	42	71	63	4.8	16.7	6.0	9.2	9	9 ⊙	4	C 0	NNW 2	C 0
4	104.2	103.6	102.3	103.4	17.5	26.6	19.5	20.8	27.6	14.5	88	43	90	74	2.4	19.7	2.2	8.1	0 ⊙	4 ⊙	3	C 0	S 3	C 0
5	103.3	101.5	98.1	101.0	18.3	26.3	18.1	20.2	27.1	16.7	87	50	94	77	2.6	16.9	1.3	6.9	9	5 ⊙	10 ●	C 0	NE 1	C 0
6	98.6	100.6	100.8	100.0	17.0	20.5	19.2	19.0	22.2	17.0	91	68	79	79	1.8	7.7	4.6	4.7	10	8 ●	7	NW 3	W 2	SSW 1
7	98.4	93.9	93.5	95.3	19.0	28.9	19.3	21.6	30.7	15.8	82	46	95	74	4.0	21.7	1.1	8.9	8	8	10 ●	SSE 2	SE 9	W 7
8	101.9	103.7	106.5	104.0	15.5	21.4	17.1	17.8	22.9	15.2	77	46	71	65	4.1	13.7	5.6	7.8	9	2	2	W 5	W 5	W 1
9	110.4	111.8	112.2	111.5	15.0	21.3	15.5	16.8	21.4	13.5	65	45	68	59	5.9	14.0	5.7	9.2	9	2	4	W 2	WNW 4	C 0
10	112.1	109.7	105.5	109.1	16.3	21.8	20.3	19.7	23.6	10.7	64	38	52	51	6.7	16.1	11.5	11.4	4	5	8	SE 2	SE 1	SE 4
11	104.0	104.3	104.7	104.3	16.7	21.7	19.1	19.2	23.4	16.1	70	55	64	63	5.7	11.8	7.9	8.5	10	6	9	WSW 3	WSW 4	C 0
12	106.9	106.3	105.3	106.2	18.7	26.8	22.8	22.8	28.3	15.8	68	43	64	58	6.9	20.1	9.8	12.3	0	1	3	W 1	S 2	C 0
13	105.3	105.2	105.6	105.4	20.7	29.2	22.9	23.9	30.6	17.7	71	43	70	61	7.2	23.1	8.4	12.9	2 ⊙	2 ⊙	1	SW 1	NW 2	NW 2
14	107.9	107.6	106.3	107.3	13.4	16.5	16.9	15.9	22.9	12.1	81	74	71	75	3.0	5.0	5.5	4.5	10	10	10	C 0	C 0	C 0
15	104.3	101.5	97.1	101.0	14.5	19.3	19.7	18.3	21.6	14.1	79	77	93	83	3.4	5.2	1.5	3.4	10	10	7	NE 2	ESE 4	SE 2
16	97.8	99.7	100.8	99.4	18.3	21.3	17.9	18.8	23.1	17.4	93	74	89	85	1.4	6.5	2.2	3.4	9 ⊙	10 ⊙	9	WSW 2	SW 1	S 2
17	102.4	102.1	100.5	101.7	16.5	25.6	18.1	19.6	26.1	14.7	86	44	77	69	2.8	18.4	4.9	8.7	3 ⊙	6 ⊙	10	C 0	S 2	NW 3
18	97.8	98.8	101.4	99.3	16.7	19.9	14.5	16.4	21.1	14.5	96	75	84	85	0.8	5.7	2.7	3.1	9 ⊙	10	7	NW 1	W 5	W 3
19	101.2	101.2	101.3	101.2	12.5	13.3	13.1	13.0	15.6	12.0	87	79	91	86	1.9	3.2	1.4	2.2	9	10	9	W 3	NW 1	W 3
20	99.3	100.9	102.5	100.9	14.3	18.7	15.5	16.0	20.1	13.0	90	77	90	86	1.6	5.0	1.7	2.8	10	9 ⊙	0	NW 3	NW 5	NW 3
21	103.2	103.1	102.6	103.0	14.5	17.9	14.1	15.2	19.2	13.0	92	69	93	85	1.3	6.3	1.1	2.9	9	9	0	NW 1	NW 1	C 0
22	102.2	103.4	104.4	103.3	13.9	16.1	14.9	15.0	17.4	11.7	94	94	88	92	0.9	1.2	2.0	1.4	3 ⊙	10	9	C 0	SW 2	C 0
23	101.9	104.7	105.5	104.0	15.7	16.7	13.9	15.0	17.7	13.6	76	61	71	69	4.3	7.5	4.6	5.5	9	9	1	SW 4	WSW 5	SW 2
24	102.7	98.4	96.6	99.2	13.2	15.1	16.5	15.3	17.6	12.0	82	89	93	88	2.8	1.9	1.4	2.0	10	10	10	SW 2	S 5	SW 4
25	99.9	100.9	103.0	101.3	13.9	17.8	14.7	15.3	18.4	13.0	87	65	78	77	2.2	7.3	3.6	4.4	9	10	2	WSW 3	WSW 5	SW 3
26	105.8	108.1	108.9	107.6	12.3	16.5	13.8	14.1	18.4	11.0	83	53	67	68	2.4	8.9	5.2	5.5	3 ⊙	8	0	WSW 5	W 3	SW 2
27	105.5	100.4	99.3	101.7	13.1	23.1	19.4	18.8	24.3	11.0	65	46	64	58	5.3	15.3	8.2	9.6	1 ⊙	2 ⊙	5	SSE 5	SSW 4	WSW 2
28	104.5	105.8	106.4	105.6	12.6	15.2	12.0	13.0	19.5	11.5	78	61	91	77	3.2	6.8	1.2	3.7	5 ⊙	8 ⊙	8	W 6	W 8	WSW 2
29	105.9	104.6	102.8	104.4	11.4	19.2	13.8	14.6	20.2	9.4	83	54	97	78	2.3	10.2	0.6	4.4	10	9	9	WSW 3	W 2	WNW 2
30	105.7	107.2	107.1	106.7	11.6	14.5	11.7	12.4	16.1	10.6	94	62	83	80	0.8	6.3	2.3	3.1	10	8	2	W 4	WNW 8	WSW 3
31	102.1	99.6	100.7	100.8	10.7	12.6	10.7	11.2	16.1	10.1	87	87	89	88	1.7	1.9	1.5	1.7	10	10 ●	5	SSW 3	SW 6	W 4
M	103.5	103.2	103.0	103.2	15.2	20.2	16.6	17.2	22.0	13.5	81	61	80	74	3.3	10.3	4.1	5.9	7.1	7.4	5.4	2.3	3.5	1.8

Warszawa-Bielany H_s=98m H_b=104,7m h_w=16m Lipiec - Juillet 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	•	•	
2	9	2.5	•	∞na; ⌓°na
3	7	2.9	•	●°na-a, 13^{10}-14^{00}
4	9	•	•	●°na
5	8	•	•	⌓°np
6	7	0.0	•	●°14^{00-05}; R 18^{50}; =na
7	8	•	•	=na; ⌓°na, np
8	9	•	•	⌓°na
9	8	•	•	=n-a; ⌓°n-a
10	7	15.2	•	●(R)16^{21-24} NW-SE ▲°16^{05-06} ●°17^{01} ●²(R)17^{20}-19^{05}; ∩ 18^{05}; =n-a ⌓°n-a
11	8	0.0	•	●°20^{50} (R)21^{30}
12	7	6.8	•	⚲²$12^{45}$ ▲°12^{46-47} ⚲²$13^{43}$; (R)12^{35}
13	7	6.8	•	⚲°8^{10} ●°10^{10}; 11^{59} ●²$17^{52}$ 18^{02} ●°⁻¹$19^{52}$-20^{20}; (R)na-7^{30}; 17^{30}-p
14	7	•	•	●°⁻¹na; =p-n; ⌓°p-n
15	8	7.3	•	●°p; ≡na=na-a; ⌓°p-n
16	7	0.4	•	●°na, a; =p-n; ⌓°p-n
17	8	•	•	⌓°n-a
18	8	•	•	⌓°n-a
19	7	0.0	•	●°p
20	8	•	•	⌓° n-a, p
21	7	•	•	∞n-a
22	7	0.0	•	●°a, p; ⌓° p-n
23	7	0.0	•	●°7^{50-55}; =na ∞ a
24	8	0.0	•	●°13^{10-12}; =na
25	9	•	•	⌓°np
26	7	0.0	•	●°21^{35-38}; R 21^{30-40}; =na ∞ a; ⌓°na
27	6	•	•	=na ∞ a
28	8	2.9	•	●°14^{45}-16^{15} ●²$19^{15-30}$
29	9	0.6	•	●°19^{00-17}; ⌓* na-a
30	8	•	•	⌓¹ n-a, p-n
31	7	0.0	•	∞n-a; ⌓² n-a
Σ	—	45.4	—	UWAGI.

Sierpień - Août

1	6	0.4	•	●°na ●¹$8^{37}$-9^{15}; 12^{40-48}
2	7	•	•	=n-a; ⌓°p-n
3	7	•	•	=n-a ∞ a-p; ⌓°n, p-n
4	6	8.1	•	●²$18^{04-45}$; 19^{03-48}; (R)17^{50}; =n-a ∞ a-p; ⌓¹n-a
5	6	13.6	•	●²$19^{30}$ ●¹⁻²$21^{00-20}$ ●²$21^{30-45}$; (R)19^{10}-n; =n-a ∞ a-p
6	7	0.0	•	⚲°a; =n-a; ⌓¹p
7	8	2.0	•	⚲°n-n; R°19^{45}-20^{15}; =n-a; ⌓¹n-a
8	8	•	•	⌓°p-np
9	8	•	•	⌓°p-n
10	5	•	•	∞n-a; ⌓¹n-a
11	8	•	•	
12	8	•	•	
13	7	1.9	•	=n-a; ⌓¹n-a
14	7	•	•	●²(R)na
15	7	11.7	•	⚲¹$15^{45}$
16	6	5.2	•	●²(R)na ●²$18^{07-12}$ 19^{25} (R)18^{30}-p; =n-p
17	8	10.3	•	●°21^{59} ●¹$22^{17-53}$; (R)22^{03}; =na
18	7	•	•	●²(R)na; =n-p
19	8	4.2	•	⚲°12^{15}; 13^{20}...16^{50}; (R)12^{10} NW-SE; =n-a
20	7	0.1	•	⚲°a; ⌓°p-n
21	7	•	•	=n-a; ⌓² n-a, p-n
22	5	0.9	•	⚲°a ●¹⁻⁰$10^{02}$ p; =n-n; ⌓² n-a; p-n
23	8	•	•	⌓²n-n
24	6	7.0	•	●°a...n; =n-p; ⌓°n-a
25	7	0.0	•	●°na, a; ⌓°p-n
26	8	•	•	⌓°na, n-n
27	7	2.4	•	●°np; ⌓°na
28	8	0.2	•	⚲°p
29	7	2.0	•	●°20^{45}-21^{30}; =na; ⌓°na
30	8	1.2	•	●°10^{50-55}; =na; ⌓¹ na-a
31	7	4.3	•	●°na, 9^{05-10}; 13^{05-40}; 16^{00-10}; 17^{15-30}; 18^{45}-20^{25}
Σ	—	75.5	—	UWAGI.

Warszawa - Bielany φ = 52°17' λ = 20°58' Wrzesień - Septembre 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D.v I	II	III
1	103.9	106.5	108.8	106.4	11.1	15.2	10.8	12.0	16.0	9.8	88	63	87	79	1.6	6.3	1.7	3.2	6 ⊙	4 ⊙	6	NW 4	WNW 5	W 2
2	111.6	111.5	109.9	111.0	9.2	17.7	14.4	13.9	19.1	7.2	88	52	67	69	1.4	9.7	5.5	5.5	2 ⊙	8 ⊙	0	WSW 3	WSW 6	W 1
3	108.3	108.1	106.7	107.7	11.5	21.6	15.4	16.0	22.5	9.8	81	46	76	68	2.7	14.0	4.3	7.0	2 ⊙	4 ⊙	0	WSW 3	WSW 2	C 0
4	103.8	101.2	97.6	100.9	14.0	26.0	21.1	20.6	27.6	10.2	75	44	56	59	4.1	18.9	10.5	11.2	0 ⊙	0	0	SSW 2	SSE 3	SSE 3
5	92.9	93.4	94.8	93.7	17.8	22.3	15.6	17.8	23.6	15.4	66	62	89	72	6.9	10.3	1.9	6.4	5 ⊙	9	8	SSE 3	WSW 5	SW 3
6	95.0	95.8	93.0	94.6	13.7	20.4	16.6	16.8	21.6	12.7	95	52	70	72	0.7	11.6	5.7	6.0	9 ⊙	4 ⊙	9	SW 3	WSW 5	SW 1
7	87.1	86.7	89.9	87.9	17.7	15.3	14.4	15.4	19.6	13.2	83	89	86	86	3.4	1.9	2.4	2.6	9	10 ●	9	SW 4	WSW 3	WSW 4
8	97.2	98.2	99.5	98.3	10.7	15.1	12.2	12.6	16.0	9.4	82	50	81	71	2.3	8.6	2.6	4.5	2 ⊙	9	8	WSW 5	W 6	SW 4
9	103.9	107.6	110.7	107.4	10.5	14.3	11.5	12.0	15.9	10.0	88	68	85	80	1.5	5.3	2.0	2.9	10	9 ●	8	W 3	WNW 5	WSW 2
10	110.2	108.4	104.9	107.8	10.3	19.7	15.3	15.2	20.9	8.7	80	40	66	62	2.5	13.6	6.0	7.4	8 ⊙	1 ⊙	0	WSW 2	SSW 4	S 3
11	101.9	100.7	103.6	102.1	12.7	18.1	14.3	14.8	18.6	11.5	75	74	94	81	3.7	5.5	0.9	3.4	8 ⊙	10	3	S 3	C 0	SW 3
12	105.0	99.2	91.1	98.4	11.6	20.9	20.7	18.5	23.5	10.5	100	61	71	77	0.0	9.6	7.2	5.6	8	10	1	SW 1	SSW 3	W 3
13	100.3	103.5	106.0	103.3	10.6	15.0	10.7	11.8	20.7	10.5	81	51	71	68	2.4	8.2	3.7	4.8	2 ⊙	5 ⊙	2	W 3	W 6	W 3
14	109.0	110.1	111.1	110.1	8.2	13.4	9.7	10.2	14.4	7.6	92	57	82	77	0.9	6.6	2.2	3.2	9	9	3	W 4	W 5	WSW 2
15	111.3	109.5	105.2	108.7	6.4	14.3	12.3	11.3	15.6	5.5	91	54	71	72	0.9	7.4	4.2	4.2	9 ⊙	9 ⊙	9	W 2	SE 2	SE 2
16	101.0	99.2	97.9	99.4	10.4	22.4	18.2	17.3	23.4	8.5	76	45	71	64	3.0	14.8	6.0	7.9	2 ⊙	7 ⊙	10	SSW 1	S 3	S 1
17	97.8	99.4	97.8	98.3	14.8	16.5	13.1	14.4	18.4	13.1	91	80	95	89	1.5	3.9	0.7	2.0	10	10	10 ●	NW 2	NW 2	NNE 2
18	97.7	96.9	90.7	95.1	9.5	13.2	11.0	11.2	13.4	9.3	91	77	96	88	1.1	3.5	0.5	1.7	10	10	10 ●	WNW 2	NNE 5	NNW 2
19	96.3	100.6	103.2	100.0	7.9	9.4	8.9	8.8	11.0	7.4	91	80	89	87	0.9	2.4	1.2	1.5	10	10	7	WSW 5	WSW 4	SSW 2
20	105.0	105.2	105.0	105.1	6.3	12.8	8.8	9.2	14.4	5.5	94	67	88	83	0.5	4.9	1.4	2.3	8	7	5	SW 2	W 2	SW 2
21	103.9	103.8	103.4	103.7	8.3	12.2	9.3	9.8	13.1	7.9	89	73	95	86	1.3	3.8	0.6	1.9	9	9	10 ●	W 5	WSW 5	W 3
22	103.2	104.6	106.5	104.8	7.9	12.5	9.4	9.8	12.8	7.6	93	69	93	85	0.7	4.5	0.8	2.0	9	9	10 ●	W 2	NNW 5	WSW 2
23	105.2	103.6	103.6	104.1	7.3	10.7	8.8	8.9	10.9	7.0	93	84	96	91	0.7	2.1	0.4	1.1	9	10	10	W 2	W 2	W 1
24	107.6	110.7	114.5	110.9	8.6	11.9	9.3	9.8	12.7	8.5	96	72	88	85	0.5	3.9	1.4	1.9	10	9	6	NW 2	NW 3	W 1
25	117.8	119.0	118.5	118.4	6.3	15.4	8.8	9.8	15.5	4.5	98	58	93	83	0.1	7.4	0.8	2.8	10 ≡	4 ⊙	2	C 0	ESE 4	ESE 2
26	116.8	115.5	113.0	115.1	6.2	15.1	8.5	9.6	15.7	5.1	91	51	86	76	0.9	8.5	1.5	3.6	0 ⊙	6 ⊙	0	E 2	E 6	E 2
27	109.8	107.7	106.1	107.9	4.7	11.3	10.4	9.2	11.6	3.7	97	80	92	90	0.2	2.6	1.0	1.3	0 ⊙	10	10	ENE 2	ENE 4	E 1
28	104.1	104.1	103.4	103.9	10.6	12.4	11.3	11.4	12.5	10.4	99	89	99	96	0.2	1.6	0.2	0.7	10	10	10 ●	E 2	E 3	ENE 2
29	102.2	102.8	104.7	103.2	11.4	13.8	10.6	11.6	14.7	10.6	98	88	100	95	0.4	2.0	0.0	0.8	10 ≡	10	0 ≡	C 0	ESE 2	C 0
30	107.0	108.6	109.9	108.5	7.6	16.2	11.7	11.8	18.4	7.4	99	76	96	90	0.1	4.4	0.5	1.7	10 ≡	0 ⊙	0	C 0	S 1	C 0
31																								
M	103.9	104.1	103.7	103.9	10.1	15.8	12.4	12.7	17.1	9.0	89	65	84	79	1.6	6.9	2.6	3.7	6.9	7.4	5.5	2.5	3.7	2.0

Październik - Octobre

1	112.3	113.7	114.6	113.5	7.6	12.3	12.4	11.2	15.1	7.2	100	95	99	98	0.0	0.7	0.2	0.3	10 ≡	9	10 ≡	C 0	SE 1	SE 1
2	115.7	116.6	115.8	116.0	9.7	19.1	12.9	13.6	20.1	9.5	100	63	87	83	0.0	8.1	1.9	3.3	4	2 ⊙	0	C 0	SE 4	SE 2
3	115.7	115.5	114.7	115.3	10.1	18.4	12.8	13.5	19.1	9.0	97	61	88	82	0.4	8.4	1.8	3.5	2 ⊙	1 ⊙	0	SE 1	SE 7	SE 2
4	114.1	113.5	112.6	113.4	8.9	17.9	13.2	13.3	18.9	8.0	86	62	91	80	1.5	7.8	1.4	3.6	6 ⊙	6 ⊙	10	C 0	SE 5	SE 1
5	111.5	112.1	111.8	111.8	9.5	17.7	13.1	13.4	17.9	9.5	100	70	94	88	0.0	6.0	0.9	2.3	9 ≡ ⊙	10	8	C 0	SSE 2	C 0
6	112.1	114.6	116.8	114.5	10.3	15.6	11.9	12.4	17.1	10.0	100	79	95	91	0.0	3.7	0.7	1.5	9 ≡ ⊙	9 ⊙	0	C 0	E 1	C 0
7	119.8	121.5	122.9	121.4	9.7	14.5	10.9	11.5	16.0	9.7	100	80	97	92	0.0	3.2	0.3	1.2	10 ● ≡	9 ⊙	0	NNE 2	NE 3	NE 2
8	124.2	124.8	123.4	124.1	6.1	14.5	9.2	9.8	15.5	6.0	100	72	96	89	0.0	4.6	0.4	1.7	10 ≡	6	6	C 0	NNE 1	C 0
9	122.1	121.8	119.5	121.1	3.3	9.5	9.5	8.0	10.3	3.1	100	96	86	94	0.0	0.5	1.7	0.7	2 ≡	10	10	C 0	C 0	ENE 2
10	117.9	116.4	114.0	116.1	6.9	9.6	5.9	7.1	11.4	5.7	85	74	94	84	1.4	3.2	0.6	1.7	10 ≡	6	0	SW 1	C 0	C 0
11	111.1	108.6	104.6	108.1	2.2	14.2	7.7	8.0	14.6	1.5	100	60	97	86	0.0	6.4	0.3	2.2	0 ≡	2	0	C 0	ESE 2	C 0
12	104.5	106.8	109.3	106.9	5.7	10.7	8.1	8.2	11.6	2.8	100	70	93	88	0.0	3.9	0.8	1.6	10 ● ≡	9	6	NW 1	NW 2	C 0
13	110.8	111.1	107.0	109.6	6.5	11.5	6.7	7.8	12.7	5.7	97	70	82	83	0.3	4.1	1.7	2.0	7	2	3	C 0	SSE 2	C 0
14	99.6	99.8	103.3	100.9	4.5	7.5	8.4	7.2	9.6	4.1	97	93	90	93	0.3	0.8	1.0	0.7	6	10	9	C 0	W 1	W 2
15	109.0	112.4	114.8	112.1	4.3	8.6	3.9	5.2	9.7	3.9	88	49	70	69	1.0	5.8	2.4	3.1	2 ⊙	8	0	NNE 1	NNW 3	NW 2
16	114.4	112.8	110.6	112.6	-1.4	9.6	5.5	4.8	10.8	-1.4	96	46	62	68	0.2	6.5	3.4	3.4	6 ⊙	2 ⊙	1	C 0	W 4	SW 3
17	110.0	111.7	110.5	110.7	5.5	9.3	9.4	8.4	10.1	3.2	81	87	89	86	1.7	1.6	1.3	1.5	10	10	10	WSW 3	WSW 5	WSW 4
18	107.4	105.6	99.5	104.2	10.4	10.5	12.1	11.3	12.1	9.0	91	99	80	90	1.1	0.2	2.8	1.4	10	10 ●	8	WSW 5	W 5	WSW 6
19	96.3	99.2	99.4	98.3	10.6	13.5	9.5	10.8	14.2	9.5	86	60	78	75	1.8	6.2	2.7	3.6	9	8 ⊙	6	WNW 5	NW 6	W 4
20	102.1	107.1	113.4	107.5	6.5	9.8	4.3	6.2	10.6	4.2	96	59	74	76	0.5	4.9	2.2	2.5	2 ⊙	8	2	WNW 4	N 6	WNW 4
21	117.6	118.1	116.7	117.5	-0.4	10.8	6.4	5.8	12.1	-0.5	92	55	73	73	0.5	5.9	2.6	3.0	2 ⊙	1 ⊙	3	W 3	W 5	WSW 4
22	116.7	117.2	116.0	116.6	6.5	8.2	7.7	7.5	8.5	6.2	96	89	86	90	0.5	1.2	1.5	1.1	10	10	10	W 3	W 2	W 2
23	113.5	113.4	112.5	113.1	6.9	7.5	7.1	7.2	8.1	6.9	85	77	81	81	1.4	2.4	1.9	1.9	10	10	10	WNW 1	W 3	WSW 2
24	109.2	108.2	109.6	109.0	3.0	12.3	3.9	5.8	12.9	2.4	96	59	95	83	0.3	5.9	0.4	2.2	3 ⊙	0 ⊙	0	S 2	SW 3	NW 1
25	110.4	109.4	109.2	109.7	3.7	7.4	4.7	5.1	8.4	2.2	98	83	90	90	0.2	1.8	0.8	0.9	10 ≡	9	0	C 0	S 1	SW 1
26	107.0	105.0	103.7	105.2	1.5	11.8	7.7	7.2	12.5	1.3	94	62	79	78	0.4	5.2	2.2	2.6	0 ⊙	0 ⊙	0	SE 3	W 4	S 3
27	99.8	101.0	106.2	102.3	5.5	10.7	6.5	7.3	12.1	5.1	80	68	96	81	1.8	4.2	0.5	2.2	0 ⊙	10 ●	10	S 3	W 3	C 0
28	102.5	99.4	98.9	100.3	6.1	9.8	7.5	7.7	10.1	5.2	97	86	94	92	0.3	1.7	0.6	0.9	10 ●	10	10 ●	SE 2	S 3	SW 1
29	99.5	100.8	104.2	101.5	4.0	5.1	5.5	5.0	7.5	4.0	95	92	92	93	0.4	0.7	0.7	0.6	10 ●	10	10	W 1	WNW 2	NW 1
30	105.8	105.8	103.2	104.9	5.3	8.7	5.7	6.4	9.4	5.2	94	65	89	83	0.6	3.9	1.0	1.8	10	3	10	C 0	SW 2	C 0
31	99.5	98.9	99.0	99.1	6.0	8.2	8.1	7.6	8.8	4.8	92	81	91	88	0.8	2.1	0.9	1.3	10	10 ●	4	SE 3	SE 3	SE 2
M	110.1	110.4	110.2	110.2	6.0	11.4	8.3	8.3	12.5	5.3	94	73	87	85	0.6	3.9	1.3	1.9	6.7	6.8	5.0	1.4	2.9	1.7

Warszawa-Bielany $H_s=98m$ $H_b=104,7m$ $h_w=16m$ Wrzesień - Septembre 1962

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	9	0.7	•	$\bullet^{\circ}11^{45-50}, 12^{15-20}, 16^{25-35}; \triangle^{2} na-a \triangle^{1} np$
2	9	•	•	$\triangle^{2} na \triangle^{1-0} a \triangle^{0} np$
3	7	•	•	$= na; \triangle^{1} na \triangle^{0} np$
4	7	•	•	$= na = a; \triangle^{2} na$
5	6	1.5	•	$\bullet^{\circ}16^{15-19^{45}}; = na-a; \triangle^{0} na$
6	8	0.6	•	$\bullet^{0} np; \triangle^{1} na$
7	7	8.9	•	$\bullet^{0} na, 9^{45-15} \bullet^{0-2} 9^{45-14^{00}} \bullet^{1} 17^{10-40} \bullet^{0} 21^{40} - n; \mathbb{R} 17^{10-30}; \triangle 17^{10-40}; \triangle^{0} na$
8	9	•	•	$\triangle^{0} np$
9	9	0.0	•	$\bullet^{0} a \ldots p$
10	8	•	•	$= n-a; \triangle^{1} n-a$
11	6	3.2	•	$\bullet^{0} 13^{05} \bullet^{1} 14^{05} \bullet^{1-2} 14^{30} - 15^{40} \bullet^{1} 16^{25} \bullet^{2} 18^{05}; = n-p; \triangle^{1} n-a$
12	6	1.2	•	$\bullet^{1} 19^{55}; (\mathbb{R}) 19^{10} \ldots 21^{30} W-E; = n-p; \triangle^{2} n-a$
13	8	•	•	$\bullet^{1} na$
14	8	•	•	$\triangle^{0} p-n$
15	7	•	•	$= n-a; \triangle^{2} n-a$
16	7	•	•	$= n-a; \triangle^{1} n-a$
17	6	12.6	•	$\bullet p-np; = n-a; \triangle n-a$
18	8	14.0	•	$\bullet^{1} na \bullet^{1-0} p-n$
19	8	•	•	$\bullet^{0-1} na$
20	6	0.1	•	$\bullet^{0} p; = n-a; \triangle^{1} n-a$
21	8	4.6	•	$\bullet^{0} 7^{30-40} \bullet 15^{55} - 16^{05} \bullet^{0} p-n$
22	8	2.7	•	$\bullet^{0} na, a, p-n$
23	7	2.5	•	$\bullet^{0} p \bullet^{0} np; = p-n$
24	8	0.0	•	$\bullet^{0} 11^{40} - 12^{00}, 14^{15-20}; = na; \triangle^{0} np$
25	8	•	•	$\equiv^{1} na - 8^{30}; \triangle^{2} na-a \triangle^{1} np$
26	7	•	•	$= na; \triangle^{2} na \triangle^{0} np$
27	7	•	•	$= na; \triangle^{2} na$
28	5	6.5	•	$\bullet^{0} 17^{40} - np; = na-a; \triangle^{0} na$
29	6	•	•	$\bullet^{0} na; \equiv^{0} na - 8^{40} = -p \equiv 19^{20} - np; \triangle^{2} np$
30	4	0.2	•	$\equiv^{1} na - 9^{20} = a-np; \triangle^{2} na \triangle^{0} a \triangle^{1} np$
31				
Σ	—	59.3	—	UWAGI.

Październik - Octobre

1	4	0.0	•	$\equiv^{2} n-a = a-p \equiv p-n; \triangle^{2-1} n-n$
2	7	0.0	•	$= n-a; \triangle^{1} n-a, p-n$
3	8	0.0	•	$= n-a; \triangle^{2} n-a \triangle^{1} np$
4	7	•	•	$= n-a = a-p; \triangle^{2} n-a \triangle^{1} p-n$
5	6	•	•	$\equiv^{2} n-a = a-n; \triangle^{2} n-a \triangle^{1} p-n$
6	6	0.1	•	$\equiv n-a = a-p; \triangle^{1} n-a, p-n$
7	6	0.0	•	$\bullet na; \equiv^{2-0} n-a = a-n; \triangle^{2} n-a \triangle^{1} p-n$
8	7	•	•	$\equiv^{2-0} n-a = p-n; \triangle^{2} n-a \triangle^{1} p-n$
9	4	•	•	$\equiv^{0-2} n-a = a-p; \triangle^{2} n-a \triangle^{0} p-n$
10	5	•	•	$= a-p \equiv p-n; \triangle^{2} p-n$
11	5	0.3	•	$\equiv^{0} n-a = a-p = p-n; \sqcup^{0} na \triangle^{2} p-n$
12	7	0.0	•	$\bullet^{2} n-a; \equiv^{2} n-a = a, p-n$
13	7	•	•	$= n-a, p-n; \triangle^{2} n-a, p-n$
14	5	0.7	•	$= a-p; \triangle^{2} a-p$
15	9	•	•	$\bullet^{0} na$
16	9	•	•	$= na-a; \sqcup^{0} na-a$
17	6	0.0	•	$\bullet^{0} p; = na-n$
18	4	0.3	•	$\bullet^{0} 7^{20} - p; = na-p$
19	9	0.5	•	$\bullet^{0} np; = na$
20	9	•	•	
21	9	•	•	$\sqcup^{0} na-a$
22	6	•	•	$= a-p$
23	6	•	•	$= a-p$
24	5	•	•	$= n-a = a-n \equiv^{2} np; \triangle^{0} n-a, p-n$
25	5	•	•	$\equiv^{2-1} na-a = a-p; \triangle^{1} n-a, p-n$
26	6	•	•	$= n-n; \sqcup^{1} n-a \triangle^{0} p-n$
27	6	3.4	•	$\bullet^{0} 12^{20} - p; = n-p; \triangle^{1} n-a$
28	5	2.8	•	$\bullet^{0} n-a, p-n; = n-a$
29	6	0.3	•	$\bullet^{0} n-a; = a-n$
30	6	•	•	$= n-n$
31	6	0.3	•	$\bullet^{0} a-p; = n-n$
Σ	—	8.7	—	UWAGI.

Warszawa - Bielany φ = 52°17' λ = 20°58' Listopad - Novembre 1962

DNI	CIŚNIENIE P 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	96.1	95.2	95.2	95.5	8.7	14.3	15.6	12.6	14.5	7.4	99	80	77	85	0.1	3.2	3.5	2.3	10 ●	9	7	SE 3	SSE 2	SW 3
2	98.4	101.2	104.3	101.3	7.9	9.9	8.7	8.8	13.6	6.6	100	99	97	99	0.0	0.2	0.3	0.2	10 ≡	10	10 ● ≡	C 0	C 0	C 0
3	106.0	106.1	105.8	106.0	7.1	10.5	10.4	9.6	11.5	7.0	91	80	96	89	0.9	2.6	0.5	1.3	10	10	10 ●	C 0	E 1	E 1
4	106.3	107.3	107.0	106.9	11.5	10.2	11.6	11.2	11.9	10.0	95	91	87	91	0.7	1.1	1.8	1.2	10 ○	10	10	SE 5	S 2	SSE 5
5	105.7	105.5	105.0	105.4	9.6	10.6	8.5	9.3	12.1	8.5	88	85	57	77	1.5	2.0	4.7	2.7	10	8	0	ESE 7	ESE 7	ESE 6
6	103.9	103.4	106.1	104.5	3.0	10.5	7.5	7.1	10.6	2.9	66	41	44	50	2.6	7.5	5.9	5.3	2	2 ⊙	2	ESE 8	E 8	ESE 8
7	108.3	110.0	110.9	109.7	3.6	8.6	6.7	6.4	9.0	3.6	73	52	53	59	2.1	5.3	4.6	4.0	6	9	2	ESE 4	ESE 7	ESE 5
8	109.1	106.7	106.6	107.5	3.6	10.2	7.2	7.0	11.4	3.1	76	59	65	67	1.9	5.1	3.6	3.5	2	0 ⊙	0	ESE 3	E 3	ESE 3
9	105.4	106.0	106.5	106.0	1.1	2.8	4.6	3.3	7.3	1.0	92	91	82	88	0.5	0.7	1.5	0.9	10	10	10	ENE 3	E 3	E 3
10	106.5	107.8	109.4	107.9	3.6	3.1	0.4	1.9	5.9	0.4	78	74	98	83	1.7	1.9	0.1	1.2	10	10	10 ✳	ENE 6	ENE 8	NE 6
11	110.2	110.6	110.5	110.4	0.4	0.7	2.2	1.4	2.2	0.1	98	100	87	95	0.1	0.0	1.0	0.4	10 ✳	10 ✳	10 ●	ENE 5	E 5	E 6
12	110.0	108.1	107.4	108.5	2.0	1.3	2.2	1.9	2.6	0.9	87	89	95	90	0.9	0.8	0.4	0.7	10	10	10 ●	E 8	E 8	ESE 4
13	108.3	109.8	109.2	109.1	3.8	4.8	4.5	4.4	5.4	2.2	97	95	98	97	0.3	0.4	0.1	0.3	10	10	10	C 0	SE 1	E 2
14	107.7	106.8	106.1	106.9	3.7	3.5	4.5	4.0	5.4	2.5	100	98	98	99	0.0	0.1	0.1	0.1	10 ≡	10	10 ●	E 1	E 1	E 1
15	102.2	98.8	92.3	97.8	5.1	7.0	6.7	6.4	7.4	4.5	98	97	99	98	0.2	0.3	0.1	0.2	10 ≡	10 ● ≡	10 ●	C 0	S 2	SSE 2
16	94.8	96.3	98.5	96.5	2.5	3.1	1.3	2.0	7.3	1.2	84	88	91	88	1.2	0.9	0.6	0.9	10	10	9	W 3	W 3	W 3
17	102.0	103.3	103.7	103.0	-1.1	0.2	-0.5	-0.5	1.6	-1.2	91	70	76	79	0.5	1.9	1.4	1.3	10	10	7	W 3	W 2	SE 3
18	98.8	96.4	94.4	96.5	-0.3	2.3	1.2	1.1	2.8	-1.5	76	71	92	80	1.5	2.0	0.5	1.3	10	10	10 ▲	E 8	ESE 6	ESE 5
19	88.4	93.5	96.0	92.6	4.4	7.1	4.0	4.9	7.3	1.1	92	67	87	82	0.7	3.3	1.1	1.7	8	5	10 ●	S 7	SW 7	SSE 2
20	93.5	91.3	92.8	92.5	3.9	4.5	1.7	3.0	4.6	1.7	100	98	96	98	0.0	0.1	0.3	0.1	10 ≡	10 ● ≡	10 ●	N 1	N 1	WNW 3
21	98.4	100.4	99.9	99.6	1.0	1.7	-0.2	0.6	1.9	-0.2	88	76	86	83	0.8	1.6	0.8	1.1	10	8	10	W 3	SW 1	ENE 2
22	98.1	100.1	104.3	100.8	0.5	2.2	2.7	2.0	2.7	-0.4	86	87	93	89	0.8	1.0	0.5	0.8	10	10	10	S 1	C 0	C 0
23	107.7	109.9	112.4	110.0	1.2	1.9	0.2	0.9	2.9	0.2	94	73	88	85	0.4	1.9	0.7	1.0	10 ●	10	10 ✳	SSE 2	W 2	NW 1
24	114.5	116.0	118.4	116.3	-0.3	1.4	0.4	0.5	1.9	-0.6	92	76	88	85	0.5	1.7	0.8	1.0	10	10	10	C 0	WNW 1	WNW 2
25	119.4	118.7	118.2	118.8	0.1	1.9	1.4	1.2	2.3	0.0	92	75	85	84	0.5	1.8	1.0	1.1	10	8	9	NW 2	C 0	C 0
26	119.1	120.0	120.1	119.7	-0.5	1.7	-0.1	0.2	2.3	-0.8	94	83	96	91	0.4	1.1	0.3	0.6	8	9	10 ≡	WNW 1	WNW 1	NW 3
27	120.2	119.8	117.7	119.2	1.0	2.8	2.4	2.2	3.2	-0.3	96	84	91	90	0.3	1.2	0.7	0.7	10	10	10	C 0	N 1	SSW 1
28	112.6	111.0	110.5	111.4	2.7	3.1	3.6	3.2	3.9	2.3	89	91	98	93	0.8	0.6	0.1	0.5	10	10	10 ●	WSW 3	W 4	WSW 4
29	109.1	109.2	104.5	107.6	4.3	4.6	5.4	4.9	5.4	3.6	93	84	92	90	0.5	1.4	0.7	0.9	10	8 ⊙	10	WSW 3	W 3	SW 7
30	99.1	100.5	103.9	101.2	4.7	5.5	1.2	3.2	5.6	0.9	94	81	92	89	0.5	1.7	0.5	0.9	10 ○	10	10 ● ✳	W 9	W 8	NNE 5
31																								
M	105.3	105.7	105.9	105.6	3.3	5.1	4.1	4.2	6.2	2.2	90	81	86	86	0.8	1.8	1.3	1.3	9.2	8.9	8.5	3.3	3.3	3.2

Grudzień - Décembre

1	115.8	120.7	125.2	120.6	-2.5	-0.4	-1.2	-1.3	1.4	-2.7	93	88	95	92	0.4	0.7	0.3	0.5	0	10	4	NW 3	NW 2	WNW 3
2	129.2	130.1	129.5	129.6	-2.1	0.8	-2.3	-1.5	1.3	-3.0	94	77	85	85	0.3	1.5	0.8	0.9	10	8 ⊙	9	W 3	W 3	WNW 4
3	126.5	125.4	120.8	124.2	-4.4	-3.3	-4.3	-4.1	-2.0	-5.3	89	83	89	87	0.5	0.8	0.5	0.6	9	6 ⊙	0	W 3	W 2	SW 2
4	114.7	112.9	109.8	112.5	-5.2	0.6	-2.2	-1.8	1.1	-4.3	81	58	74	71	0.9	2.7	1.3	1.6	5	9	1	SW 2	W 3	WSW 4
5	108.9	112.0	116.5	112.5	-0.7	1.7	2.1	1.3	2.5	-2.2	90	96	100	95	0.6	0.3	0.0	0.3	10	10	10 ●	W 2	NW 2	NW 2
6	117.2	117.2	116.1	116.8	1.3	1.3	-0.3	0.5	2.4	-0.3	100	89	98	96	0.0	0.8	0.2	0.3	10	10	10	W 1	W 5	W 3
7	113.9	113.1	114.5	113.8	-1.5	-1.5	-2.1	-1.8	-0.1	-2.1	94	94	92	93	0.3	0.3	0.4	0.3	10	10 ≡	9	W 3	SW 4	W 3
8	117.3	118.2	116.9	117.5	-5.2	-2.1	-2.6	-2.6	-1.6	-3.8	92	96	95	94	0.3	0.2	0.2	0.2	10 ≡	10 ≡	10 ≡	W 2	SW 3	SW 2
9	106.1	98.5	91.0	98.5	-1.8	1.7	1.6	0.8	2.1	-5.2	81	72	67	73	1.0	1.9	2.3	1.7	2	9	9	S 2	SW 3	SW 5
10	88.5	89.3	89.8	89.2	1.5	2.7	1.8	2.0	3.6	1.2	78	72	78	76	1.5	2.1	1.6	1.7	9	10	9	SW 5	SW 6	SW 6
11	91.1	92.2	91.0	91.4	2.8	2.5	2.4	2.5	3.0	1.3	86	95	89	90	1.1	0.4	0.8	0.8	9	10	10	WSW 4	WSW 3	SW 3
12	85.3	83.8	84.4	84.5	2.4	3.7	2.7	2.9	4.4	1.6	84	65	63	71	1.2	2.8	2.7	2.2	10 ●	10	9	S 3	S 3	S 2
13	87.1	86.6	87.5	87.1	0.0	1.5	2.1	1.4	3.4	0.0	75	83	80	79	1.5	1.1	1.4	1.5	10	9	10 ●	SSE 4	NE 5	S 3
14	88.8	90.6	92.0	90.5	1.3	0.9	0.1	0.6	2.4	0.1	94	96	86	92	0.4	0.2	0.9	0.5	10 ●	10	8	S 2	WNW 4	W 3
15	85.5	75.1	70.8	77.1	-1.9	-1.2	0.7	-0.4	0.9	-1.9	83	99	93	93	0.9	0.1	0.1	0.4	2	10 ✳ ≡	10	S 2	S 5	W 5
16	63.9	62.3	64.5	63.6	0.4	-0.1	-0.7	-0.3	1.4	-0.8	86	90	96	91	0.9	0.7	0.2	0.6	9	10 ✳	10 ✳	SW 2	ESE 2	E 1
17	75.5	79.8	83.5	79.6	-0.3	0.2	-0.4	-0.2	0.9	-1.3	98	88	96	94	0.2	0.7	0.2	0.4	10	10 ▲	10 ✳	NNW 3	NW 2	WSW 1
18	85.3	86.2	88.7	86.7	-2.7	-3.6	-3.4	-3.3	-0.3	-4.6	93	94	70	86	0.3	0.3	1.4	0.7	9	10 ✳	10	C 0	N 2	NNW 1
19	91.7	94.7	100.3	95.6	-4.6	-5.2	-6.0	-5.4	-3.2	-6.0	76	78	81	78	1.0	0.9	0.7	0.9	10	10 ✳	10	N 2	NE 2	NE 3
20	107.0	109.7	112.1	109.6	-9.2	-12.7	-14.5	-12.7	-5.8	-14.7	85	77	83	82	0.4	0.5	0.3	0.4	10	2 ⊙	7	NE 4	NNE 3	NE 1
21	110.1	109.1	111.3	110.2	-19.4	-15.6	-18.6	-18.0	-14.2	-19.3	83	86	84	84	0.2	0.3	0.2	0.2	4	0 ⊙	0	NE 3	NE 4	NE 2
22	117.2	121.6	125.7	121.5	-17.4	-15.6	-14.9	-15.7	-14.7	-19.3	85	81	73	80	0.2	0.3	0.5	0.3	5	4 ⊙	10	NNE 4	NNE 4	NNE 3
23	129.5	131.8	133.1	131.5	-14.1	-11.5	-14.4	-13.6	-11.5	-15.5	75	79	78	77	0.5	0.5	0.4	0.5	9	6 ⊙	2	NE 6	NE 5	NE 3
24	132.1	130.6	129.5	130.7	-12.4	-5.9	-7.4	-8.3	-5.3	-15.4	89	81	93	88	0.3	0.7	0.2	0.4	9	9	10	C 0	NE 4	C 0
25	125.3	121.7	115.8	120.9	-5.5	-5.8	-9.0	-7.3	-5.0	-9.1	90	73	79	80	0.4	1.1	0.6	0.7	10	9	10 ✳	C 0	SE 4	SE 3
26	108.0	103.9	101.1	104.3	-12.6	-12.0	-11.2	-11.8	-9.0	-13.2	85	82	86	84	0.4	0.4	0.4	0.4	10	9 ✳ ⊙	10	SE 4	SE 1	SE 1
27	99.9	99.7	100.6	100.1	-8.9	-7.5	-8.1	-8.2	-7.5	-13.5	89	79	90	86	0.4	0.7	0.3	0.5	10	9 ✳	10	SE 2	C 0	C 0
28	100.9	101.6	102.8	101.8	-7.7	-7.1	-5.9	-6.6	-5.9	-8.5	81	71	76	76	0.6	1.0	0.9	0.8	10	9	10	C 0	SW 2	SSW 2
29	101.3	98.8	95.6	98.6	-10.7	-7.4	-5.9	-6.5	-3.8	-11.2	87	76	85	83	0.4	0.8	0.7	0.6	9	10	10	SE 1	ESE 3	C 0
30	97.7	100.2	103.0	100.5	-9.3	-7.4	-8.4	-8.4	-3.9	-10.6	88	90	92	90	0.4	0.3	0.3	0.3	10	10	9	C 0	NW 2	NE 3
31	106.0	108.7	111.3	108.7	-11.5	-11.3	-13.6	-13.6	-8.4	-15.7	90	86	86	87	0.3	0.4	0.3	0.3	9	10	8	NE 4	NNE 4	NNE 2
M	104.1	104.1	104.3	104.2	-5.1	-3.9	-4.6	-4.6	-2.3	-6.6	87	83	85	85	0.6	0.8	0.7	0.7	8.4	8.6	8.2	2.3	3.1	2.6

Warszawa-Bielany H_s=98m H_b=104,7m h_w=16m Listopad - Novembre 1962

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	5	0.2	•	$\text{♀}^{\circ}n\text{-}a\ \bullet^{\circ}p; = n\text{-}p$
2	4	0.0	•	$\text{♀}^{\circ-2}p; \equiv^{2}n\text{-}a = a\text{-}n$
3	4	0.0	•	$\text{♀}^{\circ}p\text{-}n; = n\text{-}n$
4	5	0.0	•	$\text{♀}^{\circ}n\text{-}a; = n\text{-}a, p\text{-}n$
5	6	•	•	$= na\text{-}p$
6	7	•	•	$^{\infty}na\text{-}a$
7	7	•	•	
8	6	•	•	$= na\text{-}a\ ^{\infty}a\text{-}p$
9	6	•	•	$= na\text{-}p; \triangle^{\circ}na$
10	7	3.4	•	$\bullet^{\circ}14^{20}\text{-}16^{50} *^{\circ}\text{-}n$
11	6	5.8	1	$*^{\circ}na\text{-}17^{10}\ \bullet^{\circ}\text{-}n; = na\text{-}p$
12	6	3.2	•	$\bullet^{\circ}a, p\ \text{♀}^{\circ}p\text{-}n; = n\text{-}n$
13	6	•	•	$\equiv n = a\text{-}n; \triangle^{\circ}p\text{-}n$
14	5	0.0	•	$\text{♀}^{\circ}p\ldots n; \equiv^{2}n\text{-}a = a\text{-}n$
15	3	9.5	•	$\bullet^{\circ}a\text{-}n; \equiv^{\circ}n\text{-}p$
16	6	•	•	$= n\text{-}p$
17	7	•	•	$= n\text{-}a; \sqcup^{1}n\text{-}a$
18	7	2.5	•	$\bullet^{\circ}, \bullet^{\circ}; \triangle p\text{-}n$
19	8	10.0	•	$\bullet^{\circ}20^{30}\text{-}n; = p\text{-}n$
20	2	4.6	•	$\bullet^{\circ}na\ \text{♀}^{\circ}a\text{-}p\ \bullet^{\circ}12^{40}\text{-}np; \equiv^{1}na\text{-}p$
21	6	•	•	$= na\text{-}n$
22	6	0.8	•	$= n\text{-}a$
23	7	0.3	•	$\bullet^{\circ}na\text{-}p; *^{\circ}p; = n\text{-}a$
24	6	•	•	$= na\text{-}p; \sqcup^{\circ}na$
25	6	•	•	$= na\text{-}n$
26	6	•	•	$= n\text{-}20^{30}\ \equiv^{\circ}\text{-}n; \sqcup^{\circ}n\text{-}a$
27	7	•	•	$= n\text{-}a, p\text{-}n; \triangle^{\circ}\text{-}n\text{-}a$
28	4	4.2	•	$\bullet^{\circ}15^{55}\text{-}np; = na\text{-}p$
29	8	5.3	•	$\bullet^{\circ}na\text{-}6^{00}, p\text{-}19^{30}, 20^{50}\text{-}np$
30	7	1.1	•	$\bullet^{\circ}na\text{-}6^{50}, 9^{55}\text{-}10^{10}, 14^{30\text{-}50}, 18^{20}\text{-}20^{10}\ *^{\circ}\text{-}20^{45}; \sqcup^{\circ}np$
31				
Σ	—	50.9	—	UWAGI.

Grudzień - Décembre

1	7	0.0	•	$*^{\circ}13^{20\text{-}35}; \sqcup^{\circ}na\text{-}n$
2	7	•	•	$\sqcup^{\circ}na\text{-}p$
3	6	•	•	$= n\text{-}n; \sqcup^{1\text{-}\circ}n\text{-}n$
4	6	•	•	$= n\text{-}n; \sqcup^{\circ}n\text{-}a\ \sqcup^{1}p\text{-}n$
5	5	0.6	•	$\text{♀}p\text{-}n; = n\text{-}n; \sqcup^{\circ}n\text{-}a$
6	6	0.0	•	$\text{♀}p; = n\text{-}p$
7	3	•	•	$= n\text{-}a \equiv^{\circ}a\text{-}p = p\text{-}n; \sqcup^{1}p\text{-}n$
8	1	•	•	$\equiv^{2}n\text{-}n; \sqcup^{2}n\text{-}n$
9	6	•	•	$= a\text{-}p; \sqcup^{1}n\text{-}a$
10	6	0.4	•	$\bullet^{\circ}np; = a\text{-}p$
11	6	0.9	•	$\bullet^{\circ}na, 12^{26}\text{-}p; = a\text{-}p$
12	6	•	•	$\bullet^{1}6^{32}; = a\text{-}p; \text{☔}p\text{-}n$
13	6	3.7	•	$\bullet^{\circ}p, 20^{20}; = a\text{-}p$
14	4	1.2	•	$\bullet^{\circ}n\text{-}a\ \text{☃}6^{45}\ *^{\circ}7^{00}\text{-}a; = a\text{-}p$
15	2	2.8	•	$*^{1}a\text{-}p; \equiv^{2}a\text{-}p$
16	6	2.3	5	$*^{\circ}a\ldots n; = n\text{-}n$
17	6	0.6	6	$\triangle 12^{20\text{-}50} *^{\circ}\text{-}n; = a\text{-}p$
18	4	0.1	6	$*^{\circ}9^{50}\text{-}10^{45}, 10^{55}\text{-}p; = na\text{-}p$
19	7	0.0	6	$*^{\circ}a\text{-}p$
20	7	•	6	
21	7	•	6	$\sqcup^{\circ}na\text{-}a, np$
22	7	•	6	$\sqcup^{\circ}na\text{-}np$
23	8	•	5	$\sqcup^{\circ}np$
24	7	0.0	5	$*a\text{-}p; = p\text{-}n$
25	7	0.0	5	$*^{\circ}a, p\ldots n; = n\text{-}a$
26	6	0.3	6	$*^{\circ}n\text{-}a$
27	5	0.1	6	$*^{\circ}a\text{-}p; = n\text{-}n$
28	6	0.0	8	$*^{\circ}a; = n\text{-}p$
29	6	0.3	8	$*^{\circ}p; = n\text{-}n$
30	5	•	8	
31	6	0.0	8	
Σ	—	13.5	—	UWAGI.

Łódź - Lublinek φ = 51°44' λ = 19°24' Styczeń - Janvier 1962

DNI	CIŚNIENIE P-900 I				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	83.1	86.7	87.3	85.7	3.3	2.2	0.4	1.6	4.1	-0.8	83	77	78	79	1.3	1.9	1.4	1.5	10	10	10	SW 7	SW 7	W 5
2	86.8	88.5	92.2	89.2	-1.5	-0.9	-1.7	-1.4	0.5	-2.2	86	89	86	87	0.8	0.6	0.8	0.7	10	9*	10*	W 5	W 5	WNW 8
3	95.9	96.8	101.1	97.9	-6.1	-3.6	-1.1	-3.0	-0.2	-7.1	89	94	99	94	0.4	0.3	0.1	0.3	0	10*	10	WNW 6	W 6	NW 2
4	103.9	103.1	101.7	102.9	-1.1	-1.3	-2.7	-2.0	0.1	-2.7	91	86	89	89	0.5	0.8	0.6	0.6	10	10	10	SW 2	SW 4	W 4
5	99.7	98.5	94.9	97.7	-3.2	-3.5	-6.9	-5.1	-2.0	-7.3	92	94	91	92	0.3	0.3	0.3	0.3	10	10	0	W 4	W 5	SW 3
6	91.9	89.6	86.9	89.5	-3.1	-3.9	0.3	-2.1	1.2	-7.9	93	92	94	93	0.3	0.4	0.3	0.3	10	10	10*	W 8	WSW 7	WSW 9
7	91.2	96.7	102.7	96.9	0.8	0.6	-0.4	0.2	1.7	-0.5	96	90	92	93	0.3	0.6	0.5	0.5	10*	10△	9	W 7	WNW 7	W 3
8	103.1	102.8	102.2	102.7	-1.3	0.2	0.3	-0.1	1.1	-4.2	86	81	100	89	0.8	1.2	0.0	0.7	9	10	10≡	SSW 3	SSW 4	SW 1
9	98.5	95.9	93.3	95.9	0.3	0.8	-3.1	-1.3	1.9	-3.3	88	71	81	80	0.7	1.9	0.9	1.2	9	7	7	S 4	S 7	S 5
10	89.6	86.9	84.1	86.9	-3.7	-1.9	-1.9	-2.4	0.0	-4.4	85	79	83	82	0.7	1.1	0.9	0.9	10	10	0	S 8	S 6	S 5
11	85.2	82.4	79.6	82.4	-0.7	3.0	3.3	2.2	4.7	-2.1	87	72	88	82	0.7	2.1	0.9	1.2	0	8	10●	SSW 6	S 9	S 9
12	82.3	81.8	75.9	80.0	2.9	3.1	1.8	2.4	5.1	0.7	95	93	94	94	0.4	0.5	0.4	0.4	10	10	9	SSW 6	WSW 2	S 7
13	67.4	70.7	74.6	70.9	3.0	3.8	1.8	2.6	5.2	1.3	90	87	82	86	0.8	1.1	1.3	1.1	10●	8	0	SSW10	SSW 8	SSW 5
14	77.4	79.8	82.4	79.9	0.6	3.3	1.4	1.7	3.4	-0.5	90	68	87	82	0.6	2.5	0.9	1.3	9	2⊙	10*	SW 4	WSW 9	SW 7
15	87.2	90.8	95.6	91.2	0.2	0.4	1.0	0.6	2.2	0.0	98	100	92	97	0.1	0.0	0.5	0.2	10*	10	10	SW 8	SW 6	SW 5
16	98.7	98.1	95.0	97.3	-0.7	2.0	1.6	1.1	3.2	-1.8	87	71	69	76	0.7	2.1	2.2	1.7	5	8⊙	10	SW 5	S 4	S 8
17	93.3	93.6	94.4	93.8	2.2	2.3	-0.8	0.7	2.8	-0.9	61	66	85	71	2.8	2.4	0.9	2.0	7	7	10	SSW 8	SSW 8	S 2
18	92.5	91.6	91.6	91.9	-1.8	2.5	0.9	0.6	4.2	-2.3	92	72	83	82	0.4	2.1	1.1	1.2	10	10	10	S 2	SW 4	SSW 3
19	93.6	94.2	90.3	92.7	1.2	2.4	2.2	2.0	3.9	0.0	83	84	87	85	1.2	1.2	1.0	1.1	8	10●	9	SW 3	SW 3	SSW 6
20	90.6	92.6	97.3	95.5	3.7	5.2	3.3	3.9	6.1	1.8	75	64	71	70	2.0	3.1	2.2	2.4	2	5⊙	4	WSW 7	WSW16	WSW10
21	96.4	96.5	94.6	95.8	2.2	4.6	5.5	4.4	6.5	0.3	78	100	95	91	1.6	0.0	0.4	0.7	10	10●	10	SW 7	SW 5	SW 7
22	88.7	84.6	86.8	86.7	5.0	7.8	5.6	6.0	8.7	4.5	92	69	58	73	0.7	3.3	3.9	2.6	9	9	10	SSW 8	SSW 9	W 10
23	90.1	91.3	93.0	91.5	2.0	4.8	1.8	2.6	6.7	1.1	73	64	78	72	2.0	3.1	1.6	2.2	1	4	1	SW 9	SW 8	SW 7
24	93.9	93.5	91.4	92.9	1.2	0.2	1.0	0.8	3.0	0.0	85	98	96	93	1.1	0.1	0.3	0.5	9	10*	10	WSW 6	SSW 3	S 2
25	86.0	83.5	84.3	84.6	1.1	6.0	5.1	4.3	7.1	0.4	98	97	97	97	0.1	0.3	0.3	0.2	10●	10●	10●	SE 2	SW 7	SW 4
26	90.8	94.6	92.7	92.7	0.3	1.4	-0.6	0.2	2.8	-1.2	94	76	85	85	0.3	1.7	0.9	1.0	10	6	8	NNW 9	NNW 3	SSW 2
27	89.6	89.9	89.5	89.7	-0.7	1.4	0.4	0.4	3.4	-1.4	97	94	96	96	0.2	0.4	0.3	0.3	10*	10	8	S 1	WNW 8	WNW 5
28	88.8	87.7	91.3	89.3	-0.1	-1.5	-4.5	-2.6	2.0	-4.6	92	70	77	80	0.5	1.7	1.0	1.1	9	9	5	WNW 8	NW 10	NNW10
29	97.4	101.3	106.2	101.6	-8.1	-7.3	-9.8	-8.8	-3.6	-10.1	78	85	85	83	0.7	0.5	0.4	0.5	9*	10*	10*	NNE10	NNE10	NNE 8
30	109.4	112.5	115.1	112.3	-9.1	-7.4	-11.4	-9.3	-7.2	-11.9	88	87	86	87	0.4	0.4	0.4	0.4	10*	0⊙	0	NNE 7	NE 8	NE 5
31	114.1	113.0	108.9	112.0	-15.7	-11.0	-12.3	-12.8	-9.4	-16.8	95	80	89	88	0.1	0.5	0.3	0.3	0	3⊙	0	NE 2	E 5	E 3
M	92.2	92.6	92.8	92.5	-0.9	0.5	-0.6	-0.4	2.2	-2.7	88	82	86	85	0.8	1.2	0.9	1.0	7.9	8.2	7.4	5.9	6.5	5.5

Luty - Février

1	98.8	94.2	93.6	95.5	-12.6	-8.2	-8.2	-9.3	-5.8	-14.2	89	81	89	86	0.3	0.6	0.3	0.4	6	9	0	E 5	ESE 5	ESE 3
2	93.3	95.0	97.4	95.3	-6.7	-3.3	-7.8	-6.4	-2.5	-9.3	91	74	99	88	0.3	1.2	0.0	0.5	10*	4	0	SSE 2	SSW 1	C 0
3	100.8	102.5	102.6	102.0	-14.4	-6.5	-8.9	-9.7	-2.2	-15.4	87	94	92	91	0.3	0.2	0.3	0.3	0≡	0	0≡	C 0	C 0	C 0
4	97.2	94.6	96.9	96.2	-10.6	-2.8	-0.5	-5.6	0.5	-11.4	90	86	96	91	0.3	0.7	0.3	0.4	8	10*	9	SSE 1	SW 6	W 3
5	94.0	84.1	81.7	86.6	-3.5	0.2	1.4	-0.1	2.7	-5.6	97	74	91	87	0.1	1.6	0.7	0.8	9	10	10	SW 3	S 9	W 8
6	86.5	90.6	95.5	90.9	1.4	1.8	0.5	1.0	3.1	-0.3	79	76	90	82	1.4	1.7	0.6	1.2	10*	10	9	W 12	W 10	W 4
7	96.0	94.0	91.2	93.7	-0.2	3.0	1.9	1.6	4.8	-1.3	98	77	87	87	0.1	1.7	0.9	0.9	10	9	10	S 2	SSE 3	SE 4
8	88.3	88.9	91.2	89.5	-0.8	2.4	1.4	1.1	3.6	-1.2	83	77	96	85	1.0	1.7	0.3	1.0	9	10	10●	SE 2	S 3	SSW 3
9	95.0	100.4	106.2	100.5	1.2	1.1	0.0	0.6	2.4	0.0	98	87	90	92	0.2	0.9	0.6	0.6	10	9	9	SW 3	W 7	WNW 3
10	108.9	108.2	105.9	107.7	-3.1	2.4	0.7	0.2	3.7	-3.3	95	68	85	83	0.3	2.4	1.0	1.2	5	8	10	C 0	WSW 3	WSW 2
11	100.5	98.5	102.7	100.6	0.4	0.2	0.6	0.4	1.8	0.0	75	96	82	84	1.6	0.3	1.1	1.0	10	10*	4	SW 4	WSW 8	W 7
12	90.4	74.5	63.8	76.2	-0.2	0.0	0.2	0.0	5.6	-0.9	72	98	98	89	1.7	0.1	0.1	0.6	10	10*	10*	SSW 9	SW 16	WNW16
13	62.6	62.1	65.3	63.3	1.8	1.9	-1.0	0.4	4.2	-1.3	80	82	95	86	1.5	1.3	0.3	1.0	10	9	8	W 10	W 6	SW 3
14	68.8	70.3	75.6	71.6	-1.0	0.0	-2.5	-1.5	1.0	-3.3	97	79	93	90	0.2	1.3	0.4	0.6	10	8	1	C 0	NW 5	NW 3
15	83.7	87.3	94.8	88.6	-3.3	-2.4	-5.5	-4.2	-1.5	-5.8	97	78	72	82	0.1	1.1	1.1	0.8	10*	10*	0	NW 8	NW 12	NW 7
16	85.0	72.2	65.6	74.3	-5.5	-1.5	1.8	-0.8	2.7	-8.5	77	94	87	86	0.9	0.3	0.9	0.7	10	10△	8	SSW 9	SSW12	WSW 9
17	61.7	64.9	73.0	66.5	1.6	1.0	-1.9	-0.3	3.0	-2.4	78	88	94	87	1.6	0.8	0.3	0.9	10	10	10	W 14	W 12	W 10
18	82.8	88.2	95.6	88.9	-4.1	-2.5	-4.1	-3.7	-0.6	-4.5	77	59	77	71	1.0	2.1	1.0	1.4	10	8	10	NW 12	NW 14	NW 5
19	95.0	93.3	93.8	94.0	-3.1	-1.7	1.7	-0.4	2.6	-4.5	93	94	98	95	0.4	0.3	0.1	0.3	10*	10*	10●	W 3	S 2	W 7
20	94.1	93.3	92.0	93.1	2.0	3.4	3.2	3.0	4.9	1.5	93	76	86	83	0.6	1.9	1.1	1.2	10●	9	9	W 7	W 10	W 9
21	95.7	97.7	103.1	98.8	-0.3	-1.5	-3.5	-2.2	4.5	-5.7	72	92	85	83	1.7	0.4	0.7	0.9	10*	10*	10*	NW 12	NW 12	NW 8
22	107.4	109.6	111.7	109.6	-5.1	-4.3	-6.3	-5.3	-2.8	-6.3	90	79	81	83	0.4	0.9	0.7	0.7	10*	10	10	NNE 6	NE 7	NNE 7
23	110.6	104.9	102.7	106.1	-8.7	-1.6	-4.7	-4.0	-1.3	-9.9	83	63	86	77	0.5	2.0	0.6	1.0	10	9	10*	NW 5	NNW 7	NNE 5
24	98.1	96.5	98.0	97.5	-6.2	-5.6	-6.0	-6.0	-4.0	-6.4	89	87	89	88	0.4	0.5	0.4	0.4	10*	10*	10*	NNE 5	NE 7	ENE 7
25	100.2	100.9	100.6	100.6	-8.4	-6.7	-5.9	-6.7	-4.6	-9.5	92	86	92	90	0.3	0.5	0.3	0.4	9	10	10	E 3	ENE 7	ENE 5
26	98.7	99.2	99.0	99.0	-3.1	-1.9	-2.6	-2.6	-1.0	-6.2	93	83	85	87	0.4	0.9	0.8	0.7	10△	10	9	ENE 5	E 5	E 5
27	97.9	97.0	96.2	97.0	-4.1	-3.3	-4.5	-4.1	-1.6	-4.8	87	85	88	87	0.6	0.7	0.5	0.6	10	10	10	E 3	ENE 7	E 6
28	92.9	91.2	89.4	91.2	-7.4	-5.1	-5.3	-5.8	-3.3	-7.9	96	85	87	89	0.1	0.6	0.5	0.4	10	10	10	E 3	E 3	E 3
29																								
30																								
31																								
M	92.3	91.2	92.3	91.9	-3.7	-1.5	-2.4	-2.5	0.7	-5.2	87	82	89	86	0.7	1.0	0.6	0.8	9.1	9.0	7.7	5.4	7.1	5.4

Łódź-Lublinek $H_s = 187m$ $H_a = 187,7m$ $h_w = 11m$ Styczeń - Janvier 196.

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ OŚNIEŻU h	POGODA
1	7	•	4	≫ 9^{30}-10^{15}; = 0^{00}-7^{40}
2	6	0.0	2	* ° 12^{40}...13^{25}-17^{46}; 19^{42}-22^{48}; = 8^{20}-24
3	4	0.4	2	* °-1 9^{55}-13^{20} △° -14^{05} * °-1 -14^{30} △° -15^{40} ⊽ -18^{45}; = 0^{00}-9^{30}-24; ~ 15^{40}-18^{45}
4	6	0.0	3	= 0^{00}-24
5	5	0.3	3	⊽ 6^{50}-8^{46}; = 0^{00}-24; ~ 6^{50}-8^{46}
6	4	1.1	3	⊽ °15^{20}...17^{25} △° 17^{50}-18^{40} * °-20^{45}; 21^{50}-22^{20} * °...23^{40}; ≫ 1^{10}-2^{05}; = 0^{00}-24; ~ ° 15^{20}-17^{25}
7	6	0.1	6	* °-1 1^{55}-6^{30} * °-7^{40} * °-11^{00}...12^{00} △° -16^{40}; = 0^{00}-16^{00}
8	6	0.0	5	* °-1 10^{13-43}; = 9^{30}-18^{50} ≡ '-24
9	7	•	4	≡ '0^{00-20} ≡ ° • -1^{40} = -12^{20}
10	6	•	3	= 7^{30}-24
11	6	2.1	3	• °18^{15}-21^{30}; 22^{40}-23^{10}; = 0^{00}-24
12	5	4.2	pł.	• °3^{45}-6^{35}; 7^{15}...9^{10}; = 0^{00}-24
13	7	0.1	•	• °2^{40}-7^{45} ⊽ °13^{20-25} 14^{50-55}; ≫ 2^{30}-8^{40}; = 0^{00}-8^{30}
14	7	1.7	•	* °6^{55}...7^{38}; 19^{53}...21^{15}-23^{48}
15	6	1.2	1	* °1^{16}...2^{46} * °-1 6^{00}-7^{40} * ° 8^{40}-9^{15} * °-10^{32} * °-11^{10} ⊽ °-1 ...11^{57} * °-18^{45}-19^{30}; = 7^{40}-24
16	6	•	pł.	= 0^{00}-17^{30}; ⊽ 19^{37}-22^{15}
17	7	•	pł.	≫ 0^{37}-1^{15}; 5^{30}-6^{40}; = 16^{30}-24; ⊽ 19^{00}-24
18	6	•	•	= 0^{00}-24; ⊽ 0^{00}-2^{50}
19	6	0.8	•	• °12^{35}-13^{50}; 23^{41}...24; = 0^{00}-24
20	8	•	•	• °0^{00}...1^{56}; ≫ 9^{15}-11^{05} ☁ -14^{15} ≫ -21^{30}; = 0^{00}-3^{55}
21	4	2.3	•	• °7^{35}-9^{15} • °-11^{50}; 12^{30}...13^{00}-14^{20} • °-18^{35}; = 8^{00}-24; ⊎ 4^{30}-5^{15}
22	7	•	•	≫ 19^{45}-21^{20}; 23^{45}-24; = 0^{00}-12^{30}
23	7	•	•	≫ 0^{00}-2^{20}; 4^{18}-6^{35}
24	5	1.9	•	* °-1 11^{42}-14^{58}; = 11^{20}-24
25	6	10.6	•	• °0^{44}-3^{25} * °-4^{46} • °5^{45}-8^{30} • °-9^{40} • °-11^{00}...24; = 0^{00}-15^{00}
26	6	0.2	•	• °0^{00}...2^{30}-4^{20} * °7^{50}...8^{40}; = 1^{30}-24
27	7	3.5	1	* °2^{50}...4^{30}-8^{00}...8^{40}; 9^{35}-10^{00} • °11^{50}-12^{30} △° $15^{02...35}$ * °-1 19^{10}...23^{50}; ≫ 13^{30}-14^{20}; = 0^{00}-10^{30}
28	8	0.3	2	* '0^{25-30} * °1^{50-58} * °-2 9^{22}-10^{20} * °-1 13^{01}...24; ≫ 10^{50}...24
29	5	0.6	4	* °0^{00-15}; 0^{58}-2^{15} * °-7^{45} * °9^{20}-10^{50} * °-13^{45}; 14^{48}...17^{30}-24; ⊹ 3^{55}-24; ≫ 4^{15}-10^{30}; 11^{20}-15^{40}
30	6	0.0	6	* °0^{00}...6^{45}-8^{20}...9^{44}; ⊹ 0^{00}-5^{50}; = 9^{44}-24
31	6	•	6	= 0^{00}-24
Σ	—	31.4	—	UWAGI: W ciągu całego roku wartości ciśnienia powietrza są za niskie przeciętnie o ok. 0,6 mb.

Luty - Février

1	6	0.0	5	* °8^{50}-9^{20}; = 0^{00}-24
2	5	0.2	6	* °6^{40}...7^{10}-9^{15}...9^{43}; = 0^{00}-22^{50} ≡ °-1 -24
3	4	•	8	≡ °-1 0^{00}-7^{30} ≡ ²-8^{15} ≡ ¹⁻⁰-9^{50} = -19^{50} ≡ °-23^{35} = -24; v ° 7^{10}-9^{50}
4	5	0.2	6	* °11^{50}-13^{30}...14^{30} • °-15^{45}; = 0^{00}-23^{50} ≡ '-24; ~ 14
5	6	3.1	7	* °-1 13^{03}-17^{45}; ≡ '0^{00-45} = -18^{45}
6	7	0.0	4	⊽ °0^{40}-1^{50}; 6^{40}-7^{10} △° 9^{45-57}; 10^{50-58}; ≫ 2^{30}-18^{30}
7	6	0.0	2	• °19^{55}...20^{33}; = 4^{40}-8^{20} ≡ °-10^{05} = -24
8	6	1.6	pł.	• °15^{50}-21^{40}; = 0^{00}-24; ⊕ 10^{30}-11^{15}
9	7	0.7	pł.	• °3^{40}-6^{10} • °8^{35}-9^{30} • °-10^{00} * °-1 -10^{30} ⊽ °15^{46}-16^{20}; = 0^{00}-8^{45} ≡ °-1 -9^{50} = -11^{00}; 16^{20}-24
10	6	•	pł.	= 0^{00}-24
11	5	1.5	pł.	* °10^{40}-11^{05} * °-1 -14^{00} △° 15^{23-28} ⊽ °-1 15^{41-51}; = 0^{00}-16^{05}
12	4	9.3	pł.	* '8^{50}-14^{30} • °-20^{05} * '-20^{25} ⊽ '-21^{35}; ≫ 6^{20}-7^{15} ☁ 8^{15}-24
13	8	0.1	pł.	⊽ '12^{30-35}; 13^{06-15} ⊽ °15^{20-36} ☁ 0^{00-30} ≫ -7^{30}
14	7	0.9	•	△ °11^{45}-12^{07} ⊽ °13^{57}...19^{25}; = 6^{30}-8^{15}
15	6	0.1	1	⊽ °-1 5^{45}...18^{03}; ⊹ °8^{20-30}; ≫ 2^{30}-4^{15}; 7^{16}-15^{30}
16	4	5.0	3	* °-2 8^{35}-12^{30} △' -12^{45} * '-14^{32} * °-1 • °-19^{45} * °-2 21^{22-40} ⊽ °23^{44}-24; ⊹ °-1 ⊹ °-2 7^{40}-14^{50}; ≫ 7^{40}-18^{40}; np
17	7	0.8	5	⊽ °-1 1^{00}...20^{40}; ≫ 0^{00}-17^{40}; 19^{45}-24
18	8	0.0	6	⊽ °-1 1^{05}...14^{50}; ⊹ °7^{40}-12^{40}; ≫ 0^{00}-18^{30}; ⊽ 21^{30}-24
19	4	4.6	6	* °-1 5^{45}-7^{05} * °-7^{58} * °-1 8^{42}-10^{10}...11^{30}-15^{35} • °-16^{20} • °-19^{10}...19^{40} • °20^{35}-24; = 19^{40}-24; ⊽ 0^{00}-1^{00}
20	7	0.8	pł.	• °0^{00}-1^{20}...11^{05}; 15^{40}-17^{15}; ≫ 12^{30}-15^{35}; = 0^{00}-7^{45}; 15^{30}-20^{30}
21	6	0.5	pł.	⊽ °-1 6^{35}-9^{45} * °-21^{50}...23^{40}; ≫ 3^{10}-5^{20}; 6^{15}-16^{30}
22	6	0.1	2	* °0^{45}...1^{10}-10^{30} ⊽ °15^{04}...18^{06} * °19^{50}...24; = 10^{30}-24
23	7	0.1	3	* °0^{00}...2^{35}; 15^{45}...24; = 0^{00}-9^{20}; 17^{20}-24
24	6	0.3	4	* °0^{00}...4^{10} * °-1 -10^{30}...21^{00}-24; = 0^{00}-24
25	6	0.3	6	* °0^{00}-3^{40}; 12^{50}; 16^{32}; = 0^{00}-24
26	6	0.0	6	* °1^{15}-3^{20} △° -9^{38} * °13^{03-15} △° -16^{40}; = 0^{00}-24
27	6	0.0	6	△ °9^{48}-10^{48}; 19^{50}-24; = 0^{00}-24
28	6	0.0	6	△ °0^{00}-2^{40} * °18^{52}...19^{45}; = 0^{00}-24
29				
30				
31				
Σ	—	30.2	—	UWAGI:

Łódź - Lublinek φ = 51°44' λ = 19°24' Marzec - Mars 1962

DNI	CIŚNIENIE P - 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	87.3	86.6	85.4	86.4	-5.9	-4.2	-4.1	-4.6	-3.9	-7.1	89	89	91	90	0.4	0.5	0.4	0.4	9	10	10	NE 2	NE 5	ENE 2
2	83.0	82.2	81.9	82.4	-5.0	-2.9	-3.1	-3.5	-1.7	-7.2	95	84	88	89	0.2	0.8	0.6	0.5	10	10 ♙	10	C 0	WNW 3	C 0
3	82.4	82.2	81.7	82.1	-4.3	2.5	1.1	0.1	4.0	-5.3	91	58	85	78	0.4	3.1	1.0	1.5	10	4	10	C 0	SSE 1	SE 1
4	76.6	72.9	71.5	73.7	0.3	3.2	1.8	1.8	4.7	-0.9	88	79	96	88	0.7	1.6	0.3	0.9	10	10	10 ●	SE 1	ESE 3	ESE 1
5	74.0	74.3	71.3	73.2	0.8	1.5	2.2	1.7	3.0	0.5	98	98	96	97	0.2	0.1	0.3	0.2	10	10	10	NE 3	ENE 6	E 3
6	68.9	78.5	88.5	78.6	0.4	-0.9	-1.3	-0.8	6.4	-1.4	100	87	84	90	0.0	0.7	0.9	0.5	10 ●	10 ✳	10 ✳	W 4	W 9	NW 9
7	96.4	97.8	101.4	98.5	-5.1	-1.9	-3.2	-3.4	-0.4	-5.6	83	69	81	78	0.7	1.7	0.9	1.1	9	9	0	NW 5	N 7	N 3
8	103.4	104.2	103.5	103.7	-3.2	-0.3	-2.2	-2.0	2.0	-5.3	92	74	91	86	0.3	1.6	0.5	0.8	9	5 ⊙	4	NW 3	WNW 3	W 1
9	103.9	103.1	98.8	101.9	-4.3	0.9	-1.6	-1.6	2.5	-4.8	89	64	75	76	0.5	2.3	1.3	1.4	2	4 ⊙	3	E 2	ESE 7	ESE 9
10	93.4	90.4	88.2	90.7	-2.6	3.2	1.8	1.0	4.5	-3.1	73	45	73	64	1.4	4.3	2.0	2.6	6	10	10	ESE 6	SE 6	SSE 5
11	86.1	84.6	82.5	84.4	0.8	9.6	4.6	4.9	10.7	0.4	88	58	85	77	0.8	5.1	1.3	2.4	8 ⊙	8 ⊙	9	S 2	SW 4	C 0
12	78.5	75.2	70.7	74.8	2.2	4.4	2.2	2.8	7.1	2.0	100	97	100	99	0.0	0.3	0.0	0.1	10 ●	10 ●	10 ●≡	C 0	C 0	C 0
13	75.2	80.1	88.0	81.1	-3.8	-5.3	-5.7	-4.6	2.7	-5.9	94	88	87	90	0.3	0.6	0.5	0.5	10 ✳	9 ✳	5	NW 12	WNW 12	WNW 7
14	92.2	95.0	97.0	94.7	-7.1	-4.5	-7.9	-6.8	-2.4	-8.7	85	72	78	78	0.5	1.2	0.7	0.8	9	9 ✳	0	W 6	W 8	C 0
15	97.0	97.0	97.9	97.3	-10.0	-2.3	-4.7	-5.5	-1.7	-11.1	87	55	74	72	0.4	2.3	1.1	1.3	9	10	10	ESE 2	E 4	E 3
16	97.7	97.7	96.4	97.3	-5.2	-4.6	-5.3	-5.1	-3.8	-5.9	83	67	70	73	0.7	1.4	1.2	1.1	10	10	10	NNE 7	NNE 10	N 8
17	90.6	88.9	89.9	89.8	-6.7	-5.2	-5.4	-4.7	-2.3	-7.2	91	95	70	85	0.3	0.2	1.4	0.6	10 ✳	10 ✳	10	N 12	NNE 10	NNE 10
18	91.9	94.5	95.9	94.1	-6.5	-0.3	-3.9	-3.6	1.0	-6.9	91	68	82	80	0.3	1.9	0.8	1.0	7 ⊙	5 ⊙	1	NW 6	NNW 6	NW 2
19	97.2	97.4	97.7	97.4	-8.5	-0.8	-3.7	-4.2	0.7	-8.7	95	58	73	75	0.2	2.4	1.2	1.3	4 ⊙	5 ⊙	1	N 1	NW 2	E 1
20	97.5	97.3	96.9	97.2	-6.7	0.7	-2.7	-2.8	2.0	-7.2	94	69	67	77	0.2	2.0	1.7	1.3	8	3 ⊙	0	E 2	SSE 3	SE 2
21	95.2	93.4	91.5	93.4	-6.9	-0.1	-3.2	-3.4	1.0	-8.1	77	61	81	73	0.8	2.4	0.9	1.4	5 ⊙	4 ⊙	6	ESE 3	E 5	E 4
22	88.6	87.3	85.8	87.2	-6.9	-2.3	-2.3	-3.4	-1.0	-7.1	91	80	83	85	0.3	1.0	0.9	0.7	10	10	10	NE 3	NNE 7	NE 6
23	84.8	85.5	87.0	85.8	-2.3	-0.5	-0.9	-1.2	0.5	-5.1	89	80	89	86	0.6	1.2	0.6	0.8	10 ♙	10 ✳	10 ✳	NE 4	N 6	N 5
24	89.5	92.7	96.3	92.8	-2.8	-1.3	-1.7	-1.9	0.0	-3.2	95	82	96	91	0.2	1.0	0.2	0.5	10 ✳	10	10 ✳	NW 4	NW 4	NW 2
25	98.7	98.2	96.6	97.8	-9.3	1.8	-1.8	-2.8	3.4	-10.3	95	58	81	78	0.2	2.9	1.0	1.4	5≡	4 ⊙	0	C 0	SW 1	E 1
26	95.1	93.7	91.4	93.4	-5.2	0.2	-2.7	-2.6	2.1	-5.6	95	60	67	74	0.2	2.5	1.7	1.5	0 ⊙	0 ⊙	0	E 1	E 3	ESE 4
27	87.3	84.3	82.1	84.6	-6.4	0.0	-1.9	-2.6	1.8	-8.1	75	71	73	73	0.9	1.8	1.4	1.4	10	6 ⊙	0	ESE 4	E 7	E 6
28	79.6	80.4	82.5	80.8	-1.5	3.8	1.2	1.2	7.6	-2.5	84	85	94	88	0.9	1.2	0.4	0.8	9	9	10	ESE 2	W 3	WSW 3
29	84.7	84.3	80.3	83.1	-0.5	3.8	2.2	1.9	7.2	-0.6	88	69	82	80	0.7	2.5	1.3	1.5	10	5 ⊙	10	W 5	W 4	SE 4
30	74.2	74.7	72.7	73.9	2.7	10.6	7.1	6.9	13.4	1.8	96	80	87	88	0.2	2.6	1.3	1.4	10	9	3	SE 3	SW 6	S 3
31	67.4	68.2	72.2	69.3	7.8	12.8	6.7	8.5	15.1	5.7	93	74	90	86	0.8	3.9	1.0	1.9	10	8	10 ●	S 6	SW 9	NE 1
M	87.7	87.8	87.9	87.8	-3.6	0.8	-1.2	-1.3	2.8	-4.5	90	73	85	82	0.5	1.8	0.9	1.1	8.4	7.6	6.5	3.6	5.2	3.4

Kwiecień - Avril

1	80.6	83.6	86.3	83.5	1.0	6.2	1.8	2.7	7.9	0.4	100	78	85	88	0.0	2.2	1.1	1.1	10≡	6 ⊙	0	S 3	W 9	SSW 2
2	86.2	86.8	90.6	87.9	2.2	7.5	2.4	3.6	9.8	0.7	86	63	91	80	1.1	3.9	0.7	1.9	10	9	0	SW 6	WSW 12	SW 4
3	90.4	88.1	84.8	87.8	2.9	12.2	7.8	7.7	14.6	0.8	86	45	64	65	1.0	7.9	3.8	4.2	10 ●	10 ⊙	0	SW 7	SW 9	S 6
4	80.3	78.2	75.0	77.8	6.2	15.3	9.5	10.1	16.6	4.5	60	37	75	57	3.8	10.9	3.0	5.9	8 ⊙	8 ⊙	10 ●	SE 8	SW 6	S 8
5	65.5	65.8	67.8	66.4	7.4	7.8	6.2	6.9	10.3	6.0	80	91	95	89	2.1	0.9	0.5	1.2	10 ●	10 ●	6	E 5	WSW 4	WSW 1
6	71.6	74.0	78.2	74.6	3.0	9.7	7.0	6.7	10.6	0.6	93	69	77	80	0.6	3.7	2.3	2.2	8	10	10	SSW 1	NW 2	N 2
7	84.0	86.9	87.2	86.0	2.8	4.2	0.3	1.9	7.8	0.0	84	60	80	75	1.2	3.3	1.2	1.9	9	9 ⊙	0	NW 9	NW 12	SW 3
8	84.3	85.0	85.0	84.8	4.2	9.2	9.2	8.0	11.3	0.1	97	79	74	83	0.2	2.4	3.0	1.9	10	9	9	SW 5	SW 9	S 5
9	87.1	90.3	92.4	89.9	8.1	11.2	5.0	7.3	12.7	4.9	79	50	78	69	2.3	6.6	1.9	3.6	7	10	0	SW 4	SW 6	S 1
10	96.2	97.5	99.3	97.7	3.4	9.9	7.5	7.1	11.6	0.7	95	51	72	73	0.4	6.0	3.0	3.1	8 ⊙	6 ⊙	10	W 2	NW 3	N 2
11	100.2	99.0	98.1	99.1	4.8	6.8	6.5	6.2	9.3	3.8	92	81	93	89	0.7	1.9	0.7	1.1	10 ●	10	10	N 3	NNE 5	N 2
12	96.3	95.6	93.8	95.2	4.8	11.9	9.2	8.8	14.6	3.2	97	68	84	83	0.3	4.4	1.8	2.2	7	6 ⊙	4	WNW 1	WNW 3	C 0
13	92.1	89.9	89.4	90.5	7.0	12.0	4.9	7.2	13.0	4.8	90	61	95	82	1.0	5.4	0.5	2.3	8	9	10 ●	NNE 2	ENE 3	N 7
14	90.3	94.5	99.4	94.7	2.4	3.8	4.5	3.8	5.8	2.0	96	97	95	96	0.3	0.3	0.4	0.3	10	10 ●	10	NNW 3	NW 6	N 4
15	100.4	100.3	99.6	100.1	4.8	7.6	9.0	7.6	10.8	4.3	98	91	92	94	0.1	0.9	1.0	0.7	10	10	10	NE 6	NE 7	NE 8
16	99.3	97.3	98.0	98.2	8.8	17.8	14.8	14.0	20.0	8.0	89	57	74	73	1.2	8.7	4.3	4.7	8	3	2	E 9	E 10	ESE 7
17	100.5	99.4	97.6	99.2	10.8	20.9	15.2	15.5	22.6	8.5	75	32	55	54	3.3	16.9	7.9	9.4	2	8	9	ESE 5	SE 12	ESE 5
18	95.5	94.2	93.1	94.3	10.9	21.1	15.4	15.7	22.3	10.3	70	38	59	56	3.8	15.4	7.2	8.8	9	10	10	SE 7	SE 9	SE 4
19	93.6	93.2	93.6	93.5	12.6	23.7	15.8	17.0	24.7	9.8	70	37	66	58	4.4	18.6	6.0	9.7	9 ⊙	9	9	SW 3	S 8	SSW 2
20	95.0	95.4	95.2	95.2	13.2	23.9	19.3	18.9	25.5	11.8	77	46	63	62	3.5	15.9	8.4	9.3	9	6	6	SW 2	C 0	C 0
21	96.9	96.8	96.8	96.8	14.0	25.0	19.6	19.6	26.6	12.0	77	30	53	53	3.7	22.2	10.7	12.2	0 ⊙	0 ⊙	9	C 0	SW 3	C 0
22	97.3	97.1	96.9	97.1	14.6	25.5	18.6	19.3	27.6	11.5	72	34	59	55	4.6	21.6	8.7	11.6	5 ⊙	5 ⊙	0	E 1	E 2	E 1
23	97.7	97.6	97.7	97.7	14.6	27.1	19.3	20.1	28.0	11.8	85	26	64	58	2.5	26.4	8.0	12.3	2 ⊙	1 ⊙	0	C 0	S 3	E 1
24	100.3	101.5	102.5	101.4	18.4	25.4	18.7	20.3	26.8	13.8	64	30	71	55	7.6	22.7	6.3	12.2	3 ⊙	1 ⊙	0	ENE 3	NE 5	NE 5
25	104.1	103.8	102.9	103.6	13.7	24.1	16.4	17.6	25.3	12.0	73	44	62	60	4.2	16.9	7.0	9.4	0 ⊙	1 ⊙	0	E 3	E 2	E 4
26	100.5	95.9	90.7	95.7	12.6	23.9	15.2	16.7	25.7	8.8	73	38	84	65	3.9	18.3	2.8	8.3	2 ⊙	1 ⊙	10	C 0	W 1	NW 1
27	86.1	86.7	88.0	86.9	10.7	9.6	5.5	7.8	16.3	5.4	91	73	86	83	1.2	3.3	1.2	1.9	10	9	0	W 2	WNW 9	NW 5
28	80.0	79.1	81.9	80.3	2.8	7.8	3.8	4.6	9.9	2.5	95	72	97	88	0.4	5.0	0.3	1.2	10 ●	9	8	W 8	NW 6	NW 3
29	83.5	83.9	84.1	83.8	3.9	8.4	3.8	5.0	9.1	3.0	87	52	92	77	1.1	5.3	0.7	2.4	9	6	10 ●	NW 5	N 5	S 1
30	85.1	87.6	90.5	87.7	1.0	4.0	0.4	1.4	6.6	0.1	98	66	82	82	0.2	2.8	1.1	1.4	9 ✳	9	3	N 2	N 5	N 2
31																								
M	90.7	90.8	91.2	90.9	7.6	14.1	9.8	10.5	16.1	5.5	84	57	77	73	2.0	9.5	3.5	4.9	7.4	7.0	5.5	3.8	5.9	3.2

Łódź-Lublinek $H_s = 187m$ $H_b = 187,7m$ $h_w = 11m$ Marzec - Mars 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	5	0.0	4	⛢°12^40-15^45; = 0^00-24
2	6	0.0	3	⛢°7^45-11^45; = 0^00-24
3	6	0.4	2	*°8^00...9^43; 21^48...23^20-24; = 0^00-24
4	6	2.4	1	*°0^00-2^45 •°15^48...16^45; 19^45...20^30-24; = 0^00-24
5	4	11.0	pż.	•°0^00-3^45 •°7^43-8^34 •°-9^35 •°...11^55 •°18^48-20^35 21^55...24; = 0^00-24
6	6	1.3	•	•°0^00...0^30-8^40 ⚥^1-2-10^10 ⚥°10^50-12^10 ⚥°-13^40 ⚥° 18^20-19^48 *°-20^30...22^20; 23^35...24; = 0^00-9^30
7	7	•	pż.	*°0^00-9^40
8	7	•	•	= 0^00-11^30; 19^30-24; ⌴°23^00-24
9	7	•	•	= 0^00-9^20; ⌴ 0^00-9^30
10	7	•	•	
11	7	1.2	•	= 14^30-24; ⌴°3^00-8^00
12	4	10.8	•	•°0^45...1^30-22^40 *°*°-24; = 0^00-6^30 ≡°-9^15 = -16^10 ≡°-1-22^20 = -24
13	5	0.5	3	*°0^00-20 *°-1-12^30 ⚥°-1...17^31; ⚥ 7^10-18^35; ⚲ 3^10-18^25; = 0^00-18^30
14	8	0.0	5	⚥°4^48-5^15; 7^45-58; 8^40-9^05; 12^30-13^00; 13^05-14^05
15	7	0.0	4	= 5^15-10^30
16	7	0.3	3	*°1^20...3^35; ⚲ 8^20-18^30; 22^10-24; = 6^30-11^00
17	3	1.1	5	*°-1 2^40-20^35; ⚥°2^40-5^40 ⚥-1-13^30; ⚲ 0^00-14^40; 19^30-24
18	8	•	25	⚥°0^00-5^30 ⚥°-7^30; ⚲ 0^00-6^20
19	8	•	11	= 2^30-3^50 ≡°-4^45 = -9^30; 18^20-24
20	7	•	pż.	= 0^00-11^30; 19^30-24
21	7	•	pż.	= 0^00-9^40
22	6	0.0	pż.	*°23^40-24; = 5^30-24
23	6	1.3	pż.	*°0^00...2^50; 4^40-5^50...6^00 ⛢°...7^15 *°-9^44; 10^42...12^43; 19^47...23^15-24; = 0^00-24
24	6	0.3	2	*°0^00-9^30...14^35; 15^49-16^30...18^15-21^28; = 0^00-22^35 ≡°-1-24
25	7	•	2	≡-2 0^00-2^35 ≡2-3^45 ≡2-5^42 ≡2-0-8^25 = -12^30; 17^20-24
26	7	•	•	= 0^00-10^30; ⌴°1^00-7^00
27	7	•	•	= 4^30-7^30; 17^35-24; ⊕ 6^15-8^35
28	6	0.4	•	•°9^45...11^40 ⚥°15^45-58 •°22^50-23^30...24; = 0^00-24
29	6	0.7	•	•°0^00...30; = 0^00-13^30; 17^20-24
30	6	0.6	•	•°0^45...1^25-4^20...5^40; 9^50...10^25; = 0^00-14^20; 18^30-19^15
31	7	16.7	•	•°0^50-5^15; 8^00...10^42 ⚥°19^50-20^10 •°...21^35 •°-1-24; = 4^35-10^30; 19^30-24
Σ	—	49.0	—	UWAGI:

Kwiecień - Avril

1	7	0.1	•	•°0^00-3^45 9^58...10^35 ⚥°17^35-40; = 0^00-6^15 ≡°-6^30 ≡-1°-7^49 = 10^00
2	7	1.6	•	⚥°9^45-10^10; 12^25-37 ⚥-1°15^28-16^12; ⚲ 10^55-13^20
3	7	0.0	•	•°6^42...8^35; ⊕ 10^40-12^30
4	8	1.7	•	•°19^48-23^35...24; ⚲ 4^40-5^30 9^30-12^20
5	5	1.2	•	•°0^00...7^15-10^30...14^34; = 11^30-14^30; 21^30-23^15
6	6	0.2	•	•°18^42...20^35 = 4^30-24; ⌴°4^00-7^00
7	8	0.8	•	⚥°0^45-2^25 •°23^50...24; ⚲ 7^30-17^15; = 0^00-6^30
8	7	0.0	•	•°0^00...0^30-2^45; 3^15-5^20; 8^42-10^44; 23^45...24; = 5^00-11^30
9	8	•	•	•°0^00...3^45
10	7	3.0	•	•°22^35-24; = 6^10-9^20
11	7	1.4	•	•°0^00-2^30...6^00 •°-1-9^40 •°13^50...14^35
12	7	•	•	= 3^30-9^30 19^20-24
13	7	12.1	•	⚥°-1 13^30-15^10 •°-1-24; = 0^00-24; ⌓°1^00-8^00
14	6	0.2	•	•°0^00-1^10...3^15-6^35; 7^05...13^45; = 10^30-24
15	6	•	•	⚥°1^40-4^35; = 0^00-40 ≡°-1^50 = -2^30 ≡°-5^45 = -24
16	7	•	•	⚲ 7^40-8^30; 9^10-16^35; = 0^00-11^20
17	8	•	•	⚲ 10^30-16^06
18	8	•	•	⚶ 21^50-24
19	7	•	•	⚶ 0^00-1^40; 22^30-24
20	6	•	•	= 5^30-10^15 ∞-21^30 = -24; ⚶ 0^00-3^20
21	7	•	•	= 0^00-7^15 ∞-9^30; 19^30-24; ⌓°2^00-7^30
22	7	•	•	= 0^00-8^30 ∞-10^40; ⌓°2^00-7^20
23	7	•	•	⌓°4^00-8^20
24	7	•	•	
25	7	•	•	
26	7	9.2	•	⚥°-1 16^40-17^03; (R) NW 16^25-R°16^40-17^03; (R) 17^26 SE
27	8	5.2	•	⚥°-1 0^03-2^40; 8^20-10^10; 13^50-14^00; 16^50-17^05; (R) SW 0^45-R°1^03-2^40; (R) 2^50 NE; = 4^30-10^10
28	8	1.3	•	⚥°-1 5^50-7^35 ⚥°10^35-11^15; 13^05-20; 15^40-48; 18^42-19^00
29	8	11.8	•	⚥°2^35-48; 13^48-57; 16^00...20^10 ⚥°-2 20^30-22^30 *'-23^20 *°-24
30	8	0.4	2	*°0^00-40 •°-2^35 *°5^30-6^30 ⚥°-7^25
31				
Σ	—	50.2	—	UWAGI:

144 657

Łódź - Lublinek φ = 51°44' λ = 19°24' Maj - Mai 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D.v I	II	III
1	89.3	86.6	85.0	87.0	-0.3	3.0	2.2	1.8	4.7	-2.2	84	72	93	83	1.0	2.1	0.6	1.2	9	9	10 ●	NW 2	WNW 6	W 4
2	82.0	82.3	85.5	83.3	2.3	7.8	2.7	3.9	9.9	1.3	93	65	89	82	0.5	3.7	0.8	1.7	10 ●	8	0	SW 4	SW 3	NW 2
3	87.2	87.2	85.9	86.8	1.8	8.0	5.6	5.2	10.7	-1.5	91	50	83	75	0.7	5.3	1.6	2.5	8	8	10 ●	SSW 1	SW 4	SW 2
4	81.7	82.3	85.9	83.3	4.2	7.8	4.0	5.0	10.0	3.2	95	78	88	87	0.4	2.4	0.9	1.2	9	8	8	W 7	W 7	NW 2
5	87.9	90.1	93.4	90.5	4.4	7.6	5.7	5.8	10.2	2.8	93	86	83	87	0.6	1.4	1.6	1.2	9	10 ●	2	SW 2	WNW 4	C 0
6	96.7	96.7	95.4	96.3	7.0	12.5	9.3	9.5	15.1	0.7	80	47	71	66	2.0	7.7	3.4	4.4	0 ⊙	4 ⊙	3	E 1	E 2	ESE 2
7	92.5	92.5	92.3	92.4	9.3	10.8	11.8	10.9	18.0	6.4	71	97	95	88	3.4	0.4	0.6	1.5	10	10 ●	10	SE 2	SW 2	C 0
8	91.4	89.8	88.9	90.0	13.3	21.6	14.8	16.1	22.6	10.8	99	54	91	81	0.2	11.9	1.5	4.5	4	6 ⊙	10 ● R	SW 2	W 7	W 3
9	89.4	91.0	88.9	89.8	12.6	16.9	13.4	14.1	19.7	12.5	93	63	78	78	1.1	7.2	3.3	3.9	9	6 ⊙	4	W 5	NW 5	C 0
10	85.9	86.7	88.1	86.9	12.0	12.6	10.6	11.4	15.6	10.6	93	93	96	94	1.0	1.1	0.5	0.9	10 ●	10 ●	8	C 0	SE 4	E 1
11	89.4	89.3	89.3	89.3	9.1	13.9	9.7	10.6	17.1	6.8	91	58	83	77	1.1	6.7	2.0	3.3	9	8	2	WNW 1	WNW 3	C 0
12	91.4	92.0	92.4	91.9	9.4	16.0	12.2	12.4	18.8	3.9	88	45	72	68	1.4	10.0	4.0	5.1	2	8	8	ESE 1	E 1	E 2
13	93.2	92.4	91.2	92.3	11.6	18.6	11.2	13.2	19.4	9.4	77	49	95	74	3.1	10.9	0.7	4.9	9	8 ●	10	E 1	SW 3	SW 3
14	82.9	76.5	74.6	78.0	11.3	12.6	7.9	9.9	13.6	7.9	96	95	97	96	0.5	0.7	0.2	0.5	10 ●	10 ●	10 ●	ENE 1	NE 1	W 12
15	75.9	79.0	82.7	79.2	7.8	8.6	8.4	8.3	9.8	6.9	96	89	89	91	0.5	1.3	1.2	1.0	10 ●	10 ●	10 ●	WNW 17	WNW 12	WNW 9
16	86.3	89.2	92.6	89.4	7.6	9.4	6.4	7.4	11.1	6.2	86	74	79	80	1.4	3.1	2.0	2.2	10 ●	10 ●	4	WNW 10	NW 10	W 5
17	91.6	90.0	89.1	90.2	8.0	14.0	10.3	10.6	15.6	4.3	75	62	85	74	2.7	6.1	1.9	3.6	9	9	9 ●	SW 4	WSW 7	SW 4
18	91.2	93.4	96.5	93.7	9.0	13.2	9.0	10.0	14.6	8.0	90	57	89	79	1.1	6.6	1.3	3.0	8	9	8	W 5	W 6	C 0
19	95.5	91.9	87.2	91.5	11.2	19.4	15.4	15.4	21.7	4.4	78	41	69	63	2.9	13.3	5.5	7.2	0 ⊙	4 ⊙	8	E 1	SE 6	ESE 4
20	86.3	88.6	90.9	88.6	11.2	10.0	8.2	9.4	16.4	8.2	90	95	94	93	1.3	0.7	0.6	0.9	10	10 ●	10 ●	W 9	WNW 6	NW 2
21	92.7	93.1	92.1	92.6	9.4	12.8	8.8	10.0	13.9	7.4	85	64	93	81	1.7	5.4	0.8	2.6	9	10	10	NW 2	N 5	NE 3
22	91.1	90.2	92.5	91.3	9.2	16.4	10.9	11.8	18.4	7.7	91	49	87	76	1.1	9.4	1.6	4.0	8	8 ⊙	9	C 0	SSE 4	SW 2
23	95.7	94.0	93.0	94.2	11.4	18.0	15.0	14.8	20.0	7.8	85	55	72	71	2.0	9.2	4.7	5.3	8 ⊙	8	9	SW 2	SW 6	S 1
24	95.5	95.6	94.4	95.2	11.2	14.2	8.9	10.8	15.8	8.8	88	55	93	79	1.7	7.3	0.8	3.3	10	10	10 ⊙	WNW 4	SW 2	NW 3
25	92.1	92.2	91.9	92.1	8.6	13.4	11.6	11.3	14.6	7.6	92	62	74	76	1.0	5.8	3.6	3.5	10	9	10	NW 1	NE 3	E 3
26	89.4	87.2	89.0	88.5	9.4	11.7	11.9	11.2	13.7	8.8	93	91	90	91	0.8	1.1	1.3	1.1	10 ●	10	8	NE 3	ENE 4	SSW 2
27	92.4	94.3	94.7	93.8	8.6	14.2	11.2	11.3	15.8	7.0	97	59	92	83	0.3	6.6	1.0	2.6	9	9	8	WSW 2	SW 1	C 0
28	94.5	93.2	89.6	92.4	11.0	16.2	15.6	14.6	18.1	6.1	100	71	92	88	0.0	5.2	1.3	2.2	10	9	8 (R)	E 1	E 3	SE 3
29	93.6	93.9	94.5	94.0	11.1	17.2	12.2	13.2	19.1	10.0	84	47	80	70	2.1	10.4	2.9	5.1	8	6	8	W 4	SW 6	C 0
30	95.0	94.8	95.1	95.0	10.7	15.2	11.1	12.0	17.2	9.8	81	62	81	75	2.5	6.5	2.4	5.1	10	7 (R)	4	WSW 2	W 7	C 0
31	93.8	90.2	87.9	90.6	11.8	18.0	12.6	13.8	20.8	9.3	81	41	77	66	2.6	12.0	3.4	6.0	9	8	7	E 1	SSW 6	NNW 6
M	90.1	89.9	90.0	90.0	8.9	13.3	10.0	10.6	15.5	6.5	88	65	85	79	1.4	5.9	1.9	3.1	8.3	8.4	7.6	3.1	4.7	2.6

Czerwiec - Juin

1	92.1	94.2	92.7	93.0	7.0	9.8	8.8	8.6	13.2	7.0	70	61	75	69	3.0	4.8	2.9	3.6	10	10	10	W 8	W 7	C 0
2	93.4	95.3	97.8	95.5	5.7	10.2	7.8	7.9	10.7	4.9	97	75	89	87	0.3	3.1	1.2	1.5	10 ●	10	4	NNW 2	S 1	C 0
3	99.5	100.6	101.2	100.4	7.4	11.4	7.6	8.5	13.8	3.0	91	48	83	74	0.9	7.0	1.7	3.2	4 ⊙	8	5	NNW 3	NW 6	C 0
4	101.0	100.6	99.9	100.5	6.9	7.6	8.3	7.8	10.3	3.8	92	90	94	92	0.7	1.0	0.7	0.8	10	10 ●	10 ●	NNW 5	NNW 7	NNW 3
5	98.3	99.3	100.1	99.2	7.1	8.4	8.0	7.9	10.3	6.2	73	94	87	85	2.8	0.6	1.3	1.6	8	10 ●	9 ●	NNW 9	NNW 7	NW 6
6	100.5	101.3	101.9	101.2	7.1	12.4	9.2	9.5	14.1	4.3	70	38	62	57	3.1	9.0	4.4	5.5	9 ⊙	6 ⊙	8	NNW 9	N 14	N 7
7	103.6	105.2	104.5	104.4	6.8	10.4	9.6	9.1	14.7	4.3	72	63	67	67	2.7	4.7	4.0	3.8	10	9	8	NNE 10	NNE 9	N 2
8	105.2	104.1	102.2	103.8	10.2	17.8	12.6	13.3	19.6	4.4	75	46	73	65	3.1	11.0	3.9	6.0	2 ⊙	6 ⊙	3	N 2	NNE 3	C 0
9	97.3	93.9	91.4	94.2	13.6	20.6	14.4	15.8	22.6	6.9	66	41	79	62	5.4	14.2	3.4	7.7	2 ⊙	6 ⊙	2	W 1	W 6	N 2
10	91.2	90.3	88.7	90.1	12.7	18.5	14.8	15.2	20.9	9.3	47	35	62	48	7.9	13.8	6.4	9.4	1 ⊙	1 ⊙	2	ENE 3	N 1	E 1
11	86.8	85.3	86.6	86.2	13.4	18.4	12.0	14.0	19.8	11.0	75	64	76	72	3.8	7.6	3.3	4.9	10	8 ⊙	6	WNW 3	W 4	NW 4
12	89.2	90.1	92.1	90.5	10.9	13.6	10.2	11.2	15.6	9.4	73	54	90	72	3.5	7.2	1.2	4.0	9	8	9	WNW 3	W 6	W 1
13	94.8	94.8	94.8	94.8	11.4	16.6	13.2	15.6	19.1	7.1	73	45	68	62	3.6	10.4	4.8	6.3	2 ⊙	6 ⊙	1	NW 2	WNW 4	C 0
14	94.2	92.8	92.9	93.3	11.8	21.0	17.8	17.1	23.8	7.6	78	49	66	64	3.0	12.8	6.9	7.6	6	8 ⊙	5	E 1	S 3	C 0
15	95.9	97.4	97.8	97.0	17.6	24.6	20.2	20.6	27.0	14.0	77	38	66	60	4.5	19.2	8.1	10.6	8 ⊙	6	1	NW 1	NW 5	E 1
16	97.8	96.6	95.1	96.5	21.0	28.8	22.2	23.6	30.2	13.0	63	34	65	54	9.1	26.1	9.5	15.0	0 ⊙	0 ⊙	10 (R)	SSE 3	S 3	W 4
17	97.3	98.5	98.6	98.1	18.0	22.8	16.8	18.6	23.5	16.1	90	53	73	73	2.0	12.9	4.8	6.6	9	4 ⊙	2	NW 4	NW 6	N 3
18	98.8	98.0	96.2	97.7	16.4	21.1	16.8	17.8	24.2	10.6	71	53	70	65	5.4	11.8	5.7	7.6	4 ⊙	4 ⊙	0	C 0	NE 1	E 2
19	95.1	93.3	90.4	92.9	18.0	25.0	20.9	21.2	28.0	11.6	66	35	59	53	6.9	20.5	10.2	12.5	0 ⊙	2 ⊙	5	SE 2	S 3	SE 2
20	92.8	95.2	95.3	94.4	16.9	21.0	18.0	18.5	23.2	15.8	91	49	69	70	1.8	12.6	6.3	6.9	10	8	8	W 6	NW 5	SW 1
21	97.9	97.2	98.4	97.8	16.6	22.9	17.8	18.8	25.2	12.2	76	48	76	67	4.6	14.6	4.8	8.0	9	9	8	S 1	WSW 5	NW 2
22	100.6	100.5	99.1	100.1	17.4	24.0	21.5	21.1	25.9	12.3	86	47	68	67	2.8	15.8	8.2	8.9	1 ⊙	4 ⊙	3	WSW 1	WSW 4	C 0
23	98.4	96.9	94.8	96.7	20.6	27.3	21.7	22.9	29.3	14.2	71	45	78	65	6.9	20.2	5.8	11.0	0 ⊙	3	9	S 1	WSW 3	NE 2
24	96.3	95.2	91.3	94.3	17.4	23.6	22.4	21.4	26.4	14.3	90	60	73	74	2.1	11.7	7.4	7.1	4 ⊙	8	4	WNW 1	SW 2	SE 1
25	93.3	94.3	96.7	94.8	15.6	19.6	12.5	15.0	22.4	12.3	75	42	70	62	4.4	13.2	4.4	7.3	10	4 ⊙	1	NW 7	W 4	W 2
26	96.1	93.9	90.1	93.4	11.9	17.0	14.6	14.5	20.0	7.2	61	46	69	59	3.3	10.6	5.2	7.0	2 ⊙	7 ⊙	0	NW 3	W 5	E 1
27	88.7	89.0	90.1	89.3	12.2	16.6	9.9	12.2	17.4	9.8	81	49	76	69	2.6	9.6	3.0	5.1	8	7	4	W 6	W 8	W 3
28	89.6	88.8	85.5	88.0	9.5	11.9	8.4	9.6	14.6	6.9	78	54	94	73	2.7	6.4	0.6	3.2	7	9	10	W 7	WSW 7	SW 3
29	85.9	87.0	88.6	87.2	8.7	13.2	11.2	11.1	14.0	7.3	90	73	80	81	1.0	4.2	2.6	2.6	10	9	10	W 8	WNW 9	W 9
30	88.5	90.3	91.7	90.2	8.8	10.2	11.5	10.5	15.1	8.3	96	92	93	94	0.4	0.9	1.0	0.8	10	10	10	W 6	W 7	W 4
31																								
M	95.3	95.3	94.9	95.2	12.6	17.6	14.0	14.6	19.8	9.2	77	54	75	69	3.3	10.6	4.3	6.2	6.2	6.7	5.6	4.0	5.4	2.3

Łódź-Lublinek $H_s = 187m$ $H_b = 187,7m$ $h_w = 11m$ Maj - Mai 1962

DNI	WIEDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	3.3	•	*6^{50}-7^{10} ⚲°... 11^{25} ⚲° 12^{50}-13^{15} ⚲° 13^{21}-14^{17} •° 15^{10}... 21^{35} ⌣° 4^{00}-7^{00}
2		1.6	•	⚲° 0^{40}-1^{45} •° 4^{30}... 7^{05} ⚲° $^{0-1}$-7^{47} ⚲° 8^{05}... 17^{35}; = 4^{55}-9^{05}
3	8	5.8	•	⚲° 8^{00-20}, 16^{43}-17^{10} •° 19^{05}-24; = 2^{30}-9^{40}, ⌣ $^{0-1}$ 2^{00}-6^{00}
4	8	1.3	•	•° 0^{00}-5^{55} ⚲° 8^{07}... 14^{03} 21^{30-45} 22^{35-42}; ≫ 11^{50}-12^{06}; = 5^{53}-8^{50}
5	7	0.0	•	⚲° 1^{35-45} 7^{15}...^{27}; 12^{35}-13^{00}; = 3^{20}-8^{00} 19^{10}-24; ⌓ $^{0-1}$ 19^{30}-24
6	8	•	•	= 0^{00}-7^{40}, 23^{30}-24; ⌓ 0^{00}-3^{30} ⌣ $^{1-0}$ 6^{30}
7	4	3.2	•	•° 6^{50}-7^{10} 9^{20}-11^{25} ⚲° -12^{10} •° -12^{33} •° -13^{42} ⚲° $^{0-1}$ 16^{45}-17^{35}; ([R])NW 17^{20}-[R]° 17^{23-35}-([R]) 17^{45} SE; = 0^{00}-24
8	7	3.1	•	•° 1^{12}...^{45} ⚲° $^{0-1}$ 17^{42}-18^{05} ⚲ 19^{15}-22^{17}; 22^{50}-23^{30}; ([R])SW 17^{32}-[R] 17^{42}-18^{06} ([R]) 18^{15} SE; ([R])W 19^{38}-[R]° 19^{40}-22^{02}-([R]) 22^{10} NE; = 0^{00}-5^{15} ▬ $^{0-1}$ 6^{25} = 10^{15}; 18^{20}-24
9	8	0.6	•	⚲° 6^{18-30}; = 0^{00}-9^{15}; ⌓° 20^{30}-24
10	5	10.4	•	⚲ $^{1-0}$ 5^{35}-6^{00} •° -11^{45} •° $^{0-1}$ -12^{00}... 12^{25}-14^{15}; = p, np-np; ⌓ $^{0-1}$ na, np
11	7	•	•	= 22^{30}-24; ⌓ $^{0-1}$ 0^{00}-8^{00} ⌓° 22^{30}-24
12	8	0.0	•	= 0^{00}-8^{20}; ⌓ $^{0-2}$ 0^{00}-10^{00}
13	7	12.9	•	⚲° 1^{15-25}, 1^{30-40} ⚲ $^{0-1}$ 14^{15}...21^{20} •° 23^{45}...24; = a, np
14	6	49.4	•	•° 0^{00}...2^{20} •° $^{0-1}$ -11^{10}...12^{48}-24; ≫ 19^{20}-24; = 0^{00}-24
15	6	21.0	•	•° $^{0-1}$ 0^{00}-21^{40}; ≫ - ⚑ 0^{00}-19^{50}; = 0^{00}-22^{00}
16	7	1.9	•	⚲° 6^{40}-7^{00} •° -9^{45} ⚲° 9^{58}...14^{35}; ≫ 0^{00}-15^{45}
17	7	0.2	•	⚲° 18^{45}-19^{12} 19^{28}-21^{10}
18	7	0.0	•	⚲° 11^{12-17}; 13^{08-14}; 15^{35-58}; ([R])NW 15^{30}-[R]° 15^{40-45} ([R]) 16^{05} E; = 20^{30}-24; ⌓ $^{0-1}$ 19^{50}-24
19	8	0.0	•	= 0^{00}-7^{45}; ⌓ $^{0-2}$ 0^{00}-10^{00}
20	6	14.5	•	•° 4^{50}...10^{40}-18^{30}...22^{35}; = 8^{30}-18^{20}
21	7	0.9	•	⚲° 14^{46}-15^{25} •° ...16^{10}-19^{50}; = 2^{30}-7^{30}
22	7	0.1	•	•° 0^{15}-1^{52} ⚲° 19^{42-46}; = 4^{20}-7^{30}; 13^{30}-17^{30}, np
23	7	0.1	•	= 0^{00}-8^{30}; ⌓° 21^{30}-24
24	7	6.4	•	•° 3^{45}...4^{40}, 15^{47}...18^{30}-24; = 4^{40}-7^{30}; ⌓° 0^{00}-3^{45}
25	7	11.6	•	•° 0^{00}-3^{30}...4^{35}, 21^{50}...22^{30}-24; = 2^{50}-10^{40}
26	6	4.6	•	•° 0^{00}-5^{35}...12^{42} •° 13^{45}-17^{10}; = 8^{48}-24
27	7	0.0	•	•° 17^{35}...19^{30}; = 0^{00}-12^{30} 21^{20}-24
28	7	2.0	•	⚲ $^{0-1}$ 20^{15}-21^{07}; ([R])SW 19^{30}-[R]° 20^{25}-21^{02} ([R]) 21^{46} NE; = 0^{00}-9^{40}, 14^{40}-24
29	8	1.7	•	= 0^{00}-8^{30}
30	7	0.0	•	•° 2^{50}...6^{25} ⚲° 14^{15-17}; 14^{40-58}; ([R])WNW 13^{40}-[R]° 14^{15-30}-([R]) 14^{35} E; = 2^{20}-12^{30}, 20^{40}-24
31	7	0.0	•	•° 1^{50}-2^{35}; = 0^{00}-12^{30} ∞ -13^{30} = -24
Σ	—	156.6	—	UWAGI.

Czerwiec - Juin

1	8	2.2	•	•° 2^{50}...3^{40}; = 0^{00}-5^{30}
2	8	0.3	•	⚲° 1^{45}-3^{40} •° -7^{40}...8^{00}-11^{00}...11^{46} ⚲° 12^{38}...14^{25}
3	8	0.1	•	⚲° 15^{50}-17^{02}; ⌓ $^{0-1}$ 2^{00}-10^{00}
4	7	5.0	•	⚲° 9^{50}-10^{05}; 12^{03-15}; 12^{40}-14^{03} •° $^{0-1}$ -22^{25}; = 5^{30}-8^{30}
5	6	15.2	•	•° 4^{05}-5^{10} •° $^{0-1}$ 8^{35}-14^{30}...16^{20}-18^{10}...19^{20} ⚲° 19^{30-45}; 20^{15}-21^{10} •° 21^{30}...^{50}
6	8	0.5	•	⚲° 19^{45}-20^{05}; 22^{15-40}; ≫ 8^{10}-20^{20}
7	8	•	•	⚲° 2^{15}-4^{35}; ≫ 7^{40}-8^{15}
8	8	•	•	= 7^{20}-8^{40}; ⌓° 3^{00}-8^{30}; 23^{00}-24
9	8	•	•	⌓ $^{0-1}$ 0^{00}-8^{00}
10	8	•	•	⌓° 2^{00}-7^{30}
11	7	4.0	•	•° 8^{35}-9^{45} ⚲ $^{1-0}$ 14^{22}-15^{02}; ([R])W 14^{16}-[R] 14^{22}-15^{17} E
12	8	0.5	•	⚲° 21^{55}-22^{20}; 22^{35}-23^{10}
13	7	•	•	= 5^{20}-7^{30}; ⌓° 21^{00}-24
14	7	•	•	= 5^{30}-8^{30}; ⌓° 0^{00}-8^{00}
15	7	•	•	= 4^{00}-8^{40}; ⌓° 4^{00}-8^{30}; 23^{30}-24
16	7	0.1	•	⚲° 23^{05-50}; ([R])SW 21^{42}-[R] 23^{05-55} SE; = 4^{30}-8^{40}; ⌓° 0^{00}-8^{30}
17	7	•	•	⚲° 2^{40-54}; ([R])W 2^{20}-[R] 2^{48}-3^{50} SE; = 3^{35}-11^{30}; 21^{30}-24
18	7	•	•	= 0^{00}-9^{30} ∞ -10^{30}; ⌓° 2^{00}-7^{00}
19	7	1.0	•	⌓° 1^{30}-7^{30}
20	8	•	•	⚲° 3^{40}-4^{20}; = 5^{20}-8^{30}
21	7	•	•	= 3^{30}-8^{40}; ⌓° 2^{00}-8^{00}
22	7	•	•	= 2^{30}-9^{20}, 21^{30}-24; ⌓ $^{0-1}$ 2^{00}-8^{00} ⌓° 21^{30}-24
23	7	30.7	•	⚲° 22^{45}-23^{20} ▲ $^{0-2}$ 22^{50}-23^{17}; ([R])SW 21^{50}-[R] ^{2} 22^{43}-23^{20}-([R]) 24 NE; = 0^{00}-9^{40}; ⌓° 0^{00}-8^{30}
24	7	•	•	⚲° 2^{10-20}; ([R])SW 0^{00}-[R] 2^{10-20}-([R]) 2^{35} NE; = 3^{20}-9^{30}; 23^{30}-24
25	8	•	•	≫ 13^{00}-16^{30}; 17^{20}-19^{25}; = 0^{00}-7^{15}; ⌓° 2^{00}-8^{00}
26	8	0.3	•	⌓° 2^{00}-8^{00}
27	7	•	•	⚲° 5^{50-58}; = 5^{50}-7^{20}
28	8	2.4	•	⚲° 16^{25}...20^{35}; ≫ 18^{10-30}
29	7	15.6	•	⚲ 0^{55}...3^{14} ⚲ $^{2-0}$ 12^{32}...18^{16} •° 19^{47}...20^{46}; ▲ ^{2} 12^{42-60}
30	6	5.4	•	⚲ 5^{42}-6^{20} •° -7^{42}, 10^{40}...13^{30} ⚲° 14^{15}...24; = 7^{42}-22^{30}
31				
Σ	—	82.3	—	UWAGI.

Łódź - Lublinek φ = 51°44' λ = 19°24' Lipiec - Juillet 1962

DNI	CIŚNIENIE P-900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N.w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D.v I	II	III
1	93.1	94.1	93.6	93.6	10.7	13.0	9.8	10.8	15.6	9.8	94	77	93	88	0.9	3.5	0.8	1.7	9	9	9	WNW 3	W 2	C 0
2	92.1	90.6	88.3	90.3	9.4	15.8	9.7	11.2	17.1	8.5	95	63	87	82	0.6	6.6	1.6	2.9	10 ●	7	8	WSW 1	W 5	S 1
3	81.6	79.8	79.0	80.1	10.4	11.9	9.4	10.3	14.3	9.0	95	87	85	89	0.6	1.8	1.7	1.4	10 ●	6 ⊙	8	W 3	WSW 6	WSW 2
4	78.8	79.1	80.9	79.6	8.8	12.2	10.9	10.7	13.9	7.3	85	56	70	70	1.7	6.2	3.8	3.9	9	10	10	SW 5	SW 7	SW 6
5	83.4	85.0	87.2	85.2	10.2	14.2	12.2	12.2	16.6	9.1	82	65	83	77	2.2	5.6	2.4	3.4	10	10	10	SW 4	SW 3	S 2
6	91.2	91.9	93.1	92.1	10.9	17.0	10.8	12.4	19.6	8.5	86	52	92	77	1.8	9.4	1.0	4.1	9	9	9(R)	SW 2	SW 3	C 0
7	94.1	93.4	94.1	93.9	11.2	17.3	12.0	13.1	18.7	7.3	90	51	82	74	1.3	9.5	2.5	4.4	9	5 ⊙	10	SW 1	SW 4	W 2
8	95.4	95.8	96.7	96.0	10.6	12.6	11.6	11.6	16.4	9.8	95	84	94	91	0.7	2.4	0.8	1.3	10	9	7	W 2	WNW 5	W 2
9	98.4	97.6	96.0	97.3	10.6	17.8	12.6	13.4	18.9	8.3	99	55	86	80	0.2	9.2	2.1	3.8	10	8	1	WSW 4	W 4	C 0
10	94.1	92.9	91.0	92.7	13.2	20.0	14.4	15.5	22.0	6.5	79	42	76	66	3.2	13.6	3.9	6.9	0 ⊙	4 ⊙	3	W 1	NW 8	N 1
11	90.4	88.5	86.0	88.3	14.9	22.2	18.1	18.3	25.2	8.5	79	41	71	64	3.4	15.8	6.0	8.4	2 ⊙	5	7	W 2	W 3	C 0
12	85.7	86.0	85.6	85.8	14.7	20.8	13.8	15.8	23.5	13.7	92	57	95	81	1.3	10.6	0.7	4.2	9	5	8	W 3	W 8	SW 1
13	85.0	84.9	85.2	85.0	13.6	14.2	12.0	13.0	17.6	12.0	90	87	95	91	1.6	2.2	0.7	1.5	10 ●	9	7	SW 3	SW 3	W 2
14	85.3	85.3	85.2	85.3	12.4	14.9	13.3	13.5	17.8	11.5	95	79	90	88	0.7	3.4	1.6	1.9	9	10	10	WSW 4	WSW 4	W 4
15	84.7	84.0	84.0	84.2	12.8	19.2	15.8	15.9	22.5	11.6	98	58	85	80	0.4	9.2	2.6	4.1	9	7 ⊙	9	W 1	N 1	C 0
16	84.6	85.7	85.8	85.4	15.4	19.2	16.6	17.0	21.8	14.0	91	69	85	82	1.5	7.0	2.9	3.8	9 ●	8	8	E 2	E 3	NE 3
17	89.9	90.8	92.2	91.0	16.0	20.6	15.5	16.9	22.4	12.7	71	55	78	68	5.2	10.8	3.9	6.6	7	6 ⊙	5	E 6	NE 4	NNE 3
18	92.9	92.2	92.2	92.4	16.3	20.4	15.8	17.1	22.2	11.4	72	50	77	66	5.1	12.0	4.1	7.1	5 ⊙	8	8	E 2	NE 5	N 3
19	92.4	92.7	94.0	93.0	14.2	21.2	16.8	17.2	23.0	13.0	87	60	87	78	2.2	10.2	2.5	5.0	9	9	9	NNW 4	N 7	NW 1
20	95.5	95.0	94.7	95.1	15.4	24.2	20.8	20.3	26.2	11.0	89	40	65	64	1.9	18.2	9.0	9.7	5 ⊙	3 ⊙	10	NW 1	W 1	C 0
21	95.0	92.8	92.2	93.3	18.3	27.0	22.8	22.7	29.0	13.8	71	40	55	55	6.0	21.5	12.5	13.3	0	4 ⊙	8	C 0	SSE 5	SE 3
22	93.8	94.3	94.3	94.1	19.2	22.8	18.4	19.7	27.5	17.4	85	75	79	80	3.4	6.8	4.5	4.9	9	6 ⊙	10 ● R	W 2	W 3	NW 10
23	96.1	97.3	98.6	97.3	17.4	22.2	17.0	18.4	24.2	15.7	93	51	78	74	1.5	13.2	4.3	6.3	9	7	8	WNW 2	NW 6	WNW 1
24	100.3	100.8	101.2	100.8	14.2	18.6	13.7	15.0	20.9	10.3	82	51	79	71	2.9	10.5	3.4	5.6	8	8	0	W 4	WNW 8	C 0
25	102.4	100.8	98.7	100.6	14.2	20.8	17.6	17.6	24.2	8.6	75	48	65	63	4.1	12.7	7.0	7.9	6 ⊙	4 ⊙	4	C 0	NW 1	E 2
26	96.1	95.9	91.6	95.9	19.1	29.9	24.2	24.4	32.1	12.7	68	37	64	56	7.2	26.7	10.8	14.9	1 ⊙	0 ⊙	9	SE 4	S 4	S 1
27	92.5	93.2	92.9	92.9	21.0	23.0	18.7	20.4	26.2	18.6	85	65	76	75	3.9	9.7	5.2	6.3	4 ⊙	9	2	SW 2	SW 3	W 5
28	95.8	96.0	96.8	96.2	13.2	15.6	11.2	12.8	20.0	10.9	78	83	92	84	3.3	3.0	1.0	2.4	4 ⊙	6 ⊙	4	WNW 9	NW 6	C 0
29	98.2	97.5	97.4	97.7	11.4	18.8	12.1	13.6	21.0	4.8	88	49	73	70	1.7	11.0	3.8	5.5	2 ⊙	4 ⊙	2	NNW 2	N 2	C 0
30	98.9	98.3	98.0	98.4	13.4	18.7	12.2	14.1	21.5	7.0	82	48	82	71	2.8	11.2	2.5	5.5	9	8	3	E 1	E 1	E 2
31	99.2	97.9	96.5	97.9	15.2	22.2	17.2	18.0	23.6	8.8	70	37	59	55	5.1	17.0	8.0	10.0	2	5 ⊙	4	E 1	SW 1	C 0
M	92.2	91.9	91.7	91.9	13.8	19.0	14.7	15.6	21.5	10.7	85	58	80	74	2.5	10.0	3.8	5.4	6.9	6.7	6.8	2.6	4.1	1.8

Sierpień - Août

1	95.0	94.7	94.8	94.8	14.5	19.6	14.8	15.9	22.1	12.7	79	62	71	71	3.4	8.6	4.8	5.6	8	9	2	C 0	WNW 9	C 0
2	94.7	94.1	92.9	93.9	13.4	21.1	16.2	16.7	23.5	9.2	84	43	76	68	2.5	14.3	4.4	7.1	2 ⊙	6 ⊙	0	SW 2	NW 4	C 0
3	92.1	92.0	93.1	92.4	15.6	23.0	18.4	18.8	25.6	11.5	78	52	83	71	3.9	13.5	3.7	7.0	9	7 ⊙	8	C 0	E 1	C 0
4	93.0	91.9	92.1	92.3	17.4	26.9	19.2	20.7	28.8	14.7	88	49	93	77	2.4	18.0	1.5	7.3	9	4 ⊙	8	E 2	S 4	SE 1
5	92.6	89.3	87.3	89.7	16.5	27.3	17.8	19.8	29.1	13.8	99	42	94	78	0.2	20.9	1.2	7.4	9	9 ⊙	9	C 0	SSE 4	C 0
6	88.8	90.1	90.0	89.6	15.8	18.8	18.8	18.0	22.0	15.3	95	77	79	84	0.9	4.9	4.5	3.4	8	9	8	W 4	W 3	ESE 1
7	85.8	81.6	85.8	84.4	19.1	30.4	16.8	20.8	31.6	15.3	89	38	93	73	2.3	26.9	1.4	10.2	6 ⊙	7 ⊙	9 ●	E 2	SSE 9	W 6
8	91.8	93.6	95.7	93.7	14.0	21.1	15.0	16.3	23.0	13.5	81	46	72	66	3.0	13.6	4.7	7.1	4 ⊙	5 ⊙	2	SW 5	SW 9	SW 2
9	100.5	100.9	101.2	100.9	12.8	20.3	14.0	15.3	21.6	11.0	79	46	77	67	3.1	12.8	3.7	6.5	9	4 ⊙	2	W 1	W 4	C 0
10	100.6	97.4	94.1	97.4	14.0	23.2	17.6	18.1	24.9	8.4	77	34	71	61	3.7	18.6	5.9	9.4	2 ⊙	5	7	E 1	SSW 6	S 1
11	94.1	93.5	94.2	93.9	16.4	22.6	17.4	18.4	25.0	13.4	82	47	65	65	3.2	14.5	7.0	8.2	9	7	5	W 3	SW 7	C 0
12	95.7	95.2	94.1	95.0	15.4	27.0	21.4	21.6	29.3	12.0	78	39	69	62	4.0	21.7	8.0	11.2	0	4	0	S 1	SW 4	C 0
13	94.7	94.8	94.7	94.7	19.7	29.5	21.4	23.0	30.6	15.5	76	42	70	63	5.5	24.0	7.6	12.4	6	6 ⊙	0	C 0	NNW 2	NE 1
14	96.5	96.3	95.2	96.0	16.2	17.8	16.5	16.8	21.6	15.7	98	86	83	89	0.4	2.8	3.3	2.2	10	10	10	SE 1	NE 1	NE 2
15	92.2	89.7	86.5	89.5	15.6	21.6	20.2	19.4	25.3	13.7	85	85	89	86	2.6	3.9	2.7	3.1	10	9	10	E 5	SSE 4	SE 1
16	87.3	88.8	90.4	88.8	17.2	23.6	17.6	19.0	24.2	16.3	92	63	82	79	1.6	10.8	3.6	5.3	9	6	1	SW 3	W 4	C 0
17	91.5	90.7	89.5	90.6	15.8	25.0	16.0	18.2	26.6	12.4	90	49	96	78	1.7	16.2	0.8	6.2	3	6 ⊙	10	E 1	S 2	C 0
18	87.0	89.8	91.9	89.6	15.0	17.1	13.4	14.7	18.8	13.4	100	79	84	88	0.0	4.1	2.5	2.2	10 ≡	9	6	S 2	W 7	W 3
19	91.3	92.0	92.4	91.9	12.4	12.6	12.0	12.2	14.1	11.3	82	88	93	88	2.6	1.7	1.0	1.8	9	9	10	W 7	W 7	W 3
20	91.1	92.5	93.2	92.3	13.3	15.0	14.8	14.5	18.3	11.8	94	87	96	92	0.9	2.2	0.7	1.3	10	10	10	WNW 9	NW 9	NW 4
21	92.7	92.6	91.4	92.2	14.4	17.4	15.8	15.8	21.4	13.3	85	71	80	79	2.5	5.9	3.5	4.0	9	8	5	NNW 2	NNW 2	E 2
22	91.7	93.8	93.7	93.1	14.0	17.4	14.3	15.0	20.0	12.3	98	74	90	87	0.4	5.1	1.6	2.4	10 ●	7	7	SW 2	WNW 7	SW 1
23	92.7	94.7	94.8	94.1	14.0	17.6	12.0	13.9	17.7	12.0	79	60	83	74	3.4	8.1	2.3	4.6	6	9 ⊙	0	W 7	NW 9	W 2
24	92.0	87.7	86.9	88.9	13.2	17.4	16.1	15.7	18.0	10.5	79	79	97	85	3.2	4.2	0.6	2.7	10 ●	10	10 ●	S 2	SW 9	W 5
25	90.0	91.0	93.3	91.4	13.0	17.5	14.8	15.0	18.1	12.5	91	61	71	74	1.4	7.9	4.8	4.7	4 ⊙	10	9	WSW 4	W 7	W 5
26	96.5	98.1	97.7	97.4	12.2	17.8	11.7	13.4	18.5	10.3	83	55	83	74	2.4	9.2	2.3	4.6	4	6 ⊙	0	WSW 6	WSW 8	S 1
27	93.3	89.8	90.7	91.3	14.2	23.4	18.0	18.4	25.1	9.1	67	41	73	60	5.3	16.9	5.6	9.3	0 ⊙	4 ⊙	6	SSE 5	SW 8	W 9
28	95.3	96.3	96.7	96.1	12.6	15.7	12.1	13.1	19.1	10.5	74	55	80	70	3.7	7.9	2.8	4.8	8 ⊙	8 ⊙	9	W 9	W 9	W 3
29	95.8	93.9	93.9	94.5	12.2	19.4	13.8	14.8	21.7	8.3	82	48	93	74	2.5	11.7	1.1	5.1	9	9	10	SW 3	WSW 7	WNW 6
30	96.5	98.0	97.2	97.2	10.8	14.1	9.0	10.7	15.6	9.0	95	62	88	82	0.7	6.1	1.4	2.7	10	9	0	WNW 5	WNW 8	W 2
31	92.1	90.4	92.1	91.3	10.6	13.3	11.6	11.8	17.1	7.8	82	68	85	78	2.3	5.0	1.9	3.1	9	10	9	SW 5	W 9	W 6
M	93.1	92.7	92.8	92.9	14.6	20.3	15.8	16.7	22.5	12.1	85	59	83	76	2.4	11.0	3.3	5.6	7.1	7.5	5.9	3.2	5.9	2.2

Łódź-Lublinek $H_s = 187m$ · $H_t = 187{,}7m$ $h_w = 11m$ Lipiec - Juillet 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	7	1.6	.	$\overset{*}{\bigtriangledown}{}^{\circ}0^{00-15}\bullet^{\circ-1}0^{30}-2^{50}\ldots3^{42}\overset{*}{\bigtriangledown}{}^{1-0}10^{35}-11^{00}\bullet^{\circ}-12^{00};=0^{00}-12^{00}$
2	8	6.0	.	$\overset{*}{\bigtriangledown}{}^{\circ}7^{25}-8^{14};12^{01-10};14^{36}-15^{52};=7^{20}-8^{15}$
3	7	7.1	.	$\overset{*}{\bigtriangledown}{}^{\circ}0^{50}-1^{05}\bullet^{0-1}1^{40}-8^{48}\bullet^{\circ}8^{59}-11^{42}\overset{*}{\bigtriangledown}{}^{\circ}11^{58}\ldots18^{12}\blacktriangle'17^{56-57};=a$
4	7	0.0	.	$\bullet^{\circ}1^{45}\ldots3^{48}\overset{*}{\bigtriangledown}{}^{\circ}14^{10-25}$
5	8	.	.	$=21^{30}-24$
6	7	1.1	.	$\overset{*}{\bigtriangledown}{}^{\circ}20^{29}-21^{15};(\mathrm{R})SW20^{20}-\mathrm{R}\,20^{29}-21^{40}-(\mathrm{R})21^{40}-22^{25}NE$
7	7	1.3	.	$\bullet^{\circ}22^{45}\ldots24;=2^{10}-9^{30}$
8	7	1.6	.	$\bullet^{\circ}0^{00}-3^{30}\overset{*}{\bigtriangledown}{}^{1}4^{35-45}\overset{*}{\bigtriangledown}{}^{\circ}\ldots18^{06};=5^{30}-10^{45}$
9	8	.	.	$=3^{30}-10^{30}$
10	8	.	.	$=3^{35}-7^{30};\triangle^{0-1}2^{00}-8^{30}$
11	7	9.2	.	$\overset{*}{\bigtriangledown}{}^{0-2}23^{42}-24;(\mathrm{R})^{\circ}23^{30}-24\,SW\text{-}E;=21^{30}-24;\triangle^{\circ}0^{00}-10^{00}$
12	7	0.1	.	$\overset{*}{\bigtriangledown}{}^{\circ}0^{00}\ldots55\,17^{58}\ldots18^{28};\mathrm{R}^{\circ}0^{30}-1^{20}SW\text{-}E,17^{30-56}SW;=0^{00}-12^{30}$
13	7	16.1	.	$\overset{*}{\bigtriangledown}{}^{\circ}7^{45}-8^{10};11^{12-27}\overset{*}{\bigtriangledown}{}^{2-0}12^{30}-13^{02}\overset{*}{\bigtriangledown}{}^{\circ}\ldots15^{25}\overset{*}{\bigtriangledown}{}^{0-1}19^{50}-20^{24};(\mathrm{R})W\,12^{23}-\mathrm{R}\,12^{30}-13^{03}-(\mathrm{R})13^{20}E;(\mathrm{R})W14^{50}-15^{04-25}-(\mathrm{R})15^{42}E$
14	7	2.3	.	$\overset{*}{\bigtriangledown}{}^{0-1}11^{41}-12^{05}\overset{*}{\bigtriangledown}{}^{\circ}15^{57}-16^{20};=5^{30}-8^{30};23^{45}-24$
15	7	0.3	.	$\bullet^{\circ}22^{52}\ldots24;=0^{00}-9^{20}\,21^{30}-24$
16	6	0.0	.	$\bullet^{\circ}0^{00}\ldots2^{54}\overset{*}{\bigtriangledown}{}^{\circ}7^{44}-8^{10};=0^{00}-24$
17	8	.	.	$=0^{00}-8^{20}$
18	7	.	.	
19	8	0.2	.	$\overset{*}{\bigtriangledown}{}^{\circ}16^{40-43}\,19^{35-46}$
20	7	.	.	
21	7	.	.	$=3^{30}-9^{20}\infty-13^{30}\,19^{30}-21^{20}=-24$
22	7	0.4	.	$\bullet^{\circ}10^{30}\ldots11^{30}\overset{*}{\bigtriangledown}{}^{\circ}12^{35-45}\,21^{30}-22^{00};(\mathrm{R})W20^{40}-\mathrm{R}^{\circ}21^{30}-22^{00}-(\mathrm{R})23^{40}E;\gg21^{10}-22^{00};=0^{00}-11^{30}$
23	8	.	.	$(\mathrm{R})1^{45}-3^{30}S;=3^{00}-9^{30}$
24	7	.	.	$=20^{30}-24;\triangle^{\circ}2^{00}-10^{30};23^{00}-24$
25	7	.	.	$=0^{00}-8^{30};\triangle^{\circ}0^{00}-8^{30}$
26	7	0.1	.	$\overset{*}{\bigtriangledown}{}^{\circ}20^{52}-21^{15};=3^{30}-7^{30}$
27	7	0.1	.	$\overset{*}{\bigtriangledown}{}^{\circ}1^{50}-2^{45}\,12^{45}-13^{00}\,18^{00-06};(\mathrm{R})SW12^{25}-\mathrm{R}^{\circ}12^{47-49}-(\mathrm{R})13^{15}NE$
28	8	2.2	.	$\overset{*}{\bigtriangledown}{}^{0-1}12^{15-40}\,13^{05\ldots40}\overset{*}{\bigtriangledown}{}^{\circ}16^{01}\ldots18^{44}$
29	8	.	.	$=0^{40}-6^{20};\triangle^{\circ}2^{00}-8^{30}$
30	8	.	.	$\triangle^{\circ}2^{00}-8^{00}$
31	7	.	.	$=4^{30}-8^{30};\triangle^{\circ}2^{30}-8^{30}$
Σ	—	49.7	—	UWAGI

Sierpień - Août

1	7	0.0	.	$\overset{*}{\bigtriangledown}{}^{\circ}6^{50}-7^{10};11^{59}\ldots13^{56};=5^{30}-11^{30}\,20^{30}-24;\triangle^{\circ}23^{30}-24$
2	7	.	.	$=0^{00}-8^{15};\triangle^{\circ}0^{00}-8^{30}$
3	7	.	.	$=4^{10}-13^{30}\infty-20^{40}=-24$
4	6	0.4	.	$\overset{*}{\bigtriangledown}{}^{\circ}16^{55}-17^{15};19^{47}-20^{02};(\mathrm{R})SW16^{44}-\mathrm{R}^{\circ}16^{55}-17^{15}-(\mathrm{R})17^{50}NE;(\mathrm{R})SW19^{30}-\mathrm{R}^{\circ}19^{47}-20^{02}-(\mathrm{R})21^{40}NE;=0^{00}-12^{30}\infty-17^{30}=20^{40}-24;\triangle^{\circ}na-a$
5	7	4.7	.	$\overset{*}{\bigtriangledown}{}^{1-0}16^{38}-17^{23}\overset{*}{\bigtriangledown}{}^{\circ}17^{55}-18^{10};(\mathrm{R})W16^{10}-\mathrm{R}^{\circ}16^{38}-17^{00}-(\mathrm{R})17^{20}E;\gg16^{50}-17^{00};=na\equiv^{0-1}7^{30}=-10^{30};20^{05}-24$
6	7	0.4	.	$\overset{*}{\bigtriangledown}{}^{\circ}12^{47-56};14^{01-40};=0^{00}-8^{30}$
7	7	5.9	.	$\overset{*}{\bigtriangledown}{}^{\circ}5^{55}\ldots7^{00}\overset{*}{\bigtriangledown}{}^{0-1}17^{25}-20^{05}\overset{*}{\bigtriangledown}{}^{\circ}20^{50}-22^{12};\mathrm{R}^{\circ}17^{42-44};\gg17^{25}-18^{10};=na-a$
8	7	.	.	$\triangle^{\circ}22^{00}-24$
9	8	.	.	$=19^{30}-24;\triangle^{\circ}0^{00}-8^{40};23^{00}-24$
10	7	.	.	$=0^{00}-8^{30};\triangle^{\circ}0^{00}-9^{30}$
11	8	.	.	$\triangle^{\circ}23^{45}-24$
12	7	.	.	$=4^{30}-9^{30};\triangle^{\circ}0^{00}-8^{00}$
13	8	19.8	.	$=4^{30}-9^{45};\triangle^{\circ}3^{00}-6^{00}$
14	6	1.2	.	$\overset{*}{\bigtriangledown}{}^{\circ}1^{55}-2^{35}\overset{*}{\bigtriangledown}{}^{0-1}3^{35}-7^{25}\overset{*}{\bigtriangledown}{}^{\circ}8^{05-40};16^{05-10};(\mathrm{R})N3^{44}-\mathrm{R}^{\circ}3^{45}-6^{30}-(\mathrm{R})6^{40}SE;=7^{30}-16^{10}$
15	6	12.8	.	$\overset{*}{\bigtriangledown}{}^{\circ}8^{06}-8^{45};\bullet^{\circ}-9^{30}\ldots12^{10}\overset{*}{\bigtriangledown}{}^{\circ}12^{50}-13^{15}\,19^{15-30}\overset{*}{\bigtriangledown}{}^{0-2}22^{35}-24;(\mathrm{R})SW22^{28}-\mathrm{R}^{\circ}22^{35}-24;=9^{30}-15^{20}np$
16	7	0.0	.	$\overset{*}{\bigtriangledown}{}^{\circ}2^{16-35}\,14^{46}-15^{05};\mathrm{R}^{\circ}0^{00-50}NE;=na;\triangle^{\circ}np$
17	8	8.9	.	$\overset{*}{\bigtriangledown}{}^{0-1}15^{34}-20^{25}\ldots23^{28};(\mathrm{R})SW15^{25}-\mathrm{R}^{\circ}15^{31}-17^{02}-(\mathrm{R})17^{25}NW;=na-a,p-np;\triangle^{0-1}0^{00}-10^{00}$
18	8	0.4	.	$\overset{*}{\bigtriangledown}{}^{\circ}0^{45}-1^{10};11^{02}\ldots12^{55}\,19^{25-42};=0^{00}-3^{55}\equiv^{0-1}-7^{50}=-10^{30}$
19	7	6.5	.	$\overset{*}{\bigtriangledown}{}^{0-1}9^{50}\ldots18^{58}\overset{*}{\bigtriangledown}{}23^{27}-24$
20	8	0.0	.	$\overset{*}{\bigtriangledown}{}^{\circ}0^{00-10}\,5^{16}\ldots6^{43};10^{15-33};12^{25-33};14^{01-20}$
21	7	2.5	.	$=4^{20}-10^{30};\triangle^{\circ}21^{30}-24$
22	7	2.2	.	$\bullet^{\circ}5^{45}\ldots6^{00}-9^{05}\bullet^{\circ}-9^{35}\bullet^{\circ}-10^{15};=0^{00}-13^{30};\triangle^{\circ}0^{00}-5^{45}$
23	8	0.0	.	$=3^{30}-8^{30}$
24	7	11.2	.	$\bullet^{\circ}6^{50}\ldots19^{05}\overset{*}{\bigtriangledown}{}^{1-0}-20^{00}\bullet^{0-1}-23^{20}\ldots24$
25	8	.	.	$\bullet^{\circ}0^{00}\ldots0^{30}-2^{30}$
26	7	.	.	$\triangle^{\circ}1^{00}-8^{00}$
27	7	.	.	$\triangle^{\circ}2^{00}-7^{30}$
28	8	.	.	$\gg14^{10}-15^{40};\triangle^{\circ}23^{00}-24$
29	7	1.2	.	$\overset{*}{\bigtriangledown}{}^{0-1}18^{42}\ldots22^{37};=5^{30}-8^{30};\triangle^{\circ}0^{00}-9^{00}$
30	7	1.1	.	$\overset{*}{\bigtriangledown}{}^{0-1}5^{12}\ldots8^{35};=2^{30}-6^{15}$
31	8	0.0	.	$\overset{*}{\bigtriangledown}{}^{\circ}19^{03-05};\gg14^{15}-18^{20};=8^{20}-11^{30};\triangle^{\circ}2^{00}-8^{30}$
Σ	—	79.2	—	UWAGI

Łódź - Lublinek φ = 51°44' λ = 19°24' Wrzesień - Septembre 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	95.0	97.6	99.3	97.3	10.6	14.7	11.1	11.9	18.3	9.2	92	70	84	82	1.0	5.0	2.1	2.7	9	8⊙	0	NW 7	WNW 8	W 3
2	101.7	101.1	98.8	100.5	8.7	18.6	12.7	13.2	20.0	5.3	96	42	78	72	0.4	12.5	3.3	5.4	2	10⊙	0	SSW 1	SW 6	C 0
3	97.7	97.2	95.4	96.8	9.8	22.7	15.2	15.7	25.1	6.5	87	40	70	66	1.6	16.5	5.1	7.7	2⊙	7⊙	0	C 0	C 0	E 2
4	92.2	89.6	86.4	89.4	13.2	26.8	19.4	19.7	28.9	9.7	82	39	70	64	2.8	21.4	6.6	10.3	2⊙	1⊙	0	E 1	SSE 5	SE 2
5	82.5	84.5	84.8	83.9	16.9	20.9	13.2	16.0	22.6	13.2	73	58	95	75	5.2	10.4	0.7	5.4	0	10	3	SSE 3	WSW 8	S 1
6	85.3	85.4	82.0	84.2	13.0	18.9	16.2	16.1	21.2	10.8	86	57	83	75	2.1	9.4	3.1	4.9	6⊙	6⊙	10●	SW 3	WSW 7	SW 3
7	77.5	77.8	81.3	78.9	17.8	14.2	14.8	15.4	20.1	13.5	76	91	70	79	4.8	1.5	5.0	3.8	9	10●	8	SW 5	SW 7	SW 8
8	87.7	88.4	89.9	88.7	9.9	14.2	10.4	11.2	16.1	8.3	86	63	85	78	1.8	6.0	1.9	3.2	2⊙	10	6	WSW 5	W 7	SW 6
9	95.1	98.5	100.5	98.0	9.4	13.0	10.0	10.6	15.1	8.1	92	66	93	84	1.0	5.1	0.8	2.3	10●	8	9	W 6	W 8	SW 1
10	99.0	96.7	93.7	96.5	9.1	19.8	14.8	14.6	22.5	7.1	83	45	65	64	2.0	12.8	5.9	6.9	8	0	0	S 2	SSW 7	SSW 4
11	91.4	90.3	93.7	91.8	13.4	17.2	15.4	15.4	21.7	10.7	71	85	85	80	4.5	3.0	2.6	3.4	9	10●	8	S 3	SW 5	W 3
12	93.7	87.9	82.4	88.0	12.2	22.6	20.6	19.0	27.0	9.3	90	54	70	71	1.4	12.5	7.3	7.1	7	9	9	SSW 2	SW 9	WNW 8
13	91.5	94.2	96.9	94.2	10.2	14.4	10.4	11.4	20.8	9.8	83	55	67	68	2.0	7.3	4.1	4.5	9	5⊙	9	NW 8	W 7	W 4
14	99.8	101.3	101.2	100.8	8.0	12.3	5.8	8.0	13.6	5.7	92	59	89	80	0.9	5.9	1.0	2.6	8	10	2	W 7	W 8	W 1
15	99.6	96.9	92.6	96.4	4.4	15.8	11.3	10.7	18.6	2.7	95	50	73	73	0.5	8.9	3.6	4.3	8	6⊙	3	E 1	SSE 4	SE 3
16	89.2	87.8	86.6	87.9	10.2	23.6	17.6	17.2	25.2	6.3	82	46	73	67	2.2	15.6	5.5	7.8	7⊙	3⊙	4	SE 2	SW 3	SE 1
17	88.3	88.6	88.0	88.3	12.6	14.0	10.6	12.0	18.5	10.5	99	93	95	96	0.2	1.1	0.7	0.7	10	10●	10●	W 1	N 3	NW 6
18	87.8	85.4	82.9	85.4	9.6	11.2	8.2	9.3	11.6	8.1	97	84	97	93	0.4	2.1	0.3	0.9	10	10●	10●	NW 4	NNE 3	NNW 7
19	87.4	90.3	92.8	90.2	6.2	9.6	6.3	7.1	10.8	5.7	92	79	98	90	0.7	2.6	0.1	1.1	10	9⊙	8	W 4	WSW 7	C 0
20	94.7	94.7	95.0	94.8	5.8	13.4	7.7	8.6	14.5	3.9	100	64	91	85	0.0	5.5	0.9	2.1	10	7	4	SSW 2	W 6	SW 3
21	94.9	94.7	94.0	94.5	6.9	11.8	9.3	9.3	13.3	5.6	92	67	88	82	0.7	4.5	1.4	2.2	10	9	10	WSW 4	WNW 9	W 5
22	94.4	95.8	97.0	95.7	7.4	11.1	8.0	8.6	13.2	7.0	97	66	92	85	0.3	4.5	0.9	1.9	9	9	9	WNW 5	NW 6	NW 2
23	95.3	93.6	93.8	94.2	7.1	9.0	8.6	8.3	10.8	6.3	97	92	97	95	0.3	1.0	0.3	0.5	10●	10●	9	NW 2	WNW 6	W 2
24	98.1	100.9	103.9	101.0	6.4	9.2	5.8	6.8	11.5	5.3	100	95	100	98	0.0	0.6	0.0	0.2	10≡	10	0≡	W 3	W 2	C 0
25	106.4	106.7	105.5	106.2	3.6	14.1	9.4	9.1	15.4	2.2	100	55	88	81	0.0	7.2	1.4	2.9	0≡	4⊙	0	E 1	ESE 5	E 3
26	103.9	102.1	100.3	102.1	6.9	15.0	9.3	10.1	16.2	5.8	88	49	74	70	1.1	8.7	3.1	4.3	0⊙	2⊙	0	E 3	ESE 10	ESE 4
27	97.2	95.1	94.1	95.5	6.3	13.6	10.0	10.0	14.9	4.8	89	67	92	83	1.0	5.2	1.0	2.4	0	8	10●	ENE 4	E 6	E 3
28	92.8	92.1	91.7	92.2	10.1	11.6	11.6	11.2	13.0	9.5	95	93	95	94	0.7	1.0	0.6	0.8	10	10	10	E 2	E 2	E 3
29	91.1	91.7	93.3	92.0	11.2	14.8	10.0	11.5	16.9	10.0	99	77	99	92	0.2	3.8	0.2	1.4	10	9	0≡	C 0	S 2	C 0
30	96.0	96.7	98.1	96.9	5.4	18.9	11.3	11.7	20.3	5.2	100	54	90	81	0.0	10.1	1.3	3.8	10≡	1⊙	0	C 0	SE 2	E 2
31																								
M	93.6	93.5	93.2	93.4	9.4	15.6	11.5	12.0	17.9	7.5	90	65	85	80	1.3	7.1	2.4	3.6	6.9	7.4	5.0	3.0	5.6	3.0

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1	99.7	100.8	102.2	100.9	7.2	20.0	10.8	13.2	20.8	6.6	100	51	93	81	0.0	11.4	1.1	4.2	10≡	3⊙	0	E 2	SE 3	E 3
2	103.4	103.6	103.4	103.3	10.6	19.9	13.3	14.3	20.8	10.0	95	60	85	80	0.7	9.3	2.3	4.1	3⊙	2⊙	0	E 2	ESE 4	E 3
3	102.6	102.3	102.4	102.4	9.8	19.6	12.6	13.6	20.7	9.3	95	60	86	80	0.6	9.2	2.1	4.0	5	4⊙	0	ESE 5	SE 5	E 2
4	101.6	101.4	100.6	101.2	7.4	18.4	12.6	12.8	20.5	7.2	100	60	86	82	0.0	8.5	2.1	3.5	4≡⊙	8⊙	8	E 2	SE 2	E 3
5	99.5	100.4	100.8	100.2	9.2	16.2	12.6	12.6	18.6	8.6	97	81	95	91	0.3	3.4	0.7	1.5	9	9	10	E 3	E 2	C 0
6	101.2	102.6	105.4	103.1	12.0	16.0	11.5	12.8	16.5	11.5	100	76	94	90	0.0	4.4	0.9	1.8	10≡	9	3	C 0	NE 2	E 2
7	108.5	109.9	111.0	109.8	11.4	15.2	10.1	11.7	16.2	9.6	100	72	95	89	0.0	4.8	0.7	1.8	10	7⊙	0	NE 4	NE 4	NE 2
8	112.3	113.2	111.7	112.4	9.8	14.2	9.0	10.5	16.2	7.6	99	76	97	91	0.1	3.9	0.3	1.4	10	6	0	ENE 3	ESE 4	E 2
9	111.1	110.1	107.9	109.7	5.3	11.7	7.0	7.8	13.4	5.2	100	90	100	97	0.0	1.3	0.0	0.4	10≡	6	10≡	C 0	S 1	C 0
10	105.4	103.8	101.5	103.6	6.5	8.8	5.8	6.7	10.9	5.6	96	78	95	90	0.5	2.4	0.4	1.1	10	4⊙	0	E 2	E 4	E 2
11	98.9	96.5	93.5	96.3	1.9	14.8	6.6	7.5	16.7	1.0	100	64	97	87	0.0	6.0	0.3	2.1	5≡	2	0≡	E 2	E 1	C 0
12	94.1	96.1	98.0	96.1	4.6	8.0	5.4	5.8	10.2	1.3	100	85	97	94	0.0	1.5	0.3	0.6	10≡	10	3	C 0	E 1	C 0
13	99.0	98.3	94.6	97.3	4.4	12.1	6.4	7.3	13.1	-0.4	100	57	88	82	0.0	6.0	1.1	2.4	4≡	4⊙	0	NE 1	SE 3	ESE 2
14	88.9	90.2	93.5	90.9	5.8	7.0	7.2	6.8	8.1	4.8	100	98	93	97	0.0	0.1	0.8	0.3	10≡	10	8	W 2	W 6	W 6
15	98.3	101.8	104.2	101.5	5.6	8.9	1.3	4.4	9.9	1.3	88	46	91	75	1.1	6.2	0.6	2.6	5	4⊙	0	NE 3	NE 3	C 0
16	103.1	101.0	99.9	101.3	-1.1	10.1	3.8	4.2	11.3	-1.9	91	42	73	69	0.4	7.2	2.1	3.2	7	4⊙	5	C 0	SSE 3	C 0
17	99.8	101.2	100.8	100.6	4.6	10.5	8.9	8.2	11.6	3.5	90	79	88	86	0.8	2.7	1.4	1.6	10	10	10	SW 1	WSW 3	WSW 3
18	98.5	96.8	91.1	95.5	9.4	11.5	10.0	10.2	12.9	8.5	95	82	83	87	0.6	2.5	2.1	1.7	10	10	10	WSW 5	WSW 5	SW 8
19	88.4	90.5	91.0	90.0	10.0	10.5	9.0	9.6	13.2	8.7	95	71	76	81	0.7	3.7	2.8	2.4	10●	10	9	W 6	WNW 8	W 8
20	94.1	97.7	103.7	98.5	6.5	11.8	4.6	6.9	12.6	4.4	96	50	84	77	0.5	6.9	1.4	2.9	8	6⊙	0	NW 6	NW 9	NNE 1
21	107.8	108.0	107.1	107.6	-1.8	10.6	4.0	4.2	12.5	-2.6	100	51	83	78	0.0	6.2	1.3	2.3	0⊙	0⊙	0	C 0	W 3	C 0
22	106.6	106.2	104.8	105.9	0.6	10.7	2.0	3.8	12.1	-0.2	94	66	98	86	0.4	4.3	0.2	1.7	9	5	0≡	S 1	WNW 5	E 1
23	103.1	103.1	101.2	102.5	0.4	7.2	1.0	2.4	8.7	-1.0	100	80	100	93	0.0	2.1	0.0	0.7	10≡	9	10≡	SE 1	W 3	C 0
24	98.7	98.1	98.9	98.6	-0.9	11.9	2.7	4.1	12.6	-1.7	97	59	96	84	0.2	5.7	0.2	2.0	0	0⊙	0	SE 1	W 3	WNW 3
25	98.9	98.2	97.3	98.1	2.9	11.3	5.0	6.1	12.1	1.8	100	59	87	82	0.0	5.7	1.1	2.3	9	0⊙	0	ESE 1	SSW 2	SE 2
26	94.7	92.7	91.9	93.1	1.9	13.2	6.9	7.2	14.0	1.0	94	57	81	77	0.4	6.6	1.8	2.9	0	0⊙	0	ESE 2	WSW 8	S 4
27	88.5	91.7	94.8	91.7	5.1	9.5	5.6	6.4	12.2	4.0	86	73	100	86	1.3	3.3	0.0	1.3	3	10●	10●	S 7	WNW 6	NW 1
28	90.4	88.4	88.4	89.1	6.0	8.4	3.8	5.5	9.3	3.7	100	89	90	93	0.0	1.2	0.8	0.7	9	10●	10	E 2	W 2	W 1
29	88.3	90.0	93.6	90.6	3.6	5.6	5.3	5.0	6.1	3.3	98	91	97	95	0.1	0.9	0.3	0.4	10●	10●	10●	C 0	NW 2	NW 2
30	95.3	94.5	90.7	93.3	3.7	7.7	5.7	5.7	9.9	1.7	100	71	89	87	0.0	3.1	1.0	1.4	10≡	5	9	C 0	E 2	SE 2
31	87.6	87.0	87.2	87.3	5.4	8.4	7.0	7.0	10.0	4.5	95	83	93	90	0.3	1.8	0.7	1.0	10	9	8	C 0	C 0	E 1
M	99.0	99.2	99.1	99.1	5.4	11.9	7.1	7.9	13.3	4.1	97	70	91	86	0.3	4.6	1.0	2.0	7.4	6.0	4.3	2.0	3.6	2.1

Łódź-Lublinek H_s = 187m H_b = 187,7m h_w = 11m Wrzesień - Septembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚCIE GU h	POGODA
1	8	0.0	•	$\overset{*}{\nabla}{}^{\circ}12^{35-40}, 17^{45-50}$
2	8	•	•	$=2^{30}-9^{30}, \triangle^{0-2}2^{00}-9^{00}\triangle^{\circ}21^{30}-24$
3	8	•	•	$=4^{30}-10^{15}, 19^{30}-24; \triangle^{0-1}0^{00}-9^{00}$
4	7	•	•	$=0^{00}-9^{30}, 19^{40}-24; \triangle^{\circ}2^{00}-8^{00}$
5	7	8.3	•	$\bullet^{\circ}14^{10}...18\overset{*}{\nabla}{}^{0-1}15^{28}...18^{15}; =0^{00}-12^{30}; \triangle^{\circ}3^{00}-9^{00}$
6	8	0.7	•	$\bullet^{\circ}20^{20}-22^{30}...24$
7	7	3.2	•	$\bullet^{\circ}0^{00...15}; 2^{35}-3^{25}; 10^{30}...12^{10}\bullet^{0-1}-13^{05}\overset{*}{\nabla}{}^{\circ}-14^{28}; \gg 12^{11-17}$
8	8	0.3	•	$\overset{*}{\nabla}{}^{\circ}13^{47}-14^{05}, 20^{25-42}; \triangle^{\circ}2^{00}-9^{30}$
9	7	0.0	•	$\bullet^{\circ}5^{45}...8^{38}\overset{*}{\nabla}{}^{\circ}15^{40-45}; \triangle^{0-1}21^{00}-24$
10	7	•	•	$=6^{15}-9^{30}; \triangle^{2-1}0^{00}-8^{30}$
11	7	1.7	•	$\overset{*}{\nabla}{}^{\circ}11^{15-18}\bullet^{\circ}13^{20}-14^{40}...14^{50}\overset{*}{\nabla}{}^{\circ}18^{24-27}; 19^{02-04}$
12	7	2.5	•	$\overset{*}{\nabla}{}^{2}19^{52}-20^{08}; (K)^{\circ}NW18^{46}-K^{\circ}-18^{50}-19^{45}-(K)\ 20^{20}NE-E; \gg 16^{40}-17^{10}; 19^{55}-20^{05}; =1^{50}-12^{30}; \triangle^{0-2}2^{00}-11^{00}$
13	8	•	•	$\overset{*}{\nabla}{}^{\circ}4^{45}-5^{20}; \gg 0^{40}-3^{30}$
14	8	•	•	$\triangle^{\circ}2^{30}-8^{00}, 21^{00}-24$
15	7	•	•	$=2^{30}-10^{30}; \triangle^{0-1}0^{00}-9^{00}$
16	7	•	•	$=5^{20}-11^{30}, 19^{30}-24; \triangle^{\circ}2^{00}-11^{00}$
17	5	18.8	•	$\bullet^{0-1}12^{40}-24; =0^{00}-24; \triangle^{0-2}0^{00}-12^{00}$
18	6	18.8	•	$\bullet^{\circ}0-2^{10}...3^{05}\bullet^{0-1}12^{50}-24; =0^{00}-14^{00}$
19	8	1.0	•	$\bullet^{\circ}0^{00}-4^{05}\overset{*}{\nabla}{}^{\circ}9^{45-48}, 15^{10-20}; =20^{30}-24$
20	6	1.2	•	$\overset{*}{\nabla}{}^{\circ}14^{48}-15^{00}\blacktriangle^{\circ}14^{49-50}\overset{*}{\nabla}{}^{\circ}15^{10-25}; =0^{00-40}\equiv^{0-1}-2^{20}\equiv^{\circ}-7^{35}=-14^{10}$
21	8	0.0	•	$\overset{*}{\nabla}{}^{\circ}9^{10-25}, 14^{52}...24; =3^{30}-9^{15}$
22	8	1.4	•	$\overset{*}{\nabla}{}^{\circ}0^{00-10}\bullet^{\circ}0^{45}...2^{35}, 4^{40}...5^{20}; =2^{30}-5^{00}$
23	7	3.7	•	$\overset{*}{\nabla}{}^{\circ}3^{53}-4^{10}, 7^{32-46}, 8^{50}-9^{07}\overset{*}{\nabla}{}^{0-1}12^{58}-14^{15}\bullet^{\circ}-17^{35}, 19^{50}-20^{20}; =8^{30}-13^{30}$
24	6	0.2	•	$=2^{30}-4^{50}\equiv^{0-1}-9^{18}=-20^{50}\equiv^{0-2}-24; \triangle^{0-2}20^{00}-24$
25	8	•	•	$\equiv^{1-2}0^{00}-9^{00}=-11^{30}; \triangle^{2-0}0^{00}-10^{30}-\triangle^{\circ}20^{00}-24$
26	8	•	•	$\gg 12^{10}-14^{50}; =5^{30}-9^{30}; \triangle^{\circ}0^{00}-9^{00}$
27	7	0.0	•	$\bullet^{\circ}21^{42}...22^{25}; =5^{20}-10^{15}, 18^{30}-24; \triangle^{0-1}2^{00}-11^{00}$
28	6	0.4	•	$\bullet^{\circ}14^{50}-15^{40}; =0^{00}-24; \triangle^{\circ}4^{00}-12^{00}$
29	6	0.2	•	$\bullet^{0-1}4^{50}-7^{40}; =0^{00}-3^{40}\equiv^{\circ}-4^{50}=-21^{35}\equiv^{0-1}-24; \triangle^{0-2}20^{00}-24$
30	6	•	•	$\equiv^{0-2}0^{00}-3^{10}\equiv^{1-2}-9^{10}\equiv^{\circ}-9^{20}=-12^{30}\infty-16^{30}=-24; \triangle^{2-0}0^{00}-10^{30}$
31				
Σ	—	62.4	—	UWAGI

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1	7	•	•	$=0^{00}-5^{30}\equiv^{\circ}-5^{40}\equiv^{1}-7^{30}\equiv^{\circ}-7^{55}=-11^{30}, 16^{30}-24; \triangle^{0-2}1^{00}-12^{00}$
2	7	•	•	$=0^{00}-12^{30}; \triangle^{2-2}0^{00}-10^{00}$
3	7	•	•	$=4^{30}-11^{30}, 18^{30}-24; \triangle^{0-2}1^{00}-8^{00}\triangle^{\circ}22^{00}-24$
4	6	•	•	$=0^{00}-3^{45}\equiv^{1}-4^{50}=-5^{40}\equiv^{\circ}-8^{10}=-12^{30}\infty-17^{30}=-24; \triangle^{0-1}0^{00}-11^{30}\triangle^{\circ}-24$
5	6	•	•	$=0^{00}-8^{10}\equiv^{\circ}-8^{48}=-14^{30}\infty-17^{30}=-24; \triangle^{0-1}0^{00}-12^{00}\triangle^{\circ}20^{30}-24$
6	6	•	•	$=0^{00}-4^{55}\equiv^{0-1}-9^{30}\equiv^{\circ}-9^{50}=-24; \triangle^{0-2}0^{00}-14^{00}\triangle^{0-1}20^{00}-24$
7	6	•	•	$=0^{00}-24; \triangle^{1-0}0^{00}-9^{00}$
8	6	0.2	•	$=0^{00}-22^{50}\equiv^{\circ}-23^{30}\equiv^{1}-24; \triangle^{0-2}1^{00}-14^{00}\triangle^{0-2}20^{00}-24$
9	5	0.2	•	$\equiv^{0-2}0^{00}-9^{30}=-18^{50}\equiv^{0-1}-20^{05}\equiv^{2}-24; \triangle^{2-0}0^{00}-13^{30}, 18^{00}-24$
10	6	0.2	•	$\equiv^{2}0^{00}-2^{45}=-24; \triangle^{2-0}0^{00}-12^{00}, 17^{30}-24$
11	6	0.2	•	$=0^{00-45}\equiv^{0-1}-7^{50}=-13^{30}\infty-14^{40}, 16^{30}-17^{40}=-20^{40}\equiv^{\circ}-24; \triangle^{2-0}0^{00}-13^{00}; \triangle^{\circ}19^{40}-24$
12	6	0.3	•	$\bullet^{\circ}6^{05}-7^{30}; \equiv^{0-1}0^{00}-2^{50}\equiv^{2-1}-6^{30}\equiv^{2-1}-7^{20}=-24; \triangle^{0-2}0^{00}-6^{05}$
13	7	•	•	$=0^{00}-1^{20}\equiv^{0-1}-7^{50}=-10^{30}, 16^{30}-24; \triangle^{0-2}0^{00}-9^{00}\triangle^{\circ}22^{00}-24$
14	4	•	•	$=0^{00-20}\equiv^{0-2}-10^{40}=-24; \triangle^{0-2}0^{00}-24$
15	8	0.4	•	$\bullet^{\circ}0^{40}...6^{15}; =0^{00}-5^{30}, 19^{30}-24; \triangle^{\circ}0^{00-40}, 19^{00}-24$
16	8	•	•	$=0^{00}-10^{30}; \triangle^{\circ}0^{00}-1^{20}\sqcup^{\circ}-8^{10}$
17	6	0.0	•	$\bullet^{\circ}17^{50}-18^{10}, 23^{15}-24; =4^{00}-24$
18	6	0.2	•	$\bullet^{\circ}0^{00}-1^{45}; =0^{00}-24$
19	8	0.5	•	$\bullet^{\circ}3^{40}...4^{40}\bullet\bullet^{\circ}-5^{15}\bullet^{1}-6^{30}\bullet^{\circ}...7^{35}; =0^{00}-8^{18}$
20	8	•	•	$\overset{*}{\nabla}{}^{\circ}1^{40}-2^{15}, 2^{17}-3^{05}$
21	8	•	•	$=1^{20}-6^{15}\equiv^{\circ}-6^{38}=-8^{48}\sqcup^{0-1}1^{00}-8^{15}\triangle^{\circ}20^{30}-24$
22	7	•	•	$=a.p\equiv^{0-2}19^{20}-21^{30}\equiv^{1}-24; \triangle^{\circ}0^{00}-1^{00}\sqcup^{\circ}-7^{10}\triangle^{0-2}17^{30}-24$
23	6	•	•	$\equiv^{1-0}0^{00}-7^{40}\equiv^{\circ}-8^{40}=-14^{20}\infty-15^{40}=-18^{50}\equiv^{\circ}-20^{35}\equiv^{0-2}-24; \triangle^{1-0}0^{00}-12^{00}\triangle^{0-1}19^{30}-24$
24	6	•	•	$\equiv^{2-1}0^{00}-3^{30}\equiv^{\circ}3^{50}=-21^{20}\equiv^{0-1}-24; \sqcup^{0-2}0^{00}-9^{00}\triangle^{0-2}19^{00}-24$
25	6	•	•	$\equiv^{0-1}0^{00}-4^{50}=-11^{00}\infty 11^{00}-15^{30}=-24; \triangle^{2-0}0^{00}-9^{30}\triangle^{\circ}21^{30}-24$
26	5	•	•	$=0^{00}-12^{30}\infty-16^{30}=-24; \triangle^{0-1}0^{00}-11^{00}\triangle^{\circ}23^{00}-24$
27	6	7.2	•	$\bullet^{\circ}12^{38}...13^{00}-24; =0^{00}-24; \triangle^{\circ}0^{00}-5^{00}\sqcup^{\circ}-6^{30}$
28	5	3.3	•	$\bullet^{\circ}0^{00}-3^{40}...6^{35}12^{24}...14^{35}-16^{40}17^{15}-19^{10}...20^{35}; =0^{00}-24$
29	6	0.4	•	$\bullet^{\circ}0^{30}...3^{15}-6^{20}...14^{45}, 19^{45}...21^{30}-22^{48}; =0^{00}-24$
30	6	•	•	$=0^{00}-6^{10}\equiv^{0-1}-10^{50}=-24$
31	5	2.4	•	$\bullet^{\circ}21^{50}...22^{15}-24; =0^{00}-24$
Σ	—	15.5	—	UWAGI

Łódź - Lublinek φ=51°44' λ=19°24' Listopad - Novembre 1962

DNI	CIŚNIENIE P= 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	83.6	83.8	84.9	84.1	7.4	9.4	8.6	8.5	10.5	6.5	99	92	100	97	0.2	1.0	0.0	0.4	10	10	10 ●≡	E 3	E 3	C 0
2	88.2	90.5	93.1	90.6	6.7	7.8	6.9	7.1	9.7	6.5	99	94	91	95	0.1	0.6	0.8	0.5	10	10	10	W 1	SW 4	C 0
3	93.6	93.6	94.1	93.8	6.5	9.3	9.8	8.8	10.6	6.0	96	93	97	95	0.5	0.8	0.3	0.5	9	10	10	E 3	ESE 4	SE 5
4	94.4	94.2	93.6	94.1	8.6	13.0	9.2	10.0	14.1	8.5	97	79	96	91	0.3	3.1	0.4	1.3	10	2	8	SE 3	SE 4	ESE 4
5	92.3	91.9	90.8	91.7	8.7	13.4	9.0	10.0	14.2	8.6	93	70	85	83	0.7	4.7	1.7	2.4	10	0 ⊙	0	SE 6	SE 7	ESE 8
6	88.8	89.0	91.1	89.6	3.0	8.7	8.0	6.9	10.4	3.0	81	56	64	67	1.5	4.9	3.8	3.4	4	9	8	E 8	ESE 9	ESE 9
7	93.8	96.1	97.5	95.8	6.0	10.8	6.7	7.6	12.2	5.9	79	72	84	78	2.0	3.7	1.6	2.4	9	9 ⊙	0	ESE 9	ESE 8	E 6
8	95.7	93.8	93.0	94.2	4.0	12.2	8.3	8.2	13.8	3.9	93	70	82	82	0.5	4.3	2.0	2.3	2	1 ⊙	4	E 5	E 6	E 4
9	91.7	92.0	93.3	92.3	3.0	6.5	2.1	3.4	9.2	1.6	91	81	100	91	0.7	1.9	0.0	0.9	8	6 ⊙	10	E 3	ENE 9	ENE 8
10	93.3	94.4	96.4	94.7	3.4	2.8	0.9	2.0	5.1	0.9	85	82	94	87	1.2	1.3	0.4	1.0	10	10	10 *	ENE12	NE 8	NE 8
11	96.9	96.5	96.6	96.7	0.2	1.2	2.1	1.4	2.9	0.1	98	96	93	96	0.1	0.3	0.5	0.3	10 *	10 *	10	NE 6	ENE 7	E 7
12	95.0	94.0	94.2	94.4	2.6	1.8	3.0	2.6	3.6	1.7	95	94	98	96	0.4	0.4	0.2	0.3	10 ●	10 ●	10 ●	E 8	E 8	SE 2
13	96.3	96.9	96.4	96.5	3.3	5.4	5.7	5.0	6.9	2.9	97	94	98	96	0.2	0.6	0.2	0.3	10	10	10	ESE 1	E 2	E 3
14	95.6	95.1	94.4	95.0	4.8	5.0	4.0	4.4	6.7	3.9	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10 ≡	E 1	E 3	C 0
15	90.6	86.2	81.7	86.2	5.2	6.3	5.0	5.4	6.7	4.0	98	97	97	97	0.1	0.2	0.3	0.2	10	10 ●	10	S 2	S 2	W 4
16	84.5	86.0	88.9	86.5	1.4	2.7	0.0	1.0	5.3	-0.2	91	75	88	85	0.7	1.8	0.7	1.1	10	10	10	W 5	WNW 7	W 4
17	91.1	92.0	90.3	91.1	-0.7	0.1	-1.2	-0.8	1.7	-1.5	91	78	84	84	0.5	1.4	0.9	0.9	9	10	5	W 4	SW 4	ESE 6
18	84.4	82.7	79.4	82.2	-0.6	1.2	2.4	1.4	3.0	-1.7	81	75	84	80	1.1	1.7	1.2	1.3	8	9	10	E 6	ESE 7	ESE 5
19	76.0	82.2	82.9	80.4	5.4	6.8	4.8	5.4	7.6	2.0	81	67	79	76	1.7	3.3	1.8	2.3	10	5 ⊙	10	S 9	SW 7	E 2
20	82.3	81.5	85.1	83.0	3.5	3.0	0.0	1.6	5.6	0.0	95	95	100	97	0.4	0.4	0.0	0.3	10 ●	10 ●	10 *	NE 2	N 4	WNW 4
21	88.6	88.4	87.4	88.1	-0.9	-0.1	-0.5	-0.5	0.9	-1.0	100	94	84	93	0.0	0.4	1.0	0.5	10	10	10	N 1	SSW 1	E 5
22	86.3	88.3	92.7	89.1	0.2	2.0	1.2	1.2	3.1	-0.5	96	91	94	94	0.3	0.7	0.4	0.5	10	10	10	E 4	SE 3	SSW 2
23	96.5	98.3	100.9	98.6	-0.9	0.2	-0.7	-0.5	1.3	-1.9	89	80	93	87	0.6	1.2	0.4	0.7	6	9	9	WSW 1	WSW 4	C 0
24	103.2	105.1	107.0	105.1	-1.9	-0.4	-0.7	-0.9	0.7	-3.4	96	90	91	92	0.2	0.6	0.5	0.4	10	10	10 ▲	C 0	NNW 2	N 2
25	107.9	107.3	106.6	107.3	-0.9	0.5	0.1	0.0	1.3	-1.2	91	86	96	91	0.5	0.8	0.3	0.5	10	9	10	N 2	N 1	C 0
26	108.0	108.5	109.7	108.7	-0.2	3.2	0.2	0.8	4.3	-0.8	94	78	96	89	0.4	1.7	0.3	0.8	9	9	10	C 0	NW 2	N 2
27	108.9	108.1	106.4	107.8	0.6	2.8	1.8	1.8	3.6	-0.1	94	84	98	92	0.4	1.2	0.2	0.6	10 ●	10	10	C 0	C 0	SSW 2
28	102.1	101.1	101.0	101.4	1.1	2.2	2.4	2.0	3.2	0.8	92	98	95	95	0.5	0.2	0.4	0.4	10	10	10	SW 5	WSW 5	WSW 4
29	99.5	99.3	95.4	98.1	3.2	4.7	4.6	4.3	5.7	2.2	98	95	97	97	0.2	0.4	0.3	0.3	10 ●	10	10 ●	WSW 4	W 3	WSW 9
30	90.8	90.9	94.0	91.9	3.7	4.8	2.0	3.1	5.7	1.9	98	90	96	95	0.2	0.8	0.3	0.4	10 ●	9	10 ●	WSW 8	W 6	NW 4
31																								
M	93.3	93.6	94.0	93.6	2.9	4.9	3.5	3.7	6.3	2.0	93	85	92	90	0.5	1.5	0.7	0.9	9.1	8.6	8.8	4.1	4.7	4.0

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1	106.1	110.9	115.8	110.9	-1.7	-0.3	-1.0	-1.0	3.0	-2.0	92	86	85	88	0.4	0.9	0.9	0.7	9	9	10 *	N 6	N 6	NW 5
2	119.2	120.5	119.8	119.8	-4.9	-0.1	-4.1	-3.3	1.0	-5.2	95	76	96	89	0.2	1.5	0.2	0.6	6	7 ⊙	10 ≡	C 0	W 3	NW 1
3	116.0	113.9	109.9	113.3	-6.5	-4.5	-5.7	-5.6	-2.0	-6.6	97	96	97	97	0.1	0.2	0.1	0.1	10	10	0	W 2	SSW 2	S 1
4	105.2	103.1	101.2	103.2	-4.9	-0.3	-1.6	-2.1	1.0	-7.3	98	72	69	80	0.1	1.7	1.6	1.1	9	8	1	SW 4	WSW 5	WSW 3
5	99.5	102.4	106.2	102.7	-2.5	-0.1	0.4	-0.4	1.2	-5.7	91	98	100	96	0.5	0.2	0.0	0.2	10	10 ≡	10 ● ≡	W 4	WNW 3	WNW 2
6	107.2	106.7	106.1	106.7	0.3	0.6	-0.3	0.1	1.6	-0.5	100	96	96	97	0.0	0.3	0.3	0.2	10 ● ≡	10	10	W 2	W 3	W 4
7	103.7	103.5	105.0	104.1	-1.2	1.0	-3.5	-1.8	2.3	-3.7	99	92	98	96	0.1	0.5	0.1	0.2	10 ≡	0 ⊙	0	WSW 5	WSW 4	C 0
8	106.2	107.0	104.5	105.9	-6.1	-0.9	-5.7	-3.6	0.7	-6.6	97	91	94	94	0.1	0.5	0.3	0.3	0	0 ⊙	10	C 0	SW 2	S 1
9	94.1	87.4	80.2	87.2	-1.1	-0.1	-0.3	-0.4	0.6	-4.1	83	75	72	77	1.0	1.6	1.7	1.4	7	10	10	S 7	SSW 8	SSW 8
10	79.1	79.5	79.4	79.3	0.8	2.4	1.3	1.4	3.1	-1.1	76	77	81	78	1.6	1.7	1.3	1.5	10	6	10	SW 8	SW 10	SW 7
11	82.2	82.6	80.2	81.7	2.4	2.4	1.0	1.7	3.7	0.5	87	95	90	91	1.0	0.4	0.7	0.7	10	10 ●	10	W 7	W 7	SSW 6
12	74.0	72.3	72.8	73.0	2.2	4.0	2.6	2.8	4.5	0.6	86	64	68	73	1.1	2.9	2.4	2.1	10 ●	9	9	SSW12	SSW12	SSW12
13	75.1	74.1	76.6	75.3	1.2	2.6	3.2	2.6	3.4	0.8	79	75	91	82	1.4	1.9	0.7	1.3	9	10 ●	10 ●	SE 3	ESE 4	SSW 6
14	78.7	81.0	82.6	80.8	0.1	0.2	0.0	0.1	3.4	-0.5	100	100	84	95	0.0	0.0	0.9	0.3	10 *	10	10	C 0	NW 3	WSW 5
15	73.3	63.3	62.1	66.2	-2.2	-0.3	0.6	-0.3	1.1	-3.0	81	84	94	86	1.0	1.0	0.4	0.8	10	10 *	10	SSW 8	S 12	SW 6
16	51.1	50.4	54.4	52.0	-0.6	2.0	1.2	1.0	3.2	-1.3	97	98	98	98	0.2	0.2	0.2	0.2	10 *	10	10 ●	SE 2	W 5	W 3
17	66.7	70.2	74.0	70.3	-1.4	-0.2	0.2	-0.3	2.1	-1.7	92	98	98	96	0.4	0.1	0.1	0.2	10	10 ▲	10 *	NNW 6	W 2	WNW 5
18	74.2	75.5	77.6	75.8	-0.6	-2.6	-4.4	-3.0	1.0	-5.4	95	93	93	94	0.3	0.3	0.3	0.3	10 *	10	10	WNW 4	NNE 3	N 2
19	80.4	83.0	89.0	84.1	-4.3	-4.4	-5.8	-5.1	-3.1	-6.2	91	89	87	89	0.4	0.5	0.5	0.5	10 *	10 *	10 *	NNE 2	C 0	NE 6
20	95.6	97.9	100.0	97.8	-7.0	-6.4	-12.8	-9.8	-5.0	-13.2	93	91	92	92	0.2	0.3	0.2	0.2	10 *	10 *	9	NNE 5	N 5	C 0
21	96.5	95.3	98.9	96.9	-13.5	-13.0	-17.7	-15.5	-12.6	-18.3	96	92	90	93	0.1	0.2	0.2	0.2	10 *	0	0	E 3	E 3	E 3
22	104.8	109.1	114.2	109.4	-15.8	-16.2	-16.0	-16.0	-14.2	-19.2	95	90	86	90	0.1	0.2	0.2	0.2	10 *	10 *	0	ENE 6	NNE 4	NNE 5
23	116.9	118.6	120.2	118.6	-15.0	-11.4	-12.4	-12.8	-10.7	-16.7	78	83	74	78	0.4	0.4	0.6	0.5	4	8	0	NNE 5	NNE 9	NNE12
24	119.2	118.0	116.5	117.9	-11.1	-8.4	-8.3	-9.0	-6.9	-14.8	86	89	89	88	0.4	0.3	0.3	0.3	8 *	8	6	NE 9	NE 9	E 9
25	111.8	108.4	102.4	107.5	-7.9	-8.5	-10.6	-9.4	-6.9	-11.3	90	89	84	88	0.3	0.3	0.4	0.3	10	8 *	4	E 8	ESE 6	E 5
26	95.1	91.9	89.7	92.2	-13.5	-10.2	-11.3	-11.6	-9.3	-14.4	92	81	97	90	0.2	0.5	0.1	0.3	10 *	8	10	E 2	C 0	S 1
27	88.0	87.4	88.3	87.9	-9.1	-7.9	-8.2	-8.4	-7.0	-13.2	92	90	92	91	0.3	0.3	0.2	0.3	10 *	10 *	10 *	NE 2	ENE 3	C 0
28	89.4	90.0	90.9	90.1	-10.3	-7.3	-6.5	-7.6	-6.0	-12.3	91	88	86	88	0.3	0.4	0.5	0.4	8	10 ▲	10	SW 1	SW 3	S 2
29	88.0	85.8	84.6	86.1	-11.9	-6.7	-6.1	-7.7	-4.6	-12.8	89	83	92	88	0.3	0.6	0.3	0.4	6	10 ▲	10	ESE 3	SE 3	WSW 5
30	86.9	88.8	91.1	88.9	-9.4	-9.1	-7.7	-8.5	-5.5	-10.5	95	98	93	95	0.2	0.1	0.2	0.2	10	10	10	C 0	E 1	NE 7
31	93.0	95.5	98.8	95.8	-9.8	-10.1	-13.4	-11.7	-6.9	-14.0	88	87	84	86	0.4	0.4	0.4	0.4	10 *	10 *	9	ENE 8	NE 7	ENE 6
M	92.8	92.7	93.3	92.9	-5.3	-3.7	-4.9	-4.7	-2.1	-7.3	91	88	89	89	0.4	0.7	0.5	0.5	8.9	8.4	7.7	4.3	4.7	4.4

Łódź-Lublinek $H_s = 187m$ $H_b = 187,7m$ $h_w = 11m$ Listopad - Novembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	5	0.6	.	•°0^00-3^40 •16^48 17^40 •°-21^40; =0^00-7^35 ≡°-9^30 ≡°-10^50 =-20^30 ≡°'-24
2	6	.	.	≡°'0^00-2^40 =-4^45 ≡'-0-5^48 =-8^45 ≡°-9^25 =-24
3	5	0.0	.	⚲°7^50-8^02; =0^00-24
4	6	.	.	=0^00-24
5	7	.	.	=0^00-12^30
6	7	.	.	⌓°2^00-8^00
7	7	.	.	=15^30-24
8	7	.	.	=0^00-10^30
9	6	.	.	=6^20-24; ⌓°1^00-8^00
10	6	0.4	.	•°14^50 16^40 ⚹°° 19^10 *°-24; ≫6^00-10^10; =0^00-30 9^30-24
11	5	1.2	.	*°'0^00-14^40 ⚹°-17^35; =0^00-24
12	6	2.5	.	•°6^40 8^15-12^25 ♎°-12^35 •°-13^20 •°15^45-23^05; =0^00-24
13	5	.	.	=0^00-24
14	4	2.2	.	•°15^38-48; =; ≡°0^00-22^40 ≡'-24;
15	5	8.2	.	•°9^45-20^40 21^50-23^35 ≡'-0^00-2^45 =-24
16	7	0.3	.	•°8^42 10^35 ⚲°14^45-16^05; =0^00-10^30; 15^30-24
17	7	.	.	=0^00-8^30; 15^15-24; ⌣°1^00-9^30
18	7	5.1	.	•°16^50 17^05-19^10; =0^00-10^30 18^30-24
19	8	4.2	.	•°'0^05-3^40 ⚲°8^15-45 •°'20^44-24; =0^00-7^30; 15^30-24
20	5	10.6	.	•°0^00-1^15 4^50 ⚹°14^50-15^45 *'-0 21^40 *° 22^38; =0^00-24
21	4	0.0	2	*°5^30-45; =24
22	6	0.2	pł.	=0^00-24
23	6	.	.	*°1^00 3^10-4^40 5^35; =0^00-24
24	5	0.0	.	*°17^50 20^10 ♎°-22^15; =0^00-24; ⌣'0^00-8^00
25	5	.	.	=0^00-24
26	5	0.1	.	•°21^50-24; =0^00-24
27	6	0.0	.	•°0^00-2^40 •° 7^40 •°13^40 14^50; 15^45-17^50; =0^00-24
28	4	1.4	.	=0^00-24
29	6	2.0	.	•°3^45 4^35-6^50 7^20 •°7^30-8^40 •°•°-9^10 •°13^45-14^25 •° 15^38 •°-19^40 21^40; =0^00-24
30	7	2.1	.	•°0^35 4^38-8^40 ⚲°11^15-38; 12^03-13^22; 15^02-10; 19^15-22^05 ⚲°23^40-24; ≫3^30-4^00; =0^00-9^30
31				
Σ	—	41.1	—	UWAGI

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1	7	0.3	.	⚲°0^00-1^25 9^52-12^10 19^42-22^05; 22^45-23^10
2	7	.	.	=16^55-19^30 ≡°-21^38 =-24; ⌣'-2 17^30-24
3	5	.	.	=0^00-24 ⌣°0^00-24
4	6	.	.	=0^00-24; ⌣'-0 0^00-13^30
5	3	0.4	.	•°14^40-16^40; 18^40-24; =0^00-7^50 ≡°'-19^30 ≡'-24
6	5	0.0	.	•°0^00-7^20; ≡'-0 0^00-10^25 =-21^45 ≡°'-24
7	4	.	.	≡'-0 0^00-8^40 =-24; ⌣°'18^00-24
8	4	.	.	=0^00-24; ⌣'-0 0^00-24
9	7	.	.	≫10^50-11^30; 21^30-24; =0^00-10^30; 13^30-23^30; ⌣'0^00-20^00
10	7	0.3	.	*°21^50 23^35 ≫0^00-30; 9^50-14^30
11	6	2.4	.	•°7^45-8^25 ⚹°-9^05 •°-13^45; 17^45-19^40 ⚹°22^45-24; =7^30-24; ⌣20^25-21^20
12	7	0.1	.	⚹°0^00-15 •°-1^30 *°-2^45 •°5^45-8^35 9^15 ≫5^30 21^30; =0^00-4^15
13	6	1.2	.	•°7^35-43 11^42 12^45 18^50 20^05-22^40 =7^10-24
14	4	0.1	0	•°0^45 2^47 •°3^40-7^25; =0^00-7^25 ≡°'-8^16 ≡'-0-11^45 =-24
15	6	7.6	.	*°8^25 40 *°'-20^15 35 ⚹°21^48 22^50; ≫11^10-15^30; =0^00-24; ⌧5^30-7^10
16	5	3.8	8	*°'4^35-9^00 10^00 •°; *°-10^30 •°-11^05 •°-12^15 •°-12^40; 15^50 23^10 ⚹°-24; =0^00-p.p-24
17	5	0.4	4	⚹°0^00-35 •°-2^25 *°'9^40-12^30 ♎°-16^45 *°-23^56; =0^00-24
18	5	0.3	5	*°'2^52-8^40; =0^00-13^35 ≡°-17^50 =-24
19	5	0.4	5	*°3^50-5^20 *°'6^05 8^20-17^20 24; =0^00-24
20	6	0.2	7	*°0^00 6^45 8^45-10^40 11^45-14^00 16^45; =0^00-24
21	6	0.0	7	*°1^00-3^00 6^00-7^10 8^40-9^35; =0^00-24
22	5	0.1	7	♎°5^55-6^30 *°-7^20 ♎°-12^20 *°-13^40; =0^00-24
23	6	0.0	6	≫8^30-10^20; 16^25-23^30; =0^00-21^30
24	7	0.0	6	↔5^10-6^20 *°-7^20 22^50 23^10 ≫2^20-5^15
25	7	0.0	5	*°10^40 13^45 23^50 24; =14^30-24
26	6	0.0	5	*°0^00 3^40; 6^40-8^50; 12^45-18^50; =0^00-24
27	5	0.1	5	*°0^40 8^15 14^20 15^10; 16^10-22^30 23^20-24; =0^00-24
28	5	0.0	7	*°0^00-2^40 3^30 ♎°12^40-14^25; =0^00-24
29	5	0.0	7	♎°12^44-14^40; 23^50-24; =0^00-24
30	4	0.1	7	♎°0^00-40 *° 2^45; =0^00-24
31	5	0.1	8	*°2^50 5^10-11^20 13^45; =0^00-24
Σ	—	37.9	—	UWAGI

Wrocław-Gądów Mały φ=51°08' λ=16°59' Styczeń-Janvier 1962

DNI	CIŚNIENIE P=900 I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI I	II	III	Dies	ZACHMURZENIE N.w I	II	III	POGODA	KIERUNEK I PRĘDKOŚĆ WIATRU D.v I	II	III
1	93.0	97.1	97.3	95.8	3.6	3.4	0.5	2.0	5.4	0.2	65	68	80	71	2.8	2.5	1.2	2.2	8	10	10		SW 2	WSW 7	SW 2
2	97.4	99.3	104.0	100.2	-1.8	0.2	-1.2	-1.0	0.8	-3.3	85	82	86	74	0.9	1.1	0.8	0.9	9	10	10		W 4	WNW 5	NW 2
3	107.5	108.0	110.8	108.8	-6.2	-0.4	-0.2	-1.8	0.2	-7.5	92	90	100	94	0.3	0.6	0.0	0.3	0	10	10 ●		W 7	WNW 5	C 0
4	112.6	111.4	111.6	111.9	-0.2	1.3	-2.6	-1.0	1.6	-3.2	90	72	95	86	0.6	1.9	0.2	0.9	10	1	10		SE 1	S 2	W 1
5	110.0	108.4	105.3	107.9	-4.3	-4.4	-6.2	-5.3	-1.9	-6.8	98	98	97	98	0.1	0.1	0.1	0.1	10	10	10 ≡		W 2	W 1	S 2
6	102.6	100.7	99.2	100.8	-7.7	-0.7	1.8	-1.2	2.4	-9.7	90	77	87	85	0.3	1.3	0.9	0.8	0	0	10 ●		SW 2	SW 2	W 7
7	104.1	108.7	112.4	108.4	2.2	2.2	1.2	1.7	2.7	0.8	87	80	90	86	1.0	1.5	0.7	1.1	10	8	9		WNW 6	WNW 8	W 1
8	111.8	111.9	110.1	111.3	-0.1	1.7	1.8	1.3	2.2	-3.6	88	92	94	91	0.8	0.5	0.4	0.6	10	10	10		S 3	S 1	C 0
9	105.4	102.1	101.5	103.0	1.4	1.3	0.0	0.7	2.5	-1.4	81	72	82	78	1.3	1.9	1.1	1.4	2	10	10		S 7	S 9	S 4
10	95.9	92.7	92.3	93.6	-2.2	0.5	-1.2	-1.0	1.4	-2.5	87	76	82	82	0.7	1.5	1.0	1.1	7	4	4		SSE 4	S 6	S 6
11	92.4	88.1	87.2	89.2	0.8	5.1	5.0	4.0	6.2	-1.4	88	75	79	81	0.8	2.2	1.8	1.6	3	10	10		S 5	S 9	S 9
12	90.8	89.4	81.8	87.3	3.9	5.6	3.9	4.3	6.6	1.9	87	80	74	80	1.1	1.8	2.2	1.7	10	9	10		SSE 2	SSW 6	SSE 4
13	76.7	78.9	82.4	79.3	4.0	6.4	-0.2	2.5	6.8	-0.7	82	69	90	80	1.5	3.0	0.6	1.7	7	6	8		SW 7	SW 9	S 3
14	86.9	89.4	91.8	89.4	0.0	4.3	3.2	2.7	5.3	-1.1	86	68	76	77	0.9	2.7	1.9	1.8	8	3	10		SSW 2	SSW 7	SW 7
15	97.4	101.0	105.5	101.3	2.9	4.8	-0.1	1.9	5.1	-1.4	72	64	86	74	2.1	3.1	0.9	2.0	10	9	2		WSW 7	W 9	SW 4
16	107.4	105.4	102.5	105.1	-2.9	4.5	2.7	1.8	4.8	-3.4	91	65	67	74	0.4	2.9	2.4	1.9	2	7	9		S 3	S 5	S 6
17	101.7	102.6	102.1	102.1	1.0	3.4	-0.2	1.0	3.8	-0.3	77	65	86	76	1.5	2.8	0.8	1.7	9	10	8		SE 3	SE 3	C 0
18	100.4	99.9	101.1	100.5	-2.9	4.3	2.4	1.6	4.8	-3.4	93	66	79	79	0.3	2.8	1.6	1.6	6	9	9		C 0	SSW 4	S 1
19	102.4	102.2	98.3	101.0	1.1	4.8	4.7	3.8	5.4	0.7	89	79	81	83	0.7	1.8	1.6	1.4	9	8	10 ●		S 1	SSW 4	S 5
20	101.8	103.6	108.7	104.7	4.9	8.4	1.3	4.0	8.6	0.9	75	69	83	76	2.2	3.4	1.1	2.2	2	4	5 ✳		WSW 8	W 11	WSW 3
21	106.2	105.9	103.5	105.2	5.0	6.8	7.1	6.5	7.4	-0.8	86	94	88	89	1.2	0.6	1.2	1.0	10	10 ●	9		SW 4	SW 5	SW 6
22	96.4	91.7	96.7	94.9	5.2	9.2	3.3	5.2	9.3	3.0	86	63	74	74	1.2	4.2	1.9	2.4	9	10	5		S 3	SW 10	WSW 5
23	100.1	101.4	103.5	101.7	0.6	5.6	1.8	2.4	6.2	0.6	88	67	85	80	0.8	2.9	1.1	1.6	1	8	7		SSW 4	SW 9	SW 7
24	104.7	101.9	98.7	101.8	1.6	3.8	1.9	2.3	4.4	0.8	83	87	96	89	1.2	1.1	0.3	0.9	9	10	10 ●		SW 6	SSW 5	S 4
25	94.1	93.2	95.2	94.2	6.1	8.0	6.4	6.7	9.7	1.9	92	85	97	91	0.7	1.5	0.3	0.8	10	9	5		SSW 4	SW 5	W 6
26	102.6	104.9	100.5	102.7	2.4	3.4	0.8	1.8	6.7	0.8	95	75	98	89	0.4	2.0	0.2	0.9	10	7	10 ✳		NW 1	W 3	SE 3
27	101.6	103.1	102.3	102.3	3.6	4.8	1.9	3.0	5.5	0.6	91	76	96	88	0.7	2.0	0.3	1.0	8 ●	8	10 ✳		WNW 7	WNW 10	NW 4
28	100.6	100.4	104.4	101.8	2.0	-0.8	-4.8	-2.1	2.9	-4.9	91	85	93	90	0.7	0.9	0.3	0.6	10	8	10 ✳		WNW 6	NNW 7	WNW 8
29	108.9	112.4	116.6	112.6	-4.1	-5.2	-6.7	-5.7	-4.1	-6.7	87	73	75	78	0.6	1.1	0.9	0.9	10	9	10 ✳		NNW 5	NNW 7	N 5
30	119.5	121.6	124.0	121.7	-8.9	-6.6	-9.3	-8.5	-5.9	-10.9	86	86	88	87	0.4	0.5	0.4	0.4	10 ✳	10	0		N 4	NNE 5	NNW 3
31	122.8	121.2	117.2	120.4	-18.8	-9.0	-14.2	-14.0	-7.7	-18.8	95	76	92	88	0.1	0.7	0.2	0.3	0	8	0		C 0	NE 1	NE 1
M	101.8	101.9	102.2	102.0	-0.3	2.5	0.2	0.6	3.5	-2.6	87	77	86	83	0.9	1.8	0.9	1.2	7.1	7.9	8.1		3.9	5.8	3.8

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1	106.2	101.4	102.4	103.3	-9.6	-7.4	-9.9	-9.2	-6.0	-15.3	88	71	84	81	0.4	1.0	0.4	0.6	10	7	0		NE 2	SSE 6	SSE 1
2	102.6	102.8	105.8	103.7	-7.6	-1.9	-2.9	-3.8	-1.2	-15.7	84	60	93	79	0.5	2.1	0.3	1.0	10	6	10		C 0	S 2	C 0
3	109.8	111.7	111.8	111.1	-3.0	0.4	-3.0	-2.2	0.8	-3.2	95	87	99	94	0.3	0.8	0.0	0.4	10	10	0 ≡		C 0	NW 1	WSW 1
4	105.5	104.6	107.0	105.7	-5.3	1.1	-1.8	-2.0	2.2	-6.0	95	81	93	90	0.2	1.2	0.4	0.6	7	10	0		S 2	W 6	WSW 4
5	100.4	90.1	94.6	95.0	-1.8	0.4	2.6	1.0	3.4	-4.6	88	100	77	88	0.7	0.0	1.7	0.8	9	10 ✳	9		S 4	S 7	W 11
6	101.3	104.6	106.7	104.2	2.2	2.4	1.0	1.6	3.4	0.8	80	86	90	85	1.5	1.1	0.7	1.1	1	10 ●	6		W 8	W 10	W 2
7	103.9	101.6	97.9	101.1	1.0	4.6	1.6	2.2	5.7	-2.0	92	82	91	88	0.5	1.5	0.7	0.9	10	9	3		S 3	SSE 2	S 2
8	95.5	97.4	100.4	97.8	1.1	4.6	2.3	2.6	5.3	0.4	92	82	93	89	0.5	1.5	0.5	0.8	10	10 ●	10		SE 2	S 2	S 2
9	105.8	111.3	117.2	111.4	2.2	1.9	-0.2	0.9	2.8	-0.5	93	78	86	86	0.6	1.5	0.8	1.0	10 ●	9	1		NW 5	WNW 7	C 0
10	118.9	117.5	114.9	117.1	-3.1	3.6	0.4	0.3	4.1	-5.7	97	68	86	84	0.1	2.5	0.9	1.2	1	9	9		SW 1	SSW 2	S 1
11	109.4	110.3	114.3	111.3	1.2	3.2	0.6	1.4	5.2	-1.2	75	88	79	81	1.7	0.9	1.4	1.3	9	8	3		SSW 3	WNW 10	WSW 5
12	98.5	84.4	76.4	86.4	2.0	4.4	2.5	2.8	8.2	-1.4	62	79	93	78	2.7	1.8	0.5	1.7	10	10 ●	10 ●		SSW 9	SW 14	NW 9
13	74.0	71.8	74.1	73.3	2.3	2.3	-1.0	0.6	4.6	-1.4	89	87	94	90	0.8	0.9	0.4	0.7	10	10	4		W 8	WSW 5	W 4
14	78.7	80.1	86.3	81.7	-0.6	1.3	-1.4	-0.5	2.0	-1.9	81	67	82	77	1.1	2.2	1.0	1.4	3	6	10		NW 7	WNW 4	NNW 3
15	96.5	101.7	107.2	101.8	-2.8	-1.9	-5.0	-3.7	-0.9	-5.7	95	73	73	80	0.2	1.4	1.1	0.9	10 ✳	8	6		NNW 6	NNW 7	W 5
16	93.0	83.4	78.6	85.0	-2.6	2.6	2.8	1.4	5.5	-6.4	85	75	77	79	0.8	1.9	1.7	1.5	10 ✳	10 ●	6		SSW 11	SW 9	W 13
17	77.0	80.3	88.2	81.8	2.4	2.4	0.2	1.3	3.7	-0.9	86	86	98	90	1.1	1.1	0.1	0.8	10	9 ✳ ●	10		W 14	W 18	WNW 13
18	97.4	102.5	108.2	102.7	-1.6	0.5	0.2	-0.2	2.5	-2.5	88	76	70	78	0.6	1.3	1.9	1.3	5 ✳	4 ⊙	6		NW 7	WNW 10	NW 4
19	103.9	104.5	106.3	104.9	-0.6	2.4	3.8	2.4	4.2	-3.2	97	96	95	96	0.2	0.3	0.4	0.3	10 ✳	10 ●	10		SSW 3	WNW 6	W 7
20	106.9	106.1	105.0	106.0	3.0	5.6	6.1	5.2	6.8	2.5	84	80	79	81	1.2	1.8	2.0	1.7	10	9	4		W 7	W 8	WNW 8
21	109.2	111.3	114.7	111.7	0.2	1.2	-1.2	-0.2	6.4	-1.5	78	70	89	79	1.4	2.0	0.6	1.3	0	10	10 ✳		NW 2	NNW 9	NNW 3
22	118.6	119.2	121.0	119.6	-4.2	-3.4	-4.2	-4.0	-0.9	-4.4	79	83	89	84	0.9	0.8	0.3	0.7	10	10 ✳	10		NNE 7	NE 3	NNE 3
23	121.2	117.8	112.4	117.1	-5.4	-2.5	-1.0	-2.5	-0.3	-7.0	72	78	81	77	1.1	1.1	1.1	1.1	10	8	10 ✳		W 3	WNW 4	NNW 4
24	107.6	105.4	106.1	106.4	-2.6	-3.7	-5.3	-4.2	-0.5	-5.4	83	80	93	85	0.9	0.9	0.3	0.7	10 ✳	10 ✳	10 ✳		NNE 3	NNE 6	NE 2
25	107.7	108.1	108.7	108.2	-7.4	-4.8	-6.2	-6.2	-4.2	-7.6	93	74	78	82	0.2	1.1	0.8	0.7	10 ✳	5	10		E 3	E 4	ESE 6
26	107.5	106.9	106.1	106.8	-4.8	-2.2	-2.8	-3.2	-1.6	-6.5	86	74	73	78	0.6	1.3	1.3	1.1	10	8	8		ESE 2	SE 4	ENE 2
27	104.3	103.5	102.7	103.3	-2.4	-1.2	-2.3	-2.0	-0.5	-4.7	91	82	98	90	0.4	1.0	0.1	0.5	10	10 ⌂	10 ✳		NE 2	E 5	E 2
28	100.0	98.3	97.1	98.5	-3.4	-1.3	-1.8	-2.1	-0.9	-3.6	97	86	88	90	0.2	0.8	0.7	0.6	10	10 ✳	10		E 1	NE 2	NE 2
29																									
30																									
31																									
M	102.2	101.4	102.6	102.1	-1.8	0.5	-0.9	-0.8	2.1	-4.2	87	80	86	84	0.8	1.3	0.8	1.0	8.4	8.8	7.0		4.5	6.2	4.2

Wrocław-Gądów Mały $H_s = 116m$ $H_b = 118,6m$ $h_w = 20m$ Styczeń - Janvier 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	•	4	
2	7	•	pł.	$=7^{30}-11^{20}, 13^{30}-15^{40}, 20^{30}-22^{10}$
3	6	0.0	•	$\text{☂}^{\circ}10^{25-37}, 11^{07}-12^{30}\ast^{\circ}13^{13\ldots25}\text{☂}^{\circ}15^{10}-24; =11^{40}-16^{40}\equiv^{\circ}-19^{10}\doteq-24$
4	6	•	pł.	$\text{☂}^{\circ}0^{00}-1^{25}; =0^{00}-24$
5	4	0.0	pł.	$\ast^{\circ}9^{10-20}; =0^{00}-7^{20}\equiv^{\circ}-9^{50}=, \equiv^{\circ-1}-21^{20}$
6	6	0.2	pł.	$\ast^{\circ}17^{45}-18^{40}\bullet^{\circ}20^{20}-24; =0^{00}-24$
7	7	0.0	pł.	$\bullet^{\circ}0^{00-10}\text{☂}^{\circ}-1^{10}\bullet^{\circ}2^{35}-3^{40}\bullet\text{☂}^{\circ}-4^{00}\bullet^{\circ}-4^{05}\,5^{40}-6^{30}; =0^{00}-8^{30}$
8	5	0.8	pł.	$\ast^{\circ}5^{50}\ldots6^{36}\text{☂}^{\circ}7^{35}\ldots8^{10}\triangle8^{20-26}\ast^{\circ}\ldots8^{32}\ast^{\circ}\ldots9^{15}\bullet^{\circ}9^{30}\ldots10^{20}; =7^{30}-24$
9	7	0.0	pł.	$\bullet^{\circ}22^{40}\ldots23^{10}; =0^{00}-8^{30}, 20^{30}-24$
10	7	•	pł.	$=0^{00}-4^{40}, 16^{30}-21^{30}$
11	7	2.2	pł.	$\bullet^{\circ}14^{08-12}, 16^{50}-20^{50}; =8^{30}-9^{30}$
12	7	0.8	•	$\bullet^{\circ}1^{40}\ldots4^{50}; =16^{20}-18^{10}$
13	7	•	•	$\bullet^{\circ}1^{30}\ldots2^{43}, 5^{12}-5^{40}; =15^{30}-16^{20}$
14	8	0.3	•	$\bullet^{\circ}17^{23}-18^{25}$
15	7	0.0	•	$\bullet^{\circ}8^{45}\ldots9^{12}; \smile^{\circ}23^{00}-24$
16	7	•	•	$=7^{45}-11^{50}; \smile'0^{00}-9^{55}; \varpi\,21^{30}-22^{20}$
17	8	•	•	$\varpi\,19^{30}-21^{30}$
18	6	•	•	$=0^{50}-4^{50}, 7^{20}-20^{30}; \smile^{\circ}3^{50}-9^{00}; \varpi\,17^{50}-18^{30}$
19	6	1.0	•	$\bullet^{\circ}9^{30}-12^{55}, 20^{50}\ldots22^{20}; =1^{30}-24$
20	8	•	•	$\bullet^{\circ}0^{30}\ldots1^{20}, 2^{50}-4^{15}; =0^{00}-5^{20}, 16^{30}-21^{15}; \triangle^{\circ}$ zm. $20^{00}-24$
21	6	3.0	•	$\bullet^{\circ}7^{42}\ldots8^{30}-14^{40}\text{☂}^{\circ}-15^{45}; =8^{30}-23; \triangle\,0^{00}-2^{00}$
22	8	•	•	$\ast\!\!\ast\,12^{50}-13^{15}, 18^{05-25}; \varpi'4^{40}-7^{00}$
23	8	•	•	$=16^{30}-17^{30}; \smile^{\circ}3^{00}-8^{00}$
24	6	11.4	•	$\ast^{\circ}9^{25}-10^{08}\,10^{45}-11^{10}\bullet^{\circ}-12^{40}, 16^{35}\ldots18^{30}-22^{35}\bullet'-24; =8^{20}-15^{15}$
25	7	5.0	•	$\bullet'0^{00}-1^{10}\bullet^{\circ-1}2^{20}-6^{45}\bullet^{\circ}8^{30}-10^{45}, 11^{40}\ldots12^{45}\text{☂}^{\circ}14^{35}-15^{15}\text{☂}'18^{10\ldots45}; =1^{10}-12^{50}, np$
26	7	1.6	•	$\bullet'2^{05-15}\,2^{25}-5^{40}\ast^{\circ}19^{40}\ldots20^{20}-21^{20}\ast^{\circ}-22^{20}\bullet^{\circ}-24; =0^{00}-11^{30}, 20^{20}-24$
27	7	2.4	•	$\bullet^{\circ}0^{00}-1^{50}\text{☂}\,3^{15}-5^{40}\bullet^{\circ}6^{40}\ldots24\ast'20^{30}-21^{10}; =0^{00}-6^{50}$
28	6	2.3	•	$\bullet^{\circ}0^{00}\ldots3^{50}\ast^{\circ}\ldots8^{45}\text{☂}^{\circ}10^{10}\ldots11^{05}\text{☂}^{\circ}\ldots17^{35}\ast\,11^{45}\ldots15^{25}\ast^{\circ}17^{50}\ldots18^{50}-23^{20}; \vdash 15^{50-50}; =a$
29	7	1.2	2	$\ast^{\circ}4^{22}\ldots9^{20}\ast\!\!\ast^{\circ}12^{45}-13^{10}\ast^{\circ}\ldots14^{10}, 14^{30}-17^{30}, 20^{40}\ldots23^{20}; =0^{00}-3^{15}$
30	7	1.2	3	$\ast^{\circ}4^{40}\ldots11^{35}; =9^{30}-12^{15}, 15^{50}-24$
31	6	0.0	3	$=0^{00}-24$
Σ	—	33.4	—	UWAGI:

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1	6	0.0	3	$\ast^{\circ}0^{40}-2^{20}, 5^{35}\ldots9^{40}, 14^{15}\ldots15^{20}; =0^{00}-24$
2	6	•	3	$=0^{00}-24; \oplus\,9^{40}-12^{15}$
3	5	•	3	$=0^{00}-19^{45}\equiv^{\circ-2}-24$
4	6	0.4	2	$\ast^{\circ-1}9^{36}-11^{30}\ldots12^{02}; \equiv^{\circ}; =0^{00}-24$
5	4	4.8	2	$\ast^{\circ}9^{05}-10^{27}\ast^{\circ-2}10^{34}-14^{07}\bullet^{\circ}-14^{37}\,15^{26-40}, 17^{40}\ldots18^{15}\,22^{25}-23^{17}; \gg 20^{40}-21^{30}, np; =na, a$
6	7	0.0	pł.	$\ast^{\circ}7^{45}\ldots8^{05}\bullet^{\circ}8^{32}\ldots9^{15}\ast^{\circ}9^{27\ldots35}\bullet^{\circ}11^{40}-12^{10}\text{☂}^{\circ}-14^{18}; \gg 10^{03}-6^{20}, a-14^{30}$
7	5	•	•	$=2^{40}-24$
8	5	0.3	•	$\bullet^{\circ}12^{35}\ldots13^{07}, 14^{20}\ldots16^{05}-18^{20}; =0^{00}-24$
9	7	0.0	•	$\bullet^{\circ}6^{20}\ldots7^{30}; =0^{00}-9^{10}$
10	6	•	•	$=1^{40}-24; \smile^{\circ}2^{00}-10^{30}$
11	6	0.6	•	$\ast^{\circ}9^{40}\ldots10^{35}\ast^{\circ}10^{05-15}\ast\!\!\ast^{\circ}10^{35}-12^{17}\text{☂}^{\circ}15^{01-05}; \gg a-p; =na, a-p\,\psi\,19^{20}-24$
12	7	7.8	•	$\ast^{\circ}7^{15}\ldots7^{25}-9^{00}\bullet^{\circ}9^{45}\ldots20^{27}\text{☂}^{\circ}20^{39}\triangle^{2}-20^{45}\text{☂}^{\circ}-21^{25}\ast'-22^{27}\bullet'-23^{35}; \gg -\text{☾}\,7^{25}\ldots24; =a; \psi\,na$
13	7	0.0	•	$\bullet^{\circ}3^{20}-5^{40}, 10^{47}\ldots11^{30}; \gg na; =20^{30}-24; \smile^{\circ}22^{30}-24; \oplus\,p\varpi p$
14	8	0.8	•	$\ast^{\circ}10^{22-48}\ast-10^{57}\ast^{\circ}-11^{25}, 17^{05-15}\,19^{05-35}; =na; \smile^{\circ}0^{00}-9^{30}$
15	8	0.0	5	$\ast^{\circ}0^{45}-2^{25}\ast^{\circ-1}3^{47}-8^{20}\text{☂}^{\circ-1}13^{22}\ldots14^{52}; \gg p$
16	8	1.1	3	$\ast^{\circ}4^{40}\ldots5^{20}-7^{35}\ast\,9^{27}-10^{10}\ast^{\circ}-10^{35}\bullet^{\circ}12^{25}\ldots18^{06}; \vdash 9^{30}-10^{15}; \text{☾}\,16^{28}\ldots24; \oplus\,na$
17	7	3.6	•	$\text{☂}^{\circ}0^{40}\ldots4^{50}\text{☂}^{\circ}4^{55}, 8^{49}\ast^{\circ}10^{30}, 14^{40}\ast^{\circ}13^{50}-14^{10}\text{☂}^{\circ}15^{40}-16^{15}\text{☂}^{2-0}16^{50}\ldots24; \gg -\text{☾}\,0^{00}-np; \langle 17^{18}$
18	8	5.6	4	$\text{☂}^{2-0}0^{00}\ldots13^{30}; \vdash^{\circ}1^{30}\ldots10^{10}\vdash^{\circ}11^{10}-12^{20}\vdash^{\circ}14^{10}-15^{30}; \gg na, a-p; \varpi\,8^{45}-24$
19	6	1.6	11	$\ast^{\circ-1}1^{45}\ldots8^{08}\ast^{\circ}5^{50}-6^{35}\bullet^{\circ}8^{35}-9^{30}\text{☂}^{\circ}\ldots11^{15}\bullet\text{☂}^{\circ}-12^{20}\text{☂}^{\circ}-14^{20}\bullet^{\circ}15^{30}-19^{20}; =19^{30}-24; \varpi\,0^{00-32}$
20	6	0.0	•	$\bullet^{\circ}1^{40}\ldots2^{38}, 9^{40}-10^{35}, 17^{05}-18^{20}; \gg a, p; =0^{00}-19^{30}$
21	8	0.2	•	$\text{☂}^{\circ}10^{37-45}, 13^{40}-14^{15}\ast^{\circ}\ldots15^{00}-22^{42}$
22	6	0.1	1	$\ast^{\circ-1}7^{35}\ldots19^{10}\ast^{\circ}23^{55}-24; =0^{00}-3^{30}, 17^{34}-24$
23	7	0.0	1	$\ast^{\circ}0^{00}\ldots1^{40}, 18^{15}\ldots22^{10}; =0^{00}-6^{30}$
24	6	1.6	pł.	$\ast^{\circ}5^{38}\ldots24; =8^{30}-24$
25	6	0.2	6	$\ast^{\circ}0^{00}\ldots3^{30}-8^{20}\ldots9^{10}; =0^{00}-24$
26	6	0.0	2	$\ast^{\circ}0^{00}\ldots2^{40}\ldots6^{40}\,8^{15}-10^{20}; =0^{00}-24$
27	5	3.8	pł.	$\ast^{\circ}8^{48}\ldots9^{18}\triangle\,9^{40}-13^{43}\ast^{\circ}15^{50}\ldots16^{10}-21^{30}\ast'-22^{30}\ast^{\circ}-24; =0^{00}-24$
28	5	0.0	6	$\ast^{\circ}0^{00}-5^{50}, 7^{50}\ldots8^{20}, 9^{47}-15^{10}; =0^{00}-24$
29				
30				
31				
Σ	—	32.5	—	UWAGI:

Wrocław-Gądów Mały φ=51°08' λ=16°59' Marzec-Mars 1962

DNI	CIŚNIENIE P=900 — I	II	III	Dies	TEMPERATURA I I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N.w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D.v I	II	III
1	95.8	95.2	93.9	95.0	-4.0	-1.7	-2.9	-2.9	-0.6	-4.1	94	79	88	87	0.3	1.1	0.5	0.6	10	10	10	NNE 2	N 2	NE 2
2	91.8	90.4	90.3	90.8	-5.6	0.2	-3.4	-3.0	1.2	-6.5	95	65	85	82	0.2	2.2	0.7	1.0	6	8	2	C 0	W 3	SSW 2
3	89.9	89.5	88.7	89.4	-1.6	3.0	0.2	0.4	3.4	-4.3	88	74	94	85	0.6	2.0	0.4	1.0	10	10	10	ESE 2	S 5	C 0
4	82.9	80.7	79.5	81.0	-1.0	3.2	1.4	1.2	3.5	-4.3	99	84	98	94	0.1	1.2	0.2	0.5	7	10 ●	10 ●	E 1	N 3	NNE 2
5	81.4	81.0	78.5	80.3	0.7	3.3	2.8	2.4	4.4	0.7	100	93	98	97	0.0	0.5	0.2	0.2	10 ≡	10	10	ENE 1	ENE 3	N 2
6	83.6	91.5	100.9	92.0	-1.6	0.0	-1.2	-1.0	3.0	-1.6	98	90	97	95	0.1	0.6	0.2	0.3	10 ✳	10	10 ✳	WNW 8	WNW 8	NW 5
7	107.0	108.7	111.8	109.2	-4.7	-0.5	-5.0	-3.8	0.9	-8.7	86	70	93	83	0.6	1.8	0.3	0.9	9	7	4	NW 4	NW 6	C 0
8	113.4	114.6	113.0	113.7	-7.2	0.1	-4.3	-5.9	2.6	-11.1	99	84	94	92	0.0	1.0	0.3	0.4	3 ≡	5	0	C 0	W 4	C 0
9	110.4	107.2	102.6	106.7	-3.8	4.0	1.4	0.8	4.8	-8.6	85	62	81	76	0.7	3.0	1.3	1.7	7	6	7	SE 5	SE 9	SE 8
10	98.4	96.8	95.2	96.8	-1.0	3.0	2.2	1.6	5.0	-1.9	69	66	78	71	1.8	2.6	1.6	2.0	9	10	6	SE 4	S 6	S 3
11	93.4	92.6	90.1	92.0	1.3	7.5	2.8	3.6	10.0	-0.9	91	69	98	86	0.6	3.2	0.2	1.3	9	9	9 ●	C 0	S 1	C 0
12	86.1	83.1	82.2	83.8	2.6	4.0	1.2	2.2	5.3	1.1	100	97	89	95	0.0	0.2	0.8	0.3	10 ● ≡	10 ● ≡	10 ✳	C 0	C 0	NW 9
13	91.5	95.4	100.0	95.6	-3.6	-3.0	-4.6	-4.0	1.5	-5.3	94	77	79	83	0.3	1.1	0.9	0.8	10 ✳	9 ✳	4	NW 8	WNW 8	WNW 5
14	103.8	105.8	106.0	105.2	-6.6	-1.6	-5.8	-5.0	-0.6	-7.3	80	67	74	74	0.7	1.8	1.0	1.2	2	5	0	W 7	WNW 6	S 4
15	104.5	104.2	106.2	105.0	-6.0	-1.4	-3.6	-3.6	-0.6	-6.8	87	68	62	72	0.5	1.8	1.8	1.4	7	10	10	SE 3	SE 4	NE 1
16	107.1	108.0	108.0	107.7	-3.9	-1.8	-3.0	-2.9	-1.4	-5.1	68	67	60	65	1.4	1.8	2.0	1.7	10	10	10	N 4	NNE 9	N 7
17	104.2	101.7	102.7	102.9	-3.6	-1.1	-0.4	-1.4	0.6	-5.3	67	75	66	69	1.6	1.4	2.0	1.7	10	10 ✳	10	NNW 7	N 10	NNW 7
18	104.1	105.4	106.0	105.2	-2.7	1.2	-3.8	-2.3	2.4	-4.1	86	68	87	80	0.7	2.2	0.6	1.2	8	9 ✳	0	NNW 6	WNW 7	NW 2
19	105.9	106.5	106.0	106.1	-2.9	-2.4	-1.2	-1.9	1.4	-6.3	97	93	84	91	0.1	0.3	0.9	0.4	8	10 ✳	10	WNW 1	ESE 2	SSE 3
20	105.0	104.7	103.5	104.4	-3.1	2.6	-0.2	-0.2	3.5	-4.3	97	55	71	74	0.1	3.4	1.8	1.8	9	4	0	C 0	SW 3	E 3
21	101.8	99.6	98.5	100.0	-4.6	2.6	-0.9	-1.0	3.9	-6.2	91	53	71	72	0.4	3.5	1.6	1.8	0	9	6	E 2	NE 5	NE 3
22	96.6	95.5	94.5	95.5	-5.2	-0.2	-0.9	-1.8	0.0	-5.7	90	67	67	75	0.4	2.0	1.9	1.4	2	9	10	NE 2	NNE 4	NE 2
23	94.0	94.4	97.0	95.1	-2.4	0.6	-0.7	-0.8	1.0	-2.7	89	71	79	80	0.5	1.9	1.2	1.2	10 ✳	10	10 ✳	N 1	N 5	NNE 2
24	100.1	102.4	105.6	102.7	-2.6	2.8	-4.4	-2.2	4.0	-4.8	91	55	84	77	0.5	3.4	0.7	1.5	7	4	0	C 0	WNW 5	NE 1
25	107.3	106.8	104.9	106.3	-4.4	4.4	-0.5	-0.2	5.0	-7.4	98	51	79	76	0.1	4.2	1.2	1.8	5	5	5	C 0	SW 4	NE 2
26	103.2	100.6	97.8	100.5	-2.2	3.3	-0.6	0.0	4.8	-6.7	79	43	66	63	1.1	4.3	2.0	2.5	7	1	0	ESE 3	SSE 4	SE 6
27	92.9	89.7	88.3	90.3	-4.0	3.8	2.0	1.0	5.9	-5.0	73	54	73	67	1.2	3.7	2.0	2.3	10	5	10	ESE 4	SE 5	ENE 2
28	87.8	89.2	93.0	90.0	2.2	6.0	2.6	3.4	6.5	-4.3	91	67	91	83	0.7	3.1	0.7	1.5	10	8	6	SW 2	WNW 9	W 5
29	94.0	90.7	84.7	89.8	2.0	8.0	6.2	5.6	9.2	1.3	98	51	76	75	0.2	5.2	2.3	2.6	10	8	10	C 0	S 6	SE 6
30	81.6	81.7	78.4	80.6	7.7	13.0	10.5	10.4	15.4	5.1	89	68	80	79	1.2	4.8	2.6	2.9	10	9	9	SSW 5	S 7	SSE 5
31	74.2	77.8	82.7	78.2	11.0	12.3	6.0	8.8	14.1	5.5	75	85	92	84	3.2	2.2	0.8	2.1	10	9	10 ●	SSW 7	W 8	NW 5
M	96.6	96.5	96.5	96.5	-2.0	2.4	-0.3	0.0	3.9	-4.1	89	70	82	80	0.6	2.3	1.1	1.3	7.9	8.0	6.7	2.9	5.2	3.4

Kwiecień-Avril

1	90.2	94.2	95.4	93.3	4.1	5.0	1.2	2.9	8.7	0.7	83	83	90	85	1.4	1.5	0.7	1.2	9	8 ●	0	SSW 4	W 9	SSW 4
2	95.0	96.0	100.8	97.3	3.2	9.0	2.2	4.2	9.9	-0.4	76	63	91	77	1.9	4.2	0.7	2.3	10	7 ●	0	SSW 4	SW 10	SSW 5
3	98.6	95.5	91.1	95.1	5.4	14.6	11.0	10.5	16.4	2.1	80	42	55	59	1.8	9.6	5.8	5.7	7	9	8	SSW 6	S 11	S 8
4	86.5	85.3	81.4	84.4	7.6	10.9	8.4	8.8	14.8	5.2	66	61	85	71	3.5	5.0	1.6	3.4	9	10	10	SSE 5	S 3	C 0
5	73.1	72.8	75.9	73.9	6.7	12.7	5.2	7.4	13.6	3.8	97	47	86	77	0.3	7.9	1.2	3.1	10	9	0	S 2	WSW 5	SW 2
6	80.0	82.9	89.0	84.0	2.6	11.5	6.8	6.9	12.0	0.7	91	53	81	75	0.7	6.4	1.9	3.0	9	9	10	SW 1	NNW 2	WNW 5
7	97.5	98.5	96.1	97.4	3.4	7.7	5.0	5.3	9.4	2.9	78	40	79	66	1.7	6.3	1.8	3.3	9	6	10 ●	WNW 7	WNW 8	SSW 4
8	93.8	93.7	91.9	93.1	6.6	11.8	10.2	9.7	14.1	4.2	90	70	73	78	1.0	4.1	3.3	2.8	10	10	10	SW 5	SW 9	S 4
9	96.2	98.4	100.6	98.4	8.2	11.3	7.0	8.4	12.6	6.1	65	53	75	64	3.9	6.4	2.4	4.2	8	10	6	W 5	SSW 6	NW 3
10	106.4	107.0	108.3	107.2	3.8	9.0	6.6	6.5	10.4	1.7	85	56	69	70	1.2	5.1	2.9	3.1	7	7	10	W 5	WNW 4	NW 1
11	109.1	108.0	107.3	108.1	2.5	9.4	5.6	5.8	9.8	-0.9	93	55	86	78	0.5	5.3	1.3	2.4	7	10	9	C 0	NNE 2	W 3
12	106.0	103.6	101.9	103.8	5.2	15.1	9.0	9.6	16.4	4.0	92	47	68	69	0.7	9.1	3.7	4.5	6	0	6	C 0	C 0	SW 2
13	101.0	100.9	100.0	100.6	5.4	5.6	5.3	5.4	9.2	2.3	98	94	91	94	0.2	0.6	0.8	0.5	10	10 ●	10	WNW 1	NNW 1	C 0
14	101.7	104.3	108.6	104.9	3.4	5.9	5.0	4.8	7.2	1.3	95	86	90	90	0.4	1.3	0.8	0.8	10	10	10	WNW 5	NNE 5	NE 2
15	108.5	108.1	106.9	107.8	4.3	7.9	8.6	7.4	9.2	3.8	98	87	96	94	0.1	1.3	0.5	0.6	10	10	5	NNE 3	NNE 3	E 4
16	104.3	101.7	105.2	103.7	10.0	18.7	10.0	12.2	19.2	8.1	89	58	78	75	1.3	9.2	2.7	4.4	9	8	9	ENE 7	ESE 7	N 3
17	105.4	103.2	102.3	103.6	10.3	19.7	15.1	15.0	20.0	4.9	83	54	57	65	2.1	10.5	7.3	6.6	9	8	10	ESE 5	SSE 10	SE 6
18	99.7	99.0	98.8	99.2	12.9	22.4	16.1	16.9	23.2	11.6	67	37	58	54	4.9	17.1	7.7	9.9	8	9	10	SSE 6	S 9	SSE 6
19	99.4	100.3	101.6	100.4	15.7	24.4	16.5	18.3	25.1	13.1	58	37	70	55	7.4	19.3	5.7	10.8	9	9	9	S 8	SSW 5	SSW 3
20	104.3	103.5	102.0	103.3	14.0	23.5	17.3	18.0	25.6	11.2	91	41	58	63	1.5	17.1	8.3	9.0	6	4	6	WNW 2	C 0	E 1
21	103.9	104.1	104.5	104.2	15.7	23.8	17.5	18.6	26.3	6.6	57	42	81	60	7.6	17.1	3.8	9.5	8	1	6	SSE 3	SSW 3	NE 1
22	105.0	104.8	104.3	104.7	11.5	25.1	14.3	16.3	26.4	6.8	99	24	68	64	0.2	24.3	5.3	9.9	6	7	2	C 0	SSE 4	SE 1
23	105.7	105.5	105.1	105.4	11.5	26.6	15.9	17.5	27.1	5.4	99	26	71	65	0.2	25.8	5.3	10.4	0	0	0	C 0	E 4	NE 3
24	108.3	108.8	110.3	109.1	13.5	27.4	18.5	19.5	27.8	8.1	77	30	57	55	3.5	25.4	9.3	12.7	1	2	0	ENE 1	ENE 5	ENE 1
25	111.8	111.3	110.3	111.1	14.3	27.1	19.1	19.9	27.9	8.0	99	34	62	65	0.2	23.6	8.5	10.8	0	4	0	NE 1	ENE 3	E 2
26	107.9	104.1	99.4	103.8	13.3	25.5	18.9	19.2	27.2	6.8	81	28	60	56	3.0	23.5	8.6	11.7	3	4	10 (R)	C 0	SW 3	NW 3
27	97.0	99.1	98.8	98.3	10.7	8.5	6.4	8.0	21.6	6.0	80	89	89	86	2.6	1.2	1.0	1.6	10 ●	10	4	WNW 7	NW 7	W 2
28	90.4	90.6	93.2	91.4	5.9	6.9	5.0	5.7	8.9	5.0	86	80	92	86	1.3	2.0	0.7	1.3	10 ●	10 ●	8	WNW 9	WNW 4	NW 4
29	94.3	93.9	93.5	94.0	4.5	6.1	3.9	4.6	8.7	2.8	92	83	93	90	0.7	1.4	0.6	0.9	9	7 ⊙	3	NW 2	ESE 2	W 4
30	92.6	96.3	100.4	96.4	3.1	4.9	2.8	3.4	6.1	1.1	97	78	67	81	0.2	2.0	2.5	1.6	9	10	7	W 4	NE 5	NW 3
31																								
M	99.1	99.2	99.3	99.3	8.0	14.6	9.8	10.6	16.3	4.8	85	56	76	72	1.9	9.8	3.6	5.1	7.6	7.3	6.3	3.6	5.0	3.0

Wrocław - Gądów Mały $H_s = 116m$ $H_b = 118.6m$ $h_w = 20m$ Marzec - Mars 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	5	.	5	$=0^{00}-24$
2	6	0.0	4	$=0^{00}-24; \oplus 12^{35}-13^{40}$
3	5	0.0	pł.	$*^{\circ}2^{40}...3^{10}, 7^{40}...10^{10}; =0^{00}-24$
4	4	5.8	pł.	$\bullet^{\circ}12^{10}...14^{15}, 17^{10}...19^{10}-24; =0^{00}-24$
5	4	11.9	.	$\bullet^{\circ}0^{00}-1^{30}, \bullet^{\circ}5^{45}...7^{30}, \bullet^{\circ}18^{10}-19^{30}, 22^{10}-24$
6	6	0.3	5	$\bullet^{1-0}0^{00}-3^{40}, *^{0-1}3^{40}-9^{40}...10^{35}, *^{\circ}14^{35}...21^{35}, \triangle 16^{25}-17^{20}; \simeq 0^{00}-24$
7	8	.	8	$=0^{00}-4^{40}, 19^{30}-24; \oplus^{\circ}8^{40}-14^{15}$
8	5	.	6	$=0^{00}-3^{20}, \equiv^{2-1}3^{55}-8^{10}=-16^{15}, 18^{40}-24$
9	6	.	2	$\gg a, p, np; = 0^{00}-12^{30} \infty -17^{30}$
10	7	.	pł.	$=5^{20}-8^{35}, 16^{30}-24$
11	7	0.7	pł.	$\bullet^{\circ}11^{25...47}, 22^{25}...23^{10}-24; =0^{00}...11^{30}, 17^{20}-24; \oplus^{\circ}14^{20}-17^{15}$
12	3	10.3	pł.	$\bullet^{\circ}0^{00}...6^{40}-14^{30}, \bullet'-16^{20}, \bullet^{\circ}-20^{35}, *^{\circ}-24; \gg np; = 0^{00}-5^{50} \equiv^{0-1}-7^{20}=-12^{20} \equiv^{\circ}-16^{30}$
13	7	0.1	2	$*^{\circ}0^{00-20}, *^{\circ}-7^{30}, *^{\circ}10^{15}...14^{30}; \gg na, a, p$
14	8	0.0	1	$*^{\circ}7^{10}-8^{15}...8^{40}, *^{\circ}9^{20}-10^{07}; + 7^{30}-9^{10}$
15	6	.	1	$=5^{30}-12^{40}; \Theta 22^{10}-24$
16	8	.	1	$\Theta 0^{00}-1^{20}$
17	7	0.0	1	$*^{\circ}12^{20}...13^{20}; \gg 10^{50}-13^{30}$
18	7	0.0	pł.	$*^{\circ}12^{25-59}$
19	4	1.4	.	$*^{\circ}4^{40}...5^{05}, *^{0-1}11^{20}-13^{15}; =5^{30}-8^{30}, 19^{30}-24; \smile 1^{00}-8^{30}$
20	6	.	1	$=0^{00}-12^{45} \infty -15^{40}=17^{20}-24$
21	6	.	.	$=0^{00}-24; \text{mm}\, 6^{10}-10^{00}$
22	7	0.0	.	$*^{\circ}16^{50}-17^{20}; =0^{00}-11^{45}, 15^{30}-24$
23	6	0.0	.	$*^{\circ}1^{40}...4^{10}, 5^{40}-9^{20}, 20^{40}...21^{35}, 22^{10}...23^{15}; =0^{00}-12^{30}, 17^{10}-24$
24	7	.	.	$=0^{00}-9^{30}, 19^{15}-24$
25	6	.	.	$=0^{00}-13^{30}, 18^{30}-24; \smile 6^{10}-10^{10}$
26	8	.	.	$=0^{00}-8^{30} \infty -11^{20}=18^{30}-20^{45}; \smile 3^{00}-8^{00}$
27	7	0.0	.	$=1^{40}-10^{15}, 14^{40}-24; \text{mm}\, 17^{40}-18^{20}$
28	7	1.3	.	$\bullet^{\circ}3^{45}...9^{10}, *^{\circ}10^{02...20}, *'13^{26-27}, *^{\circ}14^{18}...20^{20}; =0^{00}-10^{50}, 18^{20}-24$
29	6	0.1	.	$\bullet^{\circ}4^{20}...6^{15}, 16^{47}...24; =0^{00}-11^{30} \infty -12^{30}=17^{30}-24$
30	8	2.1	.	$\bullet^{\circ}0^{00}...2^{40}, 9^{20}...10^{07}, 21^{59}...24; =0^{00}-6^{30}$
31	8	21.9	.	$\bullet^{\circ}0^{00}...8^{30}, *^{0-1}11^{10-45}, \bullet^{\circ}13^{30-50}, 18^{10}...18^{17}, \bullet^{0-1}-23^{15}; \gg a; = 18^{30}-24$
Σ	—	55.9	—	UWAGI.

Kwiecień - Avril

1	8	0.5	.	$\bullet^{\circ}6^{40-50}, *^{\circ}9^{22-31}, 12^{18}...15^{01}; \gg 9^{30}-12^{40}; = na$
2	7	1.6	.	$*^{0-2}11^{50}...17^{00}; \gg a-p; = 3^{40}-7^{45}; \oplus 9^{50}-10^{55}$
3	8	.	.	$\bullet^{\circ}0^{10}-2^{30}...na; \gg ap$
4	8	1.6	.	
5	8	.	.	$\bullet^{\circ}1^{45}...a; = na-a$
6	8	0.0	.	$*^{\circ}14^{06-12}; = 3^{30}-9^{30}$
7	8	3.1	.	$*^{\circ}0^{15-25}, 11^{25-31}, \bullet^{\circ}20^{45}...21^{40}, 22^{43}...23^{25}-24; =0^{00}-3^{30}$
8	8	0.0	.	$\bullet^{\circ}0^{00}-1^{40}, 2^{50}-4^{40}, 22^{00}-23^{30}$
9	8	.	.	
10	7	.	.	$=5^{20}-8^{15}; \oplus^{\circ}12^{40}-13^{30}$
11	7	0.0	.	$\bullet^{\circ}14^{45}...16^{30}; =1^{30}-10^{30}, 20^{30}-24$
12	8	.	.	$=0^{00}-10^{30}$
13	6	3.4	.	$\bullet^{\circ}8^{05}-16^{20}, 18^{10}-20^{15}; \simeq 1^{30}...5^{30}-24$
14	7	.	.	$=0^{00}-9^{30}$
15	6	0.1	.	$\bullet^{\circ}7^{10-25}, 16^{30}-17^{05}, 21^{12-45}; =1^{30}-24$
16	6	.	.	$=0^{00}-10^{40} \infty -11^{20}, 12^{20}-19^{30}=-24$
17	7	.	.	$\gg a-p; = 0^{00}-a; \Theta 2^{45}-3^{20}$
18	8	.	.	$\gg p; \infty 10^{30}-19^{30}; \Theta 20^{30}-24$
19	8	.	.	$\frown np; \Theta 0^{00-30}, 2^{50}-4^{07}$
20	6	.	.	$=1^{30}-11^{30} \infty -13^{30}; \frown 0^{00}-8^{00}, 22^{40}-24; \oplus 9^{00}-10^{30}$
21	7	.	.	$=1^{30}-5^{40} \simeq 23^{30}-24; \frown^{\circ} 0^{00}-7^{00}, 20^{00}-24$
22	8	.	.	$\simeq 0^{00}-2^{50} \equiv^{0-1}-6^{20} \simeq -9^{30}; \frown^{0-2} 0^{00}-7^{00}, 22^{00}-24$
23	8	.	.	$=0^{30}-3^{10} \simeq 2^{45}-5^{30}=4^{50}-7^{30}; \frown^{\circ} 0^{00}-8^{00}$
24	7	.	.	$\simeq 3^{20}-8^{30} \simeq 4^{20}-5^{30} \infty a-24; \frown' 1^{00}-7^{00}, np$
25	7	.	.	$\infty' 0^{00}-1^{30} \simeq -11^{00} \simeq 2^{40}-6^{40}; \frown' 0^{00}-8^{00}$
26	7	4.0	.	$*^{\circ}16^{46-58}; (R) 20^{45}-24$ SW-NE; $\frown 21^{15-55}; = 1^{30}-9^{00} \simeq 3^{50}-5^{30} \infty -12^{30} \frown^{\circ} 0^{30}-10^{30}$
27	8	1.4	.	$\bullet^{\circ}6^{30...37}, *^{\circ}11^{10}...14^{14}, \bullet^{\circ}22^{50...59}; (R) 0^{00-55}$ SW-NE
28	7	4.9	.	$*^{\circ}1^{32...p}$
29	8	5.4	.	$*^{\circ}0^{10-30} \blacktriangle 11^{07-10}, *^{0-1}11^{26}...13^{46} \blacktriangle 11^{42-44}; (R) 13^{50}-14^{05}$ S
30	7	0.0	.	$*^{\circ}1^{50}-4^{50}, 5^{50}-6^{10}, \bullet^{\circ}7^{30}-8^{10}, 10^{12}...11^{15}$
31				
Σ	—	26.0	—	UWAGI.

Wrocław-Gądów Mały φ=51°08' λ=16°59' Maj - Mai 1962

DNI	CIŚNIENIE P= 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	100.0	97.0	94.9	97.3	0.8	6.8	2.6	3.2	7.6	-4.0	76	50	95	74	1.6	4.9	0.4	2.3	6	9	10●	W 4	W 7	WNW 3
2	90.8	91.8	95.4	92.7	3.6	4.0	2.4	3.1	8.6	1.3	91	95	91	92	0.7	0.4	0.7	0.6	9	9	1	SSW 3	WNW 3	NNE 1
3	96.3	95.6	94.4	95.4	3.8	7.4	6.0	5.8	9.6	0.0	92	76	100	89	0.7	2.5	0.0	1.1	8	10	10●	NNW 1	SW 5	NNE 2
4	92.4	92.9	95.0	93.4	5.9	9.0	2.9	5.2	10.2	2.6	77	64	95	79	2.1	4.1	0.4	2.2	9	9●	2	WNW 5	WNW 5	N 1
5	96.6	98.5	101.8	99.0	4.6	9.3	6.8	6.9	9.7	-0.5	92	72	90	85	0.7	3.2	1.0	1.6	10●	10	10	SW 1	NW 4	C 0
6	104.9	103.8	101.9	103.5	4.2	14.2	12.5	10.8	16.2	0.5	100	50	62	71	0.0	8.1	5.5	4.5	3	1	9	C 0	SE 4	SE 4
7	100.3	101.2	101.1	100.9	11.1	17.3	14.7	14.4	19.8	9.1	97	81	97	92	0.3	3.7	0.5	1.5	10●●	7	9	C 0	W 5	SW 1
8	99.3	99.0	98.0	98.8	14.9	21.9	14.5	16.4	22.2	11.3	87	68	99	85	2.2	8.6	0.2	3.7	5	5	10	WSW 2	WSW 4	W 1
9	100.5	99.5	95.8	98.6	13.0	18.5	15.9	15.8	20.0	11.2	86	56	71	71	2.1	9.5	5.3	5.6	5	10	10	WNW 3	W 1	ENE 4
10	94.6	97.0	97.9	96.5	13.1	16.9	10.3	12.6	18.2	10.3	95	62	96	84	0.7	7.3	0.5	2.8	10	8	1	W 7	W 11	WSW 4
11	98.3	97.9	98.0	98.1	10.9	13.9	9.0	10.7	16.2	5.4	87	68	88	81	1.6	5.1	1.4	2.7	2	6	4	W 2	S 3	S 4
12	99.9	99.5	100.7	100.0	9.8	17.2	11.3	12.4	17.8	4.1	90	58	89	79	1.3	8.2	1.5	3.7	2	6	10	C 0	ENE 2	W 5
13	100.8	101.1	99.4	100.4	10.9	14.7	11.9	12.4	15.6	8.7	91	69	94	85	1.1	5.2	0.8	2.4	10	8	10●	SE 3	WNW 2	NNE 1
14	91.2	88.2	91.4	90.3	7.5	8.1	7.8	7.8	12.1	7.1	99	94	91	95	0.2	0.6	0.9	0.6	10●	10●	10●	N 2	NNW 7	W 11
15	92.4	94.1	96.6	94.4	7.4	7.9	8.6	8.1	11.4	6.8	93	90	93	92	0.8	1.0	0.8	0.9	10●	10●	10●	W 13	WNW10	W 7
16	99.1	102.1	101.6	100.9	8.4	9.6	5.9	7.4	11.5	5.7	94	65	80	80	0.6	4.2	1.9	2.2	8	9	6	W 7	W 8	W 2
17	99.4	98.3	98.5	98.7	9.9	14.9	11.0	11.7	16.4	4.4	77	71	89	79	2.8	4.8	1.5	3.0	10●	9●	8	SSW 5	SSW 9	WSW 4
18	100.3	102.9	104.1	102.4	10.1	14.3	10.7	11.4	17.4	7.0	85	64	84	78	2.0	5.6	2.1	3.3	9	2⊙	9	W 2	W 7	ENE 2
19	101.8	96.6	92.3	96.9	9.9	21.0	17.9	16.7	23.1	5.6	87	59	72	73	1.6	10.1	5.7	5.8	1	2⊙	8	SE 4	SE 5	ESE 4
20	97.1	98.6	100.5	98.7	9.6	11.5	9.3	9.9	18.0	9.1	99	96	97	97	0.2	0.5	0.3	0.3	10●	10●	9	W 5	N 1	C 0
21	102.5	101.5	100.2	101.4	10.0	14.5	9.8	11.0	16.0	7.4	81	59	78	73	2.4	6.8	2.7	4.0	9	9	6	WNW 2	NE 1	SSE 4
22	97.7	98.4	101.2	99.1	11.0	14.6	13.0	12.9	17.2	6.1	75	74	79	76	3.2	4.3	3.1	3.5	9	10	9	SSE 5	SSW 3	WSW 4
23	103.2	102.0	101.1	102.1	12.3	18.7	13.5	14.5	19.9	7.1	83	56	87	75	2.4	9.6	2.0	4.7	7	7	4	S 5	WSW 6	N 1
24	105.2	104.2	101.9	103.8	11.1	13.2	11.2	11.7	13.7	10.1	83	61	85	76	2.3	6.0	2.0	3.4	10	10	10	NW 5	SW 2	SE 5
25	100.6	100.4	100.3	100.4	9.2	14.3	10.4	11.1	15.2	8.1	96	54	95	82	0.4	7.4	0.6	2.8	10	8	10●	SW 1	S 2	NNW 1
26	97.1	95.6	97.5	96.7	9.3	10.9	6.2	8.2	11.3	6.1	95	94	98	96	0.6	0.8	0.2	0.5	10	10●	5≡	N 1	NNE 1	C 0
27	101.0	101.9	102.6	101.8	9.5	13.9	8.9	10.3	14.9	6.1	93	64	94	84	0.8	5.7	0.6	2.4	10	10	4	SW 2	SSW 2	NE 1
28	102.0	99.7	100.0	100.6	12.0	17.5	11.9	13.3	19.7	6.6	84	68	89	80	2.2	6.4	1.5	3.4	9	10	9	NE 2	E 4	W 2
29	102.1	102.7	103.0	102.6	12.8	18.0	12.8	14.1	19.6	6.1	70	52	79	67	4.4	9.8	3.1	5.8	6	8	10	W 4	SW 5	W 1
30	104.7	104.0	103.8	104.2	11.0	17.1	13.1	13.6	18.7	9.6	79	44	69	64	2.7	10.9	4.6	6.1	8	4	10	W 2	W 6	WSW 2
31	101.6	97.5	97.6	98.9	14.0	20.8	13.6	15.5	21.3	7.6	59	40	67	55	6.6	14.8	5.2	8.9	3	5⊙	9	NW 1	SSW 7	NW 1
M	99.2	98.8	99.0	99.0	9.4	13.9	10.2	10.9	15.8	6.0	87	67	87	80	1.7	5.8	1.8	3.1	7.7	7.8	7.8	3.2	4.6	2.7

Czerwiec - Juin

1	102.4	103.4	102.0	102.6	7.7	10.2	8.7	8.8	14.2	6.8	64	61	65	63	3.8	4.8	3.9	4.2	8	10	10	W 5	W 3	S 5
2	102.8	105.5	107.9	105.4	7.3	10.7	9.3	9.2	14.4	5.6	97	75	66	79	0.3	3.2	4.0	2.5	10●	9	5	W 2	NW 4	WNW 2
3	110.3	110.9	111.8	111.0	6.8	10.8	6.1	7.4	14.4	1.4	86	69	89	81	1.5	4.0	1.0	2.2	2	9	5	NNW 3	W 4	W 3
4	111.8	111.3	111.5	111.5	5.7	11.0	7.7	8.0	13.8	3.2	92	62	90	81	0.8	4.9	1.0	2.2	10	9	9	WNW 3	NW 5	WNW 3
5	111.7	110.7	111.2	111.2	9.1	13.5	12.0	11.6	15.6	7.1	68	42	55	55	3.7	9.0	6.3	6.3	9	9	5	NW 6	N 5	N 5
6	113.2	113.4	113.7	113.4	6.8	13.5	10.3	10.2	16.0	3.7	75	44	46	55	2.5	8.7	6.7	6.0	2	4	1	NNW 5	N 6	N 6
7	113.0	115.0	114.4	114.1	6.1	11.7	9.5	9.2	14.6	5.1	79	52	74	68	2.0	6.5	3.1	3.9	9	10	5	N 3	NNE 5	W 1
8	115.1	114.7	110.9	113.6	9.5	18.3	12.7	13.3	21.9	1.7	71	38	70	60	3.4	15.0	4.4	6.9	3	4	1	W 1	NNW 3	C 0
9	106.9	103.5	100.1	103.5	13.7	22.1	15.9	16.9	23.6	3.1	66	36	76	59	5.4	17.1	4.4	9.0	0	1	6	W 4	SW 2	NNW 3
10	99.6	98.1	96.4	98.0	15.4	21.0	16.3	17.2	23.1	7.7	75	43	79	66	4.4	14.1	3.8	7.4	0	3	8	C 0	WNW 1	C 0
11	95.4	94.9	96.5	95.6	15.4	19.3	14.1	15.7	19.6	12.1	74	60	62	65	4.6	9.0	6.1	6.6	9	9	9	C 0	W 6	WNW 3
12	100.0	100.7	101.9	100.9	11.1	13.7	10.3	11.4	15.6	9.3	64	44	75	61	4.8	8.7	3.1	5.5	9	8	7	W 6	W 7	C 0
13	104.0	103.7	102.4	103.4	11.3	17.4	14.6	14.5	19.6	2.4	72	37	52	54	3.8	12.5	8.0	8.1	0	5	7	WNW 1	ESE 2	SE 5
14	100.8	100.4	100.7	100.6	14.9	22.4	19.9	19.3	26.0	9.1	62	45	67	58	6.4	15.0	7.7	6.4	5	8	2	SSE 3	SW 3	SSE 4
15	103.0	105.7	105.1	105.3	17.9	28.0	21.9	22.4	29.4	9.1	77	41	64	61	4.8	22.3	9.4	12.2	1	1	3	WSW 4	W 1	SSE 2
16	104.7	103.1	104.0	103.9	21.1	30.5	19.5	22.6	31.4	13.8	68	41	89	66	7.9	25.6	2.4	12.0	1	2	10	ESE 1	SE 3	C 0
17	107.7	107.8	106.9	107.5	18.1	21.4	19.1	19.4	24.0	17.4	88	61	78	76	2.5	10.0	4.8	5.8	10	10	8	NNW 4	NW 5	NNE 1
18	106.7	105.2	103.1	105.0	17.7	23.2	17.7	19.1	25.2	14.0	78	51	79	69	4.4	14.0	4.2	7.5	9	6	0	NE 1	E 1	E 2
19	101.5	99.7	96.5	99.2	18.1	24.2	21.9	21.5	28.1	14.3	78	58	67	68	4.7	12.6	8.8	8.7	9	10●	8	SE 5	SSE 2	SSE 4
20	103.5	105.9	104.0	103.8	15.5	20.7	16.8	17.4	23.0	14.1	86	51	77	71	2.4	12.1	4.4	6.3	7	10	5	W 3	WSW 1	SW 2
21	106.3	106.2	107.5	106.7	17.9	24.6	17.7	19.5	25.4	10.6	79	42	78	66	4.2	18.0	4.4	8.9	3	9	2	SW 3	W 6	C 0
22	109.6	108.7	106.8	108.4	17.3	25.0	19.9	20.5	26.6	10.0	82	48	77	69	3.5	16.6	5.3	8.5	2	2	1	C 0	SW 2	SSE 1
23	106.5	105.4	103.7	105.2	21.4	28.9	24.0	24.6	30.4	13.1	67	44	66	59	8.4	22.4	10.1	13.6	1	3	5	SSW 2	W 4	WNW 2
24	103.3	103.1	101.1	103.2	19.5	28.3	21.1	22.5	30.2	16.6	82	44	59	62	4.1	21.4	10.3	11.9	6	4	0	C 0	SSW 3	C 0
25	103.3	104.8	106.3	104.9	17.5	20.5	13.9	16.4	22.5	13.7	63	36	61	53	7.4	15.5	6.2	9.7	9	5⊙	1	WNW 3	W 10	WSW 1
26	104.7	101.5	97.1	101.1	11.8	19.2	17.4	16.4	21.6	6.8	76	42	54	57	3.3	12.9	9.1	8.4	3	7	7	SW 1	SW 2	SE 3
27	98.5	99.7	100.4	99.5	12.1	15.5	9.9	11.8	17.4	7.9	77	48	81	69	3.2	9.2	2.4	4.9	7	6	1	W 5	W 9	WSW 4
28	100.4	98.2	95.8	98.1	10.5	13.3	9.4	10.7	14.5	7.5	70	49	93	71	3.8	7.9	0.8	4.2	5	7	10	W 8	W 9	WSW 6
29	97.4	99.9	100.4	99.2	8.9	11.7	11.1	10.7	15.9	8.4	92	77	72	80	0.9	3.1	3.7	2.6	10	10	8	W 8	W 9	WSW 3
30	100.4	101.6	103.3	101.8	10.3	13.8	12.3	12.2	14.8	8.3	78	61	64	68	2.7	6.2	3.1	4.7	10	10	10	WNW 8	W 7	W 2
31																								
M	105.0	104.7	104.1	104.6	13.2	18.8	14.7	15.4	21.1	8.8	76	50	71	66	3.9	12.0	5.2	7.0	5.6	6.7	3.3	3.3	4.3	2.3

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	0.6	·	$\overset{*}{\bullet}{}^{\circ}16^{10-17}\,18^{16-35}\,\bullet^{\circ}20^{40-21^{30}}\,\bullet^{\circ}-23^{20}\,\sqcup\,4^{00-6^{00}}\,\triangle^{\circ}-7^{00}$
2	8	1.7	·	$\overset{*}{\bullet}{}^{\circ}4^{30}\ldots6^{35}\,11^{15}\ldots12^{50}\,\blacktriangle\,11^{25-27}\,\overset{*}{\bullet}{}^{\circ}12^{14-50}\,=0^{40-9^{40}}\,np;\,\triangle^{\circ}20^{00}-24$
3	8	5.0	·	$\overset{*}{\bullet}{}^{\circ}9^{40}\ldots12^{45}\,\bullet^{\circ}15^{40-50}\,16^{12-24}\,=0^{00-5^{30}}\,\triangle^{\circ}0^{00-9^{30}}\oplus12^{40-13^{58}}$
4	8	0.1	·	$\bullet^{\circ}0^{00-2^{50}}\,\overset{*}{\bullet}{}^{\circ}11^{36}\ldots12^{59}\,17^{01-05}\,=2^{50-7^{30}}\,19^{30-24}=20^{30-21^{30}}$
5	7	0.0	·	$\overset{*}{\bullet}{}^{\circ}5^{25}\ldots7^{30}\,15^{57-17^{57}}\,=0^{00-11^{51}}\,19^{30-24}\,\sqcup^{\circ}na\,\triangle^{\circ}20^{00-23^{00}}$
6	7	0.0	·	$=0^{00-40}\,\overset{*}{=}{}^{0-2}-6^{30}=-10^{40}\infty-12^{30}\,\triangle'0^{00-6^{00}}\,\triangle^{\circ}-10^{30}$
7	6	6.1	·	$\bullet\bullet^{\circ}2^{57-4^{50}}\,6^{35-8^{20}}\,\overset{*}{\bullet}{}^{0-2}12^{20}\ldots16^{20}\,=2^{57-13^{30}}\,19^{10-24}$
8	7	6.4	·	$\overset{*}{\bullet}{}^{1-0}3^{15-40}\,\bullet^{\circ}\ldots3^{58}\,\overset{*}{\bullet}{}^{\circ}16^{35-19^{10}}\,\mathrm{R}\,3^{25-40}\,(\mathrm{R})^{\circ}13^{40-45}\,\mathrm{R}\,17^{00-50}\,=0^{00-12^{30}}=na=19^{30-24}\,\triangle^{\circ}na$
9	8	10.4	·	$\bullet^{\circ}15^{30}\ldots24\,=0^{00-7^{30}}\,\oplus11^{40-13^{40}}$
10	7	0.9	·	$\bullet^{\circ}0^{00-6^{37}}\,\overset{*}{\bullet}{}^{0-1}16^{25-18^{15}}\,\gg a-p;\,\triangle^{\circ}np$
11	8	0.3	·	$\bullet^{\circ}10^{30-11^{15}}\,p;\,\mathrm{R}\,10^{30-11^{15}}\,\gg10^{57-59}\,=na;\,\triangle^{\circ}na-a,np$
12	8	0.4	·	$\overset{*}{\bullet}{}^{\circ}17^{36-49}\,\bullet^{\circ}22^{40}\ldots23^{05}\,(\mathrm{R})^{\circ}17^{21-18^{21}}\,SW-W\,=na=na;\,\triangle^{\circ}0^{00-9^{00}}$
13	8	10.5	·	$\bullet^{\circ}0^{30-4^{27}}\,18^{47}\ldots22^{10}\,23^{05}\ldots24\,=1^{40-9^{30}}\,20^{30-24}$
14	6	22.1	·	$\bullet^{0-1}0^{00}\ldots1^{15-23^{30}}\ldots24;\,\gg16^{50-17^{10}}\,p-24;\,=0^{00-24}$
15	6	0.3	·	$\bullet^{\circ}0^{00-20}\,4^{00}\ldots5^{20-6^{30}}\ldots24;\,\gg0^{00}-p;\,=na$
16	8	0.0	·	$\bullet^{\circ}0^{00-1^{45}}\,\overset{*}{\bullet}{}^{\circ}9^{36-41}\,10^{47-11^{02}}\,=np;\,\triangle^{\circ}np;\,\Psi\,21^{10-23^{20}}$
17	7	0.0	·	$\bullet^{\circ}6^{40}\ldots7^{35}\,9^{25}\ldots10^{45}\,16^{10}\ldots18^{35}\,=0^{00-6^{05}}\,\triangle^{\circ}0^{00-7^{40}}\oplus12^{50-14^{00}}$
18	8	0.6	·	$\bullet^{\circ}7^{35}\ldots8^{35}\,\overset{*}{\bullet}{}^{\circ}9^{05}\ldots12^{04}\,=na,a;\,\triangle^{\circ}np$
19	8	1.3	·	$=1^{30-45}=-11^{30}\,\triangle^{\circ}0^{00-8^{00}}\,np;\,\oplus14^{40-15^{15}}$
20	7	2.0	·	$\bullet^{\circ}1^{45}\ldots2^{15-8^{10}}\,9^{25-13^{40}}\,=22^{30-24}\,\triangle^{\circ}20^{00-24}$
21	7	·	·	$=0^{00-6^{45}}\,\triangle^{0-1}0^{00-9^{00}}\,\triangle^{\circ}np$
22	8	0.0	·	$\bullet^{\circ}11^{01\ldots15}\,\overset{*}{\bullet}{}^{\circ}13^{33-41}\,15^{23-26}\,=0^{00-7^{20}}\,\triangle^{\circ}0^{00-8^{00}}\,np$
23	8	0.0	·	$=na,\,\triangle^{\circ}0^{00-10^{00}}\,20^{00-24}$
24	7	0.2	·	$\overset{*}{\bullet}{}^{\circ}0^{32-36}\,15^{35-16^{10}}\,16^{25-17^{25}}\,=1^{30-8^{30}}\,18^{30-24}\,\triangle^{\circ}na,a$
25	7	3.7	·	$\overset{*}{\bullet}{}^{\circ}16^{06-40}\,\bullet^{\circ}17^{50}\ldots18^{02}\,\bullet^{0-1}-24\,=0^{00-9^{30}}\,18^{30-24}$
26	6	2.4	·	$\overset{*}{\bullet}{}^{\circ}0^{00-35}\,4^{35-5^{16}}\,7^{40}\ldots9^{59-13^{05}}\ldots17^{10}\,=0^{00-4^{20}}\,17^{30-20^{20}}\,\overset{*}{=}{}^{0-1}-21^{15}=-24=p$
27	7	·	·	$=0^{00-8^{30}}=21^{20-22^{40}}=-24\,\triangle'21^{00-24}$
28	7	·	·	$=0^{00-9^{30}}\infty15^{30-19^{15}}\,\triangle'0^{00-9^{00}}$
29	8	0.2	·	$\overset{*}{\bullet}{}^{\circ}21^{05\ldots22}\,\bullet^{\circ}23^{15}\ldots24\,=0^{30-7^{30}}=4^{10-5^{35}}\,\triangle0^{00}-a$
30	7	0.0	·	$\bullet^{\circ}0^{00\ldots05}\,0^{16-2^{10}}\,\overset{*}{\bullet}{}^{\circ}19^{22-23}\,=4^{30-6^{10}}$
31	8	·	·	$=2^{00-9^{10}}\,\triangle^{\circ}6^{00-9^{00}}$
Σ	—	75.2	—	UWAGI

Czerwiec - Juin

1	8	5.4	·	$\bullet^{\circ}22^{50}\ldots23^{10}$
2	8	0.4	·	$\bullet^{\circ}0^{30-8^{40}}\,9^{00-10^{35}}\,\overset{*}{\bullet}{}^{\circ}11^{50-12^{15}}\,=3^{50-11^{40}}$
3	8	0.9	·	$\overset{*}{\bullet}{}^{\circ}13^{07-25}\,20^{10-40}\,=4^{20-7^{30}}\,\triangle^{\circ}1^{00-8^{00}}$
4	8	1.0	·	$\overset{*}{\bullet}{}^{0-1}6^{00}\ldots7^{35}\,\overset{*}{\bullet}{}^{\circ}11^{40}\ldots13^{42}\,\bullet^{\circ}18^{09}\ldots19^{10}\,\overset{*}{\bullet}{}^{\circ}20^{45-21^{20}}\,\triangle^{\circ}na$
5	8	0.0	·	$\overset{*}{\bullet}{}^{\circ}15^{50-16^{50}}$
6	8	·	·	
7	8	·	·	$\triangle^{\circ}np$
8	8	·	·	$=0^{30-3^{40}}=-5^{35}\,\triangle^{\circ}0^{00-9^{30}}\,\triangle'np$
9	8	·	·	$=4^{00-5^{45}}\,\triangle'0^{00-8^{00}}\,\mathrm{fm}\,6^{10-7^{35}}$
10	8	·	·	$=na=na$
11	8	·	·	
12	8	·	·	
13	8	·	·	$=na=na\,\oplus23^{00-24}$
14	8	·	·	$=22^{30-24}\,\oplus0^{00-30}$
15	8	·	·	$=0^{00-6^{30}}=4^{10-5^{30}}$
16	8	1.2	·	$\overset{*}{\bullet}{}^{\circ}19^{06-09}\,20^{15-18}\,(\mathrm{R})\,17^{35-19^{05}}\,SW-S\,=na,a\,\infty\,a=np$
17	8	·	·	$\overset{*}{\bullet}{}^{\circ}1^{05-45}\,(\mathrm{R})\,0^{10-1^{20}}\,S-SE\,=0^{00-9^{30}}$
18	7	·	·	$=2^{30-9^{30}}=21^{26-22^{35}}=21^{15-22^{40}}\,\triangle^{\circ}np;\,\mathrm{fm}\,np$
19	6	0.6	·	$\bullet^{\circ}12^{15}\ldots14^{15}\,\overset{*}{\bullet}{}^{\circ}21^{20-50}\,\mathrm{R}\,18^{15-39}\,SSW-NW\,=2^{20-8^{30}}\infty-14^{00}\,\triangle^{\circ}2^{00-8^{00}}$
20	8	·	·	$\overset{*}{\bullet}{}^{\circ}1^{45-4^{45}}\,\oplus12^{30-14^{20}}\,15^{30-18^{30}}$
21	8	·	·	$=23^{30-24}$
22	7	·	·	$=0^{00-8^{40}}=0^{30-5^{45}}=22^{20-24}$
23	8	·	·	$=0^{00-8^{20}}=3^{30-5^{30}}$
24	7	·	·	$=3^{30-8^{30}}\,\oplus17^{40-18^{05}}$
25	8	·	·	$\gg10^{50-14^{40}}\,15^{37-18^{35}}\,=1^{30-4^{40}}$
26	8	0.0	·	
27	8	0.5	·	$\overset{*}{\bullet}{}^{\circ}3^{43-59}\,\overset{*}{\bullet}{}^{0-1}18^{23-37}\,\gg1^{22-46}$
28	8	3.8	·	$\overset{*}{\bullet}{}^{\circ}8^{55-9^{00}}\,12^{50}\ldots18^{40}\,\bullet^{0-1}19^{50-21^{25}}\ldots21^{35}$
29	7	0.0	·	$\overset{*}{\bullet}{}^{\circ}5^{31}\ldots10^{38}\,13^{00-03}\,13^{10-13}\,\gg12^{10-14^{20}}$
30	8	0.0	·	$\overset{*}{\bullet}{}^{\circ}8^{48-9^{02}}$
31				
Σ	—	35.8	—	UWAGI

Wrocław-Gądów Mały φ=51°08' λ=16°59' Lipiec-Juillet 1962

DNI	CIŚNIENIE P-900 I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE N.w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D.v I	II	III
1	103.7	103.7	103.1	103.5	10.9	15.0	11.5	12.2	15.6	9.6	79	52	76	69	2.7	8.0	3.3	4.7	10	10	10	W 3	W 6	WSW 2
2	101.1	100.9	97.4	99.8	10.7	15.5	12.4	12.8	16.4	9.1	96	54	81	77	0.5	8.1	2.7	3.8	10	9	10●	W 3	W 9	SW 4
3	92.2	89.4	87.6	89.7	10.3	13.3	11.0	11.4	16.4	10.0	92	74	75	80	0.9	4.0	3.2	2.7	10	10●	10	W 6	WSW 3	W 6
4	86.2	87.2	89.3	87.6	10.5	11.8	11.6	11.4	14.8	6.4	75	70	74	73	3.2	4.1	3.6	3.6	8	10	9	SSW 7	W 6	SSW 5
5	91.7	93.3	96.4	93.8	11.6	15.5	11.9	12.7	16.5	9.6	76	53	87	72	3.2	8.2	1.8	4.4	9	8	10	SSW 3	W 3	S 3
6	99.6	100.1	101.8	100.5	12.8	18.1	11.9	13.7	19.4	8.1	81	54	81	72	2.8	9.5	2.6	5.0	1	7	8	SSW 2	WSW 4	SW 1
7	102.7	102.2	103.6	102.8	11.8	12.1	10.5	11.2	16.4	8.6	88	94	99	94	1.6	0.3	0.2	0.9	9	10	10	SSW 1	C 0	SSW 2
8	105.3	106.7	107.3	106.4	11.5	13.9	10.3	11.5	15.6	9.6	96	79	92	89	0.5	3.4	0.9	1.6	10	10	0	W 3	W 6	W 1
9	107.9	106.1	104.3	106.1	10.9	19.4	14.6	14.9	20.6	6.2	94	57	85	79	0.8	9.7	2.5	4.3	2	5⊙	8	WNW 1	C 9	NE 1
10	103.2	101.7	100.1	101.7	13.9	21.7	14.8	16.3	23.5	6.4	91	48	83	74	1.5	13.5	2.9	6.0	0	5	0	C 0	NE 1	NNE 1
11	98.8	96.6	94.5	96.6	13.4	23.7	18.9	18.7	26.4	5.6	98	58	84	80	0.4	12.4	3.5	5.4	7	8	6	C 0	SSE 4	SW 4
12	95.6	94.2	94.0	94.6	17.1	23.8	15.6	18.0	24.4	13.8	78	47	85	70	4.3	15.5	2.6	7.5	1	6⊙	9	WNW 3	SW 4	C 0
13	94.0	94.1	95.7	94.6	14.5	19.3	13.7	15.3	19.5	11.6	79	62	86	76	3.4	8.6	2.2	4.7	9	9(R)	8	WSW 5	WNW 8	WNW 2
14	94.7	94.7	94.3	94.6	12.3	15.5	14.5	14.2	17.8	9.7	98	76	86	87	0.3	4.3	2.4	2.3	10●	10	9	WSW 2	W 5	WSW 1
15	92.8	91.2	91.9	92.0	13.5	18.7	15.2	15.6	20.2	7.0	91	67	96	85	1.5	7.1	0.8	3.1	5	10	10	C 0	ESE 2	SW 2
16	92.7	93.5	95.1	93.8	15.5	18.7	16.9	17.0	20.7	13.2	90	76	89	85	1.7	5.2	2.1	3.0	10	9	10	C 0	NNW 2	NE 1
17	98.1	99.6	100.7	99.5	14.8	18.0	14.9	15.6	21.2	14.3	98	86	94	93	0.3	2.8	0.9	1.3	10●	10	6	C 0	C 0	WNW 2
18	101.9	101.4	101.9	101.7	13.3	20.1	16.3	16.5	21.7	10.1	91	52	77	73	1.4	11.3	4.2	5.6	10	9	9	WNW 1	NE 4	NNW 1
19	103.2	103.4	103.4	103.3	13.3	22.9	15.3	16.7	23.9	11.5	91	49	81	72	1.4	15.4	3.4	6.7	10	5⊙	1	WNW 4	NW 3	NE 1
20	104.0	103.1	103.0	103.4	15.9	24.4	17.3	18.7	25.6	9.5	84	44	83	70	2.9	17.1	3.3	7.8	8	5	4	WSW 1	C 0	N 1
21	102.1	99.1	98.6	99.9	17.6	27.4	22.7	22.6	29.4	10.5	84	44	66	65	3.2	20.3	9.4	11.0	0	1	3	C 0	SE 5	S 4
22	102.4	101.8	103.0	102.4	18.5	25.8	18.3	20.2	26.1	17.7	97	57	95	83	0.7	14.4	1.0	5.4	9	7	9	WSW 2	SE 1	SW 1
23	106.0	106.4	107.9	106.8	17.1	21.8	16.5	18.0	23.4	14.1	85	55	68	69	3.0	11.7	6.1	6.9	2	9	4	WNW 1	WNW 4	W 2
24	111.0	110.7	109.8	110.5	13.9	19.8	15.4	16.1	21.6	9.5	82	52	73	69	2.9	11.0	4.8	6.2	1⊙	6⊙	1	NW 3	WNW 3	NNE 3
25	110.3	107.8	104.8	107.6	14.1	23.7	21.7	20.3	25.2	7.4	79	48	57	61	3.4	15.3	11.2	10.0	0⊙	0⊙	2	C 0	ESE 2	ESE 3
26	103.0	100.8	100.3	101.4	19.7	30.9	25.0	25.2	31.9	14.0	73	48	66	62	6.1	23.3	10.7	13.4	0⊙	1⊙	8(R)	SE 2	S 4	SSW 4
27	101.7	102.4	103.8	102.6	21.2	24.5	19.3	21.1	25.5	16.6	82	67	63	71	4.6	10.0	8.2	7.6	2	7	1	NW 1	WSW 7	NW 3
28	106.4	106.1	105.8	106.1	14.5	19.8	13.5	15.3	21.6	12.7	82	48	87	72	2.9	12.1	2.0	5.7	8	3	6	WNW 5	W 8	C 0
29	107.2	106.2	105.7	106.4	12.1	20.3	12.4	14.3	22.2	6.5	89	46	81	72	1.5	12.8	2.7	5.7	4	6	2	C 0	C 0	C 0
30	106.9	105.9	105.3	106.0	11.7	22.1	12.5	14.7	22.2	6.3	87	37	76	67	1.8	16.7	3.6	7.4	8	6	4	C 0	E 1	E 2
31	106.9	105.8	104.9	105.9	12.5	23.8	15.3	16.7	24.6	6.1	82	34	88	68	2.6	19.6	2.1	8.1	3	2	10	C 0	SSE 1	SSW 1
M	101.1	100.5	100.5	100.7	13.9	20.0	15.2	16.1	21.6	10.0	87	58	81	75	2.2	10.8	3.6	5.5	6.0	6.9	6.4	1.9	3.4	2.1

Sierpień-Août

1	105.1	104.3	104.3	104.6	16.9	20.3	17.1	17.8	22.6	14.4	85	60	66	70	2.9	9.6	6.7	6.4	8	6	4	WNW 3	NW 6	W 2
2	103.9	102.1	100.0	102.0	13.2	23.1	16.7	17.4	24.7	7.6	92	45	82	73	1.3	15.5	3.5	6.8	2⊙	4⊙	4	W 1	W 2	SSE 2
3	100.0	99.8	100.1	100.0	16.1	24.6	20.0	20.2	25.8	13.5	89	57	87	77	1.9	13.4	3.1	6.1	10	8	10	NNE 1	E 2	S 1
4	100.3	100.3	101.0	100.5	17.9	25.9	20.7	21.3	29.0	12.7	91	62	75	76	1.8	12.7	6.1	6.9	3	7	0	SSE 1	SSW 3	WNW 1
5	99.6	98.5	95.8	98.0	18.7	22.4	18.7	19.6	26.3	14.4	87	73	87	82	2.8	7.4	2.8	4.3	4	10●R	6	C 0	SW 14	SSE 1
6	98.0	98.5	96.9	97.8	16.0	20.6	19.4	18.8	23.8	14.7	92	74	91	86	1.6	6.3	1.9	3.3	7	9	8	WNW 2	S 1	E 1
7	90.9	86.9	95.1	91.0	19.9	26.8	16.5	19.9	28.8	16.4	84	58	83	75	3.7	14.7	3.3	7.2	9	9●	8	SE 3	WSW 4	W 3
8	100.7	102.3	104.6	102.5	16.6	21.9	14.5	16.9	23.0	13.2	68	40	79	62	6.1	15.9	3.4	8.5	4	5	2	SW 6	W 7	C 0
9	109.1	109.7	109.6	109.5	12.0	20.5	14.5	15.4	22.2	8.9	86	43	74	68	2.0	13.7	4.3	6.7	4	6	8	W 3	WSW 2	N 1
10	107.6	104.5	102.4	104.8	13.1	24.0	15.9	17.2	25.2	6.3	83	40	77	67	2.6	18.0	4.2	8.3	0	6	4	SE 1	SSW 5	SW 2
11	103.2	102.6	102.8	102.9	16.0	23.5	16.4	18.1	25.6	12.7	85	43	88	72	2.7	16.5	2.3	7.2	7	9	5	WSW 1	WNW 3	C 0
12	103.7	102.3	101.6	102.5	15.9	29.3	19.4	21.0	30.6	9.7	79	38	82	66	3.8	25.2	4.0	11.0	0	2	1	C 0	SW 5	SSW 1
13	103.4	103.2	102.7	103.1	17.9	31.5	21.9	23.3	32.2	12.1	84	37	74	65	3.2	29.0	6.9	13.0	7	4	0	SW 1	S 2	N 4
14	105.3	104.5	103.4	104.4	17.5	19.7	18.0	18.3	23.8	16.6	95	90	89	91	1.0	2.4	2.2	1.9	9(R)	8●	10	SW 4	NNE 5	N 2
15	97.3	96.5	95.4	96.4	18.0	25.8	16.7	19.3	27.4	16.4	89	70	97	85	2.2	10.0	0.6	4.3	10●	6	8	NNE 1	SSE 3	C 0
16	97.1	97.9	99.0	98.0	17.7	24.1	15.9	18.4	25.1	15.3	83	53	93	76	3.4	14.2	1.4	6.3	5	3⊙	3	W 2	W 4	C 0
17	99.5	99.0	97.6	98.7	16.5	21.8	17.2	18.2	22.6	13.3	94	67	96	86	1.2	8.7	0.8	3.6	9	10	7	C 0	W 3	SE 3
18	95.8	100.8	102.2	99.6	15.1	17.1	14.1	15.1	19.2	12.4	98	67	73	79	0.4	6.5	4.4	3.8	10	7	7	C 0	W 9	W 4
19	101.7	102.8	103.4	102.6	13.0	12.0	13.3	12.9	14.1	10.8	88	91	92	90	1.8	1.2	1.3	1.4	9	10	9	W 6	WNW 4	W 6
20	103.2	103.7	103.5	103.5	14.6	16.9	14.7	15.2	17.5	12.7	86	73	90	83	2.4	5.2	1.6	3.1	6	10	9	W 5	WNW 6	W 1
21	101.4	99.9	99.1	100.1	14.7	21.7	16.5	17.4	23.3	12.6	92	57	81	77	1.3	11.2	3.7	5.4	3	5	6	C 0	SE 2	W 5
22	102.5	103.3	101.7	102.3	14.7	20.3	15.7	16.6	21.6	14.1	88	60	90	79	2.0	9.6	1.7	4.4	6	5	9	NW 6	WNW 4	SSW 1
23	103.4	104.4	103.9	103.9	14.5	18.8	14.8	15.7	20.8	12.0	78	59	82	73	3.6	8.8	3.1	5.2	3	7	10	WSW 4	W 4	W 1
24	99.3	96.2	96.7	97.4	14.4	19.9	16.6	16.9	24.5	12.5	95	71	94	87	0.7	6.7	1.2	2.9	10●	10	10●	S 2	SW 6	WSW 7
25	100.0	100.8	103.6	101.5	14.3	19.7	13.3	15.2	20.2	10.9	81	51	74	69	3.1	11.1	4.0	6.1	7	9	1	W 6	W 8	SW 2
26	106.9	107.3	105.4	106.5	12.5	19.9	12.3	14.2	21.0	8.5	85	45	85	72	2.2	12.6	2.2	5.7	9	5	0	WSW 4	WSW 7	E 1
27	101.0	97.6	101.0	99.9	13.8	24.0	19.4	19.2	25.8	9.7	81	45	57	61	3.0	16.4	9.7	9.7	2	8	0	SE 2	SW 8	NW 4
28	106.0	105.9	106.4	106.1	13.9	18.3	12.9	14.5	19.5	9.6	68	55	85	69	5.1	9.5	2.3	5.6	8	9	4	W 5	W 8	W 1
29	104.0	103.1	104.8	104.0	13.7	19.1	14.5	15.4	20.6	9.8	80	63	86	76	3.2	8.1	2.4	4.6	4	9	7	S 2	W 8	W 3
30	108.0	109.0	107.0	108.0	11.9	15.7	10.1	12.0	16.6	10.1	96	54	83	78	0.5	8.2	2.1	3.6	9	9	0	WNW 6	W 6	WSW 3
31	102.0	101.9	103.3	102.4	11.7	16.1	13.0	13.4	16.9	8.2	76	55	71	67	3.3	8.2	4.3	5.3	10	9	6	SW 4	W 8	W 5
M	101.9	101.6	101.8	101.8	15.2	21.5	16.2	17.3	23.2	12.0	86	58	83	76	2.3	11.3	3.3	5.8	6.3	7.2	5.4	2.6	5.1	2.2

Wrocław-Gądów Mały H_s=116m H_b=118,6m h_w=20m — Lipiec - Juillet 1962

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	5.8	.	
2	7	2.9	.	•$^{\circ}4^{25}$...5^{05} •$^{0-1}$-7^{15} •$^{\circ}21^{45}$...22^{30}-24
3	8	0.0	.	•$^{\circ}0^{00}$-3^{45}, 6^{05}-7^{40} ⚲$^{\circ}12^{11}$...17^{13}, 20^{36}...24; = a; ∩$^{z}20^{34-37}$
4	8	0.0	.	•$^{\circ}0^{00-36}$
5	8	.	.	
6	7	8.0	.	⚲$^{0-2}16^{16}$-17^{29} ⚲$^{\circ}$⚲19^{50}-20^{07}, (⚲)'16^{16}-⚲'16^{24}-17^{05} SW-NNE; = 4^{40}-6^{20}
7	7	5.3	.	⚲$^{0-1}12^{24}$...14^{35} •$^{\circ}16^{30}$...17^{30} ⚲'-17^{40} •$^{\circ}$...19^{00}-20^{36}; = 1^{40}-8^{30}, 21^{30}-24
8	7	.	.	= 0^{00}-13^{00}, ⌓$^{\circ}21^{30}$-24
9	8	.	.	= 0^{00}-10^{30}, ⌓$^{\circ}0^{00}$-7^{00}
10	8	.	.	= 2^{00}-9^{30}
11	7	0.0	.	⚲ 11^{50}-12^{10}, 17^{00-10}; = 2^{30}-9^{30} = 3^{20}-5^{40}, ⌓$^{\circ}$na
12	8	2.2	.	⚲$^{\circ}14^{57}$-15^{52}, ⚲$^{\circ}14^{52}$-15^{45} WSW-SE; = 3^{40}-4^{10}
13	8	5.6	.	⚲$^{\circ}4^{20-50}$ ⚲ 9^{59}-10^{40}, 14^{04-18} ⚲$^{\circ}$-14^{35}, 19^{50-52}; (⚲)$^{\circ}13^{58}$-14^{22} W-E; = na
14	7	0.6	.	•$^{\circ}4^{58}$-10^{40}; = 2^{30}-11^{30}, 22^{30}-24
15	6	6.7	.	⚲$^{0-1}16^{04}$-17^{15} •$^{a}19^{50}$-20^{10}; = 0^{00}-4^{20} = 3^{10}-4^{20} ≡$^{\circ}$-6^{10} = -p, np, ⌓$^{z}2^{00}$-10^{00}
16	7	11.2	.	•$^{\circ}12^{00}$-13^{05} ⚲$^{\circ}22^{50}$-23^{12} •$^{\circ}23^{40}$...24; = 0^{00}-9^{30}
17	7	1.7	.	•$^{\circ}0^{00}$ 0^{10}-7^{10} ⚲$^{\circ}7^{15-59}$ •$^{\circ}$-10^{40} ⚲$^{\circ}13^{30-45}$; = a, np, ⌓$^{\circ}$np
18	8	.	.	= 2^{00}-8^{30} = -4^{30}, ⌓$^{0-2}$ 2^{00}-9^{00}
19	8	.	.	= 8^{30}-10^{20}, ⌓$^{\circ}22^{00}$-24
20	8	.	.	= 1^{30}-5^{40} = 4^{00}-10^{30}, 22^{30}-24, ⌓ na ⌓$^{\circ}$np
21	8	1.0	.	= 0^{00}-9^{15} = 1^{00}-6^{50}, ⌓$^{0-1}$ 0^{00}-8^{00} ⌓$^{\circ}$np
22	8	10.6	.	⚲$^{\circ}0^{15-50}$, 3^{05-50}, 14^{30}-15^{40} ⚲$^{0-1}16^{38}$-18^{40}; ⚲$^{\circ}3^{03-40}$ SSW-W, 14^{08}-15^{40}, 16^{38}-18^{15}; = na-a ∩18^{25-32}
23	8	.	.	= 2^{30}-7^{20}, ⌓$^{\circ}$np, ⊕ 13^{55}-15^{20}
24	8	.	.	= 22^{30}-24, ⌓$^{\circ}0^{00}$-9^{00}
25	8	.	.	= 0^{00}-5^{50} = -6^{50} = -9^{30} 20^{20}-24
26	8	13.7	.	⚲$^{z}22^{10-30}$ ⚲$^{\circ}$-23^{20}, ⚲ 21^{35}-23^{38} SW-E, ≫ 22^{15}-23^{15}; = 0^{00}-10^{15}, ⌓$^{\circ}2^{00}$-8^{00}
27	7	1.6	.	⚲$^{0-1}10^{30}$-11^{25}, ⚲'10^{30}-11^{20} SW-NE; = 9^{30}-13^{30}, ⌓$^{\circ}$np
28	8	.	.	⌓$^{\circ}$na-a
29	8	.	.	= 4^{20}-5^{45} = 4^{20}-7^{15}, ⌓$^{\circ}$np
30	8	.	.	= 2^{30}-6^{35}, ⌓$^{\circ}0^{00}$-9^{00}, 21^{30}-24
31	8	0.1	.	⚲$^{\circ}18^{45}$-19^{02}; = 1^{30}-4^{57} = -5^{10} ≡$^{\circ}$-6^{00} = -9^{10}, ⌓'0^{00}-9^{00}
Σ	—	77.0	—	UWAGI

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1	7	0.1	.	•$^{\circ}3^{35}$...4^{10}, 5^{50}-6^{15} ⚲$^{\circ}12^{15-45}$; = 4^{30}-7^{30} 8^{30}-10^{30}
2	8	1.4	.	= 4^{00}-6^{30} = 0^{00}-10^{10}, 21^{30}-24, ⌓$^{\circ}4^{40}$-10^{00}
3	6	.	.	⚲$^{\circ}2^{30-45}$, 4^{20}-5^{05}, ⚲$^{\circ}4^{10-40}$ N-E; = 0^{00}-12^{30} ∞-15^{30} = 20^{30}-24, ⊕$^{\circ}$a
4	7	1.8	.	⚲$^{0-1}11^{50}$...13^{30} ⚲$^{\circ}16^{25-30}$; = na = na ≡$^{0-1}4^{50}$-7^{35} = -a; ⌓$^{\circ}$np
5	5	9.8	.	⚲$^{0-2}13^{32}$-14^{16} •$^{\circ}15^{20}$-16^{15}, 22^{10}-24; ⚲'13^{25}-14^{15} SW-NE; ≫p; = na-a, ⌓$^{\circ}$na-a
6	8	0.0	.	⚲$^{\circ}9^{45-58}$; = 5^{00}-8^{30}, 20^{30}-24
7	8	0.2	.	⚲ 13 13^{47-56}, 14^{43}...20^{10} •$^{\circ}20^{40}$...21^{05}; ≫15^{30}-16^{25}; = 0^{00}-12^{15}
8	8	.	.	
9	8	.	.	
10	8	.	.	= 2^{00}-a = 3^{40}-6^{45}; ⌓$^{\circ}$na
11	8	.	.	= 22^{30}-24
12	8	.	.	= 0^{00}-9^{30} = 4^{30}-6^{50}
13	8	1.6	.	= 4^{30}-6^{30} = -9^{20}
14	7	3.9	.	⚲$^{\circ}5^{20}$-6^{06}, 12^{50}-14^{20}, ⚲$^{\circ}5^{20}$-6^{04} W-NE; (⚲)$^{\circ}7^{45}$-8^{20}; = a, np
15	6	38.7	.	•$^{\circ}5^{16}$...6^{15} ⚲$^{\circ}$-10^{20} ⚲$^{0-2}16^{45}$...18^{30}, ⚲'6^{15}-7^{20} SW-NE, 8^{01}-10^{04}, 16^{45} p; = 0^{00}-13^{30} ∞-14^{30}, ⊕ 14^{30}-15^{30}
16	8	.	.	⌓' 21^{30}-24, ♒ 8^{15}-9^{30}
17	7	2.8	.	•$^{\circ}14^{50}$...15^{00}-19^{05}; = 0^{30}-1^{30} = 5^{30}-6^{30} = 19^{30}-24, ⌓$^{\circ}$na, np
18	8	0.3	.	⚲$^{\circ}6^{38}$-7^{41}, ≫a; = 0^{00}-8^{20}, ⌓$^{\circ}0^{00}$-6^{38}
19	7	2.6	.	⚲$^{\circ}2^{05-45}$, 9^{05}...17^{40}
20	7	0.0	.	•$^{\circ}2^{00}$...^{43} ⚲$^{\circ}10^{20}$...12^{45}, 16^{45}-17^{30}
21	8	4.4	.	= 2^{30}-9^{30}, ⌓$^{\circ}2^{00}$-10^{00}
22	7	.	.	•$^{\circ}0^{40}$-3^{10}...3^{40} •'-4^{45} •$^{\circ}5^{50}$...6^{10}; = 4^{40}-7^{30}, ⌓$^{\circ}$np
23	8	0.3	.	⌓$^{0-1}$na, ♒ 19^{35}-20^{30}
24	8	5.1	.	•$^{\circ}5^{40}$-10^{50}, 13^{40-50} •$^{\circ}17^{45}$...p •$^{0-1}$-22^{40}; ≫p
25	8	0.0	.	⌓$^{\circ}22^{00}$-24
26	8	.	.	⚲$^{\circ}0^{15}$-1^{40}, ⌓$^{\circ}0^{00-15}$
27	8	.	.	
28	8	.	.	
29	8	0.0	.	⚲$^{\circ}16^{10-20}$
30	8	.	.	= 0^{30}-4^{40}, ⌓$^{\circ}$np
31	8	1.9	.	⌓$^{\circ}0^{00}$-9^{00}
Σ	—	74.9	—	UWAGI

Wrocław-Gądów Mały φ = 51°08' λ = 16°59' Wrzesień-Septembre 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N.w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D.v I	II	III
1	106.1	108.5	109.7	108.1	11.2	15.3	10.3	11.8	17.6	10.2	97	70	88	85	0.3	5.3	1.4	2.3	9	7	1	W 3	NW 6	SW 1
2	110.9	109.2	106.8	109.0	7.9	20.9	10.4	12.4	22.6	2.7	99	40	93	77	0.1	14.9	0.8	5.3	1	8	0	C 0	SW 1	C 0
3	106.0	104.9	102.0	104.3	8.5	24.2	13.3	14.8	26.6	3.9	99	36	83	73	0.2	19.3	2.7	7.4	3	0 ⊙	1	C 0	SSW 1	E 1
4	99.2	96.0	92.1	95.8	14.1	30.9	21.3	21.9	31.8	10.3	79	33	62	58	3.4	29.9	9.5	14.3	1	2	0	SE 2	SSE 3	S 3
5	91.4	93.0	93.4	92.6	15.9	20.3	15.1	16.6	23.4	14.2	94	65	75	78	1.2	8.2	4.3	4.6	6	10	4	SSE 2	SSW 4	SSW 3
6	94.1	93.5	89.6	92.4	15.1	21.8	16.7	17.6	22.4	13.1	75	50	95	73	4.3	13.1	1.0	6.1	5	8	10 ●	SW 4	W 5	SSE 2
7	85.6	87.3	92.6	88.5	19.5	17.9	15.8	17.2	20.6	15.8	72	79	79	77	6.3	4.2	3.7	4.7	10	8	7	SW 7	WSW 8	W 7
8	96.5	97.4	99.5	97.8	11.9	16.5	10.1	12.2	17.5	8.9	89	63	92	81	1.5	7.0	1.0	3.2	10	6	4	WSW 2	WSW 4	SSW 2
9	106.6	108.9	109.0	108.2	10.5	14.5	7.1	9.8	16.6	7.1	92	69	100	87	1.0	5.1	0.0	2.0	9	9	2	WNW 5	W 7	W 1
10	106.3	104.2	101.5	104.0	8.4	23.7	17.1	16.6	25.0	5.1	93	32	56	60	0.7	19.9	8.5	9.7	3	0	3	SE 4	SSW 3	S 5
11	100.3	100.5	104.4	101.7	16.1	20.0	12.8	15.4	23.0	9.6	72	81	88	80	5.1	4.4	1.8	3.8	10 ●	9	1	SSW 4	WSW 6	SSW 2
12	101.0	95.6	94.0	96.9	15.7	27.0	24.0	22.7	28.8	11.4	78	45	46	56	3.9	19.6	16.0	13.2	10	3	5	S 5	SW 10	WNW 12
13	102.4	104.9	105.5	105.3	12.1	15.5	12.1	13.0	24.2	11.0	82	58	65	68	2.5	7.4	4.9	4.9	9	6	3	N 4	W 7	W 4
14	111.6	112.5	111.2	111.8	8.9	12.5	4.6	7.6	14.8	4.2	84	52	93	76	1.8	6.9	0.6	3.1	9	9	3	W 4	W 4	C 0
15	106.5	102.6	98.9	102.7	5.9	19.0	14.3	13.4	21.2	1.4	88	42	61	64	1.2	12.8	6.3	6.8	0	9	1	C 0	SE 6	SSE 4
16	96.8	95.0	96.4	96.1	10.5	25.8	17.8	18.0	27.0	8.7	92	45	83	73	1.0	18.4	3.4	7.6	4	1 ⊙	8	SSE 1	SSW 3	WNW 3
17	97.0	98.0	98.6	97.9	13.3	12.6	10.3	11.6	17.8	9.6	95	96	97	96	0.7	0.5	0.3	0.5	10 ●	10 ●	10 ●	NW 1	NW 2	NW 1
18	96.5	94.9	95.3	95.6	9.1	10.9	7.9	9.0	11.6	6.6	100	90	99	96	0.0	1.3	0.1	0.5	10 ≡	10 ●	10 ●	C 0	N 1	W 1
19	97.5	100.0	102.2	99.9	7.3	10.9	8.5	8.8	11.8	6.4	99	83	96	93	0.1	2.2	0.5	0.9	10 ●	9	8	SW 2	WSW 5	W 1
20	104.0	103.9	105.1	104.3	4.8	14.3	9.1	9.3	15.7	3.7	98	69	93	87	0.1	5.1	0.8	2.0	5	6	9	C 0	W 2	W 1
21	106.3	105.7	105.2	105.7	7.9	13.5	9.7	10.2	14.0	5.8	94	72	95	87	0.6	4.4	0.6	1.9	8	9	10 ●	W 3	W 7	W 3
22	105.5	107.0	108.2	106.9	9.3	13.1	9.7	10.4	14.9	9.0	97	74	95	89	0.3	4.0	0.6	1.6	10 ●	7	7	WNW 3	WNW 3	W 3
23	106.2	103.9	104.5	104.9	9.5	9.9	8.8	9.2	10.6	8.6	100	95	90	95	0.0	0.6	1.1	0.6	9	10 ●	8	WNW 5	W 5	WNW 2
24	108.4	110.3	112.3	110.3	7.7	11.1	8.7	9.0	12.2	6.6	97	85	99	94	0.3	2.0	0.1	0.8	10 ≡	9	9	WNW 2	WNW 3	C 0
25	113.9	113.3	111.6	112.9	7.1	13.8	10.4	10.4	15.2	4.6	100	65	81	82	0.0	5.6	2.4	2.7	10	6	0	E 1	ESE 2	E 2
26	109.4	107.7	106.3	107.8	6.5	17.5	11.9	12.0	18.3	5.7	96	53	74	74	0.5	9.3	3.6	4.5	0	0	1	E 2	E 4	ESE 5
27	103.9	102.0	101.0	102.3	6.1	14.7	10.3	10.4	16.0	4.8	94	69	94	86	0.6	5.2	0.8	2.2	3	9	6	ENE 4	E 3	NE 3
28	100.4	99.8	99.3	99.8	8.5	11.9	5.3	7.8	14.8	5.1	100	89	100	96	0.0	1.5	0.0	0.5	10 ≡	10	0 ≡	ESE 1	E 4	SE 1
29	99.0	99.4	101.4	99.9	7.3	15.7	9.5	10.5	16.8	3.6	100	76	99	92	0.0	4.3	0.2	1.5	10 ≡	9	0	C 0	SE 2	ESE 2
30	104.5	104.6	105.3	104.8	6.7	19.5	9.5	11.3	20.4	4.4	100	64	95	86	0.0	8.1	0.7	2.9	9 ≡	0	0 ≡	C 0	SSE 1	C 0
31																								
M	102.5	102.2	102.2	102.3	10.1	17.2	11.7	12.7	19.1	7.4	92	65	86	81	1.3	8.4	2.6	4.1	7.1	6.6	4.4	2.4	4.1	2.5

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1	107.0	106.9	108.5	107.5	8.2	21.9	13.5	14.3	22.8	7.4	100	56	94	83	0.0	11.6	0.9	4.2	0 ≡	1	0	ESE 2	ESE 3	ESE 1
2	110.0	110.0	109.7	109.9	10.3	21.6	14.2	15.1	22.4	8.9	99	57	86	81	0.1	11.1	2.4	4.5	0 ≡	0	0	E 1	ESE 3	ESE 2
3	109.2	108.7	108.8	108.9	10.6	19.9	14.1	14.7	22.4	10.0	97	67	90	85	0.4	7.7	1.6	3.2	10 ≡	1	0	E 1	E 3	E 1
4	108.9	108.2	108.1	108.4	9.7	20.5	14.1	14.6	22.0	9.5	100	67	97	88	0.0	7.9	0.6	2.8	10 ≡	6	10	ESE 2	E 1	C 0
5	108.4	110.3	111.0	109.9	15.1	17.3	14.2	15.2	17.7	13.6	97	76	86	86	0.6	4.7	2.4	2.6	10	7	10	WNW 2	N 2	WNW 3
6	111.3	113.0	115.0	113.1	10.9	10.7	12.5	11.6	14.6	9.9	99	97	98	98	0.1	0.4	0.4	0.3	10 ●,	10 ●,	10	W 5	NW 2	NNW 4
7	117.0	118.3	119.2	118.2	12.8	16.9	10.8	12.8	17.5	10.7	93	71	96	87	1.1	5.5	0.5	2.4	10	8	0	N 3	NNE 3	NE 2
8	120.1	120.1	119.5	119.9	10.1	14.1	10.1	11.1	16.6	4.3	99	79	97	92	0.2	3.4	0.4	1.3	10	9	0	E 2	ENE 2	E 1
9	118.9	118.0	115.1	117.3	6.9	12.0	9.5	9.5	14.8	6.1	100	80	95	92	0.0	2.8	0.7	1.2	10 ≡	8	0	SE 1	NE 3	E 2
10	112.8	111.9	109.7	111.5	5.7	8.0	4.9	5.9	9.6	3.1	100	100	98	99	0.0	0.0	0.2	0.1	10 ≡	10	10 ≡	E 2	ESE 2	C 0
11	107.1	104.7	102.4	104.7	4.4	10.3	3.6	5.5	12.8	3.4	98	88	97	94	0.2	1.4	0.3	0.6	10 ≡	0	0 ≡	SSE 3	NE 1	C 0
12	103.6	105.5	107.2	105.4	5.5	5.5	5.0	5.2	6.8	2.6	100	100	95	98	0.0	0.0	0.4	0.1	10 ●, ≡	10 ●,	10	NW 2	NNE 2	E 1
13	107.1	105.7	101.9	104.9	5.0	8.1	6.6	6.6	10.2	2.1	97	91	97	95	0.3	0.9	0.3	0.5	8	10	10 ≡	NE 2	SE 3	SE 4
14	99.0	101.5	104.6	101.7	6.5	7.3	7.6	7.2	8.0	6.1	100	97	93	97	0.0	0.3	0.7	0.3	10 ≡	10 ●	10	WNW 2	WNW 4	W 3
15	107.7	111.0	112.7	110.5	7.6	8.3	2.8	5.4	10.2	2.1	99	83	96	93	0.1	1.9	0.3	0.8	9	9	2 ≡	W 3	E 2	WNW 1
16	111.0	109.2	108.7	109.6	0.0	8.4	6.6	5.4	11.6	-3.4	100	81	90	90	0.0	2.1	1.0	1.0	10 ≡	1 ⊙	9	C 0	S 1	C 0
17	109.8	110.6	111.1	110.5	8.8	12.2	9.8	10.2	12.4	6.5	93	79	91	88	0.8	3.0	1.1	1.6	10	10	10	WNW 3	W 5	W 3
18	109.1	106.8	101.4	105.8	10.3	14.7	9.2	10.8	16.5	8.6	92	65	85	81	0.9	5.8	1.7	2.8	10	9	0	WSW 3	W 7	SW 2
19	100.0	101.6	102.6	101.4	11.0	12.2	9.9	10.8	13.2	7.6	90	62	73	75	1.3	5.4	3.3	3.3	10 ○	8	9	WNW 6	NW 8	W 5
20	105.4	108.5	113.6	109.2	8.8	12.0	6.8	8.6	13.6	6.1	93	66	87	82	0.8	4.8	1.3	2.3	10	6	2	WNW 3	WNW 3	WNW 2
21	117.6	117.2	116.5	117.1	-2.1	11.4	0.4	2.5	13.2	-2.3	100	47	96	81	0.0	7.1	0.3	2.5	0	0 ⊙	0	C 0	WSW 2	C 0
22	116.1	114.8	113.4	114.8	-5.0	13.2	-0.1	2.0	14.8	-5.5	100	46	94	80	0.0	8.1	0.4	2.8	0 ≡	0	0	C 0	S 1	C 0
23	112.2	111.0	109.2	110.8	-5.3	13.2	0.6	2.3	13.8	-6.0	95	57	98	83	0.2	6.6	0.1	2.3	0 ≡	0	0	C 0	C 0	E 2
24	107.7	107.6	109.1	108.1	-2.7	12.2	3.0	3.9	13.4	-5.3	100	62	96	86	0.0	5.4	0.3	1.9	0 ≡	0	0	SE 1	WNW 4	WNW 2
25	107.4	105.6	104.3	105.8	-0.3	13.8	5.7	6.2	14.0	-1.9	100	52	89	80	0.0	7.7	1.0	2.9	0 ≡	0	0	SE 1	S 5	ESE 1
26	102.4	101.0	99.4	100.9	-0.9	15.5	7.8	7.6	16.8	-2.3	100	51	79	77	0.0	8.6	2.2	3.6	0 ≡	5	0	E 1	S 5	S 5
27	96.9	102.3	103.6	100.9	3.2	6.4	4.2	4.5	11.0	3.1	95	95	98	96	0.4	0.4	0.1	0.3	6	10 ●	10 ●	C 0	WNW 4	C 0
28	98.6	98.5	96.2	97.9	5.2	4.8	3.8	4.4	5.6	3.1	98	98	100	99	0.1	0.1	0.0	0.1	10 ●	10 ●	9	SSE 2	WNW 1	SE 1
29	97.1	99.4	103.2	99.9	4.2	6.4	5.0	5.2	6.7	3.6	100	95	100	98	0.0	0.4	0.0	0.1	10 ●	10 ●	9	S 1	W 1	W 1
30	104.1	101.7	97.6	101.1	-0.2	9.0	5.2	4.8	9.8	-1.0	100	67	97	88	0.0	3.8	0.2	1.3	3 ≡	3 ⊙	10	C 0	SSE 4	SSE 4
31	95.1	94.7	95.4	95.1	-0.3	8.4	5.6	4.8	9.4	-1.4	100	78	98	92	0.0	2.4	0.2	0.9	4	9	10	SE 2	SE 1	C 0
M	107.7	107.9	107.7	107.8	5.3	12.1	7.3	8.0	13.7	3.5	98	75	95	89	0.2	4.2	0.8	1.7	6.8	5.8	4.8	1.8	2.8	1.7

Wrocław - Gądów Mały $H_s = 116m$ $H_b = 118{,}6m$ $h_w = 20m$ Wrzesień - Septembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	.	.	$\overset{\circ}{\bullet}\,^{0-1}0^{10}\ 4^{30}$
2	8	.	.	$=2^{30}-8^{30}=5^{30}-6^{00}=21^{30}-24;\ \triangle^{\circ}np;\ \oplus 12^{30}-16^{30}$
3	8	.	.	$=0^{00}-11^{20}=5^{00}-7^{15}\infty 11^{20}-12^{40},\ \triangle^{\circ}0^{00}-10^{00},np$
4	8	.	.	$\triangle^{\circ}0^{00}-9^{45}$
5	8	0.3	.	$\overset{\circ}{\bullet}\,^{\circ}13^{45-47}\ 16^{37-48}$
6	8	0.6	.	$\overset{\circ}{\bullet}\,^{\circ}5^{05-08}\ \overset{\circ}{\bullet}\,^{\circ}17^{30\ldots40},19^{10}-20^{15},21^{35}\ldots 22^{20}$
7	8	0.4	.	$\overset{\circ}{\bullet}\,^{0-1}9^{20}-12^{35};\ \gg p.$
8	8	0.5	.	$\overset{\circ}{\bullet}\,^{\circ}9^{20-45}\ \overset{\circ}{\bullet}\,^{\circ}10^{30}-12^{05}\ \overset{\circ}{\bullet}\,^{\circ}17^{45}-18^{05}$
9	8	.	.	$\overset{\circ}{\bullet}\,^{\circ}5^{15-40};=21^{00}-23^{30},\ \triangle^{\circ}20^{00}-24$
10	8	0.0	.	$=2^{30}-5^{30},\ \triangle^{\circ}0^{00}-11^{00}\ \ 21^{50}-22^{30}$
11	7	1.0	.	$\overset{\circ}{\bullet}\,^{\circ}7^{45}-8^{20}\ \overset{\circ}{\bullet}\,^{\circ}11^{25-50},12^{45}-13^{05};\ \triangle 22^{00}-24$
12	8	0.4	.	$\gg 11^{40}\ldots 17^{15},21^{25}-22^{20};\ \triangle 0^{00}-8^{00}$
13	8	.	.	$\overset{\circ}{\bullet}\,^{\circ}2^{45}-3^{10}\ \overset{\circ}{\bullet}\,^{\circ}3^{40}\ldots 4^{20}\ \overset{\circ}{\bullet}\,^{\circ}-5^{15},5^{25}-6^{35}$
14	8	.	.	
15	8	.	.	$=1^{30}-11^{20}=4^{50}-7^{15}$
16	8	2.9	.	$=8^{40}-10^{20},\ \triangle^{\circ}2^{00}-8^{00}$
17	5	6.6	.	$\overset{\circ}{\bullet}\,^{\circ}3^{15-30}\ \overset{\circ}{\bullet}\,^{\circ}-4^{40}\ \overset{\circ}{\bullet}\,^{0-1}5^{35}-7^{15}\ldots 7^{40}\ \overset{\circ}{\bullet}\,^{\circ}7^{45}-23^{35};=3^{00}-24$
18	6	13.9	.	$\overset{\circ}{\bullet}\,^{\circ}13^{35}-24;=2^{00-45}\equiv -5^{35}=-6^{05}\equiv -6^{30}$
19	8	0.2	.	$\overset{\circ}{\bullet}\,^{\circ}0^{00}-4^{20};\ 5^{35}-12^{20}\ \overset{\circ}{\bullet}\,^{\circ}14^{45-50};17^{03-15}$
20	8	.	.	$=5^{40}-8^{20}=-10^{30},\ \triangle^{\circ}np$
21	7	1.9	.	$\overset{\circ}{\bullet}\,^{\circ}18^{15}-19^{05},20^{25}-21^{20}\ \overset{\circ}{\bullet}\,^{\circ}21^{40}\ldots 24;=0^{30}-11^{10},\ \triangle^{\circ}0^{00}-9^{00}$
22	8	1.3	.	$\overset{\circ}{\bullet}\,^{\circ}2^{27}\ldots 8^{40}\ \overset{\circ}{\bullet}\,^{\circ}8^{45}-9^{40}\ \overset{\circ}{\bullet}\,^{\circ}18^{02-25},22^{45}-23^{08};=na$
23	6	3.2	.	$\overset{\circ}{\bullet}\,^{\circ}5^{31}-6^{02}\ \overset{\circ}{\bullet}\,^{\circ}11^{10}-16^{25}\ \overset{\circ}{\bullet}\,^{\circ}20^{30}-21^{40}$
24	7	0.0	.	$\overset{\circ}{\bullet}\,^{\circ}14^{55}\ldots 15^{09};=na-a,np$
25	7	.	.	$\equiv^{0-1}2^{00}-6^{20}\equiv^{2-0}9^{40}=-13^{15}$
26	7	.	.	$=0^{30}-11^{30}\ \triangle^{\circ}2^{00}-11^{00}$
27	7	.	.	$=3^{30}-10^{30};\ 21^{40}-24;\ \triangle^{\circ}4^{00}-9^{00},20^{00}-21^{40}$
28	5	.	.	$=0^{00}-6^{40}\equiv^{1}-9^{15}\equiv^{\circ}-12^{30}=-19^{05}=-20^{40}\equiv^{\circ}-24$
29	6	.	.	$\equiv^{0-2}0^{00}-10^{45}=-18^{45}=-24;\ \triangle^{2}21^{30}-24$
30	6	.	.	$=0^{00-45}\equiv^{1-2}-3^{50}\equiv^{2}-5^{30}\equiv^{1-0}-8^{10}=-12^{40};p,np;\ \triangle^{2}0^{00}-a$
31				
Σ	—	33.2	—	UWAGI

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1	7	.	.	$=0^{00}-4^{40}\equiv^{\circ}-7^{30}=-12^{20},17^{20}-24;\ \triangle^{\circ}np$
2	6	.	.	$=0^{00}-5^{45}=4^{40}-5^{45}\equiv^{\circ}7^{10}=-11^{30}\infty -19^{30}=-24,\ \triangle^{0-1}na-a$
3	6	.	.	$=na\equiv^{2-1}3^{40}-9^{40}=-p,p-24,\ \triangle^{2}np$
4	6	.	.	$=0^{00}-3^{45}\equiv^{\circ}-5^{45}\equiv^{1}-9^{20}=-24=17^{15}-19^{20},\ \triangle^{\circ}0^{00}-11^{00},np$
5	6	0.5	.	$\overset{\circ}{\bullet}\,^{\circ}22^{45}-23^{05}=0^{00}-24,\ \triangle^{\circ}na$
6	4	3.7	.	$\overset{\circ}{\bullet}\,^{0-2}4^{45}-8^{35}\ \overset{\circ}{\bullet}\,^{\circ}-18^{35};=19^{00}-24,\ \triangle^{\circ}na$
7	7	.	.	$=1^{00}-9^{50}=21^{30}-24,\ \triangle^{\circ}19-24$
8	6	.	.	$\equiv^{0-1}0^{14}-3^{30}\equiv^{\circ}-4^{45}\ 23^{45}-24,\ \triangle^{\circ}0^{00}-13^{00},18^{00}-24$
9	4	.	.	$\equiv^{\circ}0^{00}-na\equiv^{2-0}-9^{40}=a,\ \triangle^{\circ}20^{00}-24$
10	5	.	.	$=0^{00}-1^{50}\equiv^{1}-2^{30}\equiv^{2-0}-11^{45}=-19^{40}\equiv^{2}-24,\ \triangle^{1}0^{00}-11^{00}$
11	5	0.0	.	$\equiv^{2}0^{00}-11^{45}=-17^{10}\equiv^{1}-21^{30}\equiv^{2}-24,\ \triangle^{\circ}20^{00}-24$
12	5	0.0	.	$\overset{\circ}{\bullet}\,^{\circ}6^{00}-17^{40},\equiv^{2-0}0^{00}-9^{50}=17^{40}-24,\ \triangle^{1}na\ \triangle^{\circ}20^{00}-24$
13	5	0.0	.	$=0^{00}-20^{10}\equiv^{\circ}-24$
14	5	1.3	.	$\overset{\circ}{\bullet}\,^{\circ}3^{05}\ 7^{40}\ 12^{40}\ 14^{10}\ \overset{\circ}{\bullet}\,^{\circ}22^{45}-23^{40}\equiv^{2-0}0^{00}-4^{30}\equiv^{0-1}na,a=a-24$
15	7	0.0	.	$\overset{\circ}{\bullet}\,^{\circ}0^{35}\ 2^{10}\ 3^{20}-4^{10}\ \overset{\circ}{\bullet}\,^{0-1}9^{00}\ 10^{20}-11^{30};=0^{00}-a\equiv^{\circ}20^{50}-24$
16	6	.	.	$\equiv^{\circ}0^{00}-2^{40}=-3^{45}\equiv^{\circ}-a\equiv^{2-1}-9^{40}\equiv^{\circ}-11^{20}=-13^{50},16^{40}-24,\ \triangle^{\circ}a$
17	6	0.0	.	$\overset{\circ}{\bullet}\,^{\circ}8^{50}-9^{05};=na$
18	7	0.0	.	$=na-a,p-24$
19	8	0.0	.	$\overset{\circ}{\bullet}\,^{\circ}5^{58}\ 7^{05}-8^{15};=0^{00}-2^{30},na$
20	8	.	.	$\overset{\circ}{\bullet}\,^{\circ}1^{35\ldots50},4^{30}-5^{05},\ \triangle^{1}np$
21	8	.	.	$=1^{00}-2^{40}\equiv^{0-1}-9^{50}=-12^{00},\ \smile 3^{30}-8^{30}$
22	6	.	.	$=0^{00}-1^{15}\equiv^{\circ}6^{05}-7^{40}=-9^{30}\infty -13^{30},14^{30}-16^{30}\equiv^{\circ}21^{50}-24,\ \smile na-a,np$
23	6	.	.	$\equiv^{1}0^{00}-8^{30}\pm -12^{40}\infty -16^{20}=-21^{50}=16^{45}-18^{40}=p-np,\ \smile na-a\ p-np$
24	6	.	.	$\equiv^{0-2}0^{00}-9^{55}\ 21^{50}-24,\ \smile 0^{00}-10^{00}\ \triangle^{\circ}20^{00}-21^{50}$
25	6	.	.	$\equiv^{2-0}0^{00}-10^{30}=11^{00}-15^{00}\infty -16^{30}=-24,\ \smile 0^{00}-8^{30}$
26	6	.	.	$=1^{00}-5^{40}\equiv^{\circ}-8^{35}=-10^{30}\infty -14^{30},\ \smile 4^{00}-9^{00},\ \mathrm{fm}\ 16^{30}-18^{30}$
27	7	6.0	.	$\overset{\circ}{\bullet}\,^{\circ}10^{35}-11^{40}\ 12^{05}-23^{40};=6^{30}-8^{15}$
28	5	4.8	.	$\overset{\circ}{\bullet}\,^{\circ}1^{40}-2^{40}\ 4^{10}-13^{10};=0^{00}-24$
29	6	2.8	.	$\overset{\circ}{\bullet}\,^{\circ}5^{12}-p;=0^{00}-24$
30	7	.	.	$=0^{00}-6^{35}\equiv^{\circ}-7^{40}=-24=16^{30}-17^{40},\ \smile 4^{00}-8^{30}$
31	6	13.4	.	$\overset{\circ}{\bullet}\,^{\circ}22^{32}-24;=0^{00}-7^{45}\equiv^{\circ}-11^{20}=-24,\ \triangle 21^{00}-22^{32}$
Σ	—	32.5	—	UWAGI

Wrocław - Gądów Mały φ = 51°08' λ = 16°59' Listopad - Novembre 1962

Dni	Ciśnienie P = 900 + I	II	III	Dies	Temperatura t I	II	III	Dies	Max	Min	Wilgotność względna U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie i pogoda N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	93.8	94.2	95.0	94.3	5.0	5.2	5.5	5.3	6.4	4.8	100	100	100	100	0.0	0.0	0.0	0.0	10 ●	10 ●	10	NW 5	WNW 2	W 2
2	97.1	99.0	101.0	99.0	5.5	8.0	7.2	7.0	8.5	5.1	100	87	94	94	0.0	1.3	0.6	0.6	10 ●	7	10 ≡	W 2	WSW 3	ESE 2
3	101.6	100.9	101.4	101.3	5.4	10.4	1.0	4.4	12.2	0.7	100	81	100	94	0.0	2.4	0.0	0.8	10	4	0	SE 2	C 0	NNE 1
4	101.0	100.2	99.3	100.2	2.4	11.2	6.4	6.6	14.1	-1.2	100	85	97	94	0.0	2.0	0.3	0.8	1	7	4	E 2	SE 6	SE 4
5	97.1	95.8	94.9	95.9	6.4	15.6	11.2	11.1	15.9	3.9	95	62	77	78	0.4	6.7	3.1	3.4	3	1	4	SE 4	SE 9	SE 7
6	92.5	92.4	95.0	93.3	7.7	13.7	10.9	10.8	14.0	7.4	86	59	77	74	1.5	6.5	3.0	3.7	4	10	5	E 5	ESE 7	ESE 8
7	99.2	101.7	102.9	101.3	8.1	14.9	9.8	10.6	15.6	6.8	87	71	93	84	1.4	4.8	0.8	2.3	5	9	1	ESE 5	SSE 6	SE 2
8	100.4	97.8	97.7	98.6	8.8	17.2	13.7	13.4	17.7	7.8	89	57	69	72	1.2	8.5	4.9	4.9	1	8	5	SE 3	SE 9	SE 5
9	97.1	97.1	99.0	97.7	10.5	12.2	5.2	8.3	13.7	5.1	80	75	90	82	2.6	3.5	0.8	2.3	6	9	10	SE 3	NE 3	ENE 4
10	100.5	101.4	105.2	102.4	5.2	4.8	2.4	3.7	5.6	2.4	86	82	91	86	1.2	1.5	0.7	1.1	10	10 ●	10 ●	NE 4	NE 5	NE 5
11	105.3	104.2	103.1	104.2	1.4	2.7	3.1	2.6	3.3	1.1	96	88	91	92	0.3	0.9	0.6	0.6	10	10	10	NE 4	NNE 4	ENE 2
12	101.9	101.5	103.2	102.2	4.0	4.2	3.4	3.8	4.4	3.1	100	97	100	99	0.0	0.2	0.0	0.1	10 ●	10 ●	10	NE 2	NE 2	C 0
13	104.1	104.5	104.1	104.2	4.2	6.3	6.2	5.7	6.6	3.3	100	94	100	98	0.0	0.5	0.0	0.2	10	10	10	C 0	C 0	NE 1
14	103.5	103.6	103.4	103.5	6.3	6.4	5.4	5.9	6.6	5.4	100	100	98	99	0.0	0.0	0.2	0.1	10 ● ● ≡	10 ●	10 ●	NNE 1	C 0	W 2
15	98.6	93.6	91.4	94.5	5.0	6.2	4.3	5.0	6.3	3.7	98	97	93	96	0.1	0.3	0.5	0.3	10	10 ●	10	SE 2	S 3	WSW 3
16	94.9	96.9	99.6	97.1	1.8	4.0	-0.1	1.4	4.5	-1.1	83	72	92	82	1.2	2.2	0.5	1.3	8	8	0	W 5	W 7	W 5
17	100.7	99.0	95.0	98.2	-0.7	3.1	1.0	1.1	3.5	-2.0	91	64	75	77	0.5	2.7	1.7	1.6	10	10	9	SW 2	S 5	ESE 5
18	88.9	87.2	84.9	87.0	2.2	5.3	5.0	4.4	5.7	0.6	70	63	79	71	2.2	3.3	1.8	2.4	10	3	10	SE 8	SE 7	E 4
19	85.4	89.3	91.0	88.6	3.6	6.6	3.0	4.0	7.0	0.7	97	68	98	88	0.3	3.1	0.2	1.2	10	2 ●	10 ●	SW 6	SW 5	N 1
20	92.1	92.9	95.7	93.6	2.7	1.4	0.2	1.1	3.5	0.2	98	98	100	99	0.1	0.2	0.0	0.1	10 ●	10 ✗	0	NNW 1	NW 5	SW 1
21	97.1	96.7	95.0	96.3	-0.3	3.2	0.0	0.7	4.0	-2.5	96	78	94	89	0.3	1.7	0.4	0.8	10	7 ●	10	C 0	ESE 3	E 2
22	93.6	96.2	102.4	97.4	1.2	3.0	0.6	1.4	3.2	0.0	85	84	90	86	1.1	1.2	0.6	1.0	10	10 ✗	10	ENE 4	SSW 4	W 5
23	106.0	107.6	110.3	108.1	0.0	2.2	-1.3	-0.1	2.4	-3.3	82	66	83	77	1.1	2.5	1.0	1.5	10	5	0	SW 4	WSW 8	W 3
24	113.8	114.6	116.4	114.9	-0.5	0.0	0.4	0.0	0.6	-2.9	92	82	76	83	0.5	1.1	1.5	1.0	10	10	10	WNW 1	WNW 4	N 1
25	117.6	116.4	115.6	116.5	-0.9	1.3	-0.6	-0.2	1.7	-1.3	83	79	94	85	1.0	1.4	0.3	0.9	10	7	9	C 0	C 0	SE 1
26	116.9	118.0	119.6	118.2	1.3	2.5	2.2	2.0	3.0	-0.8	100	96	100	99	0.0	0.3	0.0	0.1	10 ≡	10	10 ● ≡	C 0	NW 1	NW 1
27	118.6	117.2	115.2	117.0	2.0	3.7	2.2	2.5	3.8	1.7	100	93	98	97	0.0	0.6	0.2	0.3	10	10 ●	10	W 1	C 0	C 0
28	111.7	111.3	111.8	111.6	2.2	3.8	2.7	2.8	4.3	1.3	91	87	91	90	0.7	1.1	0.6	0.8	10	10	10	SW 3	WSW 3	WSW 3
29	110.5	109.2	107.1	108.9	3.6	6.2	3.7	4.3	6.4	2.6	95	91	90	92	0.4	0.9	0.8	0.7	10 ●	10	10	W 4	W 5	SW 6
30	102.4	102.2	103.9	103.5	5.0	5.0	3.2	4.1	5.4	3.2	92	92	91	92	0.7	0.7	0.7	0.7	10	9	10	W 9	WNW 6	WNW 7
31																								
M	101.5	101.4	102.1	101.7	3.6	6.3	3.9	4.4	7.0	1.9	92	82	91	88	0.6	2.1	0.9	1.2	8.6	8.2	7.6	3.1	4.1	3.1

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1	117.3	122.4	126.7	122.3	0.1	1.0	0.0	0.3	3.4	-0.8	94	90	82	89	0.4	0.7	1.1	0.7	8	9	9	NW 4	NW 4	WNW 2
2	129.4	129.4	129.2	129.3	-2.7	-1.3	-2.4	-2.2	0.4	-5.2	89	80	87	85	0.6	1.1	0.7	0.8	10	8	10	WNW 3	W 3	C 0
3	124.8	122.3	119.4	122.2	-7.4	-0.9	-7.2	-5.7	0.1	-8.8	99	85	90	91	0.0	0.8	0.3	0.4	0 ≡	3	0 ≡	ESE 1	SE 1	C 0
4	116.1	114.5	113.2	114.6	-6.3	1.3	-3.3	-2.9	3.0	-10.1	91	63	68	74	0.3	2.5	1.6	1.5	8	6 ⊙	0	C 0	W 4	W 5
5	112.2	113.7	116.6	114.2	-1.3	-0.4	0.0	-0.4	1.1	-4.3	92	96	98	92	1.0	0.2	0.1	0.4	9	10 ●	10 ●	WNW 5	W 5	WNW 2
6	116.5	116.2	116.2	116.3	0.0	-0.2	-3.5	-1.8	1.6	-6.1	98	90	99	96	0.1	0.6	0.0	0.2	10	5 ⊙	10 ≡	C 0	W 4	C 0
7	114.4	114.0	114.9	114.4	-7.4	2.3	-2.8	-2.6	4.2	-8.3	90	81	91	87	0.3	1.5	0.5	0.3	2 ≡	0	0	C 0	W 2	W 1
8	116.3	116.3	112.5	115.0	-7.1	3.0	-1.9	-2.0	3.8	-7.3	91	67	90	83	0.3	2.5	0.5	1.1	0	6	8	C 0	SW 1	SE 1
9	101.4	96.1	90.1	95.9	-1.3	1.2	3.4	1.7	4.2	-3.9	83	75	75	78	1.0	1.7	2.0	1.6	8	9	9	SE 3	S 5	SSW 8
10	88.5	88.5	90.0	89.0	1.8	4.6	2.6	2.9	5.0	1.0	92	70	96	83	1.3	2.6	0.3	1.4	6	5	10 ●	SSW 7	SSW 7	SSW 8
11	93.3	92.9	87.3	91.2	3.2	4.5	3.1	3.6	5.3	2.4	88	76	83	82	0.9	2.0	1.3	1.4	10	9	10 ●	W 7	W 8	SSW 6
12	80.9	78.9	80.9	80.2	3.4	5.0	2.8	3.5	6.4	2.8	83	63	74	73	1.3	3.3	2.0	2.2	9	9	9	S 6	S 8	SSE 2
13	80.7	80.3	84.7	81.9	-0.1	6.0	2.2	2.6	6.2	-0.4	92	66	71	76	0.5	3.3	2.1	2.0	8	9	10	E 3	SSW 3	WNW 1
14	89.2	91.8	93.2	91.4	1.6	2.0	-0.7	0.6	2.9	-2.4	98	85	90	91	0.2	1.1	0.6	0.6	10	8	9	W 3	WNW 5	W 3
15	79.4	71.4	72.6	74.5	1.7	1.8	1.0	1.4	2.6	-2.4	70	91	90	84	2.0	0.7	0.7	1.1	10	10 ✗	7	SSW 10	SW 8	WSW 5
16	57.5	60.2	64.6	60.8	1.2	3.4	3.4	2.8	4.6	0.1	98	95	98	97	0.2	0.4	0.1	0.2	10	10 ●	10	SW 2	SW 6	W 4
17	78.0	80.6	84.2	80.9	0.4	1.4	-0.9	0.0	3.4	-1.6	98	94	92	95	0.1	0.4	0.5	0.3	10	10 ✗	5	WNW 4	W 7	W 5
18	83.8	84.0	86.5	84.8	-0.8	-0.4	-3.7	-2.2	0.0	-3.8	95	92	94	94	0.3	0.5	0.3	0.4	10	10 ✗	8	WNW 2	WNW 2	NNE 3
19	89.4	91.5	98.5	93.1	-5.1	-4.5	-4.5	-4.6	-3.2	-6.0	90	91	93	91	0.4	0.4	0.3	0.4	10	9 ✗	10 ✗	NNE 1	ENE 1	C 0
20	105.3	107.6	109.1	107.3	-7.3	-4.4	-5.5	-5.6	-3.9	-7.8	88	89	90	89	0.4	0.5	0.4	0.4	9	9 ✗	10 ✗	NW 1	NNW 2	C 0
21	103.3	101.0	104.4	102.9	-6.6	-8.5	-11.3	-9.4	-5.0	-12.2	75	77	86	79	0.9	0.7	0.4	0.7	10 ✗	5 ⊙	0	E 4	ENE 4	ENE 6
22	113.8	119.6	125.4	119.6	-17.9	-14.0	-15.9	-15.9	-10.9	-17.9	79	75	81	78	0.3	0.5	0.3	0.4	0	0 ✗	9	NE 3	NNW 3	NW 1
23	126.0	127.7	128.9	127.5	-15.1	-12.1	-13.7	-13.6	-11.9	-19.7	82	82	75	80	0.3	0.4	0.5	0.4	8	7	0	NNW 3	NNE 3	NE 2
24	128.6	126.1	124.2	126.3	-15.5	-8.9	-6.9	-9.6	-6.4	-16.3	81	76	83	80	0.3	0.7	0.6	0.5	1	6 ⊙	6	NE 2	NE 3	ENE 6
25	119.7	115.9	110.9	115.5	-10.1	-7.6	-8.9	-8.9	-6.7	-10.5	84	79	86	83	0.4	0.7	0.4	0.5	5	10 ✗	10 ✗	ENE 3	E 4	E 2
26	103.6	100.7	98.3	100.9	-9.9	-8.5	-7.1	-8.2	-7.1	-10.3	88	83	77	83	0.4	0.5	0.8	0.6	10 ✗	8	10	SE 2	NW 2	S 1
27	96.1	96.0	97.8	96.6	-7.7	-6.7	-16.7	-12.0	-6.4	-16.7	87	72	95	85	0.4	1.0	0.1	0.5	10 ✗	8	0	SW 1	C 0	C 0
28	98.0	98.9	98.5	98.5	-7.6	-5.2	-8.6	-7.5	-4.6	-16.9	82	83	83	83	0.6	0.7	0.5	0.6	10	10 ✗	0	SSE 2	SSE 2	SE 2
29	94.8	93.2	93.9	94.0	-11.5	-4.5	-7.9	-8.0	-4.1	-12.2	82	67	87	79	0.4	1.4	0.4	0.7	0	8	10	ESE 4	WNW 3	C 0
30	96.5	96.9	98.6	97.3	-7.3	-5.7	-5.7	-6.1	-5.3	-7.9	88	79	82	83	0.4	0.8	0.7	0.6	10	10	10	NNE 1	SE 3	ENE 3
31	101.7	103.7	106.0	103.8	-6.7	-7.1	-9.9	-8.4	-5.5	-10.2	80	88	81	83	0.7	0.4	0.5	0.5	10	10 ✗	9	NE 1	NE 3	E 4
M	101.8	101.7	102.5	102.0	-4.8	-2.0	-4.2	-3.8	-0.7	-7.2	87	81	86	85	0.5	1.1	0.7	0.8	7.5	7.6	7.0	2.8	3.7	2.7

Wrocław-Gądów Mały H_s=116m H_t=118.6m h_v=20m Listopad - Novembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	5	15.5	•	•°00-20^10, 21^20-24; =0^00-24
2	8	0.2	•	•°0^00-5^50, 6^35-7^25; =0^00-a,np-24
3	5	•	•	=0^00-8^20 ≡°-1-10^15 =-16^45 ≡-18^40 ≡°-1-24
4	6	•	•	≡°0^00-2^35 =-7^10 ≡°-8^25 = 24 =19^15-20^15, ⌓°21-24
5	6	•	•	=0^00-13^00, 23^20-24, ⌓°-1 0^00-7^00, ⊠ 20^00-22^20
6	6	0.0	•	⚲°11^43-54 =0^00-16^20
7	7	•	•	⌓°1^00-7^00, 20^00-24
8	7	•	•	=0^00-2^30, 4^30-11^30, 15^45-18^30; ⌓°-1 0^00-7^30
9	6	•	•	=7^30-14^15, 20^30-24
10	7	0.2	•	•°12^50 14^10 18^40-24, =0^00-a
11	8	0.2	•	•°0^00-1^35 ⚲°3^55 5^00 •°-5^10 ✱ ⚲°-6^10 ⚲°-6^25 ⚲°10^50-12^30, =23^30-24
12	6	2.6	•	⚲°2^40-7^20 •°-16^40 17^20-18^20, =0^00-3^30 ≡°-5^20 =-24
13	5	0.1	•	•°18^42 19^05, =0^00-24
14	5	7.7	•	⚲°2^40 4^20 •⚲°θ^30-8^05 •°-21^00 22^10, =0^00-5^30 ≡°-0-7^10 =-24
15	5	5.6	•	•°5^50 6^50, 7^20-16^40 17^10, =0^00-23^15
16	8	0.0	•	⚲°11^22 15^10 ⚲ 12^47-57, =9^30-11^40, ⌴°21^00-24
17	7	•	•	⌴0^00-10^00, ⁽ᵐ⁾8^50-9^20, ⊕'10^40-15^30
18	7	4.0	•	•°16^50 18^35, 23^40-24; =a, ⁽ᵐ⁾7^20-10^30
19	7	4.6	•	•°0^00-7^05, 20^05-23^35, =16^30-24
20	5	6.3	•	•°-1 2^25-11^30 ✱°-13^20 ✱°-14^35 ✱°-16^10 •°-17^40 18^35, =0^00-24; ⌴np
21	6	•	•	=0^00-8^45 ≡°9^40 =-16^05 ≡-16^20 =-17^30 ≡-18^40 =-24; ⌴na-a
22	6	0.0	•	✱°7^35-8^25, 20^05-22^20, =0^00-23^15
23	7	•	•	
24	6	•	•	=6^30-19^30
25	6	•	•	=7^20-24
26	5	0.2	•	⚲°10^35-11^05, 14^45-15^40, 18^45 21^30-22^40, =na ≡°-9^40 ≡°-1-22^20 =-24
27	5	0.0	•	•°12^40 13^35, 19^45-20^15, =0^00-24
28	6	0.0	•	•°19^10-45, =0^00-6^30, 7^30-20^30, 22^30-24
29	6	0.3	•	⚲°1^20 2^10 5^20-7^35 •⚲°-8^10 •° 10^10, 12^50...55 •' 13^10, =0^00-24
30	7	3.0	•	✱°4^25 5^10 ✱-5^25 •°8^40-10^20 ⚲°10^45-12^15 •°-1 13^50-15^35 ⚲° 19^50-20^10 ⚲°22^30 24; ⋙a
31				
Σ	—	50.5	—	UWAGI.

Grudzień - Décembre

1	6	0.0	•	✱°0^00-38 ⚲°a; =a-p
2	7	•	•	
3	3	•	•	=n-6^50 ≡°-8^00 =-p ≡°p-np; ⌴n-np
4	6	•	•	=n-a; ⌴°n-a
5	5	0.0	•	⚲°7^15-p, p; =n-24; ⌴°n
6	6	0.0	•	⚲°np; =n-16^35 ≡-np
7	5	0.0	•	⚲°n-a; ≡°n-10^40 =-24; ⌴'n-a
8	5	0.0	•	=0^00-24; ⌴'na
9	8	0.1	•	•°p; ⌴°na-10^00
10	8	0.6	•	•°na, 16^50-20^30, =p-24
11	8	0.0	•	•°3^30-5^30, 8^35 10^25, 18^30-np
12	8	•	•	
13	7	•	•	=5^30-10^00, p-np
14	7	0.0	•	•°9^10-11^02, =n-7^20 ≡-9^17 =-11^25
15	7	5.8	•	✱°a-p
16	7	4.2	5	•9^10 20^58, =p-24
17	6	4.5	pz.	✱ a; =n-p
18	6	0.0	5	✱n✱° 9^10-50 ✱°11^07-30 ✱°12^15 -p; =0^00-24
19	6	0.4	5	✱°a, np, =0^00-24
20	6	0.0	5	✱°n, a-24, =0^00-24.
21	5	0.0	6	✱°0^00-7^15 ⚲ 22^30-50, =7^30-24
22	6	•	6	✱°10^35-14^25, =0^00-24
23	7	•	6	✱°4^00-5^50
24	7	0.0	6	✱°7^45-10^50, =8^10-10^45
25	7	0.6	6	✱°4^05-30, 12^40 22^30
26	6	0.1	7	✱°4^50-10^50 11^00-20 =5^00-24
27	6	0.0	7	✱°6^10-11^30, =0^00-24
28	6	0.0	7	✱°12^25 13^40, =0^00-24
29	5	•	7	=0^00-24
30	4	•	7	=0^00-24
31	5	0.9	7	✱°8^05-22^30, =0^00-24
Σ	—	17.2	—	UWAGI.

Jelenia Góra φ = 50°54' λ = 15°48' Styczeń-Janvier 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU Dv I	II	III
1	67.5	70.2	70.5	69.4	5.2	2.7	-1.2	1.4	9.7	-1.7	64	67	81	71	3.1	2.4	1.1	2.2	8	10	10	WSW 7	W 5	C 0
2	71.5	72.9	77.8	74.1	-1.8	-1.0	-2.4	-1.9	-0.7	-2.5	86	83	76	82	0.8	1.0	1.2	1.0	10	10	9	NW 3	W 4	WNW 5
3	81.7	82.1	83.4	82.4	-6.8	-1.4	-0.4	-2.2	0.7	-7.7	83	86	96	88	0.6	0.8	0.2	0.5	9	10	10	S 1	SE 1	C 0
4	84.3	84.2	83.7	84.1	-2.0	-2.0	-5.4	-3.7	0.1	-6.0	87	94	90	90	0.7	0.4	0.4	0.5	10	9	0	E 1	W 3	C 0
5	82.6	80.1	78.4	80.4	-12.4	-2.8	-10.3	-9.0	-1.4	-12.5	89	84	94	89	0.3	0.8	0.2	0.4	0	9	0	ESE 2	C 0	C 0
6	76.1	73.8	73.2	74.4	-12.1	-0.6	2.2	-2.1	2.6	-13.5	89	72	87	83	0.3	1.7	1.0	1.0	2 ●	1	10 *	SE 3	SE 1	W 7
7	78.7	83.5	86.0	82.7	1.4	1.6	1.3	1.4	2.6	0.8	89	81	77	82	0.8	1.3	1.5	1.2	10 *	9	9	WNW 7	WNW 4	W 2
8	85.1	85.2	83.3	84.5	-2.4	1.2	0.4	-0.1	2.1	-7.4	87	89	92	89	0.7	0.8	0.5	0.7	10 ●	10	3	C 0	C 0	SE 2
9	77.4	74.1	73.4	75.0	1.6	1.2	0.0	0.7	2.2	-1.7	71	59	80	70	2.1	2.8	1.2	2.0	0	10	8	ESE 2	SE 4	SE 3
10	68.1	64.6	64.9	65.9	-2.0	0.4	0.0	-0.4	4.3	-3.0	77	74	76	76	1.3	1.7	1.5	1.5	10	5	3	ESE 6	SE 3	SE 3
11	64.6	61.9	61.5	62.7	4.0	7.6	8.4	7.1	9.2	-3.0	69	62	55	62	2.5	3.9	5.0	3.8	3	9	10	SE 6	SSW 3	WSW 4
12	64.4	62.3	53.0	59.9	4.3	6.0	6.4	5.8	8.4	2.1	80	64	53	66	1.6	3.4	4.5	3.2	9	5	9	C 0	S 3	SSW 11
13	51.4	53.4	56.1	53.6	3.4	4.8	1.2	2.6	7.3	-0.5	73	59	74	69	2.1	3.5	1.8	2.5	3	2	4	WSW 2	SW 7	ENE 3
14	60.9	63.1	66.1	63.4	2.0	2.9	2.6	2.5	4.0	-0.5	66	64	68	66	2.5	2.7	2.4	2.5	9	8 ⊙	7	WSW 4	WSW 6	WSW 9
15	71.4	75.0	79.3	75.2	1.6	2.3	-3.8	-0.9	2.8	-5.2	67	66	89	74	2.3	2.4	0.5	1.7	10	8	5	W 6	WSW 5	C 0
16	79.8	77.0	75.2	77.3	-6.2	3.6	-0.4	-0.8	5.3	-7.5	94	63	72	76	0.2	2.9	1.6	1.6	6	8 ⊙	6	C 0	C 0	C 0
17	74.7	75.2	75.0	75.0	0.2	2.3	-1.0	0.1	4.6	-1.2	61	63	79	68	2.4	2.7	1.2	2.1	9	9 ⊙	10	NE 3	E 3	SE 1
18	74.0	73.2	75.0	74.1	-2.4	2.0	5.4	2.6	6.9	-3.1	82	71	60	71	0.9	2.1	3.6	2.2	9	8 ⊙	9	SE 1	E 2	WSW 5
19	76.0	75.7	71.8	74.5	1.2	4.2	6.8	4.8	7.4	0.5	85	77	65	76	1.1	1.8	3.4	2.1	10	9	9 ●	SE 3	S 2	SW 6
20	76.3	78.4	83.3	79.3	6.0	8.4	2.6	4.9	8.4	2.6	74	60	68	68	2.4	4.4	2.4	3.1	9	9	3	W 6	W 10	SW 3
21	80.2	79.7	77.1	79.0	7.2	8.0	8.1	7.8	9.1	-1.1	77	79	74	77	2.4	2.2	2.8	2.5	10	10 ●	9	SW 6	WSW 6	SW 5
22	69.3	66.2	70.6	68.7	4.6	8.4	4.4	5.4	11.0	3.3	81	57	52	63	1.7	4.7	4.0	3.5	9	10	2	NE 2	WSW 5	W 5
23	73.7	74.8	77.6	75.4	2.0	3.9	1.9	2.4	4.8	0.0	68	62	73	68	2.3	3.1	1.9	2.4	1	8 ⊙	9	W 5	WSW 9	SW 4
24	76.9	74.9	71.2	74.3	1.4	3.2	1.0	1.6	3.6	0.5	76	73	96	82	1.7	2.1	0.3	1.4	9	9	10 *	SW 3	W 2	C 0
25	68.1	67.7	70.1	68.6	7.2	7.6	5.4	6.4	8.4	0.6	83	72	89	81	1.8	2.9	1.0	1.9	10	8	10 ●	WSW 7	WSW 5	WNW 6
26	76.7	78.5	72.4	75.9	1.4	2.8	1.1	1.6	5.7	0.6	96	76	96	89	0.3	1.9	0.2	0.8	10 ●	9	10 ●	NNW 3	W 1	C 0
27	76.3	78.5	77.3	77.4	2.2	2.2	1.5	1.8	4.0	0.5	84	87	80	84	1.2	1.0	1.4	1.2	9	9 ●	7 *	W 7	WNW 9	WNW 8
28	75.3	74.4	79.2	76.3	1.1	0.6	-6.4	-2.8	1.9	-6.6	85	69	83	79	1.0	2.0	0.6	1.2	10 *	9	9 *	WNW 6	NW 12	NNW 8
29	82.5	85.3	89.3	85.7	-5.6	-5.2	-6.8	-6.1	-5.0	-8.6	85	80	77	81	0.6	0.8	0.8	0.7	10 *	9 *	10 *	NW 7	NNW 4	NW 4
30	91.9	93.7	96.2	93.9	-11.2	-8.9	-9.2	-9.6	-5.8	-11.5	90	73	95	86	0.3	0.8	0.2	0.4	10 *	10 *	10 *	NNE 1	C 0	NE 2
31	94.1	92.3	88.3	91.6	-21.1	-9.2	-18.4	-16.8	-5.5	-21.4	89	82	78	83	0.1	0.5	0.3	0.3	1	1 ⊙	0	SE 2	C 0	C 0
M	75.2	75.2	75.5	75.3	-0.9	1.8	-0.2	0.1	3.8	-3.7	80	73	78	77	1.4	2.1	1.6	1.7	7.6	8.1	7.1	3.6	3.8	3.4

Luty-Février

1	76.7	72.3	74.2	74.4	-19.2	-5.8	-11.6	-12.0	-3.0	-21.5	77	56	82	72	0.3	1.7	0.4	0.8	0	2 ⊙	0	SE 1	C 0	C 0
2	74.6	75.3	79.0	76.3	-16.4	-4.8	-3.4	-7.0	-1.9	-20.4	90	69	94	84	0.2	1.3	0.3	0.6	10	7	10 ● *	ESE 2	SE 2	C 0
3	82.6	84.8	84.6	84.0	-0.9	-0.2	-9.4	-5.0	0.2	-9.8	97	90	91	93	0.2	0.6	0.3	0.4	10	9	0	WNW 3	WNW 2	C 0
4	77.9	78.4	80.7	79.0	-8.2	0.8	-1.2	-2.4	1.6	-14.0	92	88	82	87	0.2	0.8	1.0	0.7	8	9	8	C 0	W 7	WNW 2
5	72.1	63.5	70.2	68.6	-4.4	2.7	2.0	0.6	4.0	-10.1	91	82	75	83	0.4	1.3	1.8	1.2	10	10 ● *	9	C 0	SW 8	W 9
6	76.6	79.3	80.5	78.8	1.6	2.0	2.6	2.2	2.8	-1.0	85	76	79	80	1.1	1.7	1.6	1.5	10	9	9	W 8	W 8	W 3
7	77.1	74.7	70.4	74.1	0.4	3.0	1.0	1.4	4.5	-2.9	90	86	88	88	0.6	1.1	0.8	0.8	10	10	0	C 0	SE 3	C 0
8	68.9	70.7	74.1	71.2	1.6	4.4	0.0	1.5	4.6	-1.5	87	79	96	87	0.9	1.8	0.2	1.0	10	10 *	6	C 0	C 0	C 0
9	80.3	85.1	90.1	85.2	0.8	1.0	-1.6	-0.4	2.4	-2.4	92	73	90	85	0.5	1.8	0.5	0.9	9	9	7	W 4	NW 5	C 0
10	91.8	90.3	87.8	90.0	-7.1	2.7	-0.5	-1.4	4.8	-7.4	91	50	82	74	0.3	3.7	1.1	1.7	0	6	7	C 0	C 0	C 0
11	83.2	84.9	88.5	85.5	-1.5	2.8	0.1	0.4	3.1	-3.9	76	76	71	74	1.4	1.9	1.8	1.7	9	8 ●	0	C 0	W 8	WSW 3
12	70.0	59.4	52.2	60.5	1.3	5.1	4.6	3.9	6.5	-4.0	68	69	89	75	2.1	2.8	1.0	2.0	10 *	10 ●	10 ●	WSW 9	W 9	W 16
13	48.6	46.2	48.5	47.8	1.0	0.7	-1.5	-0.3	4.7	-4.0	81	88	96	88	1.3	0.7	0.2	0.7	10	10 ● *	10	W 5	W 5	C 0
14	53.1	54.4	61.3	56.3	-3.3	-1.9	-3.7	-3.2	0.3	-4.0	85	79	83	82	0.7	1.1	0.8	0.9	4	8	9	WNW 4	WNW 3	WNW 6
15	71.1	76.5	80.8	76.1	-4.5	-4.4	-5.6	-5.0	-3.2	-6.8	93	72	72	79	0.3	1.2	1.1	0.8	10 *	9 *	9	NW 6	NW 8	W 6
16	65.1	58.6	54.1	59.3	-0.3	2.5	2.3	1.7	4.1	-10.1	65	72	71	69	2.1	2.1	2.0	2.1	10	10 ● *	10 ●	WSW 7	SW 8	W 12
17	53.8	57.0	64.9	58.6	1.3	1.2	-0.1	0.6	2.5	-0.9	76	77	82	78	1.6	1.5	1.1	1.4	10 ● *	10 *	10 *	WNW 12	W 12	WNW 8
18	73.3	77.6	82.5	77.8	-2.5	0.0	-1.1	-1.2	0.3	-5.5	87	60	61	69	0.7	2.5	2.2	1.8	10 *	9	0	WNW 5	WNW 8	WNW 5
19	78.8	79.7	81.3	79.9	1.7	2.3	2.9	2.4	3.3	-2.4	96	91	83	90	0.3	0.6	1.3	0.7	10	10 ●	10	WNW 7	WNW 7	W 6
20	80.8	80.7	80.9	80.8	2.0	3.6	5.1	4.0	5.3	1.5	75	73	80	76	1.8	2.1	1.8	1.9	10	10	9	W 6	W 5	NW 8
21	83.8	85.8	88.3	86.0	-0.9	-1.1	-2.6	-1.8	5.3	-5.4	81	81	89	84	1.1	1.1	0.6	0.9	6	10 *	10 *	NW 2	WNW 6	NNW 5
22	90.7	91.8	93.0	91.8	-4.5	-4.9	-6.0	-5.4	-2.4	-6.2	88	81	87	85	0.5	0.8	0.5	0.6	10 *	10 *	10 *	NE 4	N 1	C 0
23	93.9	92.0	86.7	90.9	-7.3	-5.7	-5.0	-4.8	-2.8	-7.6	82	69	79	77	0.6	1.2	1.0	0.9	10	8	10 *	C 0	NW 3	NW 4
24	80.9	78.1	78.1	79.0	-5.6	-5.5	-7.0	-5.3	-2.6	-7.1	80	88	82	83	0.9	0.6	0.6	0.7	10 *	10 *	10 *	W 4	NE 3	E 3
25	78.9	79.1	80.0	79.3	-8.3	-6.6	-7.9	-7.7	-6.5	-8.8	83	72	73	76	0.5	1.0	0.9	0.8	10 *	6	10 *	C 0	ESE 5	E 5
26	79.0	77.9	77.7	78.2	-7.5	-4.7	-6.0	-6.0	-4.3	-10.3	84	79	79	81	0.5	0.9	0.8	0.7	10 *	1	9	ESE 4	ENE 6	E 4
27	75.9	74.5	74.0	74.8	-5.4	-3.0	-2.3	-3.2	-2.3	-6.8	85	84	87	85	0.6	0.8	0.7	0.7	10	10 *	10 *	E 6	E 6	E 5
28	71.4	69.7	69.2	70.1	-2.6	-0.1	-2.9	-2.1	0.0	-3.1	91	82	91	88	0.5	1.1	0.4	0.7	10 *	10	10	E 4	ENE 4	ENE 5
29																								
30																								
31																								
M	75.4	74.9	76.2	75.5	-3.5	-0.4	-2.0	-2.0	1.1	-6.5	85	76	85	81	0.8	1.4	1.0	1.1	8.8	8.6	7.6	3.7	3.1	4.1

Jelenia Góra H_s=342m H_t=343,9m h_w=16m Styczeń - Janvier 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	.	11	
2	6	0.0	8	▲10^{15}-12^{30},=7^{30}-24
3	6	0.0	7	*°9^{45}...11^{20},14^{30}-15^{10} ⚲ $^{1-0}$$18^{30}$-$20^{25}$,=na,a-p,np
4	6	.	6	=0^{00}-6^{00} 8^{40}-24
5	5	.	6	=0^{00}-3^{10} 9^{30}-24
6	5	1.1	6	*$^{0-1}$$17^{40}$..$19^{15}$-24,=$0^{00}$-24
7	7	0.0	6	*°0^{00}...3^{15}*°-7^{10},=0^{00}-6^{30}
8	6	0.1	4	•°6^{45}...7^{40} 9^{45}-10^{10},11^{10}-12^{40},=7^{30}-24
9	8	.	5	=0^{00}-6^{10}
10	7	.	3	≫21^{30}-22^{30}
11	7	0.0	3	•°16^{50} 17^{10}
12	7	0.6	pż.	•°4^{45}...6^{20},20^{10}...23^{10}-24; ≫20^{30}-21^{20}
13	8	0.1	.	•°0^{00}-5^{10} *°21^{35} 22^{20}-24
14	8	0.0	.	*°0^{00-30},3^{45}-5^{48} ⚲°16^{20-35},17^{50}-18^{15} 19^{40}-20^{10}
15	8	0.7	.	⚲°3^{40}-4^{15} *$^{0-1}$$7^{40}$..$8^{30}$ ⚲'-9^{20} *°..9^{35}; ⌴°22^{00}-24
16	7	.	pż.	⌴10^{00}-11^{00}; ⌴2^{40}-3^{30}
17	8	.	.	⚭17^{30}-19^{45},20^{30}-24
18	8	0.0	.	⌴°5-9; ⚭0^{00}-4^{20}; 8^{20}-14^{20}
19	8	1.1	.	•°6^{20}..7^{00},19^{40}...21^{20},23^{10}-24, ≫22^{10}-23^{20}
20	8	0.0	.	•°1^{20}...4^{10},15^{45}-16^{40}, ≫12^{55}-14^{10}
21	8	0.3	.	•°7^{20}..10^{15}-11^{30}..14^{20}
22	8	.	.	≫10^{20-40},14^{40}-15^{30}
23	8	2.4	.	⚲°13^{45}-14^{15} ⚲'17^{12-40}, ⌴°2^{00}-8
24	9	4.1	1	*°8^{50}-9^{20} •°17^{10}-19^{10} ⚲'-21^{20} •°-22^{40},23^{45}-24
25	7	4.0	.	•°0^{00}-3^{45},7^{20}..8^{15}-10^{30}...11^{20} ⚲°15^{15}..16^{45} •°..21^{45}
26	7	12.5	.	•°3^{15}...7^{40} 15^{40}-17^{35} ⚲°*°-19^{15} •°-24;=5^{15}-11^{10},15^{20}-24
27	7	2.4	.	•°0^{00}-6^{10} ⚲'-6^{40} •°8^{15}..9^{10} ⚲°-10^{10} •°..11^{00} ⚲°...14^{40} •°$16^{10...30}$ *°18^{15}...21^{40}, ≫21^{20}-22^{10},=na-a
28	7	4.8	2	*'4^{00}...5^{20} ⚹ $^{0-1}$$5^{50}$..$6^{45}$..$7^{15}$ ⚲ $^{0-1}$$9^{15}$...$11^{50}$,$20^{30}$-$23^{15}$ *'-24; ⚸ ^{2}12^{50}-15^{30} ⚸°-21^{45} ≫12^{40}-13^{30},=a
29	5	8.5	14	*$^{0-1}$$0^{00}$-$12^{15}$ ⚲°16^{45} *°17^{40}..18^{40} ⚲°20^{40}-22^{10}
30	6	0.7	18	*'5^{05}..6^{20} *°-9^{20}...9^{35},20^{15}...21^{20},=0^{00}-23^{30}
31	5	0.0	18	*°0^{40}...3^{20},10^{10}-11^{10},=6^{30},13^{10},22^{30}-24
Σ	—	45.4	—	UWAGI

Luty - Février

1	6	.	15	=0^{00}-7^{30},7^{50}-24; ⌴°0^{00}-10
2	6	0.8	12	*°16^{35}-20^{10} ⚲°*°-21^{40} ⚲ *°-22^{20} * $^{1-2}$-24;=0^{00}-24; ⌴°0^{00}-8^{00}
3	5	0.0	12	*°0^{00}-1^{05} ▲10^{30}-11^{15},=0^{00}-21^{45} ≡°-23^{45} ≡°-24
4	5	0.1	9	*'8^{15-50} *°-11^{15}, ≡°0^{00}-1^{30} ≡-6^{35}=-7^{40} 8^{15}-24; ∨°na
5	7	2.0	8	*°10^{40}...12^{15} *°-13^{40} •°-14^{35} ⚲ ^{2}16^{48}-17^{10} ⚲°-17^{35} *°22^{10}-24; ≫22^{15}-24;=0^{00}-9^{30}
6	7	0.0	6	*°0^{00}-1^{00} ▲-1^{10} ⚹ 2^{10}-4^{05} ⚲°9^{05}..12^{00}, ≫1^{10}-6^{45},=a...
7	7	0.0	3	⚲°7^{00}-8^{10},=7^{00}-8^{10}
8	6	0.0	pż.	•°12^{15}..14^{08} 15^{40}-17^{45},=10^{10}-24
9	7	.	.	=0^{00}-11^{30},20^{50}-24
10	8	.	.	=1^{00}-6^{10}
11	7	.	.	*°8^{40}..9^{35} •°-10^{40} ⚲°*°-11^{20} •°12^{45}..13^{00} ⚲ $^{1-0}$$13^{50}$..$16^{05}$, ≫$13^{45}$-$14^{00}$
12	7	6.4	.	*6^{40} 7^{05} ⚹°..9^{10} •°..16^{45} 17^{10}-20^{35} •$^{1-0}$-24, ≫a≫-⚹13^{10}-24
13	5	6.9	2	•°0^{00}-6^{05} ⚲ $^{1-8}$-6^{35} *°7^{40}-12^{40} ⚲°*°-14^{20} *°..15^{30}-17^{40}, ⚹-≫0^{00}-6^{40},=p-np
14	7	4.8	9	*2^{10}-5^{45} ⚲ $^{0-1}$$8^{20}$..$16^{10}$,=$0^{00}$-$6^{10}$
15	6	2.2	17	*°0^{00}-8^{15} *'-9^{40} ⚲°10^{05}..16^{10},=1^{00}-18^{25}
16	8	1.4	20	*°5^{45}..6^{10} ⚲°*°12^{25}-13^{05} •°..17^{05} ⚲°-19^{10} •°-20^{30} 21^{25} ⚲'21^{55}-22^{10},23^{15-25}; ⚸ ^{2} ⚸-7^{45}-11^{10}; ≫a,p-24
17	7	2.6	6	⚲°3^{15}..4^{30} ⚲°5^{50}-6^{10} ⚲'6^{35}..7^{15} ⚲ $^{0-2}$-14^{30} ⚲°14^{55}-15^{02} *⚹'15^{52}-17^{40} ⚲ $^{0-2}$-19^{35},20^{40}-21^{40}; ≫0^{00}..24
18	7	3.7	9	▲°3^{53}-4^{10} ⚲ $^{0-2}$ 5^{45}-8^{25} ⚲°8^{45}-9^{20}; ⚸'9^{45}-14^{40}, ≫na
19	6	2.0	15	*'1^{10}-2^{20} *°-5^{10} •$^{0-1}$..19^{10},=4^{25}-17^{00}
20	7	0.1	3	•°8^{45}..11^{20} 16^{20}-19^{40},=8^{20}-12^{30}
21	5	2.2	pż.	*°11^{50}..14^{40} ⚲'14^{45}-18^{05} *°-22^{20}..24
22	5	1.3	5	*°0^{00}-5^{15},6^{35}-12^{15} *'..13^{30} *°..24
23	6	0.4	7	*°0^{08}..5^{05} *$^{0-1}$$7^{20}$...$11^{40}$,$17^{45}$..24,=$11^{40}$-$13^{00}$,$16^{30}$-$19^{00}$
24	5	3.6	6	*$^{0-1}$$0^{00}$..$7^{45}$-$9^{30}$..$10^{15}$-$18^{30}$..24
25	6	0.2	14	*°0^{00}...10^{40},16^{20}-21^{10},=7^{20}-24
26	6	0.1	11	*°6^{10}..8^{15}-10^{20}=0^{00}-24
27	5	0.1	7	*°0^{25}..5^{20} *$^{0-1}$$10^{40}$..$13^{00}$-$20^{00}$..24;=$0^{00}$-24
28	6	0.0	8	*°1^{30}...9^{20},=0^{00}-24
29				
30				
31				
Σ	—	40.9	—	UWAGI

Jelenia Góra φ=50°54' λ=15°48' Marzec - Mars 1962

DNI	CIŚNIENIE P-900 I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D.w I	II	III
1	67.6	67.8	66.7	67.4	-3.6	-2.3	-3.5	-3.2	-1.7	-4.2	94	80	85	86	0.3	1.0	0.7	0.7	10	10 *	10	E 2	C 0	C 0
2	64.7	63.1	63.0	63.6	-4.5	-0.3	-2.5	-2.4	0.9	-5.0	93	68	87	83	0.3	1.9	0.7	1.0	10 *	8	10	C 0	C 0	C 0
3	62.6	62.9	61.3	62.3	-2.1	-1.2	0.1	-0.8	0.8	-5.0	89	89	81	86	0.5	0.6	1.2	0.8	10 *	9 * ●	9 ●	C 0	W 2	C 0
4	55.8	53.8	52.6	54.1	-2.5	1.3	0.8	0.1	2.1	-3.7	93	89	92	91	0.4	0.8	0.5	0.6	9	10 *	10 *	C 0	C 0	E 2
5	53.5	52.6	53.2	53.1	0.6	4.9	1.7	2.2	5.3	0.2	96	87	94	92	0.3	1.1	0.4	0.6	10	8	10 ●	C 0	C 0	WNW 2
6	59.6	66.5	74.9	67.0	-3.1	-1.8	-3.5	-3.0	1.8	-5.8	93	86	83	87	0.4	0.8	0.8	0.7	10 *	10 *	10 *	W 5	WNW 6	W 5
7	80.8	82.4	85.3	82.8	-6.1	-2.1	-2.9	-3.5	-1.0	-8.2	86	70	91	82	0.5	1.5	0.4	0.8	10 *	9	9	WNW 7	WNW 4	WNW 3
8	86.1	86.8	84.7	85.9	-4.7	0.2	-5.5	-3.9	3.0	-6.5	96	55	87	79	0.2	2.8	0.5	1.2	10	2 ⊙	0	NE 2	C 0	C 0
9	80.2	76.3	77.2	76.2	-3.6	3.4	0.5	0.2	4.0	-8.4	62	37	44	48	1.8	4.9	3.5	3.4	9	7 ⊙	2	C 0	ESE 9	SE 6
10	69.1	69.0	68.6	68.9	-0.5	4.2	1.3	1.6	4.5	-0.9	70	55	79	68	1.8	3.7	1.4	2.3	8	9 ⊙	6	ESE 3	E 2	C 0
11	67.2	65.9	64.0	65.7	1.9	6.9	2.1	3.2	8.1	0.5	85	67	89	80	1.0	3.3	0.8	1.7	9	5 ⊙	10	E 3	E 3	C 0
12	60.1	57.4	58.6	58.7	1.3	4.0	-1.0	0.8	4.2	-1.2	98	90	89	92	0.1	0.8	0.7	0.5	10 ●	10 ●	10 *	C 0	W 5	W 7
13	66.4	70.0	73.9	70.3	-5.4	-5.2	-7.1	-6.2	-0.9	-8.3	80	73	80	78	0.8	1.1	0.7	0.9	10	7 * ⊙	8	WNW 8	W 5	W 4
14	77.7	78.3	78.0	78.0	-9.1	-3.1	-8.9	-7.5	-1.4	-10.1	82	55	80	72	0.5	2.2	0.6	1.1	5	2 ⊙	0	WNW 2	NW 4	C 0
15	76.5	75.9	78.1	76.8	-13.5	-1.3	-4.9	-6.2	-0.7	-13.9	96	33	66	65	0.1	3.7	1.4	1.7	3	10	10	C 0	SSE 2	E 2
16	80.5	81.7	81.6	81.3	-6.3	-3.1	-4.3	-4.5	-2.6	-7.9	86	64	49	66	0.5	1.8	2.3	1.5	10 *	10	10	ENE 1	NE 4	NNW 4
17	78.8	76.0	77.1	77.3	-5.5	-1.0	-2.1	-2.7	-0.7	-5.8	65	57	60	61	1.4	2.5	2.1	2.0	10	8	9	NNW 3	NNW 9	NW 6
18	78.0	78.9	79.5	78.8	-4.0	-0.3	-6.9	-4.5	-0.2	-7.0	84	63	91	79	0.7	2.3	0.3	1.2	9 *	9 * ⊙	7	NW 4	NNW 6	C 0
19	79.0	78.7	78.3	78.7	-5.5	-0.1	-2.1	-2.4	1.3	-7.9	92	63	79	78	0.3	2.3	1.1	1.2	9	8	10	SE 2	NE 2	C 0
20	77.9	77.1	75.8	76.9	-3.9	0.7	-3.1	-2.4	1.3	-4.1	89	58	77	75	0.5	2.7	1.1	1.4	10	10 *	0	C 0	NW 1	SE 1
21	77.3	71.8	70.6	71.9	-4.4	0.3	-1.5	-1.8	1.7	-5.2	77	66	66	70	1.0	2.1	1.9	1.7	1	9	9	E 5	ESE 4	E 3
22	69.0	68.3	67.4	68.2	-6.7	-1.2	-2.3	-3.1	-0.3	-8.5	88	66	72	75	0.4	1.9	1.5	1.3	9	6 ⊙	10	C 0	NE 2	C 0
23	66.8	68.1	70.3	68.4	-5.7	-2.1	-2.3	-3.1	-1.3	-7.1	97	77	78	84	0.1	1.2	1.2	0.8	10 *	10 *	8 *	C 0	E 3	ENE 3
24	73.5	75.3	78.2	75.7	-6.9	1.4	-4.1	-3.4	3.2	-7.9	91	56	82	76	0.3	3.0	0.8	1.4	4	8 ⊙	0	C 0	WNW 4	C 0
25	80.0	79.3	77.6	79.0	-4.4	1.2	-1.6	-1.6	2.1	-7.1	81	64	88	78	0.8	2.4	0.6	1.3	10	9	8	C 0	NW 2	C 0
26	75.1	72.4	69.1	72.2	-2.8	3.5	-1.0	-0.3	4.1	-4.2	93	47	71	70	0.4	4.1	1.7	2.1	8	0 ⊙	0	C 0	ENE 4	E 2
27	64.3	61.8	61.4	62.5	-4.7	5.6	-0.8	-0.2	6.7	-5.1	83	49	89	74	0.7	4.6	0.6	2.0	6 ⊙	10	0	SE 1	N 2	C 0
28	61.6	63.5	67.3	64.1	2.7	4.9	1.9	2.8	5.7	-2.4	74	69	82	75	1.9	2.8	1.3	2.0	9	9	9	W 1	W 7	W 6
29	66.8	63.3	57.5	62.5	-0.1	6.5	4.7	4.0	7.5	-1.5	94	59	87	80	0.4	4.0	1.1	1.8	8	8	10	C 0	SE 3	NE 1
30	57.0	55.7	51.9	54.9	7.9	11.4	9.7	9.7	13.0	3.0	78	66	73	72	2.3	4.6	3.2	3.4	9	8	10	WNW 3	WSW 4	S 4
31	49.2	52.7	57.9	53.3	11.4	8.4	1.3	5.6	12.4	1.0	67	85	92	81	4.4	1.6	0.5	2.2	10	10 ●	10 *	SW 6	WNW 5	WSW 2
M	69.7	69.5	69.6	69.6	-3.0	1.4	-1.5	-1.2	2.7	-5.0	86	66	79	77	0.8	2.4	1.1	1.4	8.5	8.0	7.2	1.9	3.4	2.0

Kwiecień - Avril

1	64.3	67.9	69.3	67.2	2.5	6.0	0.0	2.1	7.1	-0.9	84	54	96	78	1.2	4.3	0.2	1.9	6	6	0	W 4	WSW 8	C 0
2	68.8	70.6	74.6	71.3	1.5	7.1	3.5	3.9	8.4	-0.5	78	56	71	68	1.5	4.4	2.2	2.7	9	10 ●	6	SSW 2	WSW 9	SW 3
3	71.2	68.2	64.6	68.0	6.3	12.1	9.3	9.2	15.1	1.5	59	39	48	49	3.9	8.6	6.1	6.2	9	7	0	SSW 5	S 6	S 8
4	59.7	69.4	55.4	61.5	5.7	12.6	6.3	7.7	14.7	5.4	67	43	78	63	3.1	8.3	2.1	4.5	9	8 ⊙	10 ●	E 2	WSW 2	S 3
5	47.2	48.8	50.1	48.7	3.2	7.6	3.7	4.6	10.4	2.1	100	62	80	81	0.0	3.9	1.6	1.8	6 ⊙	9	0	WSW 2	WSW 6	NE 1
6	54.1	57.7	64.5	58.8	0.5	6.9	4.2	4.0	9.4	-0.9	90	61	92	81	0.6	3.8	0.6	1.7	10	10	10 ●	C 0	WNW 3	W 5
7	72.7	72.7	69.8	71.7	0.6	5.2	4.5	3.7	6.1	0.3	88	54	66	70	0.8	4.0	2.7	2.5	9 *	7 ⊙	10	WNW 7	WNW 6	WSW 6
8	67.9	67.4	66.7	67.3	6.1	10.5	8.7	8.5	12.4	3.1	82	62	71	72	1.7	4.9	3.3	3.3	8	7 ⊙	10	WSW 5	WSW 6	WSW 5
9	70.0	72.2	75.2	72.5	6.3	8.8	3.3	5.4	11.3	2.5	53	52	97	67	4.4	5.5	0.2	3.4	7 ⊙	9 ⊙	9	WSW 7	W 7	C 0
10	79.7	80.3	81.9	80.6	-0.3	6.7	0.2	1.7	8.3	-2.2	98	54	90	81	0.2	4.5	0.6	1.8	9	7 ⊙	0	SE 1	WNW 5	C 0
11	82.3	81.2	81.0	81.5	-2.6	8.5	2.3	2.6	9.9	-3.6	95	40	95	77	0.2	6.7	0.4	2.4	8 ⊙	10	8	C 0	NE 3	E 1
12	79.6	77.0	76.5	77.7	-0.2	12.7	5.7	6.0	14.5	-1.1	100	41	76	72	0.0	8.6	2.3	3.6	0 ⊙	6 ⊙	7	C 0	E 1	SSE 2
13	75.1	74.8	74.4	74.8	3.2	4.5	2.0	2.9	5.7	0.0	97	90	96	94	0.3	0.8	0.3	0.5	10 ●	10 ●	10	NW 2	W 3	C 0
14	75.3	77.9	81.2	78.1	1.4	4.6	3.2	3.1	5.2	0.7	96	74	90	87	0.3	2.2	0.8	1.1	10	10	10	W 3	N 3	ENE 5
15	81.8	81.1	80.1	81.0	2.6	4.3	6.6	5.0	6.8	2.2	100	97	98	98	0.0	0.3	0.1	0.1	10 ●	10 ●	10 ●	ENE 2	SE 1	SE 3
16	77.0	74.9	78.8	76.9	8.5	14.0	3.7	7.5	17.0	1.4	96	68	95	86	0.5	5.1	0.4	2.0	10 ●	9	1	SE 3	E 6	C 0
17	76.3	74.4	74.6	75.1	10.2	16.1	13.9	13.5	16.8	0.1	56	46	54	52	5.4	9.9	7.4	7.6	9	10	10	SSE 9	SE 13	SSE 10
18	71.5	71.6	71.8	71.6	12.9	20.2	17.4	17.0	21.4	11.9	55	35	38	43	6.7	15.5	12.4	11.5	9	8	9	SE 12	SSE 9	SSE 9
19	73.1	74.7	77.2	75.0	15.8	24.7	15.2	17.7	25.6	12.5	50	28	73	50	8.9	22.3	4.6	11.9	9	7 ⊙	9	SSE 5	NNW 2	SE 1
20	79.1	77.1	76.4	77.5	10.0	23.0	14.0	15.2	24.9	8.5	91	41	68	67	1.1	16.5	5.1	7.6	6 ⊙	9	2	C 0	SE 4	C 0
21	78.8	78.1	79.6	78.8	12.6	23.1	14.1	16.0	23.8	9.5	87	45	89	74	1.9	15.5	1.8	6.4	0	5 ⊙	7	WSW 4	NW 2	SE 1
22	78.8	78.9	78.7	78.8	13.1	23.9	12.6	15.6	24.7	4.0	86	22	55	54	2.1	23.1	6.6	10.6	8 ⊙	4 ⊙	2	C 0	ESE 6	E 1
23	80.3	79.6	80.2	80.0	8.1	25.5	13.8	15.3	26.3	4.5	81	20	74	58	2.1	26.1	4.1	10.8	0	0 ⊙	0	C 0	SE 4	SE 1
24	82.7	83.0	84.5	83.4	9.5	25.4	13.4	15.4	25.8	4.6	84	28	63	58	1.9	23.2	5.7	10.3	0 ⊙	3 ⊙	0	SE 2	ESE 4	ESE 1
25	85.9	85.1	84.8	85.3	10.4	25.0	14.1	15.9	25.4	5.4	85	32	68	62	1.9	21.5	5.1	9.5	0	3 ⊙	0	C 0	E 3	C 0
26	82.7	79.5	75.7	79.3	10.1	20.9	14.9	15.2	22.4	5.7	86	58	73	72	1.8	10.4	4.5	5.6	1 ⊙	4	10 ●	C 0	WNW 3	W 2
27	72.2	74.6	73.6	73.5	7.9	6.1	7.1	7.0	15.3	3.1	94	94	85	91	0.6	0.6	1.3	0.9	10	10 ●	8	NW 9	W 3	NW 1
28	65.6	66.1	68.0	66.6	3.7	2.1	2.1	2.6	8.3	0.9	90	96	95	94	0.8	0.3	0.4	0.5	10 ●	10 ● *	9 ●	WSW 6	WNW 4	C 0
29	69.2	68.3	67.7	68.4	1.9	4.9	0.6	2.0	7.8	-0.3	100	82	94	92	0.0	1.6	0.4	0.7	10	7 ⊙	0	W 2	W 3	C 0
30	66.8	70.1	74.2	70.4	0.3	1.3	1.5	1.2	2.9	0.0	96	89	80	88	0.2	0.8	1.4	0.8	10 *	10 * ●	10	WNW 3	NW 2	C 0
31																								
M	73.0	73.4	73.7	73.4	5.7	12.5	7.4	8.2	14.5	2.9	84	55	78	72	1.8	8.8	2.8	4.5	7.1	7.3	5.9	3.3	4.7	2.3

Jelenia Góra $H_s = 342m$ $H_t = 343{,}9m$ $h_w = 16m$ Marzec - Mars 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘBOŚNIEGU h	POGODA
1	5	0.0	4	±7^40-11^30 *°-13^45 15^10...18^40; =0^00-24
2	5	0.0	5	*°6^05...7^20, 8^38-10^15; =0^00-24
3	5	0.1	5	*°-6^40...13^00; =0^00-24
4	5	4.2	2	*°11^40...12^30 *°-13^40 *°16^50...17^20-20^30 *°-1-24; =0^00-24
5	6	9.0	2	*'0^00-1^45 •°16^47...18^10 20^10-24; =0^00-24
6	5	2.0	5	•°0^00-2^38 *°-3^05-10^20...14^10-20^35...21^40; =0^00-24
7	6	0.2	10	*°6^40...11^00, 14^40...16^10; =0^00-24
8	8	.	6	*°1^40...2^00; =0^00-11^15; ⌣°0^00-9
9	8	.	4	»14^10-18^40
10	8	.	1	
11	8	0.1	pł.	*°23^05...24; =22^30-24
12	5	9.5	pł.	*°0^00...2^30 •°...7^00-15^25 •'-16^20 •°-17^35 *°-19^20 *°-24; =0^00-7^40 ≏°-11^35 =-24
13	6	0.0	5	*°0^00-6^20 ∇°7^10-18^10; ↓'6^20-8^10; =0^00-11^05
14	7	.	5	
15	8	0.2	2	*°23^30...24, ⌣°1^00-9^00
16	8	0.5	pł.	*°0^00...9^30
17	8	0.0	pł.	*°0^15...2^40, 8^40...10^30 ∇°12^30...15^10 ∇°-2-17^10
18	7	0.1	pł.	*°6^15...8^30 ∇°11^50...18^20; =20^10-24
19	7	0.0	1	∇°16^35-17^15 *°23^15...24
20	7	0.0	pł.	*°0^00...1^20, 12^25-13^05; =5^30-11^20
21	7	.	.	⌣°1^00-9^00
22	7	0.0	.	∇°17^05-18^02; =7^50-11^10; ⌣'1^00-8^00
23	5	0.0	.	*°6^30...14^40, 19^45-23^40; =5^20-24; ⌣1^00-6^30
24	8	.	.	=0^00-9^40; ⌣°20^30-24
25	6	0.1	.	*°7^05...11^15; =7^20-24; ⌣°0^00-7^05, 22^00-24
26	7	.	.	=0^00-9^10; ⌣°0^00-7^00
27	7	0.0	.	=5^20-10^00, 20^30-24; ⌣°1^00-9^00, 20^00-24
28	7	5.5	.	*°5^10-30, 7^45-8^30 ∇°...12^12 ∇°13^05...14^35 ∇°16^35-17^22 ∇°22^35-24; =na, p-24; ⌣°na
29	7	1.7	.	∇°0^00...20 •°...2^45 *°15^50-16^10 •°23^10-24; =2^45-9^10
30	8	0.0	.	•°0^00...1^20 13^10-45 21^40...24
31	7	13.6	.	•°0^00...2^45, 4^50-6^35, 7^40-10^10, 11^15...13^15, 15^50...17^00 •'...20^30 *'-21^20; =np
Σ	—	44.2	—	UWAGI.

Kwiecień - Avril

1	8	1.0	.	•°4^40...5^15 ∇°9^40-10^15 ∇°10^20-11^02 ∇'13^04-36 ∇°14^50...15^29 ∇°-16^10; ⌣20-24
2	8	1.5	.	∇'12^50-13^05 ∇°13^12-35 ∇°14^40-15^07, 15^30-16^35 ⌣°1^00-7^00
3	8	.	.	•°0^10...3^45; »18^30-20^30, 21^20-23^40
4	8	0.0	.	•°15^40...17^07, 18^10...22^08
5	8	.	.	=6^10-7^10; ⌓° 3-7
6	8	3.5	.	∇°17^25...18^25 •°18^35...24; ⌣'1-7
7	7	0.1	.	•°-1 0^00...1^40 •'4^02...30 *°...5^10 *°6^45...7^50 ∇°9^24-10^20 •°21^14...24
8	8	0.0	.	•°0^00...5^7 •°3^10...5^50 •°21^25-40, 22^45-23^10
9	8	1.1	.	•°3^15...35 ∇°15^10-20, 17^30-40 ∇'18^30-19^10; =19^30-24
10	7	.	.	=0^00-4^35 ≡²-6^20 =-10^35, 19^40-24; ∨°4^30-6^20 ⌣'np
11	7	0.1	.	•°16^45...19^50; =1^00-7^10, 19^00-24; ⌣'na-a
12	7	1.4	.	=1^00-7^30, 18^35-24; ⊟ 21^40-22^20
13	5	12.2	.	•°5^00...8^15-11^10 •'-13^30 •°-15^15...18^30; =0^00-24; ⊟ 0^00-25
14	7	0.9	.	∇°2^40-5^45 •°-6^40 ∇°9^50-10^05 •°15^25...16^20, 18^45...19^15 •°21^40...23^10-24; =0^00-10^30, 18^20-24
15	4	2.5	.	•°0^00-5^45 6^15-9^05 •°-9^45 •°-24; =0^00-24
16	6	2.5	.	•°0^00-4^04 •°...4^20, 6^40...7^20 •°...8^10 ∇°-1 14^43-15^43, 16^20-30; =0^00...23^40 ≡°-24; ⌣°np
17	8	.	.	»10^40-14^30, 19^20-22^15; ≡°-1 0^00-1^45 =-3^10
18	8	.	.	»6^35-7^05
19	8	.	.	=22^40-24
20	7	.	.	=4^00-10^20; ⌓°0^00-9^50
21	7	.	.	=18^15-24; ⌓'np
22	8	.	.	=0^00-2^20 5^20-6^20; ⌓°-2 0^00-10^00 ⌓° 22-24
23	8	.	.	⌓°-1 0^00-9 ⌓° 18-24
24	8	.	.	⌓' 0-8
25	8	.	.	⌓' 1-9
26	6	0.4	.	∇°12^35-30, 19^40-21^15; (R)° S 15^40-16^45 R 19^50-20^45; =3^20-9^15 ∞-19^40 =-24; ⌓'-0 3-9
27	6	1.9	.	∇°6^15-30 11^18-13^10 •' 13^25 ∇°17^50-18^05; =0^00-11^10
28	5	16.2	.	•°5^05...9^10-11^20 ∇'12^15-18 ∇°∇°12^18...24; R 13^01-35; =13^50-18^10
29	8	11.3	.	∇°0^00-15 ∇°-1^20 ∇'-1^40 ∇°...3^20 ∇°-4^15 ∇°5^40 ∇°10^50-11^10 ∇°...15^35 ∇'14^00-05 ∇'-14^10 ∇°...15^35 ∇'16^15-17^05; =18^35-19^15
30	5	1.6	5	∇°0^20...2^10 ∇'-0 3^20...7^30 ⌅ •°9^50-10^10 ∇°12^15-30 ⌅ •°-13^15 ∇°14^15...16^10 ⌅°19^35-40; =a-p
31				
Σ	—	57.6	—	UWAGI.

DNI	CIŚNIENIE P-900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	73.7	71.3	68.9	71.3	-0.9	2.9	0.9	1.0	5.5	-4.0	93	66	92	84	0.4	2.6	0.5	1.2	8	9	8	C 0	W 7	C 0
2	64.2	66.7	69.3	66.7	0.5	3.3	1.9	1.9	6.4	-0.9	96	78	89	88	0.2	1.7	0.8	0.9	10 *	9	6	C 0	NW 5	C 0
3	69.9	69.1	67.9	69.0	3.0	8.4	6.5	6.1	9.6	-1.0	86	61	85	77	1.1	4.3	1.5	2.3	8 ⊙	9	10 ●	C 0	W 5	WSW 1
4	66.6	67.4	69.1	67.7	4.3	7.0	2.9	4.3	9.6	1.9	84	61	79	75	1.4	3.8	1.6	2.3	10	10	5	W 2	W 6	SSW 1
5	70.4	72.2	75.4	72.7	3.1	6.5	4.3	4.6	8.3	-0.7	86	81	97	88	1.0	1.9	0.3	1.1	9	10 ●	0	C 0	SE 2	C 0
6	77.8	75.9	75.0	76.2	0.8	15.6	11.0	9.6	17.6	-1.0	96	46	79	74	0.3	9.5	2.7	4.2	10 ≡	4 ⊙	8	C 0	NE 3	C 0
7	75.3	76.0	75.7	75.7	10.2	17.3	13.6	13.7	18.9	9.4	99	70	91	87	0.1	5.8	1.5	2.5	10 ●	9	8	C 0	W 6	SSE 2
8	74.6	73.1	72.8	73.5	12.4	21.4	13.8	15.4	22.2	7.8	96	54	92	81	0.5	11.8	1.3	4.3	7 ⊙	9	10	SE 2	WSW 5	C 0
9	74.9	72.4	69.6	72.3	12.9	18.4	13.5	14.6	18.7	11.5	88	53	80	74	1.8	10.0	3.2	5.0	4	9	9	C 0	S 1	C 0
10	70.4	71.4	72.4	71.4	11.6	14.6	6.9	10.0	15.6	5.0	83	59	97	80	2.3	6.8	0.3	3.1	9	8	2	WNW 5	SSW 7	C 0
11	72.5	71.4	72.0	72.0	7.9	12.6	7.1	8.7	14.6	4.4	90	54	88	77	1.0	6.8	1.2	3.0	3 ⊙	8	8	SE 1	NW 2	C 0
12	73.8	73.4	74.7	74.0	7.2	12.8	8.4	9.2	14.9	0.9	88	74	96	86	1.2	3.9	0.4	1.8	9 ⊙	9 ●	10 ●	SE 1	NE 3	C 0
13	74.6	73.5	73.1	74.4	8.4	10.9	9.9	9.8	13.4	7.6	96	83	91	90	0.4	2.2	1.1	1.2	10	10	10 ●	C 0	WSW 2	C 0
14	67.1	65.4	68.5	67.0	7.1	6.2	7.1	6.9	10.0	3.2	94	94	87	92	0.6	0.6	1.3	0.8	10 ●	10 ●	10	NW 3	NW 6	WSW 6
15	68.9	70.0	72.3	70.4	6.0	7.4	7.4	7.1	10.4	4.4	85	80	77	81	1.4	2.1	2.3	1.9	10 ●	10	10	W 9	W 9	W 6
16	74.4	76.7	75.7	75.6	6.3	7.4	4.9	6.0	9.9	4.7	92	65	86	81	0.7	3.7	1.3	1.9	9 ●	9	9	W 6	W 6	C 0
17	73.3	71.8	72.8	72.6	8.7	12.9	10.5	10.6	14.5	4.8	76	65	74	72	2.7	5.3	3.3	3.8	10	10	9	S 2	S 3	NW 3
18	74.6	76.9	78.3	76.6	7.6	14.0	8.4	9.6	16.0	5.1	90	55	93	79	1.0	7.2	0.7	3.0	9	7 ●	1	C 0	WNW 8	C 0
19	73.2	69.3	68.2	70.2	8.1	20.9	14.1	14.3	21.6	0.9	89	45	80	71	1.2	13.5	3.2	6.0	7 ●	4 ●	10	C 0	SE 6	W 3
20	71.5	72.7	74.8	73.0	8.4	12.3	8.2	9.3	14.3	6.7	93	61	83	79	0.7	5.6	1.8	2.7	10 ●	8 ⊙	10	C 0	WNW 4	C 0
21	76.7	75.3	73.5	75.2	6.4	13.4	8.1	9.0	14.5	3.1	94	47	81	74	0.6	8.2	2.1	3.6	10	8 ⊙	0	C 0	WSW 6	C 0
22	70.6	72.6	76.7	73.3	9.2	13.0	10.4	10.8	15.8	3.6	80	67	88	78	2.3	4.9	1.4	2.9	9	7 ⊙	9	C 0	WSW 5	C 0
23	77.2	76.1	75.7	76.3	11.2	16.1	13.2	13.4	17.8	5.6	84	53	75	71	2.1	8.6	3.8	4.8	7 ⊙	7	8	C 0	SSW 3	C 0
24	79.2	77.9	75.9	77.7	9.2	11.8	8.2	9.4	13.3	5.7	71	59	86	72	3.3	5.6	1.3	3.5	10	10	10	W 3	NW 2	C 0
25	74.4	74.2	74.1	74.2	8.2	9.9	8.2	8.6	11.8	6.0	89	81	97	89	1.2	2.4	0.3	1.3	10	10 ●	10 ●	C 0	E 3	C 0
26	71.3	70.0	71.7	71.0	7.5	8.2	8.0	7.9	9.4	5.8	91	97	94	94	0.9	0.3	0.6	0.6	10 ●	10 ●	10 ●	ESE 2	SE 1	WNW 3
27	74.7	75.9	76.4	75.7	8.3	10.8	10.1	9.8	13.5	6.3	87	75	87	83	1.4	3.3	1.6	2.1	10	10	10	C 0	WNW 2	SE 1
28	75.2	73.4	74.8	74.5	11.0	16.0	11.2	12.4	17.7	4.8	86	72	86	81	1.8	5.1	1.8	2.9	2 ⊙	7 ⊙	6	C 0	ESE 6	NW 2
29	76.2	76.2	77.6	76.7	10.8	15.6	9.9	11.6	16.0	4.6	69	52	91	71	4.0	8.4	1.1	4.5	4	8	10 ●	WSW 3	NW 4	SSE 3
30	78.7	78.3	78.2	78.4	10.1	15.6	9.6	11.2	16.2	6.1	77	47	84	69	2.9	9.4	1.9	4.7	9	5	4	C 0	NW 5	C 0
31	74.8	71.9	72.7	73.1	12.4	17.8	10.9	13.0	19.1	5.9	69	40	70	60	4.5	12.2	5.8	6.8	7 ⊙	8	8	NE 1	SW 3	WSW 3
M	73.2	72.9	73.3	73.1	7.7	12.3	8.7	9.4	14.1	4.1	87	64	86	79	1.5	5.7	1.6	2.9	8.4	8.4	7.7	1.3	4.5	1.1

1	77.0	77.0	75.6	76.5	5.3	8.6	6.6	6.8	11.5	4.5	69	58	88	72	2.8	4.8	1.1	2.9	9	10	10	W 3	WSW 1	S 1
2	77.1	79.7	82.5	79.8	5.4	9.5	5.5	6.5	11.4	4.6	87	48	91	75	1.2	6.2	0.8	2.7	10 ●	8	9 ●	WNW 3	WNW 5	NNE 2
3	84.3	84.7	86.2	85.1	5.3	9.4	6.1	6.7	11.1	3.5	89	58	79	79	1.0	5.0	2.0	2.7	9	8 ⊙	9	WNW 4	WNW 2	WNW 2
4	86.7	86.4	86.9	86.7	3.8	8.7	7.0	6.6	11.6	3.3	93	65	90	83	0.5	3.9	1.0	1.8	10 ●	9	10 ●	WSW 3	WNW 3	WSW 1
5	87.3	85.4	86.5	86.4	5.3	13.3	9.7	9.5	15.1	2.5	77	48	54	60	2.1	8.0	5.5	5.2	10	8	7	WNW 3	NW 8	NW 5
6	88.9	88.3	88.3	88.5	3.5	12.0	9.6	8.7	13.9	1.2	78	55	48	54	1.7	9.1	6.2	5.7	7 ⊙	7 ⊙	1	WNW 3	NW 4	NNW 3
7	89.3	89.1	88.6	89.0	4.4	9.7	6.4	6.7	11.6	2.5	84	53	81	73	1.4	5.6	1.9	3.0	9	10	8	WNW 4	N 4	C 0
8	89.2	87.9	85.3	87.5	6.5	16.7	9.5	10.6	18.6	-0.9	82	43	79	68	1.7	10.9	2.5	5.0	2 ⊙	2 ⊙	0	C 0	NW 4	C 0
9	81.4	78.6	75.4	78.5	9.3	20.2	14.6	14.7	21.3	1.4	81	30	74	62	2.2	16.5	4.3	7.7	0 ⊙	1 ⊙	7	C 0	WNW 4	C 0
10	74.0	72.6	71.5	72.7	12.7	19.7	14.3	15.4	21.1	6.9	86	45	80	70	2.1	12.5	3.2	5.9	1 ⊙	4 ⊙	9	C 0	NW 3	SSE 1
11	70.9	70.2	71.7	70.9	13.5	13.5	10.2	11.8	17.3	10.0	77	73	91	80	3.5	4.2	1.1	2.9	7 ⊙	10	10	NW 4	NW 6	WSW 4
12	74.4	75.1	76.4	75.3	8.4	11.2	8.6	9.2	13.0	7.9	74	56	78	69	2.8	5.9	2.4	3.7	10	9	8	W 6	WNW 5	NW 1
13	78.2	76.8	75.4	76.8	8.9	16.8	11.1	12.0	18.7	1.6	85	42	67	65	1.7	11.1	4.3	5.7	1	5	6	C 0	E 4	SE 2
14	74.4	74.2	75.9	74.8	15.2	23.6	16.9	18.2	24.7	7.3	60	40	79	60	7.0	17.4	4.0	9.3	2 ⊙	6 ⊙	1	C 0	W 3	C 0
15	79.9	80.2	79.9	80.0	14.8	27.3	19.7	20.4	28.4	7.9	82	39	78	66	3.1	22.0	5.1	10.1	7	4 ⊙	8	SE 1	C 0	SSE 1
16	78.8	77.5	79.9	78.7	18.5	27.2	17.6	20.2	28.8	11.2	82	49	97	76	3.9	18.5	0.6	7.7	1	7	9	C 0	S 4	C 0
17	82.6	82.2	81.3	82.0	16.7	20.8	17.3	18.0	21.6	16.4	91	67	84	81	1.8	8.2	3.1	4.4	9	8	10	NNE 2	ESE 2	C 0
18	80.4	78.9	77.3	78.9	17.1	22.9	18.7	19.4	23.2	13.3	82	63	81	75	3.3	10.3	4.2	6.0	0	7 ⊙	9	SSE 2	SSE 3	E 1
19	76.0	73.8	73.5	74.4	17.0	22.8	19.4	19.6	26.1	13.5	95	71	68	78	1.0	8.1	7.2	5.4	10 ●	9	9	C 0	S 1	SW 6
20	78.2	78.6	79.2	78.7	14.3	19.1	13.2	15.0	20.4	11.2	82	61	86	76	2.9	8.7	2.1	4.6	7	9	6	S 2	WNW 2	C 0
21	80.7	80.9	82.6	81.4	14.4	20.9	15.1	16.4	22.0	9.7	86	57	88	77	2.4	10.6	2.1	5.0	2 ⊙	9	0	C 0	SSW 3	C 0
22	84.1	83.1	81.8	83.0	14.0	23.6	17.8	18.3	26.0	8.2	95	53	85	77	1.1	13.8	3.0	6.0	2 ⊙	6 ⊙	1	C 0	S 2	C 0
23	81.3	80.2	79.9	80.5	18.6	27.4	20.0	21.5	29.7	10.7	79	43	79	67	4.3	20.8	5.0	10.1	1 ⊙	4 ⊙	8	SE 1	NW 3	C 0
24	79.7	76.8	75.9	77.5	17.4	26.5	20.9	21.4	28.8	14.2	83	40	68	64	3.0	20.9	7.8	10.6	0	4	1	C 0	WSW 8	W 1
25	78.6	80.3	81.0	80.0	16.0	18.4	11.4	14.3	21.6	11.3	66	44	67	59	6.1	11.9	4.4	7.3	7	5 ⊙	1	WSW 5	W 7	C 0
26	78.6	75.5	71.1	75.1	10.2	17.5	12.6	13.2	19.9	3.1	78	43	80	67	2.7	11.4	2.9	5.7	3 ⊙	8 ⊙	6	C 0	SW 3	C 0
27	73.1	74.4	75.2	74.2	9.7	13.3	9.7	10.2	14.1	5.7	74	57	62	64	3.1	5.8	4.6	4.5	6 ⊙	8 ⊙	0	SW 5	W 6	W 2
28	74.0	72.3	70.7	72.3	9.4	10.8	9.1	9.6	11.8	5.4	58	60	74	64	3.0	3.3	3.1	4.3	8	9	10	WNW 6	W 8	WSW 6
29	73.2	75.8	75.4	74.8	7.5	10.8	9.8	9.5	12.6	7.0	89	72	70	77	1.2	3.7	3.6	2.8	10	8	10	W 7	SW 5	WSW 3
30	75.2	76.3	77.9	76.3	8.5	11.5	10.2	10.1	12.8	8.3	78	68	80	75	2.4	4.4	2.3	3.1	8	10 ●	10	W 6	NW 4	W 2
31																								
M	79.6	79.1	79.0	79.2	11.1	17.1	12.6	13.4	19.0	7.1	81	53	78	71	2.6	10.2	3.4	5.4	5.6	7.1	6.4	2.3	3.9	1.3

Jelenia Góra H_s=342m H_b=343,9m h_w=16m Maj - Mai 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	2.5	•	⚥°9^45...13^25 ⚥°15^02-06 ⚥°...15^50,16^05-38,18^20-19^10,=3^30-5^15
2	7	2.7	3	⚥°2^45-5^05 ⚥°5^10 ⚹'7^35 ⚥9^45-10^10 ⚥°10^20...12^25,16^07-15,=a;△'nn
3	7	0.6	•	⚥°10^06...11^35,18^25-20^30 •°...23^15-24,=0^05-5^15,△^{1-0}0-10
4	8	0.0	•	•°0^00-4^15 ⚥°14^05-12,=4^15-8^20
5	6	1.6	•	⚥°8^46-9^03 •°11^40-15^02 ⚥°16^50-58,=1^00-4^20,19^25-21^40≡^{1-2}-24;⌣na△²20-24
6	7	5.7	•	•°23^15-24;≡^{2-1}0^00-7^20 ⚥°-7^30=-8^15,20^25-22^30,△²0-9△°20-23^15
7	7	1.5	•	•^{0-1}0^00-7^35 •°13^40...15^40,=2^20-11^20
8	7	12.4	•	⚥'3^05-10 •^{0-1}7^45...8^40 ⚥°13^20-25 ⚥^{0-2}15^35-17^25,🌧°15^50-17^15 W-E;△'na
9	8	4.4	•	⚥°13^45-14^35,16^10-12 •°17^50...18^10,21^05...24,=4^15-7^30,nn;△'20^30-21^15⊕11^20-12^30
10	8	5.1	•	•^{1-0}0^00...5^30 ⚥^{0-1}14^25-52 ⚥°15^35-16^45,🌧°14^52-15^35 SW-NE,=na,nn
11	8	5.8	•	⚥°7^50...13^20▲⚥'8^20-30,=na;△'0^00-7^50,nn
12	8	7.6	•	⚥°12^20...14^06 •°15^07-16^20 ⚥°16^32-50 ⚥^{0-1}17^40-19^30 •°-24;=na;△'0^00-9^00
13	7	7.0	•	•°0^00-3^30...5^46,10^45...11^05,19^40...24,=5^45-11^40,19^20-24
14	4	28.8	•	•^{0-1}0^00...6^00-18^25,=0^00-24
15	6	3.1	•	•°3^45-5^35,5^45...8^15-11^20,=0^00-3^20,11^20-15^30
16	7	0.2	•	•°2^40...3^15,5^45-6^20 ⚥°6^25-7^10,=3^15-8^20,19^30-24,△°nn
17	8	0.3	•	•°3^30...5^20,7^15...8^40 ⚥°15^05-10 ⚥'-15^17 •°16^10...45,=na;△°na
18	8	0.8	•	•°5^50...6^05 ⚥°9^40...55,10^05-43,16^20-40,=20^10-24
19	8	•	•	⚥°22^40-23^15 ⚥'23^35-24,=0^00-4^20;△°na⌣°na
20	8	0.0	•	⚥^{0-1}0^00-2^35 •°3^10...5^40,6^35-8^07,△°nn
21	7	•	•	•°0^55...1^45,=2^30-10^15,20^36...24,△°na△^{1-2}nn
22	8	0.7	•	•°7^45...9^40,12^25-38,=0^00-1^40,2^30-5^20,△²0^00-7^45
23	8	0.3	•	⚥°16^10...17^10,22^40-23^20 •°...24;△'na△°6^00-9^00
24	7	0.2	•	•°0^00...2^40,18^20...19^17,23^45-24,=5^30-9^40
25	7	3.8	•	•°0^00...2^15 ⚥°9^50...13^25 •°19^20...24,=4^30-9^20
26	5	5.6	•	•°0^00...3^05-7^20...9^15-14^20...17^35,20^45...23^15,=0^00-24
27	7	•	•	•°4^15...35,=0^00-9^30
28	6	0.0	•	⚥°17^55-18^02,=4^20-11^45,13^30-24;△^{0-2}0^00-9
29	8	1.6	•	⚥^{0-1}15^50...19^05 •°20^10...24;🌧17^45-18^40 NW-SE;=na,19^40-24
30	7	0.0	•	•°0^00...1^45 ⚥°16^50-17^20,=0^00-4^10,21^30-24;△'nn
31	8	•	•	=0^00-6^10,△^{0-1}0^00-9
Σ	—	102.3	—	UWAGI:

Czerwiec - Juin

1	8	6.7	•	
2	8	3.4	•	•^{0-1}0^00...4^25-8^05...10^10 ⚥°17^20...22^10 ⚥'21^20-32▲°21^02-07,21^15-20,=0^20-11^10
3	8	5.6	•	⚥°9^46...14^28,18^05...19^35,=0^30-9^20
4	7	2.2	•	⚥°1^00-35 •°6^20...8^20 ⚥°10^30...15^11,19^48-20^35 •°21^40...24
5	8	•	•	•°0^00...1^20
6	8	•	•	△°2^00-9^00
7	8	•	•	△°1-10,nn
8	9	•	•	=0^00-4^35;△'na⌣'na
9	8	•	•	=3^20-6^30,21^20-24,△^{1-0}3^00-9
10	8	•	•	=0^00-6^20,7^20-8^10,△^{0-1}0^00-9
11	6	0.4	•	⚥°18^15-30,19^40-45,21^10-35,=a,a-n,nn
12	8	•	•	•°0^40...2^50,7^10-35,=0^50-4^40,△°nn
13	7	•	•	=0^00-4^15,5^20-7^30,△^{0-2}0^00-11△°nn
14	8	•	•	=20^30-24;△°0^00-8,nn
15	7	•	•	=0^00-8^30,△^{0-2}0^00-10
16	7	14.9	•	⚥^{0-1}15^55-18^05 ⚥°20^17-20,🌧°15^55-17^30 NW-SE,🌧20^17-21^20,=na;△°0^00-9
17	7	•	•	⚥°0^05-2^50,=0^00-12^45
18	7	1.6	•	△^{0-1}2-10
19	7	7.2	•	⚥^{1-0}6^42-8^35 •°...11^35 •🌧°22^01-24 W-E
20	8	•	•	•🌧°0^00-1^35 W-E ⚥°-1^40,=nn△°nn
21	8	0.0	•	⚥°16^40-45,=0^00-6^30,nn;△^{0-1}0^00-9△°nn
22	8	•	•	=nn;△'0^00-10^00△^{0-2}21^30-24
23	8	•	•	=0^00-4^10,nn;△²0^00-9
24	7	•	•	=0^00-3^15,23^20-24,△°0^00-9
25	7	•	•	=0^00-3^40,△°0^00-9
26	8	1.7	•	⚥°23^50-24,△^{0-1}0^00-8^00△°nn
27	8	0.1	•	⚥^{0-1}0^00-15,12^{-30},2^{15-40} ⚥°18^{15-40};(🌧)°0^50-1^10 N
28	8	1.8	•	⚥°11^40...20^35
29	7	1.2	•	⚥°2^00...10^07,=10^20-12^45
30	8	0.0	•	•°13^45...59,=21^30-24
31				
Σ	—	46.8	—	UWAGI:

Jelenia Góra φ = 50°54' λ = 15°48' Lipiec-Juillet 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N.w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D.v I	II	III
1	77.9	77.6	77.3	77.6	9.1	12.2	9.5	10.1	12.6	8.4	83	60	76	73	2.0	5.7	2.8	3.5	10	10	10	W 2	WSW 2	C 0
2	76.1	74.9	71.6	74.2	9.2	12.6	10.6	10.8	13.6	7.2	95	66	92	84	0.6	5.0	1.0	2.2	9 ●	9	10 ●	NW 4	W 6	WSW 2
3	66.5	64.1	62.7	64.4	9.9	11.1	8.1	9.3	14.0	7.6	81	68	85	77	2.4	4.2	1.8	2.8	9	9 ●	10 ●	W 8	W 6	W 6
4	60.7	61.8	65.7	62.1	8.4	10.1	9.8	9.5	11.7	2.2	68	66	70	68	3.6	4.3	3.6	3.8	9	9	10 ●	WSW 7	WSW 8	WSW 4
5	65.6	67.0	70.9	67.8	10.6	12.5	10.0	10.8	14.7	7.8	69	65	86	73	4.0	5.0	1.8	3.6	9	9	10	WSW 3	WNW 4	C 0
6	75.5	74.3	76.1	74.6	10.0	13.9	8.4	10.2	17.0	4.4	87	66	97	83	1.6	5.4	0.3	2.4	2 ⊙	9 ⊙	10 ≡	SW 1	NW 4	C 0
7	76.4	76.8	78.3	77.2	9.8	10.8	10.0	10.2	14.6	6.2	97	86	83	89	0.3	1.8	2.1	1.4	9	10 ●	3	C 0	WNW 3	NNW 2
8	80.1	80.7	81.5	80.8	10.0	14.0	11.1	11.6	14.7	8.1	96	68	78	81	0.5	5.1	2.9	2.8	7	7 ⊙	9	W 4	NW 3	NW 2
9	81.9	79.9	78.3	82.0	7.7	17.6	12.4	12.5	18.9	2.4	97	64	89	83	0.3	7.2	1.6	3.0	0	9	0	C 0	NNE 2	C 0
10	77.2	76.0	74.9	76.0	10.0	21.4	14.8	15.2	22.6	4.9	95	46	79	73	0.7	13.7	3.4	5.9	0 ⊙	7 ⊙	2	C 0	NW 3	C 0
11	72.6	70.8	70.5	71.3	10.9	24.2	16.2	16.9	24.8	5.2	92	53	86	77	1.0	14.1	2.5	5.9	8 ⊙	9	3	C 0	WNW 7	C 0
12	70.8	69.9	69.5	70.1	15.7	16.3	12.1	14.0	22.5	7.7	82	67	94	81	3.2	6.1	0.8	3.4	7 ⊙	9 ●	8	C 0	NW 7	S 2
13	68.8	69.7	71.1	69.9	13.1	14.6	12.7	13.3	16.4	8.3	79	79	87	82	3.1	3.4	1.9	2.8	9	9	9	WSW 2	WNW 4	W 1
14	69.4	69.1	69.4	69.3	11.6	16.2	11.0	12.4	17.6	10.4	98	68	95	87	0.3	6.0	0.6	2.3	10 ●	9	6	W 1	W 6	C 0
15	66.6	65.4	66.7	66.2	9.9	16.3	12.5	12.8	18.9	6.0	100	85	98	94	0.0	2.7	0.4	1.0	9	10	9	SE 1	WNW 1	C 0
16	67.4	67.9	70.0	68.4	12.4	18.7	13.3	14.4	18.9	10.0	99	71	100	90	0.2	6.3	0.0	2.2	10 ●	9	10 ●	C 0	C 0	C 0
17	72.7	74.3	75.9	74.3	13.6	13.8	13.8	13.8	18.7	12.8	100	97	94	97	0.0	0.6	0.9	0.5	10 ●	9	9	WNW 3	ESE 2	SSE 1
18	76.4	76.3	77.7	76.8	13.2	18.1	14.4	15.0	18.7	10.5	99	59	85	81	0.2	8.4	2.5	3.7	9	9	9	C 0	E 2	NW 4
19	78.5	78.4	78.6	78.5	13.4	20.7	14.7	15.9	21.4	10.9	94	58	89	80	0.9	10.4	1.8	4.4	10	7 ⊙	6	WNW 2	NW 5	SE 3
20	78.6	78.0	78.1	78.2	12.7	22.4	15.0	16.3	23.6	9.3	96	45	94	78	0.5	15.0	0.9	5.5	4	8	6	C 0	WNW 3	C 0
21	75.9	75.3	75.0	74.7	14.9	25.9	21.1	20.8	28.0	8.7	94	50	69	71	0.9	16.7	7.7	8.4	1 ⊙	9	9 R	C 0	SW 1	SW 6
22	78.1	75.9	78.4	77.5	17.8	24.5	17.7	19.4	24.8	16.2	96	63	82	80	0.8	11.4	3.6	5.3	4 ⊙	7 ⊙	6	C 0	NNW 2	WNW 2
23	81.3	81.7	83.3	82.1	13.7	19.8	12.1	14.4	21.1	10.3	97	53	89	80	0.6	10.8	1.5	4.3	5 ⊙	9	1	C 0	NW 4	C 0
24	85.7	85.2	84.7	85.2	11.8	18.9	11.4	13.4	20.6	6.7	94	55	91	80	0.8	9.7	1.2	3.9	3 ⊙	6 ⊙	0	C 0	WNW 4	C 0
25	84.1	81.0	78.5	81.2	9.7	23.7	17.0	16.8	25.5	5.2	97	45	80	74	0.3	16.1	3.9	6.8	6 ⊙	3 ⊙	1	C 0	S 2	C 0
26	77.2	75.5	76.7	76.5	19.3	30.7	22.8	23.9	31.4	11.6	82	38	70	63	4.0	27.4	8.3	13.2	0 ⊙	2	9 R	C 0	WSW 5	SW 3
27	76.9	77.5	79.2	77.9	19.6	22.4	16.8	18.9	24.0	14.3	84	70	71	75	3.6	8.1	5.5	5.7	8 ⊙	4 ⊙	8	NNE 1	WNW 5	WNW 3
28	81.2	81.0	80.8	81.0	13.1	16.7	10.1	12.5	19.1	10.0	87	60	91	79	1.9	7.7	1.2	3.6	9	5 ⊙	4	WNW 3	NW 4	SSE 2
29	81.5	80.5	80.4	80.8	9.5	17.6	11.2	12.4	19.8	4.9	95	55	89	80	0.7	9.0	1.5	3.7	5	9	4	C 0	NNE 2	C 0
30	81.1	80.2	80.0	80.4	8.5	18.7	11.3	12.4	21.4	4.5	99	46	83	76	0.2	11.7	2.3	4.7	3	7	2	C 0	E 2	C 0
31	81.1	80.4	80.1	80.5	10.7	22.4	14.6	15.6	23.1	5.6	86	41	88	72	1.8	15.9	2.0	6.6	8	7 ⊙	9	C 0	WSW 4	C 0
M	75.5	75.0	75.5	75.3	11.9	18.0	13.1	14.0	19.8	8.0	91	62	86	80	1.3	8.9	2.3	4.2	6.6	7.9	6.5	1.4	3.6	1.4

Sierpień-Août

1	79.8	79.1	79.4	79.4	14.8	20.8	13.6	15.7	22.0	12.2	91	50	89	77	1.5	12.4	1.8	5.2	8	8 ⊙	7	SE 1	WNW 7	SE 1
2	78.5	76.3	74.6	76.5	11.2	22.4	16.7	16.8	25.1	7.5	97	51	81	76	0.3	13.2	3.7	5.7	6	2 ⊙	8	C 0	C 0	C 0
3	74.1	74.8	75.3	74.7	14.0	23.7	15.8	17.3	24.2	11.5	95	51	100	82	0.7	14.5	0.0	5.1	9	2	10 ≡	C 0	NE 4	C 0
4	75.4	74.8	76.7	75.6	14.0	25.8	17.2	18.6	26.7	11.3	99	52	86	79	0.2	16.0	2.8	6.3	8	4	0	C 0	W 4	C 0
5	74.1	75.4	72.4	73.3	15.4	17.7	17.0	16.8	23.2	10.6	96	94	82	91	0.8	1.2	3.6	1.9	6 ⊙	10 ●	10 ● R	C 0	SSE 5	WNW 5
6	72.3	72.5	71.2	72.0	14.1	19.5	16.9	16.8	22.9	11.7	100	80	95	92	0.0	4.5	1.0	1.8	10	10	4	C 0	NW 1	SE 1
7	65.2	63.8	70.6	66.5	16.3	19.9	14.4	16.2	23.3	11.0	100	89	65	85	0.0	2.6	5.8	2.8	9	10	7	C 0	WNW 4	WNW 2
8	74.6	76.8	79.6	77.0	14.8	19.0	11.0	14.0	19.9	10.5	62	46	91	66	6.4	12.0	1.1	6.5	3	4	3	SW 6	W 6	C 0
9	84.0	83.7	83.9	83.9	8.8	17.6	11.0	12.1	19.9	4.2	97	57	94	83	0.3	8.6	0.8	3.2	1 ⊙	7 ⊙	0	C 0	WNW 4	C 0
10	81.9	79.6	77.5	79.6	9.8	20.2	12.6	13.8	21.9	4.3	96	48	87	77	0.5	12.3	1.9	4.9	2 ⊙	9	4	C 0	SW 4	SE 1
11	77.7	77.5	77.5	77.6	13.2	20.6	13.8	15.4	22.5	8.5	88	54	92	78	1.8	11.0	1.3	4.7	9	8	3	C 0	W 4	C 0
12	77.2	77.6	77.5	77.6	13.1	26.7	16.3	18.3	28.8	8.4	92	45	94	77	1.3	19.4	1.1	7.3	0	3	0	C 0	WSW 2	SE 1
13	78.7	78.4	78.1	78.4	15.3	29.4	18.0	20.2	30.1	10.3	89	39	87	72	1.9	24.9	2.6	9.8	2 ⊙	5 ⊙	1	C 0	W 3	SE 1
14	77.0	78.9	77.8	77.9	17.0	20.2	16.4	17.5	23.0	15.0	94	84	95	91	1.2	3.8	0.9	2.0	9	9 ●	10	C 0	E 2	NE 3
15	71.6	71.0	70.6	71.1	16.3	26.0	15.7	18.4	27.1	15.3	98	63	99	87	0.4	12.3	0.2	4.4	9 ● R	9 ⊙	10	SE 4	W 1	C 0
16	72.7	72.4	74.2	73.1	17.8	22.4	15.4	17.8	23.4	14.8	77	53	98	76	4.6	12.6	0.4	5.9	4 ⊙	8 ⊙	9	C 0	WSW 2	C 0
17	74.1	74.4	71.4	73.3	13.7	16.2	12.7	13.8	17.9	11.7	100	95	98	98	0.0	1.0	0.4	0.5	9	10 ●	1 ≡	C 0	C 0	SSE 1
18	71.9	75.3	77.1	74.8	12.2	14.3	13.2	13.2	17.1	9.8	94	74	72	80	0.9	4.3	4.3	3.2	9	10	5	W 2	W 6	WSW 3
19	77.0	77.7	78.9	77.9	11.6	12.4	12.5	12.2	13.9	10.2	84	83	88	85	2.1	2.4	1.7	2.1	9	10	10	W 6	W 6	W 6
20	78.6	79.4	78.2	78.7	12.6	15.3	12.8	13.4	16.0	11.9	93	80	94	89	1.1	3.3	0.9	1.8	9	9	10	W 5	WNW 3	C 0
21	75.6	74.0	74.7	74.8	8.9	20.7	15.9	15.4	23.1	4.7	99	47	91	79	0.2	12.8	1.6	4.9	2	5	10 ●	C 0	ESE 2	C 0
22	77.5	77.6	76.9	77.3	13.3	18.2	12.7	14.2	19.6	12.2	96	62	96	85	0.6	7.9	0.3	3.0	10 ●	9	10	W 3	NW 4	C 0
23	78.2	79.1	78.2	78.5	13.0	18.2	11.9	13.8	19.0	10.3	75	53	85	72	3.8	9.3	2.0	5.0	4	7	0	C 0	W 6	C 0
24	72.6	70.9	71.5	71.7	16.1	20.0	16.0	17.0	22.4	9.8	69	67	94	77	5.6	7.8	1.2	4.9	10 ●	7	10 ●	WSW 5	SW 5	SSW 3
25	74.9	75.1	79.1	76.4	10.4	17.4	13.4	13.6	18.3	6.9	100	60	70	77	0.0	7.9	4.7	4.2	7	10	7	C 0	SW 5	SW 4
26	81.3	81.6	78.9	80.6	11.3	17.5	9.6	12.0	19.7	9.4	83	54	92	76	2.3	9.1	1.0	4.1	6	6	0	C 0	W 2	C 0
27	74.4	72.6	77.0	74.7	10.0	22.7	16.4	16.4	24.4	8.0	91	47	63	67	1.1	14.6	6.9	7.5	2 ⊙	8 ⊙	3	NE 1	W 5	W 4
28	80.5	80.3	80.8	80.5	12.4	16.2	10.5	12.4	18.1	10.2	75	57	91	74	3.9	7.9	1.1	4.3	8	8	2	W 4	W 2	C 0
29	78.3	78.3	80.1	78.9	12.4	17.3	12.0	13.4	19.3	7.9	89	73	99	87	1.6	5.2	0.2	2.3	8	10	6	NNE 1	SSW 3	C 0
30	82.7	83.9	81.4	82.7	10.4	13.3	6.8	9.3	14.6	6.5	92	69	97	86	1.0	4.8	0.3	2.0	9	9	0	W 4	WSW 5	S 1
31	76.9	77.1	78.4	77.5	8.7	14.8	9.1	10.4	15.6	3.4	96	63	87	82	0.4	6.2	1.6	2.7	9	7	6	SW 1	SW 9	W 1
M	76.4	76.4	76.8	76.5	13.0	19.6	13.8	15.0	21.4	9.7	90	63	89	81	1.5	9.2	1.9	4.2	6.6	7.5	5.4	1.4	3.7	1.2

Jelenia Góra $H_s = 342m$ $H_t = 343{,}9m$ $h_w = 16m$ Lipiec - Juillet 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	7	0.2	•	$\overset{*}{\triangledown}{}^{\circ}11^{40-50}$, $=na,a$; $\triangle^{\circ}np$
2	8	3.2	•	$\overset{*}{\triangledown}{}^{\circ}7^{15}$-$8^{20}$ $\bullet^{\circ}16^{15...30}$, $20^{15}...21^{10}$-24; $\triangle^{\circ}na$
3	8	2.4	•	$\bullet^{\circ}0^{00}$-$3^{20}...6^{35}$ $\overset{*}{\triangledown}{}^{0-1}12^{37}$ 17^{43}, 21^{42}-23^{38}
4	8	0.7	•	$\overset{*}{\triangledown}{}^{\circ}1^{05-50}$, 13^{15-20}, 17^{35}-18^{00} $\bullet^{\circ}21^{50}...22^{20}$
5	8	•	•	$\bullet^{\circ}1^{00}...2^{15}$
6	8	4.7	•	$\overset{*}{\triangledown}{}^{0-1}13^{40}...18^{20}$, $=20^{30}$-21^{40} $\equiv{}^{1}$-24; $\triangle^{\circ}0$-9
7	6	6.6	•	$\overset{*}{\triangledown}{}^{\circ}12^{25-40}$ $\bullet^{\circ}13^{10}$-$16^{15}...18^{20}$, $\equiv{}^{1}0^{00-45}=-6^{35}$
8	6	•	•	$\bullet^{\circ}5^{40}$-7^{07} $\bullet^{1}...7^{48}$, $=6^{40}$-14^{00}, 16^{30}-24
9	7	•	•	$=0^{00}$-4^{20} $\equiv{}^{2}$-$7^{15}=-11^{10}=22^{40}$-23^{20}, $\triangle^{0-1}0^{00}$-7^{00} $\triangle^{1}np$
10	7	•	•	$=1^{30}$-10^{20}, $\triangle^{1-2}0^{00}$-10
11	7	1.6	•	$\bullet^{\circ}8^{40}$-9^{15} $\bullet$ $\boxtimes^{\circ}17^{20}$-18^{08} NW-SE $\boxtimes 19^{50}$-20^{45}, $=na,a,np$; $\triangle^{1}na$-a $\frown 20^{12-20}$
12	8	6.6	•	$\overset{*}{\triangledown}{}^{0-2}13^{55}$-$15^{00}$ $\overset{*}{\triangledown}{}^{0-1}21^{00-15}$; $\boxtimes^{\circ}14^{35-50}$ SW-E; $=na,a=np$
13	7	3.7	•	$\bullet^{\circ}1^{45}$-3^{15}, 5^{55}-6^{10} $\overset{*}{\triangledown}{}^{\circ}8^{26-43}$ $\overset{*}{\triangledown}{}^{0-1}10^{13}...16^{08}$ $\overset{*}{\triangledown}{}^{\circ}21^{01-12}$, $=0^{00}$-1^{45}
14	7	0.0	•	$\overset{*}{\triangledown}{}^{\circ}2^{10}...5^{10}$ $\bullet^{\circ}...6^{15}$-8^{10} $\overset{*}{\triangledown}{}^{\circ}16^{40-50}$, $=4^{20}$-13^{35}, 16^{15}-23^{04} $\equiv{}^{1}$-24; $\triangle^{1}np$
15	5	10.4	•	$\overset{*}{\triangledown}{}^{\circ}11^{35}$-$12^{30}$ $\overset{*}{\triangledown}{}^{0-1}17^{26}...20^{22}$; $\boxtimes^{\circ}18^{18}$-19^{36} W-E; $=1^{00}$-2^{00} $\equiv{}^{2}$-4^{40} $\equiv{}^{\circ}$-$7^{40}=-14^{40}=21^{35}$-$23^{30}=-24$; $\triangle^{1}0^{00}$-11^{00}
16	7	18.9	•	$\bullet^{0-1}6^{15}...6^{40}$, 11^{45} $\overset{*}{\triangledown}{}^{\circ}15^{20-40}$ $\overset{*}{\triangledown}{}^{0-1}17^{12}$-$19^{20}$ $\bullet^{\circ}$-$21^{50}...23^{20}$, $\boxtimes^{\circ}17^{06}$-19^{20}, $=na$-p,p,np
17	5	4.8	•	$\overset{*}{\triangledown}{}^{2-0}1^{35}$-$2^{30}$ $\bullet^{\circ}7^{15}...12^{20}$ $\bullet^{1}...12^{40}$ $\bullet^{\circ}...13^{50}$; $=0^{00}$-15^{10}, np; $\triangle^{2}np$
18	8	•	•	$=0^{00}$-11^{20}, 22^{30}-24, $\triangle^{2}0^{00}$-10
19	8	•	•	$=na,a$; $\triangle^{0-1}3$-9, 21-24
20	7	•	•	$=0^{00}$-6^{30}, 22^{05}-24, $\triangle^{0-1}0^{00}$-9 $\triangle^{2}np$
21	8	2.8	•	$\overset{*}{\triangledown}{}^{2}1^{28}$-$22^{25}$, 22^{36}-23^{31}; $\boxtimes 21^{00}$-22^{46}, $=na$, 6^{05}-9^{20}, $\triangle^{2}0^{00}$-8
22	8	0.3	•	$\overset{*}{\triangledown}{}^{\circ}2^{20-53}$, 15^{28-35} $\overset{*}{\triangledown}{}^{1}15^{53}$-$16^{05}$; $\boxtimes^{\circ}15^{48}$-16^{25} SW-SE; $=na$-a; $\triangle^{\circ}np$
23	8	•	•	$=na=na=np$; $\triangle^{0-1}0^{00}$-9, $\triangle np$
24	7	•	•	$=0^{00}$-9^{40}; $\triangle^{1-0}0^{00}$-10 $\triangle^{\circ}np$
25	7	•	•	$=2^{00}$-7^{20}, $\triangle^{0-1}0^{00}$-10 $\triangle^{\circ}np$
26	8	1.9	•	$\overset{*}{\triangledown}{}^{\circ}17^{35}$-$18^{40}$, 20^{50}-21^{20}, 21^{50}-22^{20} $\boxtimes 18^{05}$-19^{25}, 21^{11}-22^{35}, $=np$; $\triangle^{\circ}0^{00}$-9
27	7	2.5	•	$\overset{*}{\triangledown}{}^{\circ}9^{13-20}$ $\overset{*}{\triangledown}{}^{1}9^{20-46}$ $\overset{*}{\triangledown}{}^{\circ}17^{05...40}$; $\boxtimes^{\circ}9^{15-35}$ WSW-ESE; $=na,np$
28	8	•	•	$\bullet^{\circ}2^{25-45}$, 4^{35-45}; $=na,a$; $\triangle^{\circ}np$
29	8	•	•	$=na$; $\triangle^{0-1}0^{00}$-10^{00} $\triangle^{\circ}np$
30	9	•	•	$\triangle^{1-0}0^{00}$-10 $\triangle^{\circ}21$-24
31	8	0.0	•	$\overset{*}{\triangledown}{}^{\circ}16^{02-20}$, 23^{10-22}; $=21^{10}$-23^{40}; $\triangle^{0-1}0^{00}$-9
Σ	—	71.3	—	UWAGI:

Sierpień - Août

1	6	•	•	$=4^{40}$-24
2	7	•	•	$=0^{00}$-3^{10} $\equiv{}^{1}$-$5^{30}=-9^{35}$, $\triangle^{\circ}3$-10, np
3	6	2.1	•	$\overset{*}{\triangledown}{}^{1}8^{37}$-$19^{40}$, $(\boxtimes)14^{20}$-16^{27} S; $=3^{30}$-20^{20} $\equiv{}^{2}21^{40}$-24, $\triangle^{\circ}0^{00}$-10
4	7	0.0	•	$\overset{*}{\triangledown}{}^{\circ}11^{55}$-$12^{05}$, $\equiv{}^{2}0^{00}$-5^{35} $\equiv{}^{1}$-6^{30} $\equiv{}^{\circ}$-$7^{15}=-10^{30}$, 20^{40}-24; $\triangle^{\circ}20^{00}$-24
5	6	10.4	•	$\bullet^{0-1}11^{27}$-13^{30} $\overset{*}{\triangledown}{}^{0-1}13^{30}$-$14^{15}$, 21^{13}-22^{40}; $\boxtimes^{\circ}19^{09}$-22^{30} SW-SE; $=na,a=na$-a; $\triangle^{1}0^{00}$-9
6	7	0.1	•	$\bullet^{\circ}8^{20}...9^{15}$ $\overset{*}{\triangledown}{}^{\circ}14^{15-25}$; $=2^{20}$-11^{20} $\equiv{}^{2}23^{40}$-24
7	6	2.2	•	$\overset{*}{\triangledown}{}^{\circ}14^{13-23}$ $\bullet^{\circ}14^{40}$-15^{40} $\overset{*}{\triangledown}{}^{\circ}15^{45}$-$16^{07}$ $\bullet^{\circ}17^{13}$-18^{56}, 19^{05-55}; $\equiv{}^{0-1}0^{00}$-$6^{15}=-7^{20}$, n $\triangle^{2-0}0^{00}$-14
8	8	•	•	$\triangle^{1}0^{00}$-4 $\triangle^{\circ}21$-24
9	8	•	•	$=23^{00}$-24; $\triangle^{0-1}0^{00}$-10, 21-24
10	8	•	•	$=0^{00}$-4^{40} $\equiv{}^{0-1}$-$6^{45}=-9^{20}$, $\triangle^{1-2}0^{00}$-9
11	7	•	•	$\triangle^{1-0}0^{00}$-10 $\triangle^{\circ}21$-24
12	9	•	•	$=2^{00}$-$7^{30}=22^{40}$-24; $\triangle^{0-1}0^{00}$-10
13	8	5.0	•	$=0^{00}$-$6^{20}=-7^{20}$; $\triangle^{0-2}2^{00}$-10 $\triangle^{\circ}21$-24
14	7	13.2	•	$\overset{*}{\triangledown}{}^{0-2}4^{55}$-$7^{05}$ $\overset{*}{\triangledown}{}^{0-1}11^{37}...15^{40}$; $(\boxtimes)\odot^{45}$-$\boxtimes^{0-1}4^{05}$-7^{30} NW-ESE; 11^{37}-12^{40} NW-SE; $=18^{30}$-24; $\triangle^{\circ}na$
15	8	0.3	•	$\overset{*}{\triangledown}{}^{1}5^{02}$-$6^{07}$ $\overset{*}{\triangledown}{}^{\circ}$-$6^{55}$ 7^{10}-8^{20}, 16^{10-25} $\bullet^{\circ}17^{45}...18^{40}$, 19^{10-20}; $\boxtimes^{\circ}5^{10}$-8^{32}
16	8	0.5	•	$\overset{*}{\triangledown}{}^{0-1}15^{40}$-$16^{08}$; $\triangle^{\circ}np$
17	7	7.9	•	$\bullet^{\circ}11^{04}$-16^{10}; $=0^{30}$-9^{40}, 10^{50}-13^{37}; $\triangle^{0-2}0^{00}$-9^{04}
18	8	1.8	•	$\bullet^{\circ}5^{20}$-$6^{10}...6^{30}$ $\overset{*}{\triangledown}{}^{\circ}6^{50}$-$7^{35}$, 23^{40}-24; $\gg 11^{45}$-12^{15}.
19	7	0.4	•	$\overset{*}{\triangledown}{}^{\circ}0^{00}$-$2^{20}$, 12^{20}-13^{15}, 14^{40}-15^{10} $\bullet^{\circ}15^{25}...17^{40}$, 18^{48}-19^{05}; $=20^{30}$-24
20	6	•	•	$\bullet^{\circ}3^{05...40}$; $=0^{00}$-19^{30}, 20^{30}-24
21	7	3.0	•	$\bullet^{\circ}21^{45}...22^{30}$, 23^{15} $\bullet^{1}$-23^{45} $\bullet^{\circ}$-24; $=0^{00}$-2^{40} $\equiv{}^{2}$-$7^{15}=-9^{40}$, 19^{20}-24; $\triangle^{2-0}3$-10
22	7	0.0	•	$\bullet^{\circ}0^{00}$-4^{10}, $7^{45}...8^{25}$ $\overset{*}{\triangledown}{}^{\circ}14^{45}$-$15^{15}$; $=0^{00}$-10^{20}, 20^{47}-24; $\triangle^{1}np$
23	8	0.2	•	$\bullet^{\circ}19^{40}...20^{22}$; $=0^{00}$-5^{40}; $\triangle^{1-0}0^{00}$-10
24	8	5.6	•	$\bullet^{\circ}0^{40}...10^{20}$, $18^{02}...20^{10}$ $\bullet^{1-0}...23^{10}$; $=2^{20}$-5^{15}, 19^{15}-21^{40}
25	8	0.0	•	$\bullet^{\circ}1^{00...18}$; $=na$; $\triangle^{2-0}7$-10
26	8	•	•	$=22^{30}$-24; $\triangle^{1-0}3$-10, 21-24
27	8	•	•	$=0^{00}$-5^{30}; $\triangle^{0-1}0^{00}$-7
28	8	•	•	$=22^{25}$-24; $\triangle^{\circ}22$-24
29	7	2.9	•	$\bullet^{\circ}8^{44}...11^{20}$ $\overset{*}{\triangledown}{}^{1}17^{54}$-$18^{30}$; $=0^{00}$-6^{30}, 21^{45}-24; $\triangle^{1}0^{00}$-8
30	8	0.0	•	$\overset{*}{\triangledown}{}^{\circ}0^{40-45}$ $\bullet^{\circ}7^{10...25}$; $=0^{00}$-$9^{15}=21^{40}$-24; $\triangle^{1-2}21$-24
31	7	2.8	•	$\overset{*}{\triangledown}{}^{\circ}23^{35}$-$24$; $=0^{00}$-$3^{00}=-5^{40}$, a; $\triangle^{2}0^{00}$-10
Σ	—	58.4	—	UWAGI:

Jelenia Góra φ = 50°54' λ = 15°48' Wrzesień - Septembre 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	80.8	83.6	84.4	82.9	10.0	11.8	6.4	8.6	15.7	6.0	96	84	100	93	0.5	2.1	0.0	0.9	10	10	0	W 2	WNW 4	C 0
2	84.6	83.1	81.3	83.0	3.8	19.4	8.6	10.1	20.8	0.7	100	45	97	81	0.0	12.3	0.3	4.2	0 ⊙	10 ⊙	0	C 0	WNW 2	C 0
3	80.5	78.9	76.3	78.6	6.0	23.9	11.3	13.1	25.5	2.3	100	40	91	77	0.0	17.7	1.2	6.3	2 ⊙	0 ⊙	0 ⊙	SE 1	ENE 1	C 0
4	73.5	71.2	66.7	70.5	10.1	28.8	22.8	21.1	29.5	5.7	95	37	55	62	0.7	24.8	12.5	12.7	1 ⊙	3	0	C 0	SW 4	SSE 7
5	66.5	68.0	68.8	67.8	17.7	19.3	11.0	14.8	24.1	10.4	74	57	77	69	5.3	9.7	3.1	6.0	9	8	4	WSW 5	SW 8	C 0
6	68.7	68.2	64.3	67.1	13.9	19.5	19.6	18.2	20.2	8.7	82	55	65	67	2.9	10.3	7.9	7.0	4 ⊙	9	10	WSW 4	WSW 6	WSW 6
7	60.8	63.2	68.0	64.0	17.7	17.5	13.2	15.4	19.8	11.8	72	59	76	69	5.7	8.2	3.7	5.9	10 ●	6 ⊙	7	SW 8	WSW 9	WNW 4
8	70.8	71.7	74.6	72.4	10.1	15.0	10.4	11.5	15.3	9.5	93	61	75	76	0.8	6.6	3.2	3.5	9	8	1	C 0	W 4	W 4
9	80.5	83.6	82.6	82.2	9.1	12.4	6.1	8.4	14.8	5.7	88	75	97	87	1.4	3.5	0.3	1.7	9	9	0	WSW 3	WSW 5	C 0
10	79.4	77.1	75.7	77.4	6.7	23.0	11.6	13.2	24.8	0.5	91	29	75	65	0.9	20.0	3.4	8.1	3	0	3	SSE 1	WNW 2	C 0
11	74.2	75.7	79.6	76.5	18.3	19.2	10.0	14.4	22.2	7.3	58	66	95	73	8.8	7.5	0.7	5.7	9	9 ●	3	SSW 4	W 7	SE 2
12	75.4	70.8	70.1	72.1	17.7	25.4	21.0	21.3	28.0	9.3	66	48	52	55	6.8	16.8	11.9	11.8	9	5 ⊙	4	SW 7	SW 6	W 6
13	77.3	80.4	83.5	80.4	10.1	12.9	9.9	10.7	24.4	9.1	97	62	78	79	0.4	5.7	2.7	2.9	10	8	8	WNW 3	W 8	NW 2
14	86.0	86.0	83.6	85.2	8.3	11.7	4.9	7.4	12.8	4.5	79	57	97	78	2.3	5.9	0.3	2.8	10	3	4	NW 4	WNW 4	C 0
15	79.4	75.3	72.5	75.7	-0.5	19.3	7.7	8.6	20.4	-1.2	100	34	93	76	0.0	14.7	0.7	5.1	0 ≡	6	1	C 0	SE 4	C 0
16	71.0	69.5	71.8	70.8	12.0	22.6	13.4	15.4	24.9	5.0	88	52	98	79	1.7	13.1	0.4	5.1	8	7 ⊙	10 ●	SSE 2	SE 2	C 0
17	72.2	72.4	72.6	72.4	11.2	11.4	8.5	9.9	13.9	8.4	95	79	99	91	0.7	2.8	0.2	1.2	10	10 ●	9	WNW 3	ENE 1	C 0
18	70.3	69.1	69.9	69.8	5.1	8.9	6.5	6.8	10.6	4.0	100	92	99	97	0.0	0.9	0.2	0.4	7 ≡	10 ●	10 ●	C 0	W 2	C 0
19	71.2	73.8	76.1	73.7	6.1	9.0	6.4	7.0	9.6	5.2	100	79	100	93	0.0	2.5	0.0	0.8	10 ●	9 ●	6	C 0	WNW 3	SSE 1
20	78.0	77.9	79.8	78.6	0.2	12.7	5.0	5.7	13.6	-0.1	100	60	98	86	0.0	5.9	0.1	2.0	0 ≡	6	0	C 0	WNW 2	C 0
21	80.9	80.3	80.1	80.4	3.9	11.8	3.7	8.3	12.2	1.0	100	63	84	82	0.0	5.0	1.8	2.3	9	9	10 ●	SSE 1	W 7	WNW 4
22	80.9	81.9	82.9	81.9	7.7	10.8	6.7	8.0	12.4	6.3	96	81	97	91	0.5	2.5	0.3	1.1	10	9	9	WNW 3	WNW 5	C 0
23	80.6	78.8	79.4	79.6	8.2	8.2	5.8	7.0	9.2	5.6	93	87	92	91	0.8	1.4	0.7	1.0	10 ●	10 ●	10	WNW 3	WSW 5	W 3
24	82.5	84.4	86.3	84.4	7.0	9.8	7.5	8.0	10.7	4.4	97	77	100	91	0.3	2.8	0.0	1.0	10	10	9	W 4	NW 5	SE 1
25	86.6	85.7	83.7	85.3	2.3	12.4	6.1	6.7	13.4	1.4	100	61	88	83	0.0	5.6	1.1	2.2	6 ≡	7	0	C 0	ESE 5	SE 3
26	80.8	79.2	78.1	79.4	8.5	18.1	11.2	12.2	18.5	4.9	74	43	72	63	2.9	12.0	3.7	6.2	0 ⊙	0	0	E 5	ESE 5	SE 3
27	76.0	74.3	73.5	74.6	4.0	13.3	8.8	8.7	14.2	1.6	100	66	85	84	0.0	5.2	1.7	2.3	4 ⊙≡	9 ⊙	6	SE 1	NE 6	E 2
28	73.3	72.2	72.8	72.8	2.8	17.6	8.2	9.2	18.1	1.6	100	54	100	85	0.0	9.1	0.0	3.0	6 ≡	8	0 ≡	C 0	NW 1	C 0
29	72.8	73.1	75.8	73.9	7.4	17.6	7.4	10.0	18.5	6.1	100	58	100	86	0.0	8.4	0.0	2.8	9 ≡	6 ⊙	0 ≡	C 0	NE 2	C 0
30	78.4	77.8	78.7	78.3	4.6	20.3	11.8	12.1	21.3	2.9	100	55	89	81	0.0	10.8	1.5	4.1	6 ⊙≡	1	0	C 0	ESE 1	C 0
31																								
M	76.5	76.2	76.5	76.4	8.3	16.1	9.7	11.1	18.0	4.9	91	61	87	80	1.4	8.5	2.1	4.0	6.7	6.8	4.1	2.1	4.2	1.6

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1	80.2	80.9	82.8	81.3	4.0	22.9	9.8	11.6	23.7	2.6	100	38	100	79	0.0	17.3	0.0	5.8	4	2	0	SSE 2	C 0	C 0
2	83.9	83.1	82.8	83.3	5.0	23.6	12.0	13.2	23.8	3.8	100	45	83	76	0.0	16.0	2.3	6.1	0 ≡	0	0	C 0	SE 2	W 2
3	82.6	81.9	82.9	82.5	4.3	23.6	9.5	11.7	24.3	3.5	100	45	97	81	0.0	16.0	0.3	5.4	3	1	0	C 0	C 0	C 0
4	83.0	82.4	83.4	82.9	5.9	23.2	16.0	15.3	24.2	4.5	98	47	95	80	0.2	15.0	1.0	5.4	4	8 ⊙	10	C 0	E 1	NNW 1
5	83.7	84.7	85.3	84.6	13.6	14.9	12.0	13.1	16.7	11.6	100	82	99	94	0.0	3.1	0.2	1.1	10 ≡	10	10 ●	WNW 2	WNW 3	C 0
6	86.8	88.2	90.0	88.3	9.1	10.6	10.4	10.1	12.5	8.7	95	86	96	92	0.7	1.8	0.5	1.0	10 ●	10	10 ●	WSW 3	WNW 2	WNW 2
7	91.1	92.1	93.3	92.2	10.1	12.8	11.8	11.6	13.7	9.0	100	89	91	93	0.0	1.6	1.1	0.9	10 ●	9	9	W 1	E 3	ESE 2
8	92.6	92.2	92.3	92.4	9.5	15.3	9.3	10.8	16.1	8.6	95	73	93	87	0.7	4.8	0.8	2.1	1 ⊙	0	0	E 4	ENE 6	C 0
9	91.0	88.8	87.5	89.1	1.7	20.0	7.6	9.2	20.3	0.7	96	39	96	77	0.3	14.4	0.4	5.0	1	1	0	C 0	ESE 4	C 0
10	85.3	83.0	81.8	83.4	0.1	20.2	5.1	7.6	20.4	0.0	100	44	100	81	0.0	13.4	0.0	4.5	0 ≡	1	0 ≡	C 0	ENE 3	C 0
11	80.0	77.2	76.7	78.0	0.3	20.4	6.0	8.2	21.1	-0.2	100	42	100	81	0.0	13.8	0.0	4.6	0 ≡	0 ⊙	0 ≡	C 0	NNE 2	C 0
12	77.5	78.2	79.6	78.4	5.1	6.5	4.5	5.2	7.2	1.9	100	94	98	97	0.0	0.6	0.1	0.2	10 ≡	10	10 ●	C 0	NNW 1	ENE 4
13	78.9	77.1	74.6	76.9	3.6	11.2	5.4	6.4	13.2	3.5	98	82	100	93	0.1	2.5	0.0	0.9	10	0	10 ≡	ESE 3	E 2	C 0
14	73.7	75.8	78.9	76.1	5.7	5.6	6.3	6.0	6.4	3.2	100	94	88	94	0.0	0.6	1.1	0.6	10 ●	10 ●	9	W 3	W 4	NW 3
15	81.4	84.2	86.0	83.9	6.5	8.2	3.7	5.5	8.5	3.3	97	83	98	93	0.3	1.8	0.2	0.8	10	9 ●	7	NW 2	NW 4	C 0
16	84.1	82.1	82.6	82.9	-0.9	9.7	6.6	5.5	10.8	-1.2	99	62	91	84	0.0	4.6	0.8	1.8	10 ≡	5	10	C 0	C 0	C 0
17	83.8	84.6	85.5	84.6	7.3	10.7	8.4	8.7	11.3	4.5	94	76	97	89	0.6	3.1	0.3	1.3	10	10	10 ●	C 0	WNW 5	WSW 1
18	83.7	80.8	76.7	80.4	7.7	15.2	6.3	8.9	16.8	6.0	97	64	97	86	0.3	6.2	0.2	2.2	10	7 ⊙	0	NW 1	NW 3	C 0
19	75.1	76.7	77.8	76.5	9.5	8.9	8.7	9.0	11.4	5.0	95	75	74	81	0.7	2.9	2.8	2.1	10 ●	10	10	WSW 3	W 8	W 6
20	79.9	83.6	87.9	83.8	7.2	8.9	2.7	5.4	10.7	2.2	88	79	100	89	1.2	2.4	0.0	1.2	10	9	0 ≡	W 6	NW 5	C 0
21	90.5	90.3	90.0	90.3	1.4	12.3	-0.3	3.3	13.0	-1.0	100	32	98	77	0.0	9.7	0.2	3.3	10 ≡	0	0	C 0	C 0	C 0
22	89.4	88.1	87.2	88.2	-4.3	13.9	-0.4	2.2	14.7	-5.1	96	39	98	78	0.2	9.7	0.1	3.3	0	0 ⊙	0	C 0	C 0	S 1
23	85.5	84.0	83.0	84.2	-4.1	13.9	-0.6	2.2	15.7	-4.6	98	43	100	80	0.1	9.1	0.0	3.1	0	0	0 ≡	C 0	S 1	C 0
24	81.5	81.7	82.2	81.8	-4.8	11.0	-0.3	1.4	12.2	-6.2	95	65	100	87	0.2	4.6	0.0	1.6	0 ⊙	0 ⊙	0 ≡	C 0	C 0	C 0
25	80.7	78.7	77.5	79.0	-3.5	14.2	0.4	2.9	14.5	-5.8	97	50	98	82	0.1	8.1	0.1	2.8	10 ≡	0	0	C 0	C 0	C 0
26	75.7	74.5	72.5	74.2	-3.8	15.5	4.2	5.0	16.0	-4.7	96	50	90	79	0.2	8.9	0.8	3.3	0	6 ⊙	0	SE 2	S 3	SE 1
27	71.0	75.9	76.1	74.3	4.9	3.7	2.7	3.5	8.5	1.0	84	92	96	91	1.4	0.7	0.2	0.8	4	10 ●	10 ●	C 0	NW 3	C 0
28	72.1	71.1	69.6	70.9	2.2	5.8	2.6	2.8	4.9	2.1	100	95	96	97	0.0	0.4	0.3	0.2	10 ●	10	10	NW 2	SSE 1	SE 1
29	70.7	73.0	77.6	73.8	2.6	4.8	2.1	2.9	5.4	1.9	98	95	98	97	0.2	0.4	0.1	0.2	10 ●	10 ●	10 ≡	SW 1	C 0	C 0
30	77.8	74.0	70.0	73.9	-0.9	8.3	-0.9	1.4	9.4	-2.5	97	62	94	84	0.2	4.2	0.3	1.6	9	1	0	C 0	S 2	C 0
31	68.1	67.9	69.4	68.5	-2.7	7.3	3.2	2.8	7.6	-3.4	95	61	93	83	0.2	4.0	0.3	1.6	3	10	10 ●	C 0	C 0	C 0
M	81.3	81.2	81.4	81.3	3.3	12.9	5.6	6.8	14.0	1.8	97	65	95	86	0.3	6.5	0.5	2.4	6.1	5.1	4.7	1.1	2.2	0.8

Jelenia Góra $H_s = 342m$ $H_a = 343{,}9m$ $h_w = 16m$ · Wrzesień - Septembre 1962

DNI	WIDZIALNOŚĆ v	OPAD R	GRUB. ŚNIEGU h	POGODA
1	6	0.0	·	$\overset{\circ}{\bullet}4^{15-35}\overset{\circ}{\bullet}{}'5^{18}\text{-}6^{10}\overset{\circ}{\bullet}6^{20}\text{-}7^{12}; = a\text{-}p, p \equiv {}'22^{40}\text{-}24; \triangle^{2} np$
2	8	·	·	$\equiv {}'0^{00}\text{-}6^{25} \equiv {}^{\circ}\text{-}7^{15} = \text{-}8^{40}, np; \triangle^{2}0^{00}\text{-}10 \triangle^{0-2}21\text{-}24$
3	8	0.0	·	$= 0^{00}\text{-}6^{45}; \triangle^{1-2}0^{00}\text{-}9 \triangle^{\circ}21^{00}\text{-}24$
4	8	·	·	$\triangle^{0-1}0^{00}\text{-}9$
5	8	·	·	$\zeta 1^{35}\text{-}2^{20}$
6	8	0.0	·	$\bullet^{\circ}15^{48} \ldots 16^{10} 17^{20}\text{-}19^{50}$
7	8	3.7	·	$\overset{\circ}{\bullet}7^{45}\text{-}8^{00}\bullet^{\circ} \ldots 10^{35}\overset{\circ}{\bullet}{}^{2}\text{-}10^{40}\bullet^{\circ} \ldots 11^{05}\overset{\circ}{\bullet}{}^{0-1}18^{15} \ldots 19^{37}\bullet^{\circ}20^{50} \ldots 21^{10}; \rightarrow 14^{10-45}$
8	8	3.2	·	$\bullet^{\circ}8^{35} \ldots 11^{40}\overset{\circ}{\bullet}14^{38-46}; 16^{38}\text{-}17^{07}$
9	8	·	·	$\overset{\circ}{\bullet}{}'3^{25-35}\overset{\circ}{\bullet}{}^{\circ} \ldots 7^{20}; = 21^{35}\text{-}23^{45}; \triangle {}'21^{00}\text{-}24$
10	8	·	·	$\triangle {}'na \triangle {}^{\circ}20\text{-}24; \smile {}^{\circ}6\text{-}8$
11	8	1.3	·	$\overset{\circ}{\bullet}{}'8^{15-30}; 11^{55}\text{-}12^{10}\bullet^{\circ}13^{50} \ldots 14^{03}; \triangle {}^{\circ}0^{00}\text{-}8^{18}$
12	8	3.8	·	$= 3^{00}\text{-}5^{00}$
13	8	·	·	$\bullet^{\circ}3^{40} \ldots 5^{20}\text{-}7^{45}; = 7^{45}\text{-}10^{30}; \triangle^{\circ} np$
14	8	·	·	$\triangle^{\circ}0^{00}\text{-}9$
15	7	·	·	$= 0^{10}\text{-}1^{00}; 8^{40}\text{-}9^{30}$
16	7	37.2	·	$\overset{\circ}{\bullet}{}^{0-2}19^{32}\text{-}22^{00}\bullet^{0-1}\text{-}24; (\text{IZ})'17^{42}\text{-}18^{25}$ WNW-NE; $= na, 19^{30}\text{-}24 \triangle^{\circ}2\text{-}9$
17	6	0.4	·	$\bullet^{\circ}0^{00-40}; 8^{15} \ldots 10^{40} 13^{05}\text{-}16^{30}; 17^{05-20} 19^{25} \ldots 20^{20}; = 0^{00}\text{-}14^{35}; 20^{15}\text{-}24$
18	5	20.1	·	$\overset{\circ}{\bullet}12^{50}\text{-}16^{40}\bullet^{0-1}\text{-}24; = 0^{00}\text{-}6^{35} \equiv {}^{\circ}\text{-}8^{40} = \text{-}24$
19	7	1.1	·	$\bullet^{\circ}0^{00}\text{-}5^{20} \ldots 15^{38}; = na, a, p\text{-}24$
20	7	0.0	·	$\overset{\circ}{\bullet}{}^{\circ}18^{15-30}; = 0^{00}\text{-}1^{15} \equiv {}^{1-2}\text{-}7^{45} \equiv {}'\text{-}8^{45} = \text{-}11^{30}; 20^{30}\text{-}24; \triangle^{0-1}20\text{-}24$
21	7	3.4	·	$\bullet^{\circ}16^{40}\text{-}19^{20}; 21^{50}\text{-}22^{25}; 22^{50}\text{-}24; = 0^{00}\text{-}9^{30}; np; \triangle^{1-2}0^{00}\text{-}10$
22	7	3.2	·	$\bullet {}'6^{55} \ldots 7^{10}\overset{\circ}{\bullet}{}'8^{10-35}\overset{\circ}{\bullet}{}^{\circ}8^{42-45}; 23^{20-30}; = 0^{00}\text{-}12^{30}$
23	6	9.7	·	$\overset{\circ}{\bullet}{}^{0/28}\text{-}2^{40} 7^{45}\text{-}8^{30}\bullet^{\circ}9^{50} \ldots 12^{25}\bullet^{0-1}16^{45} \ldots 21^{15}; = 21^{15}\text{-}24$
24	7	0.0	·	$= 0^{00}\text{-}11^{35}; 18^{20}\text{-}24$
25	8	·	·	$= 0^{00}\text{-}1^{50} \equiv {}^{\circ}\text{-}8^{45} = \text{-}9^{45}$
26	8	0.0	·	
27	7	0.0	·	$\equiv {}^{0-1}4^{40}\text{-}8^{40} = \text{-}10^{25} \infty {}^{\circ}14^{40}\text{-}16^{20} = \text{-}24; \triangle^{2}5\text{-}9, np, \oplus {}'12^{35}\text{-}18^{10}$
28	7	0.0	·	$= 0^{00}\text{-}2^{40} \equiv {}^{0-2}\text{-}7^{40} \equiv {}'\text{-}8^{20} = \text{-}a, p \equiv {}^{\circ}20^{45}\text{-}24; \triangle^{2}0^{00}\text{-}11, 20\text{-}24$
29	7	0.0	·	$\equiv {}^{\circ}0^{00-20} \equiv {}^{0-1}\text{-}7^{25} \equiv {}^{\circ}\text{-}8^{40} = a, p \equiv {}^{0-2}19^{45}\text{-}24; \triangle^{2}0^{00}\text{-}10, 20\text{-}24$
30	6	0.0	·	$\equiv {}^{2-0}0^{00}\text{-}7^{35} = \text{-}14^{30} \equiv {}^{\circ}21^{45}\text{-}24; \triangle^{2}0^{00}\text{-}10, 20\text{-}24$
31				
Σ	—	87.1	—	UWAGI:

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1	7	0.0	·	$\equiv {}^{\circ}0^{00}\text{-}6^{30} = \text{-}9^{30}; 19^{35}\text{-}22^{40} \equiv {}^{\circ}\text{-}24; \triangle^{2-0}0^{00}\text{-}10 \triangle {}^{\circ}18\text{-}24$
2	7	·	·	$\equiv {}^{0-1}0^{00}\text{-}5^{40} \equiv {}^{2}\text{-}6^{35} \equiv {}^{1-0}\text{-}7^{45} = \text{-}11^{30}; \triangle^{2-0}0^{00}\text{-}10$
3	7	·	·	$= 0^{10}\text{-}9^{30}\text{-}24; \triangle^{1-0}2\text{-}11 \triangle {}^{\circ}20\text{-}24$
4	7	·	·	$= 0^{00}\text{-}10^{20}; 14^{45}\text{-}24; \triangle^{0-1}0^{00}\text{-}9 \triangle {}^{\circ}20\text{-}24$
5	6	5.0	·	$\bullet^{\circ}7^{40} \ldots 8^{40}\bullet^{\circ}18^{40} \ldots 20^{40} 21^{45}\text{-}24; = na \equiv {}^{\circ}6^{40}\text{-}7^{20} \equiv {}^{\circ}\text{-}8^{45} = \text{-}24 \triangle {}^{\circ}0^{00}\text{-}7^{40}$
6	7	3.3	·	$\bullet^{\circ}0^{00} \ldots 2^{40}\bullet^{0-1}5^{20} \ldots 12^{30}\bullet^{\circ}17^{45} \ldots 19^{25}\text{-}24; = 0^{00}\text{-}5^{20}; 15^{15}\text{-}24$
7	6	0.4	·	$\bullet^{\circ}0^{00}\text{-}3^{25} \ldots 5^{15}\bullet^{0-1} \ldots 9^{30}\bullet^{\circ} \ldots 11^{45}; = na \equiv {}^{\circ}8^{45}\text{-}10^{25} = \text{-}24$
8	7	0.0	·	$= 0^{00}\text{-}9^{15} \infty 12^{00}\text{-}17^{30} = \text{-}24; \triangle {}^{\circ}20^{00}\text{-}24$
9	8	·	·	$= 0^{00}\text{-}9^{00} = 22^{35}\text{-}24; \triangle^{0-1}na \smile {}^{\circ}\text{-}10 \triangle {}^{\circ}np$
10	7	·	·	$= 0^{00}\text{-}6^{35} \equiv {}'\text{-}7^{40} = \text{-}10^{20}; p = p \equiv {}^{1-2}19^{40}\text{-}24; \triangle^{0-1}na \smile {}^{\circ}\text{-}a \triangle^{2} p\text{-}np$
11	8	0.3	·	$\equiv {}^{2-0}0^{00}\text{-}7^{45} = \text{-}10^{40}; 18^{20}\text{-}20^{45} \equiv {}'\text{-}24; \triangle^{2-1}0^{00}\text{-}10 \triangle {}'20\text{-}24$
12	5	0.0	·	$\bullet^{\circ}15^{20}\text{-}24; \equiv {}'0^{00}\text{-}3^{10} \equiv {}^{2}\text{-}10^{10} \equiv {}^{\circ}\text{-}10^{45} = \text{-}18^{20}; \triangle^{2}0^{00}\text{-}12$
13	5	0.3	·	$\bullet^{\circ}0^{00}\text{-}1^{45}; = 1^{45}\text{-}17^{30} = \text{-}18^{45} \equiv {}'\text{-}24$
14	5	0.0	·	$\bullet^{\circ}4^{25}\text{-}5^{45} \ldots 7^{45}\text{-}17^{40}; \equiv {}^{2}0^{00}\text{-}4^{20} = \text{-}24$
15	6	0.4	·	$\bullet^{\circ}0^{40} \ldots 2^{40}\bullet^{\circ}8^{20}\text{-}9^{25}\overset{\circ}{\bullet}{}^{\circ}12^{45}\text{-}15^{40}; = na, a, p, p\text{-}24; \triangle {}'np$
16	7	·	·	$= 0^{00-40} \equiv {}^{1-2}\text{-}8^{45} = \text{-}10^{30}; 19^{30}\text{-}24; \triangle {}'0^{00}\text{-}4 \triangle {}^{\circ}18\text{-}24$
17	5	0.2	·	$\bullet^{\circ}20^{15} \ldots 24; = 0^{00}\text{-}24; \triangle {}^{\circ}0\text{-}9$
18	7	0.0	·	$\bullet^{\circ}0^{00} \ldots 5^{40}; = 0^{00}\text{-}8^{15}; 18^{30}\text{-}24; \triangle {}^{\circ}18\text{-}24$
19	7	0.2	·	$\bullet^{\circ}5^{45} \ldots 9^{40}; = 0^{00}\text{-}1^{30} \infty 4^{30} = \text{-}5^{40}; 9^{40}\text{-}11^{30}; \triangle {}^{\circ}0^{00}\text{-}5^{45}$
20	6	0.3	·	$\bullet^{\circ}0^{35} \ldots 9^{35}; = 6^{25}\text{-}13^{10} \equiv {}^{\circ}20^{40}\text{-}24$
21	8	0.0	·	$\equiv {}^{\circ}0^{00}\text{-}5^{30} \equiv {}^{2-0}\text{-}9^{50} = \text{-}10^{30}; 20^{30}\text{-}24; \triangle {}^{\circ}18\text{-}20 \smile {}^{\circ}\text{-}24$
22	8	0.0	·	$= 0^{00}\text{-}6^{15}; 17^{40}\text{-}24; \smile {}^{0-1}0^{00}\text{-}10, 20\text{-}24$
23	7	·	·	$= 0^{00}\text{-}12^{30} \equiv {}^{\circ}17^{45}\text{-}24; \smile {}^{1-2}0^{00}\text{-}9$
24	6	·	·	$\equiv {}^{0-1}0^{00}\text{-}5^{35} = \text{-}13^{10} = 17^{20}\text{-}19^{40} \equiv {}^{\circ}\text{-}21^{30} \equiv {}'\text{-}24$
25	6	·	·	$\equiv {}'0^{00}\text{-}7^{50} = \text{-}11^{15} \infty \text{-}17^{30} = \text{-}24; \triangle {}^{\circ}17\text{-}21$
26	7	·	·	$= 0^{00}\text{-}10^{10} \smile {}^{\circ}0^{00}\text{-}8^{00}$
27	7	6.4	·	$\bullet^{\circ}10^{30} \ldots 13^{25}\text{-}14^{40}\bullet {}'\text{-}18^{45}\bullet^{\circ} \ldots 21^{30} \smile {}'2\text{-}9$
28	6	1.1	·	$\bullet^{0-1}4^{35} \ldots 11^{20}; = 10^{00}\text{-}15^{20}; 16^{30}\text{-}24 = 0^{00}\text{-}18^{45}$
29	5	2.2	·	$\bullet^{\circ}4^{20} \ldots 9^{30}\bullet\bullet^{\circ}\text{-}10^{45}\bullet^{\circ}\text{-}14^{45}; = 0^{00}\text{-}18^{45} \equiv {}^{\circ}\text{-}20^{30} \equiv {}^{\circ}\text{-}24;$
30	7	·	·	$\equiv {}^{0-1}0^{00}\text{-}6^{46} = \text{-}10^{30} \smile {}^{\circ}21\text{-}24$
31	7	21.3	·	$\bullet^{\circ}19^{25} \ldots 21^{15}\text{-}24; = 7^{35}\text{-}9^{30}; 10^{30}\text{-}11^{20}; \sim 9^{30}\text{-}10^{30}$
Σ	—	41.4	—	UWAGI:

Jelenia Góra φ = 50°54' λ = 15°48' Listopad - Novembre 1962

DNI	CIŚNIENIE P = 900 I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI I	II	III	Dies	ZACHMURZENIE N.w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D.v I	II	III
1	68.9	68.9	70.0	69.3	0.4	1.0	0.5	0.6	3.3	0.1	98	96	100	98	0.1	0.3	0.0	0.1	10 *	10 *	10 ●	C 0	W 2	C 0
2	71.0	72.6	73.7	72.4	0.9	4.2	3.1	2.8	4.3	0.3	100	95	97	97	0.0	0.4	0.2	0.2	10	10	10	C 0	SE 1	C 0
3	74.2	73.9	74.4	74.2	1.5	7.0	-0.9	1.7	8.7	-1.4	100	84	100	95	0.0	1.6	0.0	0.5	10 ≡	7	0 ≡	C 0	SSE 2	C 0
4	73.0	71.1	70.9	71.7	-5.4	13.6	7.7	6.4	13.8	-4.2	99	48	80	76	0.0	8.1	2.1	3.4	2 ⊙ ≡	6 ⊙	1	C 0	SE 8	SE 4
5	67.6	66.3	65.8	66.6	9.5	12.8	11.0	11.1	13.1	4.0	70	62	71	68	3.6	5.7	3.8	4.4	6	2	8	SE 8	SE 12	SE 8
6	62.9	63.6	65.7	64.1	10.8	12.5	10.5	11.1	13.6	10.2	70	67	79	72	3.9	4.9	2.7	3.8	6	9	4	SE 8	SE 13	SE 9
7	70.7	75.0	74.7	73.5	9.8	14.2	11.8	11.9	15.4	7.9	82	69	77	86	2.2	5.0	3.1	3.4	8	9	3	SE 7	E 3	SE 5
8	72.0	69.5	70.6	70.7	12.2	15.3	12.6	13.2	15.6	9.7	75	67	72	71	3.5	5.8	4.1	4.5	3	5	9	SE 5	SE 9	SE 4
9	69.7	69.9	71.5	70.4	11.2	12.8	7.4	9.7	13.7	7.2	75	72	93	80	3.3	4.1	0.8	2.7	8	9	10	ESE 4	ESE 4	ESE 5
10	73.4	74.7	77.9	75.3	2.3	2.7	1.2	1.8	7.7	0.9	100	95	94	96	0.0	0.4	0.4	0.3	10 ● ≡	10 ●	10 ●	ESE 3	E 7	ENE 4
11	78.2	76.9	75.4	76.8	0.0	0.0	0.9	0.4	1.2	-0.2	96	98	92	95	0.2	0.1	0.5	0.3	10 ●	10	10	E 2	NE 2	ESE 3
12	74.7	74.6	76.1	75.1	1.8	3.3	3.2	2.9	3.9	0.6	96	95	98	96	0.3	0.4	0.2	0.3	10 ●	10 ●	10 ●	E 3	C 0	SE 1
13	76.7	77.0	76.9	76.9	3.0	6.1	5.4	5.0	7.3	1.9	98	92	98	96	0.2	0.7	0.2	0.4	10	10	10 ●	C 0	E 3	C 0
14	77.2	77.5	76.8	77.2	5.0	4.8	3.8	4.4	5.7	3.6	100	100	98	99	0.0	0.0	0.1	0.0	10 ≡	10 ●	10	C 0	C 0	C 0
15	70.8	66.6	65.1	67.5	3.4	5.1	2.7	3.5	5.3	2.4	97	94	77	89	0.3	0.6	1.7	0.9	10	10 ●	2	C 0	ENE 1	WSW 5
16	68.9	70.6	73.3	70.9	1.2	1.3	0.0	0.6	3.3	-0.5	77	87	96	87	1.5	0.9	0.2	0.9	9	10 *	0	W 6	WNW 6	W 4
17	72.6	70.8	65.3	69.6	-3.5	1.7	0.5	-0.2	1.7	-4.5	94	67	70	77	0.3	2.3	1.9	1.5	4	10	6	C 0	SE 4	SE 5
18	59.2	58.5	56.2	58.0	1.3	3.9	3.7	3.2	5.1	0.1	70	65	77	71	2.0	2.8	1.9	2.2	10	7	8	SSE 8	SE 6	SSE 2
19	59.4	62.4	64.1	62.0	0.3	6.3	1.3	2.3	6.9	-0.6	98	59	91	83	0.1	3.9	0.6	1.5	8 ●	7 ⊙	10	E 2	C 0	C 0
20	65.4	67.0	69.1	67.2	0.5	0.5	-0.8	-0.2	1.8	-1.2	98	94	96	96	0.1	0.3	0.3	0.2	10 *	10 *	7	C 0	NW 1	C 0
21	69.7	68.3	66.5	68.2	-4.9	0.8	-1.1	-1.6	0.9	-6.0	98	77	85	87	0.1	1.5	0.9	0.8	0 ≡	0 ⊙	8	C 0	E 4	E 3
22	65.1	68.9	75.4	69.8	0.3	1.5	-0.3	0.0	1.5	-1.6	85	78	77	80	0.9	1.5	1.3	1.2	10	9	10	E 2	N 3	NW 4
23	78.7	80.4	83.0	80.7	-2.1	0.1	-4.2	-2.6	0.1	-5.6	85	60	91	79	0.7	2.5	0.4	1.2	8	2 ⊙	0	SW 3	NW 4	C 0
24	85.8	86.8	89.0	87.2	-2.1	-1.1	-1.3	-1.4	-0.9	-6.9	98	85	84	89	0.1	0.9	0.9	0.6	10	10	10	WNW 3	W 1	ENE 3
25	89.8	89.0	88.3	89.0	-2.7	1.4	0.0	-0.3	1.9	-3.4	91	74	86	84	0.5	1.8	0.8	1.0	10	6	10	C 0	C 0	C 0
26	89.8	91.2	92.5	91.2	0.7	1.0	1.0	0.9	1.2	-0.4	98	98	98	98	0.1	0.2	0.2	0.2	10 ●	10 ● ≡	10 ● ≡	C 0	NW 1	WNW 2
27	91.2	90.0	87.6	89.6	0.7	1.8	1.2	1.2	1.8	0.5	98	93	98	96	0.1	0.6	0.2	0.3	10	10 *	10 ≡	C 0	C 0	C 0
28	84.8	84.6	85.4	84.9	0.6	2.7	1.3	1.5	3.1	0.2	98	84	94	92	0.1	1.2	0.4	0.6	10	9	10	SSE 1	SW 1	C 0
29	84.4	83.1	80.8	82.8	1.4	4.7	4.0	3.5	5.1	0.7	96	90	77	88	0.3	0.8	1.9	1.0	10	10	10	C 0	NW 3	WSW 6
30	77.1	77.0	80.3	78.1	4.4	3.8	1.6	2.8	4.8	0.8	87	90	81	86	1.1	0.8	1.3	1.1	10	10 ●	9	W 7	W 8	W 2
31																								
M	74.1	74.2	74.7	74.3	2.2	4.9	2.9	3.2	5.7	0.5	91	81	88	87	0.9	2.0	1.1	1.3	8.4	8.2	7.7	2.4	3.6	2.6

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1	90.8	96.0	100.0	95.6	-0.7	-1.2	-2.3	-1.6	1.9	-3.1	87	89	91	89	0.7	0.6	0.5	0.6	10	8 *	8	NW 2	NW 2	WNW 4
2	101.0	102.3	100.8	101.7	-9.3	-2.9	-11.5	-8.8	-2.1	-13.5	91	82	86	86	0.3	0.9	0.4	0.5	2	6 ⊙	0	C 0	C 0	SE 1
3	96.8	94.7	92.3	94.6	-15.3	-4.9	-12.6	-11.4	-4.7	-16.9	100	86	85	90	0.0	0.6	0.4	0.3	0	3	0	C 0	C 0	C 0
4	89.4	88.2	87.9	88.5	-13.1	-2.1	-11.2	-9.4	-0.6	-15.1	84	87	90	87	0.4	0.6	0.3	0.4	8	3	2	C 0	C 0	C 0
5	85.1	87.1	89.8	87.3	-12.9	-1.4	-2.3	-4.7	-0.9	-15.4	88	92	93	91	0.3	0.4	0.4	0.4	2	10 ●	10 ●	C 0	WNW 3	C 0
6	89.4	88.7	89.1	89.1	-5.6	0.2	-9.7	-5.7	1.4	-9.9	99	81	91	90	0.1	1.2	0.3	0.5	10 ≡	2 ⊙	0 ≡	C 0	C 0	C 0
7	87.9	87.4	89.1	88.1	-11.2	-1.3	-7.6	-6.9	-0.5	-11.9	90	93	93	92	0.3	0.4	0.2	0.3	2	0	0 ≡	C 0	C 0	NE 1
8	89.4	88.9	85.3	87.9	-11.3	-0.6	-8.1	-7.0	-0.2	-12.1	90	81	92	88	0.3	1.1	0.2	0.5	0	7	8	C 0	C 0	C 0
9	74.4	67.9	63.0	68.4	-1.7	6.7	2.3	2.4	7.0	-9.5	79	26	66	57	1.1	7.3	2.4	3.6	9	9	9 *	ENE 4	SSW 8	SW 7
10	62.6	62.5	64.9	63.3	2.7	3.1	2.5	2.7	3.3	1.4	70	73	93	79	2.2	2.1	0.5	1.6	9	8	10	WSW 5	SW 6	WNW 7
11	67.4	66.9	61.3	65.2	2.8	3.6	3.0	3.1	3.8	1.8	81	73	69	74	1.5	2.1	2.4	2.0	10	9	10	WNW 8	W 5	WSW 3
12	54.0	51.1	53.8	53.0	3.3	6.5	1.9	3.4	8.3	1.1	73	57	69	66	2.1	4.2	2.2	2.8	10	8	9	S 5	SSE 7	SE 7
13	52.8	53.6	58.1	4.8	1.6	2.3	0.7	1.3	3.2	0.3	78	84	94	85	1.6	1.2	0.4	1.1	10	8	10	SE 6	SW 2	C 0
14	62.9	65.6	66.5	65.0	1.1	1.1	-0.1	0.5	1.3	-0.6	100	66	69	78	0.0	2.2	1.9	1.4	10 ● ≡	8	10 *	C 0	WNW 5	W 4
15	51.6	46.6	46.7	48.3	0.2	1.3	1.3	1.0	3.1	-2.2	79	85	70	78	1.3	1.0	2.0	1.4	10 *	10 *	9	SSW 8	WSW 7	SW 3
16	33.2	34.8	40.2	36.1	4.7	3.1	2.2	3.0	5.1	0.4	82	90	95	89	1.5	0.8	0.4	0.9	10	10 ●	10 ●	W 6	WSW 3	W 4
17	52.5	56.0	58.0	55.5	0.1	-0.3	-0.9	-0.5	2.3	-3.1	100	98	95	98	0.0	0.2	0.3	0.2	10 *	9	10 *	WNW 6	WNW 4	C 0
18	57.7	57.1	59.2	58.0	-1.8	-1.1	-2.3	-1.9	0.6	-2.9	98	95	96	96	0.1	0.3	0.3	0.2	10	9	10	C 0	C 0	C 0
19	61.0	62.8	69.9	64.6	-5.1	-4.5	-6.0	-5.4	-2.0	-6.4	93	91	89	91	0.3	0.4	0.4	0.4	10	10	10	C 0	N 2	N 2
20	77.6	80.1	80.3	79.3	-6.9	-6.4	-16.7	-11.7	-5.8	-17.4	69	78	90	84	0.5	0.8	0.2	0.5	10 *	10 *	0	N 2	C 0	C 0
21	73.1	70.6	74.6	72.8	-21.9	-8.7	-19.8	-17.6	-8.4	-26.1	88	92	89	90	0.1	0.3	0.1	0.2	10	9	0 ≡	C 0	N 1	N 1
22	84.8	90.6	96.7	90.7	-17.7	-15.1	-16.3	-16.4	-14.8	-25.0	84	91	90	88	0.2	0.2	0.2	0.2	10 *	9	10	C 0	N 2	N 1
23	97.9	98.9	99.9	98.9	-16.8	-15.9	-14.3	-15.3	-14.3	-17.5	90	76	83	83	0.2	0.4	0.3	0.3	9 *	9	10 *	N 2	NNW 2	C 0
24	98.7	97.3	94.9	97.0	-18.0	-13.0	-10.0	-12.8	-9.9	-20.3	90	76	81	82	0.2	0.5	0.5	0.4	9	9 *	10 *	C 0	C 0	ESE 1
25	89.9	86.0	81.5	85.8	-10.8	-9.1	-11.0	-10.5	-6.4	-14.7	87	73	90	83	0.4	0.8	0.3	0.5	10	3 ⊙	10 *	SE 4	E 2	C 0
26	75.3	72.3	70.0	72.5	-13.0	-8.3	-10.4	-10.5	-8.1	-14.2	88	83	87	86	0.3	0.5	0.4	0.4	10	9 *	9 *	C 0	W 1	C 0
27	68.3	68.3	70.0	68.9	-15.3	-11.5	-18.8	-16.1	-9.9	-21.8	95	73	95	88	0.1	0.6	0.1	0.3	10 *	0 ⊙	10	C 0	C 0	C 0
28	70.0	70.6	69.8	70.1	-9.9	-7.3	-12.3	-10.4	-7.3	-18.8	84	82	89	85	0.4	0.6	0.3	0.4	10		0	C 0	NE 3	C 0
29	66.5	65.3	67.3	66.4	-19.9	-7.2	-8.2	-10.9	-6.6	-20.5	89	79	92	87	0.1	0.7	0.2	0.3	0	0	10	C 0	SW 2	WSW 1
30	67.8	68.4	70.3	68.8	-7.1	-6.3	-6.8	-6.8	-6.2	-8.6	85	83	83	84	0.5	0.6	0.6	0.6	10	10	10	SE 4	ESE 4	SE 3
31	72.5	74.5	76.4	74.5	-7.9	-9.0	-10.3	-9.4	-6.8	-10.5	90	82	84	85	0.3	0.5	0.4	0.4	10 *	10 *	10	SE 2	SSE 3	SE 3
M	74.3	74.2	75.1	74.5	-7.6	-5.6	-7.0	-6.3	-2.5	-10.7	88	81	86	85	0.6	1.1	0.6	0.8	8.1	7.5	7.2	2.1	2.4	1.7

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ SNIEGU h	POGODA
1	4	11.9	7	•0^00-4^15 *^1-0-8^40 •^0-11^40 *^0-12^10 *^0-14^40 *^0-16^15 •^0-19^20 *^0-20^00 •^0-20^30 •^0-22^25 •^0-24; =4^00-24
2	5	0.0	3	•^0^00-35 ••^0-4^10; =0^00-24
3	6	•	pł.	=0^00-5^45 ≡^0-9^40 =-14^35,n ≡^0-2 17^25-24
4	8	•	•	≡^0-1 0^00-7^30 =-9^20
5	7	•	•	⚲7^30-13^30
6	7	•	•	⚲7^40-17^15 21^20-24
7	8	•	•	⚲5^30-6^20
8	8	•	•	
9	7	1.0	•	•^0 17^45 19^35
10	5	2.7	•	•^0 4^40 6^30 •^0-13^20 •^0-14^10 •^0-14^40 •^0-22^35 *^0-24; ≡^0 6^30-9^40 =-24
11	6	0.2	•	*^0^00-6^10 •^0-7^30 10^40 •^0 14^35-19^40; =0^00-24
12	6	2.0	•	•^0 6^40-7^40 •^0-14^15 19^25 •^0-24; =0^00-24
13	6	0.0	•	•^0^00-4^35 20^35 24; =0^00-24
14	4	2.6	•	•^0^00 5^35 7^15 8^45 ••^0-10^15 •^0-15^45 16^20-18^30; =0^00-6^40 ≡^0-11^55 =-24
15	5	0.2	•	•^0 11^40 14^35; =0^00-23^15
16	5	0.3	•	⚥^0 10^45-11^35 ⚹^0-12^15 ⚹' 12^45-14^40 ⚥' 15^15-45
17	8	•	pł.	
18	8	0.0	•	*^0 21^45 22^10
19	7	3.0	•	•^0 3^10 5^00 21^45-24; =20^30-24
20	4	3.8	1	•^0^00-1^15 3^45-5^30 *^1-0 8^40 *^0-15^35; =0^00-19^30
21	6	•	1	≡^0 6^35-7^20 ≡^2-9^35 ≡^1-10^10 =-24
22	7	0.0	1	*^0 15^35 19^15; =0^00-10^15; 13^30-24
23	8	•	1	=0^00-6^30
24	6	•	1	=4^30-24
25	6	0.8	1	=0^00-11^15 ∞-15^30 =-24
26	3	0.7	pł.	•^0 2^15 3^30 •^0-24; =0^00-7^45 ≡^0-9^25 =-12^10 ≡^0-1 19^45 ≡^0-1-24
27	5	0.5	pł.	•^0 2^45-4^40 *^0 12^50 13^10 •^0-14^15; ≡^0 0^00-4^40 ≡^0-5^20 =-15^45 ≡^0-24
28	6	•	•	≡^0-1 0^00-6^30 =-24
29	6	0.0	•	
30	6	6.2	•	•^0 6^15 15^20 ⚥^0-16^20 ⚥^0 17^5-25 ⚥^0 18^10-20 ⚥^0-1 21^50-24; =1^35-3^15 6^35-19^15
31				
Σ	—	35.9	—	UWAGI

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1	7	1.9	6	⚥' 0^00-1^30 *^0-1-4^45 ⚥^0-1 7^40-17^10 *^0 22^40 24
2	6	•	8	*^0 0^00-1^10 ==15^35-17^20 ≡^0 21^40-23^45
3	6	•	8	≡0^45-5^40 =-7^15 ==16^15-17^30 =-24; ⋀⋀ 12^30-17^30
4	6	•	6	=0^00-24
5	6	0.0	6	⚥^0 12^15-13^45 20^40-23^35; =0^00-24
6	4	•	6	=0^00-6^48 ≡^0-1 10^35 ≡^0-1 12^35 =-19^40 ≡^0-1-24
7	6	•	6	≡' 0^00-6^40 =-15^50 ≡^0-24
8	5	•	5	≡^0-1 0^00-6^40 =-24
9	8	0.1	5	*^0 14^28 15^15 *^0 17^45 18^30 •^0 20^20 *^0 21^30; =na
10	8	3.1	3	•^0 2^35 3^10 15^25-16^40 *^0-18^20 *^1-20^35
11	7	0.1	pł.	•^0 7^15 9^20 11^15-30
12	7	•	•	
13	7	0.2	•	=14^30-24
14	8	0.3	•	•^0 5^45-7^15 *^0 8^20 19^40 21^10; =0^00-5^45 ≡^0-7^40 =-12^10,n
15	6	1.5	•	*^0 5^40 6^20 *^0-1-13^35 •^0 14^35 *^0-15^20 ⚥^0 16^35-17^15 18^15-25 *^0 23^45 24
16	7	14.7	•	*^0 0^00 1^40-2^35 *^0-3^40 •^0-1 4^45-6^45 •' 7^25-8^10 ⚥^0 9^45-11^40 •^0 12^05 24
17	6	9.1	9	•^0 0^00 20 *^0-1 1^35-11^15 12^30 18^10 19^20-24; =12^00-24
18	5	2.1	19	*^0-1 0^00-6^00 8^40 9^35-12^40 *^0 13^40-17^35; =0^00-24
19	6	0.1	21	*^0 14^10-15^45 16^35; =0^00-24
20	5	0.1	22	*^0 6^10 7^45 9^15-13^40; =0^00-24
21	7	0.0	22	=0^00-12^30 14^10-17^40 ≡^1-0 22^40 =-24
22	5	0.5	20	*^0 4^45 7^15 8^35-10^20 18^40-20^35 23^45-24; =0^00-24
23	6	0.5	20	*^0 0^00 3^45 6^40 8^20 15^35-24; =0^00-1^00 8^20-24
24	6	0.7	20	*^0 0^00 3^45 8^45 13^35 15^15-17^45 24; =0^00-24
25	7	0.5	22	*^0 0^00 4^10 19^45 22^15-24; =0^00-7^30 14^45-24
26	5	0.0	19	*^0 0^00-2^45 11^00 24; =0^00-24
27	5	0.0	19	*^0 6^00 10^15; =0^00-24
28	6	•	19	=0^00-24
29	4	•	16	=0^00-24
30	6	2.2	16	*9^40 10^20; =0^00-24
31	5	4.0	20	*^0 1^30 4^15-5^30 *' 7^35 *^0-14^10 22^45 24; =0^00-24
Σ	—	41.7	—	UWAGI

Śnieżka — φ = 50°44' — λ = 15°44' — Styczeń - Janvier 1962

DNI	CIŚNIENIE P= 700 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	123.2	125.9	126.3	125.1	-5.6	-8.4	-6.4	-6.7	2.2	-8.7	82	89	39	70	0.7	0.3	2.3	1.1	7	9	9	W 30	W 18	W 18
2	125.5	127.2	128.7	127.1	-9.4	-10.2	-12.4	-11.1	-6.3	-13.1	85	91	89	88	0.4	0.3	0.3	0.3	10	9	10 ≡	WNW14	NW 10	NNW18
3	133.0	136.1	137.8	135.6	-11.4	-5.6	-4.7	-6.6	-4.7	-15.6	27	92	83	67	1.9	0.3	0.7	1.0	0	10 ≡	0	NW 16	NW 16	NE 8
4	139.5	140.3	141.3	140.4	-0.4	2.2	2.2	1.6	2.5	-5.8	21	30	9	20	4.6	5.0	6.5	5.4	0	0 ⊙	0	SSE10	S 6	N 2
5	139.7	138.3	134.7	137.6	1.5	3.2	3.0	2.7	4.8	0.4	8	18	26	17	6.3	7.5	5.5	6.4	2	5 ⊙	1	N 2	N 6	SW 18
6	130.7	129.2	128.2	129.4	-2.0	-3.0	-5.6	-4.0	3.0	-6.1	98	93	95	95	0.1	0.4	0.2	0.2	2	5	10 ≡	WSW25	W 27	NW 25
7	131.6	136.1	139.7	135.8	-7.4	-7.6	-8.4	-8.0	-5.6	-9.6	93	93	92	93	0.2	0.2	0.3	0.2	10 ✱ ≡	10 ≡	10 ≡	NW 20	NW 18	NW 12
8	140.3	141.3	140.2	140.6	-1.4	-1.6	-2.4	-2.0	-1.3	-9.6	94	98	98	97	0.3	0.1	0.1	0.2	10 ≡	10 ≡	10 ≡	W 12	WNW10	WNW 6
9	134.4	132.0	131.2	132.5	-6.8	-6.8	-5.0	-5.9	-2.4	-9.2	94	94	95	94	0.2	0.2	0.2	0.2	10 ≡	9	10 ≡	WSW12	WSW20	WSW18
10	126.3	125.0	121.9	124.4	-6.2	-1.8	-3.6	-3.8	-1.8	-7.1	94	98	92	95	0.2	0.1	0.4	0.2	10 ≡	8 ⊙	10 ≡	WSW20	NW 6	SW 28
11	122.1	120.4	119.0	120.5	-4.2	-4.6	-2.6	-3.5	-1.7	-5.8	94	96	98	96	0.3	0.2	0.1	0.2	10 ≡	10 ✱ ≡	10 ✱ ≡	SW 17	SW 25	SW 22
12	124.0	120.4	110.6	118.3	-3.4	-4.3	-5.6	-4.7	-2.2	-6.6	97	96	95	96	0.2	0.2	0.2	0.2	10 ≡	10 ≡	10 ≡	SW 8	SW 16	SW 34
13	110.0	111.4	113.8	111.7	-4.6	-6.4	-6.5	-6.0	-4.1	-6.8	96	94	94	95	0.2	0.2	0.2	0.2	10 ≡	10 ≡	10 ≡	SW 26	SW 25	SW 18
14	117.9	119.5	121.4	119.6	-7.6	-7.6	-7.2	-7.4	-6.3	-9.9	93	93	93	93	0.2	0.2	0.2	0.2	10 ✱ ≡	10 ✱ ≡	10 ✱ ≡	SW 16	SW 18	SW 24
15	126.9	129.8	133.3	130.0	-8.0	-8.0	-8.3	-8.2	-6.9	-8.7	93	93	92	93	0.2	0.2	0.2	0.2	10 ✱ ≡	10 ≡	10 ≡	SW 16	SW 16	W 20
16	135.4	131.8	131.9	133.0	-9.0	-7.5	-7.8	-8.0	-7.2	-9.5	92	93	90	92	0.3	0.2	0.3	0.3	3	9	9	SW 18	SW 20	SW 20
17	130.9	131.9	132.9	131.9	-7.6	-6.8	-3.3	-5.2	-2.8	-8.3	87	88	92	89	0.4	0.4	0.4	0.4	9	8	10	SSW23	SW 17	SW 10
18	131.7	130.9	131.5	131.4	-3.2	-2.0	-3.0	-2.8	-2.0	-6.3	97	98	97	97	0.1	0.1	0.1	0.1	8	8	6	SW 12	SW 18	SW 24
19	132.8	131.0	129.0	130.9	-1.6	-2.7	-3.2	-2.7	-1.1	-3.8	98	97	97	97	0.1	0.1	0.1	0.1	10 ≡	10 ✱ ≡	10 ✱ ≡	SW 20	WNW18	SW 25
20	132.5	134.1	137.0	134.5	-2.8	-2.7	-4.6	-3.7	-2.2	-4.9	97	97	96	97	0.1	0.1	0.2	0.1	10 ✱ ≡	10 ≡	4	SW 20	SW 20	W 20
21	137.2	137.2	134.3	136.2	-1.2	-0.8	-0.6	-0.8	-0.4	-5.1	99	99	99	99	0.1	0.0	0.0	0.0	10 ≡	10 ≡	10 ≡	SW 20	W 12	WSW20
22	127.4	123.0	126.1	125.5	-1.6	-2.7	-5.6	-3.9	-0.4	-6.1	98	97	95	97	0.1	0.1	0.2	0.1	10 ≡	10 ≡	10 ≡	SW 20	SW 35	WSW20
23	128.9	129.8	131.8	130.2	-7.5	-7.2	-7.2	-7.3	-5.5	-8.6	93	93	93	93	0.2	0.2	0.2	0.2	10 ✱ ≡	10 ✱ ≡	10 ✱ ≡	WSW20	WSW20	WSW20
24	132.1	130.4	128.1	130.2	-7.8	-6.8	-4.2	-5.8	-4.1	-8.3	93	94	96	94	0.2	0.2	0.2	0.2	10 ✱ ≡	10 ✱ ≡	10 ✱ ≡	WSW20	WSW18	W 26
25	127.1	127.0	127.8	127.3	-1.4	-2.0	-2.4	-2.0	-1.4	-4.5	99	98	98	98	0.1	0.1	0.1	0.1	10 ≡	10 ≡	10 ≡	W 20	W 16	WNW14
26	131.6	133.3	129.4	131.4	-4.8	-4.4	-3.6	-4.1	-2.4	-6.6	95	91	97	94	0.2	0.4	0.2	0.3	10 ≡	9	10 ✱ ≡	WNW16	WNW11	WNW12
27	129.8	132.5	130.4	130.9	-6.6	-6.4	-7.8	-7.2	-2.3	-8.0	94	94	93	94	0.2	0.2	0.2	0.2	10 ✱ ≡	10 ✱ ≡	10 ✱ ≡	WNW25	WNW20	NW 26
28	129.3	126.9	127.2	127.8	-8.1	-8.4	-15.2	-11.7	-7.1	-15.3	92	92	86	90	0.2	0.3	0.3	0.3	10 ✱ ≡	10 ✱ ≡	10 ✱ ≡	NW 20	NW 25	NW 25
29	129.5	132.5	135.9	132.6	-15.4	-14.8	-16.0	-15.6	-13.8	-16.2	86	96	76	86	0.3	0.1	0.4	0.3	10 ✱ ≡	10 ✱ ≡	10 ✱ ≡	NW 25	NW 26	NW 20
30	136.6	140.3	142.3	139.7	-17.6	-13.0	-14.2	-14.8	-12.2	-18.3	84	80	87	84	0.2	0.5	0.3	0.3	10 ✱ ≡	9 ⊙	4	NW 20	NE 22	NE 26
31	140.7	140.5	137.5	139.6	-15.6	-15.0	-12.8	-14.0	-12.7	-16.6	86	78	88	84	0.3	0.4	0.3	0.3	10 ≡	3 ⊙	8	NE 20	NNE14	E 14
M	130.3	130.5	130.4	130.4	-6.1	-5.6	-6.0	-5.9	-3.5	-8.7	86	89	86	87	0.6	0.6	0.7	0.6	8.4	8.7	8.4	18.2	17.7	19.1

Luty - Février

1	130.0	127.3	127.9	128.4	-7.2	-5.4	-9.8	-8.0	-5.0	-12.9	71	67	76	71	1.0	1.3	0.7	1.0	1	4 ⊙	0	SE 3	NNW 3	SE 3
2	128.3	129.3	132.1	129.9	-11.4	-9.4	-8.2	-9.3	-8.1	-12.2	51	60	92	68	1.2	1.2	0.2	0.9	6	4	10 ✱ ≡	SW 4	SW 8	NW 12
3	134.4	136.8	137.9	136.4	-10.0	-8.8	-10.2	-9.8	-8.1	-10.6	91	92	84	89	0.3	0.3	0.4	0.3	8	10 ≡	1	NW 17	NW 16	NW 3
4	131.9	132.0	134.8	132.9	-8.2	-5.8	-9.4	-8.2	-4.4	-10.7	60	95	91	82	1.3	0.2	0.3	0.6	7	8	10 ≡	WNW25	W 18	W 8
5	126.6	121.1	123.5	123.7	-8.4	-5.8	-7.3	-7.2	-4.7	-10.3	92	97	93	94	0.3	0.1	0.2	0.2	10 ≡	10 ✱ ≡	10 ✱ ≡	WSW20	WSW20	NNW28
6	129.1	131.5	134.3	131.6	-8.1	-7.1	-6.8	-7.2	-6.6	-9.4	92	93	94	93	0.2	0.2	0.2	0.2	10 ≡	10 ≡	10 ≡	NW 28	NW 22	NW 18
7	134.1	133.1	128.0	131.7	-3.0	-2.4	-3.6	-3.2	-2.0	-7.0	97	96	97	97	0.1	0.2	0.2	0.2	10 ≡	10 ≡	10 ≡	NW 10	WNW 6	SW 14
8	127.5	129.5	132.0	129.7	-2.9	-1.8	-3.4	-2.9	-1.8	-4.4	97	98	97	97	0.1	0.1	0.2	0.1	10 ≡	10 ≡	6	W 8	WSW 6	W 6
9	135.0	138.2	142.2	138.5	-4.8	-7.2	-10.4	-8.2	-3.4	-10.6	95	93	90	93	0.2	0.2	0.3	0.2	10 ≡	1	0	W 6	WNW15	WNW17
10	144.4	144.3	143.4	144.0	-10.0	-5.2	-4.9	-6.2	-3.9	-11.9	59	61	57	59	1.2	1.6	1.8	1.5	1	3 ⊙	3	NNW 7	W 4	W 1
11	138.5	138.6	141.0	139.4	-2.4	-7.0	-9.4	-7.0	-2.2	-9.5	82	93	91	89	0.9	0.2	0.3	0.5	9	10 ✱ ≡	4	SW 14	WNW18	WSW16
12	124.3	115.8	107.4	115.8	-9.4	-5.9	-2.8	-5.2	-2.8	-9.7	91	97	95	94	0.3	0.1	0.2	0.2	10 ✱ ≡	10 ✱ ≡	10 ✱ ≡	SW 35	SW 35	SW 45
13	107.8	106.2	106.8	106.7	-6.7	-6.8	-8.6	-7.7	-2.8	-9.0	88	94	92	91	0.4	0.2	0.3	0.3	10 ✱ ≡	10 ✱ ≡	10 ✱ ≡	WNW14	W 6	WNW 9
14	108.4	110.3	114.3	111.0	-11.0	-10.3	-11.6	-11.1	-8.6	-12.1	90	87	89	89	0.3	0.4	0.3	0.3	10 ✱ ≡	10 ✱ ≡	10 ✱ ≡	WNW12	NNW14	NNW14
15	122.4	126.7	132.0	127.0	-13.0	-13.0	-14.6	-13.8	-11.6	-15.1	88	88	87	88	0.3	0.3	0.3	0.3	10 ✱ ≡	10 ✱ ≡	9 ✱	NNW16	NNW20	NNW12
16	121.4	115.4	108.9	115.2	-11.5	-6.5	-6.2	-7.6	-5.2	-15.0	90	94	94	93	0.3	0.2	0.2	0.2	10 ✱ ≡	10 ≡	10 ≡	SW 28	SW 32	W 40
17	107.6	111.6	114.6	111.3	-7.5	-8.2	-9.0	-8.4	-6.2	-9.1	93	92	92	92	0.2	0.2	0.3	0.2	10 ✱ ≡	10 ✱ ≡	10 ✱ ≡	NW 40	NW 35	NW 40
18	123.9	129.1	133.7	128.9	-10.8	-11.2	-11.0	-11.0	-9.0	-11.5	90	90	90	90	0.3	0.3	0.3	0.3	10 ✱ ≡	10 ✱ ≡	8	NNW40	NW 25	NNW20
19	131.5	133.1	134.7	133.1	-7.8	-5.8	-5.4	-6.1	-5.0	-11.3	93	95	95	94	0.2	0.2	0.2	0.2	10 ✱ ≡	10 ✱ ≡	10 ✱ ≡	WNW35	NW 20	NW 20
20	135.3	135.7	134.7	135.2	-7.0	-6.2	-4.2	-5.4	-4.0	-7.7	93	94	96	94	0.2	0.2	0.2	0.2	10 ≡	10 ≡	10 ✱ ≡	NW 16	NNW18	NNW28
21	134.2	135.7	137.7	135.9	-7.6	-9.3	-11.2	-9.8	-3.9	-12.0	96	91	90	92	0.1	0.3	0.3	0.2	10 ✱ ≡	10 ✱ ≡	10 ✱ ≡	NNW22	NW 18	NW 20
22	139.1	138.8	140.9	139.6	-12.8	-13.2	-13.8	-13.4	-11.0	-14.3	88	88	88	88	0.3	0.3	0.3	0.3	10 ✱ ≡	10 ✱ ≡	10 ✱ ≡	NW 16	NW 15	NW 12
23	140.3	140.2	135.4	138.6	-15.6	-14.4	-13.0	-14.0	-12.8	-16.7	86	100	88	91	0.3	0.0	0.3	0.2	9	8	10 ≡	NW 15	NW 10	NW 19
24	130.8	128.8	128.1	129.2	-12.6	-12.0	-16.0	-14.2	-10.8	-16.2	89	89	86	88	0.3	0.3	0.2	0.3	10 ✱ ≡	10 ✱ ≡	10 ✱ ≡	WNW16	NW 16	NW 18
25	127.9	129.8	129.9	129.2	-17.8	-15.8	-15.2	-16.0	-14.4	-18.1	84	86	86	85	0.2	0.3	0.3	0.3	8 ✱	10 ≡	4	NE 20	ESE 8	NE 14
26	129.3	129.4	129.1	129.3	-15.8	-13.6	-13.4	-14.0	-12.7	-16.2	86	88	88	87	0.3	0.3	0.3	0.3	10 ≡	10 ≡	10 ≡	E 12	SE 10	SE 10
27	128.1	128.6	128.0	128.2	-11.2	-9.6	-8.8	-9.6	-8.1	-13.4	90	91	92	91	0.3	0.3	0.3	0.3	8	10 ✱ ≡	10 ✱ ≡	SE 16	SE 18	SSE12
28	126.8	126.5	125.8	126.4	-8.2	-6.5	-6.1	-6.7	-5.4	-9.1	92	94	100	95	0.2	0.2	0.0	0.1	10 ≡	10 ≡	10	SE 8	SE 8	E 2
29																								
30																								
31																								
M	128.5	128.7	129.3	128.8	-9.4	-8.4	-9.1	-9.0	-6.6	-11.6	86	89	90	88	0.4	0.3	0.3	0.3	8.8	8.9	8.0	18.0	16.0	16.5

Śnieżka H_s = 1603m H_6 = 1610,6m Styczeń - Janvier 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚCIŃ GU h	POGODA
1	7	•	14	↖-≫0^00-24; ≡² ≡ 0^00-13^30 ▭-24; ▼°0^15-2^20 8^20-12^30
2	7	0.8	13	*°19^50...23^40, ⊥'19^50-24; ≫-↖0^00...24; ▭ 0^00-5^30 ≡, ≡²-24; v°8^20-24
3	0	1.0	11	⚥°14^15-15^30 ⚥°-16^30 ⚥°17^30-18^00; ⊥°0^00-1^30; ↖-≫0^00-20^30; ≡ 0^00-1^30 ▭-2^20; 6^20-9^00 ≡ 7^15-20 8^05-9^00 ≡²18^00 ≡-19^40 ▭18^00-24; v°0^00-1^30 9^00-18^00
4	9	•	10	≫4^30-8^15; ▭ 0^00-24
5	7	•	8	≫16^10-20^30 ↖-24; ▭ 0^00-24
6	8	2.9	6	*°17^00...24; ⊥²17^00-24; ↖ 0^00-24; ▭ 0^00-16^15 ≡, ≡² 11^40-24 ▭ 16^50-20^20; v°16^15-20 20^20-24
7	0	1.2	8	*°0^00-5^30 ⚥°6^45 8^50; ⊥²'0^00-18^30; ↖ 0^00-20^20 ≫-22^30; ≡²0^00-9^30 ≡ -10^20 ≡² -21^40 ▭-24; v°0^00-21^40
8	0	1.3	8	↖ 0^20-6^20 ≫-16^15; ▭ 0^00-3^30 ≡ -4^30 ≡² -16^10 ≡ -20^30 ≡² -24; v°3^30-16^10, 20^30-24
9	9	1.1	9	≫5^30-7^30 ↖ 9^25-24; ≡²0^00-9^10 ▭-15^15 ≡² -24; v°0^00-9^10, 15^15-24
10	9	1.6	10	↖ 0^00-9^30 ≫-10^20, 12^45-14^45 ↖-24; ≡²0^00-7^30 ▭-17^40 ≡² -18^45 ≡ -19^40 ≡² -24; v°0^00-7^30, 18^40-45, 20^30-24
11	0	5.2	12	*°12^45-24; ⊥³12^45-24; ↖ 0^00-24; ≡²0^00-24; v°0^00-2^30 v'-24
12	0	7.6	17	*°0^00-6^10; ⊥²'-0^00-5^10 ⊥17^10-20^30 ⊥'-24; ≡²0^00-24; v°0^00-24
13	0	4.0	26	*°0^00-5^15 ⚥°10^25...16^58 *°21^45-22^30 *'-24; ⊥² ↖ 0^00-24; ≡²0^00-13^00 ≡ -14^00 ≡² -24; v°0^00-13^00 16^00-24
14	0	4.7	30	*'0^00-2^30 *°4^50-8^40 12^50 14^20-16^50 17^50-24; ⊥²'-0^00-24; ↖ 0^00-7^30 ≫-9^30 ↖-24; ≡² v°0^00-24
15	0	1.0	33	*°0^00-7^20 10^10; ⊥²0^00-10^10; ↖ 0^00-24; ≡²0^00-10^50 ≡ -12^30 ≡² -23^30 ≡ ▭-24; v°0^00-24
16	8	0.1	34	⊥²7^00-24; ↖ 0^00-24; ≡ ▭ 0^00-7^15 ≡² -8^10 ▭-8^40 ≡ -21^20 ▭-24; v°0^00-8^10
17	8	•	32	⊥²'-0^00-18^30; ↖ 0^00-16^30 ≫-17^45; 18^30-24; ⊥²'-0^00-18^30; ▭ 0^00-24 ≡ 17^30-20^30; ⊌18^30-21^50 ⊌ 22^50-24
18	8	0.4	30	⊥°12^00-16^10 ⊥²-24; ≫0^00-12^20 ↖-24; ▭ 0^00-1^30 ≡ -13^20 ≡² -16^30 ≡ -17^40; 20^45-21^30 ≡² -21^20-24; ⊌ 0^00-5^30
19	0	2.8	31	*°8^40-11^30, 12^45-14^37, 20^40-24; ⊥²0^00-24; ↖ 0^00-24; ≡²0^00-20 ▭ 0^00-1^30 ≡² -24; v°2^10-24
20	0	2.5	34	*°0^00-8^40 13^10-15^50; ⊥²0^00-24; ↖ 0^00-24; ≡²0^00-20^10 ▭-22^20 ≡² -24; v°0^00-20^10, 22^20-24
21	0	3.6	35	⊥²0^00-8^20 ↖ 0^00-8^20 ≫-15^30 ↖-24; ≡²0^00-24; v°0^00-2^10, 17^30-24
22	0	2.0	36	⊥²9^30-24; ↖ 0^00-24; ≡²0^00-10^30 ≡ -11^25 ≡² -14^30 ≡ -15^40 ≡² 17^30-19^25 ≡ -20^10 ≡² -24; ▼°0^00-10^30, 11^25-14^30 v°18^25-19^25, 20^10-24
23	0	5.2	36	*°6^15-24; ⊥²0^00-24; ↖ 0^00-24; ≡²0^00-24; v°0^00-24
24	0	5.4	40	*°0^00-2^40 6^15-20^20 23^35; ⊥²0^00-24; ↖ 0^00-24; ≡²0^00-24; v°0^00-24
25	0	12.0	42	*°7^50-14^50, 15^50 16^50 17^50 21^20-24; ⊥²0^00-20^30 ⊥'-21^20 ⊥²-24; ↖ 0^00-20^30 ≫-21^20 ↖-24; ≡²0^00-24; v°0^00-1^30 ▼°-24
26	8	18.5	46	*°0^00-8^40, 10^40-11^15, 19^45-21^50 *'-22^15 *°-24; ⊥²0^00-9^30 ⊥'13^30-24; ↖ 0^00-8^30 ≫-9^30, 11^15-23^10 ↖-24; ≡²0^00-11^10 ≡ -11^40 ▭-13^10 ≡ -14^00 ≡² -24; ▼°0^00-11^10 v°14^00-24
27	0	14.6	52	*°0^00-20^20 *'-24; ⊥²0^00-24; ↖ 0^00-24; ≡²0^00-24; v°0^00-24
28	0	17.3	55	*'0^00-10 *°-24; ⊥²0^00-24; ↖ 0^00-24; v°0^00-24
29	0	11.8	62	*°-'0^00-24; ⊥²0^00-24; ↖ 0^00-24; ≡²0^00-24; v°0^00-24
30	8	4.9	67	*°0^00-8^20 9^35; ⊥²0^00-24; ↖ 0^00-24; ≡²0^00-9^45 ≡ -15^20 ▭ 9^45-15^20 ≡² -18^30 ≡ -22^20; v°0^00-9^45, 15^20-40 v'-19^30
31	9	0.0	67	⊥²0^00-8^05 ⊥'-12^20 ⊥°-24; ≡ 5^30-6^20 ▭ 0^00-6^20 ≡² -7^10 ≡ -8^05; 9^40-24; v°6^20-7^10
Σ	—	131.5	—	UWAGI.

Luty - Février

1	8	•	65	⊥°0^00-4^30; ≫0^00-4^30; ≡ 0^00-1^20 ▭ 6^40-24
2	8	3.1	65	⚥°15^48-18^50 *'19^45-21^55 ⚥°22^45-24; ≫19^20-24; ≡ 10^30-11^25 ≡² 13^25-24 ▭ 0^00-13^25; v°17^35-24
3	0	0.3	67	⚥°0^00-4^0 ≫0^00-4^20 ↖-13^30 ≫-16^10; ≡²0^00-1^45 ≡ -4^40 ≡² -6^15 ≡ 10^10 ≡² -17^15 ▭-24; v°0^00-1^45, 4^40-6^15 ≡ -10^00 ≡² -17^15 ▭-24; v°0^00-1^45, 4^40-6^15, 10^00-17^15
4	7	2.9	65	*°9^50...12^40, 23^50...24; ⊥²9^30-14^40 ⊥°23^50-24; ↖ 3^30-16^20 ≫-19^40; ▭ 0^00-9^30 ≡ 9^15-30 ≡² -12^40 ≡ -13^30 ≡² -19^40 ≡ -20^20 ≡² -24; v°9^30-24
5	0	12.2	68	*°0^00...9^00-11^50 *'-12^30 *°-21^30 *'-22^30 *°-24; ⊥°0^00-3^30 ⊥²-24; ≫0^20-3^30 ↖-24; ≡²0^00-24; v°0^00-24
6	0	0.2	74	*°-'0^00-6^00; ⊥²0^00-21^30; ↖ 0^00-21^30 ≫-22^10, 23^05-24; ≡²0^00-21^40 ≡ -23^30 ▭-24; v°0^00-21^40
7	0	2.1	74	*°10^00...12^30; ⊥'18^30-21^30 ⊥²-24; ≫0^00-8^30; 18^30-21^30 ↖-24; ▭ 0^00-5^30 ≡² -8^45 ≡ ▭-11^40 ≡² 13^45 ≡ ▭-16^30 ≡² 17^00 ≡ ▭-20^30 ≡² -24; v°6^10-8^05 ▼°12^30-13^45 v°16^30-17^00 ▼°20^30-24; ⊕ 14^45-16^00
8	0	0.0	75	⊥²-0^00-21^5; ↖ 0^00-10 ≫-21^5; ≡²0^00-3^0 ≡ -2^30 ▭-3^30 ≡² -7^45 ≡ ▭-12^20 ≡² -13^30 ≡ -21^20 ▭ 16^40-21^20; ▼°0^00-1^30, 3^30-7^45 v°12^20-13^30
9	9	0.0	75	*°8^10-45; ≫11^20-14^20 ↖-17^15 ≫-19^15 ↖-22^20 ≫-23^40; ≡ 2^30-6^40 ≡² -7^20 ≡ -9^10 ≡² -10^25 ▭-13^50 ≡² -15^35 ▭ ≡ -17^45 ≡² -20^25; v°6^40-7^20, 19^30-20^25
10	9	•	75	≫2^30-5^15
11	0	1.2	75	*°8^50 9^50 ⚥°10^50, 12^30 *°13^40 ⚥°15^50, 16^50; ⊥²10^50, 21^40 ⊥'-23^30 ⊥²-24; ≫4^30-8^30 ↖-21^40 ≫-23^30 ↖-24; ≡ 7^40-8^20 ≡² -13^40 ≡ -15^30 ≡² -16^40 ≡ -16^50 ≡² -18^20 ≡ -23^30; v°8^20-
12	0	8.8	78	*°3^50-7^30 *°-15^30 ⚥'-20^30 ⚥'-23^30 *'-24; ⊥²0^00-24; ↖ 0^00-24; ≡ 0^40-1^20 ≡² -24; v°0^40-24
13	0	6.2	83	*'0^00-1^30 *°12^10, 15^40-16^35, 7^40, 19^20...24; ⊥²0^00-6^20 ⊥'-12^30 ⊥²-15^30, 17^10-21^30 ⊥'-24; ↖ 0^00-6^20 ≫-12^30, 20^30-24; ≡²0^00-6^30 ≡° -8^40 ≡² -14^10 ≡ -15^30 ≡² -17^40 ≡ -19^10 ≡² -24; v°
14	0	19.2	90	*°0^00...3^30-7^40 9^00-12^30 *'-15^30 *°-21^30 *'-24; ⊥²0^00-22^30 ⊥²-24; ≫0^00-22^30 ↖-24; ≡²0^00-7^30 ≡ -8^45 ≡² -24; v°0^00-7^30, 8^45-24
15	0	13.5	120	*'0^00-15^30 *°-20^10, 21^15; ⊥²'-0^00-24; ↖ 0^00-20^40 ≫-24; ≡²0^00-20^30 ≡ -21^20; v°0^00-20^30
16	0	1.8	125	*°2^10-6^15 *°-7^40; ⊥'0^00-1^30 ⊥²-24; ≫-↖ 0^00-24; ≡² 2^10-24; v°2^10-24 [11.11: 13^40, 15^30-23^30; (⚥) 10^50-12^30
17	0	10.8	127	*²6^47 7^13 ⚥²-7^25 *²7^50 11^30 *'...13^30, 17^50...22^30; ⊥²0^00-24; ↖ 0^00-24; ≡²0^00-24; v°0^00-24
18	0	12.0	135	*'-4^50...16^40 *°23^50...24; ⊥²0^00-24; ↖ 0^00-24; ≡²0^00-16^40 ≡ -17^20 ≡² -19^30 ≡ -22^20 ≡² -24; v°0^00-24 [13.11: 0^00-14^10, 15^30-17^40, 19^10-24
19	0	10.2	145	*°-'0^00...6^30-21^10; ⊥²0^00-24; ↖ 0^00-24; ≡²0^00-24; v°0^00-24
20	1	4.5	150	*°18^50-24; ⊥²0^00-24; ↖ 0^00-24; ≡²0^00-12^20 ≡ -12^35 ≡² -13^15 ≡ -13^25 14^40-16^30 ≡² -24; v°0^00-12^20, 12^35-13^15, 16^30-24
21	0	10.6	152	*°0^00-7^48 11^50-20^30 *'-24; ⊥²0^00-24; ↖ 0^00-24; ≡²0^00-7^48 ≡ -8^10 ≡² -24; v°0^00-7^48, 8^10-24
22	0	7.6	160	*'0^00-11^15 *°-19^40 *'-24; ⊥²0^00-19^30 ⊥²-24; ↖ 0^00-19^30 ≫-24; ≡²0^00-24; v°0^00-24
23	8	9.5	170	*'0^00-5^55 *°9^50 10^40, 15^50...16^20-17^30 *'-24; ⊥'²0^00-24; ≫0^00-9^30 ↖-10^20 ≫-18^30 ↖-24; ≡²0^00-5^50 ≡ ▭-9^30 ≡² -10^20 ≡ ▭-14^40 ≡² -24; v°0^00-5^50, 9^30-24
24	0	18.5	180	*'0^00-22^20 *°-24; ⊥²0^00-24; ↖ 0^00-24; ≡²0^00-24; v°0^00-24
25	0	1.9	200	*°0^00-6^20 10^40, 12^50 14^40; ⊥²0^00-24; ↖ 0^00-10^30 ≫-11^20 ↖ 18^40-24; ≡²0^00-6^20 ≡ -9^40 ≡² -10^30 ≡ -12^20 ≡² -13^30 ≡ ▭-23^40 ≡² -24; v°0^00-6^20, 9^40-10^30, 12^20-13^30, 23^40-24
26	0	1.9	200	*°0^50...1^40; ⊥²0^00-20 ⊥²-3^30 ⊥'-24; ≫0^00-20 ↖-3^30 ≫-24; ≡²0^00-15^10 ≡ -15^50 ≡² -24; v°0^00-15^10, 15^50-24
27	0	5.1	200	*°9^50...12^20 *'-13^20, 17^35 *°18^20 *'-21^30 *°-22^20 *°...24; ⊥'0^00-4^10 ⊥²-13^20 ⊥'-24; ≫0^00-4^10 ↖-13^20 ≫-24; ⊥'0^00-4^10 ⊥²-13^20 ⊥'-24; ≡²0^00-6^30 ≡ -9^30 ≡² -24; v°0^00-6^30 v'-24
28	0	0.3	202	*°0^00...0^40-5^40; ⊥'0^00-4^30 ⊥°-14^30; ≫0^00-4^30; ≡'0^00-14^10 ≡ -14^45 ▭ 14^10-24 ≡ 21^00-22^30; v°0^00-6^30 v'-11^30 v°-14^10
29				
30				
31				
Σ	—	164.4	—	UWAGI.

Śnieżka φ=50°44' λ=15°44' Marzec - Mars 1962

DNI	CIŚNIENIE P=700+ I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	123.8	123.8	122.8	123.5	-7.5	-6.0	-7.6	-7.2	-5.9	-8.0	90	94	97	90	0.3	0.2	0.4	0.3	10✳≡	10✳≡	9	E 3	E 1	E 2
2	121.3	120.1	120.0	120.5	-7.8	-5.4	-8.0	-7.3	-4.0	-8.4	93	92	96	94	0.2	0.3	0.1	0.2	10✳	10≡	10✳	SSW 4	NW 2	W 6
3	119.1	119.0	118.7	118.9	-9.0	-6.7	-8.1	-8.5	-7.8	-9.8	89	92	92	91	0.4	0.3	0.2	0.3	10✳≡	10≡	10✳≡	SW 4	SW 8	SW 8
4	114.4	113.7	113.3	113.8	-7.4	-3.2	-2.4	-3.8	-2.2	-8.6	93	97	98	96	0.2	0.1	0.1	0.1	10✳≡	9	10✳≡	SW 14	WSW15	SW 10
5	114.1	115.2	115.2	114.8	-0.8	0.4	1.1	0.4	3.6	-3.9	99	100	96	98	0.0	0.0	0.2	0.1	10✳≡	7⊙	10●✳	SW 12	SW 14	NNW 5
6	115.0	119.2	126.9	120.4	-7.3	-10.4	-12.2	-10.5	1.1	-12.6	90	90	89	90	0.3	0.3	0.3	0.3	10✳≡	10✳≡	10✳≡	N 16	WNW18	WNW12
7	130.2	132.7	136.3	133.1	-15.0	-11.4	-11.4	-12.3	-10.7	-15.6	87	90	90	89	0.2	0.3	0.3	0.3	10✳≡	10✳≡	10✳≡	WNW12	WNW10	WNW11
8	137.0	139.6	138.6	138.4	-12.8	-9.3	-7.6	-9.3	-6.0	-13.3	81	73	51	68	0.4	0.8	1.7	1.0	0⊙	0⊙	2	WNW12	C 0	SE 10
9	134.4	131.3	128.6	131.4	-8.1	-6.0	-10.4	-8.7	-5.9	-10.9	30	41	81	51	2.3	2.3	0.5	1.7	9⊙	5⊙	3	SSW25	S 35	SSW35
10	127.7	128.4	128.3	128.1	-9.1	2.0	-0.4	-2.0	2.0	-11.7	88	96	100	95	0.4	0.3	0.0	0.2	9⊙	9	6	SW 16	NNE12	WSW12
11	128.0	127.5	124.9	126.8	-0.8	1.4	-0.5	-0.1	3.9	-5.6	99	83	100	94	0.0	1.2	0.0	0.4	8	8	10✳≡	SW 6	SW 1	NE 4
12	120.6	118.3	115.9	118.3	-2.2	-2.0	-8.6	-5.4	-0.5	-8.7	98	98	92	96	0.1	0.1	0.3	0.2	10✳≡	10✳≡	10✳≡	N 4	N 4	NNW14
13	118.3	122.1	124.1	121.5	-14.8	-14.4	-16.2	-15.4	-8.4	-16.6	74	78	86	79	0.5	0.4	0.2	0.4	10✳≡	9✳≡	10✳≡	NW 25	NW 16	NW 10
14	127.2	130.0	130.3	129.2	-16.8	-12.9	-14.7	-14.8	-12.6	-17.6	85	81	87	84	0.2	0.4	0.3	0.3	9	6⊙	0	NW 12	NW 8	SW 10
15	129.1	129.3	129.9	129.4	-16.1	-12.6	-15.0	-14.7	-11.8	-16.8	86	77	69	77	0.2	0.5	0.6	0.4	5	9	9	NW 1	NW 1	NW 9
16	129.4	130.0	129.4	129.6	-16.4	-15.0	-16.6	-16.2	-14.6	-17.3	85	87	85	85	0.2	0.2	0.2	0.2	10✳≡	10✳≡	9✳	N 18	N 18	N 16
17	127.2	126.2	126.9	126.8	-17.2	-12.6	-12.9	-13.9	-12.0	-17.7	85	85	84	85	0.2	0.4	0.4	0.3	10	10✳≡	10✳≡	N 20	N 20	N 20
18	128.2	130.8	131.3	130.1	-14.0	-9.8	-11.2	-11.6	-8.1	-14.6	83	91	90	88	0.3	0.3	0.3	0.3	10✳≡	10✳≡	10 ≡	N 20	NNW12	NNW 8
19	131.8	132.2	132.0	132.0	-11.6	-7.2	-10.8	-10.1	-5.6	-14.1	89	90	87	89	0.3	0.3	0.4	0.3	10✳≡	8✳	10✳	NNW 4	NW 2	NW 1
20	131.3	131.5	130.0	130.9	-12.1	-10.6	-11.2	-11.3	-10.1	-12.9	89	90	90	90	0.3	0.3	0.3	0.3	10✳≡	9✳	10✳≡	SW 2	SW 8	SW 14
21	126.7	126.7	125.4	126.3	-13.4	-10.4	-11.3	-11.6	-10.1	-13.7	88	90	86	88	0.3	0.3	0.4	0.3	10✳≡	9✳	10 ≡	SW 16	SE 8	ENE 8
22	122.1	121.6	120.8	121.5	-13.4	-10.6	-12.8	-12.4	-10.2	-13.9	88	90	88	89	0.3	0.3	0.3	0.3	10	9	10 ≡	NE 14	N 16	WNW20
23	119.4	120.9	123.0	121.1	-13.6	-11.2	-11.8	-12.1	-10.4	-14.1	88	90	89	89	0.3	0.3	0.3	0.3	10≡	10≡	10✳≡	N 18	N 18	N 18
24	125.7	129.9	132.4	129.3	-12.8	-6.2	-10.0	-9.8	-3.9	-13.2	88	94	84	89	0.3	0.2	0.4	0.3	10✳≡	8⊙	0	N 10	NNW 4	NNW 6
25	133.5	133.6	132.4	133.2	-10.8	-7.4	-9.6	-9.4	-5.2	-11.7	90	93	91	91	0.3	0.2	0.3	0.3	9	10✳≡	10✳	NW 6	NNW 1	NNW 3
26	130.2	128.6	126.2	128.3	-11.2	-5.5	-8.4	-8.4	-3.7	-11.8	90	85	69	81	0.3	0.6	1.0	0.6	10✳	2	0	S 4	S 2	W 7
27	122.5	120.6	120.5	121.2	-7.7	-6.2	-5.8	-6.4	-5.7	-9.6	76	94	95	88	0.8	0.2	0.2	0.4	5	10✳≡	10≡	W 8	SW 14	SW 12
28	120.0	120.7	123.5	121.4	-6.4	-5.4	-6.6	-6.2	-5.0	-7.4	94	95	94	94	0.2	0.2	0.2	0.2	10✳≡	10✳≡	9✳	WSW 8	W 14	W 16
29	123.9	121.0	117.1	120.7	-7.9	-6.0	-3.4	-5.2	-3.0	-8.5	93	89	97	93	0.2	0.4	0.2	0.3	9	10≡	10≡	WNW13	SW 18	SW 23
30	116.1	117.7	114.2	116.0	-0.4	0.2	0.8	0.4	1.6	-3.6	100	100	100	100	0.0	0.0	0.0	0.0	10≡	10✳≡	10●≡	SW 22	SW 25	SW 25
31	110.9	115.3	116.1	114.1	1.6	1.8	-4.6	-1.4	2.0	-5.1	100	100	96	99	0.0	0.0	0.2	0.1	10●≡	10≡	10✳≡	SW 28	WSW16	W 12
M	124.5	125.1	125.0	124.9	-9.8	-7.1	-8.7	-8.6	-5.5	-11.5	87	89	88	88	0.3	0.4	0.3	0.3	9.1	8.6	8.3	12.2	11.0	11.8

Kwiecień - Avril

1	121.5	124.1	125.6	123.7	-6.8	-6.4	-5.8	-6.2	-5.1	-7.5	94	94	95	94	0.2	0.2	0.2	0.2	10✳≡	9✳	10≡	WSW18	W 20	WSW23
2	125.7	126.5	130.5	127.6	-6.0	-4.8	-5.2	-5.3	-4.7	-6.4	94	95	95	95	0.2	0.2	0.2	0.2	10≡	10≡	10≡	WSW20	WSW25	W 20
3	128.5	127.3	126.7	127.5	-4.4	-1.4	-2.2	-2.6	-0.3	-5.9	96	97	98	97	0.2	0.2	0.1	0.2	10≡	7⊙	8	WSW20	SW 20	SW 20
4	120.7	121.3	119.8	119.6	-2.9	-1.0	-2.4	-2.2	-0.8	-3.3	95	99	98	97	0.2	0.1	0.1	0.1	9⊙	9	10✳≡	SW 22	SW 16	W 14
5	109.5	109.9	111.9	110.4	-3.2	-3.0	-2.8	-3.0	-2.4	-3.6	97	97	97	97	0.1	0.1	0.1	0.1	8	10≡	10≡	WSW12	WSW12	WSW14
6	114.1	118.1	122.1	118.1	-4.8	-3.0	-3.6	-3.8	-2.8	-5.6	95	97	99	97	0.2	0.1	0.1	0.1	10≡	9⊙	10✳≡	WSW 9	NW 4	NW 14
7	126.8	128.8	126.0	127.2	-8.4	-6.8	-5.0	-6.3	-3.4	-6.9	92	88	95	92	0.3	0.4	0.2	0.3	10✳≡	7⊙	10✳≡	NW 20	NW 18	NW 25
8	127.0	125.5	125.6	126.0	-2.2	-1.1	-0.8	-1.2	-0.6	-5.3	98	99	99	99	0.1	0.1	0.0	0.1	10✳≡	10≡	10✳≡	W 20	WSW20	WSW18
9	126.6	130.3	132.3	129.7	-4.4	-3.3	-4.0	-3.9	-0.8	-4.6	96	97	99	97	0.2	0.1	0.1	0.1	9	10△✳	8	WSW20	SW 10	WSW12
10	135.4	137.0	138.4	136.9	-5.7	-3.4	-4.4	-4.5	-3.0	-6.5	95	97	96	96	0.2	0.2	0.2	0.2	6	9	0	NW 3	W 3	W 5
11	137.8	137.8	138.0	137.9	-5.8	-4.2	-2.6	-3.8	-2.6	-7.1	87	84	98	90	0.5	0.7	0.1	0.4	8	9	10	N 14	NNW14	ESE 8
12	137.5	137.0	136.1	136.9	-2.6	1.0	-0.4	-0.6	1.3	-4.6	83	79	90	84	0.9	1.4	0.6	1.0	1	8⊙	6	N 10	N 3	N 6
13	133.4	131.3	130.5	131.7	-1.4	-4.2	-6.2	-4.5	-0.4	-7.1	99	96	94	96	0.1	0.2	0.2	0.2	10✳	10✳≡	9✳	SW 6	N 12	NW 12
14	130.9	133.4	135.5	133.3	-6.8	-4.8	-4.7	-5.2	-4.1	-7.5	94	95	96	95	0.2	0.2	0.2	0.2	10✳≡	10✳≡	10✳≡	N 12	N 10	N 12
15	136.0	136.9	137.5	136.8	-2.6	-1.6	-0.2	-1.2	-0.1	-5.2	98	98	100	99	0.1	0.1	0.0	0.1	10≡	10≡	10≡	N 20	NE 14	NE 12
16	136.2	135.8	138.1	136.7	1.2	3.2	-0.2	1.0	3.6	-2.7	100	100	72	91	0.0	0.0	1.7	0.6	10≡	10●≡	4	SE 6	SSE12	SW 8
17	136.6	135.3	134.0	135.3	1.6	4.2	2.4	2.6	4.3	-0.3	82	85	96	88	1.2	1.2	0.3	0.9	9	9	10	SW 28	SW 30	SW 28
18	134.8	136.2	135.9	135.6	4.2	6.5	5.8	5.6	8.0	1.8	76	81	78	78	1.9	1.8	2.0	1.9	9⊙	8⊙	10	SW 20	SSW18	SW 28
19	137.7	139.8	141.2	139.6	8.7	10.1	9.6	9.5	11.2	4.2	46	37	65	49	6.0	8.3	4.2	6.2	10	7	9	SW 12	SW 8	SSW 8
20	141.0	141.5	139.9	140.8	8.4	10.9	9.3	9.5	11.5	7.6	61	57	64	61	4.3	5.6	4.1	4.7	6	7⊙	2	S 8	SSW10	S 14
21	141.4	142.7	143.0	142.4	9.0	12.3	9.4	10.0	14.3	6.8	70	65	85	73	3.5	5.0	1.8	3.4	1⊙	4⊙	8	SW 6	SSW 4	N 6
22	141.6	142.3	142.8	142.2	8.2	10.9	10.6	10.1	12.6	8.1	40	47	45	44	6.6	6.9	7.1	6.9	7⊙	4⊙	8	SSW20	S 12	S 12
23	142.6	144.2	144.5	143.8	9.0	13.0	11.9	11.4	14.4	8.7	52	40	51	48	5.5	9.0	6.7	7.1	0⊙	0⊙	0	S 10	S 8	S 10
24	146.6	148.0	148.3	147.6	12.0	13.9	11.5	12.2	14.8	8.7	42	46	49	46	8.1	8.7	6.9	7.9	0⊙	4⊙	0	SE 6	SE 6	SE 10
25	148.5	149.2	148.2	148.6	10.9	13.1	10.6	11.4	15.1	9.4	49	47	53	50	6.7	8.3	6.0	7.0	0⊙	5⊙	2	E 8	SSE 8	SE 9
26	146.3	143.6	138.2	142.7	10.9	9.6	5.8	8.0	14.4	4.5	48	79	92	73	6.8	2.5	0.7	3.3	1⊙	8	10≡	W 1	W 4	NW 3
27	131.9	131.7	131.7	131.8	0.2	-2.2	-2.0	-1.5	6.1	-3.6	100	98	98	99	0.0	0.1	0.1	0.1	10●≡	10✳≡	10≡	N 16	NNE10	N 15
28	121.9	123.9	124.7	123.5	-4.8	-3.5	-5.0	-4.6	-1.8	-5.7	98	94	95	96	0.1	0.3	0.2	0.2	10△≡	10△≡	10✳≡	W 16	NNW14	N 14
29	125.7	126.6	125.6	126.0	-5.8	-2.4	-5.6	-4.8	-2.1	-6.4	95	98	95	96	0.2	0.1	0.2	0.2	10✳≡	6	4	N 8	NW 5	WNW12
30	123.8	125.5	128.6	126.0	-5.8	-5.0	-8.0	-6.7	-4.7	-8.3	95	95	93	94	0.2	0.2	0.2	0.2	10✳≡	10△≡	10✳≡	W 4	NNW 4	N 10
31																								
M	132.3	133.0	133.3	132.9	0.0	1.6	0.5	0.6	3.1	-1.9	82	83	86	84	1.8	2.1	1.5	1.8	7.5	8.0	7.6	13.1	11.8	13.4

Śnieżka $H_s = 1603m$ $H_b = 1610,6m$ Marzec - Mars 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	0	0.5	200	✱°5^00..8^40, 9^35..14^40, 21^45..24; ɱ 0^00-5^30 == 1^30-5^30 ≡²-14^40 ==-19^20 ɱ -24; V°5^30-14^40
2	0	0.7	200	✱°0^00-7^10, 8^50..9^30 ▲°15^50-16^30 ✱°-18^00, 20^50-24; ɱ 0^00-4^30 ≡²-5^10 ɱ -12^20 ==-12^20 ≡²-13^20 == ɱ -14^20 ≡²-18^00 == ɱ -21^30 ≡²-24; V°16^30-18^00, 23^00-24
3	0	2.1	195	✱°0^00-11^40, 16^40..24; ✛'14^00-20^30 ✛°-21^10 ✛'-24; ≫14^00-20^30, 21^10-24; ≡²0^00-24; V°0^00-4^30 V'-9^00 V°-24
4	7	2.5	196	✱°0^00-7^10, 10^50..12^40, 16^50..17^20-19^30 ✱'-24; ✛'0^00-12^40 ✛²-18^20 ✛°-20^30 ✛'-24; ≫0^00-15^30 ⫸-18^20 ≫-24; ≡²0^00-7^50 ==-9^30 ≡²-12^40 == ɱ -15^30 ≡²-24; V°0^00-7^50, 9^30-12^40, 15^30-24
5	8	9.9	185	✱'0^00-2^40, 4^50..7^50 ✱°19^55-21^30 ✱°23^50-24; ✛'0^00-30 ✛°-2^40 ✛²4^30-5^20 ✛'-9^30 ✛°23^50-24; ≫0^00-1^30, 3^30-4^30 ⫸-5^20 ≫-16^30, 23^10-24; ≡²0^00-10^20 ==-13^25 ɱ 10^20-21^10 ≡²-24; V°0^00-7^00 V°-9^30, 22^30-24
6	0	15.6	175	✱°0^00-5^00 ✱'-8^30..10^20-24; ✛°0^00-1^30 ✛'-5^00 ✛²-20^20 ✛'-24; ≡²0^00-24; V°0^00-1^30 V°-4^00 V'-9^20 V°-24
7	0	6.9	185	✱'0^00-1^30 ✱°-4^20 ✱'-17^40 ✱°-24; ✛'0^00-24; ≫0^00-24; ≡²0^00-24; V°0^00-24
8	8	•	180	✱°0^00-1^30 ✱'-4^40; ✛'0^00-4^40, 7^10-10^00; ≫0^00-10^00, 19^30-24; ≡²0^00-4^40 ɱ -17^50; V°0^00-4^40
9	9	•	170	✛²5^00-24; ⫸3^20-24
10	8	•	165	✛²0^00-6^30 ✛'-7^10; ⫸0^00-7^10 ≫16^30-24; == 3^00-11^30 ɱ 8^20-15^30 == 21^40-24
11	8	3.2	155	✱°20^50-24; ≫0^00-3^20; ≡²0^20-1^30 ==-7^20 ɱ 6^20-20^20 == 19^45-20^20 ≡²-24; V°0^20-1^30 V°21^30-24; ⊕ 14^50-15^45
12	0	12.0	150	✱°0^00-16^30 ✱'-24; ✛⁰⁻¹16^30-21^20 ✛²-24; ≫16^30-21^20 ⫸-24; ≡²0^00-24; V°0^00-13^20 V°-24
13	7	5.4	156	✱'0^00-12^30 ✱°..14^10 ✱'-24; ✛²0^00-14^30 ✛'-24; ≡²0^00-12^25 ==-16^10 ≡²-24; V°0^00-12^25, 16^10-24
14	8	0.0	160	✱'0^00-1^40, 3^10-6^20, 7^10-9^45 ✱°-11^20; ✛'0^00-3^30 ✛²-6^30 ✛'-8^30 ✛°-14^00, 19^30-24; ≡²0^00-1^40 ==-3^10 ≡²-6^35 ==-11^05; V°0^00-1^40, 3^10-6^35
15	8	1.2	160	✛°0^00-4^30; ≫0^00-4^30, 21^30-24; ⊕ 7^50-9^40 ⊕ -24
16	0	0.8	155	✱'6^10-13^30 ✱°-16^40, 19^50..22^50; ✛'1^40-5^30 ✛²-24; ≫0^00-5^30 ⫸-24; ≡²1^40-13^30 ==-14^20; V°1^40-13^30; ⊕ 0^00-1^40
17	0	4.6	155	✱'8^45-12^30..18^30 ✱°..24; ✛²0^00-24; ⫸0^00-24; == 4^20-8^20 ≡²-24; V°8^30-24
18	0	2.2	160	✱°0^00..3^30 ✱'..11^20 ✱°..16^30-21^30..24; ✛²0^00-10^30 ✛'-14^20 ✛°-23^40; ⫸0^00-10^30 ≫-14^20; ≡²0^00-21^30 ==-23^40; V°0^00-6^00 V'-9^20 V°-21^30
19	6	3.1	162	✱°1^50..6^20-7^30..8^15 ✱°-10^22 ✱'-11^32 ✱⁰⁻¹11^45-13^30 ✱²16^10 ✱'-17^15 ✱°..18^08 ✱⁰⁻¹-20^00 ✱°..24; == 1^30-5^20 ≡²-8^15 ==-18^45 = 10^30-18^45 ≡²-19^40 ==-20^30 = 19^40-23^30; V°5^20-8^15
20	7	2.0	170	✱°0^00..8^15 ✱²-8^40 ✱°-10^30..15^40, 16^50..17^40, 19^30..21^20-24; ✛°14^20-15^30 ✛'-21^20 ✛²-24; ≫14^20-21^20 ⫸-24; ≡²5^10-10^30 ==-13^20 ≡²-14^20 ==-17^40, 19^30-50 ≡²-24; V°5^10-10^30, 13^30-14^20, 19^50-24
21	7	1.0	172	✱°0^00-2^20..8^30 ✱°11^50-16^30; ✛²0^00-9^30 ✛'-12^30 ✛°-13^15, 23^30-24; ≡²0^00-8^20 == ɱ -14^45 = 13^30-14^45 ≡²-21^00 ==-23^30 ɱ 21^00-24; V°0^00-8^20, 16^30-21^00
22	7	4.4	170	✛'0^00-9^30 ✛²-24; ≫0^00-9^30 ⫸-24; ɱ 0^00-5^30 == 4^30-5^30 ≡²-8^30 ==-13^20 ≡²-14^30 ==-16^20 ≡²-24; V'5^50-8^30 V°13^20-14^20, 16^20-24
23	0	3.8	170	✱°15^40..24; ✛²0^00-6^20 ✛'-6^40 ✛²-24; ⫸0^00-6^20 ≫-6^40 ⫸-24; ≡²0^00-24; V°0^00-24
24	8	0.0	168	✱°0^00-8^40; ✛²0^00-2^30 ✛'-8^40 ✛°-11^20; ≡²0^00-9^20 ==-11^30; V°0^00-9^20
25	0	0.8	162	✱'9^20-40 ✱⁰⁻¹-11^35, 11^40-17^15..19^40 ✱°20^45..21^10-24; == 3^30-4^20 ≡²-6^30 ==-7^20 ≡²-8^00 ==-9^10 ≡²-10^30 ==-10^45 ≡²-19^30 ==-22^20, 23^15-40; V°4^20-6^30, 7^20-8^00, 9^10-10^30
26	8	0.0	160	✱°0^00-2^30..3^10, 6^50-7^30..8^40; ≫23^40-24; ≡²3^30-4^05 ==-4^20, 5^10-6^30 =-7^40; V°3^30-4^05; ⊕ 15^30-16^10
27	0	1.6	158	✱°12^15..14^40, 15^50..18^40; ✛'12^15-14^40 ✛²15^30-18^20; ≫0^00-2^30, 5^15-6^30, 8^30-15^30 ⫸-18^20 ≫-24; ≡'12^30-24; V°12^30-24
28	0	4.4	152	✱'1^50-2^30 ✱'..3^20 ✱°..14^05 ✱'-16^05 ✱°-20^05 ✱'-20^30 ✱°-22^40..24; ✛'1^50-2^30 ✛²-4^20 ✛'-6^30 ✛°-11^30 ✛'-14^40 ✛²-22^10 ✛'-24; ≫0^00-2^30 ⫸-4^20 ≫-6^30, 11^30-14^40 ⫸-22^10 ≫-24; ≡²0^00-13^10 ==-14^05 ≡²-16^05 ==-16^50 ≡²-19^00 ==-
29	0	3.0	150	✱°0^00..2^40..7^45..8^50 ▲18^48-19^30 ✱°-24; ✛'0^00-15^45 ✛²-24; ≫0^00-11^30 ⫸-24; ≡²0^00-45, 2^40-4^45 ==-5^30, 6^30-7^40 ≡²-24; V°0^00-45, 2^40-4^45, 7^40-14^30 V²-23^15 V²-24
30	0	20.1	145	✱°0^00-1^50 ⩫²3^45-4^30 •11^40-12^42 ✱°-14^10 •°-16^05 •'-18^30 •°..19^20-20^30 •'-24; ✛²0^00-4^30; ⫸0^00-24; ≡²0^00-24; V²0^00-3^45 V°4^30-11^40; ∾²3^45-4^30 ∾°-12^30
31	0	15.8	121	•'0^00-1^40 •°-12^30..14^40 •-15^40 ✱°16^50-18^20 ✱°-19^30 ✱'-20^10 ✱'-21^30 ✱°..23^40; ✛'18^20-24; ⫸0^00-13^20 ≫-17^20, 18^20-24; ≡²0^00-15^40 ==-15^50 ≡²-22^20 ==-24; V°18^20-23^40; ☇ 19^30-20^10
Σ	—	127.6	—	UWAGI: [28.III: 19^40 ≡²-20^30 ==-21^20 ≡²-22^30 ==-22^50 ≡²-23^40-24; V°0^00-13^10, 14^05-16^05, 16^50-19^00, 19^40-20^30, 21^20-22^30, 23^30-24

Kwiecień - Avril

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	8	2.6	98	✱°3^50..18^15; ✛'0^00-4^30 ✛²-24; ≫0^00-4^30 ⫸-24; == 0^00-30, 2^30-3^30 ≡²-7^30 ==-8^20 ≡²-12^40 ==-13^30 ≡²-17^10 ==-19^30 ≡²-23^40 ==-24; V°3^30-7^30, 8^20-12^40, 13^30-17^10, 19^30-23^40
2	0	4.7	100	✱°7^40..10^30 ✱'..12^20-14^20 ✱°..16^40, 19^50..20^40; ✛²0^00-14^20 ✛'-19^30 ✛²-24; ⫸0^00-14^20 ≫-19^30 ⫸-24; == 0^00-2^40 ≡²-14^20 ==-15^40 ≡²-16^40 ==-19^30 ≡²-21^40 ==-23^30 ≡²-24; V°2^40-14^20, 15^40-16^40, 19^30-
3	8	0.0	102	✛°0^00-15^30; ⫸0^00-24; ≡²0^00-7^40 ==-12^30, 21^30-22^00 ≡²-24; V°0^00-7^40, 22^00-24 [2.IV: 21^40, 23^30-24
4	7	1.5	100	✱°14^50..16^20 ✱'..18^30 ✱°-23^40; ✛²15^40-17^20 ✛'-24; ⫸0^00-14^20 ≫-15^40 ⫸-17^20 ≫-24; ≡²0^00-1^50 ==-5^30, 9^40-11^30 ≡²-12^20 ==-14^30 ≡²-24; V°0^00-1^50, 11^30-12^20, 14^30-24
5	0	0.2	95	✛'0^00-1^30; ≫0^00-24; ≡²0^00-6^30 ==-7^20 ≡²-15^30 ==-18^40 ≡²19^50 ==-20^25 ≡²-22^30 ==-23^10 ≡²-24; V°0^00-6^30, 7^20-15^30, 18^40-19^50, 20^25-22^30, 23^10-24
6	8	19.8	90	✱°13^45-16^30 ✱°-21^00..24; ✛°17^30-19^30 ✛'-24; ≫0^00-6^10, 19^30-22^15 ⫸-24; ≡²0^00-8^45 ==-16^45 ≡²-24; V°0^00-8^45, 17^30-24
7	8	5.6	95	✱°0^00..1^30-3^30 ▲'3^50-4^30 ▲°-5^05 ✱°6^00-12^40 ✱'13^40-14^10, 14^30-15^15 ✱°16^40..17^10-24; ✛'0^00-6^20 ✛²-24; ⫸0^00-24; ≡²0^00-10^10 ==-12^40, 14^30-16^40 ≡²-24; V°0^00-3^30 V'-10^10 V°16^40-24
8	0	1.5	98	✱°0^00-7^20, 11^40, 19^50..20^30-24; ✛²0^00-24; ⫸0^00-24; ≡²0^00-16^30 ==-19^30 ≡²-24; V°0^00-16^30, 19^30-24
9	0	0.2	94	✱°0^00-1^50 ▲°12^45-14^40 ▲⁰⁻¹-15^30 ✱⁰⁻¹16^57-18^00 ▲⁰⁻¹-18^25; ✛²0^00-9^30 ✛'-12^15 ✛°-19^00 ✛'-20^30 ✛°-22^30; ⫸0^00-11^30 ≫-14^30, 17^45-22^30; ≡²0^00-2^20 ==-8^30 ≡²-10^25 ==-11^40 ≡²-14^45 ==-15^30;
10	7	•	95	== 0^30-1^10, 3^30-5^30, 6^30-7^40 ɱ 6^30-13^30 == 10^30-11^15, 12^20-13^30 ≡²-16^45 ==-17^40 ≡²-18^30 ==-19^15; ⊔'21^30-24
11	7	5.9	88	✱°14^40..16^20 ✱'..19^40; ✛°14^40-19^40; ≫1^40-9^30 ⫸-12^20 ≫-19^40; ≡²16^30-21^30 ==-22^20; ⊔'0^00-8^30 V°16^30-21^30
12	8	0.0	88	≫0^30-8^10; ≡²21^20-22^40 ==-23^30; ⊕ 19^20-23^40 [9.IV: 17^40-18^05 ≡²19^30 ==-22^00 ≡²-23^30; V°0^00-2^30, 9^00-10^25, 12^00-14^45, 18^05-19^30, 22^00-23^30
13	0	24.4	80	✱°6^50-7^10 ✱²-8^20 ✱'-10^30 ✱°-11^20..12^40-17^30 ✱'-20^20 ✱°..24; ✛°9^30-13^20 ✛'-16^20 ✛²-18^30 ✛'-21^30 ✛°-24; ⫸3^40-6^30 ≫11^20-16^20 ⫸-18^30 ≫-24; == 4^40-5^15 ≡²-20^20 ==-22^30 ≡²-24; V°
14	0	8.8	95	✱°0^00..1^30-4^20 ✱'-7^30 ✱°-10^00, 12^40-21^35; ✛°0^00-20 ✛'-14^10 ✛°-16^30 ✛'-24; ≫0^00-14^10, 16^30-24; ≡²0^00-24; V°0^00-24 [13.IV: 6^30-20^20, 22^30-24
15	0	2.8	98	✛'0^00-4^30 ✛²-9^20 ✛'-21^30 ✛°-21^50; ≫0^00-4^30 ⫸-9^20 ≫-24; ≡²0^00-24; V°0^00-9^30 V°-21^30
16	0	1.6	90	•7^10-14^27 ▲'-14^42 •-15^54 ▲'-16^12 ✱'15^53-16^12 ✱°-16^15 ▲'-17^40; ☈°15^57-16^40 S-N; ≫0^00-6^10, 10^30-14^15 ⫸14^30-19^40 ≫-20^10; ≡²0^00-16^20 ==-18^30; V°16^30-18^30; ∾16^30-18^00; (☇)⁰⁻¹14^45
17	8	•	80	⫸1^10-24; == 14^15-15^50 ≡²-19^20 ==-23^35 ≡²-24; ⊕ 1^10-3^30 [16.IV: 15^15, 15^50..18^10; ⊕ 21^30-22^05
18	8	•	70	⫸0^00-24; ≡²0^00-5^25 ==-6^15
19	8	•	55	⫸0^00-6^30 ≫-12^20, 18^30-19^20
20	7	•	45	≫6^30-8^30, 11^50-22^20 ⫸-24; ⊕ 10^50-16^30 ⊍ 21^50-22^30
21	8	•	35	⫸0^00-1^20 ≫-3^30, 23^20-24; ⊕ 14^20-15^30
22	8	•	30	≫0^00-1^30 ⫸-12^30 ≫-15^30, 19^30-24; ⊕ 6^30-40
23	9	•	25	≫0^00-10^30, 19^40-24
24	9	•	20	≫0^00-1^15, 18^30-22^20
25	8	•	15	≫21^50-23^30
26	7	7.8	pł.	✱°11^00-11 ✱'12^30-50 ✱°-13^30 ▲✱°-14^15 ✱°-16^10 ✱'19^20-20^20, 22^20-24; ☈11^50-16^50 W-ENE ☈¹⁻⁰19^20-20^30-21^50 NNW-EWE ⫸13^30-15^30 ≫-19^20, 22^30-24; ≡²16^10-24; ☇ 19^20-21^50
27	0	6.1	pł.	•0^00-30 •°6^50..7^20 ✱°-7^40 ✱°11^50-17^45; ✛'11^50-20^10; ≫0^00-2^30 ⫸-11^20 ≫-24; ≡²0^00-30 ==-3^20 ≡²-24; V°7^40-24
28	0	27.6	2	✱°0^45..5^25 ▲°-8^50 ✱°-12^50 ▲°-13^00 ▲✱'-17^30 ▲'-18^30 ✱'-24; ✛'0^45-2^40 ✛²-12^30 ✛'-24; ≫0^00-2^40 ⫸-12^30 ≫-24; ≡²0^00-40 ==-2^20 ≡²-24; V°0^00-30 V°-24
29	7	5.4	30	✱'0^00-1^30 ✱°-6^10 ✱'-7^50 ✱°-9^30..11^40 ✱'14^30..15^20 ✱°..19^30-20^20..22^30-24; ✛'0^00-5^30 ✛°-9^20 ✛'15^20-17^30 p; ≫15^10-17^30, 19^20-21^30; ≡²0^00-10^30 ==-10^45 ≡²-11^45 ==-14^30 ≡²-
30	0	12.5	35	✱°0^00-9^30..10^47 ▲'-12^08 ▲°-12^15 ▲'-12^25 ▲°-12^42 ▲'-13^18 ▲°-15^40 ▲'-16^10 ▲°16^25-19^10, 19^25-22^10 ✱°..22^35, 23^40..24; ✛°13^20-16^30 ✛'-24; ≫16^30-24; ≡²0^00-22^35 ==-24
31				[29.IV: 20^20 == 21^30 ≡²24; V°0^00-10^30, 10^45-11^45, 14^30-20^20, 21^30-24
Σ	—	139.0	—	UWAGI

Śnieżka φ = 50°44' λ = 15°44' Maj – Mai 1962

DNI	CIŚNIENIE P – 700 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	128.2	128.0	125.7	127.3	-8.8	-6.4	-7.4	-7.5	-5.5	-9.8	92	94	93	93	0.3	0.2	0.3	0.3	10 ≡	10 ✳	10 ✳≡	NNW 6	NNW 6	NNW 9
2	122.1	123.2	126.7	124.0	-6.2	-3.6	-5.2	-5.0	-2.9	-7.6	94	97	95	95	0.2	0.2	0.2	0.2	10 ✳ ≡	10 △ ≡	9	WSW 9	NNW 8	NNW 4
3	126.9	128.0	127.3	127.4	-6.4	-5.0	-1.8	-3.2	-1.6	-7.2	94	97	98	96	0.2	0.1	0.1	0.1	9	10 ≡	10 ✳≡	WNW 4	NW 4	SW 16
4	124.5	125.9	127.5	126.0	-5.0	-2.8	-2.6	-3.3	-1.4	-5.8	95	97	98	97	0.2	0.1	0.1	0.1	10 ✳≡	9 ✳	10 ✳≡	SW 14	W 8	W 12
5	128.5	130.9	133.4	130.9	-4.0	-2.0	-1.8	-2.4	-0.3	-5.6	96	98	98	97	0.2	0.1	0.1	0.1	9	10 ✳≡	9	W 14	W 6	W 4
6	135.2	137.2	137.3	136.6	-2.4	1.8	4.0	1.8	4.6	-5.3	98	96	88	94	0.1	0.3	1.0	0.5	5	7	10	WNW12	W 6	W 18
7	136.3	138.3	138.9	137.8	5.6	6.2	7.2	6.6	7.5	4.0	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	10 ≡	10 ●≡	WNW16	WNW16	W 16
8	137.7	137.6	135.4	136.9	7.6	9.0	7.0	7.6	9.8	6.5	90	74	94	86	1.1	2.9	0.6	1.5	8	9	9	W 20	W 20	W 20
9	136.3	136.1	133.6	135.3	4.0	6.0	6.2	5.6	7.7	1.8	79	89	97	88	1.7	1.1	0.3	1.0	6	10	10 ●	WNW10	W 8	SW 8
10	131.1	133.1	133.0	132.4	2.1	4.0	1.2	2.1	6.2	0.4	100	79	91	90	0.0	1.7	0.7	0.8	10 ≡	9	4	W 16	WNW14	WNW15
11	132.6	132.6	132.9	132.7	-0.4	2.2	0.6	0.8	3.0	-1.5	100	80	92	91	0.0	1.5	0.5	0.7	5	8 ⊙	3	WNW10	W 10	W 13
12	133.6	134.6	134.4	134.2	0.4	4.6	0.0	1.2	5.2	-0.7	92	85	100	92	0.5	1.3	0.0	0.6	8 ⊙	9	10 ✳≡	W 6	W 4	WSW12
13	134.6	135.7	133.7	134.7	0.6	2.0	1.9	1.6	3.1	-0.1	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ● ≡	WSW 5	SW 1	WNW12
14	125.5	123.5	125.8	124.9	-1.6	-2.2	-1.6	-1.8	2.1	-2.5	98	98	98	98	0.1	0.1	0.1	0.1	10 ✳≡	10 ✳≡	10 ✳≡	WNW18	N 20	NW 22
15	125.5	127.0	130.5	127.7	-2.4	-1.8	-1.6	-1.8	-0.9	-2.9	98	98	98	98	0.1	0.1	0.1	0.1	10 ✳≡	10 ✳≡	10 ≡	NW 22	NW 22	NW 17
16	131.6	133.9	134.2	133.2	-2.0	-2.3	-2.2	-2.2	-1.2	-3.2	98	96	98	97	0.1	0.3	0.1	0.2	10 ✳≡	10	7	NW 16	NW 12	W 16
17	133.0	132.9	131.6	132.5	-0.1	1.4	1.2	0.2	2.7	-2.5	100	100	100	100	0.0	0.0	0.0	0.0	10 △ ≡	10 ● ≡	10 ● ≡	SW 16	SW 14	SW 22
18	134.5	136.9	138.9	136.8	-0.3	1.2	2.0	2.2	2.9	-1.2	100	87	84	90	0.0	1.0	1.2	0.7	9	9	6	SW 6	W 14	W 8
19	135.6	134.0	131.8	133.8	2.8	8.4	7.9	6.8	9.7	0.6	75	80	96	84	1.9	2.2	0.4	1.5	8	7 ⊙	10	WSW14	SSW18	S 7
20	130.9	132.8	134.4	132.7	-0.8	0.2	-0.6	-0.4	7.9	-1.8	97	100	99	99	0.2	0.0	0.0	0.1	10 ✳≡	10 ≡	9	NW 17	WNW 8	NW 18
21	135.5	135.9	134.7	135.4	-0.8	0.6	0.9	0.4	2.1	-1.7	99	94	90	94	0.0	0.4	0.6	0.3	10 ≡	9	1	NW 10	C 0	SSW10
22	131.7	133.1	136.8	133.9	1.1	2.2	2.2	1.9	3.2	0.0	87	100	96	94	0.9	0.0	0.3	0.4	9	7	9	SW 25	SW 25	W 17
23	137.2	136.5	137.1	136.9	0.2	3.5	4.8	3.3	5.3	-0.1	100	100	100	100	0.0	0.0	0.0	0.0	8	9	10 ≡	SW 20	SW 25	SW 20
24	137.9	137.6	135.8	137.1	0.2	0.2	-0.4	-0.1	4.8	-1.1	96	90	100	95	0.3	0.6	0.0	0.3	10	10	10 ≡	SW 6	WSW 9	WSW 8
25	134.3	134.3	133.6	134.1	-0.2	0.1	0.0	0.0	0.7	-1.1	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	9 △	10 ✳≡	WSW 2	WSW 1	NW 7
26	130.6	130.7	131.6	131.0	-0.6	0.2	0.4	0.1	1.1	-0.8	99	100	100	100	0.0	0.0	0.0	0.0	10 ✳	10 ✳ ≡	10 ● ≡	NW 12	NNE 6	SW 13
27	133.9	136.0	136.9	135.6	-1.2	2.0	2.6	1.5	4.6	-1.5	99	100	100	100	0.1	0.0	0.0	0.0	8	10 ≡	10 ≡	WNW 8	NNW 3	SSW 7
28	136.3	136.1	135.2	135.9	3.2	5.6	3.0	3.7	6.7	2.4	100	98	98	99	0.0	0.2	0.2	0.1	8 ⊙	10 ≡	6	S 9	SSW 8	WSW26
29	135.3	137.2	137.6	136.7	0.0	3.8	1.0	1.4	4.9	-0.4	100	75	96	90	0.0	1.8	0.3	0.7	6 ⊙	8 ⊙	10 ●	SW 2	SW 16	W 18
30	138.3	139.2	139.1	138.9	0.3	4.0	3.0	2.6	5.2	-0.2	100	65	77	81	0.0	3.0	1.7	1.6	9	9	2	W 15	WNW 6	W 7
31	136.3	134.5	133.1	134.6	2.6	5.8	3.2	3.7	7.3	1.1	78	62	79	73	2.1	1.4	1.8	1.8	6	9	9	W 11	SW 18	W 16
M	132.6	133.3	133.5	133.1	-0.4	1.6	1.1	0.8	3.4	-1.5	95	91	95	94	0.3	0.7	0.3	0.4	8.7	9.3	8.5	12.0	10.9	13.5

Czerwiec – Juin

1	133.6	135.0	134.0	134.2	-4.4	-1.1	-2.1	-2.4	3.2	-4.6	69	93	98	87	1.3	0.4	0.1	0.6	9	9	10 ✳≡	NW 12	C 0	N 6
2	133.9	137.0	139.3	136.7	-3.0	-2.8	-2.6	-2.8	-1.7	-3.5	97	97	98	97	0.1	0.1	0.1	0.1	10 ✳≡	9	10 ✳≡	NW 14	NW 14	NW 8
3	140.1	141.8	141.7	141.2	-3.2	-1.6	-3.0	-2.7	-1.0	-4.5	97	98	97	97	0.1	0.1	0.1	0.1	10 ≡	10 ✳ ≡	10 ≡	NW 8	NW 9	N 12
4	140.7	142.5	143.1	142.1	-4.6	-2.4	-1.6	-2.6	-0.7	-5.5	96	98	98	97	0.2	0.1	0.1	0.1	10 ✳ ≡	10 ✳ ≡	10 ✳ —	N 16	NW 8	NW 16
5	142.4	142.5	143.0	142.6	-2.3	0.0	-1.2	-1.2	0.8	-3.8	98	96	95	96	0.1	0.2	0.3	0.2	10 ✳ ≡	10 ≡	9	WNW20	NW 20	NW 20
6	141.9	143.4	144.2	143.2	-4.4	-1.7	-1.0	-2.0	1.0	-7.1	96	75	73	81	0.2	1.4	1.6	1.1	8	6	6	N 20	NW 20	NNW22
7	143.2	145.0	146.4	144.9	-3.9	-2.1	-0.6	-1.8	-0.6	-5.1	94	98	89	94	0.3	0.1	0.6	0.3	10 ≡	10 ≡	4	N 16	N 17	NNW12
8	146.8	148.0	146.6	147.1	1.4	6.2	5.0	4.4	7.7	-1.3	63	63	68	65	2.6	3.5	2.8	3.0	2 ⊙	2 ⊙	2	N 6	N 6	N 4
9	142.7	141.7	138.8	141.1	5.6	9.8	7.4	7.6	10.7	3.5	70	48	79	66	2.6	6.3	2.1	3.7	0 ⊙	3 ⊙	8	N 11	NW 5	NNW 9
10	136.7	136.9	136.0	136.5	6.0	10.6	7.5	7.9	10.7	4.7	86	75	75	79	1.4	3.2	2.7	2.4	4 ⊙	6 ⊙	9	N 4	N 4	N 1
11	133.6	132.3	132.6	132.8	5.6	4.2	1.6	3.2	7.5	1.3	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ● ≡	10 ●≡	NW 8	NW 8	NW 8
12	133.1	134.7	136.0	134.6	-0.9	-0.8	-0.4	-0.6	1.6	-2.3	99	99	100	99	0.0	0.0	0.0	0.0	10 ● ≡	9	10 ≡	NW 6	NW 9	NW 12
13	137.7	138.3	137.9	138.0	0.8	4.8	4.8	3.8	7.3	-0.9	92	68	77	79	0.5	2.7	2.0	1.7	6	8	9	C 0	SW 8	SW 14
14	137.8	139.5	141.3	139.5	6.2	11.7	11.3	10.1	13.7	3.2	78	70	84	77	2.1	4.1	2.3	2.8	4 ⊙	6 ⊙	4	SW 8	SW 8	NNW 8
15	144.3	146.0	145.7	145.3	12.0	15.3	14.3	14.0	16.9	8.8	67	65	70	67	4.7	6.2	5.1	5.3	0 ⊙	8	8	NW 8	NW 5	SW 8
16	144.0	145.5	143.8	144.4	12.5	14.1	11.5	12.4	15.9	10.6	83	89	100	91	2.4	1.9	0.0	1.4	3	9 ●R	10 ●R≡	S 16	S 12	WNW19
17	144.9	145.4	144.7	145.0	9.2	9.8	9.0	9.2	11.8	8.8	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ●(R)≡	10 ≡	WNW12	NW 4	C 0
18	144.8	143.5	142.3	143.5	10.9	10.9	10.5	10.7	12.9	8.1	90	99	96	95	1.3	0.1	0.5	0.6	8	9 R	8	NW 2	W 3	SW 10
19	140.9	139.5	138.3	139.6	9.8	12.3	12.3	11.7	14.4	8.5	100	88	73	87	0.0	1.8	3.9	1.9	10 ● ≡	8 ⊙	9	SW 12	SW 10	SW 16
20	140.2	141.7	142.3	141.4	6.8	8.2	8.0	7.8	12.4	4.4	88	84	70	81	1.2	1.7	3.2	2.0	8 ⊙	10	3	NW 10	WSW 5	WSW 9
21	143.5	144.5	145.1	144.4	7.0	10.0	8.8	8.6	11.0	6.4	86	88	85	86	1.3	1.5	1.7	1.5	4	8 ⊙	1	WSW15	WSW10	W 6
22	146.9	147.2	146.7	146.9	8.8	12.9	12.5	11.7	14.5	7.8	95	76	79	83	0.6	3.6	3.0	2.4	5 ⊙	7 ⊙	1	W 4	W 2	WSW 9
23	146.1	146.7	145.8	146.2	12.9	16.7	15.0	14.9	17.4	11.8	79	64	71	71	3.1	6.8	4.8	4.9	4 ⊙	4 ⊙	5	SW 10	SW 12	SW 4
24	143.9	142.5	142.2	142.9	10.9	14.1	13.3	12.9	17.1	10.3	95	79	78	84	0.6	3.4	3.4	2.5	8 ⊙	8	0	SW 10	SW 18	NW 2
25	140.2	141.6	141.6	141.1	6.6	6.6	2.8	4.7	13.4	2.4	89	66	83	79	1.0	3.4	1.2	1.9	9	6	1	NW 8	W 7	WNW18
26	139.4	137.8	135.1	137.4	3.0	5.0	6.2	5.1	8.1	1.3	75	77	78	77	1.9	2.0	2.1	2.0	3	8 ⊙	6	W 7	W 6	SW 12
27	132.2	133.6	134.6	133.5	-1.0	1.2	-0.4	-0.2	6.3	-1.3	100	83	96	93	0.0	1.2	0.2	0.5	10 ≡	8	3	W 18	W 26	W 16
28	133.4	131.3	129.9	131.5	-2.4	-1.0	0.0	-0.8	0.4	-2.6	98	99	98	98	0.1	0.1	0.1	0.1	9	10 ✳ ≡	10 ≡	W 16	W 16	W 18
29	130.7	134.1	135.1	133.3	-0.6	0.0	0.0	-0.2	0.9	-1.7	99	100	100	100	0.0	0.0	0.0	0.0	10 ✳≡	10 ≡	10 ≡	W 18	W 13	WNW12
30	134.4	136.3	137.5	136.1	-1.2	1.0	0.8	0.4	1.8	-1.3	99	100	100	100	0.1	0.0	0.0	0.0	10 ≡	9	10 ●≡	WNW12	NW 6	NW 6
31																								
M	139.8	140.5	140.4	140.2	3.5	5.7	5.0	4.8	7.8	1.9	89	84	87	87	1.0	1.9	1.5	1.5	7.1	8.0	6.9	10.9	9.7	10.6

Śnieżka $H_s = 1603m$ $H_n = 1610,6m$ Maj - Mai 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ SNIEGU h	POGODA
1	7	2.8	42	*0^00 3^40 7^40 12^10-24; ⊥°0^00-4^05 ⊥°-11^30 ⊥·13^30-24; ≫0^00-4^05; ≋ 0^00-20 ≡² 3^35 ≋ -4^10 ≡² -11^05 ≋ -11^50 ≡² -12^05 ≋ -15^10 ≡² -17^30 ≋ -19^40 ≡² -24; v°0^20-3^45; 4^20-11^05 22^40-24
2	0	8.4	46	*0^00-3^10 5^15-8^20 9^45 ⊥°-10^00 ⊥·10^25 *-11^05 ⊥·11^12 *-11^25 ⊥°-11^35 *-14^20 ⊥°-14^40 *-17^40 ⊥°-18^35-19^30; ⊥°-0^00-3^30 ⊥°-7^40 11^50-19^30; ≡ 0^00-13^52 ≋ -14^10 ≡² -15^45 ≋ -15^52 ≡² -16^48 ≋ -17^45-18^55-19^40-19^55-24; v°0^00-13^52
3	0	2.1	50	⊥°4^45-6^20 ⊥°9^30-11^10 *13^05 24; ⊥°7^40-8^30 ⊥°14^30-15^10 ⊥·20^30 ⊥°-24; ≫14^10-20^30 ≋-24; ≋ 0^00-40 ≡² -1^40 ≋ -1^50 ≡² -6^40 ≋ -7^10 ≡² 12^30-24; v°1^10-40 4^20-6^40
4	7	1.1	52	*°0^00 23^45; ⊥°0^00-5^30 ⊥·9^30 ⊥°-23^45 ⊥°-24; ≫0^00-5^30 ≫-9^30; 16^30-24; ≡ 0^00-7^45 ≋ -9^30 ≡² -12^15 ≋ -13^30 ≡² -14^30 ≋ -18^10 ≡² -23^45 ≋ -24; v°1^30-7^45; 8^15-24
5	0	0.3	53	*°9^50 14^40; 15^50; 17^40; ⊥°0^00-8^20; ≫0^00-8^20; ≋ 4^30-10^30 ≡² -17^20 ≋ -19^30 ≡² -20^20 ≋ -22^30
6	8	2.5	53	•°23^10-24; ⊥·5^30-7^20; ≫5^30-10^30 14^20-18^30 ≫-24; ≋ 23^10-24 [2.V: 14^20-15^45; 15^55-16^48; (☒)°10^46-52
7	0	0.7	pż.	•°0^00 1^45; 3^30-7^15 14^20; 15^40; 20^50; 21^40; ≫0^00-4^30 ≫-5^20 ≫-8^30 ≫-11^20 ≫-24; ≋ 0^00-3^10 ≡² -17^30 ≋ -19^20 ≡² -22^30 ≋ -24
8	8	7.4	pż.	⊽°5^50-6^10 ⊽°7^20-40 ⊽°8^10; 15^15-18^30 ⊽°18^50-19^10; 22^50-23^20; ≫0^00-24; ≋ 0^00-1^30 7^10-20 ≡² 7^40 ≋ -9^10 16^10-18^20 ≡² 21^30-24
9	8	7.1	pż.	⊽°100-30 •°13^25 19^30 ⊽°20^50-21^05 •°21^30-24; ≫0^00-5^30 ≫-7^30 23^30-24; ≡ °0^00-2^10 3^30-5^20 ≋ -19^25-40 ≡² -20^30 ≋ -21^10 ≡² -22^30 ≋ -24
10	8	0.2	pż.	•°0^00-30 ⊽°0^50-1^30 ⊽°-4^30 13^35-14^20 ▲⊽°15^40-16^05 ▲⊽°-16^15; ≫0^00-1^30 ≫7^30-7^30 ≫-9^30 ≫-12^20 ≫-14^20 ≫-19^30 ≫21^20 ≫-24; ≋ 0^00-1^30 ≡² 2^10 ≋ -11^30; 13^30-14^20; 15^20-16^30; ☒ 0^50-2^30 (☒)°14^20-16^30
11	8	0.2	pż.	⊽°7^30-8^05 13^26-43 ⊽°15^00-10 ⊽°-15^20 ⊽°-15^45; ☒ 20^50-22^30; ≫0^00-1^30 3^30-16^30; ≋ 2^20-4^30 ≡² -5^20 ≋ -7^30 ≡² -8^30 ≋ -9^20 15^00-10
12	8	11.4	pż.	▲⊽°-14^50-15^20 ▲⊽°-16^20 ⊽°-17^30 ⊽°-19^20 *° 22^30 •°-24; ☒ 14^20-15^50 WNW-ENE; ≫20^30-24; ≡ 1^30-2^30 ≋ 13^05-14^10 ≡² -24
13	0	15.4	pż.	•°0^00 20 *°-1^20 *° 2^20 •°-5^40 •-7^30 •°17^55 24; ≫0^00-30 ≫-4^30 ≫19^40-22^40 ≫-24; ≡ 0^00 14^50 ≋ -16^40 ≡² -24
14	0	27.8	pż.	•°0^00-2^30 *°-7^10 *-24; ⊥°4^30-24; ≫0^00-24; ≡ 0^00-24; v°2^20-9^30 v'-24; ∼°2^10-30
15	0	3.6	20	*'0^00 2^30 *-12^35 13^10 ⊥°0^00-14^30 18^10-24; ≫0^00-24; ≡ 0^00-18^30 ≋ -19^10-20^40 ≡² -24; v'0^00-3^30 v°-13^10 21^40-24
16	7	0.6	10	*°2^10-2^45 5^15-9^50 ⊥°2^00-10^30 ⊥·13^30 ⊥°-15^30; ☒ 0^00-10^00 ≫-13^30; 17^30-20^30 ≫-24; ≡ °0^00-9^40 ≋ -10^45 ≡² -11^10 ≋ 15^20; 21^50-22^30 ≡² 23^45-24; v°0^00-9^40
17	0	4.6	18	△°6^02-7^30 *°-10^45 •-12^10 •'-12^30 •'-13^05 •-13^10 ⊽°-13^50 •-14^35 ⊽°-15^25 •-19^30 •°21^40 •-23^15; ≫0^00-8^30 ≫-13^10 ≫-24; ≡ °0^00-23^15 ≋ -24; v°1^30-6^00; (☒)°13^05 30 14^50 15^10
18	8	0.0	10	⊽°9^25-50 11^10-20 ☒°-12^10 ☒°14^15-30; 14^40-55 ⊽°15^30-16^10; ≫0^00-30 ≫-5^40; 10^20-13^30 ≫-18^20 21^30-24; ≋ 0^00-1^40 ≡² -5^30 ≋ 6^30-8^10
19	8	9.9	5	⊽°22^50-23^00 ▲⊽°-23^15 ⊽°-24; ≫0^00-4^20 ≫-7^30 ≫-20^00 ≫-20^30 ≫20^50-24; ▭ 20^30-21^45 ≡² -24
20	3	0.8	pż.	⊽°-1^00-1^30 •°-3^50 *-6^40 *-8^20 *°9^10 ⊽°11^50-12^40; 14^50-15^30; ≫0^00-30 ≫-4^30-10^20 ≫17^30-20^30 ≫-24; ≡ °0^00-6^25 ≡ °-7^20 ≡² -8^05 ≋ -9^10-10^10 ≡² -14^30 ≋ -15^20 ≡² -18^10 ≋ 20^30-21^30 ≡² -24; v°∼3^30-5^30 v°-7^20-8^05
21	7	0.9	pż.	☒°10^47-11^15 ☒'-12^14 *°-12^32 13^18 14^40 15^10 45; ≫0^00-4^20 ≫-7^30 20^50-24; ≡ °0^00-7^20 ≋ -14^30 16^10-17^30 ≡² -18^05 ≋ -18^30 ▭ -22^10 ≡² -24; v°0^00-7^20 [20.V: v°23^30-24
22	7	2.4	pż.	•°7^00-7^30 10^40 •-12^30 ⊽°15^50-16^02 ▲⊽°-16^30 ⊽°-16^50 ⊽°17^30; ≫0^00-4^30 ≫-14^20 ≫-15^20 ≫16^20-19^20 ≫-20^30 ≫-24; ≡ °0^00-2^20; 3^30-4^15 ▭ 7^40 ≋ 7^30-7^40 ≡² -12^20 ≋ -13^40 ≡² -16^50 ≋ -17^30 ≡² -19^30 ≋ -24
23	7	0.6	pż.	•°16^00 17^10 ≫0^00-1^20 ≫-3^30 ≫-24; ≋ 0^00-1^30 ≡² -6^40 ≋ -15^10 ≡² -22^30 ≋ -24
24	8	0.6	pż.	*°13^30-15^40; 17^20 20^30; •°23^50-24; ≫0^00-1^30 ≫-4^10 13^30-16^20 ≋ 0^00-30 ≡² -1^40 ≋ -2^30 13^20-40 ≡² -24; v 23^50-24
25	7	8.2	pż.	•°0^00-30 ☒°9^50-10^03 11^40-13^10 ☒°13^30-18^10 *°20^40 21^05; ≡ °0^00-12^45 ≋ -13^10 ≡² 14^40-24; v°0^00-6^30
26	0	12.2	2	*°0^10-1^30 *°4^30-6^10 *'-7^20 *-11^30 *-13^20 •-15^30 *-16^40 •-18^30 20^30-22^40; ⊥°9^20-11^30; ≫5^30-10^20; 17^30-24; ≡ °0^00-24; v'6^30-13^20
27	0	•	pż.	≫0^00-7^20; ≡ °0^00-7^30 ≋ -8^40 ≡² -15^20 ≋ -21^30 ≡² -24; v 0^00-7^30
28	1	•	pż.	•4^30-5^40; ≫15^30-20^30 ≫-24; ≡ °0^00-5^40 ≋ -6^45 7^10-9^30; 10^25-11^15 ≡² 13^30-20^20 ≋ -24
29	8	2.0	pż.	⊽°18^50-19^15 19^50-22^50; 23^50-24; ≫0^00-17^20 ≫18^20-19^30 ≫20^30-22^50 ≫23^30-24; ≋ 0^00-9^20 ▭ 4^30-8^30 ≋ 18^15-19^20 ≋ 20^35-21^30
30	8	0.1	pż.	⊽°0^00-1^50 *9^25-40 ⊽°14^50-15^20; ≫0^00-6^30 ≫-7^20 ≫-12^30; 16^30-19^20; ≋ 0^50-1^30 ≡² -5^30 ≋ -10^20; 20^30-21^20
31	8	•	pż.	≫2^30-8^40 ≫-16^30 ≫-17^40; 19^30-20^30 ≫-23^30 ≫-24; ≋ 17^10-21^20
Σ	—	133.9	—	UWAGI

Czerwiec - Juin

1	7	12.2	pż.	△°19^45-21^30 *°-24 ≫0^00-8^30; ≋ 1^50-4^40 ▭ 6^20-8^05 ≋ -8^40 9^50-18^00 ≡² -24; v°18^30-24
2	7	5.3	15	*°0^00-1^30 *'-6^10 ☒'-7^50 *'-10^30 *° 12^40; 19^30 24; ⊥°6^15-13^20; ≫6^15-16^20; 19^20-20^30; ≡ °0^00-13^30 ≋ -16^20; 19^30-40 ≡² 20^30-24; v°0^00-13^30; 20^30-24
3	0	6.6	15	*°8^40 10^20 ☒'-10^45 ⊽°12^30-40; 13^50-14^10 ▲-14^20 ⊽°-14^45; 15^30-16^45 ⊽°-22^30-24; ⊥°18^30-24; ≫16^30-18^30 ≫-19^40 ≫-24; ≡ °0^00-4^20 ≋ -6^30 ≡² -11^50 ≋ -13^00 ≡² -17^20 ≋ -18^20 ≡² -24; v°0^00-4^00
4	0	5.7	20	⊽°-0^00-30 ☒'-3^00-10 ⊽°-6^40-9^30 *'-10^20 *°-13^30 14^40 ⊽°19^50-21^20 *°-24; ⊥°0^00-3^30 ⊥°-8^20 ⊥·13^30 ⊥°-15^20 ⊥°22^30-24; ≫0^00-3^30 ≫-6^30 ≫-7^30 ≫-9^30 ≫-13^30 ≫14^40-15^20 ≫16^30
5	0	0.1	25	*°0^00-2^30 10^25 ☒'-12^45-50 ☒°15^25-30; ⊥°0^00-14^30; ≫0^00-24; ≡ °0^00-5^30 ≋ -6^40 ≡² -10^25 ≋ -11^20 ≡² -14^10; v°0^00-5^30; 6^40-10^25-12^30
6	9	0.6	25	⊥°5^30-8^40; ≫0^00-24; ≋ 0^30-1^30 ≡² -7^15 ▭ ≋ -8^10 ▭ -8^30 9^30-11^10; v°0^30-7^15
7	0	0.0	pł.	≫0^00-16^30 ≫-24; ≋ 2^40-3^10 ≡² -9^00 ≋ ▭ -11^30 ≡² 13^30-16^45 ≋ -17^05; v°4^10-9^00; 13^45-16^45
8	9	•	pż.	≫0^00-2^30 [3.VI: 6^30-11^50; 13^10-17^20; 18^20-24
9	8	•	pż.	≫0^00-8^40 [4.VI: -17^30 ≫-24; ≡ °0^00-15^30 ≋ -18^20 ≡² -24; v°0^00-15^30; 18^20-24
10	8	•	pł.	
11	0	0.9	pż.	⊽°13^00-14^05; •21^30-24 (☒)'SE 10^50-13^00; ≫16^30-21^30; ≡ ² 7^15-9^30 ≋ -10^40 ≡² -15^00 ≋ -16^45; 17^20-19^30 ≡² -24
12	8	0.0	pż.	•0^00-5^30 ⊽°7^45-8^50; ≫2^30-7^30; 15^30-24; ≡ °0^00-10^30 ≋ -12^20 ≡² -22^20 ≋ -24; ∼°v°5^30-8^30 v°-10^30
13	8	•	pł.	≫0^00-3^20 17^40-24; ≋ 0^00-30 ≡² -2^30 ≋ -3^20
14	8	•	pł.	≫0^00-3^40; 14^30-19^30
15	7	0.1	pż.	⊽°16^20-40 19^02-20; (☒)°17^50-18^55 SW-SE; (☒) 18^05-19^02
16	8	33.3	pż.	⊽°13^25-14^30 15^30-40 ⊽°-16^10 ▲°-17^20 ⊽°20^50-21^20 ⊽°-22^30 ☒°-2 13^50-18^30 SW-SE ☒°20^50-22^3 SW-SE; ≫1^50-6^50 ≫-13^30 ≫-15^20 ≫-17^30; 19^20-22^30 ≡² 16^10-17^20 ≋ 18^30-19^30 ≡² -24; ☒ 15^20-18^30
17	0	8.8	pż.	⊽°0^30-2^30 •° 3^50 4^30 7^30 11^20 12^10 •°-13^10 ⊽°13^45-15^10; (☒)°W 13^50-14^50; ≫1^20-8^20; ≡ ² 0^00-14^30 ≋ -15^30 ≡² -23^30 ≋ -24
18	7	4.9	pż.	⊽°10^50-12^40; ☒°WSW 13^59-15^50; ≫19^20-24; ≋ 0^00-30 ≡² -2^50 ▭ -3^50 ≋ -4^10 ▭ -8^10 ≋ -10^30 ≡² -11^40 ≋ -14^30 ≡² 15^20 ≋ -17^40 ≡² -18^30 ≋ -20^20 ≡² -21^30
19	7	14.6	pż.	•°6^50 7^20 ⊽°-8^10 •°-10^30 ⊽°16^15-17^05; 22^00-15 ⊽°-22^40 ⊽°-23^05 ⊽°-23^40 ⊽°-24; (☒)°18^55-19^30 S-N ☒°22^00-23^10-24 W-E-NE; ≫0^00-14^30 ≫-23^40 ≫-24; ≋ 0^00-1^30 ≡² -8^10 ≋ -8^30 ≡² 11^30-12^40;
20	8	•	pż.	⊽°0^00-30 ⊽°-1^10; ☒°0^00-55 E-NE; ≫0^00-8^30 16^20-17^30; ≡ ² 0^00-50 1^30-3^40 ▭ -10^10 ≋ -11^30; ☒°0^00-55
21	8	0.0	pż.	⊽°14^50-52 16^53-17^01; ≫2^30-14^30; ≋ 22^40-23^10
22	7	•	pż.	[19.VI: 19^10-20^00; 22^10-24; (☒)' 7^30-8^10; 18^50 19^25 ☒°22^00-24
23	7	•	pż.	≫4^30-24; ≋ 22^40-24
24	7	•	pż.	≫0^00-10^30 ≫-18^30 ≫-20^30
25	8	0.0	pż.	⊽°5^45-6^02; ≫0^30-2^30 3^30-4^30 11^30-13^20 ≫14^30-18^20 ≫-20^20 ≫-24; ≋ 3^30-5^20 7^50-8^30 ≡² -9^20 ≋ -10^30
26	8	0.6	pż.	⊽°23^50-24; ≫0^00-2^30 ≫-6^20; 14^30-23^30
27	7	0.1	pż.	⊽°0^00-20 ⊽°-2^15-50 ☒°10^50-11^10 ☒°15^50-16^20; ≫1^30-2^15 ≫-14^30; 15^30-16^20 ≫-17^30 ≫-24; ≡ °0^15-1^40 ≋ 2^25-30 ≡² 5^20-8^30 ≋ -10^20 ≡² 11^40 ≋ -13^20 14^40-16^20 ≡² 22^30-23^20 ≋ -24; ☒ 2^20-30
28	0	2.3	pż.	☒°10^10-13; 10^45-11^03 ⊽°11^07-30; 11^40-13^05 *°13^15-20^30 21^40 ≫0^00-24; ≋ 0^00-2^30 ≡² -7^40 ≋ -8^10 ≡² -24; v°2^30-7^40 8^10-17^40; 22^30-23^40 v°-24
29	0	0.0	4	*3^40-9^40 •°14^50-15^40 ⊥°3^40-9^40; ≫0^00-13^30 ≫-24; ≡ °0^00-16^40 ≋ -17^30 ≡² -18^40 ≋ -21^20 ≡² -24; v°0^00-10^30
30	7	0.0	pż.	•17^30-24; ≫0^00-9^10; ≡ °0^00-13^40 ≋ -14^40 ≡² -24
31				
Σ	—	96.1	—	UWAGI

Śnieżka $\varphi = 50°44'$ $\lambda = 15°44'$ Lipiec - Juillet 1962

DNI	CIŚNIENIE P= 700 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	137.2	137.2	136.9	137.1	-0.8	0.2	1.0	0.4	1.1	-1.1	97	100	100	99	0.2	0.0	0.0	0.1	10	9	10 ☂	NW 3	W 8	WNW10
2	135.7	135.8	133.3	134.9	1.4	1.9	2.8	2.2	3.0	0.6	100	100	100	100	0.0	0.0	0.0	0.0	10 ═	10 ☂ ═	10 ● ═	NW 14	NW 10	NW 12
3	126.9	125.7	123.7	125.4	0.2	0.4	0.2	0.2	3.2	-0.2	100	100	100	100	0.0	0.0	0.0	0.0	10 ☂ ═	10 ═	10 ✳ ═	W 16	W 20	W 22
4	119.0	122.0	124.5	121.8	-2.0	-0.6	0.2	-0.6	0.3	-2.2	98	99	100	99	0.1	0.0	0.0	0.0	10 ═	10 ✳ ═	10 ☂ ═	W 26	W 20	W 18
5	126.0	129.2	132.0	129.1	0.2	1.2	1.8	1.2	4.0	-0.2	100	100	100	100	0.0	0.0	0.0	0.0	10 ☂ ═	9	10 ☂ ═	W 16	SW 8	W 8
6	134.1	136.1	136.9	135.7	1.0	2.8	2.2	2.0	3.8	0.4	100	96	90	95	0.0	0.3	0.7	0.3	9	9 ▲●	2	SW 10	SW 15	W 12
7	136.1	136.0	137.6	136.6	1.4	1.2	1.6	1.4	2.7	0.1	100	100	100	100	0.0	0.0	0.0	0.0	10 ═	10 ☂ ═	10 ═	W 22	W 18	W 11
8	139.2	141.2	141.7	140.7	2.6	4.6	4.2	3.9	5.4	0.6	100	100	76	92	0.0	0.0	1.9	0.6	10 ═	8	0	W 10	W 6	WNW11
9	141.6	141.7	141.0	141.4	4.6	7.8	7.2	6.7	8.3	3.5	65	84	87	79	3.0	1.7	1.4	2.0	3	9	4	W 7	W 6	SW 2
10	139.8	140.2	138.9	139.6	7.6	10.7	9.9	9.5	11.9	6.7	78	81	58	72	2.3	2.6	5.2	3.4	2 ⊙	8 ⊙	4	SW 2	NW 2	NW 6
11	137.2	137.1	135.4	136.6	10.5	12.5	10.0	10.8	13.2	9.4	78	86	73	79	2.7	2.0	3.3	2.7	8	9	2	SW 16	SW 8	SW 20
12	134.8	134.0	132.7	133.8	6.8	8.1	6.0	6.7	10.1	5.9	89	88	90	89	1.1	1.3	1.0	1.1	7 ⊙	9	8	SW 12	SW 14	W 12
13	130.8	132.2	133.2	132.1	3.4	3.6	3.8	3.6	6.3	2.8	100	100	97	99	0.0	0.0	0.3	0.1	10 ═	8	8	W 12	W 12	W 14
14	131.8	131.7	131.8	131.8	4.2	4.4	4.8	4.6	5.7	3.2	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ═	9	9	W 20	W 18	NW 10
15	130.6	129.6	130.8	130.3	5.8	5.6	6.2	6.0	8.8	4.8	100	94	100	98	0.0	0.6	0.0	0.2	10 ═	10 ●	9 ●	SW 8	SW 7	W 2
16	130.9	131.9	134.3	132.4	6.6	8.0	6.3	6.8	8.6	6.0	100	100	97	99	0.0	0.0	0.2	0.1	10 ● ═	10	10 ●	W 2	W 1	NW 11
17	134.9	136.7	138.6	136.7	6.8	6.4	6.4	6.5	7.7	5.8	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ═	10 ● ═	10 ═	NW 14	NW 10	N 6
18	138.4	138.9	139.3	138.9	5.6	6.9	6.4	6.3	7.5	4.1	100	94	100	98	0.0	0.5	0.0	0.2	10 ═	10	10 ═	N 12	N 8	N 16
19	140.0	141.4	142.2	141.2	6.4	8.5	8.2	7.8	11.0	5.3	100	89	91	93	0.0	1.3	1.0	0.8	10 ☂ ═	4	8	N 11	N 10	N 6
20	141.7	142.3	142.7	142.2	8.4	10.4	10.3	9.8	10.9	7.0	81	72	91	81	2.0	3.5	1.2	2.2	6	8	4	SW 11	SW 8	SW 1
21	140.7	139.9	140.8	140.5	10.1	14.2	12.8	12.5	16.4	9.4	100	78	100	93	0.0	3.6	0.0	1.2	2 ⊙	8	10	SW 12	SSW20	SSW13
22	141.5	142.0	142.4	142.0	11.1	14.7	10.0	11.4	15.1	10.0	79	75	95	83	2.8	4.2	0.7	2.6	3	7 ⊙	8	W 7	SW 6	W 4
23	143.5	144.5	145.2	144.4	7.8	9.9	7.0	7.9	10.6	6.8	90	74	76	80	1.1	3.1	2.4	2.2	8	9	2	NW 2	WNW 2	WNW 6
24	145.8	146.6	146.4	146.3	4.8	7.2	6.5	6.2	9.0	3.8	94	94	91	93	0.6	0.6	0.9	0.7	5	9	1	W 8	WNW 6	NNW 4
25	145.9	145.3	144.0	145.1	7.9	11.7	12.2	11.0	14.1	5.5	80	70	87	79	2.1	4.1	1.9	2.7	1	3	3	WSW 3	SW 12	SW 16
26	143.5	144.6	143.2	143.8	14.7	18.7	12.9	14.8	19.3	10.7	75	66	100	80	4.2	7.4	0.0	3.9	0	2	10 ● R ═	SW 12	SW 12	WSW30
27	142.5	142.0	141.6	142.0	14.3	11.3	7.6	10.2	15.0	7.2	87	94	100	94	2.2	0.8	0.0	1.0	6	9	9	WSW20	SW 18	NW 14
28	141.5	142.8	142.5	142.3	4.2	6.6	4.8	5.1	8.3	4.2	100	94	80	91	0.0	0.5	1.7	0.7	10 ☂ ═	9	3	NW 13	NW 5	NW 12
29	141.7	142.1	142.3	142.0	3.8	5.3	5.6	5.1	8.8	3.5	97	95	86	93	0.3	0.4	1.3	0.7	6	9	7	NNW12	N 3	NE 3
30	142.6	142.6	143.0	142.7	6.2	7.6	7.2	7.0	12.4	4.7	63	68	62	64	3.5	3.3	3.9	3.6	4 ⊙	8	3	C 0	C 0	C 0
31	143.4	143.7	143.5	143.5	7.3	10.3	9.4	9.1	11.9	6.3	65	68	78	70	3.6	4.0	2.6	3.4	9	7 ⊙	8	C 0	SW 6	W 8
M	137.4	138.0	138.1	137.8	5.6	7.2	6.3	6.4	8.9	4.3	91	89	90	90	1.0	1.5	1.0	1.2	7.4	8.4	6.8	10.7	9.6	10.3

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1	142.2	142.9	141.8	142.3	7.6	10.3	7.6	8.3	10.8	7.2	94	67	71	77	0.6	4.1	3.0	2.6	8 ⊙	7 ⊙	4	W 12	W 11	W 14
2	141.0	140.9	140.0	140.6	6.8	11.8	12.9	11.1	14.5	5.9	87	73	76	79	1.4	3.6	3.6	2.9	3 ⊙	6 ⊙	9	W 8	SW 8	W 12
3	139.2	140.2	140.6	140.0	11.3	13.2	11.1	11.7	14.2	10.3	90	87	100	92	1.4	2.0	0.0	1.1	9	9	5	C 0	C 0	SW 6
4	139.9	140.8	142.2	141.0	11.5	13.3	12.0	12.2	15.0	10.3	100	88	82	90	0.0	1.9	2.5	1.5	10 ═	9	0	SW 16	SW 14	NW 6
5	139.2	138.8	137.0	138.3	11.1	8.8	11.1	10.5	12.4	8.6	89	100	100	96	1.5	0.0	0.0	0.5	9	10 ●	10 R ═	SW 12	SW 7	SW 8
6	135.2	136.2	136.5	136.0	8.6	9.8	11.1	10.2	11.4	8.1	100	100	100	100	0.0	0.0	0.0	0.0	10 ☂ ═	10 ═	10 ═	SW 24	SW 20	SW 14
7	132.2	131.0	131.6	131.6	12.1	12.7	3.8	8.1	13.2	3.8	99	100	81	93	0.1	0.0	1.5	0.5	9	10 ═	7	SW 20	SW 18	SW 35
8	135.3	139.0	141.3	138.5	3.4	5.6	6.3	5.4	7.4	2.3	100	82	80	87	0.0	1.6	1.9	1.2	10 ☂ ═	6 ⊙	2	SW 20	SW 24	SW 20
9	144.1	145.3	145.5	145.0	4.4	8.4	6.0	6.2	9.6	3.8	76	71	94	80	2.0	5.3	0.6	2.0	2 ⊙	8 ⊙	0	SW 4	W 4	SE 6
10	143.3	142.6	141.1	142.3	5.8	7.8	9.3	8.0	10.0	5.2	92	82	79	84	0.7	1.9	2.5	1.7	3 ⊙	9	4	SW 12	S 9	S 14
11	140.3	141.2	141.8	141.1	6.8	8.2	9.8	8.6	10.7	6.3	100	94	89	94	0.0	0.6	1.3	0.6	10 ═	8	3	SW 12	SSW12	SSW20
12	142.2	143.7	143.8	143.2	10.3	14.1	14.7	13.4	16.6	8.8	92	77	67	79	1.0	3.8	5.4	3.4	1 ⊙	3 ⊙	2	SSW12	SW 7	W 6
13	144.3	145.1	145.2	144.9	15.4	18.7	16.7	16.9	19.5	13.9	66	63	63	64	6.0	7.9	7.2	7.0	3 ⊙	6 ⊙	2	W 6	C 0	NW 4
14	143.2	143.3	142.0	142.8	15.5	14.1	14.3	14.6	16.8	11.1	45	71	82	66	9.5	4.7	2.9	5.7	8 ●	9 ●	6	SW 10	SW 18	SW 8
15	138.5	138.8	136.4	137.9	15.5	15.8	10.7	13.2	17.1	10.3	68	73	87	76	5.6	4.7	1.7	4.0	9 (R)	9	10	SW 12	SW 8	W 20
16	136.2	137.5	138.7	137.5	8.6	10.9	9.9	9.8	12.9	7.3	79	79	87	82	2.5	2.7	1.7	2.3	7	8	9	W 7	SW 12	W 4
17	138.6	137.7	136.0	137.4	8.8	7.6	7.0	7.6	10.4	6.5	90	100	100	97	1.1	0.0	0.0	0.4	9	10 ●	10 ═	SW 7	SW 10	W 6
18	134.0	136.8	137.5	136.1	5.2	4.0	3.5	4.0	8.9	3.2	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ═	10 ═	10	WSW21	WNW12	WNW22
19	136.6	137.6	139.2	137.8	2.2	2.0	4.6	3.4	4.8	1.6	100	100	100	100	0.0	0.0	0.0	0.0	10 ═	10 ═	10 ☂ ═	NW 12	W 25	WNW24
20	139.0	140.4	139.6	139.7	4.3	5.3	4.5	4.6	5.7	3.8	100	100	100	100	0.0	0.0	0.0	0.0	10 ☂ ═	10 ☂ ═	10	NNW17	NNW17	N 10
21	137.8	138.3	138.2	138.1	7.0	10.4	8.8	8.8	11.9	3.9	79	77	97	84	2.1	2.9	0.3	1.8	1 ⊙	4 ⊙	10 ● ═	NW 2	SW 4	C 0
22	138.7	140.5	138.2	139.1	5.4	7.0	6.2	6.2	8.8	3.9	100	88	84	91	0.0	1.2	1.5	0.9	10 ● ═	9 ⊙	10	WNW10	SW 8	SSW22
23	138.5	141.0	139.4	139.6	2.8	5.2	5.6	4.8	7.6	2.3	100	88	77	88	0.0	1.0	2.0	1.0	7 ⊙	8 ⊙	6	W 20	W 9	W 22
24	135.2	134.7	135.1	135.0	6.4	9.0	8.4	8.0	11.4	4.4	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ═	10 ☂ ═	10 ● ═	WSW40	WSW27	WSW28
25	135.9	137.7	139.9	137.8	4.0	5.6	4.6	4.7	8.5	2.6	79	89	88	85	1.7	1.0	1.0	1.2	8	9	2	W 23	W 16	W 24
26	140.9	143.2	140.7	141.6	2.4	5.2	6.6	5.2	7.5	0.6	80	85	80	82	1.5	1.3	1.9	1.6	6	7	0	W 20	WSW11	WSW22
27	137.0	137.3	138.9	137.7	6.8	9.8	6.4	7.4	11.9	5.0	74	87	86	82	2.6	1.6	1.3	1.8	4 ⊙	8 ⊙	2	SW 28	SW 25	W 17
28	139.8	141.8	142.0	141.2	1.6	5.2	6.6	5.0	6.9	1.3	98	82	66	82	0.2	1.5	3.2	1.6	8 ⊙	7 ⊙	5	W 25	W 10	WSW20
29	140.4	140.6	140.9	140.6	6.1	6.5	4.9	5.6	7.6	4.4	76	100	100	92	2.2	0.0	0.0	0.7	7 ⊙	10 ☂ ═	10 ☂ ═	W 18	W 18	NNW20
30	140.8	143.1	141.7	141.9	1.3	1.8	5.4	2.5	4.9	0.7	100	100	74	91	0.0	0.0	2.1	0.7	10 ☂ ═	8	3	NW 20	WNW14	NW 14
31	137.6	137.5	137.1	137.4	2.8	3.6	1.6	2.4	4.8	1.0	100	91	100	97	0.0	0.7	0.0	0.2	9	8 ⊙	10 ☂ ═	W 26	W 17	NW 28
M	138.9	139.9	139.7	139.5	7.2	8.8	8.1	8.0	10.8	5.4	89	87	87	88	1.4	1.7	1.6	1.6	7.4	8.2	6.2	15.4	12.7	13.4

Śnieżka H_s = 1603m H_t = 1610,6m Lipiec - Juillet 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ SNIEGU h	P O G O D A
1	7	2.3	pł.	◆0⁰⁰-5⁰⁵ ✱0⁴⁵-11¹⁵,12¹⁵ 13²⁰ ⚥ ▽ 18¹⁰-20 ◆-24 ⚥ ▽ 20⁴⁵-21¹⁰, ≫16³⁰-20³⁰,21³⁰-24, ≡ ²0⁰⁰-9⁵⁰ ═ -11¹⁵ ≡ ²12⁴⁰-13¹⁰ ═ -14³⁰,15⁵⁰-18²⁰ ≡ ²-24
2	0	6.5	pł.	⚥ ▽ 0⁴⁰-1¹⁰ ◆0⁰⁰-2¹⁰ 3²⁰-4⁵⁰ ⚥ ▽ ⚥ ▽ 7²⁵-8²¹ ◆8³⁰-16⁵⁰ ◆. 17⁴⁰ ◆19¹⁰-21³⁰ ◆. 24, ≫ 0⁰⁰-3⁰ 4³⁰-24, ≡ ²0⁰⁰-2¹⁰ ═ -3²⁰ ≡ ²-4⁵⁰ ═ -7⁰⁵ ≡ ²-17⁵⁰,18¹⁵-24
3	0	4.2	pł.	◆. ⁰0⁰⁰-3⁴⁰ ◆-6³⁰ ✱ ⁰-7⁴⁰ ◆-9⁴⁰ ⚥ ⁰-11⁵⁰-12⁰⁵ ⚥ ⁰12³⁰-13²⁰ ⚥ ▽ ¹³7⁰-14³⁰ ▽ ⚥ 16⁰⁰-10 ▽ ▽ ⁰-16²⁵ ⚥ ⁰17¹⁵-20 17⁴⁵-⁵⁵ ▽ ⚥ ⁰19⁵⁰-20²⁰ ⚥ ⁰20⁵⁰-21¹⁰ ▽ ⁰21⁴⁰-22²⁰,23⁵⁰-24, ≫ 0⁰⁰-30 ◆-24, ≡ ²0⁰⁰-9⁴⁰ ═ -11⁵⁰ ≡ ²24
4	0	2.0	pł.	⚥ ⁰0⁰⁰-2⁰ ✱13⁵⁰-15³⁰-16⁴⁰ ◆17³⁰-24, ⚥ 13⁵⁰-16⁴⁰ ◆ 0⁰⁰-24, ≡ ²0⁰⁰-24, ∨ ⁰0³⁰-17³⁰
5	7	1.4	pł.	◆0⁰⁰-3³⁰,7³⁰-13³⁰ ✱ ⁰19⁵⁰-20¹⁰ ◆ 0⁰⁰-13³⁰ ≫ 14¹⁰-16³⁰ 22²⁰-24, ≡ ²0⁰⁰-13³⁰ ═ -14³⁰-15¹⁰ ≡ ²19²⁰-22³⁰ ═ -24
6	7	4.1	pł.	◆3²⁰-5⁴⁰ ▲ ▽ ⁰-13⁵⁵-14¹⁰ ▲ ▽ ⁰14⁴⁰-15¹⁵ ⚥ ⁰-15⁴⁰ ▲ ▽ ⚥ ⁰17⁵⁰-18³⁰ ◆23⁵⁰ 24, ☈ 17⁵⁵-19⁵⁰ SW-SE, ≫ 0⁰⁰-3³⁰ ◆-6³⁰ ≫ -11³⁰ ◆-12⁰⁰ ≫ -14⁴⁰ ◆-16²⁰,17³⁰-18³⁰ ≫ 24, ═ 0⁰⁰-1³⁰ ≡ ²-2³⁰ ═ -3²⁰ ≡ ²-5⁴⁰
7	0	0.9	pł.	◆. ⁰0⁰⁰ 1⁴⁰ ◆13¹⁰-14¹⁰ ◆. -16⁴⁰ 17¹⁵ ◆-20¹⁰, ≫ 0⁰⁰-2²⁰ 3⁴⁰-6³⁰ ◆-15³⁰ ≫ 18¹⁵-24, ≡ ²1³⁰-12⁰⁵ ═ -13¹⁰ ≡ ²-20¹⁰ ═ -20⁴⁵ ≡ ²-23³⁰ ═ -24
8	7	.	pł.	≫ 0⁰⁰-8¹⁰ 8⁴⁰-9²⁰ 20³⁰-24, ═ 0⁰⁰-4⁴⁰ ≡ ²11³⁰ ═ -15²⁰ ≡ ²-18³⁰ ═ -19²⁰ ▭ 18³⁰-24
9	7	.	pł.	▭ 0⁰⁰-7³⁰ ═ 11⁴⁰-13³⁰,16¹⁰-19⁴⁰ ≡ ²-20¹⁵ [6.VI: ═ -6²⁰ ▭ -7¹⁰ ═ -14³⁰ ≡ ²-16²⁰ ═ -17³⁰ ≡ ²-18³⁰ ═ -20²⁰
10	7	.	pł.	
11	7	2.0	pł.	◆. ⁰8²⁰...30 gos...¹⁸ ⚥ ⁰17⁵⁰-18³⁰,19³⁰-20⁴⁰ ☈ ⁰17⁵⁰-20³⁰ SW-S, ≫ 4³⁰-7²⁰ ◆-10²⁰ ≫ -13¹⁰,14¹⁵-18¹⁰ ◆-20³⁰-23¹⁰ ≡ ²19⁴⁵-20⁰⁵, (☾) ⁰17⁵⁰-18³⁰,19³⁰-20²⁰, ∩ 18⁴⁵-⁵⁷
12	7	4.7	pł.	⚥ ▽ ⁰-14¹⁰-⁴⁵ ⚥ ▽ ⁰20⁵⁵-21⁴⁰ 22⁵⁰-23¹⁰ ☈ ⁰14³⁰-15¹⁵ SW-NE, ≫ 4⁴⁰-11³⁰ ◆-13³⁰ ≫ -14³⁰ ◆-16³⁰ ≫ -20³⁰,21³⁰-22⁴⁰ ◆-24, ═ 0¹⁰-3⁴⁰ ≡ ²-4³⁰ ═ 6³⁰-7¹⁰,18¹⁰-19⁴⁰ ═ -21⁴⁰, (☾) ⁰14³⁰-15⁰⁵
13	7	7.0	pł.	⚥ ▽ ⁰13⁵⁰-3⁴⁰ ⚥ ▽ ⁰-6¹⁰-7²⁰ ◆8³⁰-9⁵⁰ ◆. 11⁵⁰ ⚥ ▽ ⁰12³⁰,14¹⁰-³⁰ 16¹⁰-⁴⁰ ◆, 0⁰⁰-7³⁰ ≫ -9³⁰ ◆-10⁵⁰ ≫ 11¹⁵⁰-16²⁰ ◆-18³⁰ ≫ 24, ≡ ²1⁵⁰-13³⁰ ═ -16¹⁰ ≡ ²-16⁴⁰ ═ -20³⁰ ≡ ²-21²⁰ ═ -22³⁰ ≡ ²24, (☾) 11⁵⁰-12³⁰
14	7	0.6	pł.	⚥ ▽ ⁰4⁵⁰-6³⁰ ◆. ⁰10⁴⁰ ⚥ ▽ ⁰18⁰⁵-18²⁰, ≫ 0⁰⁰-2⁴⁰ ◆-17³⁰ ≫ -24, ≡ ²0⁰⁰-20 ═ -2⁴⁰ ≡ ²12⁴⁵ ═ -16³⁰,17⁴⁰-19⁴⁰ ≡ ²-20³⁰ ═ -21³⁰-24
15	7	8.2	pł.	⚥ ▽ ⁰10⁵⁰-12³⁰ ◆. ⁰⁻¹ 14⁴⁰ ⚥ ▽ 17⁵⁰-18²⁰ ⚥ ▽ ⁰19⁵⁰-20¹⁰ ◆. ⁰21⁵⁰ 22²⁰-23⁴⁰, ≫ ◆ 0⁰⁰-6³⁰ ≫ 11³⁰-12²⁰ 14²⁰-17³⁰ ═ 3³⁰-4³⁰ ≡ ²-13³⁰ ═ -17²⁰ ≡ ²-20³⁰,22³⁰-24
16	7	36.8	pł.	◆. ⁰⁻²4⁵⁰-6³⁰ 8⁴⁰-10⁴³ 12³⁵ ⚥ ▽ ⁰16⁴⁸-18¹⁵ ⚥ ▽ 19⁰⁴,21³⁰ ◆. ⁰21⁴⁵ 22⁴⁰; (☈) SE 14⁵⁵-15¹⁰; ≫ 20⁴⁰,24, ≡ ²0⁰⁰-10⁴⁰ ═ -11⁴⁰ ≡ ²-13³⁰ ═ -14⁴⁰ ≡ ²-16³⁰ ═ -18³⁰ ≡ ²-20⁴⁰ ═ -21³⁰ ≡ ²22⁰⁵-24, (☾) ⁰14⁴⁵
17	0	22.7	pł.	◆. ⁰⁻¹10⁵-4⁴⁵ ◆. ⁰⁻²5³⁰-14⁴⁰ ◆. ⁰15⁵⁰ 16⁴⁰,17⁵⁰ 18⁵⁰ ⚥ ▽ ¹19⁴⁰ ◆. ⁰⁻¹ 20¹⁰ ◆. ⁰21⁵⁰,23⁵⁰ 24, ≫ 0⁰⁰-9²⁰ 10³⁰-14⁴⁰,19⁴⁰,21³⁰, ≡ ²0⁰⁰-16⁴⁰ ═ -17³⁰ ≡ ²-19⁴⁰ ═ -20¹⁰ ≡ ²-24, (☾) 18⁵⁰-19⁴⁰
18	8	0.3	pł.	◆. ⁰0⁰⁰-5⁰ ≫ 3³⁰-11¹⁰ ◆ 21¹⁰-24, ≡ ²0⁰⁰-12¹⁰ ═ -13¹⁵ ≡ ²21⁰⁵-24
19	8	.	pł.	◆2⁴⁰-4³⁰,6¹⁵-11⁴⁰ ◆ 0⁰⁰-3³⁰ ≫ -8³⁰,13¹⁵-14²⁰, ═ 0⁰⁰-4³⁰ ═ -5¹⁰ ≡ ²-11⁴⁰ ═ -12⁰⁵
20	8	.	pł.	≫ 7¹⁵-8¹⁰,15³⁰-18¹⁰, ▭ 0²⁵-3³⁰ [16.VII: 15³⁰,19⁰⁴ 21³⁰
21	8	7.0	pł.	⚥ ▽ ⁰21¹⁶-22⁵⁰ (☈) ⁰⁻¹ 21⁰⁶-24 W-NE, ≫ ◆ 3¹⁰-24, ═ ²2⁴⁰-5³⁰ ═ -7⁴⁰ ≡ ²21²⁵-22¹⁸ ═ -22³⁵
22	8	0.6	pł.	⚥ ▽ ⁰0⁵³,1⁰⁸ ⚥ ▽ ²2⁰⁵-17⁵ ⚥ ▽ ⁰15³⁰-16³⁰, (☈) ⁰⁻¹ NE 0⁰⁰-⁴⁵ 15²⁰-16³⁰ SW-NE, ≫ 0⁰⁰-¹⁵ 15³⁰-17³⁰, 20⁴⁰-21²⁰, 23³⁰-24, ═ ²2²⁵-3²⁵ ▭ -9³⁰ ═ 16³⁰-⁴⁰, 21³⁰-22¹⁰
23	8	.	pł.	≫ 0⁰⁰-1⁴⁰, 22³⁰-24, ═ 7⁵⁰-9⁵⁰
24	8	.	pł.	≫ 0⁰⁰-6³⁰, ═ 3³⁰-8³⁰
25	8	.	pł.	≫ 13¹⁰-18³⁰ ◆-24
26	8	1.6	pł.	⚥ ▽ 18¹⁵-⁴⁰,19⁵⁰-20⁵⁰ ⚥ ▽ ²21¹⁰ ⚥ ▽ ⁰-24; (☈) ⁰17⁵⁰-20⁵⁰ W-SW ☈ ²⁻⁰-24, ◆ 0⁰⁰-1³⁰ ≫ -4³⁰ 5⁴⁰-9³⁰ ◆-13³⁰ ≫ -16²⁰ ◆-18³⁰ ≫ -19⁵⁰ ◆-24, ═ ²20³⁰-23³⁰ ═ -24, (☾) 17⁵⁰-24
27	8	2.8	pł.	⚥ ▽ ⁰0⁰⁰-5⁰ ⚥ ▽ ²⁻⁸9¹⁰-³⁰ ⚥ ▽ ⁰10⁵⁰-11¹⁰ 16⁴⁵-17²⁰, ☈ ⁰0⁰⁰-5⁰ ☈ ⁰9¹⁰-⁴⁰ SW-NE, ◆ 0⁰⁰-1²⁰ ≫ -13⁴⁰ ◆-16³⁰ ≫ 17³⁰-19³⁰ ◆-20³⁰ ≫ -24, ═ 0⁰⁰-1³⁰ ≡ ²-13⁴⁰ ═ 16⁴⁰-17²⁰ 19³⁰-22³⁰ ≡ ²24, (☾) 0⁰⁰-⁵⁰
28	7	.	pł.	◆1³⁰-10⁴⁰, ≫ 5³⁰-10⁴⁰ 18³⁰-23³⁰, ≡ ²0³⁰-10⁴⁰ ═ -12⁴⁰ ≡ ²-13³⁰ ═ -15²⁰, 23³⁰-24 [27.VII: (☾) 9¹⁰-³⁰
29	8	.	pł.	≫ 3³⁰-8³⁰, ═ 0⁰⁰-6²⁰ ▭ 5²⁰-6²⁰ ═ 7³⁰-8²⁰; 11⁰⁰-14²⁰
30	8	.	pł.	
31	8	0.0	pł.	≫ 23²⁰-24
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1	7	.	pł.	◆4⁴⁵ 5¹⁰, ≫ 0⁰⁰-2³⁰ ◆-6⁰⁰ ≫ -18¹⁰,10¹⁵-15³⁰,20¹⁵-22⁰⁵ ◆, 22¹⁰-24, ═ 15⁴⁰-16³⁰
2	7	.	pł.	◆, 0⁰⁰-2⁴⁰ ≫ -3³⁰,10³⁰-11²⁰,14³⁰-16³⁰,20⁴⁰-22³⁰ ◆-24
3	7	0.0	pł.	⚥ ▽ ⁰16⁴⁰-⁵⁰ ◆. ²17⁰⁶ ☈ ⁰14²⁸-17³⁰ N-S, ◆ 0⁰⁰-3⁰ ≫ -3⁵⁰, ≡ ²22³⁰-24
4	7	0.0	pł.	⚥ ▽ ⁰14¹⁰-²⁵, ≫ 0³⁰-3⁴⁰ ◆-9³⁰ ≫ -19²⁰, ≡ ²0⁰⁰-⁴⁵ 7³⁰-8⁴⁵ ═ -9²⁰,14³⁰-15²⁰
5	7	9.0	pł.	⚥ ▽ ⁰11³⁰-⁴⁰ ⚥ ▽ ¹19²⁰ ◆. ⁰13³⁰ ⚥ ▽ ⁰14⁵⁰,22³⁰-⁵⁰, (☈) ⁰21¹⁵-22³⁰ SW ☈ ²⁻⁰22⁴⁰ (☈) ⁰24, ≫ 4³⁰-11³⁰ ◆-12²⁰ 14³⁰-16²⁰ ≫ 20³⁰ ◆-21²⁰ 22⁴⁰-24, ═ ²11⁴⁰-13³⁰ ═ -14⁵⁰ ═ 15¹⁰-17⁴⁰ ≡ ²21³⁰-22⁴⁰
6	0	0.1	pł.	◆, 7¹⁰-11¹⁰ ⚥ ▽ ⁰12⁴⁰-13²⁰ (☈) ⁰0⁰⁰-⁵⁰ ◆, 0⁰⁰-1²⁰ ≫ -13³⁰ ◆-17³⁰ ≫ -22³⁰ ◆-24, ═ ²0³⁰-1³⁰ ═ -6²⁰ ≡ ²-16²⁰ ═ -17³⁰ ≡ ²-24
7	0	2.9	pł.	◆, 13⁵⁰-14¹⁰ ◆. ⁰14¹⁰ 15⁴⁰,17²⁰ 20⁵⁰, ◆, 23²⁰-24 ◆ 0⁰⁰-14³⁰ ≫ -15³⁰ ◆-24, ═ ²0⁰⁰-⁵⁰ ═ 2²⁰-6³⁰ ≡ ²-7⁴⁰ ═ -8³⁰ ≡ ²-18³⁰ ═ -19²⁰ ≡ ²-20¹⁵ ═ -20³⁰ ≡ ²-24
8	8	.	.	◆, 0⁰⁰-9⁰⁵, ◆ 0⁰⁰-17¹⁰ ≫ -20⁴⁰ ◆-24, ═ ²0⁰⁰-9⁰⁵ ═ -10³⁰
9	8	.	.	◆ 0⁰⁰-4⁴⁰ ≫ -6¹⁰
10	7	.	.	≫ 7³⁰-8¹⁰,14¹⁵-22¹⁵ ◆-24
11	8	.	.	◆ 0⁰⁰-3³⁰ ≫ -20¹⁵ ◆-24, ═ ²4²⁰-9¹⁵
12	8	.	.	◆ 0⁰⁰-5¹⁵ ≫ -13²⁰, ═ 3²⁰-5⁴⁰
13	8	11.4	.	
14	7	2.3	.	⚥ ▽ ⁰5⁴⁰-⁴⁵ ▲ ⁰6⁰³-⁰⁵ ⚥ ▽ ⁰-8⁰⁵ ⚥ ▽ ⁰11²⁵-12²⁰ 13⁵⁰-14²⁰,14⁴⁰-⁵⁰ 15⁵⁵-16⁰⁵, ☈ ⁰5⁵⁰-6¹⁰-7¹⁵ N-S, 11⁵⁰-12³⁵ W-E (☈) ⁰20²⁰-21⁵⁰ W-E, ≫ 7¹⁰-5³⁰ ◆, 7¹⁰-⁴⁰ ≫ ◆ 8²⁰,18³⁰ ≫ 23³⁰,24, ═ ²4³⁰-5⁴⁰ 11³⁰-12²⁰ ▭ 16¹⁰
15	7	1.1	.	⚥ ▽ ⁰5²⁰-6⁰⁵ 8⁰⁵-⁵⁰ 17²⁴,18¹⁰ (☈) ⁰W 5¹⁰-8⁵⁵ 9²⁵-³⁵ ☾ ²21²³-⁴⁵ E, ≫ ◆ 0⁰⁰-5²⁰ 6³⁰-12⁴⁰ 15²⁰-24, ▭ 0⁰⁰-5⁴⁰ ═ ²-5⁵⁰ ═ ²17⁴³-18¹⁵, ☾ ²4⁵⁰-5⁴⁰ (☈) ⁰-7³⁰
16	8	0.2	.	◆, 1⁴⁰-5²⁵ ⚥ ▽ ⁰16⁵⁴-17⁰⁵ 23¹⁰-²⁰, ◆ 0⁰⁰-2³⁰ ≫ -4¹⁰ 12³⁰-14³⁰ ◆-15³⁰, ═ ²1⁴⁰-5²⁵ ═ 16¹⁰-³⁰
17	7	4.5	.	◆. ⁰10⁵⁰ 12³⁰-16⁴⁰, ≫ 11²⁰-19³⁰, ═ ²10³⁰-12²⁰ ═ -12⁵⁰ ═ ²-13³⁰ ═ -15⁴⁰ ═ ²-24
18	0	2.2	.	◆, 4³⁰-5⁵⁰ ◆. ⁰8¹⁰ ◆ 13⁰-10³⁰ ≫ -15⁴⁵ ◆-16³⁰ ≫ -17¹⁰ ◆-24, ═ ²0⁰⁰-8¹⁵ ▭ -8⁵⁰ ═ 9⁰⁵-10⁴⁰ ═ ²14¹⁵ ═ -15³⁰,16³⁰-17³⁰,18⁴⁰-24
19	0	5.3	.	◆. ⁰0¹⁴-2⁴⁵ ⚥ ▽ 17³⁰-24, ◆ 0⁰⁰-7³⁰ ≫ -9³⁰ ◆-24, ═ 0⁰⁰-6⁴⁰ ═ ²-24
20	0	0.3	.	◆, 0⁰⁰-14³⁰, ◆ 0⁰⁰-4³⁰ ≫ -6⁵⁰ ◆-14³⁰ ≫ -22³⁰, ═ ²0⁰⁰-20⁰⁵ ═ -24
21	8	2.7	.	◆. ⁰21⁵⁰-23⁴⁰, ═ 0⁰⁰-3⁰ 23⁰-6³⁰ ▭ -8³⁰ ═ -10⁴⁰, 20³⁰-21¹⁰ ═ ²-24
22	7	0.3	.	◆. ⁰7³¹-8⁴⁵, ≫ 2³⁰-10¹⁵,15⁵⁰-20³⁰ ◆-24 [14.VIII: -24, (☾) ⁰5⁴⁰ 7¹⁵,7⁴⁰ 8³⁰,11⁵⁰-12⁴⁰
23	8	0.0	.	◆. ⁰7²⁰ 3⁴⁵, ◆ 0⁰⁰-11⁴⁰ ≫ -11⁴⁵,18³⁰-20³⁰ ◆-24, ═ ²2¹⁵-4³⁰,6¹⁰-8³⁰, ∪ 4⁵⁰-6³⁰
24	0	5.6	.	◆. ⁰7³⁰ 12⁵⁵ ◆. ⁰15²⁵ ◆ 15⁵⁵ 16¹⁰ 19⁵⁰ 24, ◆ 0⁰⁰-24, ═ ²5³⁰-6²⁰ ═ ²-15²⁵ 20²⁵-24, ∩ 15⁵⁵-16³⁰
25	7	.	.	◆. ⁰0⁰⁰...¹⁵ ◆. ⁰⁻²2²⁸, ◆ 0⁰⁰-24, ═ ²0⁰⁰-2³³ 11⁴⁵-12⁰⁵ ═ -13¹⁰ 23⁴⁰-24
26	8	.	.	◆, 0⁰⁰-10³⁰ ≫ -19²⁰ ◆-24, ═ 0⁰⁰-1⁰ ═ ²-1³⁰ ═ -2³⁰ 4¹⁰-8²⁰ 11⁴⁰-12²⁰
27	8	.	.	◆, 0⁰⁰-24, ═ ▭ 7³⁰-8²⁰ ═ 9³⁰-11²⁵
28	8	.	.	◆, 0⁰⁰-10²⁰ ≫ -18³⁰ ◆-19²⁰ ≫ -20³⁰ ◆-24, ═ ²2³⁰-3³⁰ ═ -5⁴⁵ ═ ²-6³⁰ ═ -8¹⁵
29	0	1.6	.	◆. ⁰8³³ 9⁰⁵-9⁴⁵,12³⁰...13⁴⁵ ◆, 10³⁰-16³⁵ ◆. ⁰18³²-19⁴⁰ ◆, 20³⁰-24, ◆ 0⁰⁰-2³⁰ ≫ -7⁴⁵ ◆-24, ═ 9¹⁰-²⁵ ═ ²-16³⁵ ═ -20³⁰ ═ ²-24
30	7	.	.	◆, ⁰0⁰⁰-⁴⁵ ◆, ⁰-1³⁰ ◆, -4³⁰ 5⁴⁵-9²⁰, ◆ 0⁰⁰-10³⁰ ≫ -11²⁰,13³⁰-14²⁰,20³⁰-24, ═ ²0⁰⁰-4³⁰ ═ -5⁴⁵ ═ ²-12²⁰ ═ -12⁴⁰ ═ ²-13³⁰ ═ -15⁴⁰,17³⁰-18²⁰
31	7	4.4	.	◆, 10¹⁰-11¹⁰,21²⁰-24, ≫ 0⁰⁰-3⁰ ◆-14³⁰ ≫ -15⁵⁰ ◆-24, ═ 1⁴⁰-8⁰⁵ ═ ²-11¹⁰ ═ -13³⁰,17⁰⁵-⁴⁰ ═ ²21²⁰-24
Σ	—	52.9	—	UWAGI

Śnieżka φ=50°44' λ=15°44' Wrzesień - Septembre 1962

DNI	CIŚNIENIE P=700 I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE N I	II	III	POGODA	KIERUNEK I PRĘDKOŚĆ WIATRU D.v I	II	III
1	139.2	142.8	144.4	142.1	1.7	2.4	2.4	2.2	3.4	1.3	100	100	100	100	0.0	0.0	0.0	0.0	10	10	3		N 25	N 12	NW 12
2	144.5	145.2	143.9	144.5	5.5	8.2	8.4	7.6	9.4	1.7	38	72	61	57	5.5	3.1	4.3	4.3	1	10	0		C 0	SW 8	SW 12
3	143.5	143.9	141.8	143.1	10.0	13.8	12.6	12.2	15.7	7.2	59	57	49	55	5.1	6.9	7.4	6.5	5	1	1		N 3	S 2	SW 12
4	140.1	138.8	134.2	137.7	13.7	16.1	13.5	14.2	17.0	10.8	56	56	74	62	6.8	8.0	4.1	6.3	1	5	0		SW 4	SW 14	SW 26
5	130.8	132.2	131.9	131.6	8.0	6.6	6.3	6.8	13.5	5.8	100	100	80	93	0.0	0.0	1.9	0.6	10	9	4		SW 18	SW 22	SW 20
6	131.0	131.4	128.7	130.4	5.0	7.2	9.9	8.0	9.9	4.5	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10		SW 26	SW 26	SW 30
7	124.1	126.0	129.5	126.5	8.0	4.3	3.7	4.9	9.9	3.3	100	100	100	100	0.0	0.0	0.0	0.0	10	8	6		SW 30	SW 35	W 25
8	131.9	133.6	134.2	133.2	2.2	2.8	1.0	1.8	3.7	0.7	100	93	96	96	0.0	0.6	0.3	0.3	10	8	10		WSW10	WSW12	WSW26
9	138.7	142.8	143.3	141.6	-0.2	1.6	3.6	2.2	3.7	-0.6	100	100	78	93	0.0	0.0	1.7	0.6	10	10	4		W 14	NW 4	SW 12
10	141.3	141.9	139.5	140.9	4.0	11.5	9.0	8.4	12.9	2.0	77	32	79	63	1.8	9.2	2.5	4.5	1	0	6		SSW14	SW 12	SW 30
11	138.5	139.3	141.4	139.7	8.2	8.8	7.3	7.9	14.5	6.7	100	100	93	98	0.0	0.0	0.7	0.2	9	9	5		SW 24	WSW17	NNW20
12	138.2	134.8	134.9	136.0	8.1	11.5	10.1	10.0	15.5	6.7	100	100	83	94	0.0	0.0	2.2	0.7	10	7	7		WSW30	WSW36	WSW32
13	136.9	139.2	141.3	139.1	3.4	1.4	0.8	1.6	10.1	0.4	100	92	96	96	0.0	0.6	0.3	0.3	10	8	10		WSW14	NW 18	NW 18
14	142.9	144.7	143.1	143.6	-1.4	5.1	6.4	4.1	7.1	-2.0	99	82	26	69	0.1	1.6	7.2	3.0	10	3	5		NW 12	SW 4	SW 4
15	140.3	138.2	137.1	138.5	5.8	7.2	7.2	6.8	7.9	4.4	5	36	82	41	5.0	6.5	1.9	4.5	1	8	2		SW 8	S 18	SW 20
16	135.6	135.8	135.8	135.7	11.1	13.1	6.8	9.4	14.4	6.6	83	72	100	85	2.2	4.2	0.0	2.1	8	3	10		SW 24	SW 8	SW 14
17	133.8	133.2	133.5	133.5	4.0	2.0	1.0	2.0	7.5	0.6	100	100	96	99	0.0	0.0	0.3	0.1	10	10	10		NW 9	NW 5	NW 4
18	130.8	129.9	129.5	130.1	-0.2	-0.4	-1.6	-1.0	2.2	-1.9	96	100	98	98	0.2	0.0	0.1	0.1	8	10	10		NW 8	NW 8	NW 2
19	131.0	133.1	135.1	133.1	-1.8	-0.6	-1.0	-1.1	0.1	-1.9	98	99	99	99	0.1	0.0	0.1	0.1	10	10	10		NW 1	W 8	WNW10
20	136.5	137.8	138.1	137.5	-0.4	0.4	-0.2	-0.1	1.0	-1.7	94	100	96	97	0.4	0.0	0.2	0.2	1	9	0		W 2	N 4	NW 16
21	138.3	139.0	138.0	138.4	-0.8	-1.2	-0.4	-0.7	0.3	-1.9	99	95	100	98	0.0	0.3	0.0	0.1	10	8	10		NW 16	NW 12	WNW15
22	137.9	140.0	140.7	139.5	-0.2	0.2	0.3	0.2	0.4	-0.7	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10		NW 20	NW 18	NW 22
23	137.9	136.7	136.5	137.0	-0.7	-0.6	-1.8	-1.2	0.4	-2.1	99	99	98	99	0.0	0.0	0.1	0.0	10	10	10		NW 20	NW 18	NW 16
24	139.4	142.0	143.9	141.8	-0.6	0.1	-0.2	-0.2	0.4	-1.9	99	100	100	100	0.0	0.0	0.0	0.0	10	10	10		NW 12	NW 8	NW 4
25	144.2	144.3	141.9	143.5	-0.8	1.7	0.4	0.4	1.8	-1.9	99	86	100	95	0.0	0.9	0.0	0.3	10	8	10		SE 6	SSE 6	S 20
26	139.6	140.4	139.1	139.7	0.8	5.8	4.2	3.8	6.9	0.3	100	66	93	86	0.0	3.2	0.5	1.2	0	1	0		SW 20	SW 18	SSW18
27	138.1	137.1	136.0	137.1	7.6	7.4	3.5	5.5	8.3	3.5	38	69	98	68	6.4	3.2	0.1	3.2	7	7	8		S 6	SSW 3	S 6
28	135.2	135.6	135.4	135.4	3.2	7.2	4.1	4.6	7.7	2.1	87	82	100	90	1.0	1.9	0.0	1.0	8	9	8		C 0	S 3	S 8
29	135.0	136.0	138.2	136.4	4.8	7.2	6.0	6.0	8.4	3.3	82	84	73	80	1.6	1.7	2.6	2.0	7	7	2		S 1	SW 3	NNW 4
30	140.1	141.1	141.7	141.0	5.4	8.4	5.8	6.4	10.5	4.5	100	84	100	95	0.0	1.7	0.0	0.6	10	4	0		SW 7	SW 7	S 13
31																									
M	137.2	137.9	137.8	137.6	3.8	5.3	4.3	4.4	7.5	2.0	87	85	88	87	1.2	1.8	1.3	1.4	7.6	7.4	6.0		12.8	12.3	15.7

Październik - Octobre

1	143.0	144.6	145.9	144.5	7.3	11.0	8.7	8.9	12.9	3.2	63	62	90	72	3.7	5.0	1.1	3.3	4	2	2		S 6	S 8	S 3
2	146.6	147.1	146.3	146.7	11.0	12.7	8.6	10.2	13.2	7.9	31	68	82	60	9.1	4.8	2.1	5.3	2	1	0		S 3	S 6	S 14
3	145.4	146.1	147.1	146.2	7.4	11.1	9.7	9.5	11.9	7.0	100	68	87	85	0.0	4.2	1.6	1.9	5	1	0		SSW16	SSW12	SSW 5
4	146.5	146.9	145.8	146.4	11.1	14.5	9.4	11.1	15.4	8.9	43	70	100	71	7.5	5.1	0.0	4.2	6	7	10		NNE 3	N 2	NNW 8
5	145.1	145.3	145.5	145.3	7.2	6.2	4.8	5.8	9.4	4.3	100	100	100	100	0.0	0.0	0.0	0.0	10(R)	10	10		N 10	NNW 3	N 5
6	144.5	144.8	148.1	145.8	1.5	0.0	3.0	1.9	5.0	-0.5	100	93	100	98	0.0	0.4	0.0	0.1	10	10	10		NNW14	NNW19	NNW15
7	149.1	150.0	151.4	150.2	3.5	4.1	3.4	3.6	4.3	3.0	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10		NNW11	N 14	NE 12
8	151.5	152.5	152.3	152.1	3.8	8.2	8.2	7.1	9.3	1.7	86	70	52	69	1.1	3.3	5.3	3.2	0	0	1		SE 6	S 11	S 13
9	151.3	151.0	149.1	150.5	7.6	10.9	9.0	9.1	11.4	6.6	50	42	44	45	5.2	7.5	6.5	6.4	1	1	0		S 10	SW 4	S 8
10	146.9	146.3	144.4	145.9	8.8	11.7	8.2	9.2	12.8	7.8	31	42	52	42	7.8	7.9	5.3	7.0	0	2	0		SE 4	SE 3	S 7
11	142.4	141.1	139.1	140.9	7.8	10.4	7.1	8.1	11.5	5.8	34	37	60	44	7.1	8.1	4.0	6.4	2	1	1		S 7	S 5	S 6
12	137.9	138.8	139.2	138.6	5.6	9.4	4.8	6.2	9.8	4.7	72	59	94	75	2.5	4.8	0.6	2.6	0	1	0		NNE 5	SSW 1	E 6
13	139.0	138.3	135.6	137.3	4.2	6.2	4.8	5.0	6.7	4.0	100	83	97	93	0.0	1.6	0.3	0.6	8	3	8		S 12	S 13	SW 28
14	133.9	134.2	135.9	134.7	2.8	0.5	-1.2	0.2	4.8	-2.6	96	100	99	98	0.3	0.0	0.1	0.1	8	10	10		S 4	N 13	N 15
15	138.9	141.4	142.8	141.0	-1.2	-1.2	-5.0	-2.1	0.2	-5.3	99	97	93	96	0.1	0.2	0.4	0.2	10	9	8		N 10	NNW 3	N 2
16	141.2	140.4	141.1	140.9	-3.2	0.6	0.1	-0.6	1.6	-3.6	95	96	100	97	0.2	0.3	0.0	0.2	8	7	9		W 3	C 0	NW 8
17	142.2	143.4	143.9	143.2	0.4	1.7	1.4	1.2	2.2	-0.7	96	100	100	99	0.3	0.0	0.0	0.1	4	10	10		W 6	NW 3	NW 14
18	142.8	142.2	137.5	140.8	5.6	8.6	6.1	6.6	9.3	0.1	44	85	100	76	5.1	1.8	0.0	2.3	8	8	6		NNW12	NNW12	W 26
19	134.2	135.4	135.4	135.0	2.2	-0.4	-1.0	0.0	6.3	-2.0	100	98	99	99	0.0	0.1	0.1	0.1	10	9	10		NW 20	NW 16	NW 20
20	136.9	140.2	144.5	140.5	-1.6	-0.9	-1.2	-1.2	-0.4	-1.9	98	99	99	99	0.1	0.0	0.1	0.1	10	10	10		NW 16	NW 16	NW 12
21	146.7	148.7	148.5	148.0	0.4	3.8	5.8	4.0	6.5	-6.6	60	61	28	50	2.5	3.1	6.6	4.1	0	0	0		N 10	N 2	N 4
22	147.7	147.6	146.8	147.4	6.8	8.7	8.0	7.9	9.1	5.0	24	45	31	33	7.5	6.1	7.5	7.0	0	0	0		ENE 3	SSW 1	S 2
23	145.2	144.9	143.6	144.6	7.2	7.6	7.6	7.5	8.3	6.2	35	41	19	32	6.7	6.1	8.3	7.0	1	1	0		SSW 2	SW 9	SSW 2
24	141.1	141.3	140.5	141.0	6.2	7.0	0.0	3.3	8.4	-0.4	11	56	100	56	19.4	4.4	0.0	7.9	0	0	1		S 6	C 0	N 8
25	139.8	139.6	137.5	139.0	0.4	3.2	-1.2	0.3	4.7	-1.6	94	80	99	91	0.4	1.5	0.1	0.7	0	5	10		NW 2	N 1	S 10
26	136.2	136.2	134.5	135.6	-0.6	2.6	0.3	0.6	3.4	-2.5	99	98	100	99	0.0	0.2	0.0	0.1	8	7	10		SW 9	SW 7	SW 17
27	133.2	134.3	134.1	133.9	3.6	2.4	0.8	1.9	6.1	-0.5	66	93	100	86	2.7	0.6	0.0	1.1	6	10	10		SW 12	SW 8	SW 18
28	131.1	130.1	129.9	130.4	0.2	-2.0	-0.8	-0.9	3.0	-4.3	100	62	31	64	0.0	2.0	5.0	2.3	10	9	9		SW 14	SW 16	W 4
29	129.3	130.7	134.4	131.5	-5.9	-2.3	-5.6	-4.5	-0.3	-5.9	96	97	95	96	0.2	0.1	0.2	0.2	10	10	9		W 3	N 6	N 8
30	135.0	133.1	128.8	132.3	-3.2	-2.4	-3.8	-3.3	-1.9	-6.4	65	59	96	73	1.6	2.1	0.2	1.3	1	1	10		S 2	SSW12	SW 25
31	127.8	127.7	128.2	127.9	-1.7	-1.2	-2.2	-1.8	1.4	-6.2	47	56	98	67	2.9	2.5	0.1	1.8	7	9	10		WSW 8	SW 8	NE 4
M	141.0	141.4	141.2	141.2	3.5	4.9	3.2	3.7	6.7	0.9	72	75	82	76	3.0	2.7	1.8	2.5	5.1	5.3	5.9		8.0	7.5	10.6

Śnieżka H_s = 1603m H_t = 1610,6m Wrzesień - Septembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	0	•	•	,0^00-40 •^150 ,-3^50 •^0 ..6^30 ,-15^10; ≡²0^00-16^00 ==-18^15; ⊼ 0^00-13^30 ≫-22^20
2	7	•	•	≫16^30-18^30 ⊼-21^20 ≫-23^30; ⊔°5^00-10^00; ⊕ 12^30-16^10
3	8	•	•	≫20^40-24
4	8	0.2	•	⟨23^50-24; ≫0^00-3^10 10^30-15^30 ⊼-24
5	7	0.8	•	▽°1^50-2^10 ,5^30-7^30 9^40-11^50 ▽°-12^05 ,-13^10 ▲°▽°14^41-43; ⟨0^00-30; ⊼ 0^00-2^30 ≫-3^30 ⊼-24; ≡²0^30-2^30 ==-5^30 ≡²-13^10 ==-15^30
6	0	3.6	•	▽°2^40-3^10 ,6^30-18^50 ▽°-20^30 •-24; ⊼ 0^00-24; == 1^30-2^30 ≡²-24
7	9	7.0	•	,0^00-5^50 ▽°-8^05 •²-0 10^05-13^45 ▽°17^50 ..20^30; ⊼ 0^00-24; ≡²0^00-11^05 ==-20^40 ≡²-21^30 ==-24; ⌒ 18^05-06
8	7	3.2	•	•°3^50-4^30 5^45 6^20 •-7^45 •°7^50 ,-10^50 •°11^40 ▽°14^50-15^10 ▽°▲16^50-17^20; ⊼ 0^00-30 ≫-9^30 ⊼ 11^40-12^30 ≫-14^30 ⊼-24; == 0^40-2^30 ≡²1^40 ==-14^40 ≡²-15^20 ==-16^40 ≡²-17^30 ==-19^20 ≡²-22^20 ==-24; ⌒ 15^10-20
9	7	0.0	•	▲2^50-3^20; ⊼ 0^00-7^30 ≫-9^30 20^50-24; ≡ 0^00-10 ≡²-10^10 ==-10^40 ≡²-13^20 ==-15^30; 17^45-19^20; ∨°5^20-8^50
10	9	0.1	•	≫0^00-3^30 ⊼-6^20 ≫-11^30 ⊼-13^20 ≫-14^20 ⊼-24
11	7	0.5	•	•°7^50-8^45 •'10^23 ..12^45 •°14^25-44; ⊼ 0^00-24; == 8^30-9^40 10^35-11^05 ≡²-13^20 ==-15^30; 23^30-24
12	7	2.0	•	,3^05-5^40 6^30-9^20 11^20-13^30; ⊼ 0^00-24; ≡ 0^00-3^05 ≡²-5^30 ==-6^30 ≡²-13^30
13	8	0.0	•	,5^20-8^30; 23^30-24; == 2^30-3^20 ≡²-8^30 ==-13^35; 14^42-15^27; 16^40-21^35 ≡²-24; ⊼ 0^00-5^20 ≫-9^40 ⊼-24
14	8	0.0	•	,0^00-5^10; ⊼ 0^00-7^20 ≫-9^40; ≡²0^00-9^20 ▭-11^30 == 17^10-18^05; ∨5^10-9^10
15	8	•	•	≫8^20-13^15 ⊼-24; ⊕ 14^20-15^10
16	8	18.5	•	▽°8^01-08 ▽°-20^05-18 20^50-22^05 •°22^15 24; ⊼ 0^00-13^20 ≫21^40-22^30 ⊼-24; == 16^50-17^30 ≡²18^40-19^40 == -20^50 ≡²-22^10
17	0	2.6	•	•°0^30 ..2^40 ,-7^40 •-10^53 ,11^15-13^50 •-18^45; ⊼ 0^00-4^30 ≫-6^30; ≡²0^30-11^02 ==-11^15 ≡²-18^05 ==-18^20; 18^45-19^20; 19^35-21^10
18	0	11.7	•	*°10^50 12^40-13^10 *-14^30 *'-15^10 *-21^30 *'-22^40 *°-24; ≫10^40-11^05; 15^10-20^15; ▭ 6^30-7^40 == 7^20-9^40 ≡²-24; ⌓°1^30-6^00; ⊖ 2^30-3^10
19	0	0.2	4	*°0^00-4^30 10^20-11^40 12^40; ≫14^30-15^20; 21^40-24; ≡²0^00-17^30 == -20^20 ≡²-22^30 == -24; ∨°5^00-6^30 ∨'-7^30 ∨°-14^50; 19^30-24
20	7	1.0	pz.	⚘°1^30 ..14^05 ⚘°-14^45 ..15^50 ⚘°18^20-19^15; ≫0^00-4^20 18^30-21^30 ⊼-24; == 0^00-6^30; 9^10-10^30 == 12^50-14^10; 16^15-17^30 ≡²-18^15; 19^30-20^40; ∨°0^00-6^30
21	7	4.6	pz.	,18^30-19^20 *°23^50 24; ⊥²23^50-24; ⊼ 0^00-8^30 ≫-9^20 11^30-14^20 17^30-22^30 ⊼-24; == 0^30-2^30 ≡²4^10-8^40 == -9^20 ≡²12^30-13^20 == -14^30; 15^30-16^20 ≡²-24; ∨°4^10-9^20; 12^30-14^30; 15^30-16^20; 19^20-24
22	0	5.1	pz.	*°0^00 ..1^40 8^30; 9^50 ⚘°23^50-24; ⊥²0^00-1^40; ⊼ 0^00-24; ≡²0^00-22^30 == 23^10 ≡²-24; ∨°0^00-10^10
23	0	11.1	pz.	⚘°0^00-05 ⚘'3^50 4^05 ⚘°7^50; 10^30 *-17^20 •..18^30 •°-19^50 ▽22^20 *'23^20 *-24; ⊥²8^30-15^20 ⊥°-16^30 ⊥²-24; ⊼-0^00-17^20 ≫-20^30 ⊼-24; ≡²0^00-24; ∨°5^30-17^20; 19^50-24; ⟨19^50-22^20
24	0	•	5	*°0^00 7^10 ⊥²0^00-3^20 ⊼ 0^00-13^30 ≫-1^30; ≡²0^00-22^30; ∨°0^00-9^30; 18^30-22^30
25	8	•	pz.	,21^30-22^45; ≫18^30-19^30 ⊼-24; == 3^50-6^10 ≡²-8^10 == -9^30 ▭ 8^10-11^30 == 17^10-50 ≡²-22^45 == -24; ∨°6^10-8^10
26	8	•	pz.	⊼ 0^00-24; == 0^00-6^30
27	7	•	pz.	⊼ 0^00-3^20 ≫-6^30; ▭ 11^30-17^30 == 23^30-24; ⊕ 12^30-18^30
28	7	•	pz.	== 0^00-2^30 ▭ 7^30-9^40 == 19^40-23^05
29	7	•	pz.	
30	7	•	pz.	≫8^30-11^20; 18^30-21^30 ⊼-24; == 5^30-6^05 ≡²-8^02 == -8^30 ≡²-9^20 == -11^20 ≡²23^30-24
31				
Σ	—	72.2	—	UWAGI.

Październik - Octobre

1	8	•	•	⊼ 0^00-4^10; ≡²0^00-2^30 == -4^10
2	8	•	•	≫16^30-24
3	8	•	•	⊼ 6^30-8^40 ≫-14^20; == 6^30-9^15; ⌓ 6^30-10^00
4	8	1.2	•	≫16^30-18^20; == 15^10-30 ≡²-16^30 == -17^20 ≡²-24
5	0	12.1	•	•°3^50 4^50 ,12^40-18^40 •°-20^30 ,-22^30 •°-24; (R)*4^57-5^50 NW-NE, 6^35-7^40 N-SSE; ≫5^30-7^20; 23^10-24; ≡²0^00-7^30 == -12^30 ≡²-24
6	7	30.9	•	•°0^00-2^10 ,-5^45 •° 8^35 11^40 13^15 15^10-20 ,-17^30 •-19^10 •-23^30 •°-24; ≫0^00-8^30 ⊼-19^40 ≫-24; ≡²0^00-9^10 == 13^20-45 ≡²-24
7	0	2.7	•	•°0^00-2^30 ,-6^10 •'-7^35 •°..8^10 ,-10^45 •°..11^40 ,-24; ≫0^00-8^30; 12^45-13^30; 14^50-21; ≡²0^00-24
8	8	•	•	,0^00-30; ≫4^50-5^40; 8^30-24; ≡²0^00-30 ▭ 4^50-10^10
9	8	•	•	≫0^00-8^30; ▭ 8^50..13^00
10	9	•	•	
11	9	•	•	
12	9	•	•	▭ 8^30-21^10 == -22^30 ▭ -24; ⌓ 1^30-7^30
13	8	•	•	,23^20-24; ≫6^20-11^30 ⊼-12^20 ≫-13^30 ⊼-24 == 5^30-12^20; 17^30-21^40 ≡²-24
14	0	2.6	•	,0^00-2^30; ⊼ 0^00-13^0 ≫-3^20; 12^30-14^15; 17^10-22^20; ≡²0^00-3^30 == -5^20 ▭ -6^20 == -8^35 ≡²10^05-24; ∨°18^40-24
15	8	0.1	1	*°0^30-45 2^35-4^40; 15^55 17^50; ≫3^15-8^20; ≡²0^00-11^20 == -15^40 ≡²-19^20 == -20^40 ▭ 20^25-22^20; ∨°0^00-11^20; 17^30-19^20 ⌓°21^10-24; ⊖ 22^35-23^20.
16	7	•	1	≫19^30-20^30; ▭ 4^20-6^20 == 6^12-7^35 12^15-30 13^10-30 14^30-18^20; 20^30-21^30 ≡²-22^20; ⌓°0^00-11^00
17	0	0.1	pz.	,16^45-24; ≫7^30-9^10; 16^20-24; ≡²1^20-6^30 == 6^40-10^20 ≡²-14^10 == -16^45 ≡²-24
18	9	0.8	•	,0^00-4^20; ≫0^00-3^40 6^20-14^30 ⊼ 16^30-18^30; ≡ 0^00-4^20 == -6^20 ▭ 5^10-17^50 == 20^30-22^30
19	8	1.2	•	▽°3^50-4^10; ,4^30-11^40 ⊼ 0^00-24; ≡²2^20-12^25 == -13^10 ≡²-24; ∨°13^20-24
20	0	4.2	•	▽°7^50-9^05 *°9^10-10^50; ⊥ 7^50-18^30; ⊼ 0^00-18^30 ≫-24; ≡²0^00-24; ∨°0^00-24
21	9	•	1	≫0^00-3^30 ⊼-4^30 ≫-8^20; ≡²0^00-1^50 == -3^10 ▭ 5^30-14^30; ∨°0^00-3^10
22	9	•	pz.	
23	9	•	pz.	≫14^30-16^20
24	7	0.2	•	== 14^35-15^40 ▭ -23^30 == -21^50-22^30
25	7	0.1	•	≫17^30-24; == 18^30-20^40 ≡²-21^20 == -22^30 ≡²-24; ≫17^30-24; ⌓°5-10 ∨°19^20-24
26	8	•	•	≫0^00-2^20; 4^30-6^20 ⊼ 7^30-9^30 ≫17^30-19^30 ⊼-24; ≡²0^00-1^30 == 5^30-13^15 ▭ 8^30-11^10 == 18^50-19^30 ≡²-21^10 == -24; ∨°0^00-1^30 ⌓°5^30-10^20
27	7	3.3	•	•°12^15-50; 13^50 ..16^10-22^30; ⊼ 0^00-15 ≫-6^15 ⊼-6^40 ≫-8^30; 16^30-19^30 ⊼-24; == 0^00-30; 10^50-12^30 == 16^30-17^10 ≡²-24
28	8	1.0	•	•°1^30-3^40 ▽°-8^50 •°10^20-12^05 ⚘°-12^05-40; ⊼ 0^00-4^30 ≫-9^20 ⊼-11^30; 12^20-16^30; ≡²0^00-12^10 == -12^30 ▭ 13^10-21^30; ~°4^10-8^50
29	0	2.0	1	*°3^50 4^20-5^20 ..10^10-15^30; ≫16^30-20^30; ≡²4^20-15^50 == 16^10-19^30 ≡²-20^45; ∨°6^30-15^50; 16^10-20^45
30	8	0.1	2	≫10^30-15^15 ⊼-24; == 5^40-6^10 ▭ -20^30 == 11^05-30; 17^50-18^15 ≡²20^30-24; ∨°5^40-6^10; 20^30-22^30 ∨°-24
31	8	22.5	2	▽°10^50-20^05 *'20^10-24; ⊥°22^30-24; ⊼ 0^00-3^10 ≫-4^30; 22^30-24; ≡²0^00-1^30 == -2^50 ≡²-3^30 ▭ -21^50 ≡²-24; ∨'0^00-1^30 ∨°-3^30; 21^50-24
Σ	—	85.1	—	UWAGI.

Śnieżka — φ = 50°44' — λ = 15°44' — Listopad - Novembre 1962

DNI	CIŚNIENIE P= 700 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	125.9	126.3	127.6	126.6	-3.4	-3.4	-2.2	-2.8	-1.9	-4.2	97	97	98	97	0.2	0.2	0.1	0.2	10 ✳ ≡	10 ✳ ≡	10 ≡	N 14	N 16	N 12
2	129.9	131.3	132.4	131.2	-0.4	2.2	1.4	1.2	2.2	-2.8	100	90	72	87	0.0	0.7	2.0	0.9	10	4 ⊙	3	WSW 2	SSW 4	SSW18
3	132.2	132.7	135.3	133.4	-0.1	0.4	6.4	3.3	6.5	-1.6	92	70	5	56	0.5	1.9	9.1	3.8	6 ⊙	4 ⊙	0	SSW22	SSW24	SSW 6
4	134.0	133.0	131.3	132.8	4.2	1.2	-0.6	1.0	7.0	-0.7	46	92	99	79	4.4	0.5	0.0	1.6	3 ⊙	5 ⊙	10 ≡	SSW20	SW 33	SW 22
5	128.8	127.6	124.9	127.1	0.2	1.6	1.8	1.4	2.2	-1.2	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	9 ⊙	10 ≡	SW 26	SW 40	SSW40
6	124.4	124.3	127.9	125.5	1.4	1.8	2.0	1.8	2.8	0.9	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	10 ● ≡	10 ● ≡	SSW30	S 35	S 34
7	133.5	137.6	137.4	136.2	2.4	10.8	3.4	5.0	11.2	1.6	100	45	100	82	0.0	7.2	0.0	2.4	10 ● ≡	9 ⊙	10 ● ≡	S 18	SSE 2	SE 16
8	132.5	131.2	130.5	131.4	4.2	4.8	3.0	3.8	4.9	2.8	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	10 ● ≡	10 ● ≡	SSW35	SSW33	SSW30
9	131.5	131.3	132.1	131.6	2.4	2.9	3.3	3.0	3.8	1.9	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	10 ● ≡	10 ● ≡	SSW22	SSW16	S 13
10	130.6	130.5	132.4	131.2	-0.2	-3.2	-6.4	-4.0	3.5	-6.7	100	97	94	97	0.0	0.1	0.2	0.1	10 ≡	10 ≡	10 ≡	NNE12	NNE18	NNE16
11	131.8	132.3	132.1	132.1	-8.0	-5.4	-1.8	-4.2	-1.8	-9.1	93	95	98	95	0.2	0.2	0.1	0.2	10 ≡	10 ≡	10 ≡	NNE18	NE 3	S 8
12	132.3	132.4	133.8	132.8	-1.3	0.2	-2.0	-1.3	0.6	-2.3	99	100	98	99	0.1	0.0	0.1	0.1	10 ♁ ≡	10 ✳ ≡	10 ≡	SE 4	C 0	W 4
13	134.2	134.8	135.5	134.8	-2.4	-2.1	-0.4	-1.3	-0.4	-3.2	98	98	100	99	0.1	0.1	0.0	0.1	10 ≡	10 ≡	10 ● ≡	SW 8	SW 10	WSW 2
14	135.5	135.6	134.9	135.3	-0.6	-0.4	-1.6	-1.0	-0.3	-1.8	99	100	98	99	0.0	0.0	0.1	0.0	10 ✳ ≡	10 ✳ ≡	10 ≡	N 3	NE 2	SW 8
15	129.2	125.7	123.1	126.0	-5.6	-3.5	-6.7	-5.1	-1.4	-7.2	97	97	94	96	0.2	0.1	0.2	0.2	10 ✳ ≡	10 ✳ ≡	10 ≡	SW 10	WSW10	SW 10
16	124.3	126.3	128.0	126.2	-8.2	-7.4	-9.0	-8.4	-6.4	-9.3	89	93	58	80	0.3	0.2	1.3	0.6	8	10 ✳ ≡	2	W 12	W 13	WNW13
17	128.8	126.6	121.4	125.6	-10.0	-9.1	-9.0	-9.3	-9.0	-10.6	91	92	92	92	0.3	0.3	0.3	0.3	9	10 ≡	10 ≡	NW 2	SSW 9	S 30
18	118.6	118.9	114.8	117.4	-8.5	-6.3	-4.4	-5.9	-4.4	-9.3	92	94	96	94	0.3	0.2	0.2	0.2	10 ≡	10 ≡	10 ≡	S 15	S 20	S 20
19	117.4	120.8	122.5	120.2	-6.0	-5.4	-4.6	-5.2	-3.5	-6.6	94	95	91	93	0.2	0.2	0.4	0.3	10 ≡	10 ≡	10 ✳	S 9	SW 15	SW 3
20	123.3	123.6	125.3	124.1	-5.7	-6.8	-7.6	-6.9	-4.4	-7.7	95	94	93	94	0.2	0.2	0.2	0.2	10 ≡	10 ≡	10 ≡	N 12	N 8	WNW 7
21	125.8	124.5	122.5	124.3	-10.0	-8.6	-7.8	-8.6	-7.6	-10.5	82	92	93	89	0.5	0.3	0.2	0.3	4	10 ≡	10 ≡	WNW 7	S 8	S 14
22	121.8	124.6	129.4	125.3	-8.6	-7.8	-9.3	-8.8	-7.8	-9.8	92	90	85	89	0.3	0.3	0.4	0.3	10 ≡	10 ≡	10 ≡	S 16	W 14	SW 10
23	132.0	134.1	136.1	134.1	-10.8	-8.4	-10.0	-9.8	-8.0	-11.5	90	92	91	91	0.3	0.3	0.3	0.3	10 ≡	2 ⊙	9	WSW14	NW 6	N 12
24	138.4	139.3	141.4	139.7	-9.4	-9.2	-5.4	-7.4	-5.4	-10.5	91	88	55	78	0.3	0.4	1.8	0.8	10 ≡	5 ⊙	0	N 12	N 8	NE 8
25	143.5	143.6	143.1	143.4	-2.2	-5.4	-4.6	-3.7	-1.6	-6.9	87	60	67	71	0.7	1.9	1.4	1.3	0	8	10 ✳	NNE 4	N 10	N 16
26	144.7	145.4	146.2	145.4	-1.0	-1.4	-3.4	-2.3	-0.9	-4.6	99	99	97	98	0.1	0.1	0.2	0.1	10 ≡	10 ≡	10 ≡	N 8	N 6	N 8
27	145.5	144.2	142.8	144.2	-2.4	-3.6	-2.2	-2.6	-1.1	-4.4	93	97	98	96	0.3	0.2	0.1	0.2	5	10 ≡	10 ✳ ≡	N 7	N 8	SE 6
28	140.1	140.1	139.9	140.0	-5.8	-3.6	-5.6	-5.2	-2.1	-6.7	82	69	95	82	0.7	1.5	0.2	0.8	0	1 ⊙	10 ≡	SW 2	N 4	N 8
29	139.9	140.0	137.1	139.0	-3.2	-1.6	-4.2	-3.3	-1.3	-6.1	97	98	96	97	0.1	0.1	0.2	0.1	9	10 ≡	10 ≡	N 6	NNW 5	WNW12
30	133.1	133.3	133.9	133.4	-2.8	-3.8	-7.2	-5.2	-2.3	-7.4	100	96	93	96	0.0	0.2	0.2	0.1	10 ≡	10 ✳ ≡	10 ✳ ≡	NW 16	NW 15	NW 17
31																								
M	131.4	131.7	131.9	131.7	-3.3	-2.6	-3.2	-3.1	-0.9	-5.2	93	91	89	91	0.3	0.6	0.6	0.5	8.5	8.6	8.8	12.9	13.2	14.1

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1	142.1	146.1	148.3	145.5	-9.4	-9.4	-11.4	-10.4	-7.2	-11.7	91	95	93	93	0.3	0.2	0.2	0.2	10 ✳ ≡	10 ✳ ≡	10 ✳ ≡	NW 16	NW 14	NNW18
2	150.8	152.2	151.5	151.5	-11.8	-9.7	-6.3	-8.5	-6.0	-13.1	71	60	42	58	0.7	1.2	2.2	1.4	7	3 ⊙	1	NNE10	E 3	C 0
3	149.2	148.2	146.5	148.0	-4.0	-0.8	-3.8	-3.1	-0.6	-8.0	39	60	40	46	2.8	2.4	2.8	2.7	0	5 ⊙	0	NE 3	SE 2	N 2
4	143.8	144.2	143.4	143.9	-5.4	0.2	-2.3	-2.4	0.2	-5.8	50	32	43	42	2.0	4.2	3.0	3.1	8	4 ⊙	4	N 8	N 8	N 12
5	140.5	141.4	144.1	142.0	-3.2	-2.2	-0.6	-1.6	-0.3	-3.9	52	74	76	67	2.3	1.4	1.5	1.7	10	2 ⊙	3	NNW22	NW 10	NW 10
6	145.2	145.8	145.7	145.6	0.6	2.6	1.6	1.6	4.3	-1.1	62	50	45	52	2.4	3.7	3.9	3.3	2	2 ⊙	4	N 12	C 0	N 2
7	144.4	144.9	145.6	145.0	-0.2	6.2	-0.6	1.2	6.7	-1.1	78	60	81	75	1.3	3.8	1.1	2.1	1	1 ⊙	0	N 2	N 2	NW 4
8	145.7	145.9	142.6	144.7	-0.2	1.8	-0.6	0.1	3.6	-1.3	82	60	60	67	1.1	2.8	2.4	2.1	3	8	10	NW 10	S 4	SW 16
9	132.6	123.7	120.4	125.6	-0.6	-7.6	-7.4	-5.8	0.1	-9.6	64	68	93	75	2.1	1.1	0.2	1.1	10	10	10 ✳ ≡	SW 30	SW 34	SW 26
10	120.2	118.8	121.0	120.0	-6.8	-6.6	-4.8	-5.8	-4.7	-8.7	94	94	95	94	0.2	0.2	0.2	0.2	10 ≡	10 ≡	10 ✳ ≡	SW 20	SW 22	NNW30
11	124.1	123.1	119.3	122.2	-5.6	-6.4	-6.4	-6.2	-4.8	-6.9	95	94	94	94	0.2	0.2	0.2	0.2	10 ✳ ≡	10 ✳ ≡	10 ≡	NNW26	W 24	SW 22
12	114.3	110.3	112.6	112.4	-6.0	-5.2	-8.2	-6.9	-4.4	-8.4	94	95	92	94	0.2	0.2	0.2	0.2	10 ✳ ≡	10 ≡	10 ✳ ≡	SW 24	SW 28	SW 18
13	112.7	113.1	116.7	114.2	-6.2	-6.2	-5.8	-6.0	-4.8	-8.5	94	94	95	94	0.2	0.2	0.2	0.2	10 ≡	10 ≡	10 ≡	S 14	SW 16	N 6
14	120.4	122.2	121.6	121.4	-6.0	-7.6	-10.8	-8.8	-5.5	-11.3	94	93	90	92	0.2	0.2	0.3	0.2	10 ≡	10 ≡	10 ✳ ≡	NW 10	W 10	W 20
15	108.4	105.9	105.9	106.7	-9.6	-7.4	-8.2	-8.4	-6.9	-11.6	91	96	95	94	0.3	0.1	0.2	0.2	10 ✳ ≡	10	9	SW 40	SW 20	NW 18
16	96.9	97.4	101.4	98.6	-5.8	-5.2	-4.8	-4.6	-3.6	-8.3	96	95	95	95	0.2	0.2	0.2	0.2	10 ✳ ≡	10 ✳ ≡	10 ✳ ≡	W 18	W 16	WNW14
17	110.0	112.6	115.5	112.7	-7.6	-7.6	-7.8	-7.7	-4.7	-8.6	93	96	93	94	0.2	0.1	0.2	0.2	10 ✳ ≡	10 ✳ ≡	10 ✳ ≡	WNW16	NW 18	NW 16
18	114.7	114.8	115.6	115.0	-7.8	-8.0	-8.8	-8.4	-6.5	-9.6	96	93	92	94	0.1	0.2	0.3	0.2	10 ✳ ≡	10 ✳ ≡	10 ≡	W 10	W 4	WNW 6
19	116.5	118.1	122.6	119.1	-10.4	-9.4	-13.8	-11.8	-8.5	-14.1	97	91	88	92	0.1	0.3	0.3	0.2	7	10 ✳ ≡	7	NW 10	W 2	NW 4
20	127.7	130.8	131.7	130.1	-16.0	-12.4	-12.9	-13.6	-12.1	-17.3	86	81	81	83	0.2	0.4	0.4	0.3	10 ≡	0 ⊙	0	W 16	ENE 2	C 0
21	126.3	124.3	127.2	125.9	-12.5	-10.8	-9.6	-10.6	-9.4	-14.1	59	44	38	47	1.0	1.5	1.8	1.4	8	8 ⊙	0	SW 14	S 14	S 4
22	130.9	135.5	138.8	135.1	-17.4	-18.4	-21.4	-19.6	-9.6	-23.4	85	84	81	83	0.2	0.2	0.2	0.2	2	3 ⊙	10 ≡	NE 18	NE 16	N 18
23	139.5	140.8	142.7	141.0	-21.0	-18.0	-16.0	-17.8	-16.0	-23.9	89	41	86	72	0.1	0.9	0.2	0.4	10 ≡	7	6	N 22	NE 26	NE 28
24	142.5	142.6	141.7	142.3	-17.0	-18.2	-16.8	-17.2	-15.6	-18.7	95	84	85	88	0.1	0.2	0.2	0.2	4	9	10 ✳ ≡	ENE35	E 16	ESE16
25	138.4	136.4	133.2	136.0	-12.6	-11.6	-10.7	-11.4	-10.0	-17.1	89	89	90	89	0.3	0.3	0.3	0.3	10 ≡	7	10 ✳	SE 14	S 13	S 9
26	128.2	126.1	123.4	125.9	-9.8	-7.6	-11.2	-10.0	-7.2	-11.6	91	93	97	94	0.3	0.2	0.1	0.2	4	8 ⊙	0	S 7	S 7	WSW 5
27	121.6	121.9	122.7	122.1	-11.2	-6.8	-11.9	-10.4	-6.2	-12.6	80	80	86	82	0.5	0.7	0.4	0.5	1	1 ⊙	1	W 3	WNW 3	N 4
28	123.7	124.6	124.2	124.2	-11.0	-9.8	-11.2	-10.8	-9.8	-12.6	80	85	59	75	0.5	0.4	1.1	0.7	4	1 ⊙	4	NW 3	SW 4	SW 14
29	121.2	121.5	122.1	121.6	-9.0	-7.4	-6.8	-7.5	-6.1	-11.5	59	46	53	53	1.3	1.9	1.7	1.6	6	8	4	SW 14	SW 7	SW 4
30	122.4	123.5	124.6	123.5	-4.9	-3.4	-9.8	-7.0	-3.3	-13.1	93	97	91	94	0.3	0.2	0.3	0.3	9	9	9	SW 4	C 0	E 10
31	125.2	126.5	128.0	126.6	-11.8	-12.5	-13.2	-12.7	-7.2	-14.0	89	92	84	88	0.3	0.2	0.4	0.3	10 ✳ ≡	10 ✳ ≡	10 ≡	SE 14	SE 18	SE 10
M	128.4	128.5	129.1	128.7	-8.3	-7.3	-8.5	-8.2	-5.4	-11.0	82	78	78	79	0.7	1.0	0.9	0.9	7.3	7.0	6.5	15.0	11.7	11.8

Śnieżka $H_s = 1603m$ $H_t = 1610{,}6m$ Listopad - Novembre 1962

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	0	26.5	20	*'0^00-1^30 *°-11^15 △°-12^20 *°-13^05 *'-14^30 *°-19^45 °21^50-23^45; ⊕°0^00-11^30 ⊕'-19^30 ⊕°-21^30; ⋗0^00-11^30 ⋖-17^30 ⋗21^30; ≡²0^00-24; v°0^00-11^15 v°-24; ∿°21^50-23^45
2	8	0.0	30	*°0^45-4^45; ⋗18^50-20^40 ⋖-24; ≡²0^00-3^30 = -5^50 ≡²-6^40 = -7^05 ▭ 6^40-8^05 ≡²-9^40 ▭-24 = 10^20-35; 11^45-12^10; 13^45-15^05; v°0^00-3^30
3	9	•	25	⋖0^00-16^10 ⋗-20^20; ▭ 0^00-2^50 = 2^20-4^35 ≡²-6^23 = -6^45 ▭ 6^23-20^30 = 10^45-14^15; v°6^10-23
4	9	1.4	20	⋗0^40-3^10 ⋖-24; ▭ 3^30-16^10 = 7^45-16^10 ≡²-24; v°18^45-19^30 v'-24
5	8	0.9	12	⋖0^00-24; ≡²0^00-10^10 = -14^20 ≡²-24; v°0^00-6^10
6	0	8.4	pł.	●1^30-24; ≡²0^00-24; ⋖0^00-24
7	9	1.8	pł.	●0^00-6^05 ●'-6^45 ●-7^05 20^45-24; ⋖0^00-8^10 ⋗-9^20; 19^20-20^30 ⋖-24; ≡²0^00-7^05 ▭-18^40 = 18^30-20^45 ≡²-24
8	0	4.0	pł.	●0^00-24; ⋖0^00-24; ≡²0^00-24
9	0	3.8	•	●0^00-13^40; 14^50-24; ⋖0^00-18^20 ⋗-22^30; ≡²0^00-13^40 = -14^50 ≡²-24
10	0	12.1	•	●0^00-3^52 ●°-5^55 *°7^40-8^30; ⋗4^30-9^30 ⋖-24; ≡²0^00-24; v°8^30-16^30 v'-24; ∿°7^40-8^30
11	0	3.6	1	*°1^20-2^50 ⋖0^00-9^30 ⋗-10^10; ⊕°1^20-2^50; ≡²0^00-11^40 = ▭-12^30 ≡²-15^45 = -16^10 ▭ 15^45-18^30 = 17^10-18^30 ≡²-24; v¹0^00-10^10 v°-11^40; 19^30-24
12	0	1.7	2	△°2^50-3^30 △'-5^50 △°-9^30 *°-14^20; 15^30..16^50; ≡²0^00-24; v°0^00-11^20; 17^30-24
13	0	1.0	2	●°19^50-20^30 ●-24; ⋗13^0-3^30 9^30-10^30 11^50-13^30; ≡²0^00-24; v°0^00-14^30 v°-19^20
14	0	6.5	2	●0^00-4^30 *°6^50-18^30; ⋗22^30-24; ≡²0^00-24; v°20^30-24
15	0	2.3	5	*°6^20-7^30; 8^05..12^30-14^25; 16^45..20^50 △°21^50-22^30; ⊕°1^30-6^30 ⊕°7^30 ⊕°13^30 ⊕°-16^30 ⊕°-21^30; ⋗0^00-13^30 ⋖-6^30 ⋗-13^50; 16^30-21^20; ≡²0^00-14^30 = -16^20 ≡²-24; v°0^00-14^30; 16^20-24
16	0	0.9	7	*°3^50 5^30; 12^40; 13^45; 14^30..16^45; 17^05...07 ⊕°3^30; 23^40; ⋗3^30-23^40; ≡²0^00-13^30 = -3^40 ≡²-4^30 = -8^40 ≡²-10^05 = -12^30 ≡²-13^40 = -14^20 ≡²-20^30 = -20^45 ≡²21^20-45 = 23^30-24; v°0^00-13^30-310
17	1	3.5	7	△°9^40-10^50; ⋗13^30-14^20 ⋖-24; = 0^00-2^45 ▭-4^20 = -7^30 ▭-8^05 = -9^15 ≡²-24; v°19^35-23^50 v²-24 [16.XI: -4^30 9^10-10^05 12^30-13^40 14^20-20^30 21^20-45
18	0	4.4	9	⋖0^00-6^30 ⋗-10^40 ⋖-22^30 ⋗-24; ≡²0^00-24; v²0^00-24
19	0	7.1	10	*°19^52-21^55; ⋗0^00-1^10 7^30-8^20 ⋖-10^30 ⋗-17^15 22^40-24; ≡²0^00-8^05 = -8^15 ≡²9^20-15^30 = -16^15 ≡²21^30-24; v²0^00-8^05 v°9^25-16^15; 22^25-24
20	0	5.4	15	*°13^40-15^15; ⋗0^00-8^40; ≡²0^00-15^40 ▭-17^30 = -18^30 ≡²-24; v°0^00-15^40; 18^30-24
21	0	1.5	20	⊕°19^30-24; ⋗15^40-23^30 ⋖-24; ≡²0^00-2^30 = -3^40 ≡²-4^20 = -6^40 ▭-8^10 = -12^30 ≡²-13^40 = -14^30 ≡²-24; v°0^00-2^30; 3^40-4^20; 8^10-24
22	0	2.8	20	⊕°0^00-24; ⋖0^00-9^30 ⋗-21^30; ≡²0^00-24; v°0^00-24
23	8	0.7	22	⊕°0^00-8^10; 20^30-24; ⋗13^0-8^10 20^30-24; ≡²0^00-7^05 = -11^30 ▭ 7^05-19^30 = 21^30-22^30 ≡²-24; v°0^00-7^05; 22^30-24
24	8	0.0	22	⊕°0^00-9^30; ⋗0^00-8^30; ≡²0^00-7^40 = -9^10 ▭ 7^40-24; v°0^00-8^30
25	8	1.4	20	*'20^30-21^50; ⋗10^30-13^10; 15^30-20^30 ⋖-22^30 ⋗-24; ▭ 0^00-11^10 ≡²21^30-24; v°21^30-24
26	0	3.3	21	⋗0^00-1^20 3^30-5^30; ≡²0^00-23^40; v°0^00-11^30 15^30-23^40
27	0	2.2	25	*°19^30-21^30; ≡²0^30-3^40 = 5^30 ▭-11^30 = 10^50-11^30 ≡²-21^50 ▭-24 = 23^50-24; v°0^30-3^40; 11^30-21^50
28	8	1.9	25	= 0^00-2^30; 14^15-15^30 ≡²-24 ▭ 0^00-14^15; v°1^30-2^30; 15^30-24
29	0	2.0	25	⋗19^15-23^05 ⋖-24; ≡²0^00-6^30 = -7^10 ≡²-10^08 = -11^15 ≡²-14^28 = -20^45 ▭ 14^40-19^25 ≡²20^45-24; v°0^00-6^30 8^05-10^08 12^30-14^28; 21^10-24; ⊛ 14^45-15^25
30	0	14.7	25	*°9^10-15^50 △°-16^10 ⊕°16^10-17^05 ⊕°-18^30 *'-21^40 *°-24; ⊕'9^10-17^40 ⊕²-24; ⋖0^00-8^30; 17^40-24; ≡²0^00-24; v°0^00-24; (ζ)°16^10-18^30
31				
Σ	—	125.6	—	UWAGI:

Grudzień - Décembre

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	0	7.9	33	*°0^00-9^25 *'-11^20 *°-24; ⊕²0^00-7^40 ⊕'-17^30 ⊕²-24; ⋖0^00-7^40 ⋗-17^30 ⋖-24; ≡°0^00-24; v°0^00-24
2	9	•	40	*°0^00-3^50; ⊕²0^00-2^30 ⊕'-5^20 ⊕'-6^10 ⊕°-6^40 7^30-12^00 ⋖0^00-2^30 ⋗-7^05; ≡²0^00-5^20 = -5^25 ▭-16^00; v°0^00-5^20
3	9	•	38	
4	9	•	35	virga 10^50-13^10; ⊕°7^20-13^30; ⋗14^30-24; ⊖ 19^50-22^30
5	8	•	32	⊕²4^15-10^20 ⊕°-12^30; ⋗0^00-4^15 ⋖-10^20 ⋗-22^30; = 7^15-8^20 ≡²-9^30 = -11^20 ▭ 9^30-24
6	9	•	28	⋗0^30-8^05; ▭ 0^00-24; ⊔ 16^30-24
7	9	•	26	⋗18^30-20^20; ▭ 0^00-24 = 9^30-10^10; ⊔°5^00-9^20; ⊔ 0^00-1^30
8	9	•	22	⋗1^30-8^30; 17^30-19^30 ⋖-24; ▭ 0^00-24
9	9	3.6	20	*'14^19-15^50 *°-21^50 *'22^50-23^30 *°-24; ⊕²6^30-24; ⋖0^00-24; ▭ 0^00-14^10 ≡²-24; v'14^10-24
10	0	6.1	22	*°0^00-1^30 *'2^50-4^10 *13^45-18^30 *'-22^40 *°-24; ⊕²0^00-24; ⋖0^00-24; ≡²0^00-24; v'0^00-10 v°-24
11	0	7.7	30	*°0^00-13^30; ⊕²0^00-24; ⋖0^00-24; ≡²0^00-24; v°0^00-24
12	0	5.2	35	*°6^10-12^30; 13^40-23^10; ⊕²0^00-24; ⋖0^00-24; ≡²0^00-24; v°0^00-24
13	0	5.5	36	*°9^50-11^30; ⊕²0^00-3^30 ⊕'-16^30 ⊕°-19^30; ⋖0^00-3^40 ⋗-9^30 ⋖-14^30 ⋗-19^30; ≡²0^00-3^40 4^10-5^30 = -6^40 ≡²-24; v°0^00-24
14	0	2.8	37	*°7^40-8^10 10^50 14^50..16^20 *'-17^30 *°-22^50; ⊕°0^20-8^20 ⊕'-17^30 ⊕²-24; ⋗0^20-8^30 9^30-17^30 ⋖-24; ≡²0^00-9^30 = -12^20 ▭ 11^30-12^20 ≡²-24; v°0^00-24
15	6	6.7	42	*°3^50-6^30 *'-10^20 *°-11^40..12^50; 13^50 16^10-16^25 *'-18^15 *°-19^30 20^45; ⊕²0^00-24; ⋖0^00-24; ≡²0^00-12^40 = -19^50 ≡²20^50 = -21^45 ≡²-24; v°0^00-12^40; 13^55-20^50; 22^10-24
16	0	10.2	48	*°2^45-5^20 *'-7^10 *°-19^30 *'-24; ⊕²0^00-13^30 ⊕'-21^30 ⊕²-24; ⋖0^00-13^30 ⋗-21^30 ⋖-24; ≡²0^00-24; v°0^00-24
17	0	9.5	63	*'0^00-9^15 *°-12^20 15^40-21^20 *'-24; ⊕²0^00-13^10 ⊕'-15^25 ⊕²-24 ⋖0^00-13^10 ⋗-15^25 ⋖-24; ≡²0^00-13^30 = -15^35 ≡²-24; v°0^00-13^30; 15^40-24
18	0	1.4	70	*'0^00-2^20 *°-3^30 *'-6^40 *°-7^20 8^30-13^40 17^50; ⊕²0^00-5^40 ⊕'-7^10 ⊕°-10^30; ⋖0^00-5^40 ⋗-7^10; ≡²0^00-7^20 = -8^30 ≡²-24; v°0^00-7^20; 8^30-24
19	0	2.6	72	*11^20 15^40; ⋗5^30-7^20 23^30-24; ≡²0^00-2^30 = -9^10 ▭ 7^20-9^10 ≡²-20^30 = -21^30 ≡²-24; v°0^00-24
20	9	0.0	73	⊕°4^10-11^10; ⋗0^00-3^30 ⋖-9^30 ⋗-11^10; ≡²0^00-9^10 = -9^40 ▭ 9^10-24; v°0^00-9^10; ⊛ 8^40-13^50
21	8	0.3	70	⊕'6^10-17^30 ⊕°-19^30; ⋗6^10-14^30 ⋖-16^30 ⋗-17^30; ▭ 0^00-11^30; ⊔ 5^30..7^20
22	8	3.4	68	⊕'5^30-24; ⋗4^30-5^30 ⋖-24; ▭ 3^10-4^10 ≡²-5^30 = -6^30 ▭ 5^30-16^10 ≡ 7^05-9^10; 16^10-16^10 ≡²-21^30 = -23^50 ≡²-24; v°4^10-6^30 7^05-9^10; 15^40-21^30; 23^50-24; ⊛ 8^50..15^15
23	8	2.3	65	⊕'0^00-4^30 ⊕²-24; ⋖0^00-24; ≡²0^00-3^30 ▭-6^30 = 5^10-6^30 ≡²-8^00 ▭-15^40 = -17^30 ≡²-20^30 = -22^30; v°0^00-3^30; 5^10-8^00; 15^40-22^30
24	7	6.8	62	*°17^50 22^30-23^20..24; ⊕²0^00-24; ⋖0^00-24; ▭ 7^30-14^30 = 11^10-14^30 ≡²-24; v°11^10-24
25	8	0.2	67	*°0^00 1^50; 20^40..21^10-23^40; ⊕²0^00-1^50 ⊕'-20^30 ⊕°-22^10; ⋖0^00-1^50 ⋗-20^30; ≡²0^00-2^30 = -4^20 ≡²-7^30 = -21^30; v°0^00-21^30
26	8	•	65	▭ 2^30-24; ⊕ 9^30-11^20
27	8	•	61	▭ 0^00-24
28	8	•	58	⊕'20^10-24; ⋗18^20-24; ▭ 0^00-24; ⊔°4^00-11^00
29	8	0.0	56	*°22^45 23^30; ⊕'0^00-7^10; ⋗0^00-1^30 ⋖-5^30 ⋗-7^10; ▭ 0^00-24
30	8	4.7	55	*°5^40 6^10 22^30-24; ⋗19^30-24; ▭ 0^00-8^20 = -9^10 ≡²-11^40 ▭-15^10 = 12^10-40; 13^30-15^10 ≡²-19^30 = -23^10 ≡²-24; v°9^10-11^40; 14^10-24
31	0	3.6	58	*°0^00-15^45; ⊕'4^30-12^30 ⊕²-16^30 ⊕'-17^30 ⊕²-19^30 ⊕'-24; ⋗0^00-3^30; 4^30-7^30 ⋖-8^30 ⋗-12^30 ⋖-16^30 ⋗-17^30 ⋖-19^30 ⋗-24; ≡²0^00-21^50; v°0^00-21^50
Σ	—	88.5	—	UWAGI:

Sandomierz φ=50°41' λ=21°45' Styczeń-Janvier 1962

DNI	CIŚNIENIE P=900+ I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N.w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D.v I	II	III
1	84.3	87.5	87.8	86.5	0.3	2.9	1.2	1.4	4.0	-2.0	94	84	87	88	0.3	1.2	0.9	0.8	2	10	10	SW 5	WSW 3	WSW 3
2	86.0	86.8	89.9	87.6	-0.4	-0.6	-0.9	-0.7	1.4	-1.6	80	77	73	77	1.2	1.3	1.5	1.3	10	10	10	WSW 3	W 4	W 4
3	94.4	95.5	100.0	96.6	-4.5	-3.3	-1.7	-2.8	-0.8	-6.5	72	72	92	79	1.2	1.4	0.4	1.0	9	10	10	WNW 5	W 7	WNW 3
4	103.5	101.9	100.0	101.8	-2.1	-0.1	-5.2	-3.2	0.1	-5.4	92	71	85	83	0.4	1.8	0.6	0.9	10	2	0	SW 2	SW 4	WSW 3
5	99.2	97.9	94.7	97.3	-3.9	-3.3	-7.2	-5.4	-2.8	-7.5	89	90	88	89	0.5	0.5	0.4	0.5	10	10	3	W 4	WSW 3	SW 2
6	91.0	90.1	87.9	89.7	-8.5	-3.5	-4.0	-5.0	-2.6	-9.4	89	76	82	82	0.3	1.1	0.8	0.7	1	0 ⊙	10	SW 6	SW 6	SW 6
7	89.5	93.8	100.6	94.6	0.8	1.6	0.4	0.8	2.5	-4.8	88	85	89	87	0.8	1.1	0.7	0.9	10	9	10 △	W 6	NW 5	NW 2
8	104.0	104.1	102.8	103.6	-1.9	-1.6	-1.1	-1.4	0.5	-3.8	87	75	81	81	0.7	1.3	1.1	1.0	10	8 ⊙	10	SW 2	SSW 1	SSW 4
9	101.0	98.8	96.0	98.6	-1.8	-1.7	-6.0	-3.9	-1.0	-6.4	86	67	79	77	0.8	1.8	0.8	1.1	10	0 ⊙	0	SW 4	SW 5	S 2
10	92.0	89.5	86.8	89.4	-6.1	-1.7	-2.3	-3.1	-1.1	-6.8	79	71	76	75	0.8	1.6	1.3	1.2	3	8	10	S 3	SSW 5	S 5
11	88.1	86.0	83.6	85.9	-1.3	4.0	1.8	1.6	4.4	-2.4	80	61	74	72	1.1	3.2	1.8	2.0	3	0	2	SW 4	SSW 5	SW 5
12	84.6	83.4	80.2	82.7	1.8	1.4	0.9	1.2	3.3	0.7	94	91	92	92	0.4	0.7	0.5	0.5	10 ●	10 ●	4	SSW 4	SW 2	SW 3
13	70.8	72.6	76.0	73.1	2.5	2.0	1.4	1.8	3.0	0.4	91	93	87	90	0.6	0.6	0.9	0.7	10 ●	10	10	S 3	SSW 5	SSW 4
14	77.1	80.2	84.2	80.5	0.8	2.7	0.3	1.0	3.1	-0.9	94	86	86	89	0.4	1.0	0.8	0.7	10	1 ⊙	8	WSW 3	WSW 3	SSW 3
15	87.5	91.4	95.8	91.6	1.2	1.8	1.3	1.4	2.1	-0.3	81	74	85	80	1.3	1.8	1.0	1.4	9	9	10	SW 6	SW 7	SW 4
16	99.2	100.5	98.6	99.4	-2.7	1.5	-0.7	-0.6	3.1	-2.9	95	72	73	80	0.2	1.9	1.6	1.2	0	1 ⊙	0	SW 4	SSW 5	S 3
17	96.3	96.1	96.2	96.2	-1.2	2.6	-0.7	0.0	3.1	-2.4	70	62	85	72	1.7	2.9	0.8	1.8	10	6 ⊙	10	SSW 7	SSW 8	SSW 6
18	93.7	92.6	93.3	93.2	-2.1	1.0	-0.7	-0.6	1.6	-2.6	84	81	87	84	0.8	1.3	0.7	0.9	9	9	9	SSW 3	SSW 3	SW 5
19	95.1	94.7	93.2	94.3	-1.3	1.8	0.6	0.4	2.4	-2.0	84	82	90	85	0.9	1.3	0.6	0.9	3	10	2	SW 2	SW 3	SW 3
20	91.9	93.0	97.5	94.1	2.6	5.6	1.8	3.0	5.9	-0.4	86	71	83	80	1.1	2.7	1.2	1.7	7	0 ⊙	0	SW 7	WSW 9	W 4
21	97.9	96.7	96.2	96.9	-0.9	2.4	2.2	1.5	3.4	-1.6	92	91	98	94	0.5	0.7	0.2	0.5	3	10	10	WSW 4	SW 4	SW 3
22	91.9	87.0	87.6	88.8	2.3	5.6	2.8	3.4	6.5	1.7	95	75	79	83	0.4	2.2	1.6	1.4	10	9	8	SW 4	SSW 4	SW 5
23	91.2	93.1	95.2	93.2	0.4	4.8	0.7	1.6	5.0	-0.3	86	65	85	79	0.9	3.0	1.0	1.6	1	1 ⊙	4	SW 4	SW 3	SW 3
24	95.4	94.4	92.4	94.1	0.0	2.7	1.0	1.2	3.6	-1.1	92	72	92	85	0.5	2.1	0.5	1.0	6	0 ⊙	10	WSW 5	SW 5	WSW 5
25	88.5	85.4	84.8	86.2	0.2	2.4	2.2	1.8	3.0	-0.5	94	96	98	96	0.4	0.3	0.2	0.3	10	10 ●	10 ●	SW 3	SSW 4	SW 3
26	84.7	91.5	92.6	89.6	3.2	0.4	-0.2	0.8	4.1	-0.6	93	90	90	91	0.5	0.6	0.6	0.6	10 ●	10	10	W 5	NW 4	NW 2
27	89.0	88.3	88.9	88.7	-1.2	-1.0	1.0	0.0	1.5	-1.9	89	95	88	91	0.6	0.3	0.8	0.6	9	10	10	WSW 1	SW 2	WSW 4
28	85.9	84.8	86.0	85.6	0.4	0.5	-4.2	-1.9	1.2	-4.2	90	83	79	84	0.6	1.0	0.9	0.8	10	9	10 ✳	NW 5	WSW 6	NW 7
29	90.6	95.6	100.9	95.7	-7.7	-6.8	-7.1	-7.2	-3.9	-8.4	84	77	85	82	0.5	0.8	0.5	0.6	10 ✳	10	10 ✳	NNW 8	N 8	N 8
30	106.0	109.1	112.0	109.0	-5.7	-8.3	-13.1	-10.0	-4.4	-13.1	82	72	80	78	0.7	0.9	0.4	0.7	10	0 ⊙	0	NE 7	NNE 7	NNE 5
31	111.3	110.3	107.4	109.7	-17.0	-9.8	-10.7	-12.0	-9.0	-17.4	80	72	80	77	0.3	0.8	0.5	0.5	8	9	0	N 3	NE 3	NE 3
M	92.3	92.7	93.2	92.7	-1.7	0.2	-1.5	-1.1	1.4	-3.7	87	78	85	83	0.7	1.4	0.8	1.0	7.5	6.5	6.8	4.3	4.6	3.9

Luty-Février

1	98.0	94.2	94.3	95.5	-10.1	-4.7	-7.7	-7.6	-3.4	-11.0	74	74	79	76	0.7	1.1	0.7	0.8	1	9	0	E 6	ESE 3	ESE 3
2	93.6	95.1	97.1	95.3	-8.1	-4.9	-5.7	-6.1	-4.5	-9.1	84	78	87	83	0.5	0.9	0.5	0.6	10	8 ⊙	0	ESE 2	S 3	C 0
3	98.4	99.9	101.0	99.8	-6.6	-3.3	-3.9	-4.4	-3.3	-7.0	86	81	85	84	0.5	0.9	0.7	0.7	10	10 ✳	10 ✳	NNW 3	N 4	N 3
4	97.2	94.9	95.8	96.0	-4.3	-1.7	-0.8	-1.9	-0.8	-5.4	89	71	87	82	0.5	1.6	0.7	0.9	10	9	10	N 1	NW 3	W 3
5	95.2	87.9	81.7	88.3	-1.9	1.3	0.1	-0.1	2.0	-3.1	92	56	98	82	0.4	3.0	0.2	1.2	8	9	10	SW 3	S 4	SW 6
6	86.7	88.7	92.7	89.4	1.6	1.9	1.6	1.7	2.4	-0.2	78	76	72	75	1.6	1.7	1.9	1.7	10	9	10	WSW 7	W 9	WNW 5
7	95.6	95.7	93.3	94.9	-0.2	2.0	-1.9	-0.5	3.1	-2.1	69	64	79	71	1.9	2.6	1.1	1.9	8	4 ⊙	0	WNW 2	WSW 2	SSE 2
8	90.6	90.9	92.8	91.4	-5.3	2.5	-0.4	-0.9	2.9	-5.7	85	68	92	82	0.6	2.3	0.5	1.1	8	9 ⊙	10 ✳	SSE 3	S 3	S 3
9	95.4	98.5	104.2	99.4	-1.1	0.2	0.4	0.0	1.8	-1.4	95	96	84	92	0.3	0.3	1.0	0.5	10 ✳	10	10	SSW 5	SW 4	SW 4
10	107.9	108.1	107.0	107.7	-1.1	1.2	-3.6	-1.8	1.5	-3.9	77	70	87	78	1.3	2.0	0.6	1.3	10	2 ⊙	6	NW 2	WSW 3	WSW 1
11	102.0	98.8	101.9	100.9	-2.3	0.8	0.2	-0.3	2.3	-3.9	84	71	78	78	0.9	1.9	1.4	1.4	10	10	1	SW 2	SW 5	W 5
12	96.0	81.1	66.8	81.3	-2.7	-0.5	3.2	0.8	3.6	-4.4	82	94	73	83	0.9	0.4	2.1	1.1	6	10 ✳	10	SW 6	SSW17	SW 9
13	63.9	62.0	63.9	63.3	2.2	2.1	0.4	1.3	6.2	0.2	78	80	88	82	1.6	1.4	0.8	1.3	10	10	10	WSW10	SW 7	W 5
14	66.1	67.4	70.4	68.0	-1.9	-0.7	-1.4	-1.4	0.9	-2.2	96	93	80	90	0.2	0.4	1.1	0.6	10	10	10	W 2	NE 4	NNW 6
15	77.0	81.5	90.9	83.1	-3.9	-2.7	-4.1	-3.7	-1.1	-4.7	73	54	84	70	1.2	2.3	0.7	1.4	9	8	10 ✳	NNW10	NNW14	NW 8
16	89.7	78.7	68.2	78.9	-7.9	-4.5	1.0	-2.6	1.4	-8.9	78	88	88	85	0.7	0.5	0.8	0.7	2	10 ✳	10 ✳	WSW 4	SW 14	SW 12
17	62.1	64.3	70.0	65.5	0.4	1.4	-1.3	-0.2	2.6	-1.9	96	81	80	86	0.3	1.3	1.1	0.9	10 ✳	10 ✳	10	WSW10	WSW10	WNW 9
18	78.0	83.2	90.9	84.0	-4.7	-3.2	-3.7	-3.8	-1.3	-5.7	79	72	73	75	0.9	1.3	1.2	1.1	10	8	9	W 12	NW 9	NW 9
19	93.7	93.4	92.4	93.2	-6.1	-1.1	-1.8	-2.7	-0.7	-6.5	79	75	96	83	0.8	1.4	0.2	0.8	4	9 ✳	10 ✳	W 5	W 4	SW 2
20	92.6	93.2	90.2	92.0	1.6	2.2	1.8	1.8	2.6	-2.1	89	82	89	87	0.8	1.3	0.8	1.0	10	10	9	W 4	W 6	W 8
21	90.9	92.7	98.4	94.0	-0.1	-0.7	-3.4	-1.9	2.9	-3.5	71	79	83	78	1.8	1.2	0.8	1.3	10	10	10 ✳	NNW 9	NW 8	N 8
22	104.7	106.2	108.2	106.4	-5.5	-3.7	-5.1	-4.8	-3.2	-6.4	85	71	78	78	0.6	1.3	0.9	0.9	10	10 ✳	10 ✳	NE 5	NNE 3	NNE 3
23	106.3	102.0	100.1	102.8	-8.9	-5.9	-7.7	-7.6	-4.8	-9.2	76	76	81	78	0.7	0.9	0.6	0.7	8	10 ✳	10	NW 4	WNW 5	N 3
24	95.1	94.1	96.0	95.1	-7.5	-5.5	-8.1	-7.3	-5.0	-8.4	90	72	90	84	0.3	1.1	0.3	0.6	10 ✳	10	9	N 2	N 2	ENE 3
25	98.7	99.1	98.7	98.8	-11.9	-4.4	-5.5	-6.8	-4.0	-12.1	86	74	92	84	0.4	1.1	0.3	0.6	6	10 ✳	10 ✳	ENE 2	E 2	NE 3
26	97.5	98.3	98.5	98.1	-3.2	-2.3	-2.9	-2.8	-1.5	-6.5	88	87	88	88	0.6	0.7	0.5	0.6	10	10	10	ENE 1	SW 1	E 3
27	97.0	96.2	94.9	96.0	-4.1	-2.3	-6.6	-4.9	-2.1	-6.7	87	78	80	82	0.6	1.2	0.7	0.8	10	10	1	E 2	E 5	ENE 4
28	91.6	90.1	87.6	89.8	-5.7	-2.7	-5.0	-3.6	-1.4	-7.5	90	78	93	87	0.4	1.1	0.4	0.6	10	10	10 ✳	ESE 3	SE 3	E 2
29																								
30																								
31																								
M	91.5	90.6	91.0	91.0	-3.9	-1.4	-2.5	-2.6	0.0	-5.3	84	76	84	81	0.8	1.3	0.8	1.0	8.6	9.1	8.0	4.5	5.6	4.6

Sandomierz $H_s = 202m$ $H_b = 200{,}3m$ $h_w = 20{,}1m$ Styczeń - Janvier 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	6	.	12	≡ 1-0 0^00-4^20 = -24
2	6	.	11	= 0^00-24
3	7	0.7	10	* 14^12-17 △ 14^20-15^08 * 0-1-16^20 18^12, ≫ 10^40-11^20, = 0^00-8^15, 14^30-24
4	7	.	11	= 0^00-10^30
5	6	.	10	= 0^30-24
6	6	0.2	10	= 0^00-24
7	6	0.0	10	* 0^30-1^15 * ... 2^45, 7^34 10^15, 13^45 ... 14^15 △ 19^43-21^35, = 0^00-24
8	7	.	10	= 0^00-9^45
9	7	.	10	= 6^20 ↓ 11^30
10	7	.	9	
11	7	0.5	9	
12	6	2.1	9	• 0^40 ... 1^20-3^45 ... 5^20-8^45 ... 9^50 * 0-11^20 • ... 12^45, = 2^30-24
13	6	4.5	6	• 5^55 ... 6^05-7^35 7^45-12^15, = 0^00-24
14	6	0.6	6	• 5^43-6^25, 6^52-7^30, = 0^00-22^10
15	7	.	6	* 4^35-5^15
16	7	.	5	= 1^30-12^30, ⊽ 18^20-19^45
17	7	.	5	⊽ 17^05-23^10
18	6	.	5	= 9^30-24, ⊽ 0^40-2^30, 17^50-23^30
19	6	0.3	4	= 0^00-13^15, 20^15-24
20	7	.	4	• 4^08 ... 30-5^40, = 0^00-9^30, 17^43-24
21	6	3.8	pł.	• 14^01-15^15 • -19^45 • ... 20^15, = 0^00-16^20 ≡ 0-1-18^50 = -24
22	7	.	pł.	= 0^00-12^15, ⊽ 20^30-23^30
23	7	.	pł.	= 23^30-24, ⊔ 22-24, ⊽ 1^40-2^15, 21^40-24
24	7	0.9	pł.	* 8^12 ... 42 • 20^45 ... 21^50 • 23^35-24, = 0^00-12^15, 18^30-24, ⊔ 0^00-10, ⊽ 0^00-1^15
25	6	6.8	1	• 0^00-10 * ... 3^40 △ 6^35-7^20 • -8^15 ... 9^10 • -10^30 • • -11^25 • -12^10 • -12^45 • 13^02-16^20, 20^28-50, = 0^00-9^50 ≡ -10^45 = -24
26	6	0.0	pł.	• 3^39-5^45 • 6^10-52 * 9^50 ... 11^30, = 0^00-13^15, 22^30-24
27	6	3.3	pł.	△ 7^32-8^05 * 0-1-12^20 15^50 * 15^50-16^15 16^40-17^35 * 21^38 ... 22^30-23^40, = 0^00-24
28	7	1.1	2	* 12^34-41 * 13^40-14^05 * 18^40-19^20 * 19^30 21^15-23^20, = 0^00-8^30
29	6	2.0	4	* 3^45 ... 24, + 21^10-23^30 + -24, ≫ 0^20-3^40 7^15-9^50 22^20-24, = 4^30-24
30	7	.	6	* 0^00 ... 3^35, + 0^00-4^50, ≫ 0^00-2^20, = 0^00-10^30
31	6	.	5	= 11^20-24
Σ	—	26.8	—	UWAGI.

Luty - Février

1	7	0.0	5	= 0^00-9^30 23^30-24
2	6	.	5	* 3^50-4^43, = 0^00-24
3	6	1.1	4	△ 7^45-9^20 * 0-11^30 ... 12^15 △ 0-12^23 * △ 0-12^28 * 0 ... 13^40, 19^40 ... 20^20-23^45, = 0^10-24
4	6	0.1	6	* 0^2^45-3^30 ... 4^30, 7^50 ... 9^35, 10^15 ... 30, = 0^00-24
5	7	2.2	6	* 0^15^25-17^30 * -18^01 * 0-20^20, = 0^00-12^10, 15^30-24
6	7	0.0	8	* 0^8^50-9^40, 10^50 ... 11^38, = 0^00-11^30
7	7	.	4	
8	7	3.7	4	* 0-1 19^45-24, = 18^30-24
9	6	1.8	9	* 1-0 0^00-6^15 ... 7^38-11^25 ... 12^15 * 0 22^50-23^20, = 0^00-18^40, 20^15-24
10	7	.	10	= 0^00-6^15, 20^15-24
11	6	0.2	7	* 0-1 15^42-16^48, = 0^00-24
12	6	6.2	8	* 0^11^43-15^42 * 0-16^10 • 0-17^50, 20^35-22^40 ... 23^08 * -23^10 * 23^15 • 1-0-24, ⊽ 23^15-25 W-S, + 13^15-15^30, ≫ ↖ 9^10-24, = 0^00-9^15, a-24
13	7	0.0	7	• 0^00-2^30 8^15 ... 10^10, 17^50 ... 18^15 ≫ 0^00-8^20, = 0^00-3^30, 18^30-24
14	6	0.0	6	△ 12^45-13^50, = 0^00-20^10, ⊽ 20^10-21^40
15	7	0.4	5	* 0-1 14^56 ... 20^40, ≫ 3^10-10^20 ≫ - ↖ 12^10-17^20, ⊕ 12^13-13^12
16	6	3.6	5	* 0^11^15-17^50, 18^45 ... 21^40 • 0-22^25, + 12^45-17^30 + -21^30, ≫ - ↖ 11^05-24
17	7	9.4	11	* 0^1^45-2^15, 4^40-6^20 * 0-7^10 * 0-7^15 * 2-0 19^30 * 0 10^45-11^10 * 0 22^45-24, ≫ 0^00-8^30, 9^20-20^20, = na
18	7	0.3	14	* 0^12^50-13^06 △ 15^55-16^08 * 0 ... 18^45, + 7^45-8^40 + -12^50, ≫ 1^30-9^30, 11^50-14^25, = na
19	7	1.9	16	* 0^11^55 12^38 △ 18^40-19^12 * 0-23^30 • 0-24, = 18^30-24, ⊽ 1^30-2^20
20	6	0.5	14	• 0^00-1^45 2^25-3^50 * 0-16^12 ... 40, 17^48-18^30 • 18^45-20^40, = 0^00-24
21	7	1.9	11	* 0^3^50-4^04 * 0^5^28 ... 6^12 * 0^6^54-7^40, 7^45-8^10 * 7^50-53 * 18^30-19^10 * 0 ... 20^05-23^15, ≫ na ...; = na, a, p
22	6	0.1	12	* 2^52 9^40 12^30 15^25 19^50 24, ≫ 0^00-10, = 0^00-15^10, 22^30-24
23	6	1.6	13	* 0^00 19^40 △ 0 9^24-36 9^50-10^10 * 14^06-15^05, = na, a-24
24	6	1.1	14	* 0^3^45 ... 10^40, 22^45-24, = 0^00-24
25	7	4.0	14	* 0^00 1^25 7^38-9^30 11^45 ... 20^10-24, = 0^00-11^30, 15^20-24
26	6	0.0	17	* 0^00-4^45 △ 7^51-10^45, = 0^00-24
27	6	.	17	= 0^00-24
28	6	2.4	16	* 0^16^40 ... 52, 17^35-24, = 0^00-12^45, 16^30-24
29				
30				
31				
Σ	—	42.5	—	UWAGI.

Sandomierz φ = 50°41' λ = 21°45' Marzec - Mars 1962

DNI	CIŚNIENIE P - 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N.w			KIERUNEK i PRĘDKOŚĆ WIATRU D.v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	85.0	84.5	83.4	84.3	-4.0	-2.5	-2.5	-2.9	-2.0	-4.5	94	87	87	89	0.3	0.7	0.7	0.6	10	10	10	NNE 3	N 3	N 2
2	81.5	80.7	81.2	81.1	-4.5	-1.5	-2.1	-2.6	-1.1	-4.6	88	76	89	84	0.5	1.4	0.5	0.8	10	10	10	NNE 1	NE 1	SW 1
3	82.1	82.6	82.4	82.4	-6.3	1.0	-0.1	-1.4	2.5	-6.6	91	72	84	82	0.3	1.9	1.0	1.1	8	10	10	SW 1	SW 1	SSE 1
4	77.6	73.9	71.4	74.3	0.2	5.9	4.6	3.8	7.0	-1.2	86	74	95	85	0.9	2.4	0.4	1.2	10	9	10 ●	SSE 2	S 4	SSW 2
5	71.7	73.2	72.1	72.3	5.0	10.5	8.6	8.2	13.4	4.3	98	76	90	88	0.1	3.0	1.1	1.4	10	9	10 ●	SW 1	C 0	S 2
6	68.0	77.9	86.5	77.5	8.6	2.2	0.0	2.7	10.5	-0.3	86	75	86	82	1.6	1.8	0.8	1.4	9	8	10 ✳	SSE 3	WSW 10	W 4
7	91.8	94.2	98.3	94.8	-1.9	-1.5	-2.2	-2.0	0.0	-2.5	92	72	72	79	0.4	1.6	1.5	1.2	10 ✳	10 ✳	10	NNW 4	N 6	N 6
8	101.3	102.5	101.9	101.9	-4.8	-0.5	-1.9	-2.3	1.1	-5.1	83	60	83	75	0.7	2.4	0.9	1.3	6 ⊙	6 ⊙	0	N 4	N 3	N 2
9	102.3	103.8	102.2	102.8	-4.0	-1.7	-3.2	-3.0	0.7	-4.3	87	69	67	74	0.6	1.7	1.6	1.3	0 ⊙	6 ⊙	0	NW 2	NE 1	SE 3
10	96.3	92.9	90.6	93.3	-4.9	0.8	0.3	-0.9	1.4	-5.3	69	60	91	73	1.3	2.6	0.5	1.5	4	9	10	SE 7	SE 6	S 3
11	87.4	85.6	83.3	85.4	-0.2	7.6	2.1	2.9	8.2	-0.9	86	61	93	80	0.8	4.0	0.5	1.8	8	9 ⊙	10	SSE 2	SSE 3	SSW 2
12	78.3	74.2	69.2	73.9	0.1	5.0	2.2	2.4	5.2	0.0	96	76	96	89	0.3	2.0	0.3	0.9	10	10	10 ●	SE 2	ESE 2	SE 1
13	70.9	76.8	85.6	77.8	-2.5	-2.6	-4.3	-3.4	2.3	-4.9	87	85	75	82	0.7	0.8	1.1	0.9	10	10	7	WSW 10	W 14	W 6
14	91.8	94.1	96.9	94.3	-8.1	-4.1	-6.8	-6.4	-3.2	-8.9	78	63	75	72	0.7	1.6	0.9	1.1	1 ⊙	7 ⊙	10	W 4	WSW 4	WSW 2
15	96.3	94.9	94.0	95.1	-8.0	-4.7	-6.4	-6.4	-4.4	-8.3	90	69	86	82	0.3	1.3	0.5	0.7	10	10	10 ✳	C 0	NE 5	NE 9
16	91.2	89.6	88.1	89.6	-5.9	-5.9	-7.3	-6.6	-5.6	-7.4	74	89	90	84	1.0	0.4	0.3	0.6	10 ✳	10 ✳	10 ✳	NE 12	NNE 12	NNE 14
17	84.4	83.4	83.7	83.8	-7.7	-5.4	-5.1	-5.8	-4.4	-7.7	87	77	88	84	0.4	0.9	0.5	0.6	10 ✳	10 ✳	10 ✳	NNW 8	NNW 7	NNW 6
18	85.7	90.1	93.2	89.7	-6.5	-2.1	-5.0	-4.6	-0.3	-6.8	86	54	76	72	0.5	2.4	1.0	1.3	10 ✳	2 ⊙	0	NNW 7	NW 6	NW 3
19	95.8	96.9	97.5	96.7	-7.6	-1.1	-4.7	-4.5	-0.4	-8.4	82	53	74	70	0.6	2.7	1.1	1.5	7	2 ⊙	9	NW 3	WNW 2	SW 1
20	97.9	98.1	97.4	97.8	-10.5	-0.6	-5.9	-5.7	-0.4	-11.3	87	50	69	69	0.4	2.9	1.2	1.5	8	0 ⊙	0	SSE 1	SSE 3	SE 1
21	94.7	92.1	89.7	92.2	-10.5	-0.1	-4.7	-5.0	1.5	-11.5	90	50	74	71	0.3	3.0	1.1	1.5	0 ⊙	1 ⊙	10	SE 3	E 3	ENE 4
22	86.1	84.6	83.2	84.6	-6.1	-1.8	-3.2	-3.6	-1.6	-6.4	81	77	92	83	0.7	1.2	0.3	0.7	10	10	10 ✳	ENE 2	NNE 3	N 3
23	81.3	82.3	83.9	82.5	-3.8	-0.3	-1.5	-1.8	0.0	-4.9	92	86	92	90	0.4	0.9	0.4	0.6	10	10 △	10 ✳	NNW 3	N 2	NNW 3
24	86.9	90.2	94.8	90.6	-5.1	0.4	-0.9	-1.1	0.9	-3.5	93	77	89	86	0.4	1.4	0.6	0.8	10	10	10 △	WNW 2	[illegible] 4	W 2
25	97.3	97.6	95.7	96.9	-3.2	0.0	-4.3	-3.0	0.8	-4.5	93	68	68	76	0.3	1.9	1.4	1.2	9 ✳	9 ⊙	0	C 0	NW 1	NNE 1
26	93.7	92.1	90.7	92.2	-9.1	-0.2	-5.1	-4.9	0.6	-10.3	79	50	66	65	0.6	3.0	1.4	1.7	0 ⊙	0 ⊙	0	NNE 2	NE 3	ENE 2
27	86.9	84.2	82.7	84.6	-8.3	0.6	-1.7	-2.8	1.9	-9.4	72	50	69	64	0.9	3.2	1.7	1.9	0 ⊙	1 ⊙	5	E 4	ESE 5	SE 2
28	80.4	79.8	82.1	80.8	-4.3	4.2	1.0	0.5	5.2	-5.4	86	64	92	81	0.6	2.9	0.5	1.3	8 ⊙	7 ⊙	7	SE 1	SW 3	WSW 4
29	83.9	84.3	82.3	83.5	0.8	4.3	1.6	2.1	5.1	-0.9	92	65	83	80	0.5	2.9	1.2	1.5	10	3 ⊙	0	SW 3	SW 3	SSW 1
30	76.7	76.6	74.9	76.1	2.2	4.5	5.3	4.3	7.3	0.4	93	85	86	88	0.6	1.2	1.3	1.0	10 ●	10	5	S 2	SSW 2	S 3
31	70.6	70.5	71.9	71.0	5.8	11.5	8.0	8.3	13.1	4.4	95	78	92	88	0.4	3.0	0.9	1.4	10	8 ⊙	0	SSW 4	SW 6	SSW 3
M	86.3	86.6	86.8	86.6	-3.6	0.7	-1.5	-1.5	2.1	-4.7	87	69	83	80	0.6	2.0	0.9	1.2	7.7	7.3	6.9	3.3	4.1	3.2

Kwiecień - Avril

1	79.0	83.2	86.9	83.0	1.6	4.9	2.2	2.7	8.2	1.2	93	84	84	87	0.6	1.4	1.2	1.1	10	9	0	NW 4	W 4	WSW 4
2	87.0	87.2	90.7	88.3	0.8	8.5	2.4	3.5	9.8	-0.3	81	45	89	72	1.3	6.1	0.8	2.7	0 ⊙	10 ⊙	2	SW 6	WSW 8	WSW 5
3	93.1	91.5	88.2	90.9	0.7	10.8	7.4	6.6	12.7	-0.3	94	51	63	69	0.4	6.4	3.8	3.5	2 ⊙	9 ⊙	0	SW 4	SW 6	S 5
4	84.0	80.6	77.1	80.6	6.2	15.0	10.2	10.4	15.9	4.0	63	38	61	54	3.5	10.4	4.8	6.2	1 ⊙	6 ⊙	10	S 5	SSW 8	S 5
5	68.3	66.2	67.6	67.4	7.4	10.2	7.0	7.9	11.7	6.5	68	64	97	76	3.3	4.5	0.3	2.7	9	10	10 ●	SE 4	S 9	S 1
6	70.0	70.8	73.1	71.3	5.4	12.2	7.6	8.2	13.1	4.9	98	62	82	81	0.2	5.4	1.9	2.5	9	9	10	S 1	E 1	ENE 3
7	75.6	81.4	87.1	81.4	5.8	5.7	1.6	3.7	7.7	1.5	85	56	71	71	1.4	4.0	2.1	2.5	10	10	0	NNW 12	NW 14	W 5
8	86.2	86.7	87.9	86.9	1.8	8.2	6.4	5.7	9.3	-0.6	93	77	81	84	0.6	2.6	1.9	1.7	10 ●	10	2	SW 6	SW 6	SW 5
9	88.3	89.4	91.2	89.6	5.7	14.7	7.5	8.8	16.5	5.0	82	43	84	70	1.7	9.4	1.7	4.3	8	3 ⊙	4	SSW 5	SSW 4	N 4
10	94.7	95.5	96.6	95.6	6.2	13.1	10.2	9.9	14.2	5.1	82	52	68	67	1.7	7.2	3.9	4.3	8 ⊙	3 ⊙	10	C 0	NE 2	NE 2
11	96.8	95.5	95.5	95.9	7.8	15.7	10.2	11.0	17.5	6.8	96	55	86	79	0.5	7.9	1.7	3.4	10	3 ⊙	9	NE 1	N 2	NNE 2
12	94.7	93.5	91.9	93.4	8.6	15.2	12.8	12.4	17.2	6.8	88	54	69	70	1.4	8.0	4.6	4.7	1 ⊙	8 ⊙	8	C 0	WNW 1	NW 2
13	90.0	87.2	85.7	87.6	7.1	16.1	9.0	10.3	16.3	6.1	83	49	79	70	1.8	9.4	2.5	4.6	7 ⊙	8	10	NE 1	N 3	SE 2
14	86.1	91.3	95.8	91.1	6.4	5.6	6.0	6.0	9.5	5.3	95	91	94	93	0.4	0.9	0.6	0.6	10 ●	10	7	NW 4	WNW 3	NNW 4
15	96.9	95.9	96.0	96.3	7.9	12.6	13.1	11.7	16.5	5.8	91	78	73	81	0.9	3.2	4.1	2.7	10	4 ⊙	1	NE 5	N 6	NE 4
16	97.4	97.6	99.2	98.1	11.5	20.4	14.0	15.0	20.9	9.7	75	33	58	55	3.5	16.1	6.7	8.8	4 ⊙	1 ⊙	0	E 4	E 5	ESE 3
17	102.0	101.2	100.0	101.1	10.0	21.7	14.0	14.9	22.7	8.3	76	23	59	53	3.0	20.0	6.6	9.9	0 ⊙	3 ⊙	9	ESE 3	SE 6	SE 3
18	98.0	96.5	95.2	96.6	12.2	19.5	15.2	15.5	21.2	10.1	67	41	50	53	4.6	13.4	8.7	8.9	10	9	7	SE 5	SSE 8	SE 3
19	95.0	94.7	94.1	94.6	10.5	22.2	17.4	16.9	24.0	9.6	75	36	56	56	3.2	17.2	8.8	9.7	7 ⊙	9 ⊙	9	SSE 2	S 3	SSW 2
20	95.2	95.4	95.1	95.2	11.2	24.2	19.2	18.4	24.5	10.4	85	34	51	57	2.0	19.9	10.9	10.9	7	2 ⊙	3	SSW 1	SW 5	WSW 2
21	96.9	96.5	96.4	96.6	13.2	24.1	18.6	18.6	25.8	10.7	67	40	48	52	5.0	18.1	11.1	11.4	5 ⊙	2 ⊙	3	SW 1	SW 2	C 0
22	96.9	96.7	96.3	96.6	13.2	26.2	19.6	19.6	27.0	11.4	83	33	54	57	2.6	22.9	10.5	12.0	2 ⊙	3 ⊙	1	SE 1	SE 1	SE 1
23	97.1	96.9	97.1	97.0	15.2	26.4	18.9	19.8	27.2	11.9	50	20	45	38	8.7	27.4	12.0	16.0	0 ⊙	0 ⊙	0	SE 1	SE 1	NE 1
24	98.5	99.5	100.7	99.6	13.4	26.0	18.8	19.2	26.7	11.1	68	26	49	48	5.0	24.7	11.2	13.6	0 ⊙	0 ⊙	0	NNW 1	NE 3	NE 5
25	103.2	102.8	102.3	102.8	13.6	23.4	15.0	16.8	23.8	11.9	82	43	45	57	2.8	16.5	9.3	9.5	1 ⊙	0 ⊙	0	NNE 3	NE 5	NE 3
26	100.8	96.8	90.4	96.0	10.4	20.6	16.2	15.8	22.7	6.4	60	23	35	39	5.0	18.5	12.0	11.8	1 ⊙	0 ⊙	3	NE 2	SE 2	SE 1
27	84.1	83.8	85.7	84.5	12.0	11.0	6.4	9.0	16.9	6.1	98	86	87	90	0.3	1.8	1.3	1.1	10	10 ●	9	N 1	NW 5	NW 6
28	79.5	77.2	78.8	78.5	5.5	8.2	4.8	5.8	8.9	4.3	91	71	89	84	0.8	3.2	1.0	1.7	10	9	9	WSW 4	W 4	N 2
29	81.1	82.0	83.8	82.3	4.0	6.4	3.8	4.5	9.2	1.6	85	69	90	81	1.2	3.0	0.8	1.7	10	9	4	WNW 2	NNW 5	SW 3
30	82.8	83.4	86.9	84.4	1.7	7.5	2.6	3.6	9.1	0.1	98	69	82	83	0.1	3.2	1.3	1.5	10 ● ≡	9	1	C 0	N 3	N 3
31																								
M	90.0	89.9	90.4	90.1	7.9	15.2	10.6	11.1	16.9	6.0	82	52	69	68	2.2	10.4	4.9	5.8	6.1	5.9	4.7	3.0	4.5	2.9

Sandomierz $H_s = 202m$ $H_b = 200{,}3m$ $h_w = 20{,}1m$ Marzec - Mars 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	6	•	17	$*^{\circ}0^{00}-3^{20}...3^{45};=0^{00}-24$
2	6	0.0	17	$\triangle 7^{45}-12^{20},14^{40-51}*^{\circ}22^{45}...23^{10};=0^{00}-24$
3	6	0.0	17	$*^{\circ}12^{55}-13^{35};=0^{00}-24$
4	7	1.4	13	$\bullet^{\circ}15^{10}-16^{20},17^{50}...19^{25}-21^{50};=0^{00}-9^{15},15^{30}-24$
5	7	1.8	9	$\bullet^{\circ}14^{45}...21^{10}-23^{20};=0^{00}-8^{20},17^{30}-24$
6	7	1.1	pł.	$\bullet^{\circ}2^{45}...3^{30},6^{12...25},18^{50}...19^{40}-21^{20}...22^{15},\gg 10^{20}-14^{30};=na,p-24$
7	6	1.1	2	$*^{\circ}1^{45}...4^{10}-12^{35};=0^{00}-20^{20}$
8	7	•	2	
9	7	•	pł.	$\sqcup^{\circ}5-9$
10	7	0.0	pł.	$*^{\circ}18^{40}...19^{12},\gg 2^{15}-4^{30};=19^{10}-20^{20}$
11	7	0.1	pł.	$\bullet^{\circ}20^{45}...21^{10}-22^{40};=20^{50}-24$
12	6	7.2	pł.	$\bullet^{\circ}14^{45}...15^{10}-23^{25}*^{\circ}-24;=0^{00}-24$
13	6	1.5	3	$*^{\circ}0^{00}-6^{30},10^{20}-13^{40}\overset{\bullet}{\nabla}{}^{\circ}15^{00}...20^{05},23^{50}-24;+,+5^{35}-7^{45},a-p;\gg-\nwarrow 5^{20}-15^{40},p;=0^{00}-7^{40}$
14	7	0.2	7	$\overset{\bullet}{\nabla}{}^{\circ}0^{00-02},9^{52}...14^{56};\varpi 18^{40}-22^{30}$
15	7	2.5	6	$\triangle 14^{42}-15^{20}*^{\circ}-24;+^{\circ}20^{50}-24;\gg 21^{30}-24;=16^{15}-24$
16	5	19.7	8	$*^{\circ}0^{00}-3^{20}...6^{20}-20^{15}*^{\prime\prime\circ}-24;+^{\circ},+^{\circ},+0^{00}-24;\gg-\nwarrow 0^{00}-17^{20}$
17	6	5.2	19	$*^{\circ\prime}0^{00}-15^{15}\triangle^{\circ}-17^{20}*^{\circ}-24,+,+^{\circ}0^{00}-7^{50},\gg na,np;=0^{00}-24$
18	7	0.0	26	$*^{\circ}0^{00}-8^{35};\gg 0^{00}-3^{30};=0^{00}-9^{15}$
19	7	•	18	
20	7	•	17	$=5^{30}-9^{20}$
21	7	•	14	$=6^{40}-9^{15}$
22	6	3.2	14	$*^{\circ}12^{43}...13^{15}-21^{20}...24;=6^{15}-24$
23	6	6.9	16	$*^{\circ}0^{00}...1^{30}\triangle 7^{15}-10^{15}*^{\circ}-11^{50}\triangle-12^{40}*^{\circ}-13^{20}*\triangle^{\circ}-13^{40}\triangle-14^{25}*^{\circ}-21^{10}*^{\prime\circ}21^{40}-23^{45};=0^{00}-24$
24	6	0.5	20	$*^{\circ}1^{40}...6^{42}\triangle 9^{15}-10^{45},20^{10}-22^{45}*^{\circ}...23^{30}-24;=0^{00}-24$
25	6	0.0	17	$*^{\circ}0^{00}...1^{30},2^{40}-4^{45},6^{20}...7^{20};=0^{00}-14^{20}$
26	7	•	16	$=4^{50}-8^{15}$
27	7	•	15	$\oplus 14^{45}-17^{15}$
28	7	0.0	15	$*^{\circ}10^{20...55};=4^{20}-11^{30},21^{20}-24$
29	7	0.8	12	$\bullet^{\circ}8^{05...55};=0^{00}-10^{30},20^{40}-24$
30	6	1.4	8	$\bullet^{\circ}2^{45}...5^{45}-9^{40},18^{35}...20^{10};=0^{00}-24$
31	7	1.4	4	$\bullet^{\circ}3^{45}...4^{30}-5^{30},7^{05...25},10^{45}...11^{25};=0^{00}-12^{15};np$
Σ	—	56.0	—	UWAGI

Kwiecień - Avril

1	6	0.3	pł.	$\bullet^{\circ}1^{35}-2^{45}\overset{\bullet}{\nabla}{}^{\circ}13^{45-52},15^{53}-16^{06};=0^{00}-14^{30}$
2	7	0.0	pł.	$\overset{\bullet}{\nabla}{}^{\circ}17^{07}...19^{21};=1^{00}-6^{15},\sqcup 2-8;\oplus 7^{40}-13^{00}$
3	8	•	pł.	$=3^{20}-9^{15},\sqcup 1-7$
4	7	•	pł.	
5	7	2.9	•	$\bullet^{\circ}13^{43}...14^{25},p-21^{50};\gg 8^{30}-11^{40};=14^{45}-24$
6	7	0.0	•	$\overset{\bullet}{\nabla}{}^{\circ}p;=0^{00}-9^{40}$
7	7	0.0	•	$\gg 3^{20}-17^{30};=3^{15}-10^{15}$
8	7	0.0	•	$\bullet^{\circ}4^{55}...5^{20}-6^{15}...7^{40}-8^{15};=5^{30}-11^{20}$
9	7	0.0	•	$\overset{\bullet}{\nabla}{}^{\circ}15^{55}-16^{08},16^{12-14};=6^{15}-8^{30}$
10	7	0.0	•	$=5^{30}-7^{20}$
11	7	21.5	•	$\bullet^{\circ}5^{50}...6^{12}\overset{\bullet}{\nabla}{}^{0-2}13^{52}...18^{43}\blacktriangle 15^{15-25},R'14^{42}-16^{50}NE-SSW\,R^{\circ}18^{05}-19^{15}E-WSW;=5^{50}-10^{15}$
12	7	•	•	$=6^{10}-9^{30}$
13	7	3.4	•	$\overset{\bullet}{\nabla}{}^{\circ}14^{56}-15^{05},16^{22}-18^{05};=3^{30}-9^{50}$
14	6	0.0	•	$\bullet^{\circ}3^{53}...8^{22};=3^{30}-24$
15	7	0.0	•	$\bullet^{\circ}9^{48}...10^{05};=0^{00}-12^{15}$
16	7	•	•	$\triangle^{0-1}2-9;23-24$
17	7	•	•	$\triangle^{\circ}0^{00}-9$
18	7	•	•	$\varpi 20^{15}-24$
19	7	•	•	$\triangle^{\circ}4-10,21-23;\varpi 0^{00-100}1^{15-320},21^{25}-24$
20	7	•	•	$\triangle^{0-2}0^{00}-9\triangle^{\circ}21-24;\varpi 0^{00}-1^{15}$
21	7	•	•	$\triangle^{0-1}0^{00}-10$
22	7	•	•	$\triangle^{0-1}2-8$
23	8	•	•	$\triangle^{0-1}2-8$
24	7	•	•	$\triangle^{\circ}23-24$
25	7	•	•	$\triangle^{\circ}0^{00}-8$
26	7	3.6	•	$\overset{\bullet}{\nabla}{}^{\circ}23^{46}-24;\triangle^{\circ}1-9$
27	7	5.2	•	$\overset{\bullet}{\nabla}{}^{0-1}0^{00}...13^{30}\overset{\bullet}{\nabla}{}^{\circ}17^{52}-18^{03}$
28	7	7.1	•	$\overset{\bullet}{\nabla}{}^{\circ}7^{02}...11^{05},14^{20}...15^{43}\blacktriangle 17^{05-09}\overset{\bullet}{\nabla}{}^{\circ}-17^{17}\overset{\bullet}{\nabla}{}^{\circ}19^{30}-20^{05}$
29	7	1.5	•	$\overset{\bullet}{\nabla}{}^{\circ}7^{54}...11^{42}\blacktriangle\overset{\bullet}{\nabla}{}^{\circ}-11^{44}\blacktriangle\overset{\bullet}{\nabla}{}^{\circ}16^{12-15}$
30	7	0.2	•	$\bullet^{\circ}4^{55}...7^{03}\overset{\bullet}{\nabla}{}^{\circ}9^{04}...10^{35}\blacktriangle 9^{50}-10^{00}\overset{\bullet}{\nabla}{}^{\circ}13^{03-08};=3^{30-45}\equiv^{0-2}-5^{20}=-5^{25}\equiv^{0-1}-7^{15}=-9^{30}$
31				
Σ	—	45.5	—	UWAGI

Sandomierz φ=50°41' λ=21°45' Maj-Mai 1962

DNI	CIŚNIENIE P=900+ I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D.v I	II	III
1	86.5	85.9	85.1	85.8	0.4	3.1	1.8	1.8	4.9	-1.5	80	58	91	76	1.3	3.2	0.7	1.7	1 ⊙	10	8	WNW 4	WNW 5	W 3
2	83.1	82.8	84.6	83.5	1.8	7.7	4.8	4.8	9.1	-0.1	93	51	82	75	0.6	5.2	1.5	2.4	8 ⊙	8	10	WSW 3	SW 6	SW 2
3	86.4	86.3	85.7	86.1	3.6	10.2	4.9	5.9	11.4	1.2	88	44	79	70	0.9	7.0	1.8	3.2	9	7 ⊙	1	SW 1	WSW 3	WSW 4
4	81.3	81.1	84.2	82.2	4.6	8.4	4.4	5.4	10.1	2.0	92.	69	85	82	0.7	3.4	1.3	1.6	10 ●	8 ⊙	0	WSW 3	NW 3	WNW 2
5	87.5	89.4	91.9	89.6	4.0	10.6	6.0	6.6	12.3	1.7	93	55	89	79	0.5	5.8	1.1	2.5	7	9 ⊙	6	W 2	WNW 3	NNW 1
6	95.0	95.9	95.8	95.6	7.4	13.0	8.7	9.4	14.1	4.4	87	59	74	73	1.3	6.2	2.8	3.4	7 ⊙	8 ⊙	0	N 1	N 3	ENE 1
7	93.6	92.3	91.6	92.5	7.4	15.5	10.4	10.9	16.1	4.1	87	51	99	79	1.3	8.7	0.2	3.4	6 ⊙	10	10	C 0	SSW 5	SW 1
8	91.6	89.5	88.9	90.0	10.8	21.3	14.0	15.0	23.0	8.1	100	55	95	83	0.0	11.3	0.7	4.0	10 ≡	7 ⊙	10 ●R	C 0	WSW 6	SW 2
9	88.0	89.0	88.7	88.6	14.7	18.0	13.5	14.9	20.0	12.6	90	65	83	79	1.6	7.2	2.7	3.8	5 ⊙	8 ⊙	3	WNW 4	WSW 5	WNW 1
10	85.2	85.9	87.4	86.2	10.2	11.7	10.7	10.8	14.1	10.0	96	94	97	96	0.4	0.8	0.4	0.5	10 ●	10 ●	10	C 0	NE 1	C 0
11	88.6	88.3	89.1	88.7	9.8	14.4	10.0	11.0	16.9	6.6	99	56	92	82	0.1	7.1	1.0	2.7	8	10 ●	10	WNW 1	WNW 3	W 1
12	90.8	91.4	91.4	91.2	10.4	16.2	12.4	12.8	18.1	6.3	92	52	74	73	1.0	8.9	3.7	4.5	0	7 ⊙	8	WSW 2	C 0	WSW 2
13	93.1	92.3	91.2	92.2	11.7	16.6	12.6	13.4	18.6	7.6	76	66	84	75	3.3	6.4	2.4	4.0	2 ⊙	10 ●	8	W 1	SSW 2	C 0
14	82.4	75.4	75.9	77.9	11.0	20.2	9.0	12.3	20.5	8.9	99	72	80	84	0.1	6.7	2.3	3.0	10 ●	9	9	ESE 2	SE 3	SW 12
15	75.4	78.0	80.6	78.0	8.1	7.8	8.1	8.0	9.1	7.5	89	90	86	88	1.2	1.1	1.5	1.3	10	10 ●	10	WSW10	SW 17	W 7
16	83.6	87.4	91.5	87.5	8.2	10.3	7.5	8.4	12.4	7.5	87	72	83	81	1.4	3.5	1.8	2.2	10	10	8	W 9	W 8	W 6
17	92.7	91.0	90.1	91.3	6.0	14.5	10.9	10.6	15.5	3.3	83	57	91	77	1.6	7.1	1.1	3.3	9	9	5	SW 4	SW 6	SW 2
18	90.2	92.8	96.2	93.1	9.5	11.9	9.4	10.0	13.3	9.1	97	81	88	89	0.3	2.6	1.4	1.4	10 ●	10	2	WSW 1	WSW 3	WSW 3
19	96.8	93.5	88.9	93.1	9.0	18.6	15.0	14.4	20.8	4.1	89	47	73	70	1.3	11.2	4.5	5.7	0 ⊙	2 ⊙	2	W 1	SSE 6	SE 3
20	85.2	84.9	88.0	86.0	14.0	21.5	9.9	13.8	21.7	9.7	82	59	92	78	2.9	10.4	1.0	4.8	10	9	10	SE 2	C 0	NNW 7
21	90.6	90.6	89.6	90.3	8.8	11.7	9.5	9.9	12.0	8.2	90	77	97	88	1.1	3.1	0.3	1.5	10	10	10 ●	N 3	NNE 3	NNW 2
22	90.3	91.8	92.8	91.6	9.2	15.0	13.0	12.6	17.1	8.4	95	61	83	80	0.6	6.6	2.6	3.3	10 ●	7 ⊙	8	WNW 2	SW 5	SSW 1
23	95.9	95.0	93.6	94.8	11.4	18.7	15.6	15.3	19.9	8.7	86	57	73	72	1.8	9.4	4.8	5.3	9 ⊙	5 ⊙	8	SW 2	SSW 4	SW 1
24	93.4	94.6	92.1	93.4	12.1	14.8	13.1	13.3	16.6	11.4	95	79	85	86	0.7	3.4	2.3	2.1	10	9	10	SW 1	NNE 3	N 1
25	89.2	90.9	90.6	90.2	9.2	11.1	10.8	10.5	13.7	9.1	99	91	94	95	0.1	1.1	0.9	0.7	10	10	10	NNW 3	N 6	N 4
26	87.1	87.4	88.1	87.5	11.4	14.0	14.3	13.5	19.1	9.9	99	98	92	96	0.2	0.4	1.3	0.6	10	10 ●	10	ENE 2	SSW 1	NW 3
27	91.3	92.4	92.0	91.9	13.6	16.8	15.5	15.4	19.1	11.1	90	82	94	89	1.6	3.5	1.1	2.1	10	10	8	NW 2	NE 1	NNW 2
28	92.2	91.9	89.9	91.3	13.8	21.0	17.4	17.4	21.5	12.1	90	71	94	85	1.6	7.3	1.3	3.4	10	8 ⊙	4	N 2	NNW 1	SW 1
29	92.6	94.2	93.0	93.3	14.5	14.2	14.0	14.2	18.4	13.6	84	89	88	87	2.7	1.8	2.0	2.2	10	10	2	WNW 2	WSW 2	SW 1
30	92.5	94.7	95.6	94.3	11.6	12.2	9.6	10.8	15.3	9.6	100	89	99	96	0.0	1.5	0.2	0.6	10 ●	8	0	NW 4	NW 2	W 2
31	94.9	92.2	88.0	91.7	9.0	19.4	15.3	14.8	20.7	6.5	97	49	73	73	0.3	11.5	4.8	5.5	9	3 ⊙	4	WSW 2	SW 4	SSW 1
M	89.3	89.3	89.4	89.3	9.3	14.2'	10.7	11.2	16.0	7.2	91	68	87	82	1.0	5.6	1.8	2.8	8.1	8.4	6.6	2.5	3.9	2.5

Czerwiec-Juin

1	90.3	94.1	92.9	92.4	9.3	8.5	5.4	7.2	15.5	5.2	95	81	95	90	0.6	2.1	0.5	1.1	10 ●	10	10 ●	NW 3	WSW 4	S 1
2	90.1	93.2	96.4	93.2	4.8	7.3	6.4	6.2	8.0	3.9	97	94	92	94	0.3	0.6	0.7	0.5	10 ●	10	0	N 4	N 3	NW 3
3	97.4	98.7	98.9	98.3	7.0	10.9	8.4	8.7	12.3	4.4	98	89	93	93	0.1	1.4	0.7	0.7	10 ●	9	10	NW 2	NNE 1	N 2
4	96.9	95.5	92.5	95.0	7.6	8.4	7.4	7.7	8.7	7.1	99	94	96	96	0.1	0.6	0.5	0.4	10 ●	10 ●	10 ●	NW 5	NW 5	N 6
5	89.9	91.1	94.1	91.7	6.5	7.4	7.0	7.0	8.3	6.0	94	96	96	95	0.6	0.5	0.4	0.5	10 ●	10 ●	10 ●	NW 9	NNW 7	N 7
6	94.3	96.4	98.6	96.4	4.0	5.6	4.3	4.6	7.3	3.2	95	86	90	90	0.4	1.3	0.8	0.8	10 ●	10 ●	10	N 8	NW 8	N 7
7	99.2	101.5	101.8	100.8	4.2	7.0	8.6	7.1	9.6	3.5	98	78	77	84	0.1	2.2	2.6	1.6	10	10	10	NNE 4	N 3	W 4
8	102.5	103.1	101.3	102.3	9.1	15.5	12.4	12.4	17.5	5.5	81	51	73	68	2.2	8.6	3.9	4.9	8	9	1	N 4	N 3	C 0
9	97.2	94.1	89.8	93.7	10.8	19.3	15.3	15.2	21.0	5.9	86	55	72	71	1.8	10.1	5.0	5.6	1 ⊙	4 ⊙	8	WSW 2	WSW 5	SW 3
10	89.4	88.7	88.2	88.8	12.5	18.6	13.4	14.5	20.0	10.2	72	53	73	66	4.1	10.0	4.2	6.1	2 ⊙	3 ⊙	1	NW 3	N 3	NNE 1
11	85.8	83.8	84.8	84.8	13.2	19.8	14.0	15.2	20.7	8.5	78	54	88	73	3.3	10.6	2.0	5.3	1 ⊙	8	4	NNE 1	NW 3	W 2
12	87.9	88.6	90.3	88.9	12.8	15.2	10.2	12.1	15.6	10.0	83	59	68	70	2.6	7.2	3.9	4.6	8	9	2	NW 3	WNW 3	WNW 2
13	92.8	93.9	94.8	93.8	10.7	15.7	11.6	12.4	18.1	8.1	85	60	79	75	2.0	7.1	2.8	4.0	7	7 ⊙	2	NW 3	WNW 3	WSW 1
14	95.1	93.6	93.5	94.1	12.2	20.0	15.9	16.0	21.5	7.5	85	46	73	68	2.2	12.7	4.9	6.6	4 ⊙	2 ⊙	1	C 0	SW 5	SW 1
15	95.9	95.7	97.1	96.2	12.2	26.3	18.9	19.1	27.3	11.1	93	44	72	70	1.0	19.1	6.1	8.7	10	4 ⊙	0	SW 3	WSW 4	N 1
16	98.1	97.0	95.2	96.8	18.4	28.3	23.9	23.6	29.4	13.1	74	40	65	60	5.5	23.0	10.2	12.9	0 ⊙	0 ⊙	8	N 1	E 1	C 0
17	95.4	96.7	96.7	96.3	20.2	23.4	19.7	20.8	24.7	17.8	82	67	78	76	4.2	9.5	5.1	6.3	6 ⊙	9 ⊙	9	NNW 2	W 3	NNW 2
18	97.4	96.6	95.3	96.4	16.6	22.0	17.0	18.2	22.9	13.4	79	49	71	66	4.1	13.4	5.6	7.7	2 ⊙	3 ⊙	0	NNW 3	NW 3	N 1
19	95.0	93.1	90.8	93.0	17.2	25.5	20.3	20.8	26.6	12.2	80	48	78	69	3.9	17.1	5.2	8.7	1 ⊙	3 ⊙	0	N 1	ESE 3	SE 1
20	90.7	93.0	95.4	93.0	18.2	23.6	18.4	19.6	24.7	14.6	89	64	69	74	2.3	10.4	6.7	6.5	1	7 ⊙	9	SE 2	NW 3	NNW 3
21	97.5	97.7	97.4	97.5	18.2	22.6	17.6	19.0	23.6	14.1	67	50	87	68	7.0	13.7	2.6	7.8	9	9	5	C 0	NNW 1	NNW 1
22	99.9	100.1	99.2	99.7	18.5	24.7	19.3	20.4	26.1	16.3	79	49	77	68	4.5	16.0	5.2	8.6	3 ⊙	2 ⊙	1	NNW 3	WNW 2	C 0
23	99.1	97.3	95.1	97.2	18.6	27.1	22.4	22.6	28.5	14.8	80	45	75	67	4.3	19.6	6.7	10.2	0	1 ⊙	2	C 0	SSW 4	WNW 2
24	95.1	94.8	92.0	94.0	20.0	25.4	23.0	22.8	27.0	17.1	85	53	68	69	3.5	15.1	8.9	9.2	3 ⊙	7 ⊙	1	N 3	WNW 2	W 1
25	90.6	92.6	95.0	92.7	19.9	22.4	15.5	18.3	23.6	15.3	87	57	65	70	3.0	11.6	6.2	6.9	0 ⊙	9	2	SW 2	WNW 4	NNW 2
26	95.4	93.4	90.7	93.2	14.2	18.5	14.0	15.2	19.9	9.4	62	46	66	58	6.1	11.6	5.4	7.7	3 ⊙	8 ⊙	6	NW 2	WSW 3	W 1
27	87.7	88.3	89.5	88.5	13.2	17.3	13.1	14.2	19.8	10.3	80	63	58	67	3.0	7.3	6.4	5.6	7 ⊙	9	6	SW 1	NW 5	NW 3
28	89.5	88.9	87.0	88.3	9.9	14.1	9.3	10.6	15.6	6.8	81	45	91	72	2.4	8.8	1.1	4.1	3 ⊙	8 ⊙	10	W 3	W 6	WSW 1
29	86.0	87.3	88.2	87.2	9.5	12.4	12.0	11.5	14.7	7.8	79	67	70	72	2.5	4.8	4.1	3.8	6 ⊙	7 ⊙	10	W 7	W 9	WSW 8
30	87.6	89.5	90.8	89.3	10.9	11.7	10.8	11.0	12.9	9.6	75	77	94	82	3.2	3.1	0.9	2.4	9	10	10	WSW 7	W 7	W 4
31																								
M	93.7	94.0	93.8	93.8	12.7	17.5	13.8	14.4	19.0	9.8	84	62	78	75	2.7	9.3	4.0	5.3	5.5	6.9	5.3	3.0	3.9	2.4

Sandomierz $H_s = 202m$ $H_b = 200{,}3m$ $h_w = 20{,}1m$ Maj - Mai 1962

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	0.3	•	⛆°13^{55}-14^{04}, 14^{51}-15^{10} ⛆°15^{55}-16^{10} ⛆°16^{36-50}; ⌣°4-7
2	7	0.4	•	⛆'11^{25-32} ⛆'11^{35-40} ⛆°$15^{17...42}$ 17^{35-47}; $=1^{20}$-7^{30}
3	7	1.6	•	$=1^{00}$-8^{30}, 23^{15}-24; ⌓$^{0-1}$3-10, 20-24
4	7	2.8	•	•$^{0-1}2^{56}$...5^{15}-8^{35} 9^{05}...10^{00} ⛆$^{0-2}10^{05-21}$; ⛆°13^{12}...15^{57} ▲13^{14-20}; $=0^{10}$-10^{25}; ⌓' na
5	7	•	•	$=3^{30}$-9^{50}; ⌓°21-24
6	7	•	•	⌓°0^{00}-8 ⌓'20-24
7	7	0.3	•	•°14^{48}...15^{30}-17^{40}; $=3^{20}$-9^{45}; 15^{15}-24; ⌓$^{0-2}0^{00}$-9^{30}
8	7	5.9	•	⛆°15^{43-47} 18^{23}-20^{12} ⛆$^{0-1}22^{25}$-24; ☈°18^{25}-19^{40} SSW-SE, 19^{50}-20^{10}W; $=0^{00}$-2^{48} ≡$^{0-2}$-8^{30} = -10^{10}
9	7	2.7	•	⛆°0^{00}...1^{29}; $=1^{30}$-7^{15} 22^{15}-24; ⌓°19-24
10	6	5.6	•	⛆°3^{45}-4^{03} •$^{0-1}4^{05}$...5^{10}-9^{20}...9^{50}-14^{30}...17^{30}; $=0^{00}$-23^{50} ≡'-24; ⌓°na
11	7	3.6	•	⛆°12^{30-56} •°19^{45}-22^{35}; ≡$^{1-0}0^{00}$-5^{50} = -9^{30}, 20^{10}-24
12	7	•	•	$=0^{00}$-8^{30}; ⌓$^{0-1}$19-24
13	7	14.0	•	⛆$^{0-2}12^{25}$-13^{06} •°21^{30}...22^{15}-24; $=3^{20}$-8^{30}, 22^{00}-24; ⌓$^{1-2}0^{00}$-9 ⌓°20-21^{30}; ⌔ 20^{30-45}
14	7	12.9	•	•$^{0-2}0^{00}$-9^{45} ⛆$^{0-1}13^{30}$-14^{05}, 16^{15}-17^{05} 22^{50}-23^{05}; ☈'13^{28}-14^{10} SSW-NNW ☈°16^{15-40} S-NNE; ⛷p...24; $=0^{00}$-10^{30}
15	7	0.8	•	⛆°2^{30}-3^{05} •°-4^{30}...9^{42}, 10^{12}-12^{47}, 17^{35}-18^{48}; ⛷ na-10^{15} ⛷-16^{40} ⛷-18^{25}; =na-a,p
16	7	0.1	•	•°0^{50}-1^{16}, 5^{55}...6^{05}, $9^{23...35}$; $10^{05...20}$ ⛆°15^{20-32}; 16^{44}-17^{03}; ⛷ 11^{30}-12^{15}; $=0^{00}$-11^{15}
17	7	3.6	•	⛆°16^{43-46}; $=3^{15}$-8^{40}
18	6	3.7	•	•$^{0-1}2^{35}$-9^{32} •°12^{47-59} ⛆'15^{31-38}; $=2^{15}$-14^{30}; ⌔ 21^{50}-22^{50}
19	7	0.0	•	$=1^{50}$-4^{50} ≡$^{2-0}$-5^{45} = -8^{45}; ⌓$^{0-1}$4-10 ⌓°22-24
20	7	12.5	•	•°6^{10-14} ⛆$^{0-2}13^{50}$-14^{48} •°20^{48}-22^{35} 23^{52}-24; ☈°14^{20}-15^{05} W-SE; $=3^{30}$-8^{15}; np; ⌓' na
21	6	8.5	•	•$^{0-1}0^{00}$-2^{25} ⛆°11^{43}-12^{06}, 13^{50}-14^{15} •$^{0-1}$-22^{35}...23^{20}; $=0^{00}$-24
22	7	0.0	•	•°0^{35}...3^{30}-6^{15}...6^{45} ⛆°18^{55}-19^{01}; $=0^{00}$-11^{30}; ⌓°22-24
23	7	0.3	•	$=1^{00}$-8^{30}; ⌓$^{0-1}0^{00}$-9, 20-24
24	6	14.6	•	⛆°5^{35}...10^{15} •°-12^{02}...12^{10}, 21^{45}-22^{38}; $=3^{30}$-14^{30}, 21^{15}-24; ⌓$^{1-2}$na
25	6	4.4	•	•$^{0-1}0^{45}$...1^{53}-3^{30} •°10^{05}-11^{25} •°23^{28}-24; $=0^{00}$-13^{40}, np
26	6	2.1	•	•°0^{00-22}, 1^{30}-2^{25} ⛆$^{0-1}12^{11-45}$ ⛆°12^{53}-13^{43} •°13^{50}...14^{16} ⛆°17^{33}-18^{05}; $=0^{00}$-15^{20}
27	6	0.1	•	⛆°11^{56}...15^{47}; $=5^{20}$-14^{40}, 22^{30}-24
28	7	0.7	•	⛆°15^{25}-16^{20}; $=0^{00}$-6^{20}, 21^{30}-24
29	6	5.0	•	⛆°2^{50}-3^{03}, 3^{26-31}, 8^{03-16} •°12^{52}...13^{08} ⛆°15^{58}-16^{08}; ☈°2^{48}-3^{40} SW-N; $=0^{00}$-24
30	6	5.5	•	⛆°5^{05-12} ⛆$^{0-1}6^{15}$-8^{23} ⛆°10^{05}...14^{09} ⛆$^{0-1}18^{54}$-19^{15}; ☈°18^{48}-19^{25} W-SE; $=0^{00}$-15^{30}, 21^{15}-24; ⌓$^{0-1}$na
31	7	1.7	•	$=0^{00}$-3^{45} ≡ •-5^{40} = -10^{30}; ⌓°21-24
Σ	—	113.7	—	UWAGI

Czerwiec - Juin

1	6	30.7	•	•°5^{10}...6^{05}-7^{15} •°...8^{00} •°-9^{35} •'11^{25-40} •°18^{17}...19^{05} •$^{0-1}$-24; (☈)°22^{43}-24 S; $=5^{30}$-13^{40}, 18^{30}-24; ⌓° na
2	6	2.9	•	⛆$^{0-2}0^{00}$-3^{30} •°-12^{15} •°-13^{05}, 17^{40}...18^{27}; (☈)°0^{00}-1^{25} S-NW; $=0^{00}$-14^{15}, 17^{45}-24
3	7	5.6	•	•°4^{50}...6^{45}-10^{30}...12^{05} ⛆°...19^{35}; $=0^{00}$-12^{15}
4	6	38.2	•	•$^{0-1}2^{45}$-24; $=0^{30}$-24
5	6	12.1	•	•°0^{00}-7^{20}...9^{30}-13^{35}...19^{30}, 20^{45}...22^{25}-24; ⛷ 0^{15}-9^{30}; $=0^{00}$-24
6	6	7.0	•	•°0^{00}-4^{20}...5^{40} •$^{0-1}$-11^{15} •°11^{38}-14^{20}...17^{21} ⛆▲-17^{23} ⛆°...22^{05}; ⛷ 18^{40}-19^{30}; $=0^{00}$-24
7	7	0.0	•	•°1^{10}...3^{40}-5^{15}...6^{25} ⛆°16^{45-56}; $=0^{00}$-11^{20}
8	7	•	•	⌓° np-24
9	7	•	•	⌓°0^{00}-9
10	7	•	•	⌓$^{0-1}$2-9, 21-24
11	7	2.7	•	⛆°11^{39-41}, 13^{54}...16^{06}; (☈)°14^{03-35} W-S; ⌓$^{0-2}0^{00}$-11
12	7	•	•	$=3^{15}$-8^{30}; ⌓°22-24
13	7	1.6	•	⛆°10^{50}...13^{58}; ⌓°0^{00}-9, 21-23
14	7	0.0	•	⌓$^{1-0}0^{00}$-10 ⌓°23-24
15	7	•	•	⛆°7^{48-52}; $=2^{50}$-10^{20} ∞ 10^{30}-12^{15}; ⌓$^{0-1}0^{00}$-7^{48}, 19-24
16	7	0.0	•	⌓$^{0-2}0^{00}$-10 ⌓°22-24
17	7	0.8	•	⛆°5^{05-08} ⛆$^{0-1}8^{55}$-9^{03}; ☈°3^{20-55} SW-W-NW, 4^{05}-5^{40} S-N, 8^{47}-10^{20} W-N; =na; ⌓° na
18	7	•	•	⌓$^{0-1}0^{00}$-10
19	7	•	•	⌓$^{0-1}$2-9 ⌓°21-24
20	7	•	•	⌓$^{0-1}0^{00}$-10
21	7	0.0	•	•°$8^{26...35}$; ⌓°0^{00}-8^{30}, 21-24
22	7	•	•	⌓°0^{00}-9, 21-24
23	7	•	•	⌓°0^{00}-9, 22-24
24	7	•	•	☾1^{40}-2^{35} W-NW; ⌓°0^{00}-10
25	7	•	•	$=4^{50}$-8^{10}; ⌓$^{0-1}$2-9
26	7	•	•	⌓°0^{00}-3, 22-24
27	7	•	•	⌓$^{0-1}0^{00}$-10; ⊕ 7^{28}-10^{20}
28	7	1.9	•	⛆$^{0-1}18^{38}$-19^{23}; ⛷ 15^{10-22}, 18^{12-21}; $=22^{20}$-24; ⊕ 16^{45}-18^{05}
29	7	0.0	•	•°2^{10}...3^{25} ⛆°11^{35-42}; $=0^{00}$-4^{30}
30	7	0.8	•	⛆°11^{08-12}, 16^{31-40}, 19^{12-26}, 22^{46}-23^{10}
31				
Σ	—	104.5	—	UWAGI

Sandomierz φ = 50°41' λ = 21°45' Lipiec-Juillet 1962

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N.w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D.v I	II	III
1	91.9	92.8	92.3	92.3	11.8	14.7	12.6	12.9	17.9	10.3	89	76	76	80	1.5	4.0	3.6	3.0	9	9 ●	9	NW 3	NW 3	WNW 2
2	91.9	89.9	88.4	90.1	11.4	15.9	11.3	12.5	17.1	8.0	79	57	84	73	2.8	7.9	2.2	4.3	5	7	8	WNW 1	WSW 3	W 2
3	83.1	80.4	79.6	81.0	10.4	12.0	9.8	10.5	15.1	7.9	97	88	96	94	0.3	1.7	0.5	0.8	10 ●	10	8	SW 3	SW 5	SW 2
4	79.1	80.5	81.8	80.5	9.0	14.8	11.0	11.4	17.1	8.1	95	61	71	76	0.7	6.5	3.8	3.7	10 ●	4 ⊙	5	SW 2	SSW 5	C 0
5	83.9	84.6	86.2	84.9	9.5	17.8	14.4	14.0	18.9	7.4	86	44	73	68	1.7	11.5	4.4	5.9	2 ⊙	7 ⊙	10 ●	C 0	SW 5	SW 1
6	91.7	92.2	93.2	92.4	11.4	17.6	13.8	14.2	20.0	9.6	91	61	84	79	1.2	7.9	2.5	3.9	6 ⊙	5 ⊙	7	SW 3	SW 3	S 2
7	93.2	92.8	92.8	92.9	12.2	17.1	13.2	13.9	19.7	9.4	92	72	88	84	1.2	5.4	1.8	2.8	7 ⊙	9	10 ●	SSW 2	NW 4	SW 5
8	93.8	94.2	95.5	94.5	10.1	16.8	11.8	12.6	18.3	9.6	97	62	85	81	0.4	7.3	2.0	3.2	10	6 ⊙	2	W 3	WNW 5	W 3
9	96.9	96.0	94.4	95.8	11.4	18.2	13.6	14.2	20.3	8.2	94	56	82	77	0.9	9.2	2.8	4.3	10	4 ⊙	0	NW 3	WNW 4	NW 1
10	92.7	91.4	89.3	91.1	15.2	21.1	16.4	17.3	22.2	10.5	76	42	62	60	4.3	14.5	7.0	8.6	1 ⊙	4 ⊙	1	NW 2	W 4	WNW 3
11	88.9	87.9	86.3	87.7	15.4	23.6	18.6	19.0	24.8	10.0	77	46	73	65	4.1	15.6	5.7	8.5	0 ⊙	3 ⊙	10	WSW 2	W 5	SW 2
12	84.6	85.2	85.7	85.2	17.2	23.6	18.6	19.5	24.7	15.3	88	46	64	66	2.4	15.8	7.8	8.7	10	3 ⊙	9	SW 4	WNW 6	WSW 1
13	84.1	84.0	85.1	84.4	15.3	20.1	13.0	15.4	20.4	12.9	86	56	80	74	2.4	10.3	3.0	5.2	9	4 ⊙	5	SW 2	WSW 7	NW 1
14	84.5	84.7	84.7	84.6	13.0	16.6	13.0	13.9	18.7	10.6	87	71	93	84	1.9	5.5	1.1	2.8	10	9 ⊙	10	WSW 6	W 5	W 4
15	84.8	83.8	83.3	84.0	14.0	20.8	14.6	16.0	22.0	11.1	90	58	97	82	1.6	10.4	0.5	4.2	4 ⊙	4 ⊙	9	SW 2	SW 3	WSW 1
16	83.9	84.2	85.4	84.5	14.2	19.3	16.0	16.4	21.6	12.6	100	76	94	90	0.0	5.4	1.2	2.2	9 ≡	9 ●(R)	3	W 1	W 2	E 0
17	87.5	88.6	89.5	88.5	14.3	22.2	17.2	17.7	22.7	12.5	100	61	79	80	0.0	10.4	4.1	4.8	10	9 ⊙	10	W 1	NNE 3	NE 3
18	89.3	88.2	88.1	88.5	15.2	19.9	15.4	16.5	20.2	13.1	82	67	98	82	3.2	7.5	0.4	3.7	10	10	10 ●	N 3	NNE 6	N 4
19	87.2	88.7	90.5	88.8	14.2	17.2	16.1	15.9	18.0	14.1	99	98	96	98	0.2	0.4	0.8	0.5	10 ●	10 ●	5	WNW 5	NW 4	C 0
20	93.5	94.4	94.7	94.2	16.0	23.2	17.7	18.6	25.0	12.8	86	49	73	69	2.5	14.4	5.5	7.5	1 ⊙	2 ⊙	4	NW 3	NW 2	SSW 2
21	95.5	94.3	93.5	94.4	15.8	26.1	20.2	20.6	26.6	12.5	87	48	64	66	2.2	17.7	8.7	9.5	0 ⊙	2 ⊙	0	SSW 2	S 2	S 1
22	93.9	93.1	93.1	93.4	16.9	26.8	19.9	20.9	28.0	14.0	80	56	90	75	3.8	15.4	2.4	7.2	2 ⊙	1 ⊙	7(R)	SSE 1	S 2	N 1
23	94.1	95.0	96.8	95.3	17.2	24.0	18.2	19.4	25.0	16.6	98	60	91	83	0.4	11.8	1.9	4.7	9	6 ⊙	3	NNW 1	WNW 1	N 1
24	98.3	99.1	100.1	99.2	16.6	21.6	14.8	17.0	22.2	14.7	81	52	75	69	3.7	12.3	4.1	6.7	9	7 ⊙	0	SW 5	NW 4	NW 1
25	101.7	100.7	99.5	100.6	13.8	21.4	16.7	17.2	22.8	10.2	80	52	70	67	3.2	12.2	5.7	7.0	2 ⊙	6 ⊙	2	C 0	W 1	C 0
26	97.8	95.8	93.9	95.8	14.9	27.1	22.4	21.7	28.7	11.9	83	46	70	66	2.9	19.2	8.1	10.1	0	0 ⊙	0	SSE 2	SSW 2	C 0
27	93.3	92.1	92.4	92.6	19.8	27.3	19.4	21.5	27.7	17.1	80	57	93	77	4.5	15.5	1.5	7.2	8 ⊙	4 ⊙	9	SW 2	SW 2	SW 2
28	94.4	95.1	94.8	94.8	13.6	18.8	13.3	14.8	20.9	12.2	85	55	93	78	2.3	9.7	1.1	4.4	8 ⊙	4 ⊙	2	WNW 4	W 6	NW 1
29	96.7	95.7	96.2	96.2	12.6	18.6	12.5	14.0	20.0	9.0	85	52	80	72	2.2	10.3	2.9	5.1	1 ⊙	6 ⊙	0	NW 3	N 3	NW 1
30	97.4	96.7	97.0	97.0	12.5	19.8	14.5	15.3	21.7	9.1	85	52	76	71	2.2	11.0	3.9	5.7	2 ⊙	6 ⊙	9	SW 2	NNE 2	NNE 1
31	97.9	97.5	97.1	97.5	12.8	21.2	14.4	15.7	22.0	9.6	84	49	78	70	2.4	12.9	3.6	6.3	2 ⊙	5 ⊙	1	N 1	NE 2	SSW 1
M	91.2	91.0	91.0	91.1	13.8	20.2	15.3	16.2	21.6	11.3	88	59	82	76	2.0	10.3	3.4	5.2	6.0	5.6	5.4	2.4	3.6	1.6

Sierpień-Août

1	96.1	94.3	94.1	94.8	11.8	21.6	15.4	16.0	23.1	8.9	90	62	92	81	1.3	9.9	1.3	4.2	1	8 ⊙	8	SW 3	SW 3	WNW 1
2	93.8	93.3	92.8	93.3	15.9	21.5	16.0	17.4	23.4	11.6	75	48	78	67	4.5	13.3	4.0	7.3	0 ⊙	8 ⊙	2	WNW 1	WSW 6	C 0
3	92.2	92.6	92.4	92.4	13.4	16.1	16.4	15.6	19.5	12.1	94	98	97	96	0.9	0.4	0.6	0.6	10 ●	10	1	NW 2	N 1	SE 1
4	93.5	93.3	91.9	92.9	13.9	23.6	22.0	20.4	26.3	13.0	100	71	76	82	0.0	8.4	6.4	4.9	10 ≡	1 ⊙	3	C 0	SE 1	SSE 1
5	91.8	89.7	86.2	89.2	18.4	26.4	18.2	20.3	28.0	16.5	90	57	97	81	2.1	14.8	0.6	5.8	4 ⊙	3 ⊙	10 ●R	NW 2	NW 1	WNW 1
6	87.8	89.4	89.8	89.0	17.2	23.2	19.1	19.6	24.3	16.0	96	69	88	84	0.8	8.7	2.8	4.1	0 ⊙	7 ⊙	2	W 2	NW 3	C 0
7	87.9	84.5	82.9	85.1	17.6	29.5	24.2	23.9	30.0	15.2	93	43	71	69	1.4	23.6	8.8	11.3	1	2 ⊙	3	SE 1	SSW 6	SSW 5
8	93.5	94.0	95.4	94.3	15.6	22.6	17.3	18.2	24.2	15.3	79	47	74	67	3.7	14.5	5.1	7.8	9	1 ⊙	1	WSW 5	SW 3	C 0
9	99.0	99.3	99.9	99.4	17.9	23.6	15.8	18.3	24.1	15.6	68	45	72	62	6.5	16.0	5.0	9.2	6 ⊙	3 ⊙	1	N 2	NNW 1	N 1
10	100.5	97.8	95.1	97.8	14.6	23.0	19.0	18.9	24.3	10.3	77	46	67	63	3.8	15.1	7.2	8.7	9	1 ⊙	7	N 1	NE 1	E 1
11	93.4	93.5	94.6	93.8	15.6	24.1	17.9	18.9	25.0	13.5	94	47	76	72	1.1	15.9	5.0	7.3	1 ⊙	7 ⊙	6	SE 1	WSW 3	C 0
12	96.2	95.5	94.5	95.4	17.2	27.2	22.2	22.2	29.0	13.6	88	48	70	69	2.4	18.7	8.0	9.7	0 ⊙	0 ⊙	2	C 0	WSW 2	C 0
13	94.7	94.4	93.6	94.2	18.4	28.9	24.2	23.9	30.0	16.4	93	51	62	69	1.5	19.6	11.5	10.9	8	6 ⊙	6	C 0	SW 2	SW 1
14	94.8	94.3	93.6	94.2	17.3	24.2	18.2	19.5	26.2	17.2	94	65	93	84	1.2	10.6	1.5	4.4	10	6 ⊙	0	NNW 5	N 2	N 1
15	91.7	90.0	85.3	89.0	17.1	24.4	21.8	21.3	27.2	15.6	90	69	88	82	2.0	9.6	3.0	4.9	9	8 ⊙	5	NNE 2	E 4	SE 1
16	87.0	89.2	89.8	88.7	18.1	18.8	18.0	18.2	22.3	17.1	96	94	95	95	0.9	1.3	1.0	1.1	10	10	8	S 1	SW 1	WSW 1
17	91.4	91.1	89.0	90.5	14.4	24.4	19.4	19.4	26.0	12.7	100	52	84	79	0.0	14.8	3.6	6.1	2 ⊙ ≡	7 ⊙	5	WSW 1	WSW 1	C 0
18	87.2	87.7	91.0	88.6	16.2	23.6	15.4	17.6	24.7	15.3	97	53	73	74	0.6	13.8	4.8	6.4	8 ⊙	8 ⊙	4	WSW 3	W 4	W 2
19	91.2	91.2	91.4	91.3	12.4	14.4	11.7	12.6	16.1	11.0	85	73	90	83	2.2	4.4	1.3	2.6	9	9	9	WSW 5	WNW 4	W 4
20	87.9	89.2	90.1	89.1	12.8	14.5	15.0	14.3	17.4	11.2	95	93	92	93	0.7	1.1	1.3	1.0	10 ●	10 ●	6	W 6	WNW 7	WNW 6
21	91.0	91.2	91.2	91.1	14.6	18.5	13.7	15.1	20.1	13.5	90	72	92	85	1.6	5.9	1.3	2.9	9	9	0	NW 3	NW 2	W 1
22	91.7	92.7	94.3	92.9	13.1	18.6	14.6	15.2	19.5	10.8	98	80	99	92	0.4	4.3	0.2	1.6	8	10	7	WNW 1	WSW 1	W 1
23	92.9	94.6	95.6	94.4	12.2	20.3	14.2	15.2	21.5	11.0	100	46	72	73	0.0	12.8	4.6	5.8	10 ≡	7 ⊙	5	W 3	W 6	WNW 2
24	92.9	90.4	87.1	90.1	13.4	18.8	18.4	17.2	21.1	12.7	86	72	74	77	2.1	6.1	5.5	4.6	10	10	4	SW 3	SW 4	SW 2
25	90.2	91.1	93.7	91.7	15.9	18.0	14.2	15.6	18.9	13.8	96	69	97	87	0.8	6.3	0.6	2.6	7	8 ⊙	0	WSW 5	WSW 3	WSW 2
26	97.2	98.5	98.6	98.1	12.5	18.6	12.0	13.8	20.1	10.6	86	48	81	72	2.1	11.1	2.7	5.3	4 ⊙	6 ⊙	1	WSW 5	W 7	W 1
27	94.9	91.0	90.3	92.1	10.3	24.4	19.2	18.3	26.2	7.4	88	46	66	67	1.4	16.5	7.5	8.5	1 ⊙	0 ⊙	3	SSE 2	SW 5	W 2
28	95.5	96.4	96.5	96.1	13.6	18.3	14.8	15.4	19.3	12.7	72	48	61	60	4.4	11.0	6.5	7.3	6 ⊙	9	10	W 4	WSW 8	WNW 5
29	96.5	94.6	92.6	94.6	10.2	21.6	15.3	15.6	22.4	7.5	87	42	90	73	1.6	14.9	1.7	6.1	10	1 ⊙	9	WSW 1	SW 5	WSW 4
30	95.6	97.0	97.1	96.6	11.4	15.0	11.0	12.1	17.1	9.8	86	67	77	77	1.8	5.5	3.1	3.5	2 ⊙	9	2	W 3	WNW 7	W 3
31	93.8	90.9	91.1	91.9	7.8	15.4	11.7	11.6	16.3	6.3	90	58	71	73	1.1	7.4	3.9	4.1	9	10	9	SW 3	WSW 4	W 3
M	93.0	92.7	92.3	92.7	14.5	21.4	17.0	17.5	23.0	12.7	89	61	81	77	1.8	10.8	3.9	5.5	6.2	6.3	4.5	2.5	3.5	1.7

Sandomierz $H_s = 202m$ $H_b = 200{,}3m$ $h_w = 20{,}1m$ Liniec - Juillet 1962

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚNIEGU h	POGODA
1	7	2.8	•	$\overset{\bullet}{\nabla}{}^{0-1}10^{15}...16^{30}$
2	7	2.2	•	$\overset{\bullet}{\nabla}{}^{\circ}13^{52}-14^{03}; \triangle^{\circ}21-24$
3	7	4.5	•	$\bullet^{\circ}5^{20}...11^{40}\overset{\bullet}{\nabla}{}^{0-1}13^{10}-18^{22} = 2^{30}-12^{15}, 22^{30}-24; \triangle^{\circ}na$
4	7	0.3	•	$\bullet^{\circ}5^{44-49}, 7^{28}-8^{42}; = 0^{00}-9^{20}; \triangle^{\circ}np$
5	7	1.2	•	$\overset{\bullet}{\nabla}{}^{\circ}20^{52}...22^{05}; = 22^{45}-24; \triangle^{0-1}0^{00}-9; \oplus 13^{40}-14^{10}$
6	7	0.0	•	$\bullet^{\circ}0^{40}-3^{45}\overset{\bullet}{\nabla}{}^{\circ}19^{57}-20^{06}; (\mathfrak{R})^{\circ}19^{53}-20^{08}$ NNW-N-NE; $= 0^{00}-8^{15}$
7	7	8.2	•	$\overset{\bullet}{\nabla}{}^{1}12^{07-17}\overset{\bullet}{\nabla}{}^{\circ}12^{27}-13^{12}, 21^{21}...23^{05}; \mathfrak{R}^{\circ}12^{12-45}$ SSW-NNE; $= 4^{30}-10^{15}, np$
8	7	•	•	$\overset{\bullet}{\nabla}{}^{\circ}1^{30}-2^{22}, 3^{37}-4^{05}\bullet^{\circ}-7^{08}...7^{30}; = 0^{00}-11^{30}; \triangle^{\circ}np$
9	7	•	•	$\triangle^{0-1}0^{00}-10, np$
10	7	•	•	$\triangle^{0-1}0^{00}-9$
11	7	•	•	$= 23^{30}-24; \triangle^{\circ}np$
12	7	0.0	•	$\overset{\bullet}{\nabla}{}^{\circ}21^{55}-22^{04}; = 0^{00}-9^{15}; \triangle^{\circ}0^{00}-8$
13	7	0.0	•	$\overset{\bullet}{\nabla}{}^{\circ}14^{49-55}; (\mathfrak{R})^{\circ}12^{10-40}$ SSE-E-ENE
14	7	0.0	•	$\overset{\bullet}{\nabla}{}^{\circ}19^{06-13}; = 23^{45}-24$
15	7	3.8	•	$\overset{\bullet}{\nabla}{}^{\circ}16^{20}...18^{15}\bullet^{\circ}...19^{30}\overset{\bullet}{\nabla}{}^{0-1}22^{40}-23^{38}; = 0^{00}-8^{30}, 23^{40}-24; \triangle^{\circ}na-a$
16	7	0.1	•	$\overset{\bullet}{\nabla}{}^{\circ}0^{25-39}, 12^{23}...14^{02}; (\mathfrak{R})^{\circ}12^{45}-13^{35}$ N-SSW; $= 0^{00}-4^{40} \equiv^{0-2}-8^{20} = -12^{30}, 22^{10}-24$
17	7	•	•	$= 0^{00}-3^{40} \equiv^{1-0}-7^{30} = -11^{30}; \oplus 14^{30}-15^{45}$
18	7	33.0	•	$\overset{\bullet}{\nabla}{}^{\circ}14^{05-10}\overset{\bullet}{\nabla}{}^{0-1}14^{25}-16^{20}\bullet^{0-1}-24; = 17^{20}-24$
19	6	15.7	•	$\bullet^{0-2}0^{00}-17^{45}; = 0^{00}-24$
20	7	•	•	$= 0^{00}-5^{15}; \triangle^{0-1}20-24$
21	7	•	•	$= 4^{30}-8^{30}; \triangle^{0-2}0^{00}-11 \triangle^{\circ}21-24$
22	7	1.6	•	$(\mathfrak{R})^{\circ}20^{35}-24; \triangle^{0-1}0^{00}-9$
23	7	•	•	$\overset{\bullet}{\nabla}{}^{\circ}0^{25-27}, 1^{45}...6^{45}, 16^{48-55}; (\mathfrak{R})^{\circ}0^{00-10}$ SE-E-NE, $1^{57}-4^{30}$ E-S; $\triangle^{0-1}20-24$
24	7	0.0	•	$\overset{\bullet}{\nabla}{}^{\circ}15^{53-55}; \triangle^{1-0}0^{00}-10 \triangle^{\circ}21-24$
25	7	•	•	$\triangle^{0-1}0^{00}-10 \triangle^{\circ}20-24$
26	7	•	•	$\triangle^{0-1}0^{00}-9, 20-24$
27	7	1.0	•	$\overset{\bullet}{\nabla}{}^{\circ}10^{20}...12^{01}, 15^{40}...19^{34}, 21^{37-42}, 22^{48}-23^{12}; (\mathfrak{R})^{\circ}15^{15}-16^{20}$ S-SE-E; $= 4^{15}-8^{30}; \triangle^{1-0}0^{00}-8$
28	7	•	•	$\triangle^{\circ}21-24$
29	7	•	•	$\triangle^{0-1}0^{00}-9, 20-24$
30	7	•	•	$= 21-24; \triangle^{1-0}0^{00}-10; \oplus 13^{15}-14^{30}$
31	7	0.0	•	$\overset{\bullet}{\nabla}{}^{\circ}14^{36}-15^{02}; \triangle^{0-1}0^{00}-8 \triangle^{\circ}20-24$
Σ	—	74.4	—	UWAGI.

Sierpień - Août

1	7	•	•	$= 4^{20}-10^{30}; \triangle^{0-2}0^{00}-9$
2	7	0.3	•	$= 5^{15}-8^{30}; \triangle^{\circ}5-9, 21-24$
3	6	8.0	•	$\overset{\bullet}{\nabla}{}^{0-1}7^{21}...13^{50}\bullet^{\circ}-14^{33}...15^{12}; = 4^{30}-24; \triangle^{1}-7^{21}$
4	7	2.1	•	$\mathfrak{R}^{\circ}23^{50}-24$ NW-NE; $= 0^{00}-1^{40} \equiv^{2-0}-9^{50} = -13^{15}$
5	7	7.6	•	$\overset{\bullet}{\nabla}{}^{1-0}0^{14-44}\overset{\bullet}{\nabla}{}^{\circ}20^{23}-21^{35}; \mathfrak{R}^{\circ}0^{00-42}$ NW-NE $\mathfrak{R}^{1}20^{14}-21^{45}$ SW-NNE; $= 4^{30}-10^{30}$
6	7	0.0	•	$\overset{\bullet}{\nabla}{}^{\circ}20^{05-12}; = 6^{40}-9^{15}$
7	7	•	•	$\mathfrak{W}16^{15}-17^{30}; = 4^{30}-6^{40}; \triangle^{0-2}2-11$
8	7	•	•	$\triangle^{\circ}21-24$
9	7	•	•	$\triangle^{0-1}0^{00}-10 \triangle^{\circ}20-24$
10	7	•	•	$\triangle^{\circ}0^{00}-9$
11	7	•	•	$= 6^{30}-8^{45}; \triangle^{0-1}2-10 \triangle^{\circ}20-23$
12	7	•	•	$\triangle^{1-2}0^{00}-10 \triangle^{\circ}21-24; \oplus 22^{30}-23^{40}$
13	7	•	•	$= 5^{15}-8^{30}; \triangle^{0-1}0^{00}-10$
14	7	0.0	•	$\overset{\bullet}{\nabla}{}^{\circ}19^{39-48}; = 7^{30}-10^{20}; \triangle^{\circ}3-8, 21-24$
15	7	0.2	•	$\langle 23^{40}-24$ W-NW; $= 2^{30}-9^{40}; \triangle^{0-1}0^{00}-9$
16	6	5.6	•	$\overset{\bullet}{\nabla}{}^{0-1}7^{38}-9^{40}\bullet^{\circ}-a; \langle 0^{00-30}$ W-NW; $= 10^{15}-14^{30}$
17	7	0.0	•	$= 0^{40}-4^{40} \equiv^{0-2}-7^{38} = -11^{15}; \triangle^{\circ}21-24$
18	7	•	•	$\bullet^{\circ}6^{54}-7^{03}; = 3^{15}-11^{15}; \triangle^{0-1}0^{00}-6^{54}$
19	7	1.1	•	$\overset{\bullet}{\nabla}{}^{0-1}10^{46}...16^{05}$
20	7	0.6	•	$\overset{\bullet}{\nabla}{}^{\circ}1^{55}-2^{03}\bullet^{\circ}7^{10}-9^{15}...9^{40}, 13^{05}...14^{40}; = 7^{30}-11^{15}, 13^{45}-15^{10}$
21	7	•	•	$= 1^{15}-11^{20}, 20^{20}-24; \triangle^{\circ}19-23$
22	7	•	•	$= 0^{00}-12^{30}, 21^{15}-22^{45} \equiv^{0-1}-24; \triangle^{0-2}0^{00}-10 \triangle^{\circ}20-23$
23	7	•	•	$\equiv^{1-0}0^{00}-10^{50} = -11^{30}$
24	7	4.4	•	$\bullet^{\circ}9^{38}...12^{42}, 14^{05...40}; = 5^{15}-13^{10}$
25	7	•	•	$\bullet^{\circ}2^{10}-3^{42}, 4^{40-52}; = 2^{40}-10^{10}; \triangle^{\circ}20-24$
26	7	•	•	$= 0^{15}-6^{30}, 7^{15}-9^{20}; \triangle^{0-1}0^{00}-9, 20-24$
27	7	•	•	$\triangle^{1-0}0^{00}-11$
28	7	•	•	
29	7	0.1	•	$\overset{\bullet}{\nabla}{}^{\circ}17^{14}...21^{16}; = 4^{30}-10^{45}; 22^{15}-24; \triangle^{\circ}3-9$
30	7	0.0	•	$\overset{\bullet}{\nabla}{}^{\circ}11^{55}-12^{04}, 13^{42-45}; = 0^{00}-5^{30}; \triangle^{\circ}2-8$
31	7	0.0	•	$\overset{\bullet}{\nabla}{}^{\circ}14^{55}-15^{07}$
Σ	—	30.0	—	UWAGI.

Sandomierz φ = 50°41' λ = 21°45' Wrzesień - Septembre 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	92.6	95.0	98.1	95.2	10.8	15.6	10.0	11.6	17.4	8.5	86	54	84	75	1.8	8.1	1.9	3.9	9	7 ●	1	WNW 3	WNW 6	W 5
2	101.5	101.4	99.5	100.8	8.2	19.3	12.3	13.0	19.8	7.1	90	45	76	70	1.1	12.3	3.4	5.6	0 ⊙	5 ⊙	0	W 1	WSW 5	WSW 1
3	97.7	97.1	95.3	96.7	9.7	23.0	15.4	15.9	24.6	7.6	89	43	76	69	1.2	16.1	4.3	7.2	0	0 ⊙	0	SW 3	W 4	WSW 1
4	94.0	91.4	87.3	90.9	10.8	26.2	19.0	18.8	27.5	8.6	85	38	59	61	2.0	20.9	9.1	10.7	0 ⊙	0 ⊙	0	S 1	S 2	S 1
5	84.4	82.9	85.7	84.3	14.8	26.2	15.9	18.2	26.7	12.0	73	51	96	73	4.5	16.7	0.8	7.3	0 ⊙	8 ⊙	10	S 1	SW 8	WSW 1
6	86.4	86.2	84.2	85.6	11.8	19.4	17.0	16.3	21.6	10.3	95	64	85	81	0.6	8.2	3.0	3.9	9	9	10	SW 4	SW 6	WSW 2
7	79.4	79.4	82.8	80.5	17.7	17.7	15.1	16.4	20.1	15.0	82	90	80	84	3.6	2.0	3.5	3.0	9	10 ●	9	SW 4	SW 3	SW 2
8	87.4	88.3	90.4	88.7	12.4	16.0	11.1	12.6	17.8	11.0	89	69	90	83	1.6	5.6	1.3	2.8	9	9	1	W 2	W 2	WNW 2
9	94.4	97.0	100.4	97.3	9.6	14.2	10.3	11.1	15.1	8.5	88	66	76	77	1.5	5.4	3.0	3.3	6 ⊙	8 ⊙	4	SW 3	WNW 6	WNW 2
10	100.7	98.9	95.8	98.5	6.4	18.2	13.2	12.8	20.0	5.2	97	48	71	72	0.3	10.9	4.5	5.2	3 ⊙	1 ⊙	0	SSW 2	SSW 6	SSW 1
11	93.9	91.4	93.5	92.9	9.4	22.0	15.8	15.8	25.0	7.8	79	53	88	73	2.5	12.4	2.1	5.7	3	9	2	SW 2	SW 6	W 5
12	95.1	91.1	83.3	89.8	11.0	21.9	20.0	18.2	25.0	10.0	96	58	68	74	0.5	11.0	7.4	6.3	1 ⊙	9 ⊙	9	WSW 2	SW 5	SW 2
13	89.3	93.1	95.9	92.8	12.2	15.3	10.2	12.0	20.2	10.2	92	57	73	74	1.2	7.5	3.3	4.0	1	4 ⊙	2	NW 3	WNW 6	W 3
14	98.7	100.5	100.6	99.9	8.6	12.4	6.4	8.4	13.6	6.2	85	53	84	74	1.7	6.7	1.6	3.3	0 ⊙	9	2	W 5	WNW 5	W 2
15	99.9	97.7	95.9	97.2	4.0	17.3	10.2	10.4	18.1	2.6	93	51	88	77	0.5	9.7	1.4	3.9	2 ⊙	3 ⊙	0	W 2	SE 3	SSE 2
16	91.2	89.3	87.8	89.4	7.2	22.9	15.6	15.3	24.1	6.0	84	41	68	64	1.7	16.4	5.7	7.9	0 ⊙	2 ⊙	0	SE 2	SW 3	SW 1
17	87.2	86.3	84.4	86.0	11.3	17.2	14.4	14.3	18.3	10.2	83	79	98	87	2.3	4.1	0.4	2.3	1 ⊙	9	10 ●	SW 2	NNE 2	N' 1
18	84.2	82.8	80.8	82.6	11.4	11.8	11.0	11.3	14.4	10.7	98	100	99	99	0.4	0.0	0.1	0.2	10 ●	10 ●	10	NW 3	N 2	WSW 4
19	87.7	90.9	92.4	90.3	8.3	10.8	7.8	8.7	13.6	7.6	89	69	90	83	1.3	4.0	1.1	2.1	9	10	8	WSW 3	W 5	W 1
20	94.6	95.1	94.7	94.8	5.8	13.0	7.8	8.6	14.4	4.1	97	62	87	82	0.3	5.8	1.4	2.5	9	6 ⊙	0	WSW 2	WSW 5	WSW 2
21	94.7	94.2	93.4	94.1	5.2	11.1	8.4	8.3	13.2	4.1	97	69	89	85	0.2	4.0	1.2	1.8	9	10	10	SW 1	WNW 5	WSW 2
22	92.4	93.4	94.9	93.6	7.4	11.2	8.3	8.8	12.6	6.9	96	75	90	87	0.5	3.3	1.1	1.6	9	9 ●	10	WNW 4	W 5	WNW 4
23	94.3	93.5	93.3	93.7	7.2	8.8	7.5	7.8	10.2	6.7	93	85	99	92	0.8	1.7	0.2	0.9	10	10	10 ●	W 2	WSW 4	W 1
24	96.3	99.1	102.6	99.3	7.8	11.8	7.4	8.6	12.2	7.2	96	76	94	89	0.5	3.3	0.6	1.5	10	9	0	WNW 3	NW 2	N 2
25	105.5	106.2	105.5	105.7	3.8	12.9	8.8	8.6	15.3	2.8	100	79	90	90	0.0	3.1	1.1	1.4	10 ≡	2 ⊙	0	NW 1	NW 1	ESE 1
26	103.5	101.6	99.3	101.5	6.6	15.2	9.2	10.0	16.3	4.7	90	56	79	75	1.0	7.7	2.4	3.7	0	4 ⊙	6	ESE 3	ENE 5	NE 3
27	95.8	94.0	93.1	94.3	8.7	12.8	10.3	10.5	13.1	8.1	92	76	95	88	0.9	3.6	0.6	1.7	10	9	10	NNE 2	E 3	E 1
28	91.5	91.0	90.5	91.0	10.4	12.8	11.3	11.4	13.4	10.0	99	94	98	97	0.2	0.9	0.4	0.5	10	10 ●	10	ENE 1	ENE 1	C 0
29	90.5	91.5	93.0	91.7	8.2	13.4	11.2	11.0	15.4	8.0	100	86	96	94	0.0	2.1	0.5	0.9	10 ≡	6 ⊙	9	C 0	SSW 2	C 0
30	95.6	96.8	96.6	97.0	9.0	15.4	10.7	11.4	16.3	8.5	100	83	99	94	0.0	3.0	0.2	1.1	10 ≡	2 ⊙	0	C 0	N 1	ESE 1
31																								
M	93.3	93.2	93.0	93.2	9.2	16.2	11.7	12.2	17.8	7.9	91	66	86	81	1.2	7.2	2.3	3.6	5.6	6.6	4.8	2.2	4.0	1.9

Październik - Octobre

1	100.1	101.2	102.3	101.2	8.1	15.6	11.4	11.6	18.1	7.8	100	88	96	95	0.0	2.1	0.5	0.9	10 ≡	2 ⊙	1	ESE 1	SE 1	C 0
2	103.3	104.0	103.7	103.7	9.4	19.6	12.6	13.6	20.4	6.8	100	67	87	85	0.0	7.5	1.9	3.1	1 ⊙	3 ⊙	0	C 0	ESE 1	ENE 1
3	103.1	103.1	102.8	103.0	9.6	15.5	11.4	12.0	17.9	9.1	99	84	98	94	0.2	2.8	0.4	1.1	3 ⊙	4 ⊙	0	E 3	ESE 2	SE 2
4	101.6	101.4	100.1	101.0	7.6	18.5	12.0	12.5	18.9	6.9	100	70	98	89	0.0	6.5	0.3	2.3	1 ⊙	2 ⊙	4	SE 1	SE 1	WNW 1
5	99.4	99.7	99.9	99.7	9.4	14.7	10.0	11.0	17.6	8.3	100	86	97	94	0.0	2.4	0.3	0.9	10 ≡	9 ⊙	1	C 0	NE 1	WSW 1
6	100.2	101.4	103.2	101.6	9.6	15.8	11.7	12.2	17.2	8.8	100	80	93	91	0.0	3.5	1.0	1.5	10 ≡	2 ⊙	8	C 0	W 1	W 1
7	105.2	107.3	109.3	107.3	7.4	16.0	11.0	11.4	17.3	7.1	100	69	94	88	0.0	5.6	0.8	2.1	10 ≡	6 ⊙	0	N 5	NE 5	NNW 4
8	111.0	112.2	111.1	111.4	9.0	12.6	8.4	9.6	15.0	7.4	99	95	99	98	0.2	0.7	0.1	0.3	10 ≡	10	0	NNE 5	SE 2	N 1
9	109.9	109.0	107.2	108.7	8.7	12.3	7.8	9.2	14.0	7.2	100	81	99	93	0.0	2.7	0.2	1.0	10 ≡	9	9	NW 1	N 1	NNE 2
10	104.5	103.1	101.2	102.9	7.8	10.6	6.2	7.7	12.1	5.8	94	77	92	88	0.6	2.9	0.7	1.4	10	10	0	NNE 1	E 1	ENE 1
11	98.7	96.7	93.2	96.2	2.8	11.4	8.4	7.8	13.5	2.1	96	76	87	86	0.3	3.3	1.4	1.7	0	1 ⊙	0	ENE 1	SE 3	SW 3
12	91.7	93.8	97.2	94.2	3.8	9.3	4.5	5.5	10.3	2.1	98	87	95	93	0.1	1.6	0.4	0.7	0 ≡	10	2	W 2	N 3	NNW 1
13	98.6	98.0	95.1	97.2	4.8	12.0	7.4	7.9	12.9	3.1	95	64	88	82	0.4	5.1	1.2	2.2	9	3 ⊙	0	ENE 2	ESE 2	SSE 1
14	89.3	87.6	92.5	89.8	2.9	12.0	7.9	7.7	15.3	2.2	98	79	89	89	0.1	3.0	1.2	1.4	10 ≡	8 ⊙	9	C 0	SW 5	WNW 4
15	95.2	99.6	103.1	99.3	7.2	9.3	2.4	5.3	9.7	2.2	96	49	75	73	0.5	6.0	1.8	2.8	10 ●	3 ⊙	0	WNW 3	NNW 4	NNW 1
16	103.0	100.9	99.8	101.2	-2.5	10.1	2.2	3.0	10.4	-5.8	93	59	71	68	0.4	7.6	2.1	3.4	2 ⊙	3 ⊙	0	SE 1	SSW 2	S 1
17	100.0	101.2	100.9	100.7	-3.0	9.2	7.5	5.3	10.0	-3.3	93	65	84	81	0.4	4.1	1.7	2.1	0	10	10	WSW 1	SW 5	W 3
18	98.6	97.1	92.1	95.9	8.2	11.0	9.8	9.7	11.9	6.8	87	74	72	78	1.4	3.4	3.4	2.7	10	10	2	SW 5	WSW 5	SW 6
19	87.5	88.3	90.1	88.6	9.4	14.0	8.9	10.3	14.1	6.5	76	64	75	72	2.8	5.8	2.9	3.8	10	9	9	WSW 7	W 5	W 6
20	90.8	94.8	101.5	95.7	7.8	11.0	5.6	7.5	12.3	4.9	84	48	75	69	1.7	6.9	2.2	3.6	9	8 ⊙	10	WNW 4	NW 7	NW 3
21	106.4	107.2	106.8	106.8	0.9	10.6	5.8	5.8	11.5	0.6	88	48	64	67	0.7	6.7	3.3	3.6	1	1 ⊙	0	NW 5	WNW 2	W 1
22	106.1	105.2	104.3	105.2	-1.5	13.2	4.8	5.3	14.2	-2.1	89	47	90	75	0.6	8.0	0.8	3.1	0 ⊙	0 ⊙	0	WSW 1	SW 1	NNW 1
23	102.3	102.1	100.9	101.8	-1.3	7.6	3.6	3.4	8.8	-1.9	98	80	97	92	0.2	2.0	0.3	0.8	10 ≡	0 ⊙	0	N 1	SW 2	SSE 1
24	99.2	98.2	98.1	98.5	-1.7	10.7	6.0	5.2	14.1	-2.0	96	70	80	82	0.2	3.9	1.9	2.0	10 ≡	0 ⊙	0	C 0	SSE 1	WNW 3
25	98.9	98.7	98.0	98.5	-0.1	4.9	2.8	2.6	6.3	-1.8	98	87	96	94	0.2	1.1	0.3	0.5	10 ≡	10	10 ≡	NW 2	W 1	C 0
26	96.3	95.7	93.7	95.2	-0.1	3.0	5.8	4.1	9.2	-0.6	98	92	89	93	0.2	0.7	1.0	0.6	10 ≡	0 ≡	0	SSE 1	SSW 2	WSW 1
27	90.9	90.6	93.6	91.7	0.3	15.4	6.6	7.3	16.1	-0.3	94	45	85	75	0.3	9.7	1.4	3.8	0 ⊙	1 ⊙	0	S 1	SW 5	N 5
28	90.9	89.1	86.4	88.8	2.8	10.9	6.4	6.6	12.0	2.5	91	61	87	80	0.7	5.0	1.3	2.3	8	9	2	ENE 2	SW 2	C 0
29	86.2	87.5	91.9	88.3	4.6	5.2	4.8	4.8	6.9	3.7	98	97	92	96	0.2	0.2	0.7	0.4	10 ● ≡	10 ≡	10	C 0	N 2	NW 3
30	94.1	94.6	92.2	93.6	4.0	8.0	5.2	4.6	8.3	3.0	92	75	93	87	0.6	2.7	0.5	1.3	10	10	0	WNW 1	W 1	SW 3
31	88.1	87.3	86.4	87.3	3.0	7.3	7.2	6.2	8.4	2.4	96	96	96	96	0.3	0.4	0.5	0.4	10	10	10	SE 1	SE 1	ENE 1
M	98.4	98.6	98.7	98.7	4.5	11.6	7.2	7.6	13.1	3.3	95	72	88	85	0.4	4.0	1.2	1.9	6.9	5.6	3.1	1.8	2.5	2.0

Sandomierz $H_s = 202\,m$ $H_b = 200{,}3\,m$ $h_w = 20{,}1\,m$ Wrzesień - Septembre 1962

DNI	WIDZIALNOŚĆ	OPAD	GRUBOŚĆ LODU	POGODA
1	7	0.1	•	$\overset{\bullet}{\nabla}{}^{\circ}7^{42-52}, 13^{32}...17^{58}$
2	7	•	•	$\triangle^{\circ}21-24$
3	7	•	•	$\triangle^{0-1}0^{00}-10\,\triangle^{\circ}21-24$
4	7	•	•	$=5^{20}-8^{30}; \triangle^{0-1}0^{00}-9$
5	7	1.4	•	$\overset{\bullet}{\nabla}{}^{\circ}16^{25}...21^{50}; \overset{\bullet}{\nabla}{}^{\circ}17^{10-36}$ SW-E; $=20^{45}-24$
6	7	0.0	•	$\bullet^{\circ}11^{01...48}\,\overset{\bullet}{\nabla}\,23^{10-35}; =0^{00}-12^{30}$
7	6	2.6	•	$\overset{\bullet}{\nabla}{}^{\circ}8^{45}-9^{12}\,\bullet^{\circ}10^{28}...11^{30}-14^{20}...15^{35}; =11^{30}-24$
8	7	8.1	•	$\overset{\bullet}{\nabla}{}^{\circ}16^{32}-17^{05}; \overset{\bullet}{\nabla}{}^{\circ}16^{35}-17^{05}$ NW-SE; $=0^{00}-12^{30}, 19^{30}-24; \frown 16^{55}-17^{08}$
9	7	0.2	•	$\overset{\bullet}{\nabla}{}^{\circ}13^{46-56}, 14^{10-17}; =0^{00}-8^{20}; \triangle^{\circ}22-23$
10	7	•	•	$=3^{30}-12^{30}; \triangle^{1-2}0^{00}-10\,\triangle^{\circ}21-24$
11	7	0.7	•	$\overset{\bullet}{\nabla}{}^{\circ}15^{07}...17^{34}; \triangle^{0-1}0^{00}-9$
12	7	0.0	•	$=2^{30}-11^{40}; \oplus 11^{50}-12^{40}; \triangle^{0-1}3-10$
13	7	0.0	•	$\overset{\bullet}{\nabla}{}^{\circ}6^{55}-7^{15}, 8^{50}-9^{02}$
14	7	•	•	$\triangle^{\circ}22-24; \varpi\, 23^{15}-24$
15	7	•	•	$\triangle^{0-1}0^{00}-9\,\triangle^{\circ}21-24; \varpi\, 0^{00}-1^{30}$
16	7	•	•	$\triangle^{\circ}0^{00}-10$
17	7	13.0	•	$\overset{\bullet}{\nabla}{}^{\circ}14^{51}-15^{05}\,\bullet^{0-1}18^{35}...20^{28}-24; =6^{00}-8^{20} \equiv^{0-1}-9^{45} = -12^{15}, 17^{10}-24; \triangle^{\circ}5-8$
18	5	17.8	•	$\bullet^{\circ}0^{00}...4^{10}\,\bullet^{\circ}6^{05}-7^{36}\,\bullet^{\circ}12^{50}...13^{20}\,\bullet^{0-1}-17^{34}\,\bullet 18^{45}...19^{26}\,\bullet^{1-0}-20^{40}; =0^{00}-24$
19	7	•	•	$=0^{00}-8^{30}; \triangle^{\circ}21-23$
20	7	•	•	$=4^{30}-12^{30}, 19^{30}-24; \triangle^{1}0^{00}-11$
21	7	1.5	•	$\overset{\bullet}{\nabla}{}^{\circ}9^{08-18}; =0^{00}-10^{30}; \triangle^{0-1}2-9$
22	7	2.0	•	$\bullet^{\circ}4^{18}-6^{10}...6^{17}\,\overset{\bullet}{\nabla}{}^{\circ}9^{35}...17^{50}\,\bullet^{\circ}19^{35}...20^{20}\,\overset{\bullet}{\nabla}{}^{\circ}20^{45}...23^{15}\,\bullet^{\circ}...24; =0^{30}-12^{30}, 19^{30}-24$
23	7	3.8	•	$\bullet^{\circ}0^{00}-1^{30}\,\overset{\bullet}{\nabla}{}^{\circ}4^{03-12}\,\overset{\bullet}{\nabla}{}^{0-1}12^{44}...19^{05}\,\bullet^{\circ}-23^{40}; =0^{00}-11^{25}, 19^{05}-24$
24	7	0.4	•	$\overset{\bullet}{\nabla}{}^{\circ}15^{36-48}; =0^{00}-9^{30}$
25	7	•	•	$=0^{30}-5^{45} =^{0-2}-11^{50} = -12^{30}, 22^{30}-24; \triangle^{0-1}1-5^{45}\,\triangle^{\circ}19-24$
26	7	•	•	$=0^{00}-9^{15}; \triangle^{0-1}0^{00}-9\,\triangle^{\circ}10-11$
27	7	•	•	$=22^{30}-24$
28	6	0.2	•	$\bullet^{\circ}7^{50}-11^{15}, 12^{20}-13^{05}\,\bullet^{\circ}-14^{20}; =0^{00}-24$
29	6	..	•	$=0^{00}-3^{50} \equiv^{0-2}-11^{20} = -14^{30}, 19^{30}-24; \triangle^{\circ}2-3^{50}, 21-24$
30	5	0.3	•	$=0^{00}-4^{40} \equiv^{0-2}-11^{50} = -22^{45} \equiv^{0-1}-24; \triangle^{0-1}0^{00}-4^{35}$
31				
Σ	—	52.1	—	UWAGI.

Październik - Octobre

1	6	•	•	$\equiv^{2-0}0^{00}-11^{10} = -14^{30}, 17^{30}-24; \triangle^{\circ}18-24$
2	7	0.1	•	$=0^{00}-10^{45}, 23^{30}-24; \triangle^{0-1}0^{00}-11\,\triangle^{\circ}20-24$
3	5	0.1	•	$=0^{00}-7^{45} \equiv^{0-1}-10^{50} = -13^{30}, 20^{45}-24; \triangle^{\circ}0^{00}-1, 20-22$
4	7	•	•	$=0^{00}-11^{30}, 20^{20}-24; \triangle^{1-2}0^{00}-10\,\triangle^{\circ}22-24$
5	6	0.2	•	$=0^{00}-6^{30} \equiv^{1-0}-11^{35} = -21^{45} \equiv^{0-1}-24; \triangle^{0-2}0^{00}-6^{30}\,\triangle^{0-1}19-21^{45}$
6	6	•	•	$\equiv^{0-2}0^{00}-9^{45} = -24; \triangle^{\circ}20-23$
7	6	0.0	•	$=0^{00}-4^{45} \equiv^{0-1}-7^{30} = -13^{40}, 21^{30}-24; \triangle^{1}0^{00}-4^{45}\,\triangle^{\circ}23-24$
8	6	•	•	$=0^{00}-1^{40} \equiv^{0-1}-10^{35} = -24; \triangle^{\circ}0^{00}-1^{40}, 22-23$
9	6	•	•	$=0^{00}-5^{40} \equiv^{0-2}-7^{50} = -24; \triangle^{1-2}0^{00}-5^{40}\,\triangle^{\circ}21-24$
10	6	•	•	$=0^{00}-24; \triangle^{\circ}0^{00}-10\,\triangle^{0-1}19-24$
11	7	•	•	$=0^{00}-11^{30}, 16^{45}-24; \triangle^{1-2}0^{00}-10\,\triangle^{0-1}19-24$
12	6	•	•	$=0^{00}-5^{45} \equiv^{0-1}-6^{45} = -24; \triangle^{1-2}0^{00}-5^{45}\,\triangle^{0-2}20-24$
13	6	•	•	$=0^{00}-24; \triangle^{1}0^{00}-8$
14	6	0.8	•	$=0^{00}-4^{40} \equiv^{0-2}-9^{30} = -24; \triangle^{1}0^{00}-4^{40}$
15	7	0.0	•	$\bullet^{1-0}4^{36}...5^{05}-7^{05}...7^{20}; =0^{00}-10^{30}; \triangle^{0-1}20-24$
16	7	•	•	$=5^{30}-10^{15}; \sqcup^{0-1}1-9$
17	6	•	•	$=6^{50}-24; \sqcup^{0-1}1-10$
18	6	•	•	$=0^{00}-24$
19	7	0.1	•	$\bullet^{\circ}6^{58}-8^{20}\,\bullet^{\circ}9^{10-40}; =0^{00}-12^{20}$
20	7	0.0	•	$\bullet^{\circ}3^{15...35}, 4^{45}...5^{25}\,\overset{\bullet}{\nabla}{}^{\circ}13^{50-55}; =3^{15}-6^{10}$
21	7	•	•	$\sqcup 4-7$
22	7	•	•	$=20^{20}-24; \sqcup^{\circ}3-8\,\triangle^{\circ}23-24; \varpi\, 3^{20}-5^{10}$
23	6	•	•	$=0^{00}-2^{45} \equiv^{0-2}-11^{45} = -24; \triangle^{\circ}0^{00}-2^{45}\,\sqcup^{1}5-9\,\triangle^{0-1}20-24$
24	6	•	•	$=0^{00}-1^{45} \equiv^{0-2}-10^{45} = -24; \sqcup^{1}1-9$
25	5	0.3	•	$=0^{00}-2^{50} \equiv^{0-2}-10^{40} = -17^{50} \equiv^{2-0}-24; \sqcup^{0-1}2-8$
26	3	•	•	$\equiv^{2-0}0^{00}-12^{50} = -24; \triangle^{\circ}21-23$
27	7	•	•	$=0^{00}-9^{30}, 20^{15}-24; \sqcup^{0-1}1-8$
28	7	0.0	•	$=0^{00}-13^{15}, 19^{30}-24; \triangle^{0-1}3-8; \oplus 8^{30}-11^{40}$
29	3	0.3	•	$\bullet^{\circ}6^{18}-11^{42}; =0^{00}-3^{45} \equiv^{1-0}-13^{20} = -24; \triangle^{\circ}23-24$
30	6	•	•	$=na, 8^{20}-24; \triangle^{\circ}0^{00}-9, 23-24$
31	6	0.7	•	$\bullet^{\circ}8^{35}-9^{20}...10^{30}\,\bullet^{\circ}10^{45}-11^{35}, 12^{30}-13^{20}; =0^{00}-24; \triangle^{\circ}0^{00}-8^{30}$
Σ	—	2.6	—	UWAGI.

Sandomierz φ=50°41' λ=21°45' Listopad - Novembre 1962

DNI	CISNIENIE P=900+ I	II	III	Dies	TEMPERATURA t I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI d I	II	III	Dies	ZACHMURZENIE N.w I	II	III	POGODA	KIERUNEK I PRĘDKOŚĆ WIATRU D.v I	II	III
1	83.4	82.4	83.3	83.0	9.4	14.7	11.2	11.6	16.1	7.1	99	76	91	89	0.2	4.0	1.2	1.8	10	8 ⊘	2		ESE 5	E 4	SE 1
2	87.0	89.5	92.1	89.5	6.8	10.0	9.6	9.0	11.2	5.9	100	93	96	96	0.0	0.8	0.5	0.4	10 ≡	10	7		W 2	W 1	C 0
3	93.0	92.8	93.9	93.2	7.6	11.6	11.4	10.5	12.6	7.4	100	90	94	95	0.0	1.3	0.9	0.7	10 ≡	10	7		C 0	NE 3	ENE 1
4	95.2	95.3	95.6	95.4	8.7	12.6	10.1	10.4	13.2	7.6	100	82	92	91	0.0	2.6	1.0	1.2	10 ≡	9	10		SE 1	SSE 3	SE 4
5	94.8	94.1	93.6	94.2	8.2	10.4	6.2	7.8	11.5	6.1	96	86	72	85	0.5	1.8	2.7	1.7	10	8 ⊙	0		SE 5	SE 5	ESE 4
6	92.0	92.1	94.5	92.9	2.0	10.0	6.3	6.2	10.5	1.4	76	47	63	62	1.7	6.6	3.5	3.9	1 ⊙	6 ⊙	9		SE 6	SE 6	SE 5
7	96.5	97.8	99.2	97.8	3.8	8.6	6.8	6.5	10.5	3.5	82	70	74	75	1.5	3.3	2.6	2.5	10	9	9		ESE 5	E 3	E 5
8	97.4	95.7	94.7	95.9	5.4	12.8	6.1	7.6	13.5	4.5	83	58	70	70	1.6	6.2	2.8	3.5	8	1 ⊙	1		E 3	SE 6	ESE 4
9	92.1	91.2	91.6	91.6	1.6	10.6	4.2	5.2	11.6	1.6	93	62	84	80	0.6	4.9	1.3	2.3	6	6 ⊙	10		E 5	ESE 3	E 4
10	90.6	90.9	92.9	91.5	4.7	2.6	1.1	2.4	5.5	1.0	70	82	94	82	2.5	1.3	0.4	1.4	10	10	10 ●		NE 7	NE 7	NE 6
11	94.7	95.7	96.1	95.5	0.8	2.4	3.4	2.5	3.4	-0.1	96	89	91	92	0.3	0.8	0.7	0.6	10	10	10		ENE 3	E 5	E 6
12	94.4	93.2	94.3	94.0	2.2	2.8	3.8	3.2	3.8	1.8	93	91	86	91	0.6	0.7	0.9	0.7	10 ●	10	10		E 8	E 5	ESE 3
13	96.8	96.8	96.1	96.6	-3.2	5.0	4.2	4.2	5.5	3.0	97	94	92	94	0.3	0.5	0.6	0.5	10	10	10		SE 1	ESE 4	SE 4
14	94.6	94.4	93.4	94.1	2.8	4.4	5.5	4.6	5.6	2.5	96	97	98	97	0.3	0.3	0.1	0.2	10	10 ≡	10 ●		E 1	E 1	C 0
15	91.9	88.4	81.5	87.3	5.0	7.4	6.5	6.4	8.1	4.5	98	87	97	94	0.1	1.3	0.3	0.6	10	10	10 ●		SE 1	SW 1	SSE 3
16	83.2	84.0	87.4	84.9	0.5	2.7	1.7	1.6	6.5	0.3	96	81	83	87	0.2	1.4	1.1	0.9	10 *	10	10		WNW 4	WNW 4	NW 3
17	91.0	92.1	91.6	91.6	-0.5	1.2	-1.3	-0.5	2.0	-1.7	88	70	91	83	0.7	2.0	0.5	1.1	1	8 ⊙	10		SW 2	WSW 2	S 2
18	86.6	84.6	81.9	84.4	-1.5	4.2	1.4	1.4	5.1	-2.3	86	68	91	82	0.8	2.6	0.7	1.4	6	4 ⊙	10		SE 3	SE 6	ESE 5
19	79.7	83.6	81.6	81.6	4.4	10.4	6.4	6.9	10.6	1.1	90	62	95	82	0.9	4.8	0.4	2.0	8	2 ⊙	10		SE 3	SW 6	E 4
20	80.9	78.6	82.4	80.6	8.0	9.3	3.5	6.1	9.5	3.1	87	85	91	88	1.3	1.7	0.6	1.2	10	10	10 ●		S 2	ESE 2	W 4
21	87.6	87.6	86.2	87.1	1.2	1.2	1.2	1.2	3.6	0.6	90	90	94	91	0.7	0.7	0.4	0.6	10	10	10		NW 3	N 3	NNE 2
22	85.3	87.6	93.4	88.8	1.4	4.2	1.1	2.0	5.0	0.8	98	80	94	91	0.2	1.6	0.4	0.7	10 ●	4 ⊙	9		C 0	SW 2	WSW 2
23	96.0	97.7	99.2	97.6	0.8	0.9	-0.9	0.0	1.5	-1.1	96	92	95	94	0.3	0.5	0.3	0.4	10 ●	10	10 *		NW 4	NW 5	N 2
24	101.4	102.6	105.2	103.1	-0.6	-0.2	-0.2	-0.3	0.2	-1.1	91	90	96	92	0.5	0.6	0.2	0.4	10	10	10		N 3	NNE 3	N 2
25	105.8	104.5	103.5	104.6	-0.1	1.2	1.6	1.1	1.8	-0.8	96	98	98	97	0.3	0.2	0.2	0.2	10	10	10 ● ≡		N 1	N 4	NNE 5
26	104.3	105.3	105.6	105.1	2.4	2.8	3.4	3.0	3.5	1.3	96	96	97	96	0.3	0.3	0.3	0.3	10 ●	10	10 ●		N 5	N 3	N 4
27	106.7	107.7	106.8	107.1	0.7	1.4	1.9	1.5	3.6	0.4	98	98	96	97	0.1	0.2	0.3	0.2	10	10 ≡	10		NNW 5	NW 1	WNW 2
28	102.5	101.4	100.9	101.6	-0.2	2.0	1.0	1.0	2.5	-0.6	96	76	92	88	0.2	1.7	0.5	0.8	10	10	10		SW 2	WSW 6	SW 5
29	99.5	99.1	96.9	98.5	1.3	3.0	2.4	2.3	3.2	0.8	92	90	93	92	0.5	0.8	0.6	0.6	10	10	10		WSW 5	WSW 4	SW 6
30	91.5	91.0	92.1	91.5	3.2	3.4	3.0	3.2	3.9	2.2	81	88	90	86	1.5	0.9	0.8	1.1	10	10	7		SW 9	WSW 8	W 4
31																									
M	93.2	93.3	93.6	93.4	3.1	5.8	4.1	4.3	6.8	2.0	92	82	90	88	0.6	1.9	0.9	1.1	9.0	8.5	8.7		3.5	3.9	3.4

Grudzień - Décembre

1	101.7	107.8	112.4	107.3	-1.1	-0.9	-0.4	-0.7	3.1	-2.7	79	69	84	77	1.2	1.8	0.9	1.3	4	6 ⊘	8		N 6	N 5	NW 3
2	117.6	119.3	119.0	118.6	-3.1	0.0	-3.9	-2.7	0.3	-4.2	86	73	88	82	0.7	1.7	0.6	1.0	1	3 ⊙	0		NNE 2	W 4	W 2
3	115.1	113.2	110.1	112.8	-6.9	-2.4	-4.9	-4.8	-1.1	-7.3	88	85	95	89	0.4	0.8	0.2	0.5	0	0	10		C 0	SW 2	WSW 4
4	105.0	102.6	99.7	102.4	-6.5	-1.7	-1.5	-2.8	0.1	-7.1	91	84	64	80	0.3	0.9	2.0	1.1	10 ≡	3 ⊙	2		SW 5	SW 5	WSW 5
5	97.6	100.2	104.1	100.6	-1.1	0.0	0.6	0.0	0.8	-2.5	59	92	96	82	2.3	0.5	0.3	1.0	3	10	10 ●		WSW 4	WNW 4	WNW 2
6	105.6	106.0	105.5	105.7	0.4	2.4	0.8	1.1	2.6	-0.1	96	93	96	95	0.3	0.6	0.3	0.4	10	10	10		C 0	WSW 1	SW 1
7	102.8	102.5	103.1	102.8	-0.3	0.7	-1.3	-0.6	1.3	-1.6	98	94	98	97	0.2	0.4	0.2	0.3	10 ≡	10	10 ≡		WSW 4	WSW 6	WSW 3
8	105.1	106.9	106.2	106.1	-4.3	-2.2	-5.6	-3.4	-1.2	-4.8	89	94	94	92	0.5	0.3	0.3	0.4	0	10	10 ≡		SW 2	WSW 1	SW 1
9	98.4	91.6	84.2	91.4	-5.3	1.2	-0.7	-1.4	1.6	-5.6	90	77	64	77	0.4	1.5	2.1	1.3	2	5	9		SW 1	SSW 5	SSW 7
10	81.9	82.1	81.9	82.0	-1.9	0.2	-2.9	-1.9	0.6	-3.3	79	73	79	77	1.1	1.7	1.0	1.3	10	8 ⊙	8		SW 7	SW 6	SSW 3
11	82.5	83.0	82.9	82.8	0.2	2.0	0.6	0.8	2.2	-3.9	96	89	92	92	0.3	0.8	0.5	0.5	10	10	10		SW 3	WSW 6	SW 4
12	77.8	76.5	76.7	77.0	-0.5	2.2	-0.7	0.1	2.7	-1.7	79	64	73	72	1.2	2.6	1.5	1.8	8	8 ⊘	2		SSW 7	SSW 7	SSW 4
13	76.9	76.7	76.7	76.8	0.0	3.2	1.9	1.8	3.9	-2.1	72	51	60	61	1.7	3.6	2.8	2.8	10	10	1		S 3	S 3	S 4
14	76.7	79.3	80.8	78.9	-0.1	0.8	0.3	0.3	2.0	-1.5	90	96	98	95	0.7	0.3	0.1	0.4	10 ●	10	10 *		S 2	WSW 1	WNW 4
15	76.7	67.8	62.6	69.0	-2.9	-0.4	-0.5	-1.1	0.6	-4.4	91	80	96	89	0.4	1.2	0.3	0.6	8	10 *	10 *		WSW 2	SSW 3	SW 7
16	54.0	50.7	54.0	52.9	-1.5	0.4	0.9	0.2	1.4	-2.1	84	100	94	93	0.9	0.0	0.4	0.4	10	10	10 ●		WSW 3	SSW 3	SW 2
17	61.1	68.2	72.6	67.3	-0.5	-0.4	-0.1	-0.3	1.3	-1.0	90	88	100	93	0.6	0.7	0.0	0.4	10	10	10		WNW 6	WNW 2	W 1
18	74.0	72.0	76.1	74.0	-0.9	-0.2	-3.2	-1.9	0.2	-5.9	89	94	88	90	0.6	0.4	0.6	0.5	10	10 *	9		W 2	SW 3	NW 2
19	78.4	80.7	86.5	81.9	-5.1	-5.8	-8.8	-7.1	-2.9	-8.9	95	84	89	89	0.3	0.6	0.4	0.4	10 *	8	0		NW 1	N 1	N 2
20	92.7	94.9	98.3	95.3	-7.9	-8.6	-10.3	-9.3	-6.1	-11.7	90	80	81	84	0.3	0.6	0.5	0.5	10	10	10		N 5	N 3	N 1
21	96.1	94.7	96.0	95.6	-16.1	-14.7	-17.5	-16.4	-9.9	-17.7	86	78	85	83	0.2	0.4	0.2	0.3	1	0 ⊙	0		NNW 2	N 1	NE 1
22	101.1	104.6	109.5	105.1	-14.7	-13.1	-15.3	-14.6	-12.7	-21.1	82	84	82	83	0.3	0.4	0.3	0.3	10	9 *	8 *		N 2	N 6	NNE 5
23	112.5	114.3	116.4	114.4	-13.6	-11.7	-12.3	-12.5	-11.3	-17.3	71	78	78	76	0.6	0.5	0.5	0.5	10	8 ⊙	3		NE 8	NE 7	NE 9
24	115.7	115.0	115.3	115.3	-13.5	-9.3	-10.0	-10.7	-8.9	-13.9	84	76	78	79	0.4	0.7	0.6	0.6	9 *	9	10		NE 8	NE 6	NE 3
25	111.3	107.7	102.4	107.1	-11.7	-9.5	-13.5	-12.0	-8.9	-14.1	82	79	84	82	0.4	0.6	0.4	0.5	7	9	4		E 2	ENE 5	E 4
26	94.5	91.9	89.9	92.1	-13.5	-10.9	-11.3	-11.8	-10.5	-14.0	84	73	79	79	0.4	0.7	0.5	0.5	8	7	10		E 3	S 1	S 1
27	87.8	86.6	87.2	87.2	-9.9	-7.4	-7.5	-8.1	-6.8	-11.5	88	82	87	86	0.4	0.6	0.4	0.5	10 *	0	10		S 1	S 2	ESE 2
28	88.7	90.3	91.7	90.2	-7.9	-6.9	-10.1	-8.8	-6.5	-10.4	87	80	84	84	0.4	0.7	0.4	0.5	10	9	0		S 1	S 1	SSW 1
29	90.1	87.9	84.4	87.5	-14.0	-5.3	-2.3	-6.0	-2.3	-14.4	83	82	70	78	0.3	0.7	1.6	0.9	0	1 ⊙	10		SE 3	SE 2	S 3
30	85.3	86.5	88.6	86.8	-3.3	-5.5	-6.0	-5.2	-2.0	-6.2	79	83	89	84	1.0	0.6	0.4	0.7	10	10	10		NW 3	N 4	NNE 4
31	90.6	92.7	95.8	93.0	-8.4	-9.6	-13.3	-11.2	-5.9	-13.4	83	78	76	79	0.5	0.6	0.5	0.5	10	10	10		NE 8	NE 7	NE 7
M	92.1	92.1	92.6	92.3	-5.7	-5.7	-5.1	-4.9	-2.3	-7.6	85	82	84	84	0.6	0.9	0.7	0.7	7.5	7.5	7.2		3.4	3.6	3.3

Sandomierz $H_s = 202m$ $H_t = 200{,}3m$ $h_w = 20{,}1m$ Listopad - Novembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU A	POGODA
1	6	0.2	•	•°6^15-25; = 0^00-12^45
2	6	•	•	= 0^00-3^40 ≡°-2 -10^35 = -24
3	6	0.3	•	= 0^00-4^45 ≡2-0 -9^40 = -22^50 ≡°-2 -24
4	7	•	•	•4^40-6^10; ≡2-0 0^00-7^40 = -12^15, 21^30-24
5	6	•	•	= 0^00-18^30
6	7	•	•	⊔ 5-9; ⊠ 17^50-18^20
7	7	0.0	•	•°6^49 ... 7^18, 9^20 ... 11^10
8	7	•	•	
9	7	•	•	= 3^30-10^15
10	7	3.4	•	•°19^40-22^35 *°-24; = 3^30-8^30, 13^15-24
11	6	1.4	2	*°0^00-2^15 3^30 ... 4^40 •°7^35-8^50, 14^47-15^20; = 0^00-24
12	6	1.4	•	•°3^40 ... 4^15-7^40, 9^45 ... 10^30-11^05 ... 12^10; •°22^50-24 = 0^00-14^10, 15^30-16^20, 21^45-24
13	6	3.9	•	•0^00-2^25 •°13^25 ... 18^40 •1-0 21^05 ... 23^40; = 0^00-8^30 ≡1-0 -11^15 = -24
14	3	3.8	•	•°0^00 ... 1^25 •°-1 15^40-19^35 •°-21^20 ... 22^10; = 0^00-8^15 ≡°-1 -12^50 = -24
15	6	18.0	•	•°13^48 ... 14^05-24; = 0^00-6^50 ≡°-1 -8^40 = -24
16	6	0.3	•	•°0^00-4^15 •'-6^10 *'-6^20 *°-7^40 •°-8^35; = 0^00-24
17	7	•	•	= 0^00-10^20, ⊔°3-9, 23-24
18	7	0.0	•	•°21^50 ... 22^10; = 21^30-24; ⊔°0^00-9; ⊠ 3^40-5^10 ⊠ 5^50-6
19	7	3.1	•	•°17^10-19^30 ... 20^10; = 0^00-2^20
20	7	1.1	•	•°16^15-17^35 •°-18^40 •°19^35-20^20 ... 20^45 •°23^45 ... 24; = 15^30-18^45; ⊠ 4^20-5^50
21	6	0.2	•	•°0^00 ... 1^15; = 0^30-24
22	6	0.0	•	•°0^50 ... 2^15-3^30 ... 4^10, 6^20 ... 7^35; = 0^00-24; ⊔°22-24
23	6	4.2	•	•°1^40-4^20 ... 6^15-7^35 *•°-8^20 •°-11^40 *°14^05-23^20; = 0^00-24, ⊔°0^00-1^40
24	6	0.0	3	*°1^15-2^45 8^40 ... 9^30; = 0^00-24
25	5	6.7	2	•°6^50-8^40 13^20-14^15 •°15^20-17^30 19^15-21^40 •°-22^30 •°-23^35 ... 24; = 0^00-15^50 ≡°-1 -22^50 = -24
26	5	6.9	•	•°0^00 ... 1^20 •°-4^15 •°-5^30 ... 7^25 •°... 8^40 •°18^25-24; = 0^00-12^45 ≡°-2 -19^35 = -24
27	2	0.0	•	•°0^00-1^28 •°1^34-3^35 •°-4^25 •°4^40 ... 10^30; = 0^00-10^50 ≡°-2 -19^30 = 24
28	7	•	•	= 0^00-11^10, 13^30-24
29	6	0.0	•	•°7^50-9^15 ... 9^45 •°15^50 ... 16^15; = 0^00-24
30	6	1.3	•	•°7^48 ... 8^30-9^35 ... 11^05, 17^55-18^35; = 0^00-24
31				
Σ	—	56.2	—	UWAGI

Grudzień - Décembre

1	7	0.0	•	•°2^45-3^22 △°17^45-18^30, 18^35-19^05; = 0^00-4^15
2	7	•	•	⊔°1-11, 17-24
3	6	•	•	≡'8^50-10^40 ≡°-11^10 = -24; ⊔°0^00-24
4	6	•	•	= 0^00-1^17 ≡°-6^50 = -24; ⊔°0^00-12 ∨°1^25-12
5	6	0.0	•	•°19^15-22^20 ... 23^10; = 0^00-6^15, 9^30-24
6	5	0.3	•	•°2^40-3^25 •°8^50 ... 9^35; = 0^00-7^20 ≡1-0 -10^50 = -24
7	5	•	•	= 0^00-5^45 ≡°-1 -11^20 = -15^30 ≡2-0 -20^50 = -24; ⊔°23-24
8	5	•	•	= 0^00-8^50 ≡°-10^48 = -13^50 ≡°-15^40 ≡'-24; ⊔°0^00-24
9	6	•	•	≡1-0 0^00-6^20 = -13^30 ⊔°0^00-2 ∨°2^50-12^00; ⊠ 16^00-18^00
10	7	•	•	⊠ 19^15-21^10
11	6	0.1	•	•°12^48 ... 13^15-14^10 ... 16^40; = 12^20-24
12	7	•	•	= 0^00-9^30; ⊔°22-24
13	7	0.0	•	= 5^30-7^20; ⊔°0^00-7
14	5	5.0	•	•°4^55 ... 7^20 *°7^30 ... 9^15, 9^17-10^40 •°11^45 ... 12^20 *°12^40-13^10 *°13^12-15 •°-13^50, 14^40 ... 15^10 *°15^20-20^35 ... 21^10; = na-np
15	6	1.9	4	*°12^30-14^45 *°-1 17^45-21^45; = 12^30-24
16	6	3.9	10	*°7^40-12^20 •°14^04-25 •°15^15-17^07 •°18^35-24; = 0^00-6^15 = 8^10-14^10 ≡°... 15^50 = -24; ⊠ 2^30-3^37
17	7	0.6	8	•°0^00-3^20 △°10^50-12^15 *°12^58-15^40, 17^15 ... 19^10; = 0^00-8^30, 13^05-24
18	5	4.1	10	*°2^46-3^30 *°-1 8^40-12^42 *°21^45 ... 22^30-23^25 ... 24; = 0^00-24
19	6	0.0	16	*°0^00 ... 1^0, 3^45 ... 4^15-5^25 ... 7^40, 13^58 ... 15^09; = 0^00-24
20	6	0.5	15	*°8^10-10^55; = 0^00-24
21	6	•	16	= 0^00-13^30, 15^40-24
22	6	0.5	16	*°8^35 ... 12^40, 15^40-20^40 ↔ -23^30 *°... 24; = 0^00-24
23	7	0.0	15	*°0^00 ... 1^40; ⊠ 18^40-20^20; = 0^00-3^10
24	7	0.0	15	*°5^40 ... 7^20
25	7	•	15	
26	6	0.5	14	*°7^40-8^20 ... 9^40 23^35 ... 24; = 1^50-12^48, 16^15-24
27	6	0.1	16	*°0^00-8^10-10^35; = 0^00-24
28	6	0.1	16	*°6^45 ... 7^20-8^50 *'-9^15 *°... 11^40; = 0^00-24
29	6	•	17	= 0^00-20^30; ⊔°4-12
30	6	•	16	= 8^30-24
31	6	•	15	= 0^00-24
Σ	—	17.4	—	UWAGI.

Kraków, Obserw. Astr. UJ φ = 50°04' λ = 19°58' Styczeń – Janvier 1962

DNI	CIŚNIENIE P+900 I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	82.3	84.9	84.9	84.0	-0.3	6.0	3.0	2.9	6.2	-4.0	98	60	71	76	0.2	3.8	2.2	2.1	10 ≡	10	10	SW 1	WSW 3	WSW 2
2	84.1	85.1	88.9	86.0	1.3	0.9	-0.3	0.4	3.0	-0.3	74	77	78	76	1.8	1.5	1.4	1.6	10	10	10	C 0	W 1	W 4
3	93.6	94.6	97.8	95.3	-5.3	-2.1	-1.2	-2.0	0.0	-4.1	70	72	97	80	1.5	1.4	0.2	1.0	8	5 ⊙	10 ≡	W 5	SW 6	SW 2
4	100.3	98.8	98.1	99.1	-0.9	1.2	-3.2	-1.5	2.6	-4.4	97	75	97	90	0.2	1.7	0.1	0.7	10	2 ⊙	0	C 0	SE 1	SW 2
5	97.0	95.3	92.3	94.9	-6.1	-0.4	-5.3	-4.3	0.1	-6.4	94	76	98	89	0.2	1.4	0.1	0.6	3	8 ⊙ ≡	0 ≡	WSW 2	SW 2	C 0
6	90.5	88.4	86.9	88.6	-5.3	-0.6	-0.1	-1.5	0.6	-7.5	93	77	90	87	0.3	1.3	0.7	0.8	0 ≡	3 ⊙	10	WSW 1	WSW 3	WSW 8
7	90.2	94.1	99.4	94.6	0.7	1.9	0.7	1.0	2.1	-0.2	96	96	90	94	0.2	0.3	0.6	0.4	10 ✳	10 ✳	10	WSW 3	SW 2	W 2
8	100.9	101.3	99.7	100.6	-1.7	2.3	1.6	1.0	2.7	-2.5	90	68	80	79	0.6	2.3	1.4	1.4	10 ≡	9	10	C 0	SSW 4	SW 2
9	96.4	94.4	92.2	94.3	-4.7	0.2	-4.1	-3.2	2.2	-4.7	98	81	87	89	0.1	1.2	0.6	0.6	10 ≡	0 ⊙	2 ≡	C 0	C 0	SW 1
10	87.8	85.0	83.0	85.3	-7.7	-2.1	-1.6	-3.2	-1.1	-8.6	99	85	98	94	0.0	0.7	0.1	0.3	10 ≡	8 ≡	8 ≡	SW 1	NNW 1	ESE 1
11	84.2	81.6	79.5	81.9	-4.0	9.2	2.8	2.7	9.2	-4.5	89	47	84	73	0.5	6.1	1.2	2.6	1 ≡	5 ⊙	10 ≡	C 0	S 2	S 1
12	80.7	80.0	74.8	78.5	2.4	4.5	0.4	1.9	4.7	0.4	100	93	100	98	0.0	0.5	0.0	0.2	10 ● ≡	10	0 ≡	C 0	C 0	C 0
13	67.3	69.6	72.2	69.7	2.9	6.0	4.7	4.6	6.5	0.4	93	67	71	77	0.5	3.1	2.4	2.0	10 ●	7 ⊙	9	C 0	SW 2	S 2
14	75.3	78.0	81.9	78.4	2.7	4.8	2.5	3.1	5.1	1.9	91	59	67	72	0.6	3.5	2.4	2.2	10	2 ⊙	7	W 3	WSW 8	S 1
15	86.2	89.2	94.1	89.8	0.7	3.9	1.3	1.8	4.7	-0.1	77	59	74	70	1.5	3.3	1.8	2.2	2	8	7	SW 2	SW 4	SW 2
16	96.5	96.4	94.4	95.8	-2.8	5.3	-1.1	0.1	5.8	-2.9	93	43	85	74	0.4	5.1	0.8	2.1	2 ≡	3 ⊙	3 ≡	C 0	SW 3	SE 1
17	92.6	92.7	92.5	92.6	-3.0	4.9	-0.7	0.4	5.4	-3.0	89	46	92	76	0.6	4.7	0.5	1.9	5 ≡	4 ⊙	8	C 0	SW 2	SW 2
18	90.7	90.1	90.7	90.5	-3.4	0.8	-1.1	-1.2	1.6	-4.0	97	85	93	92	0.2	1.0	0.4	0.5	5 ≡	9 ≡	9 ≡	C 0	SW 1	SW 1
19	91.3	91.9	90.6	91.3	-2.3	2.5	1.9	1.0	3.6	-2.9	96	77	91	88	0.3	1.7	0.6	0.9	3 ≡	10 ≡ ⊙	7 ≡	C 0	SW 1	SW 3
20	90.5	92.4	96.2	93.0	4.9	8.7	5.8	6.3	8.8	0.6	82	64	83	76	1.6	4.0	1.5	2.4	10	7 ⊙	9	SW 3	SW 7	W 3
21	95.4	94.8	93.7	94.6	3.1	8.5	5.2	5.5	9.2	1.4	86	74	97	86	1.0	2.9	0.2	1.4	10	9 ⊙	10	WSW 1	SW 3	SW 3
22	87.6	83.5	86.1	85.7	1.6	10.4	7.0	6.5	11.1	1.0	100	59	59	73	0.0	5.1	4.1	3.1	7 ≡	7 ⊙	10	C 0	C 0	SW 6
23	89.1	90.3	92.8	90.7	2.2	6.4	2.7	3.5	7.1	1.2	75	52	70	66	1.8	4.6	2.2	2.9	3 ≡	2 ⊙	10	C 0	SW 6	SW 2
24	93.2	91.4	89.3	91.3	2.0	5.5	2.6	3.2	6.3	0.9	78	53	82	71	1.6	4.2	1.3	2.4	8	3 ⊙	10 ☂	WSW 2	SW 5	SW 1
25	85.3	83.1	82.9	83.8	3.7	6.0	5.9	5.4	7.8	2.1	98	91	83	91	0.2	0.9	1.6	0.9	10 ●	10 ≡	10 ☂	SW 1	SW 1	WSW 2
26	85.0	90.3	89.8	88.4	5.0	2.3	1.2	2.4	7.1	1.1	87	80	90	86	1.1	1.4	0.7	1.1	10	10	8	NW 5	NW 4	C 0
27	86.3	87.9	88.6	87.6	0.6	3.1	2.1	2.0	3.5	0.0	100	84	85	90	0.0	1.2	1.0	0.7	10 ✳ ≡	10 ☂	9	C 0	WSW 6	WSW 5
28	86.3	84.5	87.3	86.2	1.4	2.8	-3.0	-0.4	2.9	-3.1	85	69	90	81	1.0	2.4	0.5	1.3	10 ✳	8	8	WNW 6	W 4	WSW 6
29	91.3	94.5	98.9	94.9	-7.0	-7.0	-8.1	-7.6	-2.8	-8.1	91	88	92	90	0.3	0.4	0.2	0.3	10 ✳	10 ✳	10 ✳	NNW 4	NNW 6	NNW 3
30	101.6	104.4	107.8	104.6	-7.2	-5.5	-11.3	-8.8	-4.2	-11.3	96	92	90	93	0.1	0.3	0.3	0.2	10 ✳ ≡	10	4	C 0	NNE 5	NNE 4
31	107.5	106.1	102.0	105.2	-14.2	-12.5	-9.9	-11.6	-9.8	-14.2	87	81	84	84	0.3	0.4	0.4	0.4	10 ≡	10 ✳	10	NNE 3	NNE 4	NE 5
M	89.9	90.1	90.6	90.2	-1.2	2.5	0.0	0.3	3.6	-2.8	90	72	85	82	0.6	2.3	1.0	1.3	7.6	7.1	7.7	1.4	3.1	2.5

Luty – Février

1	92.4	91.0	90.1	91.2	-9.2	-7.2	-8.7	-8.4	-6.5	-9.9	92	90	92	91	0.3	0.3	0.3	0.3	10	4 ⊙	10	ENE 3	E 1	C 0
2	90.2	91.5	93.5	91.7	-6.4	-1.7	-8.5	-6.3	-1.4	-9.2	91	86	92	90	0.3	0.8	0.3	0.5	10 ≡	9 ⊙	8	S 1	C 0	C 0
3	95.9	97.2	97.9	97.0	-10.8	-5.4	-3.5	-5.8	-3.3	-11.5	97	85	94	92	0.1	0.6	0.3	0.3	10 ≡	10 ⊙ ≡	10	C 0	W 1	WSW 1
4	95.6	91.6	94.2	93.8	-3.6	0.6	-0.3	-0.9	1.0	-4.6	94	82	100	92	0.3	1.2	0.0	0.5	10 ≡	10 ⊙	10	WSW 1	WSW 1	WSW 3
5	92.5	83.3	81.0	85.6	-1.5	2.5	3.3	1.9	3.8	-2.1	92	60	79	77	0.4	2.9	1.5	1.6	9 ≡	10	9	C 0	SSE 3	WSW 2
6	87.7	89.9	93.1	90.2	1.6	2.1	2.1	2.0	3.8	0.5	83	84	78	82	1.2	1.2	1.5	1.3	10 ✳	10 ✳ ⊙	9	SW 4	WSW 7	WSW 6
7	93.1	91.7	88.4	91.1	0.1	5.7	-0.4	1.2	6.5	-0.7	90	54	86	77	0.7	4.3	0.8	1.9	10 ≡	0 ⊙	5	SW 1	SSW 2	SSW 1
8	85.6	86.4	89.3	87.1	-2.6	2.4	2.9	1.4	3.6	-2.9	93	79	91	88	0.3	1.6	0.6	0.8	7	9 ⊙	10 ≡	C 0	C 0	SSW 1
9	93.1	96.9	103.1	97.7	0.5	2.2	1.4	1.4	3.0	-0.3	98	89	78	88	0.1	0.8	1.6	0.8	10 ✳ ≡	10	10	SW 1	WSW 3	WSW 2
10	105.7	105.5	103.7	105.0	-2.3	0.7	-0.7	-0.8	2.7	-3.0	93	83	89	88	0.4	1.1	0.6	0.7	7 ≡	7	10 ≡	WSW 2	WNW 3	C 0
11	99.3	96.9	101.4	99.2	0.4	3.8	0.9	1.5	4.1	-1.0	86	54	81	74	0.9	3.7	1.2	1.9	8	10	0	C 0	SSW 3	WSW 4
12	92.8	78.2	65.8	78.9	-0.7	3.6	7.1	4.3	8.1	-2.2	77	68	62	69	1.3	2.5	3.9	2.6	2	10	10 ●	SW 1	SW 10	SW 10
13	63.5	60.5	61.7	61.9	4.1	1.5	0.5	1.6	7.5	0.2	67	96	96	86	2.7	0.3	0.2	1.1	8	10 ● ≡	10 ✳	SW 3	SW 2	C 0
14	64.3	65.2	70.0	66.5	-0.3	-0.4	-1.4	-0.9	0.8	-1.7	94	92	94	93	0.4	0.5	0.3	0.4	10 ≡	10 ✳	10	C 0	NNW 4	WNW 2
15	79.2	83.1	91.8	84.7	-2.5	-1.5	-3.8	-2.9	-1.0	-4.1	82	84	96	87	0.9	0.9	0.2	0.7	9	10 ✳	9 ✳	NW 6	NW 7	W 4
16	86.8	76.4	68.4	77.2	-3.3	-1.8	3.4	-0.1	4.7	-6.1	93	100	76	90	0.3	0.0	1.9	0.7	10 ⊙	10 ✳ ≡	10 ●	SSW 3	SSW 6	SW 10
17	64.6	66.0	72.4	67.7	1.1	1.9	0.6	1.0	3.6	-0.1	96	82	100	93	0.2	1.3	0.0	0.5	10 ✳ ≡	10 ✳	10	SW 7	W 8	W 6
18	79.9	84.9	93.3	86.0	-2.3	-1.0	-2.6	-2.1	0.7	-4.2	85	65	95	82	0.8	2.0	0.2	1.0	10	9 ⊙	8	WNW 7	W 6	WSW 3
19	92.6	90.7	91.5	91.6	-2.5	-0.9	2.6	0.4	2.6	-3.1	93	98	95	95	0.4	0.1	0.4	0.3	10 ✳ ≡	10 ✳ ≡	10 ≡	WSW 2	SW 2	WSW 5
20	93.0	93.3	91.2	92.5	2.7	2.8	3.2	3.0	4.1	2.2	89	98	90	92	0.8	0.2	0.8	0.6	10 ☂	10	10	WSW 5	WSW 4	WSW 8
21	91.8	93.6	97.0	94.1	1.1	-0.1	-1.4	-0.4	4.3	-1.6	75	82	99	85	1.6	1.1	0.1	0.9	4	10	10 ✳	WNW 4	NW 6	NW 4
22	101.8	103.3	105.8	103.6	-4.3	-4.6	-4.7	-4.6	-1.1	-5.6	91	88	88	89	0.4	0.5	0.5	0.5	10 ✳	10 ✳	10 ✳	N 5	NE 3	N 3
23	104.9	101.7	97.4	101.3	-6.0	-5.0	-5.2	-5.4	-3.8	-7.1	81	73	98	84	0.7	1.1	0.1	0.6	10 ✳	9 ⊙	10 ✳	NW 4	WNW 4	E 2
24	92.4	90.8	91.7	91.6	-6.3	-5.4	-8.2	-7.1	-4.9	-9.1	94	83	92	90	0.2	0.6	0.2	0.3	10 ✳	10	9	W 1	NNE 2	NE 1
25	93.8	94.5	94.4	94.2	-10.4	-8.2	-5.3	-7.3	-3.1	-11.3	94	81	90	88	0.2	0.6	0.4	0.4	10 ✳	8	10	ENE 5	NE 5	NE 1
26	94.2	94.1	93.7	94.0	-5.7	-3.3	-3.0	-4.8	-3.0	-5.9	95	72	95	87	0.2	1.3	0.2	0.6	10	4 ⊙	10	NE 1	E 2	NE 5
27	91.6	89.7	89.8	90.4	-5.3	0.3	-3.4	-2.4	0.7	-5.4	93	82	97	91	0.3	1.1	0.2	0.5	10	9	10	NE 4	NE 5	NE 3
28	87.3	85.7	83.9	85.7	-3.9	-2.1	-2.3	-2.6	-1.5	-4.4	96	92	100	96	0.2	0.4	0.0	0.2	10 ✳	10 ✳	10	ENE 2	NE 3	NE 3
29																								
30																								
31																								
M	89.5	88.3	89.1	89.0	-2.8	-0.7	-1.3	-1.5	1.2	-4.1	90	82	90	87	0.6	1.2	0.7	0.8	5.1	8.9	9.2	2.6	3.7	3.3

Kraków, Obserw. Astr. UJ H_s=206m H_b=219,8m h_w=10m Styczeń - Janvier 1962

DNI	WIDZIALNOŚĆ	OPAD R	GRUB. ŚNIEGU h	POGODA
1	5	0.4	11	•°8⁰⁰-9³⁰,p; ≡°I,=II,III
2	5	•	8	=I,II,III
3	6	•	8	≡°III
4	7	•	7	=I≡°ok.7⁰⁰-8⁰⁰=III
5	3	•	7	=I≡°II,III,⌣'I
6	4	0.5	6	*°np; ≡°I=II,III;⌣'I
7	5	0.1	7	*'⁻⁰na-a,II,np; =I,II
8	7	•	7	≡°I=III
9	5	•	7	≡'I=II≡'III;⌣'I; V°III
10	3	•	7	≡'I≡°II≡'III; V'I
11	8	4.0	5	≡°V°I≡°III; V°I;ω ok.18⁰⁰...20⁰⁰
12	4	3.4	3	•⁰⁻¹na,I-do ok.10⁰⁰; ≡°I≡'11³⁰-12⁰⁰=II≡'III
13	8	1.9	2	•°6²⁰-7³⁰,p...np; =I≡°ok.7³⁰-8¹⁵
14	8	•	2	ωIII
15	8	•	pż.	=III
16	8	•	pż.	≡°I≡°III;⌣°I
17	5	•	pż.	≡°I=II,III;⌣°I;ω17⁰⁰-19⁰⁰
18	3	•	pż.	≡°I,II,III;⌣'I⌣°III;ω ok.18⁰⁰-20³⁰
19	3	1.0	pż.	•°ok.14⁰⁰-16⁰⁰,np;≡°I,II≡°III;⌣°I
20	8	•	pż.	=I,III
21	7	0.4	pż.	•ok.16³⁰; =I,III;ϖ ok.22⁰⁰
22	4	•	•	≡°I=II;⌣°I
23	7	0.0	•	≡°I
24	7	2.3	•	*°na...ϑ ok.18⁰⁰•°18¹⁵ϑIII; =I,III
25	3	2.3	•	•°na - ok.10⁰⁰,p ϑ ok.20⁴⁵np ϑ ok.21²⁰ =I≡°10⁰⁰,II=III
26	4	2.3	•	ϑa...; =I,II
27	4	2.9	2	*na *'I ϑa...ϑ*p...; ≡°I=II
28	6	3.2	1	*'na...,I ⚹ ok.7⁰⁰⁻³⁰ *²p...⊥ 14³⁰-15⁰⁰
29	4	3.1	5	*°na...np
30	6	0.7	9	*°na...p; ≡°I
31	5	0.1	11	*°a,II; ≡°I,II,III
Σ	—	28.6	—	UWAGI. W ciągu całego roku uwagi dotyczące mgły są niepewne. W ciągu całego roku wartości ciśnienia powietrza są za niskie przeciętnie o ok. 0,5 mb.

Luty - Février

1	4	0.9	9	=I,II,III
2	5	0.8	10	*na; ≡°I=II,III
3	3	0.0	9	♎°ok.11⁰⁰II; ≡°I,II=III,⌣'I
4	5	0.0	8	*°ok.19⁰⁰; ≡°I=II,III
5	6	4.5	8	*'14⁰⁰-17⁰⁰; ≡°I
6	5	0.6	6	*'na *°I *⁰⁻¹ 9⁰⁰...12³⁰ *°...p; =II
7	8	•	5	≡°I=III
8	4	1.8	2	=I,II≡°III;⌣'I
9	4	1.2	3	*'na,I •°⚹ - ok.9⁰⁰; ≡'I=II,III
10	6	•	pż.	≡°I≡'III;⌣'I
11	6	0.3	pż.	*²13⁵⁷-14¹⁰ *°-ok.17⁰⁰
12	7	6.6	pż.	*⁰⁻¹ok.10⁰⁰...11³⁰ •°ok.16³⁰III ⚹°np,⚳'23⁵⁰-ok.0⁰⁰;⌣'I; ⚳II ⚳p ⚳III
13	3	7.6	pż.	•⁰⁻⁰ok.9⁰⁰II •²p...*²ok.17⁰⁰-np; ≡°II=III
14	4	0.1	3	*²⁻⁰a...p, *°ok.18⁰⁰;
15	4	0.2	3	*°na *¹⁻²a...,II *°ok.13⁰⁰ *'ok17⁰⁰ *°III;=I,II,III
16	3	4.1	4	*²a-II •*p •'p- ok.21¹⁵; ≡°II
17	5	7.3	5	*°na *²I *°a *'II *p...⊥ 11³⁰-12¹⁵; ≡°I=II
18	7	0.3	13	*²na,a *p; ⊥ ok.11⁰⁰-12⁰⁰
19	3	5.9	15	*⁰⁻¹na *°I *⁰⁻²a,II,p •°p ϑ ok.19⁰⁰; ≡°I,II≡°III
20	5	0.1	8	ϑna - ok.8³⁰ •°ok.19³⁰; =I,II,III
21	7	1.2	pż.	*²⁻⁰a... ok.11⁰⁰ •°ϑp *'p *°III; =I,III
22	4	0.0	3	*°I *'II *°ok.19⁰⁰ *°III *np; =I,II,III
23	6	2.7	2	*°I,a *⁰⁻²p,III; =I,III
24	6	0.5	13	*'na,I, ok.9¹⁰ *°p...;⌣°III
25	6	0.2	9	*°na,I ⚹p; =I
26	5	•	6	=I,II,III
27	5	0.6	6	=I,II,III
28	5	0.3	5	*'na,I ⚹° ok.11⁰⁰-p *°p; =I,II,III
29				
30				
31				
Σ	—	47.8	—	UWAGI.

Kraków, Obserw. Astr. UJ φ = 50°04' λ = 19°58' Marzec - Mars 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	81.7	80.6	79.8	80.7	-2.5	-1.5	-1.6	-1.8	-1.0	-2.9	100	94	96	97	0.0	0.3	0.2	0.2	10 ═	10	10	SE 2	ENE 4	NE 3
2	78.5	77.4	78.3	78.1	-2.1	1.4	-0.3	-0.3	2.1	-2.5	96	83	88	89	0.2	1.1	0.8	0.7	10 ═	7 ⊙	10 ═	C 0	C 0	C 0
3	78.7	78.5	77.9	78.4	-1.9	4.1	1.8	1.4	5.2	-5.2	90	75	80	82	0.5	2.0	1.5	1.5	10 * ═	9 ⊙	10	C 0	C 0	SW 1
4	72.3	68.5	66.9	69.2	0.5	6.8	4.7	4.2	9.2	-0.3	86	75	87	83	0.8	2.5	1.1	1.5	7 ⊙	10	9	SW 1	SE 1	C 0
5	68.5	68.8	67.2	68.2	2.2	10.1	8.2	7.2	10.7	1.7	95	77	95	88	0.4	2.9	0.8	1.4	9 ═	10	10 ●	C 0	E 1	E 1
6	67.0	78.9	85.3	77.4	3.5	1.6	0.6	1.6	8.4	0.5	91	81	88	87	0.6	1.3	0.8	0.9	10 ○	10	10	WSW 7	WSW 3	W 3
7	90.9	92.7	96.8	95.5	-2.3	-1.7	-1.9	-2.0	0.8	-2.7	98	71	71	80	0.1	1.6	1.5	1.1	10 *	10	10	NW 2	NW 4	NNW 3
8	99.0	100.3	99.9	99.7	-3.7	-0.5	-1.7	-1.9	1.2	-4.5	85	72	77	78	0.7	1.7	1.2	1.2	9 ⊙	9	0	NW 1	WNW 3	SSW 1
9	99.7	98.4	95.3	97.8	-5.7	2.5	-2.1	-1.8	3.6	-6.3	90	50	77	72	0.4	3.7	1.2	1.8	6 ═	3 ⊙	0	C 0	E 5	ENE 6
10	89.2	86.8	86.0	87.3	-2.2	4.7	1.6	1.4	7.4	-3.8	56	45	85	62	2.3	4.6	1.1	2.7	9	10 ⊙	4 ═	ENE 1	ENE 2	NE 1
11	83.5	81.9	79.3	81.6	-0.6	9.0	4.2	4.2	9.3	-1.6	81	66	97	81	1.1	4.0	0.2	1.8	8	10 ⊙	9 ●	C 0	C 0	C 0
12	74.1	70.7	67.1	70.6	1.5	2.0	1.0	1.4	4.4	0.8	98	96	96	97	0.1	0.3	0.3	0.2	10 ●	10 * ═	10 * ═	C 0	SE 1	WSW 3
13	74.0	79.2	85.9	79.7	-2.1	-2.0	-4.2	-3.1	1.3	-4.6	81	60	82	74	1.0	2.1	0.8	1.3	9 *	9 *	3	W 8	WNW 9	W 4
14	90.6	92.1	94.2	92.3	-6.9	-2.8	-4.8	-4.8	-1.5	-7.2	91	58	76	75	0.3	2.1	1.0	1.1	7 ⊙	7 ⊙	10	SW 4	W 3	C 0
15	92.4	90.2	89.8	90.8	-5.8	-4.2	-6.2	-5.6	-3.8	-6.7	89	63	89	80	0.4	1.6	0.4	0.8	10	10	10 ═	NE 1	NNE 5	ENE 8
16	87.6	87.5	88.1	87.7	-6.3	-5.5	-7.0	-6.4	-5.3	-7.2	94	90	91	92	0.2	0.4	0.3	0.3	10 *	10 *	10	N 8	NNE 8	N 8
17	84.5	83.3	84.4	84.1	-7.1	-5.0	-4.3	-5.2	-3.8	-7.8	91	88	94	91	0.3	0.5	0.3	0.4	10 *	10	10 *	NW 3	NW 6	NNW 5
18	86.3	90.0	91.9	89.4	-4.2	-0.9	-4.0	-3.3	0.3	-5.6	79	50	68	66	0.9	2.9	1.4	1.7	10	2 ⊙	8	NE 5	NW 3	N 1
19	92.9	93.4	93.9	93.4	-5.5	-1.3	-2.4	-2.9	-0.4	-5.6	82	70	85	79	0.7	1.7	0.8	1.1	8 ═ ⊙	9	10	N 1	NE 4	ENE 1
20	93.7	93.5	92.5	93.2	-7.0	-0.5	-3.5	-3.6	1.1	-7.2	91	76	90	86	0.3	1.4	0.5	0.7	6 ⊙	2 ⊙	0	C 0	ENE 3	ENE 1
21	90.3	87.2	85.2	87.6	-9.4	-0.9	-3.3	-4.2	-0.2	-10.8	98	69	90	86	0.1	1.8	0.5	0.8	4 ⊙	0 ⊙	10	C 0	NNE 4	NNE 4
22	82.4	81.4	80.5	81.4	-4.4	-2.9	-3.4	-3.5	-2.4	-5.0	93	93	94	93	0.3	0.3	0.3	0.3	10	10 *	10 *	NE 4	NE 3	NNE 2
23	79.7	80.1	82.2	80.7	-4.9	-0.7	-1.3	-2.0	-0.3	-5.6	98	93	95	95	0.1	0.4	0.3	0.3	10 *	10 *	10 ═ *	N 2	NNW 1	NNW 1
24	85.7	88.6	92.4	88.9	-2.5	1.5	-0.9	-0.7	2.3	-3.2	100	69	87	85	0.0	2.1	0.7	0.9	10 * ═	9	9	WSW 2	W 3	SW 1
25	95.1	94.0	92.3	93.8	-5.4	0.6	-3.9	-3.2	0.9	-6.0	92	69	89	83	0.3	2.0	0.5	0.9	10	9	8	C 0	NE 1	C 0
26	90.3	88.7	86.2	88.4	-11.3	-1.8	-4.6	-5.6	-0.6	-12.1	97	73	91	87	0.1	1.4	0.4	0.6	6 ═ ⊙	0 ⊙	3	C 0	NE 5	NE 2
27	81.7	80.0	78.0	79.9	-9.4	-1.5	-1.3	-3.4	1.7	-10.7	91	72	90	84	0.3	1.6	0.5	0.8	0 ⊙	4 ⊙	4	NE 1	ENE 2	NNE 2
28	76.2	77.4	80.6	78.1	-1.7	3.5	1.4	1.2	6.4	-3.5	94	86	94	91	0.3	1.0	0.4	0.6	8 ═	10 ●	8	C 0	SW 2	SW 3
29	82.2	80.9	76.8	80.0	2.0	7.7	2.8	3.8	8.6	0.9	87	57	79	74	0.9	4.5	1.6	2.3	10	2	10	W 2	SSW 2	E 1
30	72.8	72.8	70.2	71.9	4.3	12.7	6.6	7.6	14.6	2.1	95	62	82	80	0.4	5.5	1.7	2.5	10 ═	6 ⊙	5	C 0	SW 5	E 2
31	66.8	68.0	68.3	67.7	7.0	15.7	10.3	10.8	16.0	4.2	91	58	80	76	0.9	7.4	2.5	3.6	6 ═ ⊙	9 ⊙	9	C 0	SW 4	SSW 1
M	83.5	83.6	83.6	83.6	-3.0	1.6	-0.6	-0.6	3.1	-4.1	90	72	86	83	0.5	2.2	0.8	1.2	8.5°	7.6	7.7	1.8	3.1	2.2

Kwiecień - Avril

1	77.5	82.3	84.7	81.5	3.8	3.4	5.4	4.5	10.5	2.1	92	90	62	81	0.7	0.8	3.5	1.7	10	9 ● ⊙	4	WSW 1	WSW 1	WSW 2
2	84.7	84.9	89.5	86.4	3.3	10.7	3.1	5.0	10.9	0.3	64	43	91	66	2.7	7.4	0.6	3.6	4 ⊙	6 ⊙	4	WSW 1	SW 7	SW 2
3	89.9	87.3	83.4	86.9	2.4	13.3	7.8	7.8	14.9	0.3	82	43	64	63	1.3	8.8	3.8	4.6	0 ⊙	4 ⊙	8	C 0	SW 5	SSE 3
4	79.1	75.8	72.9	75.9	7.1	15.9	12.0	11.8	17.4	3.0	59	40	57	52	4.2	10.8	6.0	7.0	2 ⊙	8 ⊙	10	ESE 2	SSE 5	S 4
5	62.1	62.7	64.6	63.1	10.2	9.0	7.7	8.6	12.1	7.4	66	86	80	77	4.2	1.6	2.1	2.6	9	10 ● ⊙	9	SE 4	WSW 3	WNW 2
6	66.8	69.6	72.7	69.7	4.9	5.7	5.6	5.4	7.8	4.2	92	89	92	91	0.7	1.0	0.7	0.8	10 ═	10 ●	10 ●	C 0	WNW 2	W 5
7	78.6	83.7	85.8	82.7	4.4	4.9	2.7	3.7	7.3	2.4	87	59	72	73	1.1	3.6	2.1	2.3	10 ●	10	5	NW 8	WNW 7	WSW 2
8	84.1	84.8	83.8	84.2	4.4	8.9	9.3	8.0	12.4	2.3	89	69	66	75	1.0	3.5	4.0	2.8	10 ●	10	1	SW 3	SW 7	S 3
9	84.6	86.1	89.5	86.7	6.3	13.5	7.4	8.6	14.9	3.8	81	54	80	72	1.8	7.1	2.1	3.7	9	8 ⊙	10 ●	C 0	NW 5	WSW 3
10	91.7	92.3	93.5	92.5	6.4	10.0	7.3	7.8	10.6	4.7	88	72	90	83	1.1	3.5	1.0	1.9	10	10	10	WSW 1	NNW 1	NW 1
11	93.7	93.2	93.1	93.3	5.9	7.7	7.1	7.0	8.3	5.5	89	90	99	93	1.0	1.0	0.2	0.7	10	10	10 ═	NW 3	NNW 2	SW 4
12	92.3	90.8	89.0	90.7	6.9	12.9	9.3	9.6	15.6	5.7	99	71	88	86	0.1	4.3	1.4	1.9	10 ═	4 ⊙	4 ═	WSW 3	SW 2	C 0
13	87.2	85.0	83.7	85.3	6.1	10.3	8.1	8.2	12.3	4.9	100	80	90	90	0.0	2.5	1.1	1.2	10 ═	10 ●	10	SW 1	W 3	WNW 2
14	86.3	89.6	93.5	89.8	3.7	5.1	5.1	4.8	8.2	3.2	92	87	94	91	0.7	1.1	0.6	0.8	10 ●	10	10	WSW 3	W 2	N 2
15	93.2	92.4	91.9	92.5	6.9	10.4	11.9	10.3	13.3	4.8	97	82	87	89	0.3	2.2	1.8	1.4	10	10	8	NW 3	WNW 5	NE 3
16	92.4	92.0	94.0	92.8	10.0	19.1	13.7	14.1	21.2	7.4	76	49	67	64	3.0	11.3	5.2	6.5	6 ⊙	3 ⊙	4	NE 4	SE 9	C 0
17	96.5	95.3	94.1	95.4	11.7	21.6	13.2	14.9	22.3	6.8	70	32	66	56	4.1	17.5	5.1	8.9	3 ⊙	7 ⊙	10	NE 1	SSE 4	C 0
18	93.0	91.5	90.5	91.7	9.6	20.7	14.7	14.9	22.2	8.5	69	37	60	55	3.8	15.4	6.7	8.6	9	9 ⊙	10	NE 1	SSE 4	SSE 1
19	90.5	90.6	91.5	90.9	10.7	24.5	18.6	18.1	25.4	7.9	78	32	57	56	2.9	21.0	9.3	11.1	8	6 ⊙	8	C 0	SW 2	SW 1
20	92.8	91.9	91.5	92.1	13.0	23.4	17.3	17.8	24.3	9.3	73	31	70	58	4.1	19.9	6.0	10.0	3 ⊙	7 ⊙	8	C 0	E 3	C 0
21	93.7	93.1	93.1	93.3	13.3	24.0	16.9	17.8	25.1	9.6	75	28	68	57	3.8	21.4	6.1	10.4	4 ⊙	2 ⊙	1	C 0	ENE 2	C 0
22	94.0	93.3	93.1	93.5	13.4	25.1	17.7	18.5	25.8	9.1	74	28	68	57	4.0	23.0	6.4	11.1	1 ⊙	1 ⊙	2	C 0	E 2	C 0
23	94.2	93.7	93.3	93.7	12.9	25.7	17.9	18.6	26.3	9.5	79	37	71	62	3.1	21.0	5.9	10.0	0 ⊙	1 ⊙	4	NE 1	ENE 3	NE 1
24	95.6	96.1	96.8	96.2	13.8	25.6	19.3	19.5	25.9	9.5	72	29	50	50	4.4	23.4	11.2	13.0	0 ⊙	0 ⊙	2	NNE 1	ENE 3	NNE 3
25	99.2	98.9	98.0	98.7	14.7	23.6	18.3	18.7	23.4	10.8	74	44	57	58	4.3	16.4	9.0	9.9	0 ⊙	0 ⊙	2	ENE 2	NNE 4	NE 3
26	96.7	92.7	86.9	92.1	11.5	22.6	15.9	16.5	24.0	7.9	72	36	71	60	3.8	17.5	5.3	8.9	0 ⊙	0 ⊙	8	NNE 1	ENE 3	C 0
27	82.4	83.3	85.4	83.7	13.3	11.1	7.6	9.9	16.2	7.3	87	72	69	76	2.0	3.7	3.2	3.0	10 ●	10	10	W 2	WNW 6	WNW 5
28	78.5	76.2	77.8	77.5	5.9	6.1	5.6	5.8	9.2	4.6	89	88	86	88	1.0	1.1	1.3	1.1	10 ●	6	9	W 5	WNW 3	WSW 3
29	80.1	80.5	80.7	80.4	4.8	8.3	3.4	5.0	9.1	3.2	76	56	95	76	2.0	4.9	0.4	2.4	10 ●	8	3	NW 5	W 3	C 0
30	80.0	81.0	84.9	82.0	4.5	5.1	3.5	4.2	8.3	2.7	79	80	75	78	1.8	1.8	1.9	1.8	9	9	10	WSW 2	NE 2	N 2
31																								
M	87.0	87.0	87.4	87.1	8.2	14.3	10.4	10.8	16.2	5.6	81	58	75	71	2.3	9.3	3.8	5.1	6.6	6.6	6.8	1.9	3.7	1.9

Kraków, Obserw. Astr. UJ H_s=206m H_L=219,8m h_w=10m Marzec - Mars 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	4	0.0	5	⛆°p...,np..., ≡°I=II,III
2	4	0.4	5	⛆ na ok 9³⁰, ≡°I,=II≡°III
3	4	0.2	4	*°na.. ok.8³⁰, ≡°I=II,III
4	6	0.0	pż.	•°ok 15⁰⁰-16⁰⁰, ⌣°I
5	4	6.4	pż.	•⁰⁻¹19⁰⁴-np, ≡'I=II,III
6	5	1.2	•	•⁰⁻¹na-ok.8⁰⁰ *°p; =I,II,III
7	7	1.1	1	*°n-a; =I
8	8	•	1	=I,III
9	8	•	pż.	≡°I; ⌣²I
10	8	•	•	≡°III; ⌣°I
11	5	1.1	•	•°13⁵⁰, •°p-np, =I,II,III; ⌣²I
12	3	8.2	•	*na •°I *°ok 12⁰⁰..np, =I≡°II,III
13	5	0.0	1	*na-a *¹⁻²a...p; ⊥ na,a; =I,II
14	6	0.0	1	*²9⁰⁰-ok.9²⁰ *⁰⁻²ok.11⁰⁰⁻⁴⁰ *°p; =I,II; ⌣'I, ⊟III
15	6	2.6	1	*p..., ⊥ p; ≡°III
16	4	4.0	6	*²na-a *²⁻¹a...p; =I,II; ≫ na,a
17	5	2.9	15	*°na *'I-a,p.. *°III; =I,II,III
18	7	•	22	*°na; =III
19	7	0.0	16	*²13⁰⁰-ok.13⁵⁰, ≡'I
20	6	•	10	=I,II, ⌣°I
21	6	•	8	=I, ⌣'I
22	4	2.1	8	*°ok.11⁰⁰ *'II, ok.14⁰⁰, ok.20⁰⁰, III; =II,III, ⌣°I
23	4	6.2	10	*°na-p *'p...np, =I,II≡°III
24	5	0.2	17	*°na-ok.8³⁰, ≡°I,III
25	6	•	11	=I
26	6	•	10	≡'na-a =III, ⌣'I
27	6	•	7	=I,III; ⌣'I, ⊕ II
28	4	0.6	5	•°10⁵⁵-np,p..., ≡°I,II,III, ⌣°I
29	6	1.1	2	*°n, =I
30	7	0.6	pż.	•°n, ok 8⁰⁰, ok 14¹⁰⁻⁴⁰, ≡°I
31	7	3.9	•	•°n, a, ≡°I
Σ	—	42.8	—	UWAGI

Kwiecień - Avril

1	5	2.4	•	•n •² 11⁴⁰-12⁴⁰ •°13⁰⁵, ⚢ 11⁵², =I,II
2	8	0.2	•	•⁰⁻¹18⁵⁰-ok 19²⁰, =I,III; ⌣'I
3	8	•	•	=I; ⌣°I
4	9	•	•	
5	5	2.0	•	•'11⁰⁵-ok 13³⁰, =II,III
6	4	40.7	•	•⁰⁻²ok 8³⁰-np; ≡°I=II,III
7	7	0.3	•	•²⁻¹na-ok 8⁰⁰ •°a...; =I
8	8	0.1	•	•°I, ok 11⁰⁰-12⁰⁰
9	5	0.4	•	•⁰⁻¹14⁰⁵-16⁴⁵, ok 20⁰⁰-np; =I,II,III, △°I
10	7	5.4	•	•°n ⊽ ok.12⁰⁰ •⁰⁻¹14³⁰-p; =I,III
11	5	0.1	•	•n •°10³⁰-ok 10⁵⁰; =I,II≡°III
12	4	•	•	≡°I=II≡°III
13	5	9.4	•	•°II,p..., ≡²I=II,III
14	5	4.0	•	•°na-a •' ok 9³⁰ •°ok 20⁰⁰; =II,III
15	7	0.6	•	•'na, 18²⁶-ok 19⁰⁰, =I
16	8	•	•	△'III
17	8	•	•	△'I
18	8	•	•	△²I
19	7	•	•	=I,II
20	8	•	•	=I,III
21	7	•	•	=I, △²I
22	6	•	•	△²I
23	7	•	•	△²I △°III
24	7	•	•	△'I
25	8	•	•	
26	7	0.0	•	△'I
27	7	6.5	•	•°na-8⁰⁰ •²⁻¹-9¹⁵ ⊽ °p; =I
28	7	10.4	•	•⁰⁻²4⁴⁵-7⁴⁵ •² 9³⁰-10⁴⁰ •'18¹⁰ ▲ 12⁰⁹⁻¹⁴, 14⁰⁹⁻¹², ⚢°14¹⁵⁻²³ =I
29	8	5.2	•	•°6³⁰-a •' 9³⁰⁻⁵⁵ •°10⁴⁵ ▲ 10⁴⁵⁻⁴⁸ •²11¹⁵ •°-ok.11⁴⁵ •²13²⁰⁻³⁵, 16¹⁰⁻³⁵, (⚢) 12³⁷N, ⊕ a
30	8	3.4	•	•°11⁵⁵-12¹⁰ •²-12³⁰, 13⁰⁴-14⁰⁰ ▲ 13⁰⁴...²¹, =I
31				
Σ	—	93.1	—	UWAGI

Kraków, Obserw. Astr. UJ φ = 50°04' λ = 19°58' Maj - Mai 1962

DNI	CIŚNIENIE P∞ 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D.v I	II	III
1	85.0	83.8	83.2	84.0	1.5	5.4	2.5	3.0	6.9	-0.1	74	56	88	73	1.8	4.0	0.9	2.2	10	8	9	NW 1	W 4	SW 3
2	80.4	79.6	82.2	80.7	4.1	5.7	4.5	4.7	9.1	1.6	74	77	85	79	2.2	2.1	1.2	1.8	8	6 ●⊙	10 ●	SW 2	WNW 3	W 2
3	84.2	83.8	82.7	83.6	2.9	9.1	6.7	6.4	10.9	1.6	89	63	72	75	0.8	4.3	2.7	2.6	8	7 ⊙	8	W 2	SSE 2	SW 2
4	79.0	79.9	82.3	80.4	6.0	7.4	6.6	6.6	11.0	5.3	92	80	71	81	0.8	2.1	2.8	1.9	10 ●	7 ⊙	7	W 2	SW 5	WNW 2
5	84.7	86.2	89.1	86.7	4.8	10.2	7.7	7.6	12.6	1.1	84	59	86	76	1.4	5.1	1.5	2.7	9	10	10 ●	C 0	NE 3	NNW 3
6	92.0	93.0	92.0	92.3	6.6	14.1	9.2	9.8	14.5	4.6	94	52	76	74	0.5	7.7	2.7	3.6	10	7 ⊙	0	NNW 1	ESE 3	E 1
7	89.9	89.3	89.5	89.6	6.6	15.6	14.0	12.6	16.3	3.6	90	64	85	80	1.0	6.4	2.3	3.2	9 ⊙	9	5	C 0	S 2	WSW 1
8	89.0	87.0	86.3	87.4	14.0	22.3	18.1	18.2	23.6	11.3	88	56	73	72	2.0	12.0	5.6	6.5	6 ⊙	6 ⊙	10 ●K	S 1	SW 6	SW 1
9	87.1	87.3	84.6	86.3	14.4	19.5	16.0	16.5	20.5	13.6	82	49	67	66	2.9	11.6	6.0	6.8	9	6 ⊙	9	WSW 3	WSW 4	ENE 2
10	81.4	83.7	85.1	83.4	12.5	13.8	11.9	12.5	18.3	11.6	94	82	88	88	0.9	2.9	1.7	1.8	10	10	5	NNE 1	W 4	C 0
11	86.0	85.5	85.8	85.8	11.6	15.5	9.0	11.3	16.0	8.7	83	52	96	77	2.3	8.4	0.5	3.7	9 ⊙	10	2	WSW 1	W 2	C 0
12	88.2	87.9	88.4	88.2	9.0	17.1	12.0	12.3	17.7	5.3	86	42	79	69	1.6	11.2	3.0	5.3	1 ⊙	9 ⊙	10 ●	C 0	NE 2	SSE 2
13	89.3	88.8	87.9	88.7	10.7	18.1	12.6	13.5	18.7	7.0	86	48	88	74	1.8	10.8	1.7	4.8	4 ⊙	10	10 ●	S 1	SE 2	SE 1
14	77.4	72.8	77.1	75.8	12.0	14.8	6.9	10.2	18.2	6.6	96	88	91	92	0.5	2.0	0.8	1.1	10 ●	10	10 ●	ENE 3	SW 2	SW 9
15	78.0	80.3	82.1	80.1	8.3	7.7	7.8	7.9	8.9	6.4	79	87	87	84	2.3	1.3	1.4	1.7	10 ●	10 ●	10 ●	WNW 8	WSW 7	WSW 6
16	85.4	87.4	90.4	87.7	8.3	12.0	8.4	9.3	12.7	7.3	82	60	68	70	2.0	5.5	3.6	3.7	10	9	8	WSW 8	WSW 7	WSW 1
17	90.0	88.2	87.7	88.6	8.1	16.1	13.3	12.7	17.9	4.3	76	55	73	68	2.5	8.2	4.2	5.0	8 ⊙	8	6	C 0	SW 4	WSW 4
18	88.4	90.8	93.2	90.8	10.5	10.7	10.2	10.4	15.8	9.6	96	94	83	91	0.3	0.9	2.0	1.1	10 ●	10	7	SW 1	NW 1	C 0
19	91.9	87.4	82.7	87.3	9.7	20.9	16.7	16.0	24.0	4.7	86	49	75	70	1.7	12.3	4.8	6.3	9 ⊙	4 ⊙	8	C 0	SE 5	SE 2
20	82.6	85.0	87.1	84.9	16.7	11.3	9.1	11.6	17.0	8.8	76	89	93	86	4.6	1.5	0.8	2.3	9	10 ●	10 ●	SW 4	WNW 5	W 1
21	88.7	88.6	88.2	88.5	8.2	9.7	8.9	8.9	9.9	7.6	94	88	93	92	0.6	1.4	0.8	0.9	10 ●	10 ●	10	WNW 1	C 0	WNW 1
22	88.3	87.7	90.3	88.8	7.4	18.9	13.0	13.1	19.1	6.3	97	45	79	74	0.3	11.9	3.1	5.1	6 ⊙	7 ⊙	5	SW 1	SW 3	WSW 2
23	92.9	91.5	90.2	91.5	12.7	19.9	14.3	15.3	21.9	7.9	75	44	82	67	3.7	13.0	2.9	6.5	2 ⊙	4 ⊙	4	C 0	SW 3	C 0
24	92.2	91.8	89.2	91.1	13.9	15.2	11.9	13.2	15.5	11.0	88	70	93	84	2.0	5.1	1.0	2.7	10 ●	10	10	W 2	WNW 1	W 1
25	87.6	87.8	86.3	87.2	8.9	10.7	10.0	9.9	12.4	8.4	96	89	97	94	0.5	1.5	0.3	0.8	10 ●	10 ●	10	W 1	WNW 1	NNE 3
26	83.7	82.1	86.4	84.1	10.7	14.7	12.5	12.6	15.9	9.7	99	85	90	91	0.2	2.5	1.4	1.4	10 ●	10	10	NE 2	E 5	W 1
27	88.5	89.1	89.4	89.0	10.7	14.3	13.9	13.2	16.5	9.9	94	78	88	87	0.9	3.6	2.0	2.2	10 ●	10 ⊙	10	C 0	WSW 1	NNE 2
28	89.4	88.5	86.9	88.3	13.7	19.3	17.1	16.8	21.1	12.2	90	72	92	85	1.6	6.2	1.6	3.1	9	9	4	NNE 1	E 1	C 0
29	90.3	90.8	89.7	90.3	13.3	17.3	15.8	15.6	20.5	12.2	90	69	78	79	1.6	6.2	3.9	3.9	10	5 ⊙	10	C 0	ENE 3	SW 1
30	91.7	92.9	92.1	92.2	10.5	12.3	10.8	11.1	16.3	10.1	95	83	92	90	0.7	2.4	1.0	1.4	10 ●	10 ●	0	W 1	WSW 2	C 0
31	91.3	87.9	83.7	87.6	12.3	21.0	17.0	16.8	22.9	6.0	75	40	66	60	3.5	15.0	6.7	8.4	0 ⊙	1 ⊙	3	C 0	SW 2	SW 1
M	86.9	86.7	86.8	86.8	9.7	14.2	11.2	11.6	16.2	7.2	87	67	83	79	1.6	6.1	2.4	3.4	8.3	8.1	7.4	1.5	3.1	1.8

Czerwiec - Juin

1	89.7	91.0	90.2	90.3	7.9	8.9	5.4	6.9	17.8	5.1	89	86	95	90	1.2	1.5	0.5	1.1	10 ●	10	10 ●	NNW 2	WSW 1	NNE 2
2	87.4	91.9	93.9	91.1	4.8	7.3	8.7	7.4	10.4	3.4	97	83	85	88	0.3	1.7	1.6	1.2	10	10	10	N 4	NW 3	NW 1
3	95.8	95.8	96.9	96.2	8.3	11.7	7.7	8.8	12.9	7.1	83	63	94	80	1.9	5.0	0.6	2.5	10	10	10 ●	NW 1	NE 3	WNW 1
4	95.7	95.9	94.6	95.4	6.8	8.9	6.3	7.1	9.4	6.1	94	85	91	90	0.6	1.7	0.8	1.0	10 ●	10	10 ●	W 2	WSW 4	W 4
5	92.9	93.5	94.4	93.6	7.1	7.6	8.2	7.8	9.1	5.9	90	86	85	87	1.0	1.4	1.7	1.4	10 ●	10 ●	10 ●	SW 4	NW 6	NNW 3
6	94.3	94.8	97.5	95.5	6.6	10.8	7.3	8.0	12.8	6.0	76	53	70	66	2.3	6.2	3.0	3.8	10	10	10	NW 5	NW 9	NNE 2
7	97.6	99.7	100.8	99.4	5.3	7.6	7.0	6.7	8.3	4.0	89	80	93	87	1.0	2.0	0.7	1.2	10 ●	10	10 ●	NNW 3	N 2	W 2
8	100.2	100.5	98.8	99.8	9.3	15.4	10.8	11.6	16.3	5.7	80	51	87	73	2.3	8.3	1.7	4.2	0 ⊙	10	1	C 0	N 3	C 0
9	95.0	92.0	88.3	91.8	10.6	20.0	15.1	15.2	21.0	5.0	82	43	70	66	2.3	12.9	5.1	6.8	6 ⊙	1 ⊙	3	WNW 2	SSW 3	C 0
10	86.3	84.6	84.6	85.2	15.5	20.3	16.0	17.0	23.4	11.6	59	49	81	63	7.2	12.4	3.4	7.7	4 ⊙	8 ⊙	7	W 3	WSW 6	C 0
11	83.0	82.2	83.2	82.8	14.8	17.7	13.3	14.8	21.7	10.2	76	66	86	76	4.0	6.8	2.1	4.3	8	8	10	C 0	NW 6	W 2
12	86.3	86.9	89.0	87.4	11.8	15.6	10.1	11.4	15.5	9.8	78	61	70	70	3.0	6.2	3.8	4.3	10 ●	10	1	W 2	W 1	NE 1
13	91.4	92.4	91.6	91.8	10.3	16.2	11.5	12.4	18.5	8.1	81	53	84	73	2.4	8.6	2.2	4.4	9	9 ●	7	WSW 1	WNW 1	C 0
14	91.0	89.2	90.4	90.2	11.9	22.4	15.6	16.4	23.6	5.8	77	43	87	69	3.1	15.5	2.3	7.0	7 ⊙	7 ⊙	0	C 0	SW 2	C 0
15	92.6	92.9	93.4	93.0	18.2	27.0	19.9	21.2	28.4	11.9	74	46	74	65	5.5	19.1	5.9	10.5	0 ⊙	4 ⊙	0	W 1	SW 3	C 0
16	94.4	92.7	91.9	93.0	19.2	29.6	22.8	23.6	29.9	13.4	75	41	71	62	5.6	24.5	8.1	12.7	0 ⊙	1 ⊙	7	C 0	E 1	C 0
17	93.9	93.7	93.7	93.8	18.8	22.7	18.8	19.8	23.4	17.8	90	67	93	83	2.1	9.2	1.5	4.3	9(K)	9 ●(K)	10	SW 2	NNE 1	C 0
18	93.7	93.0	91.6	92.8	17.9	22.3	18.0	19.0	24.0	15.3	74	60	84	73	5.4	10.7	3.2	6.4	5 ⊙	8 ⊙	2	ENE 4	ENE 2	NNE 1
19	91.2	89.2	87.1	89.2	17.4	25.1	21.1	21.2	26.4	12.1	77	45	76	66	4.6	17.4	6.0	9.3	0 ⊙	0 ⊙	0	NE 2	ESE 1	C 0
20	89.0	91.0	91.5	90.5	20.2	20.8	18.9	19.7	23.3	15.3	75	69	74	73	6.1	7.6	5.7	6.5	10 ⊙	10	7	WSW 2	WNW 3	C 0
21	94.3	95.3	94.6	94.7	17.3	21.1	19.0	19.1	24.2	15.0	82	56	76	71	3.5	10.9	5.2	6.3	9	9 ⊙	1	C 0	NW 2	C 0
22	97.1	96.6	95.9	96.5	18.1	24.8	19.6	20.5	26.6	14.2	79	55	83	72	4.3	14.1	3.9	7.5	0	4 ⊙	0	C 0	NNE 2	C 0
23	95.7	94.3	92.4	94.1	19.7	28.5	22.5	23.3	30.4	14.4	75	38	73	62	5.7	24.3	7.4	12.5	0 ⊙	1 ⊙	3	ENE 1	WSW 3	C 0
24	92.8	90.9	88.8	90.8	20.6	27.6	22.0	23.0	30.1	17.6	74	48	72	63	6.3	19.3	7.2	10.9	6 ⊙	1 ⊙	0	C 0	WSW 2	C 0
25	88.9	90.8	93.4	91.0	21.0	22.8	17.7	19.8	23.9	16.7	68	45	46	53	7.9	13.1	8.9	10.6	0	4 ⊙	9	W 1	WNW 5	WNW 2
26	92.3	90.0	87.2	89.8	14.4	18.7	13.4	16.0	19.2	10.0	63	40	63	56	6.1	13.1	6.2	8.5	2 ⊙	9 ⊙	10	C 0	SE 1	E 1
27	85.5	85.9	87.5	86.3	12.9	17.6	14.7	15.0	19.7	8.9	79	52	46	59	3.1	9.7	9.0	7.3	9 ⊙	6 ⊙	10	WSW 2	WNW 3	WNW 2
28	87.9	87.5	84.9	86.8	11.3	11.1	11.5	11.4	14.8	9.1	66	72	72	70	4.5	3.7	3.8	4.0	1 ⊙	9 ⊙	10 ●	WSW 3	WSW 1	SW 3
29	85.3	86.6	87.4	86.4	10.6	13.7	13.0	12.6	16.1	8.1	75	62	62	66	3.2	6.0	5.8	5.0	8	8	4	WSW 6	SW 6	WSW 4
30	87.0	88.4	89.9	88.4	11.1	13.8	11.5	12.0	14.4	8.0	71	55	82	69	3.9	7.2	2.5	4.3	9	10	10	WSW 6	WSW 5	W 3
31																								
M	91.6	91.6	91.5	91.6	13.3	17.9	14.3	15.0	19.9	10.1	78	58	78	71	3.7	10.1	4.0	5.9	6.1	7.2	6.1	2.0	3.0	1.1

Kraków, Obserw. Astr. UJ H_s=206m H_t=219,8m h_w=10m Maj - Mai 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ LODU h	POGODA
1	8	0.0	•	*°10^30-42,10^49-54 ⚲°n
2	5	1.1	•	•°12^30-45 II, 14^35-15^40 •² 20^00-30 •'-np; =II,III; ⌓°I
3	7	0.4	•	⚲° ok. 11^30-12^00; =I
4	6	2.0	•	•'6^20-25 •²-7^40 •°-8^30; =I
5	6	0.3	•	•° ok. 19^00 . np; =I,III
6	7	•	•	⌓° III
7	5	4.3	•	•°9^28-ok. 10^00 •² 10^55-13^50 •°-ok. 15^00; =I,II; ⌓'I
8	7	4.4	•	•'20^20-40 •²-21^20 •'-np; ⚲12^12 ⚲'20^49 ⚲² 21^00-27; =I,III
9	7	10.6	•	•' ok. 1^00-40 •²-4^00 •'-5^50; =I
10	5	2.9	•	•'7^40-11^10; =I,II
11	7	5.1	•	•² 16^50-18^15; =I,III; ⌓'I
12	7	0.0	•	•°20^20-np; =I; ⊕ II
13	8	15.5	•	•°18^40-19^20 •²-24; =III; ⌓²I
14	9	6.2	•	•0^00-a •² 11^40-12^15 •° ok. 20^00-np; ⚲'11^08-⚲° 11^46-56; ⚲ 11^08-56
15	5	4.2	•	•na-8^35 •'-ok. 14^30 •° 19^30-np; =II
16	7	0.0	•	•° ok. 11^10-12^00
17	8	2.6	•	=I
18	6	4.0	•	•°-I 3^45-8^00 •² 11^45-12^20
19	8	•	•	=I
20	5	11.7	•	•°-I 2^10-np
21	6	11.9	•	•I-° na-ok. 18^00; =I,III
22	8	•	•	=I,III
23	8	0.0	•	=III; ⌓'I
24	7	7.0	•	•° na-a •'14^40-ok. 17^45; =I
25	6	15.3	•	•°-I 2^10-14^50 •° ok. 17^00-np; =I
26	6	13.4	•	•2-I 5^30-ok. 9^00 •² 13^30-14^20 •'14^30-15^00; ⚲ 15^21 SW; =I
27	5	0.1	•	•° na •na-a •° ok. 13^00 ⚲°n; =I,II,III
28	6	8.4	•	•°23^20-23^30 •²-24; ⚲° 23^30; =I; ⌓² III
29	6	2.1	•	⚲a; =I,III; ⌓° III
30	5	0.5	•	•° na-ok. 10^00, a-n, ok. 16^30; =I,II,III
31	8	6.9	•	=I, ⌓°I,III
Σ	—	140.9	—	UWAGI

Czerwiec - Juin

1	6	31.9	•	•°2^20-3^00 •²-na •'-8^10; 14^20-16^05 •²-I-24; ⚲'23^59 =I,III
2	6	1.1	•	•0^00-7^30; =I
3	7	4.6	•	•° ok. 10^40, 14^10-30, 17^05-20^30 •'-np
4	6	16.2	•	•° na-a •² 8^50-9^15, 16^10-np; =I
5	6	4.2	•	•na-a •'9^55-ok. 12^00 •°-15^20 •'-18^30 •°-np
6	8	2.2	•	•° na
7	7	0.4	•	•° na-10^00 •°, •17^56-np
8	8	•	•	=I; ⌓° II
9	8	•	•	⌓'I ⌓° III
10	7	•	•	⌓°I, III; =III
11	7	0.6	•	•°14^42-15^00 •'19^40-50; (⚲) 11^28-42 NW; =I; ⌓°I
12	6	•	•	•°I, ⌓' III
13	7	0.0	•	•°II ⚲°n; =I
14	7	•	•	=I,III; ⌓°I ⌓' III
15	6	•	•	⌓°I ⌓' III
16	7	1.6	•	•² 4^20-6^45; ⊂ III; =I
17	6	2.1	•	⚲°12^15, 13^30-40 •² 17^29-18^25; ⚲'4^19 ⚲°7^20 (⚲) 7^34, (⚲) W 13^30, II (⚲) 17^26; =I,III
18	7	•	•	=III; ⌓° III
19	7	•	•	⌓'I ⌓° III
20	7	0.0	•	=I
21	7	0.0	•	•° ok. 11^00; =I; ⌓°I,III
22	7	•	•	=I,III; ⌓'I ⌓° III
23	7	•	•	=I; ⌓'I ⌓° III
24	6	•	•	=I
25	7	•	•	=I, ⌓'I
26	7	•	•	=I; ⌓'I ⊕ ok. 12^00 II
27	7	0.0	•	•°9^28-38; =I; ⊕ I
28	7	1.0	•	•° ok. 12^15-13^00 II
29	7	0.9	•	•° ok. 0^30-3^00
30	7	1.1	•	•° ok. 15^00
31				
Σ	—	67.9	—	UWAGI

Kraków, Obserw. Astr. UJ φ = 50°04' λ = 19°58' Lipiec - Juillet 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	90.6	90.6	90.6	90.6	10.5	14.4	13.4	12.9	17.1	10.4	94	68	69	77	0.8	5.3	4.8	3.6	10 ●	10	10	WSW 3	W 2	C 0
2	89.3	88.2	86.3	87.9	12.2	15.1	12.2	12.9	16.9	8.5	70	54	81	68	4.3	8.0	2.6	5.0	6 ⊙	4 ⊙	10 ●	WSW 2	WSW 4	SW 2
3	79.8	78.8	76.8	78.5	11.5	13.7	12.6	12.6	16.2	9.2	90	69	87	82	1.4	4.9	1.9	2.7	10 ●	10 ●	10	C 0	SSW 4	SW 1
4	77.1	77.4	79.0	77.8	9.6	15.3	12.0	12.2	17.1	9.1	87	40	60	62	1.6	10.5	5.5	5.9	9 ●⊙	7 ⊙	3	WNW 2	WNW 6	SSW 2
5	80.8	81.4	85.1	82.4	12.7	17.7	11.3	13.2	18.8	6.8	61	55	91	69	5.7	9.2	1.2	5.4	2 ⊙	10 ⊙	10 ●	SSW 2	SW 1	WNW 1
6	88.8	89.3	89.8	89.3	11.4	18.3	13.8	14.3	20.4	7.9	78	49	81	69	3.0	10.8	3.0	5.6	0 ⊙	9	5	SW 1	SW 3	C 0
7	90.0	89.8	91.2	90.3	13.3	18.4	14.7	15.3	20.4	10.5	78	60	67	68	3.3	8.5	5.5	5.8	10 ⊙	9	10	WSW 2	SW 2	W 5
8	92.3	92.6	93.8	92.9	11.5	14.9	12.6	12.9	17.5	9.9	89	74	87	83	1.3	4.3	1.9	2.6	10	8	7	W 2	WSW 3	C 0
9	94.7	93.7	92.4	93.6	12.6	19.2	14.3	15.1	20.0	10.8	82	54	84	73	2.6	10.2	2.5	5.1	8 ⊙	7	8	SW 1	WSW 3	C 0
10	90.6	89.3	87.8	89.2	12.2	22.2	17.5	17.4	25.2	9.1	86	39	63	63	2.0	16.4	7.4	8.6	2 ⊙	4 ⊙	1	W 1	WSW 5	C 0
11	87.6	85.3	83.9	85.6	15.2	25.7	17.9	19.2	25.9	9.8	72	37	94	68	4.8	21.0	1.2	9.0	3 ⊙	3 ⊙	7	C 0	SW 2	C 0
12	84.1	83.7	83.4	83.7	16.8	22.6	17.3	18.5	25.1	15.1	89	49	78	72	2.1	13.9	4.3	6.8	9 ⊙	5 ⊙	9	SW 1	W 3	C 0
13	82.6	83.4	84.2	83.4	15.9	14.8	14.1	14.7	19.6	13.4	82	77	87	82	3.3	3.8	2.2	3.1	4 ⊙	10 ●	2	W 1	NW 1	WSW 1
14	84.3	83.7	83.2	83.7	14.0	17.3	15.2	15.4	18.2	12.6	79	64	87	77	3.4	7.1	2.3	4.3	10	10	10	WSW 1	WSW 4	SW 1
15	82.5	80.4	81.0	81.3	13.4	18.3	15.2	15.5	22.3	10.9	92	73	98	88	1.3	5.6	0.4	2.4	10	10 ●	10 ●	C 0	SSW 3	S 2
16	80.9	81.8	82.4	81.7	14.9	19.3	16.1	16.6	21.4	11.9	94	69	95	86	0.9	7.0	1.0	3.0	9	10 ●R	6	C 0	WNW 4	C 0
17	84.1	85.3	86.7	85.4	15.1	19.8	14.7	16.1	20.0	12.6	85	73	94	84	2.6	6.1	0.9	3.2	8 ⊙	10	10 ●	C 0	NNE 3	WNW 1
18	87.1	86.7	87.5	87.1	14.3	16.2	15.7	15.5	18.9	13.9	90	95	97	94	1.6	1.0	0.6	1.1	10 ●	10 ●	10 ●	NW 1	WSW 1	C 0
19	87.2	88.1	90.2	88.5	14.3	16.3	17.0	16.2	19.5	14.0	98	90	81	90	0.4	1.9	3.8	1.7	10 ●	10 ●	7	C 0	WNW 3	W 2
20	92.0	91.2	92.4	91.9	15.5	23.4	17.5	18.5	25.1	13.6	87	47	89	74	2.3	15.3	2.2	6.6	3 ⊙	4 ⊙	2	C 0	NW 1	C 0
21	92.0	89.5	88.9	90.1	16.3	26.5	20.9	21.2	27.0	12.1	81	48	81	70	3.4	18.2	4.7	8.8	0 ⊙	0 ⊙	0	C 0	ESE 2	ENE 1
22	91.1	90.4	90.0	90.5	19.2	28.2	22.0	22.8	28.5	14.6	81	45	67	64	4.2	21.1	8.7	11.3	1 ⊙	8 ⊙	10 (R)	C 0	ESE 2	SSE 6
23	92.1	92.4	93.8	92.8	17.7	22.5	19.3	19.7	24.3	16.9	95	76	75	82	1.0	6.5	5.6	4.4	10 ●═	9 ●	4	SW 1	SE 1	NW 1
24	96.7	96.7	97.4	96.9	16.8	21.6	16.1	17.6	22.4	16.1	79	47	73	66	4.1	13.6	4.9	7.5	8 ⊙	7 ⊙	2	W 1	WNW 3	C 0
25	98.3	96.8	95.4	96.8	15.2	23.2	17.9	18.6	24.3	10.9	77	47	76	67	4.1	15.0	5.0	8.0	0 ⊙	0 ⊙	1	C 0	C 0	NNE 1
26	93.7	91.8	91.3	92.3	17.7	29.4	22.0	22.8	31.1	12.3	76	37	79	64	4.7	25.8	5.5	12.0	0 ⊙	0 ⊙	2	C 0	SSW 2	C 0
27	90.4	89.3	90.0	89.9	21.0	30.4	22.2	24.0	30.9	17.7	81	44	83	69	4.7	24.4	4.7	11.3	9	4 ⊙	9 ●	C 0	SW 2	C 0
28	94.1	93.0	92.1	93.1	14.8	19.5	16.3	16.7	22.5	14.2	71	48	66	62	4.8	11.8	6.3	7.6	9	6	7	WNW 3	WNW 2	NW 1
29	94.7	93.6	93.7	94.0	13.7	18.6	13.4	14.8	20.0	9.7	75	46	77	66	3.9	11.6	3.5	6.3	4 ⊙	7 ⊙	1	NNW 1	N 1	C 0
30	94.1	93.3	94.0	93.8	12.5	20.2	15.8	16.1	21.0	7.6	78	41	69	63	3.2	14.1	5.5	7.6	8	10 ⊙	2	C 0	NE 2	NNE 1
31	94.7	94.0	93.7	94.1	14.0	22.0	15.4	16.7	22.9	8.8	73	43	82	66	4.3	15.1	3.2	7.5	5 ⊙	4 ⊙	1	C 0	ENE 1	C 0
M	89.0	88.4	88.6	88.7	14.4	20.2	16.0	16.6	21.9	11.6	82	57	81	73	2.9	11.2	3.6	5.9	6.4	6.9	6.0	0.8	2.5	0.9

Sierpień - Août

1	93.0	91.6	92.1	92.2	14.7	24.0	19.3	19.3	25.4	10.5	71	47	67	62	4.8	15.8	7.4	9.3	2 ⊙	4 ⊙	9	C 0	WSW 3	C 0
2	91.5	90.7	89.2	90.5	16.4	25.3	18.7	19.3	25.0	14.5	80	39	74	64	3.6	17.4	5.8	8.9	9	7 ⊙	0	WNW 1	SW 3	C 0
3	87.2	88.5	89.6	88.4	16.5	18.0	18.8	18.0	22.8	12.5	79	86	90	85	4.1	2.8	2.1	3.0	10 ⊙	10	10 ●	C 0	ENE 3	NNE 3
4	90.0	89.4	89.1	89.5	16.1	26.9	21.3	21.4	29.3	15.9	99	52	83	78	0.2	17.1	4.3	7.2	10═	0 ⊙	3	NE 1	SW 2	WSW 1
5	88.9	85.5	84.3	86.2	19.8	27.4	17.9	20.8	28.2	16.6	85	50	97	77	3.5	18.1	0.6	7.4	9 ⊙	1 ⊙	7	C 0	E 3	C 0
6	85.6	86.1	86.5	86.1	17.7	25.4	19.9	20.7	26.5	15.6	93	57	88	79	1.4	14.0	2.8	6.1	3 ⊙	10 ●R	4	C 0	WNW 3	NNE 1
7	83.2	78.8	84.4	82.1	19.2	32.3	20.2	23.0	33.0	15.7	86	28	74	63	3.2	34.9	6.3	14.8	0 ⊙	2 ⊙	10	NNE 2	SE 6	WSW 5
8	90.5	91.5	93.3	91.8	16.1	22.3	18.8	19.0	24.0	15.3	71	45	72	63	5.2	14.7	6.1	8.7	2 ⊙	2 ⊙	9	SW 1	NE 3	C 0
9	96.2	96.1	97.4	96.6	16.8	21.8	17.5	18.4	22.6	15.5	85	52	68	68	2.9	12.5	6.4	7.3	7 ⊙	8 ⊙	8	C 0	NNW 3	N 2
10	96.5	95.4	91.4	93.8	17.7	22.9	17.7	19.0	24.5	11.3	69	53	83	68	6.2	13.2	3.4	7.6	7 ⊙═	0 ⊙	7	E 3	E 4	C 0
11	91.6	90.9	91.7	91.4	17.2	25.4	18.3	19.8	26.9	13.7	79	51	85	72	4.1	16.0	3.0	7.7	0 ⊙	9 ⊙	5	C 0	SW 4	C 0
12	92.7	91.6	91.2	91.8	16.8	27.4	20.6	21.4	29.4	12.7	80	54	87	74	3.9	16.7	3.1	7.9	2 ⊙	2 ⊙	6	C 0	SW 2	W 1
13	92.1	91.5	91.1	91.6	19.2	30.5	21.4	23.2	30.8	15.0	82	55	92	76	4.0	19.7	2.1	8.6	3 ⊙	9 ⊙	7	C 0	W 3	C 0
14	91.6	91.2	90.3	91.0	19.0	21.9	20.6	20.5	26.2	15.9	87	81	90	86	3.0	5.1	2.4	3.5	0 ⊙	9	2	NNW 3	SSE 2	C 0
15	87.8	86.6	85.0	85.8	16.7	25.4	23.1	22.1	28.4	16.2	100	73	90	88	0.0	8.7	2.9	3.9	10═	10 ⊙	10	ENE 1	E 3	C 0
16	85.8	85.9	87.3	86.3	17.9	21.1	17.1	18.3	23.1	16.9	96	78	96	90	0.8	5.6	0.8	2.4	10 ●	10 ⊙	4	S 1	WSW 4	C 0
17	88.3	87.2	85.4	87.0	16.0	25.2	18.4	19.5	26.0	13.4	92	55	88	78	1.6	14.5	2.5	6.2	1 ⊙	9 ⊙	10	SW 1	E 1	W 1
18	84.2	86.0	89.8	86.7	16.3	21.4	15.7	17.3	22.3	15.2	95	68	69	77	1.0	8.2	5.5	4.9	10 ⊙	7 ⊙	9	C 0	WSW 4	W 2
19	89.8	89.6	90.5	90.0	13.3	16.5	13.0	14.0	17.6	12.7	79	55	77	70	3.2	8.5	3.5	5.1	10 ●	10	10	W 1	WNW 5	W 5
20	88.9	89.8	89.8	89.5	13.3	15.7	14.5	14.5	16.7	11.5	86	75	87	83	2.1	4.4	2.2	2.9	9	10	9	WSW 5	SW 4	WSW 3
21	89.1	88.4	88.4	88.6	14.7	18.7	14.5	15.6	20.5	13.7	90	70	93	84	1.6	6.5	1.1	3.1	10	10	4	C 0	C 0	C 0
22	89.7	91.3	91.1	90.7	13.0	15.5	13.0	13.6	18.0	9.8	93	95	98	95	1.1	0.9	0.4	0.8	10	10	3	S 1	C 0	C 0
23	91.1	92.2	92.3	91.9	13.3	20.7	14.3	15.6	21.5	10.5	91	43	86	73	1.4	13.9	2.4	5.9	9 ⊙	5 ⊙	7	C 0	SW 5	C 0
24	90.8	87.3	84.7	87.6	15.4	23.0	17.1	18.2	24.8	12.3	85	48	86	73	2.6	14.7	2.8	6.7	10	9	3	C 0	SSW 4	C 0
25	88.3	88.6	92.6	89.8	16.9	20.2	13.9	16.2	21.6	13.4	88	70	91	83	2.3	7.1	1.5	3.6	10	10	9	W 1	WSW 1	C 0
26	95.5	95.9	95.1	95.5	13.0	19.4	12.7	14.4	21.3	11.1	75	44	84	68	3.8	12.6	2.4	6.3	4 ⊙	2 ⊙	2	W 1	WSW 2	C 0
27	91.1	87.5	87.6	88.7	11.1	26.2	17.7	18.2	27.8	7.3	84	48	80	71	2.1	17.5	4.0	7.9	1 ⊙	2 ⊙	7	C 0	WSW 2	C 0
28	94.0	93.6	93.8	93.8	15.6	20.0	13.5	15.6	21.3	13.5	56	55	75	55	7.7	15.2	3.9	8.9	7 ⊙	8 ⊙	0	WNW 4	WSW 5	WNW 1
29	93.3	91.4	91.1	91.9	10.1	23.2	17.0	16.8	24.7	7.7	87	56	80	68	1.6	18.1	3.9	7.9	10═	6 ⊙	7	C 0	WSW 4	C 0
30	94.1	95.4	94.8	94.8	13.7	17.7	9.9	12.8	18.8	9.9	86	42	84	71	2.2	11.7	1.9	5.3	9	8 ⊙	4	WSW 5	W 6	C 0
31	92.1	88.4	89.9	90.1	10.1	18.8	13.3	14.0	19.2	7.1	82	48	61	63	2.4	11.3	6.0	6.6	4 ⊙	10	8	W 1	WSW 5	SW 3
M	90.5	89.7	90.0	90.1	15.6	22.5	17.1	18.1	24.1	13.0	84	56	83	74	2.8	12.8	3.3	6.3	6.4	6.7	6.2	1.0	3.2	0.8

Kraków, Obserw. Astr. UJ H_s=206m H_w=219,8m h_w=10m Lipiec - Juillet 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBE ŚNIEGU h	POGODA
1	6	0.0	•	•$^{1-0}3^{30}$-na •1; =1
2	7	2.9	•	•'17^{35}-18^{15}; 21^{25}-22^{05}; ⟨°17^{33-48} N-NE; =III
3	7	1.9	•	•$^{1-0}0^{05}$-7^{55} •$^{2}9^{30-40}$ •°-p
4	8	0.0	•	•°1
5	8	2.5	•	•'17^{45}-ok. 22^{00}; ⊕II
6	8	•	•	⌓°III
7	7	1.9	•	•°9^{05}-ok. 10^{00}; ok. 16^{25-45} •'22^{05}-23^{00}; =1
8	6	1.8	•	•°4^{10-40} •'11^{25-40} •°11^{53}-ok. 12^{00} •$^{2-0}15^{20-27}$; ⟨°14^{20-31} ⟨'15^{18-40} SW-NE; =1
9	7	•	•	=1
10	7	•	•	=1; ⌓^{2}1 ⌓°III
11	7	1.5	•	•°ok. 15^{00-50} •'ok. 19^{30}-20^{05}; ⟨°20^{20-40}; =1; ⌓°1
12	7	1.0	•	•°0^{30}-1^{25} •^{2}-1^{30}; ⟨III; =1
13	7	3.9	•	•°12^{30} •$^{2}13^{00-15}$ •'13^{25-40}; II •$^{2}14^{00-15}$; (⟨) 12^{30} ⟨ 14^{00-15}
14	7	0.2	•	⚲ ok. 15^{00} •° ok. 22^{30}
15	7	17.3	•	•'13^{30}-14^{50} •$^{2-1}17^{00}$-22^{30}; ⟨ 17^{00} ⟨ $^{2}21^{00-30}$
16	5	0.2	•	•'13^{35-50}; ⟨' 13^{21-40}; =I, II, ⌓'III
17	7	57.9	•	•°15^{45}-16^{00} •$^{2}18^{30}$-np; ⟨°17^{55} SE; ⟨' 20^{30}; ⌓'1
18	5	28.4	•	•'na-8^{45} •$^{0-2}$... np; =I, II
19	6	8.4	•	•$^{2-0}$na-17^{00}; =1
20	7	•	•	=1
21	7	•	•	=1; ⌓^{2}1 ⌓III
22	7	17.0	•	⟨°21^{10}-np ⟨' 22^{11}-23^{25}; ⌓1
23	7	0.9	•	•°na-a, ok. 13^{00-20} •$^{2}13^{43}$-14^{00} ⚲'15^{00-10}; ≡°1; ⌓°III
24	7	•	•	=1; ⌓°1 ⌓'III
25	8	•	•	=1; ⌓^{2}1, III
26	7	•	•	=1; ⌓^{2}1
27	7	0.0	•	•°19^{25-35}; 21^{32}-22^{05}; =1; ⌓'1
28	7	•	•	
29	8	•	•	⌓1 ⌓°III; ⊕II
30	8	•	•	=1; ⌓^{2}1; ⊕II
31	8	•	•	⌓^{2}1
Σ	—	147.7	—	UWAGI.

Sierpień - Août

1	6	•	•	⌓'1
2	7	•	•	=1; ⌓°1, III
3	5	3.3	•	•°10^{03-06} •'10^{16-22} •^{2}-10^{25} •'-10^{52}; III; =I, II, III; ⌓'1
4	6	•	•	≡^{2}1 = III
5	7	13.8	•	•°16^{47}-17^{05} •$^{2}17^{55}$-18^{25} •°19^{15-32}; (⟨) S 16^{50} ⟨' ok. 18^{30} = I, III; ⌓'1
6	7	0.0	•	•°⟨°II; = I, III
7	8	0.7	•	•'19^{30-37}; ⌓'1
8	8	•	•	
9	7	•	•	=1
10	8	•	•	≡°1; ⌓°III
11	7	•	•	=1; ⌓'1 ⌓°III
12	7	•	•	=I, III; ⌓'1 ⌓°III
13	7	•	•	=I, III; ⌓'1 ⌓°III
14	7	0.8	•	•°12^{10-15} •'12^{29-33} •°-ok. 13^{00}; =1; ⌓°1 ⌓III
15	7	4.5	•	≡°1-a
16	5	10.0	•	•'3^{30}-4^{30} •$^{2}6^{55}$-ok. 9^{00} •'-10^{20}; 12^{30-35}; ⟨°na = I, II, III
17	8	•	•	=1; ⌓^{2}1
18	6	0.0	•	•°15^{00-30}; =1; ⌓'1
19	7	1.1	•	•°7^{15}-ok. 8^{00}
20	6	0.0	•	•'0^{10-18}; 6^{00-25} •-7^{30}; =1
21	6	•	•	=1; ⌓'III
22	4	1.5	•	•°ok. 11^{00} •°12^{35}-ok. 13^{00}; =1 ≡° ok. 10^{30} = II, III
23	7	•	•	=I, III; ⌓^{2}1 ⌓°III
24	8	1.9	•	=1; ⌓°III
25	6	0.0	•	⚲°13^{40-40}; = III; ⌓^{2}III
26	7	•	•	=1; ⌓°1 ⌓'III
27	7	•	•	⚲°21^{45}; =1; ⌓^{2}1
28	8	•	•	⌓III
29	7	0.4	•	⚲° ok. 18^{40}; ok. 21^{15} •° ok. 23^{00}-24; ≡°1
30	7	•	•	•°0^{00}-ok. 2^{00}; =1; ⌓°III
31	7	•	•	
Σ	—	38.0	—	UWAGI.

Kraków, Obserw. Astr. UJ φ = 50°04' λ = 19°58' Wrzesień - Septembre 1962

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	91.9	95.9	96.4	94.0	10.7	16.5	11.7	12.6	17.6	9.9	89	49	87	75	1.5	9.6	1.8	4.3	10	6 ⊙	9	W 2	WNW 5	C 0
2	99.2	98.2	96.1	97.8	9.6	20.4	12.9	14.0	21.2	7.2	89	39	85	71	1.3	14.6	2.3	6.1	0 ⊙	2 ⊙	1	W 1	SSW 1	C 0
3	95.2	93.4	91.9	93.5	10.1	24.2	15.6	16.4	25.8	6.7	86	34	82	67	1.8	19.9	3.2	8.3	0 ⊙	0 ⊙	0	C 0	WSW 1	C 0
4	90.0	87.2	84.1	87.1	11.9	28.1	13.0	19.0	29.3	8.8	85	37	83	68	2.0	25.9	3.4	9.8	0 ⊙	0 ⊙	3	C 0	E 2	C 0
5	80.2	83.1	83.9	82.4	15.8	23.7	15.4	17.6	25.6	12.2	75	54	88	72	4.4	13.6	2.1	6.7	1 ⊙	10 ○	3	C 0	W 6	WSW 1
6	84.1	83.8	81.1	83.0	12.8	20.0	17.9	17.2	20.3	10.1	95	66	84	82	0.7	8.0	3.2	4.0	10 ●	9	8 ☂	C 0	WSW 5	SW 1
7	77.4	77.5	81.4	78.8	19.9	16.9	14.9	16.6	20.7	14.8	71	88	79	79	6.7	2.3	3.4	4.1	10 ●	10 ●	8	SW 4	SSW 4	SW 1
8	85.4	85.0	88.1	86.2	13.3	18.1	10.7	13.2	19.2	10.5	87	61	96	81	2.0	8.1	0.5	3.5	10	8 ● ⊙	7	SW 1	SW 4	WNW 1
9	93.8	96.6	98.5	96.3	10.1	13.3	9.1	10.4	15.9	8.3	90	66	93	83	1.3	5.2	0.8	2.4	7 ⊙	5 ⊙	7	WSW 3	WNW 3	W 1
10	97.2	94.5	92.6	94.8	5.9	21.3	13.7	13.6	23.3	3.8	94	42	76	71	0.6	14.8	3.7	6.4	8 ⊙	0 ⊙	8	W 1	ESE 4	W 1
11	90.2	89.0	93.8	91.0	10.6	23.8	15.9	16.6	25.0	7.2	85	46	82	71	2.0	15.9	3.3	7.1	8 ⊙	9 ⊙	0	C 0	SSW 4	SSW 2
12	92.7	88.0	81.4	87.4	12.2	25.7	24.6	21.8	27.1	10.2	98	43	50	64	0.3	18.7	15.3	11.4	10	3 ⊙	7	C 0	SSW 4	SSW 5
13	88.0	92.0	95.2	91.7	17.3	13.7	10.5	13.0	24.6	10.3	64	76	90	77	7.1	3.7	1.3	4.0	9	10	5	W 3	S 3	WSW 1
14	98.3	99.5	99.3	99.0	8.9	13.7	6.4	8.8	15.4	6.2	84	47	92	74	1.8	8.3	0.7	3.6	10	7 ⊙	2	SW 4	W 5	C 0
15	95.9	93.3	89.8	95.0	5.4	18.8	10.6	11.4	20.2	2.7	86	41	92	73	1.3	12.7	1.0	5.0	4 ⊙	8 ⊙	7 ≡	C 0	NE 1	C 0
16	88.1	85.3	83.9	85.8	7.6	24.1	13.6	14.7	25.8	4.7	90	40	87	72	1.0	17.9	2.0	7.0	0 ⊙	0 ⊙	1	C 0	C 0	W 1
17	84.3	82.6	82.3	83.1	11.9	16.7	13.7	14.0	17.9	8.5	95	84	98	92	0.7	3.1	0.4	1.4	10	10 ●	10 ●	C 0	NE 2	C 0
18	82.3	80.3	80.6	81.1	11.0	11.6	10.5	10.9	13.9	10.2	97	96	94	96	0.3	0.5	0.8	0.5	10 ☂	10 ●	10	WSW 1	N 1	SW 4
19	85.9	88.1	90.2	88.1	8.5	12.1	6.7	8.5	14.3	6.5	92	73	97	87	0.9	3.8	0.3	1.7	10	9	7	SW 1	WSW 2	W 1
20	92.5	92.6	92.7	92.6	4.4	15.3	7.9	8.9	15.9	3.7	98	60	93	84	0.2	7.0	0.7	2.6	4 ≡ ⊙	3 ⊙	6	C 0	SW 3	C 0
21	94.0	93.1	92.5	93.2	6.8	13.1	10.2	10.1	14.3	4.6	93	62	80	78	0.8	5.8	2.5	3.0	8	9 ⊙	10	WSW 2	W 4	WSW 4
22	91.3	92.9	94.6	92.9	8.7	10.1	9.5	9.4	13.9	7.9	96	76	86	86	0.4	3.0	1.7	1.7	10	8 ⊙	8	SW 1	NW 4	W 3
23	93.3	91.9	91.4	92.2	8.4	11.0	8.0	8.8	11.3	7.9	97	75	99	90	0.3	3.2	0.1	1.2	10	10	10 ●	WSW 2	W 4	WSW 3
24	94.8	97.2	100.1	97.4	8.8	12.0	7.9	9.2	12.4	7.5	95	69	96	87	0.6	4.3	0.4	1.8	10	7 ⊙	9	WSW 1	SSW 3	C 0
25	103.6	103.4	100.8	102.6	4.9	11.0	8.3	8.1	12.9	3.0	100	81	96	92	0.0	2.4	0.5	1.0	10 ≡	9 ⊙	4	NE 1	NE 5	C 0
26	97.9	96.0	95.2	96.4	4.9	16.0	8.7	9.6	16.3	3.0	98	56	89	81	0.2	8.0	1.2	3.1	3 ≡ ⊙	2 ⊙	0	ENE 2	E 6	ENE 2
27	92.2	89.5	89.0	90.2	3.1	12.5	11.4	9.6	15.4	1.7	98	77	88	88	0.1	3.4	1.7	1.7	10 ≡	5 ⊙	10	C 0	NE 2	ENE 4
28	88.2	87.5	87.1	87.6	9.7	11.2	11.7	11.1	12.5	9.4	97	92	94	94	0.3	1.0	0.8	0.7	10 ≡	10	10	C 0	E 1	C 0
29	87.7	87.6	90.4	88.6	9.9	16.0	10.7	11.3	17.5	9.5	100	78	99	92	0.0	4.0	0.2	1.4	10 ≡	4 ⊙	9	C 0	NE 1	C 0
30	92.5	93.2	94.5	93.4	7.7	18.6	11.0	12.1	19.7	7.4	100	68	96	88	0.0	6.8	0.5	2.4	10 ≡	4 ⊙	4	C 0	E 1	C 0
31																								
M	90.9	90.5	90.6	90.7	9.7	17.0	11.9	12.6	18.8	7.5	91	63	88	81	1.4	8.4	2.0	3.9	7.4	6.2	6.1	1.0	3.0	1.2

Październik - Octobre

1	96.4	96.7	98.2	97.1	7.2	17.2	12.3	12.2	19.0	6.7	100	79	94	91	0.0	4.1	0.9	1.7	10 ≡	0 ⊙	0 ≡	C 0	E 2	NE 1
2	99.3	99.9	99.3	99.5	8.3	16.0	13.7	12.9	17.8	7.6	100	83	91	91	0.0	3.1	1.5	1.5	10 ≡	3 ⊙	0	C 0	ENE 4	NE 3
3	98.7	98.8	98.5	98.7	9.5	11.5	9.1	9.8	13.8	8.4	100	99	100	100	0.0	0.2	0.0	0.1	10 ≡	10 ≡	5 ≡	NE 1	E 1	NNE 1
4	98.3	98.1	97.6	98.0	8.5	11.1	9.4	9.6	11.6	7.5	100	96	100	99	0.0	0.5	0.0	0.2	10 ☂ ≡	10 ≡	10 ☂ ≡	NNE 1	NE 1	ENE 1
5	95.9	96.1	97.4	96.5	8.6	12.1	10.6	10.5	12.6	8.1	100	93	100	98	0.0	1.0	0.0	0.3	10 ≡	10 ≡	10 ≡	C 0	ENE 1	ENE 1
6	97.2	97.9	100.7	98.6	11.7	14.1	12.4	12.6	14.3	10.2	99	91	95	95	0.1	1.5	0.7	0.8	10 ≡	10 ≡	7 ≡	C 0	NNW 1	NE 1
7	102.5	103.7	105.7	104.0	7.9	16.7	9.8	11.0	17.9	7.6	100	65	93	86	0.0	6.6	0.3	2.5	6 ≡ ⊙	8 ⊙	0	C 0	NE 2	NNE 1
8	106.9	107.9	107.7	107.5	8.9	11.0	8.6	9.3	11.3	7.8	88	92	100	93	1.4	1.0	0.0	0.8	10 ≡	10	10 ≡	NE 3	E 1	ENE 1
9	106.3	104.6	103.4	104.8	9.7	14.9	8.6	10.4	15.7	7.8	99	70	97	89	0.1	5.0	0.3	1.8	10	0 ⊙	0	ENE 2	E 1	NE 1
10	100.9	99.0	97.3	99.1	6.7	11.6	6.4	7.8	12.9	6.1	100	77	97	91	0.0	3.1	0.3	1.1	10 ≡	4 ⊙	5	E 1	ENE 2	C 0
11	95.2	92.7	90.6	92.8	3.1	11.3	7.3	7.2	15.1	2.3	100	82	100	94	0.0	2.5	0.0	0.8	10 ≡	3 ⊙	0 ≡	C 0	C 0	C 0
12	89.6	89.8	94.2	91.2	4.1	18.5	7.3	9.3	18.5	2.8	100	55	86	80	0.0	9.6	1.5	3.7	0 ≡ ⊙	2 ⊙	10	C 0	WSW 1	NNE 1
13	94.5	94.2	91.5	93.4	6.6	9.0	8.4	8.1	9.2	6.3	91	86	96	91	0.8	1.6	0.4	0.9	10	10	10	NE 3	NE 4	ENE 3
14	86.0	87.2	91.7	88.3	5.8	12.1	7.7	8.3	13.8	5.5	100	76	94	90	0.0	3.3	0.6	1.3	10 ≡	9 ⊙	10 ☂	C 0	W 4	W 2
15	93.9	96.9	100.0	96.9	7.4	7.3	3.0	5.2	9.3	2.7	94	87	98	93	0.6	1.4	0.2	0.7	10 ≡ ☂	10	3 ≡	WSW 1	NE 2	NNE 1
16	99.0	96.4	97.1	97.5	-0.3	10.3	1.8	3.4	10.8	-0.4	100	59	89	83	0.0	5.2	0.8	2.0	10 ≡	6 ⊙	3 ≡	C 0	ESE 2	NNE 1
17	97.7	98.6	98.5	98.3	1.1	9.7	7.3	6.4	11.8	-0.3	96	73	93	87	0.2	3.2	0.7	1.4	8 ≡ ⊙	9	10 ≡	W 1	SSW 1	C 0
18	97.6	95.7	90.9	94.7	8.1	12.4	7.6	8.9	13.1	7.0	89	72	87	83	1.2	4.0	1.3	2.2	10 ≡	10	0	SW 1	SW 2	WSW 2
19	87.4	88.2	89.7	88.4	9.9	10.2	8.0	9.0	11.4	7.2	76	92	85	84	3.0	0.9	1.3	1.8	9 ⊙	9 ≡	9	WSW 3	SW 3	SW 2
20	90.8	93.9	99.1	94.6	7.7	12.7	9.0	9.6	13.4	7.3	96	62	76	78	0.5	5.5	2.8	2.9	10 ●	4 ⊙	9	SW 1	WNW 5	NW 1
21	103.9	104.2	103.7	103.9	1.8	10.0	3.1	4.5	11.8	1.4	94	66	95	85	0.4	4.2	0.4	1.7	1 ⊙	0 ⊙	0	C 0	N 1	NW 1
22	103.8	102.3	101.6	102.6	-0.7	14.3	3.9	5.4	14.8	-1.2	98	60	97	85	0.1	6.5	0.3	2.3	0 ≡ ⊙	0	0 ≡	C 0	SW 1	SSW 1
23	100.0	98.6	97.9	98.8	0.3	14.0	4.3	5.7	15.4	-0.6	100	59	93	84	0.0	6.6	0.5	2.4	0 ≡ ⊙	0 ⊙	0 ≡	C 0	W 3	C 0
24	96.4	95.1	95.3	95.7	-0.9	14.6	5.0	5.9	15.1	-1.1	100	59	97	85	0.0	6.8	0.3	2.4	0 ≡ ⊙	0 ⊙	0	C 0	WSW 3	C 0
25	96.0	94.5	94.0	94.8	1.0	10.6	3.9	4.8	11.1	0.4	100	73	97	90	0.0	3.3	0.3	1.3	10 ≡	0 ⊙	0	C 0	E 1	ENE 1
26	92.9	91.6	90.7	91.7	-0.5	10.1	4.3	4.6	13.2	-1.6	100	77	97	91	0.0	2.9	0.3	1.1	10 ≡	0 ≡ ⊙	0 ≡	C 0	C 0	C 0
27	87.3	87.4	89.9	88.2	-1.1	15.8	7.3	7.3	16.9	-2.3	98	58	90	82	0.1	7.4	1.0	2.8	2 ≡ ⊙	3 ⊙	8	C 0	WNW 1	C 0
28	87.4	85.4	84.1	85.6	2.3	8.6	8.8	7.1	9.5	1.6	100	84	88	91	0.0	1.9	1.4	1.1	10 ≡	8 ≡ ⊙	10	C 0	C 0	W 1
29	84.2	85.2	90.2	86.3	4.3	5.2	5.3	5.1	8.8	4.3	98	92	94	95	0.1	0.7	0.6	0.5	10 ☂ ≡	10	10	SW 1	NNW 3	NW 1
30	91.8	90.8	87.2	89.9	5.5	7.1	6.0	6.2	7.3	4.9	95	87	89	90	0.4	1.3	1.1	0.9	10 ≡	10	10	C 0	W 1	NE 2
31	84.6	83.0	81.7	83.1	3.6	6.9	8.0	6.6	8.4	2.8	97	92	100	96	0.3	0.7	0.0	0.3	10 ≡	10	10 ≡	C 0	C 0	NNE 2
M	95.6	95.3	95.7	95.5	5.0	11.8	7.4	7.9	13.1	4.1	97	77	94	89	0.3	3.4	0.7	1.5	7.9	5.7	5.2	0.6	1.7	1.1

Krakow, Obserw. Astr. UJ H_s=206m H_t=219,8m h_w=10m Wrzesień - Septembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBSZE GOŁOŚ h	POGODA
1	7	0.6	•	•' 7^{40-55}, 10^{18-30}, ok. 15^{30}, 17^{15-25}; = I
2	8	•	•	= I; ⌓° III
3	8	•	•	= I
4	7	•	•	= I; ⌓' I ⌓° III
5	7	2.6	•	•° II, 13^{48-55} •' - 14^{00} •° ok. 17^{00-20}; = I; ⌓' I
6	8	0.0	•	•° na - a, p • III; = I
7	7	3.5	•	•° I, ok. 11^{20} - 12^{45} •' - 14^{00} •° - 15^{30}
8	8	8.5	•	•' III •² 14^{45-55}, 22^{50} - 23^{00} •' - 24; = I
9	7	0.1	•	•' 0^{00} - 2^{40}; = I
10	8	•	•	= III
11	8	3.0	•	= I; ⌓² I ⌓° III
12	8	•	•	•' 17^{25-40}, 18^{50} - 19^{20}; = I, III; ⌓² I
13	5	0.1	•	= I
14	7	•	•	•° a; = I
15	8	•	•	= I; ⌓° I ⌓ III
16	8	•	••	= I ≡° III, ⌓² I ⌓° III
17	4	13.1	•	•°-² 13^{05} - 23^{50}; = I, II, III; ⌓' I
18	5	18.2	•	• 5^{10} - a •'-² 10^{00} - 18^{50}; = I, II
19	7	•	•	
20	7	•	•	≡° I; ⌓' I
21	7	2.1	•	= I; ⌓² I ⌓° III
22	7	0.5	•	•' II 11^{30-40} •° ok. 13^{25}; = I, III
23	7	10.1	•	•² 14^{40} - 16^{10} •' - ok. 18^{00}, III; = III
24	7	0.0	•	= I
25	7	•	•	≡² I = I; ⌓² III
26	8	•	•	≡° I, ⌓²
27	7	•	•	≡² I = III; ⌓° I, III
28	5	•	•	≡° I = II, ⌓° I
29	4	0.1	•	≡' I = II, III, ⌓° I ⌓² III
30	5	0.1	•	• p, ≡² I = II, III; ⌓² I, III
31				
Σ	—	62.6	—	UWAGI

Październik-Octobre

1	5	0.1	•	• p; ≡² na - ok. 10^{00} = II ≡° III; ⌓' III
2	5	0.2	•	• na; ≡² na - a = II
3	5	0.2	•	• na ≡² na - a ≡° - p ≡° - np
4	5	0.5	•	• na, I, III; ≡² na - a ≡° - p ≡² - np
5	5	0.1	•	• na; ≡² na - a ≡° - p ≡² - np; ⌓' III
6	5	0.1	•	• 8^{05-45}; ≡' na - a ≡° - np
7	7	•	•	• p; ≡² I; ⌓' I ⌓° III
8	5	0.0	•	≡' na - a = II ≡° III; ⌓' III; • p
9	7	0.1	•	• na; ≡² na - a = II - np
10	5	0.1	•	• na; ≡² na - a = a - np
11	4	0.0	•	•° p; ≡² na - ok. 10^{00} = II ≡° III; ⌓² III
12	5	•	•	≡° na - a = II; ⌓² I
13	5	•	•	= na - np
14	5	0.1	•	• ok. 20^{00} - np; ≡² na - a = II, III
15	7	0.5	•	• I •° 10^{00} - 11^{00}; ≡° na - a ≡° III
16	8	•	•	≡² na - ok. 9^{45} ≡° - 10^{15} ≡° III; ⌓² I
17	5	•	•	≡° na - a = II ≡° III; ⌐° I; ⌓° III
18	6	•	•	≡° I
19	5	0.7	•	•° 8^{20} - ok. 9^{00}, ok. 12^{00}; = I ≡° II
20	7	0.5	•	•° ok. 5^{00} - ok. 8^{00}; = I
21	7	•	•	= I, III; ⌓° III
22	7	•	•	≡' I ≡° III; ⌐° I
23	5	•	•	≡' na - ok. 7^{30} = II ≡° III; ⌐° I
24	7	•	•	≡' na - ok. 7^{30} = III; ⌐' I; ⌓° III
25	5	•	•	≡² na - ok. 8^{00} = II, III
26	5	•	•	≡² na - a ≡' - ok. 9^{00} ≡° - np; ⌐° I; ⌓ III
27	5	•	•	≡° na - 8^{30} = II; ⌐' I
28	5	1.5	•	≡² na - a ≡' ; ok. 11^{30} ≡° - p = III; ⌓° I
29	5	0.2	•	• na - ok. 10^{00}, p; ≡° na - a = II, III
30	5	0.2	•	≡° I = II, II
31	4	3.1	•	•°-¹ 6^{15-40} •' do ok. 9^{30} • p; ≡° na - a II ≡' III
Σ	—	7.6	—	UWAGI

Kraków, Obserw. Astr. UJ φ = 50°04' λ = 19°58' Listopad - Novembre 1962

DNI	CIŚNIENIE Pw 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	78.6	79.4	80.7	79.6	7.3	9.0	7.2	7.7	9.0	6.9	100	96	97	98	0.0	0.5	0.3	0.3	10	10	10	ENE 3	WSW 1	SW 1
2	84.6	86.6	88.9	86.7	6.5	8.5	8.3	7.9	8.8	6.1	99	89	94	94	0.2	1.2	0.7	0.7	10	10	10	SW 1	SW 1	C 0
3	89.3	89.3	90.5	89.7	8.3	11.3	9.9	9.8	11.9	7.7	100	86	96	94	0.0	1.8	0.5	0.8	10	7 ⊙	10	C 0	NNE 2	NE 2
4	91.3	90.5	89.8	90.5	7.6	11.1	7.5	8.4	13.8	6.8	100	89	99	96	0.0	1.5	0.2	0.6	10	4 ⊙	0	E 1	ENE 1	C 0
5	89.4	87.6	86.5	87.8	1.1	15.5	8.9	8.6	17.0	0.7	100	61	86	82	0.0	6.9	1.5	2.8	10	0 ⊙	3	C 0	ENE 2	ENE 4
6	84.6	85.6	88.3	86.2	4.9	15.4	10.2	10.2	15.5	3.7	75	43	80	65	2.4	10.0	2.5	5.0	4 ⊙	10 ⊙	9	ENE 1	E 5	ENE 2
7	90.8	92.2	94.2	92.4	7.2	17.5	9.7	11.0	17.6	5.7	94	58	88	80	0.6	8.4	1.4	3.5	8	3 ⊙	0	NE 1	S 3	NNE 1
8	92.7	90.1	89.3	90.7	2.6	16.1	8.5	8.9	17.4	2.1	100	65	86	84	0.0	6.5	1.5	2.7	1	5 ⊙	4	NNE 1	NE 2	NNE 1
9	87.2	86.5	87.0	86.9	3.5	11.7	7.3	7.4	12.4	3.4	100	74	83	86	0.0	3.6	1.7	1.8	9	7	10	NNE 1	NNE 2	NNE 3
10	86.1	86.7	89.9	87.6	5.0	3.9	2.1	3.3	7.3	1.7	90	90	95	92	0.8	0.8	0.4	0.7	10	10 ●	10 ●	NE 5	NW 6	NE 4
11	91.2	91.3	90.8	91.1	1.1	2.4	4.6	3.2	4.8	0.9	94	96	97	96	0.4	0.3	0.3	0.3	10 ●	10 ●	10	NE 3	ENE 3	NE 4
12	88.5	87.8	91.8	89.4	3.6	4.7	5.3	4.7	5.4	3.4	95	95	97	96	0.4	0.4	0.3	0.4	10	10 ●	10	NE 6	NE 3	C 0
13	92.4	91.9	91.3	91.9	4.9	8.1	6.4	6.4	8.3	4.4	97	89	100	95	0.3	1.2	0.0	0.5	10	10	10 ●	WNW 1	NE 2	NE 1
14	90.9	91.1	92.2	91.4	4.1	4.9	5.1	4.8	6.4	3.7	100	100	98	99	0.0	0.0	0.2	0.1	10	10	10	NNE 1	NNE 1	C 0
15	88.5	83.6	79.6	83.9	4.4	5.8	6.2	5.6	7.2	3.8	100	98	94	97	0.0	0.1	0.6	0.2	10	10 ●	10 ●	C 0	ENE 2	W 3
16	82.4	85.1	86.4	84.6	3.2	3.3	2.4	2.8	6.5	2.2	88	71	79	79	0.9	2.2	1.6	1.6	10	10	10	WNW 2	W 4	W 3
17	89.3	88.7	85.4	87.8	0.7	3.5	-0.7	0.7	4.6	-0.8	86	55	92	78	0.9	3.5	0.5	1.6	9	3 ⊙	7	SW 2	C 0	NNE 3
18	80.3	78.3	74.4	77.7	-1.0	4.6	3.8	2.8	5.9	-1.6	87	67	82	79	0.7	2.9	1.5	1.7	5	9 ⊙	9	E 1	NE 4	NE 3
19	75.3	79.8	76.0	77.0	7.3	9.5	6.8	7.6	10.9	2.2	61	58	88	69	4.0	5.0	1.2	3.4	5	8	9	S 4	NW 2	ENE 5
20	77.7	77.0	82.7	79.1	4.9	3.9	1.4	2.9	7.0	0.6	98	95	92	95	0.2	0.4	0.6	0.4	10	10 ●	10 ●	SW 1	SW 4	WSW 3
21	84.8	84.2	82.7	83.9	1.3	1.7	1.3	1.4	2.0	0.9	89	81	87	86	0.8	1.3	0.9	1.0	10	10	10	C 0	ENE 2	NE 3
22	81.9	84.8	90.1	85.6	0.2	3.3	1.9	1.8	4.0	-0.1	100	93	93	95	0.0	0.5	0.5	0.3	10	9	10	C 0	C 0	WSW 2
23	93.9	95.2	97.0	95.4	0.2	-0.5	-1.2	-0.7	1.9	-1.4	98	98	97	98	0.1	0.2	0.2	0.2	10 *	10 *	10	C 0	C 0	C 0
24	98.8	99.6	102.0	100.1	-1.1	-0.3	-0.4	-0.6	0.0	-1.6	99	98	96	98	0.1	0.2	0.2	0.2	10	10	10	C 0	N 1	N 1
25	102.9	102.1	102.0	102.3	-0.3	0.5	0.7	0.4	1.0	-0.6	100	98	98	99	0.0	0.1	0.1	0.1	10	10	10	C 0	NNE 1	NW 1
26	103.0	103.3	103.6	103.3	0.8	1.3	1.2	1.1	1.7	0.5	100	98	98	99	0.0	0.1	0.2	0.1	10 ●	10	10 ●	C 0	WNW 1	W 1
27	104.5	105.9	103.8	104.7	0.7	1.3	0.9	1.0	1.6	0.3	98	98	98	98	0.1	0.1	0.1	0.1	10 ●	10	10	NW 1	C 0	C 0
28	100.3	99.5	100.0	99.9	0.2	2.0	0.9	1.0	2.2	0.1	92	76	83	84	0.5	1.7	1.1	1.1	10	3 ⊙	10	W 2	SSW 2	SW 2
29	98.5	97.7	95.9	97.4	0.9	2.3	2.9	2.2	2.9	0.4	87	84	96	89	0.9	1.2	0.2	0.8	10	10	10	SW 4	WSW 4	WSW 1
30	91.3	90.4	91.3	91.0	3.3	3.3	2.6	3.0	3.8	1.8	79	88	93	87	1.5	0.9	0.6	1.0	10	10	10	WSW 6	SW 5	WSW 3
31																								
M	89.7	89.7	90.1	89.8	3.1	6.2	4.4	4.5	7.3	2.1	93	83	92	89	0.5	2.1	0.7	1.1	9.0	8.3	8.7	1.6	2.2	1.9

Grudzień - Décembre

1	100.2	106.5	111.0	105.9	0.7	0.7	-0.3	0.2	2.9	-0.4	71	67	63	67	1.8	2.1	2.3	2.1	10	7	10	N 6	NW 2	NW 2
2	115.5	116.5	115.9	116.0	-1.4	-0.6	-1.3	-1.4	0.0	-1.9	90	79	86	85	0.5	1.2	0.8	0.8	10	7	8	N 1	NW 3	C 0
3	112.4	109.5	106.8	109.6	-6.2	-1.0	-4.0	-3.8	-0.7	-6.6	94	79	91	88	0.2	1.2	0.4	0.6	5	1 ⊙	7	C 0	E 1	NE 1
4	103.3	101.3	99.7	101.4	-6.2	1.5	0.4	-1.0	2.5	-6.6	89	67	57	71	0.4	2.3	2.7	1.8	4	8	8 ●	C 0	WSW 4	WSW 3
5	97.1	99.4	102.8	99.8	-1.3	-0.7	-0.3	-0.6	0.6	-1.6	60	89	100	83	2.2	0.6	0.0	0.9	4	10	10	WSW 5	SW 3	SW 3
6	103.9	103.9	103.6	103.8	0.0	0.9	1.3	0.9	1.5	-0.5	98	94	87	90	0.1	0.4	0.9	0.5	10	10	10	SW 1	SW 1	SW 3
7	101.5	101.4	102.5	101.8	-1.4	-0.3	-0.2	-0.5	1.4	-1.8	97	94	96	96	0.2	0.4	0.2	0.3	10	10 ⊙	4	WSW 3	SSW 2	WSW 1
8	103.9	104.8	102.6	103.8	-2.9	1.6	-2.5	-1.6	2.0	-3.0	95	74	98	89	0.2	1.8	0.1	0.7	0	0 ⊙	7	WSW 1	SW 3	SW 1
9	94.4	88.0	82.1	88.2	-5.3	-0.9	0.5	-1.3	3.7	-6.2	100	95	90	95	0.0	0.3	0.6	0.3	10	7	10	C 0	C 0	WNW 2
10	80.0	79.6	79.5	79.7	1.0	4.1	0.1	1.3	5.2	-0.7	70	63	78	70	2.0	3.1	1.4	2.2	9	8	8	SW 3	SSW 4	SW 1
11	82.1	82.0	79.7	81.3	2.3	3.1	3.0	2.8	3.7	-0.9	87	83	72	81	0.9	1.3	2.1	1.4	10	10	10	WSW 2	SW 4	SSW 4
12	74.5	71.9	72.2	72.9	0.9	6.7	1.4	2.6	7.1	0.5	79	40	70	63	1.4	5.8	2.1	3.1	9	8	5	C 0	SSE 2	N 2
13	72.0	71.1	73.1	72.1	1.9	4.8	3.4	3.4	5.7	-0.4	76	59	73	69	1.7	3.5	2.1	2.4	8	9 ⊙	10	C 0	E 2	N 2
14	75.0	77.0	80.2	77.4	0.9	1.6	0.5	0.9	3.6	0.3	96	96	90	94	0.2	0.3	0.6	0.4	10 *	10 *	10	W 1	WSW 2	WSW 3
15	73.6	64.5	62.1	66.7	-2.2	2.1	2.3	1.1	2.4	-2.6	83	63	77	74	0.9	2.6	1.7	1.7	2	9	10 *	SW 1	SW 4	SSW 3
16	48.6	49.6	52.5	50.2	-0.3	3.5	3.1	2.4	4.2	-0.6	96	90	88	91	0.3	0.8	0.9	0.7	10 *	10 ●	10 ●	ESE 1	SSW 5	SW 3
17	62.1	67.5	71.9	67.2	0.1	0.6	1.0	0.7	3.2	-0.2	98	88	88	91	0.2	0.3	0.3	0.6	10 *	10 *	10 *	NW 3	SW 3	WSW 3
18	71.0	71.4	73.1	71.8	0.0	0.5	-1.2	-0.5	1.1	-1.4	94	92	95	94	0.4	0.5	0.3	0.4	10 *	10	10	SW 2	WNW 3	C 0
19	75.3	77.5	83.5	78.8	-2.7	-3.7	-4.6	-3.9	-1.0	-4.7	100	90	93	94	0.0	0.5	0.3	0.3	10 *	10	10 *	C 0	NNE 3	NNE 4
20	90.1	92.4	95.6	92.7	-8.2	-6.7	-7.0	-7.2	-4.4	-8.8	92	88	88	89	0.2	0.4	0.4	0.3	10	10	10	C 0	NNW 3	N 2
21	92.1	89.8	91.4	91.1	-11.4	-10.2	-10.6	-10.7	-6.3	-13.0	86	81	84	84	0.4	0.5	0.4	0.4	3	3 ⊙	10 *	E 3	NE 1	ENE 5
22	98.0	101.9	107.6	102.5	-15.2	-13.0	-14.8	-14.4	-10.4	-15.6	91	84	78	84	0.2	0.4	0.4	0.3	10	10	9	NE 4	N 4	NNE 4
23	109.3	110.9	112.4	110.9	-14.1	-12.3	-12.6	-12.9	-8.9	-15.2	87	66	85	79	0.3	0.8	0.4	0.5	10 *	9 ⊙	10	NNE 3	NE 5	NE 5
24	111.8	111.0	110.8	111.2	-12.4	-11.4	-9.8	-10.8	-9.5	-12.7	81	75	85	80	0.4	0.6	0.4	0.5	10	10 *	10	NE 6	NE 4	NNE 4
25	106.7	102.8	98.4	102.6	-10.0	-9.4	-10.7	-10.2	-8.8	-10.8	87	88	90	88	0.4	0.4	0.3	0.4	10	10 *	10 *	ENE 6	ENE 3	ENE 2
26	91.8	89.0	86.7	89.2	-12.4	-8.2	-10.5	-10.4	-8.0	-15.0	85	95	90	90	0.4	0.2	0.3	0.3	10	9 *	10	C 0	E 1	C 0
27	83.5	83.1	84.7	83.8	-9.2	-7.3	-11.9	-10.1	-7.0	-12.9	95	82	89	89	0.2	0.6	0.3	0.4	10	2 ⊙	10	C 0	E 1	NNE 1
28	86.0	86.9	88.2	87.0	-10.4	-7.0	-14.3	-11.5	-6.2	-14.4	90	88	91	90	0.3	0.4	0.2	0.3	10	6 ⊙	3	NNE 1	C 0	C 0
29	85.1	82.7	80.4	82.7	-18.4	-6.8	-1.9	-7.2	-0.4	-18.9	90	96	91	92	0.2	0.1	0.5	0.3	2	10 ⊙	10	C 0	ESE 1	WNW 1
30	81.9	82.7	84.2	82.9	-2.1	-3.4	-5.3	-4.1	-1.6	-5.7	87	92	97	92	0.6	0.4	0.1	0.4	10	10 *	10 *	WNW 1	NE 3	NNE 5
31	86.5	89.4	93.0	89.6	-7.4	-8.6	-11.7	-9.8	-5.3	-12.0	96	98	89	94	0.1	0.1	0.3	0.2	10 *	10 *	10	NE 5	NE 5	NE 3
M	89.3	89.2	89.9	89.5	-4.9	-2.6	-5.8	-5.8	-0.9	-6.5	88	82	85	85	0.6	1.1	0.8	0.8	8.3	8.2	9.0	1.9	2.6	2.4

Kraków, Obserw. Astr. UJ H_s=206m H_t=219,8m h_w=10m Listopad - Novembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	4	0.2	•	₊na •°ok.15⁰⁰; =na-np
2	4	0.0	•	≡°I=II≡°III
3	5	0.1	•	•°na-a; ≡'na-a≡°III
4	4	0.1	•	•°-a; ≡²na-a≡'-ok.9³⁰=II,III; ⌓°III
5	7	•	•	≡²na-7⁴⁰≡'-9⁰⁰≡°-10⁰⁰; ⌓'I ⌓°III
6	8	1.5	•	•°⁻¹14⁴⁰-19³⁰; ⌓°I
7	8	•	•	⌓ III
8	7	•	•	≡'na-a; ⌓²I
9	6	0.0	•	
10	6	5.5	•	•°ok.6⁰⁰ •a-np; =III
11	4	5.5	•	•na-a ⁂8⁰⁰-10¹⁵ ₊II •p...; =II,III
12	4	3.2	•	•a... ₊II •p...; =II
13	4	0.2	•	₊ok.19⁰⁰-np; =na-p≡²III
14	4	3.8	•	₊na,a •p; ≡²na-a=II≡°III
15	5	17.6	•	•°a-p •16⁰⁰-np; ≡²na-a=II
16	6	0.0	•	•na ₊ ok.10⁴⁰; =I
17	8	•	•	=na-a, III; ⌣°III
18	6	•	•	⌣'I
19	8	1.0	•	•°16⁵⁵ ₊18²⁰-19¹⁰
20	4	6.3	•	•°a... ₊ok.11³⁰-p •°ok.13⁰⁰-15³⁰ ⁂-16⁰⁵ ⁂-16²⁰ ⁂-ok.18⁰⁰ ₊-np; ='na-a, II-np
21	5	0.0	•	⁂°16⁴⁵-17¹⁰; =na-np
22	4	8.5	•	•18³⁰ ⁂°23⁰⁰-24; ≡°na-7⁰⁵≡'-7¹⁵≡²-8¹⁰≡°-9⁰⁰=II,III
23	3	10.6	6	⁂'na-a ⁂°⁻¹a-p; ≡°na-a≡'-p≡°-np
24	5	0.3	15	⁂°na ⁂a... ⁂°p; ≡°na-a=II-np
25	2	8.0	11	⁂ •a ⁂°⁻¹p; ≡°na-a≡'-p≡°-np
26	3	11.6	11	⁂ •na •'I ⁂'7⁰⁵-8⁰⁰ •'p-np; ≡° na-a≡°-np
27	5	0.1	8	•°I-a; ≡'na-a≡°-p=III
28	5	•	pł.	•°n; =Ina-np
29	4	0.0	pł.	•°n ₊ ok.12⁰⁰; =na-p
30	5	2.1	pł.	₊ ok.9⁰⁰; 12⁰⁰ •'18³⁰-19³⁰ •₊ np; =II,III
31				
Σ	—	85.8	—	UWAGI

Grudzień - Décembre

1	6	0.1	•	⁂17⁰⁰-18⁰⁰
2	6	••	pł.	
3	6	•	•	≡°I,III; ⌣'I ⌣III
4	5	•	•	=na-np; ⌣²I; ψ17⁰⁰
5	3	0.7	•	₊ ok.14⁰⁰, ok.18³⁰-np; ≡°a-np
6	3	•	1	⁂°n; ≡°na-a≡°II=III
7	3	0.0	pł.	₊p...; ≡'I≡°III≡°III; ψ ok.20⁰⁰
8	5	•	•	≡°na-a=II≡'III; ⌣'I ⌣²III
9	2	0.0	•	⁂p; ≡²na-a≡'-p=III; ⌣²I
10	6	0.1	pł.	⁂n; =III; ⌣°III; ψ20⁰⁰-21⁰⁰
11	4	0.0	pł.	•°a; =I,II
12	8	•	•	≡°na-a; ψ ok.21⁰⁰
13	8	8.3	•	•°22³⁰-np ⁂-np; =III
14	3	7.3	1	⁂°na-a •⁂°a... ⁂°II •⁂°ok.16⁰⁰-19⁰⁰; ≡°na-p; ψ np
15	8	3.0	2	•⁂p... ⁂°III
16	5	3.6	6	⁂ •na-a ⁂ •°-ok.12⁰⁰ •°⁻¹-np; =I,II
17	5	0.6	5	⁂°⁻¹na-a ⁂°...np; ≡°I=II,III
18	4	6.1	2	⁂°na-a, a... ⁂' ok.19⁰⁰ ⁂°np; ≡°I=II≡°III
19	6	1.6	11	⁂°na-a, p-np; =I,II
20	5	0.4	13	⁂a... ⁂p; ≡°I=II
21	4	1.4	12	⁂°n, p-np ⁂²-np; =I,II,III
22	4	0.9	15	⁂°a, p; =na-np
23	7	0.3	14	⁂na ⁂'-a ⁂°a... ⁂'p...; =I,III
24	5	0.3	15	⁂²na ⁂°⁻¹a... ⁂'II; + na; =I,II
25	5	1.5	14	⁂°na ⁂'a... p ⁂°... p, III; =II
26	3	0.2	13	•°II, p...; =I≡°II≡°III; VI; ⌣°III
27	5	0.0	14	=I,II≡°III; ⌣°III
28	3	•	13	⁂°na; ≡°I, II≡'III; ⌣°I; V'III
29	4	•	13	≡°I=II≡°III; V²I
30	4	7.0	12	⁂'8⁰⁰-9³⁰, 11³⁰-p ⁂°⁻¹p...; ≡°I, II≡°III
31	3	5.8	21	⁂ + na-p; =I≡°II=III
Σ	—	49.2	—	UWAGI

Przemyśl φ=49°48' λ=22°46' Styczeń-Janvier 1962

DNI	CISNIENIE P-900+ I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	80.0	83.0	83.2	82.1	5.6	6.0	3.4	4.6	8.1	3.1	83	79	86	83	1.6	2.0	1.1	1.6	9	10	10	SW 3	W 2	W 1
2	81.1	81.7	84.8	82.5	1.3	0.5	-0.6	0.2	3.7	-0.9	85	83	70	79	1.0	1.0	1.8	1.3	10	10 *	10	C 0	NW 3	WNW 3
3	88.7	90.3	94.6	91.2	-2.5	-2.7	-1.8	-2.2	-0.6	-4.0	67	65	88	73	1.7	1.8	0.7	1.4	10	6	10 *	NW 7	W 7	W 3
4	98.8	97.6	95.2	97.2	-1.4	0.4	-3.4	-2.0	0.7	-3.9	94	66	81	80	0.3	2.1	0.9	1.1	10 *	9	0	W 1	W 2	W 2
5	94.3	93.0	90.7	92.7	-4.5	1.0	-2.3	-2.0	1.4	-5.8	81	68	74	74	0.8	2.2	1.4	1.5	1	8	0	W 1	W 3	W 3
6	86.9	86.0	83.8	85.6	-3.2	-1.1	-3.0	-2.6	-1.0	-4.3	74	65	77	72	1.2	2.0	1.1	1.4	0	0 ⊙	0	W 4	SW 7	WSW 5
7	86.1	89.1	95.1	90.1	-2.8	-0.8	0.7	-0.6	1.3	-3.8	84	87	90	87	0.8	0.7	0.6	0.7	10	10 *	10 *	W 5	W 5	NW 5
8	99.4	99.8	99.3	99.5	-0.7	1.3	-5.5	-2.6	1.7	-6.7	91	63	82	79	0.5	2.5	0.7	1.2	10	1 ⊙	0	W 1	W 1	W 2
9	97.2	95.5	92.8	95.2	-2.0	1.2	-4.6	-2.5	1.4	-5.7	75	59	72	69	1.4	2.7	1.2	1.8	10	0 ⊙	0	W 2	SSW 3	C 0
10	88.7	86.1	84.0	86.3	-3.1	2.9	1.6	0.8	3.5	-6.3	57	60	58	58	2.1	3.0	2.9	2.7	2	9	10	C 0	S 7	SW 6
11	84.5	83.4	81.1	83.0	4.0	7.6	5.6	5.7	8.3	1.1	64	48	55	56	2.9	5.4	4.1	4.1	3	1	3	WSW 6	SW 6	SW 5
12	80.7	79.9	77.0	79.2	5.6	4.6	1.9	3.5	6.4	1.6	65	84	84	78	3.2	1.4	1.2	1.9	10	10 ●	10	SW 2	C 0	C 0
13	68.3	69.9	71.7	70.0	5.7	4.4	5.0	5.0	6.1	0.5	73	73	72	73	2.6	2.3	2.4	2.4	9	8	10	SSW 5	SW 7	SW 3
14	72.3	75.4	80.8	76.2	0.8	2.6	0.2	1.0	5.1	-0.6	100	89	90	93	0.0	0.8	0.6	0.5	10 ●	9	3	C 0	W 3	C 0
15	84.3	87.6	92.1	88.0	0.6	3.6	0.3	1.2	3.9	-0.9	73	60	78	70	1.8	3.1	1.3	2.1	1	1	8	WSW 3	SW 5	SW 2
16	95.1	96.5	95.7	95.8	-1.0	3.6	-0.3	0.5	4.8	-1.7	79	59	70	69	1.2	3.3	1.8	2.1	0	1 ⊙	0	W 2	WSW 1	C 0
17	92.9	92.6	92.3	92.6	0.8	3.8	2.5	2.4	4.1	-0.9	51	60	70	60	3.2	3.2	2.2	2.9	4	7 ⊙	3	SSW 4	SW 7	SW 3
18	89.9	88.4	89.1	89.1	3.1	6.8	3.4	4.2	7.3	0.7	66	56	75	66	2.6	4.4	2.0	3.0	8	8	0	SSW 2	SW 4	SW 2
19	90.6	90.5	89.9	90.3	2.4	5.1	5.8	4.8	7.3	1.2	73	73	67	71	2.0	2.4	3.0	2.5	3	6	10	W 1	W 1	SW 3
20	89.0	90.3	92.9	90.7	4.6	5.6	3.1	4.1	6.4	2.4	71	64	76	70	2.5	3.3	1.8	2.5	10	6	8	SW 4	W 5	WSW 3
21	94.7	93.2	93.0	93.6	0.7	5.7	4.0	3.6	5.9	0.2	83	68	87	79	1.1	3.0	1.1	1.7	1	8	10 ●	WSW 2	SW 7	W 3
22	88.8	84.4	83.4	85.5	6.2	9.0	7.1	7.4	10.6	3.7	73	58	56	62	2.6	4.8	4.4	3.9	9	9	9	W 2	S 3	WSW 3
23	87.4	89.1	91.4	89.3	1.9	5.9	-0.4	1.8	7.1	-0.8	82	52	88	74	1.3	4.4	0.7	2.1	2	4	5	C 0	W 2	C 0
24	91.8	90.7	88.6	90.4	-0.8	4.3	2.2	2.0	5.4	-1.9	87	55	63	68	0.8	3.7	2.7	2.4	2	1 ⊙	10	W 3	W 3	WSW 5
25	85.0	83.0	81.7	83.2	1.6	3.2	3.8	3.1	4.4	0.7	85	86	82	84	1.1	1.1	1.5	1.2	10 *	10 ●	10	WSW 3	SW 3	SW 3
26	80.7	85.4	88.1	84.7	3.0	0.3	-0.5	0.6	3.9	-0.8	93	92	84	90	0.6	0.5	1.0	0.7	10 ●	10	10 *	W 4	WNW 7	NW 2
27	84.8	83.8	84.5	84.4	-1.5	-0.5	1.2	0.1	1.6	-2.1	90	96	81	89	0.5	0.3	1.3	0.7	10	10 *	10	C 0	W 2	W 6
28	81.1	81.0	80.7	80.9	0.6	1.0	-2.4	-0.8	1.3	-2.4	92	75	78	82	0.5	1.7	1.1	1.1	10	9	9 *	W 3	WNW 7	W 5
29	85.8	87.9	93.1	88.3	-6.7	-5.2	-5.0	-5.5	-2.4	-7.3	86	93	95	91	0.5	0.3	0.2	0.3	9 *	10 *	10 *	NW 7	NW 6	NNW 3
30	99.1	102.0	104.7	101.9	-4.6	-6.9	-10.9	-8.3	-2.3	-11.1	93	85	87	88	0.3	0.5	0.4	0.4	10	10	10	NE 7	NE 5	NE 7
31	104.6	103.6	100.6	102.9	-13.6	-9.1	-8.6	-10.0	-7.5	-14.0	84	79	89	84	0.4	0.6	0.4	0.5	10	9	0	NNE 4	E 5	E 5
M	88.1	88.4	88.9	88.5	0.0	2.1	0.1	0.6	3.5	-2.3	79	71	78	76	1.4	2.3	1.5	1.7	6.9	6.8	6.4	2.8	4.2	3.0

Luty-Février

1	93.1	90.3	89.0	90.8	-8.3	-4.9	-9.3	-8.0	-4.7	-10.4	92	78	88	86	0.2	0.9	0.4	0.5	10 *	9	8	E 6	ESE 3	E 1
2	88.7	90.5	91.2	90.1	-6.9	-3.5	-5.5	-5.4	-2.5	-10.9	85	78	85	83	0.5	1.0	0.6	0.7	10	10	8	C 0	SE 1	C 0
3	92.0	93.2	94.5	93.2	-4.1	-3.0	-3.3	-3.4	-2.6	-5.7	94	93	92	93	0.3	0.4	0.4	0.4	10 *	10 *	10 *	C 0	N 3	N 2
4	91.9	90.7	90.8	91.1	-3.9	-1.7	-1.8	-2.3	-1.3	-4.2	92	82	88	87	0.4	1.0	0.7	0.7	10	10	10 *	C 0	NW 1	W 2
5	91.1	85.9	79.0	85.3	-1.6	2.0	0.1	0.2	2.3	-2.1	90	59	85	78	0.5	3.0	1.0	1.5	10	3 ⊙	10 *	W 1	SE 5	WSW 6
6	83.1	85.3	88.0	85.5	1.6	2.5	1.5	1.8	2.9	-0.7	81	70	78	76	1.3	2.2	1.5	1.7	10	9 *	10	W 5	W 7	W 4
7	90.7	91.3	89.5	90.5	0.1	1.4	-1.8	-0.5	1.7	-3.4	74	63	73	70	1.6	2.5	1.4	1.8	9	9	4	W 3	W 2	C 0
8	87.4	87.8	89.2	88.1	-4.9	3.2	-0.6	-0.7	3.9	-7.0	78	50	74	67	0.9	3.9	1.5	2.1	1	3	4	C 0	SE 2	SE 1
9	91.5	94.5	99.3	95.1	-2.6	1.6	1.1	0.3	2.1	-2.8	83	76	79	79	0.9	1.7	1.4	1.3	10	10	10	C 0	SW 2	W 6
10	102.4	103.6	103.0	103.0	-0.4	0.8	-3.8	-1.8	1.5	-4.0	80	78	76	78	1.2	1.4	1.1	1.2	10	9	0	NW 3	W 2	C 0
11	98.5	95.8	96.7	97.0	-8.1	2.6	1.9	-0.4	2.9	-10.0	95	55	76	75	0.2	3.4	1.7	1.8	8	10	9	C 0	W 3	W 5
12	94.4	79.0	66.4	79.9	-1.7	1.9	3.1	1.6	3.3	-3.4	75	59	71	68	1.3	2.8	2.2	2.1	5	10	10 *	SW 3	SW 10	SW 14
13	62.1	58.9	59.2	60.1	2.4	2.5	0.1	1.3	3.9	0.0	86	88	98	91	1.1	0.9	0.2	0.7	10 ●	10 ●	10 *	SW 7	WSW 3	W 1
14	59.9	60.4	63.2	61.2	-0.6	-0.9	-2.2	-1.5	0.1	-2.3	91	89	85	88	0.5	0.6	0.8	0.6	10 *	10	10	NW 3	NW 6	NW 5
15	69.7	74.9	84.4	76.3	-3.4	-4.6	-4.1	-4.0	-2.2	-5.0	83	74	84	80	0.8	1.1	0.7	0.9	10	10 *	10 *	NW 7	NW 9	NW 7
16	87.2	77.9	66.8	77.3	-8.9	-3.0	-1.8	-3.9	-1.4	-9.0	76	57	83	72	0.7	2.1	0.9	1.2	1	10	10 *	WSW 2	SW 7	SW 10
17	61.2	61.3	64.8	62.4	-0.6	2.0	1.0	0.8	2.3	-2.5	83	75	73	77	1.0	1.8	1.8	1.5	10 *	10 *	10 *	SW 10	W 9	W 10
18	72.7	77.7	84.7	78.4	-3.6	-3.4	-3.6	-3.6	1.0	-4.9	74	88	74	79	1.3	0.6	1.3	1.1	10 *	10 *	10 *	WNW 7	W 10	W 10
19	88.6	88.5	88.1	88.4	-4.8	-0.6	-1.7	-2.2	-0.6	-5.2	76	68	92	79	1.0	1.9	0.4	1.1	3	9	10 *	W 3	W 6	W 1
20	87.8	88.7	85.7	87.4	2.0	3.1	3.0	2.8	3.2	-2.0	87	74	74	78	0.9	1.9	2.0	1.6	10	10	10	W 5	W 7	SW 7
21	84.3	86.3	90.8	87.1	0.6	-1.2	-2.4	-1.4	3.6	-2.5	92	86	87	88	0.5	0.8	0.7	0.7	10 *	10 *	10 *	W 9	NW 10	NW 7
22	97.5	99.8	101.8	99.7	-5.0	-4.8	-5.6	-5.2	-2.4	-6.1	88	71	85	81	0.5	1.2	0.6	0.8	10 *	4 ⊙	10 *	E 6	N 4	N 2
23	100.4	97.1	93.9	97.1	-7.9	-7.0	-7.2	-7.3	-5.5	-8.8	73	74	85	77	0.9	0.9	0.5	0.8	10 *	10 *	10 *	NW 5	WNW 6	NW 5
24	89.8	88.8	90.6	89.7	-8.9	-5.8	-9.1	-8.2	-5.4	-9.1	86	79	92	86	0.4	0.8	0.3	0.5	7	4	4	WNW 2	NE 2	C 0
25	92.7	93.1	92.4	92.7	-11.1	-5.0	-5.8	-6.9	-4.0	-14.4	90	76	92	86	0.3	1.0	0.3	0.5	10	9	10 *	NE 2	E 2	E 1
26	92.7	93.3	93.2	93.1	-8.4	-5.7	-2.2	-4.1	-1.8	-8.9	92	87	94	91	0.3	0.6	0.3	0.4	10	10	10	C 0	C 0	E 2
27	91.9	91.0	89.7	90.9	-3.4	-3.1	-4.5	-3.9	-2.2	-4.5	83	86	88	86	0.8	0.7	0.3	0.7	10	10	10 *	SE 3	E 6	E 6
28	86.7	85.4	83.0	85.0	-5.2	-2.6	-2.9	-3.4	-1.7	-5.5	93	81	86	87	0.3	1.0	0.7	0.7	10	10	10	E 3	E 3	ESE 1
29																								
30																								
31																								
M	86.8	86.1	86.0	86.3	-5.8	-1.3	-2.4	-2.5	-0.1	-5.5	85	75	83	81	0.7	1.5	0.9	1.0	8.7	8.9	8.8	3.4	4.7	4.1

Przemyśl $H_s = 237m$ $H_n = 238{,}9m$ $h_w = 20{,}6m$ Styczeń - Janvier 1962

DNI	WIDZIALNOŚĆ V	OPAD E	GRUBOŚĆ CU A	POGODA
1	8	0.0	15	•°15^44 16^10 = 9^16-11^26
2	6	0.0	9	♎°10^25-45 *°11^50-12^50 22^45-23^30 = 6^20-21^30
3	7	0.0	7	*°1^50-2^35 ▽°-3^45 *°15^50-22^10
4	7	.	7	*°6^20-40 = 7^21-12^20 16^30-21^30
5	7	.	7	= 7^10-10^20 16^18-23^20
6	7	0.1	6	
7	6	0.3	7	*°1^35-5^30 7^20-9^45 ▽°10^10-11^45 *°12^25-22^50 = na
8	7	0.0	8	*°8^38-9^10 = 19^30-24
9	7	.	7	= 0^00-1^10
10	7	.	6	
11	7	0.0	6	
12	5	0.4	pł.	•°5^40 6^06 10^10-13^35 = 6^20-9^40 10^15-23^30
13	8	9.9	pz.	▽°11^20-27 •°23^50-24
14	6	0.5	pł.	•°0^00-5^35 ▽°-7^25 •°-8^40 = 5^20-21^30
15	7	.	pł.	
16	7	.	pł.	= 6^50-12^20
17	8	.	pł.	
18	8	.	pł.	▽0^00-3^00
19	6	.	pł.	= 6^50-9^10 ∞-14^40
20	8	0.0	pł.	▽°10^40-50
21	7	0.8	pł.	•°15^40 20^20-21^40
22	8	.	pł.	
23	7	.	.	▽°21^30-23^10
24	7	0.1	.	*°23^50-24 ▽1^40-4^20
25	7	1.1	.	*°0^00-7^05 •°9^40 13^10 = 4^50-6^45
26	6	4.2	.	▽°1^35-2^05 •°5^10-9^50 *°-11^45 *°20^25-21^40 = a-p
27	5	5.3	.	*°7^40-19^10 = 6^10-19^10
28	8	0.7	6	*°0^10-1^20 3^20-6^20 6^24-8^25 20^20-22^10
29	6	4.5	7	*°3^15-15^01 *'-19^20 *°-24
30	7	0.0	14	*°0^00-1^40 2^25-3^10 8^20-9^40 = 1^40-9^30 16^40-24
31	6	0.0	14	*°7^45-9^35 = 0^00-13^15 15^20-24
Σ	—	27.9	—	UWAGI

Luty - Février

1	6	0.6	14	*°5^40-6^48 7^17-8^40 = 0^00-24
2	6	0.8	9	*°23^15-24 = 0^00-24
3	5	1.3	12	*°0^00-10^20 11^35-21^25 = 0^00-24
4	6	0.0	15	*°7^45-8^50 15^50-16^40 = 0^00-24
5	7	2.6	15	*°17^40-21^25 = 0^00-9^50
6	7	1.2	15	▽°0^15-1^20 •°-6^15 *°7^45-9^07 ▽°-1 12^20 20^10 *°22^15-24
7	7	.	11	*°1^00-20 = 16^25-21^30
8	7	.	11	= 6^15-10^20
9	6	0.5	10	*°9^30-12^15 •°19^45-20^20 = 2^40-22^50
10	8	.	10	*°1^50-4^20 5^50-6^10 = p
11	7	0.2	9	*°17^10-19^20
12	7	5.1	9	*°13^50-16^20 17^43 20^20-21^10 •°-24 ≫ 11^30-24
13	7	9.2	7	•°0^00-4^50 5^45-8^15 11^35-13^30 *°-15^10 *°-2-24 ≫ 0^00-5^45
14	7	1.1	15	*'-°0^00-10^46
15	6	0.0	14	*°8^15 14^30 16^03-18^20 ▽°-6 19^40-22^20 ⊢ 7^50-24 ≫ 7^50-9^40
16	7	1.6	15	*°13^40-19^20 20^15-24 ⊢ 0^00-40 ⊢ p ≫ 16^30-24
17	7	3.9	15	*°0^00-1^10 4^20-11^40 ▽°-1 12^05-18^35 ▽°-2 20^20-23^35 ⊢ 0^00-11^48 ≫ 0^00-8^30 20^20-24
18	7	0.3	20	▽°6^15 20^20 •°-24 ⊢2-6 ⊢°1^40-7^10 24 ≫ na 10^20 24
19	7	4.7	25	*°0^00-1^25 15^48-17^50 19^35-24 ⊢ 0^00-5^40
20	7	2.0	15	*°0^00-2^20 *•°-4^10 •°-6^15 *°19^35-20^10 *°22^20-23^15
21	7	0.5	10	•°0^20-1^10 *2^10-3^05 ▽°na *°12^45 24 ⊢ 11^50-14^45
22	7	0.3	10	*°0^00-10^17 10^35-11^14 ▽°-1 16^17-17^25 *°19^15-24
23	5	1.4	11	*°0^00-24
24	7	0.3	14	*°0^00-12^10 18^40-20^20 = 21^10-24
25	6	0.9	15	*°4^34-6^20 15^45-16^30 p = 0^00-24 ⌣° 2-11
26	6	.	15	= 0^00-5^50 ≡°-1-8^46 = -24
27	6	0.0	10	*°20^20-21^10 22^40-24 = 0^00-24
28	6	0.1	10	*°21^50-24 = 0^00-24
29				
30				
31				
Σ	—	38.6	—	UWAGI

Przemyśl $\varphi = 49°48'$ $\lambda = 22°46'$ Marzec - Mars 1962

DNI	CIŚNIENIE P-900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N.w			KIERUNEK I PRĘDKOŚĆ WIATRU D.v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	80.0	78.7	77.1	78.6	-2.9	-0.9	-1.2	-1.6	0.1	-3.7	88	79	86	84	0.5	1.2	0.8	0.8	10	10	10	C 0	NE 1	NE 2
2	76.2	75.4	76.3	76.0	-3.8	-1.4	-2.0	-2.3	-0.9	-4.0	85	78	94	86	0.7	1.2	0.4	0.8	10 *	0 ⊙	10	NE 2	NE 3	C 0
3	77.4	77.8	78.4	77.9	-1.6	3.0	1.9	1.3	4.6	-2.8	90	72	71	78	0.5	2.1	2.0	1.5	10	9	0	C 0	E 1	SW 1
4	74.0	70.9	68.8	71.2	1.1	8.8	9.7	7.3	9.9	-0.2	85	58	73	72	1.0	4.8	3.2	3.0	9	8	10	C 0	SSE 4	S 3
5	68.0	69.3	68.8	68.7	9.6	14.9	12.6	12.4	15.1	8.1	77	56	66	66	2.8	7.4	5.0	5.1	6	9	10	SW 1	SW 5	S 3
6	65.3	73.4	81.8	73.5	10.9	4.9	0.2	4.0	14.8	-0.1	77	69	90	79	3.0	2.8	0.6	2.1	9	9	10 *	SSE 3	W 5	W 5
7	85.6	86.9	91.2	87.9	-1.4	-1.2	-3.0	-2.2	0.3	-3.4	94	93	88	92	0.3	0.4	0.6	0.4	10 *	10 *	10 *	NW 5	NW 5	NNW 7
8	95.0	96.3	96.8	96.0	-4.8	-2.5	-5.4	-4.5	1.4	-5.4	73	69	80	76	0.9	1.6	0.8	1.1	10	8	0	NNW 3	NW 5	NW 1
9	97.1	99.0	98.2	98.1	-8.2	-2.5	-8.1	-6.7	-0.8	-9.7	87	67	84	79	0.4	1.7	0.5	0.9	2	9	0	W 2	N 2	C 0
10	93.8	91.1	87.9	90.9	-7.6	0.4	-0.9	-2.2	0.4	-9.7	79	59	85	74	0.7	2.6	0.8	1.4	3	9	6	ESE 5	SE 4	SE 3
11	84.0	82.0	79.7	81.9	-1.7	7.6	1.5	2.2	7.9	-3.5	82	54	87	74	1.0	4.7	0.9	2.2	6 ⊙	10	10	C 0	SSW 5	C 0
12	73.7	69.5	65.0	69.4	0.3	3.3	2.0	1.9	3.7	-0.2	94	85	98	92	0.3	1.2	0.2	0.6	10	10	10 ▬	C 0	E 2	C 0
13	66.9	72.4	80.8	73.4	-0.6	-1.5	-3.6	-2.3	2.5	-3.8	77	66	65	69	1.3	1.9	1.7	1.6	10	9 *	4	W 10	WNW 8	W 7
14	87.2	89.3	92.0	89.5	-5.4	-3.2	-4.5	-4.4	-2.7	-5.5	70	61	74	68	1.2	1.8	1.1	1.4	9 *	8	10	W 5	WNW 6	W 2
15	91.3	88.5	85.5	88.4	-5.4	-6.5	-6.5	-6.2	-4.3	-6.9	75	89	86	83	1.0	0.4	0.5	0.6	10	10 *	10 *	E 3	E 8	ENE 10
16	82.0	81.2	79.3	80.8	-6.6	-5.8	-7.5	-6.8	-5.6	-7.7	88	89	87	88	0.4	0.4	0.4	0.4	10 *	10 *	10 *	NE 12	NE 12	NW 12
17	77.8	77.3	77.6	77.6	-7.9	-5.2	-6.2	-6.4	-5.1	-8.3	81	70	81	77	0.6	1.2	0.7	0.8	10 *	10 *	10 *	NW 8	NW 5	WNW 6
18	79.4	83.6	88.0	83.7	-5.8	-4.8	-5.5	-4.4	-2.6	-6.2	84	78	81	81	0.6	0.9	0.9	0.8	10 *	10 *	0	NW 7	WNW 9	NW 3
19	90.4	91.7	92.6	91.6	-9.2	-5.2	-7.0	-6.6	-1.1	-11.1	88	61	69	73	0.4	1.8	1.1	1.1	6 * ⊙	3 ⊙	2	SW 1	NW 3	C 0
20	93.0	93.3	92.6	93.0	-15.8	-2.6	-7.9	-8.6	-1.4	-18.1	91	77	81	83	0.2	1.2	0.6	0.7	9	2 ⊙	0	C 0	NE 1	C 0
21	90.0	87.2	83.8	87.0	-15.9	-2.8	-5.4	-6.4	-2.0	-17.4	91	69	79	80	0.2	1.6	1.0	0.9	8	0 ⊙	10	C 0	E 5	E 5
22	80.1	78.9	77.0	78.7	-4.0	-1.3	-1.4	-2.0	-0.5	-4.6	91	86	97	91	0.4	0.8	0.2	0.5	10 *	10 *	10 *	E 2	E 3	N 2
23	75.4	76.4	78.4	76.7	-2.2	0.4	-0.6	-0.8	0.8	-2.4	96	77	91	88	0.2	1.4	0.5	0.7	10 *	10	10 *	NW 1	WNW 2	C 0
24	82.4	85.6	89.8	85.9	-1.6	1.2	-0.6	-0.4	1.8	-1.7	84	68	72	75	0.9	2.2	1.7	1.6	10 *	8	4	W 2	W 4	WNW 2
25	92.3	92.2	89.9	91.5	-4.4	-0.3	-3.3	-2.8	0.4	-6.2	91	68	70	76	0.4	1.9	1.5	1.3	10 *	9	9	W 1	N 3	NE 2
26	87.4	86.4	85.0	86.3	-8.7	-0.2	-4.6	-4.5	0.3	-9.2	80	55	69	68	0.6	2.7	1.3	1.5	3	2 ⊙	0	NNE 2	E 4	E 3
27	81.6	79.5	78.6	79.9	-7.7	0.1	-2.0	-2.9	0.3	-8.6	84	69	83	79	0.5	1.9	0.9	1.1	10	5	10	E 2	E 3	E 1
28	76.0	75.5	77.7	76.4	-4.0	6.3	2.2	1.7	7.6	-6.1	87	56	89	77	0.6	4.1	0.8	1.8	9	5 ⊙	10	C 0	W 3	W 3
29	79.8	80.4	78.8	79.7	1.9	5.8	1.5	2.7	7.5	0.7	84	55	78	72	1.2	4.1	1.5	2.3	8	6	0	W 1	W 3	C 0
30	73.8	73.5	71.8	73.0	3.9	8.4	7.1	6.6	11.3	0.3	87	66	84	79	1.1	3.7	1.6	2.1	10 ●	9	10	SW 2	SW 3	SW 2
31	67.5	67.9	68.5	68.0	9.2	12.5	9.2	10.0	15.0	6.7	80	70	85	78	2.3	4.4	1.7	2.8	10	7	9	SW 2	SW 5	C 0
M	81.4	81.6	81.9	81.6	-3.2	1.0	-1.1	-1.1	2.5	-4.9	85	70	81	79	0.8	2.3	1.1	1.4	8.6	7.5	6.9	2.6	4.3	2.7

Kwiecień - Avril

1	71.3	78.1	82.7	77.4	4.8	4.3	1.6	3.1	9.5	1.4	94	76	89	86	0.6	2.0	0.8	1.1	10 ●	10	0	W 7	WNW 5	W 2
2	83.6	83.9	86.1	84.5	2.5	10.3	5.4	5.9	10.6	-0.1	67	41	72	60	2.4	7.4	2.4	4.1	3 ⊙	9	0	SW 2	WSW 6	C 0
3	89.6	89.5	86.1	88.4	2.6	12.5	6.4	7.0	13.3	0.7	82	31	70	61	1.3	10.0	2.8	4.7	1 ⊙	4 ⊙	0	C 0	SW 5	SSW 1
4	81.8	78.1	74.6	78.2	6.9	16.3	9.9	10.8	16.5	4.9	60	38	68	55	3.9	11.4	3.9	6.4	6 ⊙	2 ⊙	3	SE 1	SSW 7	S 2
5	65.8	63.5	63.7	64.3	7.2	11.4	7.3	8.3	11.9	6.4	71	65	81	72	2.9	4.7	1.9	3.2	8	10	10	SE 2	SE 4	C 0
6	65.4	65.6	66.1	65.7	4.2	7.4	6.6	6.2	10.9	2.5	90	83	94	89	0.8	1.8	0.5	1.0	9	9	10	S 2	E 4	NE 4
7	67.7	75.1	82.5	75.1	5.6	4.2	2.2	3.6	6.6	2.2	89	74	68	77	1.0	2.1	2.3	1.8	10 ●	10	0	NW 9	NW 12	W 3
8	83.2	84.3	84.9	84.1	2.1	7.4	5.8	5.3	9.7	0.5	80	70	79	76	1.4	3.1	2.0	2.2	10	10	0	WSW 3	SW 5	SW 1
9	84.6	84.9	86.4	85.3	8.7	16.6	10.4	11.5	17.7	5.6	64	38	60	54	4.0	11.7	5.0	6.9	9	2 ⊙	0	W 1	WSW 3	C 0
10	89.6	90.4	91.3	90.4	6.1	12.5	10.4	9.8	13.9	5.2	91	62	85	79	0.8	5.5	1.9	2.7	5 ⊙	4 ⊙	6	W 2	NW 3	NE 3
11	91.5	90.0	89.9	90.5	5.4	16.9	10.8	11.0	17.0	4.2	97	42	78	72	0.3	11.1	3.0	4.8	10 ▬	6 ⊙	3	NE 1	ESE 5	NE 1
12	89.8	88.5	87.2	88.5	3.7	15.2	11.6	10.5	16.1	3.0	98	51	62	70	0.2	8.5	5.1	4.6	1 ▬ ⊙	5	1	S 3	NE 3	NE 1
13	85.1	82.0	80.4	82.5	5.6	15.1	7.2	8.8	15.2	2.9	92	41	87	73	0.7	10.1	1.4	4.1	2 ⊙	8	10	C 0	E 7	E 2
14	81.3	86.5	90.2	86.0	6.2	5.7	6.2	6.1	7.2	5.6	97	92	92	94	0.3	0.8	0.7	0.6	10 ●	10	10 ●	WSW 2	W 4	W 4
15	90.7	88.8	89.4	89.6	7.4	15.7	12.4	12.0	18.8	5.9	97	61	64	74	0.3	6.9	5.2	4.1	10	8	3	N 2	NNE 5	NE 5
16	92.5	92.7	94.7	93.3	10.1	20.1	12.8	14.0	21.3	8.2	76	40	71	62	3.0	14.0	4.3	7.1	0 ⊙	2 ⊙	0	E 1	E 7	C 0
17	97.9	97.1	96.0	97.0	9.5	21.2	14.1	14.7	21.5	7.3	75	32	67	58	3.0	17.1	5.3	8.5	0 ⊙	1 ⊙	7	E 2	ESE 7	E 1
18	95.5	93.8	92.2	93.8	9.6	20.8	16.0	15.6	21.7	9.0	84	31	48	54	1.9	16.9	9.6	9.5	10	9	8	ESE 1	SSE 6	SSE 2
19	91.6	91.0	90.8	91.1	13.2	23.7	17.7	18.1	24.3	10.5	64	28	46	46	5.5	21.0	8.9	11.8	6	0 ⊙	8	SSE 1	SW 5	S 1
20	91.2	91.2	90.9	91.1	14.8	23.2	18.0	18.5	24.3	11.3	55	42	56	51	7.5	16.5	9.1	11.0	5 ⊙	0 ⊙	4	W 3	N 3	NW 2
21	92.4	92.1	91.7	92.1	11.6	24.9	18.9	18.6	25.3	8.9	78	39	63	60	2.9	19.2	8.0	10.0	0 ⊙	0 ⊙	0	W 2	NE 2	C 0
22	92.2	92.0	91.8	92.0	11.5	24.5	15.8	16.9	25.5	8.6	90	32	55	59	1.4	21.0	8.1	10.2	0	2 ⊙	0	S 1	E 2	C 0
23	92.1	91.8	91.5	91.8	10.7	24.5	16.4	17.0	25.5	6.4	75	32	58	55	3.2	20.8	7.7	10.6	0 ⊙	0 ⊙	0	SW 1	E 1	C 0
24	93.3	94.4	95.1	94.3	12.2	24.1	18.5	18.3	25.8	6.8	72	42	58	57	4.0	17.3	8.9	10.1	0 ⊙	1 ⊙	0	W 3	NE 4	C 0
25	97.6	97.4	97.3	97.4	11.2	22.9	13.6	15.3	23.2	8.6	91	57	61	70	1.2	12.0	6.2	6.5	1 ⊙	1 ⊙	0	WNW 2	ENE 3	NE 2
26	96.1	92.2	87.0	91.8	7.2	20.1	13.9	13.8	21.2	3.5	87	56	58	60	1.4	15.1	6.7	7.7	0 ⊙	0 ⊙	0	C 0	E 2	C 0
27	80.1	78.6	79.8	79.5	7.8	11.2	7.1	8.3	17.0	4.5	89	96	93	93	1.2	0.5	0.8	0.8	10	10 ●	10	NW 1	W 6	W 5
28	76.5	74.2	73.8	74.8	6.3	6.8	4.6	5.6	10.0	4.4	86	90	97	91	1.2	1.0	0.3	0.8	9	8	9	W 3	SW 5	W 1
29	75.9	76.9	79.1	77.3	4.1	7.7	3.3	4.6	8.3	2.6	92	63	90	82	0.7	3.9	0.7	1.8	8	8	1	W 2	W 5	NW 2
30	78.1	77.8	79.8	78.6	1.5	8.8	4.5	4.8	9.6	-1.3	98	71	85	85	0.1	3.3	1.2	1.5	0	8	0	C 0	NW 4	NNW 6
31																								
M	85.5	85.4	85.8	85.6	7.3	15.2	10.5	10.8	16.7	5.0	83	53	72	69	2.0	9.9	4.2	5.4	5.1	5.2	3.4	2.0	4.7	1.7

Przemyśl $H_s = 237m$ $H_u = 238{,}9m$ $h_u = 20{,}6m$ Marzec - Mars 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	6	0.0	11	*°0^{00}-5^{20}, 7^{05}-9^{20}, 21^{50}-24; = 0^{00}-24
2	6	0.0	10	*°0^{00}-10^{15}; = 0^{00}-24
3	6	0.1	9	*°6^{34}-8^{20}; = 0^{00}-24
4	7	0.6	6	•°14^{26}...15^{26}; 17^{16}...18^{40}, 21^{45}...22^{50}; = na...
5	8	.	pż.	
6	8	3.3	pż.	•°1^{05}-3^{15}; = 15^{40}-18^{20}
7	4	6.0	7	*°2^{10}-24; = 1^{40}-24
8	7	.	15	*°0^{00}-2^{20}; = 0^{00}-2^{40}; ⊕' 10^{40}-13^{50}
9	7	.	14	= a, np
10	7	0.0	12	* 13^{04-15}, 17^{45}-18^{15}; = na
11	7	0.0	11	•°15^{48}-17^{30}; = 4^{40}-5^{20}, 6^{20}-10^{40}, 17^{50}-24
12	6	8.1	5	•°14^{48}...15^{30}-21^{40} *°22^{45}-23^{20} •°-24; = 0^{00}-17^{44} ≡°-21^{45} = -23^{20}
13	8	0.0	2	•°0^{00}-2^{35} *°-6^{15} ⚥°6^{50}...19^{30}; ≫ 6^{10}-9^{40}
14	7	0.0	1	⚥°6^{20}-8^{10}, 11^{50}-12^{15}, 13^{20-35}
15	5	3.6	pż.	*°9^{15}-24; ⊹'14^{50}-24; ≫ 13^{50}-24
16	4	4.4	8	*°0^{00}-24; ⊹'0^{00}-24; ≫ 0^{00}-24
17	5	1.9	30	*°0^{00}-24; ⊹'-°0^{00}-9^{10} ⊹-11^{30}; ≫ 0^{00}-5^{30}
18	6	0.1	31	*°-'0^{00}-14^{35}; ⊹11^{20}-14^{40}
19	8	0.0	31	*°2^{40}-3^{10}, 6^{16}-7^{12}
20	7	.	25	= 7^{20}-10^{30}, 17^{45}-24; ⊔°na-a
21	6	0.2	22	= 0^{00}-6^{45} ≡°-8^{50} = -12^{40}, 18^{30}-24
22	6	2.7	21	*°4^{10}-10^{40}, 11^{50}-24; = 0^{00}-24
23	6	1.4	23	*°0^{00}-4^{40}, 5^{20}-8^{20}, 16^{20}-22^{35}; = 0^{00}-24
24	7	0.0	21	*°3^{50}-7^{50}; = 0^{00}-10^{30}, 17^{26}-24
25	7	0.0	19	*°5^{50}-7^{15}; = 0^{00}-11^{20}
26	7	.	17	= 3^{50}-10^{40}
27	7	.	16	= 2^{30}-4^{10}
28	7	.	16	= 1^{30}-9^{45}, 21^{20}-24
29	7	0.8	7	= 0^{00}-7^{50}
30	7	1.5	pż.	•°5^{20}-9^{45}
31	8	0.2	pż.	•°10^{25}-11^{05}; = 17^{50}-19^{20}
Σ	—	54.9	—	UWAGI

Kwiecień - Avril

1	7	0.4	.	⚥°4^{06-20} •°6^{15}-7^{10} •°13^{03}...14^{04} ⚥°15^{42}-16^{10}; = 7^{10}-8^{15}
2	8	0.1	.	
3	8	.	.	⊔°4-7
4	8	.	.	
5	8	0.0	.	⚥°21^{20-47}, 22^{30}-23^{05}
6	7	16.7	.	•°22^{10}-23^{00} •°-24; = 6^{20}-7^{40}
7	7	3.4	.	•°0^{00}-10^{48}
8	7	0.2	.	*°4^{40}-5^{25}, 6^{45}-7^{10} •°9^{48}-10^{28}
9	8	.	.	
10	7	0.0	.	⚥°18^{10-50}
11	8	.	.	= 2^{30}-6^{28} ≡°-8^{40} = -18^{28}; ⌓°2-8, np
12	7	.	.	= 1^{20}-5^{45} ≡°-'-8^{25} = -10^{34}, 18^{36}-24; ⌓°0^{00}-8; ⊕ 12^{20}-14^{50}
13	7	3.0	.	•°23^{35}-24; = 0^{00}-9^{50}
14	6	1.1	.	•°0^{00}-2^{40}, 3^{20}-7^{40}, 20^{20}-21^{25}; = 3^{50}-7^{45}, 11^{25}-24
15	8	.	.	•°2^{05}-3^{10}; = 0^{00}-10^{30}
16	7	.	.	
17	8	.	.	= 4^{40}-7^{40}
18	7	.	.	= 4^{30}-9^{40}
19	8	.	.	⌓° na-a
20	8	.	.	⌓° na-a
21	7	.	.	= 5^{20}-10^{20}; ⌓° np
22	8	.	.	= 3^{50}-8^{40}; ⌓°0^{00}-6, np
23	8	.	.	⌓° na-a, np
24	8	.	.	⌓° na-a
25	7	.	.	= 3^{45}-8^{25}
26	8	.	.	⌓° na-a, n-np
27	6	4.4	.	⚥°11^{15-30}, 12^{10}-13^{15} •°13^{25}-15^{30}; = 15^{30}-17^{20}; ⌓° na-a
28	7	2.3	.	•°9^{48}...12^{10} ⚥°18^{34-48}
29	8	0.4	.	⚥°4^{10-35} 5^{45}-6^{05}, 13^{25-37}, 16^{01-22}
30	8	.	.	= 6^{25}-7^{10}; ⊔' na
31				
Σ	—	32.0	—	UWAGI

Przemyśl φ = 49°48' λ = 22°46' Maj - Mai 1962

DNI	CIŚNIENIE P - 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N.w			KIERUNEK i PRĘDKOŚĆ WIATRU D.v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	80.7	80.7	81.6	81.0	2.0	5.1	1.8	2.7	6.2	0.6	75	49	91	72	1.8	1.5	0.7	1.3	1	9	0	NW 7	W 7	W 1
2	79.5	77.8	79.3	78.9	1.6	8.5	4.3	4.7	9.4	-2.2	85	50	85	73	1.1	5.6	1.2	2.6	0 ⊙	9	4	W 1	N 1	W 2
3	81.3	81.7	81.0	81.3	3.0	8.0	4.9	5.2	10.3	-2.4	96	67	82	82	0.3	3.5	1.6	1.8	10 ●	8	0	W 1	W 3	W 2
4	77.6	77.8	80.1	78.5	5.5	5.4	6.2	5.8	8.7	-0.7	80	92	91	88	1.8	0.7	0.9	1.1	9	10	8	W 2	W 6	SW 1
5	83.4	84.2	86.6	84.7	5.0	11.9	9.5	9.0	13.1	1.2	89	58	74	74	1.0	5.8	3.1	3.3	3 ⊙	4	10	SW 1	WNW 3	N 3
6	89.6	90.7	90.7	90.3	6.8	12.0	8.4	8.9	13.4	6.3	97	72	86	85	0.3	4.0	1.5	1.9	10	8	0	W 1	N 2	N 1
7	89.6	88.2	87.9	88.6	4.6	17.3	11.8	11.4	18.6	1.4	100	49	97	82	0.0	10.1	0.3	3.5	2 ⊙ ═	6 ⊙	10 ●	W 3	W 2	W 1
8	87.5	86.1	84.5	86.0	12.6	21.5	16.3	16.7	23.0	9.6	93	61	75	76	1.1	10.0	4.5	5.2	8	9	9	W 1	W 2	WSW 3
9	83.1	84.4	84.2	83.9	14.8	18.6	13.8	15.2	19.9	13.5	93	60	88	80	1.1	8.5	2.0	3.9	9	4 ⊙	2	W 4	W 7	C 0
10	78.7	80.1	82.8	80.5	11.6	12.2	11.1	11.5	13.8	10.9	99	99	100	99	0.1	0.2	0.0	0.1	10 ●	10 ●	10	NE 4	NE 5	C 0
11	83.5	83.3	84.4	83.7	11.4	15.1	9.9	11.6	15.5	9.7	94	72	97	88	0.9	4.8	0.3	2.0	9	9	10 ●	NW 1	N 2	W 2
12	86.3	87.0	86.6	86.6	9.4	16.6	12.0	12.5	17.0	7.8	89	54	83	75	1.3	8.7	2.3	4.1	2 ⊙	9	8	W 2	W 1	C 0
13	88.2	87.9	86.2	87.4	12.8	19.3	12.6	14.3	20.1	10.2	88	52	93	78	1.8	10.8	1.1	4.6	1 ⊙	9	10	SE 3	SSW 3	C 0
14	79.3	72.1	72.5	74.6	12.0	24.0	11.9	15.0	25.0	10.0	98	48	87	78	0.3	15.6	1.8	5.9	10	8	10	WSW 1	S 7	W 10
15	74.0	75.4	77.3	75.6	9.6	11.3	8.4	9.4	12.1	7.9	78	76	90	81	2.7	3.3	1.0	2.3	10	10	10	SW 10	WSW 10	WSW 7
16	79.8	83.2	87.2	83.4	7.7	11.6	7.6	8.6	12.4	7.4	96	75	99	90	0.5	3.4	0.1	1.3	10 ●	9	3	W 6	W 7	W 4
17	88.7	87.8	87.1	87.9	8.2	15.6	11.8	11.8	17.4	4.1	83	57	94	78	1.8	7.6	0.8	3.4	5 ⊙	6 ⊙	2	W 2	SW 6	SW 1
18	85.0	88.1	91.9	88.3	11.5	13.3	9.0	10.7	15.4	8.8	91	91	97	93	1.2	1.4	0.3	1.0	10 ●	8	4	W 2	W 4	W 2
19	92.7	89.7	85.8	89.4	8.1	19.3	14.5	14.1	22.4	3.4	94	55	85	78	0.6	10.1	2.5	4.4	3 ⊙	2 ⊙	1	W 1	E 5	C 0
20	82.6	80.7	82.7	82.0	14.3	22.4	11.4	14.9	23.3	10.4	86	70	99	85	2.4	8.3	0.2	3.6	10 ●	10	9 ●	S 2	S 4	W 4
21	84.9	85.1	84.3	84.8	9.4	9.2	9.4	9.4	11.5	9.0	97	100	100	99	0.3	0.0	0.0	0.1	10	10 ●	10 ●	WNW 3	N 3	N 1
22	86.5	87.6	89.5	87.9	9.2	15.6	13.8	13.1	17.7	8.4	93	68	75	79	0.8	5.7	3.9	3.5	8	5	8	W 2	W 4	SW 2
23	91.8	91.1	89.4	90.8	13.0	19.4	15.2	15.7	20.2	8.8	80	58	81	73	3.0	9.3	3.4	5.2	4	8	0	W 1	SW 2	S 1
24	88.9	88.3	86.7	88.0	13.6	19.4	15.2	15.8	20.4	8.8	89	75	92	85	1.8	5.6	1.3	2.9	4 ⊙	7 ⊙	9	S 2	NW 8	N 6
25	83.9	84.7	84.5	84.4	12.8	15.8	12.8	13.6	15.9	12.2	96	83	92	90	0.5	3.0	1.2	1.6	10	10	10	NW 3	NW 3	NW 3
26	82.1	82.6	82.5	82.4	12.8	16.6	17.8	16.2	20.6	11.6	100	96	88	95	0.0	0.8	2.4	1.1	10 ═	10 ● R	7	NNW 1	NW 4	NW 3
27	86.2	86.5	87.0	86.6	14.2	20.6	16.8	17.1	21.6	11.5	88	74	95	86	2.0	6.3	1.0	3.1	9	9	0	W 2	W 2	NNE 2
28	88.5	86.4	85.9	86.9	17.2	23.0	17.5	18.8	23.4	14.3	89	71	96	85	2.2	8.2	0.8	3.7	3 ⊙	7	8	NW 2	NE 3	NE 1
29	88.0	88.4	88.4	88.3	16.5	19.5	13.2	15.6	19.8	12.8	88	72	90	83	2.4	6.3	1.6	3.4	9	6	1	W 2	W 2	C 0
30	86.5	89.8	91.1	89.1	15.2	12.2	10.0	11.8	15.4	9.8	84	87	96	89	2.8	1.9	0.5	1.7	8	10	0	WNW 1	WNW 5	W 1
31	91.3	88.5	85.5	88.4	8.8	19.5	15.7	14.9	21.0	5.4	100	47	62	70	0.0	12.0	6.7	6.2	0 ═	3 ⊙	1	W 2	SSW 2	C 0
M	84.8	84.7	85.0	84.8	10.2	15.5	11.4	12.1	16.9	7.4	91	69	89	83	1.2	5.9	1.6	2.9	6.7	7.8	5.6	2.5	4.0	2.1

Czerwiec - Juin

1	83.8	89.6	87.0	86.8	12.4	9.2	6.1	8.4	16.3	6.1	90	91	95	92	1.4	1.1	0.4	1.0	10 ●	10	10 ● R	W 6	NW 2	NE 4
2	82.2	87.1	91.0	86.8	7.2	8.2	7.3	7.5	8.6	5.1	99	96	96	97	0.2	0.5	0.4	0.4	10	10 ●	10	E 7	WNW 5	NW 3
3	91.8	93.3	93.1	92.7	7.8	8.2	8.6	8.3	9.5	6.8	96	97	96	96	0.5	0.3	0.5	0.4	10	10 ●	10 ●	NW 3	NNW 4	NNW 2
4	91.0	90.5	88.9	90.1	8.3	8.9	6.0	7.3	9.7	5.8	97	93	91	94	0.4	0.8	0.9	0.7	10 ●	10 ●	10	NW 2	W 5	W 6
5	83.4	85.2	85.9	84.8	5.7	6.6	8.1	7.1	8.6	4.8	95	97	99	97	0.5	0.3	0.2	0.3	10 ●	10 ●	10 ●	W 7	W 7	W 7
6	87.0	89.2	91.5	89.2	4.6	4.4	3.4	4.0	8.1	3.4	95	93	97	95	0.4	0.6	0.3	0.4	10 ●	10 ●	10 ●	NW 5	NW 7	NNW 4
7	92.7	94.9	96.6	94.7	5.8	5.4	6.8	5.7	6.9	2.9	100	95	97	97	0.0	0.5	0.3	0.3	10 ●	10 ●	10 ●	NNW 4	NNW 3	NW 2
8	96.4	97.5	96.8	96.9	9.3	14.4	11.4	11.6	15.3	5.0	83	54	85	74	2.0	7.6	2.0	3.9	2 ⊙	9	3	W 2	N 3	NW 1
9	93.7	90.6	86.4	90.2	9.6	19.0	14.5	14.4	19.6	5.5	92	51	64	69	1.0	10.9	6.0	6.0	0 ⊙	5 ⊙	2	W 1	W 4	W 5
10	84.3	83.4	83.3	83.7	13.1	20.6	15.2	16.0	20.9	11.6	75	54	80	70	3.8	11.0	3.5	6.1	5	6	9	W 3	W 3	W 2
11	81.5	79.3	80.1	80.3	12.4	22.2	15.1	16.2	22.7	8.2	95	50	87	77	0.7	13.4	2.3	5.5	1 ⊙	4 ⊙	10	WNW 1	W 2	C 0
12	82.7	83.7	85.4	83.9	11.0	14.0	11.4	12.0	15.1	10.8	96	72	73	80	0.5	4.4	3.6	2.8	10 ●	10	2	NW 3	NW 2	WNW 3
13	87.8	89.2	90.3	89.1	10.6	14.0	11.8	12.0	16.4	7.2	85	75	82	81	2.0	4.1	2.5	2.9	2 ⊙	9	7	W 2	W 4	C 0
14	91.0	90.0	89.6	90.2	10.6	20.5	15.6	15.6	21.0	6.5	87	48	66	67	1.6	12.5	6.0	6.7	1 ⊙	8	2	W 2	SW 4	SW 3
15	91.6	91.7	92.4	91.9	16.5	24.8	20.9	20.8	26.4	12.6	70	60	71	67	5.7	12.4	7.2	8.4	2 ⊙	4 ⊙	0	W 3	WSW 3	WSW 2
16	93.6	92.8	91.2	92.5	17.0	27.4	20.7	21.4	28.0	13.0	91	55	84	77	1.8	16.3	4.0	7.4	0 ⊙	1 ⊙	0	W 1	NNE 3	C 0
17	90.8	91.4	91.5	91.2	19.6	24.0	19.0	20.4	24.4	15.4	77	65	84	75	5.3	10.5	3.6	6.5	10 (R)	4 ⊙	10 ● R	W 4	WNW 3	NW 3
18	91.6	91.5	90.2	91.1	16.5	19.2	17.8	17.8	22.3	15.1	92	82	74	83	1.6	4.0	5.4	3.7	10	9	6	NW 1	NW 1	NW 2
19	90.1	88.4	86.5	88.3	13.4	23.8	19.4	19.0	24.4	11.1	100	64	87	84	0.0	10.7	3.0	4.6	0 ═ ⊙	4 ⊙	0	NW 2	E 7	C 0
20	86.6	87.0	89.7	87.8	19.4	25.6	19.4	21.0	27.0	12.9	82	69	86	76	4.0	10.2	3.2	5.8	0 ⊙	2 ⊙	2	WSW 3	W 3	WNW 1
21	92.3	92.7	92.7	92.6	18.1	23.2	19.0	19.8	24.1	15.7	91	61	89	80	1.9	11.1	2.4	5.1	5	7	10 ●	W 1	E 3	C 0
22	94.8	95.0	94.6	94.8	19.0	24.7	18.8	20.3	25.1	16.7	87	57	86	77	2.8	13.5	3.1	6.5	0 ⊙	4 ⊙	0	W 1	NW 3	C 0
23	94.6	93.4	91.5	93.2	16.6	26.8	21.2	21.4	28.2	12.7	95	53	79	76	1.0	16.6	5.2	7.6	0 ⊙	2 ⊙	1	WNW 1	W 3	C 0
24	90.2	90.3	88.5	89.7	22.0	26.1	19.3	21.7	27.1	16.5	77	62	98	79	6.2	13.0	0.5	6.6	2 ⊙	3 ⊙	7	W 3	NW 3	C 0
25	86.3	86.3	89.2	87.3	20.8	25.9	19.0	21.2	27.1	15.3	85	61	67	71	3.8	13.1	7.4	8.1	1 ⊙	2 ⊙	10	W 3	NW 6	WNW 2
26	91.1	88.6	86.0	88.6	13.9	18.4	14.4	15.3	19.0	11.2	69	53	89	70	4.9	10.0	1.8	5.6	8	7	4	NW 3	E 2	C 0
27	83.8	83.1	84.4	83.8	12.2	20.0	15.7	15.9	20.1	9.6	98	63	65	75	0.3	8.6	6.2	5.0	7	10	10	S 2	W 3	W 3
28	85.3	84.9	83.8	84.7	11.0	14.5	10.2	11.5	16.6	9.9	89	62	87	79	1.5	6.3	1.6	3.1	10	9	6	WNW 1	W 5	C 0
29	82.5	84.0	84.8	83.8	10.4	13.8	12.4	12.2	15.3	8.2	82	66	74	74	2.2	5.4	3.7	3.8	4 ⊙	7	8	W 7	WNW 8	W 4
30	84.3	85.0	86.6	85.3	11.8	15.0	11.1	12.2	16.0	8.1	78	62	89	76	3.0	6.4	1.5	3.6	2 ⊙	9	9 ●	W 6	W 7	W 3
31																								
M	88.6	89.0	89.0	88.9	12.8	17.6	14.0	14.6	19.0	9.8	88	69	84	80	2.0	7.9	3.0	4.3	5.1	6.8	5.3	3.0	3.9	2.1

Przemyśl $H_s = 237m$ $H_b = 238{,}9m$ $h_w = 20{,}6m$ Maj - Mai 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ SNIEGU h	POGODA
1	8	•	•	
2	8	0.0	•	⌴°1-6
3	7	0.8	•	⚲°4^05-15, 6^20-7^10; ⌓° na
4	6	1.0	•	⚲°4^20-40 •°7^25-8^50, 10^30-40, 12^40...13^10
5	7	4.8	•	•°21^10-20; =5^40-7^40; ⌓°1-8
6	7	•	•	⚲°1^40-50, 2^10-3^20 •°-4^40; =3^10-10^40, nn; ⌓' nn
7	7	0.4	•	•°17^40-19^10, 20^20...21^04; =0^00-2^30 ≡°-7^50 = 22^10-24; ⌓² 0^00-7
8	8	6.7	•	⚲'17^15-20 •°23^10-24; ⚿°17^10-50; =0^00-9^30
9	7	2.4	•	•°0^00-1^20, 2^15-50 •'-4^35; =2^10-6^40
10	6	16.0	•	•°4^50-6^40 •°-7^15 •°-14^15, 17^20-18^40 •°19^35-20^10; =3^30-24
11	7	13.4	•	⚲°15^50-16^10 •°'-22^15; =0^00-4^40, 22^15-24
12	8	0.5	•	=0^00-1^50; ⊕11^30-12^40
13	7	3.8	•	⚲°3^20-35 •°15^40-16^10
14	8	3.5	•	•°'0^00-4^45 •°5^05-6^10 ⚲°'16^50-17^45 ⚲°21^35-22^10; ⚿°17^25-18^20; ⩔ 20^15-21^30; =4^45-8^20
15	7	7.1	•	•°6^10-13 ⚲°10^50-11^15 ⚲°'22^35-24; ⩔ 5^40-16^45
16	7	0.8	•	•'°0^00-8^20 ⚲°19^40-20^10
17	8	0.5	•	⚲°17^50-18^10, 19^45-20^03
18	7	11.9	•	•°'6^15-10^50 ⚲°14^10-15^10
19	7	0.0	•	≡°2^45-4^50 ≡²-5^40 = -8^25
20	7	20.0	•	•°6^20-7^10, 14^00-18 ⚲°17^20-42, 19^40-20^35 •°21^50...22^10 ⚲°'-24; ⚿°22^50-24; ⌓² na
21	6	3.4	•	⚲'°0^00-30 •°1^10-2^15 •°²10^10-11^45 •°12^15-21^10; ⚿°0^00-40; =9^20-23^20
22	8	0.0	•	•°21^40...22^10; =3^30-5^50
23	8	•	•	⌓° nn
24	7	•	•	⌓' 0^00-8 ⌓° 22-24
25	6	•	•	=6^40-24; ⌓°0^00-7
26	6	8.1	•	⚲°'12^04-40 ⚲°21^45-22^05; ⚿11^25-13^30 ⚿°21^40-22^45; =0^00-4^50 ≡°'-7^35 = -14^10, 19^25-22^15
27	7	1.7	•	⚲°14^50-15^45; ⚿°14^45-15^15; =20^20-24
28	7	5.5	•	⚲°14^35-15^25, 16^35-17^10; ⚿°13^35-15^40, 16^25-17^40; =0^00-9^20
29	7	0.9	•	⚲°7^05-18, 16^03-28; ⚿°15^45-16^40, 22^50-24; =10^30-11^45
30	6	2.0	•	•°11^18-32 •°13^50-15^04, 15^28-16^26; ⚿°0^00-40; =4^50-24
31	7	0.3	•	=0^00-6^45 ≡°-9^10 = -9^30; ⌓' nn
Σ	—	115.5	—	UWAGI

Czerwiec - Juin

1	6	14.9	•	⚲°6^50-9^45 •°-12^45, 14^45-17^20 ⚲'°-18^45, 20^10-21^10...24; ⚿°17^50-18^40, 20^45-22^40; ⌓' na
2	6	9.0	•	⚲°0^00-24 ▲°-0^26 ⚲°-0^46, 2^03-4^10 •°8^35-9^10 •'°-13^55 •°15^15-17^50; ⚿°0^35-2^45, 10^25 (pojed. grzmot); =8^20-15^50
3	7	8.4		•°8^45-9^36 ⚲°10^00-12 •°10^42...16^25, 21^25-24
4	7	13.5	•	•°0^00-14^40, 15^40-17^20; =3^20-11^15
5	6	14.3	•	•°0^25-1^25 •°'-1^50-16^35 •°17^45...20^05-24
6	6	12.8	•	•°0^00-3^25, 10^15...17^20 ⚲°18^07...19^30 •°20^10-24
7	6	6.4	•	•°0^00-7^10 •°-10^40 •'11^15-12^30 •°-14^20, 15^20-23^45; =5^40-21^30
8	8	•	•	
9	8	•	•	⌓' 2-9
10	7	•	•	⌓° 21-24
11	7	4.2	•	⚿°15^20-17^40; =1^40-8^20; ⌓' 0^00-8
12	7	3.3	•	•°'4^50-11^25 ⚲°13^55-14^20
13	8	•	•	⌓' nn
14	8	•	•	⌓' na-a
15	7	•	•	⌓° nn
16	7	•	•	=2^20-10^30, 20^40-24; ⌓' 0^00-9 ⌓° nn
17	7	10.7	•	⚲°10^30-40, 16^05-15 ⚲²-°21^20-23^15; (⚿)6^45-9^40, 19^50-21^20 ⚿'-22^45; =0^00-4^30; ⌓' na
18	7	0.0	•	•°10^45...12^20 ⚲°13^15-25; =0^30-6^45 a, nn
19	7	•	•	=0^00-4^40 ≡°'-7^45 = -11^20; ⌓°'2-9 ⌓' nn
20	7	0.2	•	⚲°12^35-13^05; =0^30-3^40 ≡°-5^50 = 6^30-8^30; ⌓² 0^00-8
21	8	2.7	•	•°21^07-23^20; =4^40-8^50
22	7	•	•	=4^30-10^25, 21^20-24; ⌓° nn
23	7	•	•	=0^00-9^30, 22^40-24; ⌓ °-²0^00-a ⌓° nn
24	7	14.4	•	⚲²-°17^40-18^35; ⚿17^40-18^40; =0^00-5^40, 20^30-24; ⌓' na
25	7	•	•	=0^00-50 ≡°'-5^50 = -7^20, 22^30-24; ⌓' nn
26	8	•	•	=0^00-3^40; ⌓' 0^00-9
27	7	0.0	•	=2^00-4^40, 7^20-9^50, 20^50-22^30; ⌓'-² 0^00-8
28	7	2.5	•	•°5^45-6^15, 23^50-24
29	8	0.2	•	•°0^00-1^50 ⚲°'5^05-6^15 ⚲°9^15-35, 10^55-11^04, 11^49-55
30	7	0.6	•	•°18^10-20, 21^15-30; =19^20-22^40
31				
Σ	—	118.1	—	UWAGI.

Przemyśl φ = 49°48' λ = 22°46' Lipiec - Juillet 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	87.1	88.0	88.0	87.7	11.8	12.4	11.0	11.6	16.1	10.1	96	95	97	96	0.5	0.7	0.3	0.5	9	9 ●	2	W 4	NW 4	C 0
2	87.4	86.2	84.4	86.0	11.6	12.4	10.6	11.3	15.3	10.1	98	90	99	96	0.3	1.4	0.2	0.6	10	10 ●⚡	2	C 0	WNW 3	C 0
3	79.9	76.6	75.6	77.4	11.7	16.8	11.6	12.9	16.9	8.4	93	75	96	88	1.0	4.8	0.5	2.1	8	9	10	W 1	SW 6	C 0
4	74.4	76.7	77.4	76.2	11.2	10.9	11.4	11.2	13.5	9.4	97	95	94	95	0.3	0.6	0.9	0.6	10 ●	10 ●	9	SW 1	NW 1	C 0
5	79.5	80.2	82.5	80.7	12.0	16.5	13.0	13.6	17.6	9.8	93	70	96	86	1.0	5.7	0.6	2.4	10	9	10	S 1	ESE 3	C 0
6	87.6	88.3	88.5	88.1	12.8	17.3	14.9	15.0	18.9	9.9	81	65	87	78	2.8	6.9	2.2	4.0	2 ⊙	9	9	W 4	W 1	C 0
7	88.7	87.3	88.6	88.2	12.1	19.5	13.7	14.8	20.4	9.1	95	67	93	85	0.7	7.5	1.1	3.1	9 ●	8	8	SW 1	NW 1	NW 1
8	89.1	89.8	90.9	89.9	10.9	12.4	11.5	11.6	16.0	10.3	95	96	95	95	0.6	0.5	0.7	0.6	8	10	1	W 3	W 2	WNW 1
9	92.1	91.3	89.6	91.0	12.4	17.0	14.0	14.4	19.2	8.4	93	72	79	81	1.0	5.4	3.4	3.3	8	5 ⊙	1	W 4	W 3	W 2
10	88.1	86.7	85.2	86.7	13.2	20.2	15.0	15.8	21.4	7.6	85	62	77	75	2.3	9.1	3.8	5.1	3	5 ⊙	1	W 3	WNW 7	W 1
11	85.2	84.2	82.4	83.9	15.8	23.2	19.2	19.4	25.1	10.2	81	53	85	73	3.3	13.4	3.4	6.7	0 ⊙	3	5	W 4	WSW 5	W 2
12	80.8	81.2	80.9	81.0	18.2	22.8	18.6	19.6	24.0	16.6	93	70	85	83	1.5	8.3	3.3	4.4	10	5 ⊙	1	W 3	W 3	C 0
13	80.0	79.4	80.8	80.1	15.1	21.7	14.2	16.3	21.9	13.0	96	77	92	88	0.8	6.0	1.3	2.7	10	8 ⊙	4	C 0	W 3	C 0
14	80.9	80.6	81.0	80.8	13.2	18.6	14.1	15.0	18.9	9.7	91	73	100	88	1.4	5.7	0.0	2.4	9	9	10	W 3	W 5	SW 1
15	80.8	80.5	79.2	80.2	14.8	21.3	15.7	16.9	21.7	12.4	90	70	87	82	1.6	7.5	2.2	3.8	0 ⊙	4 ⊙	3	SW 1	SW 4	C 0
16	79.4	79.7	80.7	79.9	17.6	19.0	14.5	16.4	21.8	13.5	89	92	99	93	2.2	1.8	0.2	1.4	1	10 ●⚡	2	C 0	WNW 4	W 1
17	82.4	82.9	84.0	83.1	13.8	21.9	17.3	17.6	22.7	11.4	99	64	98	87	0.2	9.4	0.4	3.3	0 ═ ⊙	8	10 ●	W 1	NE 2	SE 2
18	83.3	82.3	81.2	82.3	15.6	17.2	16.1	16.2	17.8	14.9	99	94	95	96	0.2	1.2	1.0	0.8	10	10 ●	10 ●	NW 3	NNE 4	NW 6
19	80.3	81.4	84.6	82.1	15.4	17.2	15.6	16.0	17.2	15.1	96	94	92	94	0.8	1.2	1.3	1.1	10 ●	10	10 ●	NW 5	NW 7	NW 5
20	88.3	89.3	90.3	89.3	16.6	21.6	15.6	17.4	22.8	13.9	79	55	88	74	4.1	11.5	2.1	5.9	2 ⊙	5 ⊙	0	W 2	NW 3	C 0
21	91.1	90.4	89.4	90.3	15.5	25.1	18.3	19.3	25.5	10.6	83	43	73	66	3.0	18.1	5.6	8.9	0 ⊙	1 ⊙	0	W 2	E 2	C 0
22	90.0	89.0	88.7	89.2	16.8	26.7	20.7	21.2	27.3	11.6	83	58	76	72	3.3	14.7	5.9	8.0	0 ⊙	2 ⊙	0	C 0	SE 2	SE 1
23	89.5	90.1	91.6	90.4	18.9	18.8	16.4	17.6	21.9	16.2	87	89	93	90	2.7	2.3	1.3	2.1	9	10	6 ⚡	W 3	NW 3	N 1
24	93.5	94.3	94.9	94.2	17.0	20.6	15.8	17.3	21.9	14.5	96	56	80	77	0.8	10.6	3.5	5.0	6	5 ⊙	1	W 2	NW 3	C 0
25	96.8	96.6	95.6	96.3	13.6	20.8	16.2	16.7	22.4	9.7	87	52	78	72	2.0	11.8	4.0	5.9	0 ⊙	5 ⊙	0	W 3	NW 4	C 0
26	94.4	92.1	90.5	92.3	16.5	27.7	22.0	22.0	28.4	10.6	78	42	64	61	4.3	21.4	9.6	11.8	0 ⊙	0 ⊙	0	C 0	SW 4	SW 1
27	89.3	88.3	87.8	88.5	23.7	30.1	19.7	23.3	30.7	19.4	71	54	91	72	8.6	19.4	1.9	10.0	0 ⊙	4 ⊙	10	W 1	W 3	W 1
28	88.6	90.4	89.8	89.6	15.5	18.4	14.8	15.9	19.9	14.7	79	58	69	69	3.7	8.9	5.2	5.9	1	5 ⊙	2	W 5	W 7	W 3
29	91.6	90.8	91.1	91.2	13.3	17.0	12.3	13.7	18.5	9.6	81	57	90	76	3.0	8.3	1.4	4.2	1 ⊙	8	0	W 2	NNW 3	N 1
30	92.4	91.9	91.3	91.9	10.8	20.7	16.2	16.0	21.6	7.1	94	47	76	72	0.9	12.8	4.4	6.0	0 ⊙	5 ⊙	10	W 2	E 3	ENE 3
31	92.4	93.0	92.9	92.8	13.7	14.4	12.4	13.2	16.9	12.1	93	91	96	93	1.1	1.4	0.5	1.0	9	10	0	NE 3	NNE 4	C 0
M	86.6	86.4	86.4	86.5	14.6	19.4	15.2	16.1	20.8	11.6	89	70	88	82	1.9	7.7	2.3	4.0	5.0	6.8	4.4	2.2	3.5	1.1

Sierpień - Août

1	92.7	90.6	90.2	91.2	10.6	23.5	14.8	15.9	24.7	7.4	100	46	96	81	0.0	15.7	0.7	5.5	0 ═ ⊙	5 ⊙	8	SW 2	SW 2	W 3
2	89.5	89.3	88.9	89.2	15.4	21.0	15.4	16.8	22.3	13.1	92	55	90	79	1.3	11.3	1.7	4.8	5 ⊙	3 ⊙	0	W 2	W 2	C 0
3	87.0	87.1	87.6	87.2	13.8	22.6	18.5	18.4	24.3	10.0	94	79	97	90	0.9	5.9	0.7	2.5	2	10	8	W 1	NW 2	C 0
4	88.5	88.9	88.1	88.5	16.5	23.8	20.6	20.4	25.8	15.8	100	74	93	89	0.0	7.6	1.5	3.0	10 ═	2 ⊙	0	C 0	ESE 2	E 1
5	87.4	85.0	82.1	84.8	19.7	26.8	20.7	22.0	27.5	17.3	93	64	94	84	1.5	12.6	1.4	5.2	4 ⊙	2 ⊙	10	W 2	N 3	C 0
6	83.6	84.5	85.7	84.6	19.4	26.3	18.2	20.5	26.8	16.0	84	62	94	80	3.6	12.8	1.3	5.9	0 ⊙	7 ⊙	1	W 3	W 4	C 0
7	84.4	82.0	79.9	82.1	17.5	29.9	25.0	24.4	30.4	13.9	94	47	69	70	1.2	22.5	9.8	11.2	0	1 ⊙	0	C 0	S 7	SE 6
8	89.4	89.9	90.3	89.9	16.1	21.7	18.2	18.6	25.9	15.7	93	67	90	83	1.3	8.5	2.1	4.0	10 ●⚡	9	2	W 3	SW 1	C 0
9	93.4	93.9	94.6	94.0	16.4	20.8	17.4	18.0	20.8	15.8	89	64	87	80	2.1	8.8	2.6	4.5	10	10	9	C 0	NW 5	C 0
10	95.0	93.0	90.5	92.8	14.0	21.6	18.3	18.0	22.4	12.1	92	63	92	82	1.3	9.7	1.6	4.2	9	3 ⊙	1	C 0	E 7	E 1
11	89.5	89.4	89.8	89.6	14.6	24.9	18.6	19.2	25.5	12.6	100	51	84	78	0.0	15.5	3.5	6.3	0 ═	3 ⊙	6	SW 3	W 4	C 0
12	91.8	91.2	90.5	91.2	15.2	27.1	21.8	21.5	27.9	12.6	94	56	81	77	1.0	15.6	4.8	7.1	1	2 ⊙	2	W 1	E 5	C 0
13	90.9	90.3	89.4	90.2	18.1	29.1	20.8	22.2	30.0	14.6	88	50	86	75	2.5	20.2	3.4	8.7	5	4	2	C 0	WSW 2	SW 3
14	89.2	88.9	88.3	88.8	19.3	26.6	19.8	21.4	27.3	17.7	89	61	82	77	2.6	13.5	4.1	6.7	2 ⊙	1 ⊙	0	W 2	NW 5	C 0
15	87.3	85.8	82.4	85.2	16.4	27.5	22.4	22.2	28.1	13.9	97	64	90	84	0.6	13.2	2.7	5.5	1 ═	2 ⊙	8	C 0	SE 4	S 1
16	83.3	84.1	86.5	84.6	20.1	17.9	17.3	18.2	23.3	17.3	81	95	98	91	4.5	1.0	0.4	2.0	9	10 ●⚡	0	W 1	NW 1	NW 1
17	87.1	86.7	84.7	86.2	15.6	23.9	18.5	19.1	24.4	13.5	99	63	87	83	0.2	10.9	2.7	4.6	1 ═ ⊙	6 ⊙	8	W 2	NNE 2	C 0
18	83.0	83.3	86.2	84.2	17.6	23.2	15.8	18.1	24.2	14.0	87	69	86	81	2.6	8.9	2.4	4.6	8	6 ⊙	10 ●	SW 2	SW 4	W 4
19	87.3	87.1	87.4	87.3	12.8	15.3	11.2	12.6	17.4	10.7	86	68	86	80	2.1	5.7	1.8	3.2	3	9	0	W 3	W 5	SW 5
20	83.6	83.7	84.9	84.1	12.9	14.3	14.8	14.2	15.4	10.7	86	89	87	87	2.1	1.8	2.2	2.0	10	10 ●	9	W 7	W 7	W 6
21	85.7	86.0	86.6	86.1	14.9	19.2	13.8	15.4	19.9	13.5	89	61	90	80	1.8	8.7	1.6	4.0	9	4 ⊙	0	WNW 5	NNW 5	C 0
22	87.3	88.0	89.9	88.4	11.5	22.4	15.7	16.3	23.0	9.4	97	56	91	81	0.4	12.0	1.5	4.6	9	7	10	W 1	WSW 2	C 0
23	89.2	90.1	91.1	90.1	14.8	19.7	13.6	15.4	20.9	13.4	99	62	90	84	0.2	8.6	1.6	3.5	10	8	1	W 1	W 5	C 0
24	89.7	88.1	84.1	87.3	13.4	20.0	21.0	18.8	21.6	11.1	96	65	56	72	0.6	8.2	10.9	6.6	10	10	0	C 0	SSW 6	SW 6
25	86.5	86.7	89.5	87.6	16.4	21.3	16.0	17.4	22.5	15.8	91	72	93	85	1.7	7.1	1.4	3.4	10 ●	9	5	W 2	W 2	C 0
26	93.2	94.2	94.3	93.9	12.9	19.5	12.0	14.1	20.1	11.8	95	59	93	82	0.7	9.2	1.0	3.6	1	4 ⊙	0	W 2	W 6	C 0
27	91.4	87.6	86.4	88.5	11.8	26.5	20.5	19.8	26.8	8.8	85	50	70	68	2.0	17.3	7.3	8.9	9	1 ⊙	0	S 2	SW 3	SW 1
28	91.2	91.8	92.5	91.8	15.4	20.2	13.1	15.4	20.5	12.8	80	49	77	69	3.5	12.1	3.5	6.4	8	7	0	W 2	W 6	C 0
29	92.5	90.7	88.1	90.4	9.0	22.2	17.4	16.5	23.6	6.1	93	50	85	76	0.8	13.4	3.0	5.7	0	5 ⊙	10	W 1	W 2	W 2
30	90.7	91.7	92.5	91.6	13.3	17.0	10.2	12.7	17.4	10.2	81	57	82	73	3.0	8.3	2.2	4.5	8	5	0	W 5	W 5	W 1
31	90.3	87.2	86.8	88.1	8.6	18.2	12.4	12.9	18.2	6.3	89	51	74	71	1.3	10.2	3.7	5.1	8	9	0	W 2	WSW 4	C 0
M	88.8	88.3	88.1	88.4	15.0	22.4	17.2	18.0	23.5	12.7	91	62	86	80	1.5	10.9	2.9	5.1	5.3	5.6	3.5	1.8	3.9	1.3

Nr	Widzialność V	Opad R	Grubość pokrywy	POGODA
1	7	6.5	•	$\overset{*}{\nabla}{}^{\circ}0^{50}-1^{30}, 13^{10}-14^{25}, 15^{20-30}, = 3^{10}-8^{30}$
2	6	3.0	•	$\bullet^{0-1}2^{05}-5^{10}, 8^{10}-9^{20}\overset{*}{\nabla}{}^{\circ}13^{03}\ldots 17^{35}, \mathfrak{K}^{\circ}13^{46}-14^{15}, = 5^{10}-11^{30}, 21^{10}-24$
3	8	3.8	• $\bullet^{\circ}9^{50}-10^{05}\overset{*}{\nabla}{}^{\circ}11^{50}-12^{10}\overset{*}{\nabla}{}^{0-1}14^{08-47}\overset{*}{\nabla}{}^{\circ}19^{20-35}, = 0^{00}-6^{40}$
4	6	3.8	• $\bullet^{\circ}7^{20}-11^{35}, 13^{15-50}, = 21^{20}-23^{10}$
5	7	3.5	• $\bullet^{\circ}19^{15}-20^{20}\bullet'-21^{10}\bullet^{\circ}-21^{19}, = 4^{40}-9^{30}$
6	8	0.0	• $\triangle np$
7	7	1.2	• $\overset{*}{\nabla}{}^{\circ}6^{55}-7^{05}\bullet^{\circ}-8^{02}\overset{*}{\nabla}{}^{\circ}22^{45}-23^{05}, = 3^{40}-6^{50}, \triangle' na$
8	7	1.7	• $\bullet^{\circ}0^{35}-2^{45}\overset{*}{\nabla}{}^{\circ}8^{50}-9^{30}\bullet^{\circ}11^{35}-13^{15}\overset{*}{\nabla}{}^{\circ}16^{50}-17^{02}\overset{*}{\nabla}{}^{\circ}18^{22-45}\overset{*}{\nabla}{}^{\circ}19^{50}-20^{05} = 5^{40}-8^{20}$
9	8	•	• $\triangle' np$
10	7	•	• $\triangle^{2} na-a$
11	8	•	•
12	7	5.4	• $= 20^{35}-22^{30}, \triangle^{\circ}3-7$
13	7	0.5	• $\overset{*}{\nabla}{}^{1-\circ}2^{25}-4^{05}\bullet^{\circ}10^{42}-11^{02}\overset{*}{\nabla}{}^{\circ}14^{38}\ldots 16^{06}, \mathfrak{K}^{\circ}2^{05}-4^{35}, 14^{25}-15^{20}, \triangle^{\circ} na$
14	8	0.5	• $\overset{*}{\nabla}{}^{0-1}15^{40}-16^{15}$
15	7	•	• $= 2^{10}-4^{40}, \triangle^{\circ} np$
16	7	9.5	• $\overset{*}{\nabla}{}^{\circ}11^{50}-12^{00}\overset{*}{\nabla}{}^{0-1}13^{12}-14^{10}\ 17^{15}-19^{21}, \mathfrak{K}^{\circ}12^{50}-14^{20}\ 16^{47}-18^{45}, \triangle^{\circ}0^{00}-8, \frown^{\circ}18^{48}-19^{08}$
17	7	6.2	• $\overset{*}{\nabla}{}^{\circ}19^{15}-20^{45}, 21^{10-42}, \mathfrak{K}^{\circ}18^{50}-19^{35}, \equiv^{\circ}2^{50}-7^{40} = -8^{50}, 22^{30}-24$
18	6	28.1	• $\overset{*}{\nabla}{}^{0-1}0^{20}-2^{45}\bullet^{\circ}4^{00}-5^{20}\bullet^{0-1}8^{10}-23^{20}, = 0^{00}-23^{30}$
19	7	18.4	• $\bullet^{0-1}1^{30}-9^{34}\ldots 12^{16}, 13^{50}-22^{05}$
20	8	•	• $\triangle^{\circ} np$
21	8	•	• $\triangle^{1-2}0^{00}-8$
22	8	•	• $\triangle^{2}0^{00}-9$
23	6	5.8	• $\overset{*}{\nabla}{}^{\circ}9^{15-35}\overset{*}{\nabla}{}^{\circ}10^{05}-11^{55}\bullet^{\circ}12^{35}\ldots 13^{20}\overset{*}{\nabla}{}^{\circ}20^{40}-21^{05}, \mathfrak{K}^{\circ}20^{45}-21^{40}, = 11^{20}-15^{40}$
24	7	•	• $= 3^{20}-5^{40}, 6^{45}-10^{20}, \triangle^{2} np$
25	8	•	• $= 3^{30}-8^{20}, \triangle^{2} na-a$
26	7	•	• $= 3^{20}-8^{30}, \triangle^{2}0^{00}-9\ \triangle^{\circ} np$
27	7	0.9	• $\overset{*}{\nabla}{}^{\circ}17^{10-25}, 22^{25-29}, \mathfrak{K}^{\circ}16^{50}-20^{45}, 21^{55}-24, = 6^{30}-8^{11}, \triangle^{\circ}0^{00}-2^{00}, \frown 18^{45}-19^{00}$
28	8	•	• $\overset{*}{\nabla}{}^{\circ}0^{45}-1^{15}, \mathfrak{K}^{\circ}0^{00-35}$
29	8	•	• $\triangle' na-a\ \triangle^{\circ} np$
30	8	0.9	• $\triangle^{0-2}0^{00}-8$
31	7	5.0	– $\overset{*}{\nabla}{}^{\circ}5^{15}-6^{20}\bullet^{0-1}9^{40}\ldots 13^{10}$
Σ	–	104.5	– UWAGI

Sierpień - Août

1	8	9.9	• $\overset{*}{\nabla}{}^{2-\circ}16^{35}-17^{10}\overset{*}{\nabla}{}^{\circ}19^{35}-20^{06}, \mathfrak{K}'16^{36}-17^{08}, 19^{38}-20^{35}, \equiv^{0-1}2^{00}-8^{35} = -9^{15}, 22^{10}-24$
2	7	•	• $= 0^{00}-9^{20}$
3	6	0.1	• $\bullet^{\circ}12^{10-25}, 15^{51}-16^{07}, \mathfrak{K}^{\circ}16^{48}-17^{32}, 19^{26}-20^{40}, = 0^{15}-24, \triangle^{2}2-10$
4	6	•	• $= 0^{00}-4^{20} \equiv^{0-1}-9^{50} = -14^{50}\ 19^{40}-24, \triangle^{\circ}20-24$
5	7	5.6	• $\overset{*}{\nabla}{}'15^{05}-16^{05}\overset{*}{\nabla}{}^{\circ}22^{55}-23^{35}, 23^{47-55}, \mathfrak{K}^{\circ}14^{35}-16^{20}, 21^{45}-23^{20}, = 0^{00}-11^{30}, \triangle^{0-2}0^{00}-8$
6	8	0.0	• $\overset{*}{\nabla}{}^{\circ}0^{04-15}, 15^{12-18}, \mathfrak{K}^{\circ}15^{16-45}, \triangle' np$
7	8	2.0	• $= 2^{15}-3^{45} \equiv^{0-1}-6^{30} = -8^{30}, \triangle^{2}0^{00}-8$
8	7	1.5	• $\overset{*}{\nabla}{}^{\circ}7^{00-40}, 8^{05-36}, \mathfrak{K}^{\circ}6^{50}-7^{40}, \triangle^{2} np$
9	7	0.7	• $\bullet^{\circ}5^{50}-6^{20}\overset{*}{\nabla}{}^{\circ}-6^{50}, 8^{05-38}, \mathfrak{K}^{\circ}6^{20-55}, 8^{05}-9^{05}, 10^{50}-11^{40}, \triangle^{2}0^{00}-5$
10	8	•	• $= 4^{20}-7^{15}, 23^{20}-24, \triangle' 21-24$
11	7	•	• $= 0^{00}-2^{50} \equiv^{0-2}-8^{20} = -9^{05}, \triangle^{1-2}0^{00}-a\ \triangle^{\circ} np$
12	7	•	• $= 3^{30}-10^{40}, \triangle^{0-2}0^{00}-9^{00}-\triangle^{\circ} np$
13	7	•	• $= 1^{50}-9^{20}, 23^{20}-24, \triangle^{1-2}0^{00}-a\ \triangle^{\circ} np$
14	7	•	• $= 0^{00}-9^{15}, \triangle^{\circ}0^{00}-8\ \triangle' 22-24$
15	7	•	• $= 2^{30}-4^{50} \equiv^{0-1}-8^{20} = -11^{05}$
16	6	7.4	• $\overset{*}{\nabla}{}^{0-2}11^{35}-12^{48}\overset{*}{\nabla}{}^{\circ}13^{04-50}, \mathfrak{K}^{\circ}12^{12}-13^{35}, = 22^{20}-24$
17	7	•	• $= 0^{00}-5^{40} \equiv^{\circ}-7^{55} = -11^{30}, \triangle' 22-24$
18	7	1.7	• $\overset{*}{\nabla}{}^{\circ}9^{15}\ldots 10^{10}, 15^{20}\ldots 20^{40}\bullet^{\circ}21^{10}-24, = 1^{20}-3^{30} \equiv^{\circ}-6^{50} = -7^{15}, \triangle^{2}0^{00}-9$
19	7	0.2	• $\bullet^{\circ}0^{00-20}\overset{*}{\nabla}{}^{\circ}18^{50}-19^{10}, = 4^{30}-9^{50}, \triangle^{2}2-9$
20	6	3.1	• $\overset{*}{\nabla}{}^{\circ}6^{05-10}\bullet^{\circ}8^{40}-12^{35}\bullet^{\circ}13^{20}\ldots 14^{40}\bullet^{\circ}15^{45}-16^{20}\bullet'23^{15}-24$
21	7	•	• $\bullet^{\circ}0^{00-20}, = 4^{30}-9^{40}$
22	7	17.9	• $\overset{*}{\nabla}{}'23^{01}-24, \mathfrak{K}'22^{50}-24, = 0^{50}-11^{30}, 16^{40}-24, \triangle^{2}2-10$
23	7	•	• $\overset{*}{\nabla}{}'0^{00}\ldots 5^{05}\bullet^{\circ}5^{45}-6^{10}, \mathfrak{K}'0^{00}-3^{30}, = 0^{00}-9^{40}, 20^{20}-24, \triangle' 19-24$
24	7	0.4	• $= 0^{00}-8^{40}, \triangle^{2}0^{00}-8$
25	7	3.8	• $\overset{*}{\nabla}{}^{\circ}5^{15-50}, 6^{45}-8^{15}\bullet^{\circ}8^{40}-9^{35}\overset{*}{\nabla}{}^{\circ}13^{32}-14^{20}\overset{*}{\nabla}{}^{2}17^{50}-18^{00}\overset{*}{\nabla}{}'-18^{20}, = 19^{30}-24$
26	7	•	• $= 0^{00}-7^{15}, \triangle' np$
27	8	•	• $= 0^{20}-9^{15}, \triangle^{2}0^{00}-8$
28	8	•	• $\triangle^{\circ}0^{00}-7, 22-24$
29	7	0.1	• $= 3^{30}-9^{40}, 21^{20}-23^{30}, \triangle' 0^{00}-9$
30	8	•	• $\overset{*}{\nabla}{}^{\circ}0^{01-26}$
31	8	1.4	• $= 6^{30}-7^{40}, \triangle^{2} n$
Σ	–	55.6	– UWAGI

Przemyśl φ = 49°48' λ = 22°46' Wrzesień-Septembre 1962

DNI	CIŚNIENIE P+ 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	87.8	89.9	93.2	90.3	10.6	14.0	9.7	11.0	16.0	8.4	92	69	91	84	1.0	4.9	1.1	2.3	9	8	0	W 2	NW 6	W 2
2	96.5	97.5	95.9	96.6	10.8	18.0	12.4	13.4	20.6	8.1	89	46	85	73	1.5	11.0	2.4	5.0	1	3 ⊙	0	W 3	W 5	C 0
3	94.1	93.0	91.5	92.9	14.3	22.9	14.4	16.5	23.7	8.7	68	41	79	63	5.3	16.4	3.4	8.4	0	0 ⊙	0	W 5	WSW 3	C 0
4	90.3	88.1	85.2	87.9	10.1	26.1	18.1	18.1	26.6	6.8	97	38	63	66	0.4	20.8	7.7	9.6	0	0 ⊙	0	C 0	S 5	C 0
5	81.5	79.9	82.1	81.2	16.4	26.9	15.8	18.7	28.6	11.8	74	43	99	72	4.7	20.2	0.1	8.3	0	2	8	S 1	SW 7	C 0
6	82.7	82.8	81.0	82.2	14.5	20.7	17.6	17.6	22.0	12.5	88	68	81	79	2.0	7.8	3.8	4.5	9	9	3	W 2	W 5	C 0
7	76.9	75.9	79.2	77.3	20.2	24.1	14.8	18.5	24.5	14.5	72	66	90	76	6.7	10.1	1.6	6.1	9 ●	10	10	WSW 3	W 4	C 0
8	83.3	84.1	85.8	84.4	14.2	17.2	12.8	14.2	18.6	12.3	84	75	94	84	2.5	4.9	0.9	2.8	9	10	10	C 0	C 0	C 0
9	89.9	92.4	97.1	93.1	11.0	13.4	9.0	10.6	14.6	8.6	89	65	92	82	1.5	5.3	1.0	2.6	10	9	0	W 5	W 5	W 2
10	97.0	95.2	92.7	95.0	5.6	18.1	13.4	12.6	19.6	3.3	98	53	63	71	0.2	9.9	5.7	5.3	1	2	0	W 1	WSW 4	SW 3
11	90.6	89.0	89.2	89.6	15.2	23.7	17.4	18.4	23.7	11.8	54	42	59	52	8.0	17.1	8.3	11.1	1	3	10	WSW 6	SW 6	W 2
12	90.8	88.2	81.8	86.9	13.1	23.0	21.5	19.8	24.6	12.1	91	54	55	67	1.4	12.9	11.4	8.6	1	9	3	W 2	WSW 4	SW 5
13	84.1	87.8	90.9	87.6	18.5	16.4	10.3	13.9	23.3	10.1	56	67	75	66	9.3	6.2	3.1	6.3	6	7	1	W 7	WNW 7	WNW 2
14	94.6	96.0	96.4	95.7	8.7	12.4	6.9	8.7	14.2	6.7	88	67	85	80	1.3	4.8	1.4	2.5	0 ⊙	9	0	W 3	W 5	W 2
15	95.6	93.6	90.7	93.3	3.0	17.1	10.8	10.4	18.5	1.4	96	56	80	77	0.3	8.3	2.6	3.8	0	1 ⊙	0	W 1	ESE 1	SE 1
16	87.6	85.9	84.7	86.1	8.0	23.2	14.2	14.9	23.5	5.6	92	45	73	70	0.9	15.8	4.4	7.0	0 ⊙	1	1	C 0	SW 7	C 0
17	83.0	81.4	79.1	81.2	12.5	24.1	17.4	17.8	23.3	7.6	83	44	80	69	2.4	16.9	4.0	7.8	1	5	10	SSW 1	S 5	C 0
18	79.5	78.2	76.8	78.2	14.9	15.0	15.0	15.0	17.9	13.4	97	91	87	92	0.3	1.3	2.2	1.4	10	10	1	W 1	E 2	W 5
19	83.7	86.2	87.4	85.8	9.8	14.1	11.1	11.5	15.1	9.3	87	59	84	77	1.6	6.6	2.1	3.4	9	6	10 ●	W 3	W 3	NW 1
20	89.9	90.7	90.7	90.4	9.0	14.8	7.5	9.7	14.9	7.2	97	57	97	84	0.3	7.2	0.3	2.6	7	2 ⊙	9	C 0	W 4	C 0
21	90.6	90.2	89.9	90.2	6.4	11.8	8.4	8.8	14.5	5.9	94	71	87	84	0.6	3.9	1.4	2.0	3	7	10	W 3	WSW 6	W 1
22	87.8	88.8	90.2	88.9	8.1	7.4	8.6	8.2	11.1	6.7	99	94	89	94	0.2	0.6	1.3	0.7	10 ●	10 ●	10 ●	W 2	W 4	W 4
23	89.9	89.5	89.2	89.5	7.2	10.2	7.8	8.2	11.9	6.5	94	81	96	90	0.6	2.4	0.5	1.2	10	8	10 ●	WNW 2	SW 4	W 2
24	91.8	94.2	98.0	94.7	7.4	11.2	7.3	8.4	12.1	6.1	97	80	96	91	0.3	2.6	0.5	1.1	10 ●	9	0	W 1	W 2	NW 1
25	100.5	100.9	100.1	100.3	3.7	13.1	8.0	8.2	15.0	2.2	100	77	89	89	0.0	3.5	1.2	1.6	10 ═	3 ⊙	0	W 1	SE 2	C 0
26	98.4	96.1	94.0	96.2	5.3	13.7	9.6	9.6	14.9	3.8	95	54	86	78	0.4	7.2	1.8	3.1	1	5 ⊙	10	E 1	E 7	C 0
27	90.6	89.1	88.0	89.2	8.4	12.2	10.8	10.6	12.3	7.7	94	82	96	91	0.6	2.5	0.5	1.2	10	10	10	NE 2	NE 4	NE 1
28	86.2	85.7	85.4	85.8	10.5	12.9	10.2	11.0	14.9	10.1	99	88	57	95	0.2	1.8	0.3	0.8	10	10	9	ENE 1	ENE 1	C 0
29	85.7	86.6	88.5	86.9	7.0	15.7	12.0	11.7	17.4	5.7	100	82	96	93	0.0	3.2	0.5	1.2	10 ═	1 ⊙	0	C 0	E 1	C 0
30	90.8	91.8	93.6	92.1	7.0	18.4	11.9	12.3	18.8	6.1	100	70	97	89	0.0	6.5	0.3	2.3	2 ═	2	0	SW 1	SW 1	E 1
31																								
M	89.1	89.0	88.9	89.0	10.4	17.1	12.2	13.0	18.6	8.0	89	64	85	79	1.8	8.1	2.5	4.1	5.3	5.7	4.5	2.0	3.9	1.2

Październik - Octobre

1	95.2	96.0	97.0	96.1	10.0	13.7	12.7	12.3	16.9	9.1	100	93	96	96	0.0	1.1	0.5	0.5	10 ═	10	0	E 1	ESE 1	C 0
2	98.2	99.2	98.7	98.7	10.3	16.8	12.6	13.1	18.4	9.5	100	84	94	93	0.0	3.1	0.9	1.3	10 ═	2 ⊙	0	C 0	E 2	C 0
3	98.2	98.6	98.0	98.3	10.0	14.0	10.3	11.2	16.2	9.3	100	85	96	94	0.0	2.3	0.5	0.9	10 ═	10	0	SE 4	SE 3	C 0
4	96.7	96.7	95.6	96.3	7.7	16.2	13.2	12.6	18.2	6.4	100	79	93	91	0.0	3.8	1.1	1.6	10 ═	1	7	C 0	SSW 1	C 0
5	94.0	94.7	94.7	94.3	10.6	12.0	12.0	11.6	13.2	10.4	100	98	93	97	0.0	0.3	1.0	0.4	10 ═	10	3	SE 2	E 1	W 1
6	94.9	95.8	97.1	95.9	10.1	13.9	10.8	11.4	14.7	9.9	100	82	95	92	0.0	2.9	0.7	1.2	10 ═	9	0	NW 1	NNW 2	W 3
7	99.2	100.9	103.1	101.1	7.6	15.0	11.3	11.3	16.2	6.8	100	71	82	84	0.0	4.8	2.5	2.4	8	9	1	W 1	NE 1	W 1
8	105.5	106.3	105.6	105.8	4.9	14.6	10.4	10.1	17.0	3.2	100	75	96	90	0.0	4.1	0.5	1.5	0 ═	0 ⊙	2	W 1	NE 1	C 0
9	104.6	103.6	102.2	103.5	9.8	12.6	7.3	9.2	13.2	7.2	90	73	99	87	1.3	3.9	0.1	1.8	9	4	8	W 1	NW 2	W 1
10	99.7	98.2	95.9	97.9	7.7	10.7	6.4	7.8	11.9	6.1	86	76	97	86	1.5	3.1	0.3	1.6	10	9	0	NE 1	E 2	C 0
11	93.6	91.9	88.9	91.5	2.8	14.1	8.6	8.5	16.2	2.3	100	74	97	90	0.0	4.3	0.3	1.5	10 ═	0 ⊙	0	E 1	E 1	SW 2
12	87.6	87.6	92.1	89.1	8.9	17.9	8.6	11.0	18.4	5.9	80	53	86	73	2.3	9.6	1.6	4.5	0	0 ⊙	10	W 4	W 5	W 2
13	93.5	93.1	90.8	92.5	6.4	11.5	7.1	8.0	12.2	5.7	91	82	93	89	0.9	2.5	0.8	1.4	10	9	0	W 1	ENE 1	C 0
14	85.7	83.3	87.3	85.4	4.4	16.0	8.6	9.4	16.6	1.4	100	59	90	83	0.0	7.5	1.1	2.9	6	10	10	C 0	SW 6	W 6
15	90.2	93.7	98.1	94.0	7.0	5.8	0.7	3.6	8.6	0.7	91	95	96	94	0.9	0.4	0.2	0.5	9	10 ○	0	W 2	ENE 4	C 0
16	98.4	96.1	94.4	96.3	-3.4	8.4	0.0	1.2	9.3	-3.4	99	50	96	82	0.0	5.3	0.2	1.9	6 ⊙	5 ⊙	0	C 0	ESE 5	C 0
17	96.0	96.8	97.0	96.6	-1.2	11.0	6.3	5.7	11.9	-1.7	95	58	88	80	0.3	5.3	1.2	2.3	0	1 ⊙	0	WSW 3	SW 3	C 0
18	95.4	94.1	89.2	92.9	7.2	10.8	6.2	7.6	12.0	4.0	83	68	88	80	1.8	4.2	1.2	2.4	10	10	0	W 1	W 5	C 0
19	84.2	85.0	85.7	85.0	10.4	8.9	9.4	9.3	11.2	5.4	65	99	83	82	4.4	0.2	2.0	2.2	9	10 ●	10	W 4	W 3	W 3
20	85.7	89.3	96.0	90.3	8.3	10.4	6.2	7.8	11.3	6.1	79	58	76	71	2.3	3.3	2.3	3.3	10 ●	4 ⊙	2	W 5	WNW 8	NW 4
21	101.1	102.2	102.3	101.9	0.9	9.2	2.0	3.3	9.7	0.3	96	59	89	81	0.2	4.8	0.8	1.9	1	3 ⊙	0	WNW 2	WNW 2	W 1
22	101.7	100.4	99.6	100.6	-0.4	11.8	3.6	4.6	12.9	-1.8	96	49	86	77	0.2	7.0	1.1	2.8	1 ⊙	1	0	W 1	WSW 2	C 0
23	97.8	96.8	96.1	96.9	0.3	13.6	3.6	5.3	13.9	-1.5	90	50	98	79	0.6	7.8	0.1	2.8	0	0 ⊙	0	W 3	W 4	NW 1
24	94.9	93.6	93.8	94.1	-2.8	13.9	3.2	4.4	14.7	-2.8	100	49	93	81	0.0	8.2	0.5	2.9	0 ═	0	0	NW 1	WSW 1	W 1
25	94.2	93.3	93.0	93.5	1.6	12.4	3.0	3.0	12.7	-0.3	91	58	96	82	0.7	6.1	0.3	2.4	0 ⊙	0	0	C 0	NNW 2	E 1
26	91.8	90.9	89.9	90.9	-1.8	14.6	6.0	6.2	17.9	-2.0	100	54	67	74	0.0	7.7	3.1	3.6	10 ═	0 ⊙	0	NNW 1	NW 1	C 0
27	87.4	86.6	88.3	87.3	4.0	16.8	10.0	10.2	17.3	1.7	67	37	62	55	2.6	12.1	4.7	6.3	0 ⊙	0 ⊙	0	S 2	SW 6	W 3
28	87.4	84.8	82.6	84.9	3.0	16.4	7.4	8.6	16.8	2.4	86	41	72	66	1.1	10.9	2.9	5.0	3 ⊙	6	0	C 0	SSE 2	C 0
29	81.3	81.7	86.1	83.0	-1.4	9.7	5.7	4.9	10.0	-1.4	96	73	98	90	0.2	2.9	0.2	1.1	9	10	10 ●	C 0	W 2	NW 1
30	89.5	90.0	87.4	89.0	4.4	7.3	3.3	4.7	7.6	2.9	90	79	93	88	0.9	2.2	0.4	1.2	6	10	0	C 0	W 2	C 0
31	83.9	83.2	82.1	83.1	3.8	7.4	7.8	6.7	9.3	1.9	98	96	97	97	0.1	0.3	0.3	0.3	10	10	10	C 0	C 0	E 2
M	93.8	93.7	93.8	93.8	4.9	12.3	7.2	8.0	13.8	3.4	93	70	90	84	0.7	4.7	1.1	2.2	6.4	5.3	2.4	1.4	2.6	1.1

Przemyśl $H_s = 237m$ $H_a = 238{,}9m$ $h_w = 20{,}6m$ Wrzesień - Septembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	0.6	•	•°5^30-6^10 ⚲°-8^35, 11^50-12^05 ⚲' 14^40-47
2	8	•	•	⌓² n-9
3	8	•	•	
4	8	•	•	=7^15-9^21; ⌓² n-9
5	8	8.5	•	⚲°⁻¹ 18^40-20^50 ⚲° 22^10-np; ⌓' n-8
6	8	0.0	•	
7	8	14.4	•	⚲° 7^25-35 ⚲² 13^48-14^10 ⚲°-15^50 16^40-55; 17^02-15, 18^50-19^25; ⚲° 13^50-14^35
8	7	4.4	•	⚲²⁻⁰ 19^08-40 ⚲° 21^45-n; (⚲) 16^50-17^40, 18^55-19^35
9	8	3.5	•	⚲° 7^55-8^50, 14^55-15^07 ⚲' 16^25-45 ⚲°-17^05
10	8	•	•	
11	8	0.5	•	•° 22^01-n
12	7	•	•	=7^10-9^40; ⌓² n-8
13	8	0.0	•	⚲° 10^31-11^05, 11^40-50
14	7	•	•	⌓² n-9
15	8	•	•	=8^30-9^20; ⌓² 2-10 ⌓' np
16	8	•	•	=7^40-8^30; ⌓¹⁻² 0^00-9 ⌓' 21-24
17	7	2.4	•	=8^20-9^22; ⌓' 0^00-9
18	5	0.7	•	•° 0^50-1^20, 2^05-3^20, 3^35-5^45 •° 10^50-11^25 •° 16^01-17^40; =3^55-18^30
19	8	1.3	•	•° 21^30-23^20
20	7	0.8	•	⚲° 22^50-23^40; =2^00-12^40, 18^30-23^10; ⌓² np
21	7	1.0	•	⚲° 12^55-13^05; =3^30-12^40
22	7	16.6	•	⚲° 2^20-53 •⁰⁻¹ 5^21...10^40 ⚲° 11^53...24 ⚲² 13^07-12; =6^10-10^40
23	7	0.7	•	⚲° 0^00-15 •° 1^10...3^25 ⚲⁰⁻¹ 5^50...7^05 ⚲° 14^34...22^35
24	7	1.7	•	•² 7^15-8^02 •° -8^10 •² 9^50-10^10 •° -10^40; =7^20-8^30
25	5	•	•	=0^00-1^50 ≡²⁻⁰ -12^40 = -14^20, ⌓' 20-24
26	7	•	•	=5^40-10^26; ⌓¹⁻² 0^00-10
27	6	0.0	•	•° 10^20...11^15; =3^30-24
28	7	0.2	•	•° 7^22-8^12, 10^30-12^10; =0^00-12^10, 18^50-24; ⌓² p-24
29	6	•	•	=0^00-2^40 ≡⁰⁻² 2^50-11^42 = -14^36, 18^16-24; ⌓² 0^00-11, np
30	6	•	•	=0^00-40 ≡ -9^35 = -13^10 ∞ -16^40 = -21^40 ≡² -24; ⌓² 0^00-8
31				
Σ	—	57.7	—	UWAGI.

Październik - Octobre

1	6	•	•	≡²⁻⁰ 0^00-11^40 = -14^20, 15^35-22^40 ≡°-24; ⌓² 0^00-12
2	6	•	•	≡⁰⁻² 0^00-9^35 = 17^14-24; ⌓² 20-24
3	6	•	•	=0^00-1^40 ≡⁰⁻² -9^45 = -12^50, 17^26-24; ⌓² 0^00-9, 20-24
4	7	•	•	=0^00-3^40 ≡° -4^35 = -5^40 ≡²⁻¹ -9^40 = -12^20, 16^40-24; ⌓² p-24
5	5	•	•	=0^00-1^35 ≡⁰⁻² -9^38 = -24; ⌓² 0^00-9 ⌓' 19-24
6	6	•	•	=0^00-5^45 ≡⁰⁻² -8^50 = -24; ⌓' 0^00-11 ⌓° 19-24
7	7	•	•	=0^00-9^50 16^10-22^10; ⌓² 0^00-9 ⌓' 19-24
8	6	•	•	=2^30-5^40 ≡⁰⁻² -10^35 = -15^13, 16^20-24; ⌓² 0^00-10 ⌓' 19-24
9	7	•	•	=0^00-11^30, 16^50-24; ⌓° 0^00-11 ⌓' 18-24
10	7	•	•	=0^00-7^40, 16^20-22^40 ≡⁰⁻² -24; ⌓²⁻¹ 0^00-9 ⌓' p-24
11	6	•	•	≡²⁻¹ 0^00-10^35 = -12^40; ⌓² 0^00-10 ⌓° 18-24
12	7	•	•	=13^40-24; ⌓' 0^00-10
13	6	•	•	=0^00-24; ⌓° 17-24
14	7	0.0	•	⚲° 18^23-30; =0^00-1^20 ≡° -5^50 = 10^26, 16^45-18^10; ⌓² 0^00-9
15	6	0.8	•	•° 8^50-9^30 •⁰⁻² -11^10 •² 11^45-12^20 •° -12^50; =2^40-12^50; ⌣⁰⁻¹ 20-24
16	8	•	•	=3^40-10^45; ⌣² 0^00-9 ⌣' 20^00-24
17	7	•	•	=7^40-10^36; 15^36-20^20; ⌣' 0^00-9
18	7	•	•	=5^36-9^40, 16^30-24; ⌓° 20^00-24
19	6	0.4	•	•²⁻⁰ 10^25-13^05 •° -13^45 ⚲° 14^55-15^05; =0^00-2^26, 10^10-19^20; ⌓° 0-3
20	7	•	•	•° 6^30-45
21	8	•	•	⌓° 20-22 ⌣° -24
22	8	•	•	=16^40-20^20; ⌣° 0^00-8 ⌓° 18-24
23	7	•	•	=7^20-9^50 ∞ 16^12-40 = -23^40 ≡° -24; ⌓° 0^00-1 ⌣° -8, 23-24
24	7	•	•	≡⁰⁻² 0^00-7^45 = 15^40-24; ⌣° 0^00-9 ⌓° 20-24
25	6	•	•	=0^00-23^35 ≡⁰⁻² -24; ⌣° 0^00-9
26	7	•	•	≡² 0^00-9^40 = -12^10; ⌣' 0^00-9
27	8	•	•	⌣° 4-9
28	7	•	•	=5^30-11^50; ⌓° 0^00-4 ⌣° -7
29	6	0.0	•	•° 19^40-21^15; =7^24-24; ⌣° 4-7
30	6	0.3	•	=0^00-12^50, 14^50-17^20, 19^20-24; ⌓° 21-22 ⌣° -24
31	4	1.2	•	•° 6^03-19, 7^40-9^35, 11^20-12^10; =0^00-18^20; ⌣° 0^00-4
Σ	—	2.7	—	UWAGI.

Przemyśl φ = 49°48' λ = 22°46' Listopad - Novembre 1962

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D.v I	II	III
1	79.5	77.9	78.9	78.8	8.6	16.0	11.7	12.0	16.8	7.4	99	63	90	84	0.2	6.8	1.3	2.8	10	8	0	SE 4	SE 7	SE 1
2	82.2	84.4	87.0	84.5	7.8	11.2	10.2	9.8	12.1	7.7	97	91	95	94	0.3	1.2	0.6	0.7	8	10 ═	9	C 0	C 0	C 0
3	88.4	88.2	89.1	88.6	9.2	12.4	9.2	10.0	12.8	8.9	100	92	100	97	0.0	1.2	0.0	0.4	10 ═	10	0	C 0	NE 3	C 0
4	90.8	91.5	91.6	91.3	7.6	10.4	10.2	9.6	11.3	7.3	100	97	95	97	0.0	0.3	0.6	0.3	10 ═	10	10	SSE 1	SE 1	ESE 3
5	90.9	90.6	89.9	90.5	8.5	8.5	5.1	6.8	11.2	5.0	100	94	75	90	0.0	0.6	2.2	0.9	10	10	1	SE 2	ESE 3	E 3
6	88.3	88.1	90.7	89.0	-0.2	10.5	5.8	5.5	10.6	-0.2	94	53	79	75	0.4	5.9	2.0	2.8	1	7 ⊙	9	E 1	E 4	E 3
7	92.9	94.5	95.4	94.3	3.2	6.5	6.7	5.8	7.8	-0.5	91	93	85	90	0.7	0.7	1.4	0.9	9	9	8	SE 1	E 1	E 1
8	94.2	92.2	90.7	92.4	4.6	10.9	4.2	6.0	11.9	4.1	93	71	87	84	0.6	3.7	1.0	1.8	8	0	3	ESE 1	SE 2	C 0
9	88.4	87.0	86.3	87.2	0.6	8.2	5.0	4.7	8.3	0.6	96	78	84	86	0.3	2.4	1.4	1.4	6	8	9	C 0	ENE 2	E 1
10	84.3	84.1	85.7	84.7	4.9	3.4	2.0	3.1	5.0	2.0	87	98	96	94	1.1	0.1	0.3	0.5	10	10 ●	10 ●	E 5	NE 4	NE 3
11	88.9	90.3	91.2	90.1	1.8	3.8	4.6	3.7	4.8	1.4	96	97	97	97	0.3	0.3	0.3	0.3	10	10	10	ENE 3	ESE 4	E 7
12	90.1	89.5	90.4	90.0	2.6	3.8	3.8	3.5	4.7	2.4	98	93	95	95	0.2	0.5	0.4	0.4	10	10	10	E 7	ESE 6	ESE 1
13	92.1	92.4	91.7	92.1	3.0	5.0	3.2	3.6	5.2	2.6	100	94	100	98	0.0	0.5	0.0	0.2	10 ═	10	10	SE 1	SE 1	E 3
14	89.8	89.7	89.4	89.6	3.2	6.0	6.6	5.6	7.4	2.8	100	95	98	98	0.0	0.5	0.1	0.2	10 ═	10 ●	6	C 0	SE 1	C 0
15	88.1	84.4	78.0	83.5	3.5	10.4	6.1	6.5	10.7	0.9	98	77	91	89	0.1	2.9	0.8	1.3	5	10	10	C 0	SSE 1	C 0
16	77.6	79.2	81.9	79.6	2.1	1.2	1.2	1.4	8.1	0.8	96	96	87	93	0.3	0.3	0.9	0.5	10 ● *	10 *	10	W 1	WNW 3	W 3
17	86.0	87.8	87.9	87.2	-0.1	2.5	-1.7	-0.2	2.7	-1.7	94	70	93	86	0.4	2.2	0.4	1.0	9	5 ⊙	0	W 2	WSW 2	C 0
18	83.4	81.4	79.3	81.4	-1.7	2.0	1.2	0.7	2.3	-3.3	92	82	96	90	0.4	1.3	0.3	0.7	10	6	10	SE 1	E 4	E 1
19	77.3	79.6	78.3	78.4	6.4	11.2	6.6	7.7	11.8	1.1	75	57	88	73	2.4	5.7	1.1	3.1	9	8	0	S 3	S 2	SE 1
20	77.3	75.1	77.4	76.6	6.4	10.9	5.8	7.2	13.2	4.9	88	78	88	85	1.1	2.9	1.1	1.7	8	10	10	C 0	ENE 4	W 5
21	82.4	81.8	80.7	81.6	1.8	2.2	1.3	1.6	5.9	0.9	96	93	98	96	0.3	0.6	0.1	0.3	10	10 ●	10 ●	W 3	NW 2	N 1
22	81.0	83.4	88.7	84.4	2.0	5.8	3.9	3.9	6.7	1.3	96	70	82	83	0.3	2.8	1.5	1.5	10	8	0	C 0	SW 5	C 0
23	90.6	92.4	92.7	91.9	2.9	2.0	1.2	1.8	3.9	1.0	93	93	96	94	0.5	0.6	0.3	0.5	10	10	10 ●	SW 2	W 1	NW 4
24	95.8	96.9	99.0	97.2	-0.2	0.4	1.2	0.6	1.4	-0.3	100	100	100	100	0.0	0.0	0.0	0.0	10	10 ═	10	NW 3	NW 2	NE 2
25	98.7	98.1	97.1	98.0	2.2	2.8	3.8	3.2	3.9	1.0	100	98	98	99	0.0	0.2	0.1	0.1	10 ═ ●	10	10	NE 3	N 3	NW 2
26	98.3	98.4	98.9	98.5	1.9	4.4	6.5	4.8	6.5	1.2	98	100	100	99	0.1	0.0	0.0	0.0	10 ●	10 ● ═	10	W 2	WNW 4	N 4
27	101.8	102.4	101.5	101.9	2.6	3.2	1.7	2.3	6.5	1.4	95	90	94	93	0.4	0.8	0.4	0.5	10	10	10	W 3	W 3	C 0
28	98.1	96.9	97.1	97.4	1.1	3.7	0.8	1.6	3.8	0.2	92	75	86	84	0.5	2.0	0.9	1.1	9	3 ⊙	7	W 1	SW 1	C 0
29	95.7	95.2	95.8	94.9	1.4	3.4	3.4	2.9	3.9	0.5	85	80	88	84	1.0	1.6	0.9	1.2	10	9	10	WSW 2	WSW 5	SW 1
30	89.2	87.4	88.1	88.2	2.6	3.2	2.8	2.8	3.4	2.0	77	79	88	81	1.7	1.6	1.0	1.4	10	10	10 ●	SW 5	WSW 7	W 3
31																								
M	88.7	88.7	88.9	88.8	3.3	6.2	4.5	4.6	7.5	2.1	94	85	92	90	0.5	1.7	0.7	1.0	9.1	8.7	7.4	1.9	2.9	1.8

Grudzień - Décembre

1	94.0	101.5	106.5	100.7	0.0	-1.2	-1.6	-1.1	2.8	-2.1	90	76	88	85	0.6	1.3	0.6	0.8	10 *	10	9 *	W 8	NW 5	NW 2
2	111.9	113.9	114.1	113.3	-4.3	-0.9	-4.8	-3.7	-0.9	-5.0	89	65	93	82	0.5	2.0	0.3	0.9	0	3	0	NW 2	W 2	C 0
3	110.8	108.7	105.2	108.2	-8.6	-3.0	-6.6	-6.2	-2.1	-9.3	92	79	97	89	0.3	1.0	0.1	0.5	2	2	9	C 0	C 0	C 0
4	100.9	98.6	94.8	98.1	-9.3	-0.5	-0.4	-2.6	0.8	-9.4	88	74	53	72	0.4	1.6	2.6	1.3	1	1 ⊙	4	W 2	W 3	WSW 3
5	91.9	94.7	98.8	95.1	1.7	-0.2	0.2	0.5	1.9	-1.1	47	84	96	76	3.7	0.9	0.3	1.6	9	10 ●	10 *	W 7	W 6	W 3
6	101.0	101.3	100.8	101.0	0.4	1.7	1.2	1.1	1.7	-1.2	96	92	96	95	0.3	0.5	0.3	0.4	10	10	10	W 2	W 4	W 2
7	97.9	97.5	98.1	97.8	-0.8	2.6	0.6	0.8	2.7	-1.8	83	79	90	84	1.0	1.6	0.6	1.1	1	2 ⊙	0	W 3	W 7	W 4
8	99.8	101.6	102.0	101.1	-0.6	0.5	-1.8	-0.9	1.4	-2.0	89	83	98	90	0.6	1.0	0.1	0.6	1	0 ⊙	10 ═	W 2	W 3	NW 1
9	95.6	89.2	82.3	89.0	-7.2	3.1	-0.2	-1.1	3.3	-7.5	96	48	54	66	0.1	4.0	2.8	2.3	2	7	4	C 0	WSW 7	SW 7
10	78.9	79.2	77.9	78.7	-1.0	0.1	-0.4	-0.4	0.5	-2.1	75	67	72	71	1.5	2.1	1.6	1.7	9	10	10	WSW 5	SW 4	SW 2
11	78.8	79.6	80.2	79.5	-0.9	1.8	-0.8	-0.2	2.2	-2.7	89	78	81	83	0.6	1.6	1.1	1.1	10 *	10	3	W 4	W 6	W 2
12	76.2	74.2	73.3	74.6	1.4	2.3	0.2	1.0	3.4	-1.8	78	66	63	69	1.6	2.4	2.3	2.1	9	8	2	SW 6	WSW 7	SW 2
13	74.0	74.1	73.1	73.7	1.9	4.8	1.2	2.3	6.3	-0.6	66	46	66	59	2.4	4.7	2.3	3.1	9	10	9	S 2	S 2	E 1
14	72.5	74.0	75.8	74.1	0.5	3.9	0.9	1.6	8.5	-1.3	79	92	94	88	1.3	0.7	0.4	0.8	10	10 ●	10	C 0	W 5	W 3
15	74.1	66.3	59.9	66.8	-2.6	0.7	0.1	-0.4	1.5	-3.4	93	73	71	79	0.3	1.7	1.8	1.3	9	9	10	C 0	SSW 9	SW 8
16	51.0	47.6	50.1	49.6	-0.2	1.8	2.5	1.6	2.5	-1.3	78	87	80	82	1.3	0.9	1.4	1.2	10	10 ● *	9	SSW 2	SW 3	W 2
17	54.8	62.3	67.8	61.6	1.6	-0.2	0.1	0.4	2.5	-1.7	93	86	98	92	0.6	0.8	0.2	0.5	10 ●	10	10 *	W 3	WNW 7	W 1
18	70.1	68.9	70.9	70.0	-1.1	0.9	-1.6	-0.8	1.1	-2.2	93	77	90	87	0.4	1.5	0.5	0.8	8	9	10	C 0	WSW 5	C 0
19	72.4	74.7	80.5	75.9	-2.7	-3.4	-3.6	-4.3	-1.6	-5.6	93	92	90	92	0.3	0.4	0.4	0.4	10 *	9	10	W 2	NW 1	C 0
20	86.4	88.6	92.4	89.1	-6.8	-7.8	-9.1	-8.2	-5.2	-9.1	91	87	85	88	0.3	0.4	0.4	0.4	10 *	10 *	10	N 2	NW 3	NW 2
21	90.8	89.2	89.6	89.9	-10.8	-10.9	-10.1	-10.3	-9.0	-11.0	90	87	84	87	0.3	0.4	0.4	0.4	10 *	9	10 *	NW 1	N 1	NE 1
22	94.0	97.3	101.6	97.6	-14.0	-11.7	-12.8	-12.8	-10.1	-14.9	87	89	85	87	0.3	0.3	0.4	0.3	10 *	10 *	10	NE 3	NNW 4	NE 3
23	105.3	107.0	109.3	107.2	-13.1	-12.3	-13.1	-12.9	-12.0	-14.2	84	81	88	84	0.4	0.4	0.3	0.4	8	1 ●	10	NE 4	NW 4	NE 6
24	108.5	108.5	108.7	108.6	-11.9	-9.3	-9.4	-10.0	-9.1	-13.4	89	79	88	85	0.3	0.6	0.4	0.4	10 *	9	10	NE 6	NE 5	NE 3
25	105.8	102.6	97.1	101.8	-10.4	-11.7	-12.3	-11.8	-9.3	-13.1	87	86	81	85	0.4	0.3	0.4	0.4	10	10	10 *	E 4	E 3	E 3
26	89.8	86.6	85.0	87.1	-13.7	-8.4	-9.0	-10.0	-8.3	-13.4	88	80	92	87	0.3	0.6	0.3	0.4	10	2	10	C 0	E 1	C 0
27	82.1	80.3	81.7	81.4	-8.7	-6.4	-8.3	-8.0	-6.4	-9.2	92	83	92	89	0.3	0.6	0.3	0.4	10	9 *	10	E 1	ENE 4	NE 2
28	83.7	83.6	87.3	85.6	-8.1	-5.3	-10.3	-8.6	-3.3	-10.4	92	77	91	87	0.2	0.9	0.3	0.3	10	10	0	C 0	NE 1	C 0
29	86.2	84.9	80.9	84.0	-12.7	-6.6	-4.4	-7.0	-2.4	-13.9	88	70	86	81	0.3	1.1	0.6	0.7	0	6	10	C 0	C 0	C 0
30	80.2	80.7	81.8	80.9	-5.6	-2.1	-3.3	-3.1	2.4	-4.3	87	92	97	92	0.6	0.4	0.1	0.4	10	10 *	10 *	C 0	C 0	NE 3
31	83.5	84.9	90.4	86.3	-7.4	-9.0	-12.3	-10.2	-3.3	-12.3	90	93	93	93	0.3	0.2	0.2	0.2	10 *	10 *	0	NE 4	NE 6	NE 2
M	87.2	87.2	87.7	87.4	-4.9	-2.8	-4.2	-4.0	-1.3	-6.6	86	79	85	83	0.7	1.2	0.8	0.9	7.7	7.6	7.7	2.4	3.0	2.3

Przemyśl H_s=237m H_b=238,9m h_w=20,6m Listopad - Novembre 1962

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	•	•	=0^00-8^32
2	3	0.3	•	•°7^50-8^10 9^15-11^05; =5^30-11^50≡-12^45=-24
3	5	•	•	,°6^20-7^20; =0^00-5^40≡^2-1-9^50=-24; ⌓' 18-24
4	6	•	•	=0^00-45≡^0-2-11^38=-16^40; ⌓^2 0^00-10
5	6	•	•	=5^20-12^30
6	7	•	•	=5^40-9^10; ⌣°1-9; ⊽°17^00-18^30
7	7	0.4	•	•°8^40...11^07, 16^00-12; =16^01-19^38
8	7	•	•	⌓°22-24
9	7	•	•	=5^36-9^45; ⌓°0^00-2⌣°-9
10	6	4.4	•	•°10^31...14^40-19^30...21^40,°-22^20...24
11	6	1.6	•	,°0^00-10, 2^45...5^15 •°14^10-35,°17^40-19^26; =0^00-8^30, 11^20-24
12	8	1.7	•	•°4^20-5^12 7^42-9^05; =0^00-6^35
13	7	0.2	•	•°17^40...19^10, 23^50-24; =1^20-2^40≡°-5^50=-6^40≡°-7^38=-12^28
14	4	0.9	•	•°0^00-15, 10^35-13^20; =0^00-6^50≡°-8^40=-15^50≡-16^45=-22^40≡^2-24
15	7	7.5	•	≡^2-0^00-2^45=-9^30, 14^40-17^15
16	5	10.8	•	•°1^45-6^25 *°-7^00 •°-7^20 *°-9^13 *°-9^32 *°-9^40 *°-10^30 *°-10^50 *°-18^40
17	7	•	1	
18	7	•	pł.	⊽°1^00-3^40
19	8	0.0	•	*°15^18-29
20	8	6.5	•	•°20^40...21^10-24
21	6	1.3	•	•°0^00-1^35 *°-4^20,°12^30-15^45 *°-16^20, *°-17^40,°-18^30 •°20^20-21^05; =6^10-24
22	8	•	•	,°2^40-4^15; =0^00-9^40
23	6	0.7	•	,°18^40-19^40 •°...21^20 *°-24; =8^30-15^35≡°-16^45=-24
24	3	0.2	•	*°0^00-1^20,°14^25-15^40,'-20^15; =0^00-11^45≡°-'-18^40
25	5	10.4	•	,°-'3^40-9^36 •°-11^22, 14^01-09,°14^38-17^30 •°-20^20 •2^15-22^05 •°-23^20,°-24=, ≡°-^2 0^00-24
26	2	7.7	•	,°0^00-3^30,°4^20-5^40 •°-8^25,'-^2-14^25 •°-20^20,°21^35-23^20; =0^00-10^50≡'-°-16^45=-24
27	7	•	•	,°1^38-5^37; =0^00-6^20, 15^30-17^20, 21^40-24
28	7	•	•	=0^00-9^04, 13^36-16^20
29	7	•	•	=6^15-7^30
30	7	2.4	•	•°13^01-15^30, 18^40-19^45, 20^15-23^35; =15^20-24
31				
Σ	—	57.0	—	UWAGI

Grudzień - Décembre

1	8	0.0	pł.	•°3^20-4^28 *°-5^05 *° ...12^20, 18^38-20^20; =0^00-2^40
2	8	•	1	
3	6	•	1	=6^20-24; ⌣°2-8
4	7	•	•	=0^00-11^40; ⌣°1^00-11
5	6	0.4	•	,°12^15-13^25 △°-15^40 *°20^10-24; =10^20-24
6	4	0.2	1	*°0^00-4^40 5^20-6^20; =0^00-24
7	7	•	•	=0^00-2^30, 15^40-19^15; ⌣°2-8
8	5	•	•	=6^30-14^40≡°-19^25≡^2-24; ⌣°na-24
9	7	•	•	≡^2 0^00-6^20=-9^30; ⌣°-'0^00-12
10	7	0.0	•	⊽20^25-24
11	7	0.0	•	*°5^45-7^20 △°-9^20; ⊽0^00-40
12	8	•	•	
13	7	•	•	
14	6	6.2	•	•°10^40-16^20 *°-17^10 *°-20^22, 22^40-23^10; =12^20-23^10
15	8	0.0	4	*°15^10-18^30, 23^10-24; ⌓ 14^40-19^30; =6^20-7^30
16	7	1.3	3	*°0^00-1^00 *°-'6^40-9^46...12^02 *°-13^38 •°14^40-16^14, 16^40...17^00
17	7	4.2	2	•°5^45-7^40 *°15^30-19^30 *°-20^10 *°-22^20, 23^20-24
18	7	4.9	9	*°-'0^00-2^39 *°13^10-15^50 21^40-24; =3^20-12^20, 13^20-24
19	6	0.6	12	*°0^00-5^40, 6^10-11^38, 21^50-24; =0^00-24
20	6	0.0	12	*°0^00-10 5^50-14^40; =0^00-30, 1^40-24
21	6	0.1	11	*°4^40-6^40 8^25-12^25, 19^35-24; =0^00-6^10 8^15-24
22	6	0.3	11	*°0^00-15^24, 17^20-18^10, 19^20-20^10, 21^15-24; =0^00-20^10
23	8	0.2	12	*°0^00-6^10, 21^38-24
24	7	0.0	15	*°0^00-12^15, 13^25...14^50, 15^20-20^10
25	7	0.4	15	*°8^20-9^18, 17^40-24
26	5	0.0	15	*°0^00-1^20, 6^20-12^15, 13^40-17^10; =4^25-24
27	5	0.0	15	*°4^40...5^10, 10^45-15^10; =0^00-24
28	6	•	15	=0^00-24; ⌣°20-24
29	5	•	12	=0^00-8^50≡°-10^40=-24; ⌣'0^00-10
30	4	8.7	10	*°10^40-12^35 *'-14^30 *°-24; =0^00-1^40, 3^30-24
31	5	8.6	20	*°0^00-14^40 *'-16^26 *°-20^15; ⊥°13^40-16^44; =0^00-24
Σ	—	56.1	—	UWAGI

Zakopane φ=49°18' λ=19°57' Styczeń - Janvier 1962

DNI	CIŚNIENIE P=800+ I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	114.0	115.2	114.3	114.5	4.4	2.9	0.5	2.1	5.4	-2.1	75	61	88	75	2.1	2.9	0.7	1.9	9	10	10	SW 1	WSW 2	C 0
2	111.4	113.1	116.9	113.8	-1.9	-2.4	-5.2	-3.7	0.5	-5.4	83	82	60	82	0.9	0.9	0.8	0.9	10●	10⚠	10	C 0	C 0	NW 3
3	120.5	121.9	124.6	122.3	-7.0	-3.5	-3.4	-4.3	-2.3	-8.9	75	60	76	70	0.9	1.9	1.1	1.3	1	0⊙	9	NNW 2	SW 3	C 0
4	127.1	126.0	126.1	126.4	-6.4	-2.6	-8.7	-6.6	0.3	-8.9	83	69	74	75	0.6	1.6	0.8	1.0	10	0⊙	0	C 0	ENE 1	C 0
5	124.8	123.1	121.4	123.1	-8.9	3.8	-7.7	-5.1	4.0	-10.4	73	36	70	60	0.8	5.1	1.0	2.3	6	7⊙	0	C 0	C 0	C 0
6	118.0	117.1	115.7	116.9	-8.0	3.1	1.1	-0.7	4.6	-10.5	81	51	68	67	0.6	3.7	2.1	2.1	1	3⊙	1	ESE 1	C 0	W 5
7	118.6	121.9	127.1	122.5	-2.5	-2.1	-3.4	-2.8	2.0	-3.7	84	85	81	83	0.8	0.7	0.9	0.8	10✳	10✳	10✳	WNW 3	WNW 2	NW 2
8	128.5	127.9	127.2	127.9	-9.0	-2.8	-3.4	-4.6	-1.3	-12.6	76	73	81	77	0.8	1.3	0.9	1.0	1	0⊙	8	C 0	ESE 1	C 0
9	125.0	122.6	121.4	123.0	-7.3	-6.5	-11.9	-9.4	-3.4	-12.8	88	91	86	88	0.4	0.3	0.4	0.4	10≡	7	0	C 0	NE 1	C 0
10	116.7	112.2	113.8	114.2	-13.4	2.9	-1.2	-3.2	4.0	-15.1	80	55	76	70	0.4	3.4	1.3	1.7	8	9	7	C 0	NNE 5	NE 2
11	114.9	111.9	110.6	112.5	-7.5	5.8	5.8	2.5	6.7	-7.8	87	33	56	65	0.4	4.3	4.0	2.9	1	8⊙	8	NE 1	SW 3	NE 4
12	110.0	109.6	106.1	108.6	1.9	1.9	0.4	1.2	6.0	0.4	86	86	94	89	0.9	0.9	0.4	0.7	10	10	8	ENE 1	C 0	C 0
13	98.2	100.7	103.4	100.8	5.2	4.3	0.0	2.4	7.0	0.0	50	60	92	67	4.3	3.3	0.5	2.7	10	10	10✳	SW 6	ENE 2	C 0
14	105.6	108.3	112.4	108.8	0.1	0.8	-0.3	0.1	1.1	-1.8	86	58	63	69	0.9	2.8	2.3	2.0	9	1⊙	3	SW 3	WSW 4	SW 4
15	115.9	118.6	121.9	118.8	-2.4	0.5	-4.6	-2.8	0.8	-5.6	63	54	69	62	1.9	2.9	1.3	2.0	1	1⊙	1	NW 4	WNW 5	W 2
16	125.3	124.6	124.1	124.7	-8.9	-0.2	-9.7	-7.1	1.6	-10.5	86	45	78	70	0.4	3.2	0.6	1.4	0	2⊙	8	C 0	C 0	C 0
17	122.2	121.8	120.8	121.6	-10.5	0.2	-7.7	-6.4	1.3	-11.3	80	49	81	70	0.5	3.2	0.6	1.4	8	4⊙	8	SW 1	SW 1	C 0
18	119.2	118.8	120.3	119.4	-9.2	-0.3	-6.3	-5.5	0.6	-10.0	85	59	83	76	0.4	2.5	0.6	1.2	10	9	8	C 0	ESE 2	C 0
19	121.1	121.2	120.8	121.0	-2.5	4.1	0.2	0.5	4.3	-7.3	89	58	82	76	0.6	3.4	1.1	1.7	9	9	2	SW 1	C 0	C 0
20	122.3	124.1	125.8	124.1	3.4	4.0	3.3	3.5	6.4	-2.8	76	60	80	72	1.9	3.6	1.4	2.3	10	4⊙	10	W 6	W 8	WNW 3
21	126.1	125.3	124.0	125.1	3.5	5.3	4.2	4.3	5.4	2.4	74	64	76	71	2.0	3.2	1.9	2.4	9	8	8	WSW 2	WNW 3	SW 3
22	118.7	114.6	117.1	116.8	-1.7	4.8	3.3	2.4	6.0	-1.9	91	65	50	69	0.5	3.0	3.9	2.5	9	9⊙	10	C 0	E 2	W 3
23	119.4	119.2	122.2	120.3	-0.8	3.9	-2.4	-0.4	4.1	-2.5	69	35	76	60	1.8	5.3	1.2	2.8	5	6⊙	10	NE 2	SE 2	C 0
24	122.3	120.5	117.9	120.2	-3.2	1.4	-0.5	-0.7	1.8	-4.1	76	56	76	69	1.1	3.1	1.5	1.9	6	8	9	SW 1	WSW 5	NE 3
25	115.6	114.2	114.4	114.7	2.6	5.7	3.6	3.9	6.0	-1.2	83	63	68	71	1.2	3.4	2.5	2.4	10●	10	10	SW 3	WSW 4	W 3
26	114.6	118.2	117.8	116.9	1.0	-1.2	-4.8	-2.4	3.6	-4.9	92	89	86	89	0.5	0.6	0.6	0.6	10●	10✳	0	WSW 2	C 0	C 0
27	115.4	117.9	118.9	117.4	-0.3	-1.5	-2.3	-1.6	-0.2	-5.0	90	88	87	88	0.6	0.7	0.7	0.7	10✳	10✳	9✳	W 4	W 5	W 5
28	114.9	113.3	113.5	113.9	-3.1	-2.9	-7.5	-5.2	-2.0	-7.5	93	84	82	86	0.4	0.8	0.6	0.6	10✳	7⊙	10✳	WSW 4	S 2	NW 2
29	115.9	119.2	123.1	119.4	-10.9	-11.6	-12.7	-12.0	-7.5	-12.9	73	68	81	74	0.7	0.8	0.4	0.6	10✳	10✳	10✳	E 1	NE 1	E 2
30	125.4	127.6	130.1	127.7	-12.7	-8.1	-11.0	-10.7	-8.1	-13.5	81	84	80	82	0.4	0.5	0.5	0.5	10✳	10✳	10✳	C 0	NE 3	C 0
31	128.5	126.7	124.7	126.6	-14.1	-11.8	-15.1	-14.0	-11.0	-19.0	75	82	77	78	0.5	0.4	0.4	0.4	7	9✳	10	ENE 2	E 2	C 0
M	118.6	118.6	119.3	118.8	-4.2	-0.1	-3.5	-2.8	1.7	-7.0	80	65	77	74	1.0	2.4	1.2	1.5	7.4	6.8	7.0	1.6	2.2	1.5

Luty - Février

1	117.2	116.3	116.7	116.7	-15.8	-5.1	-7.4	-8.9	-3.7	-17.5	76	68	82	75	0.4	1.3	0.6	0.8	9	1⊙	10✳	C 0	C 0	E 1
2	116.8	118.0	119.4	118.1	-8.1	-3.0	-9.7	-7.6	-1.4	-12.1	84	72	85	80	0.5	1.4	0.4	0.8	10	4⊙	6	C 0	ENE 1	C 0
3	120.9	122.6	123.6	122.4	-7.3	-6.0	-4.9	-5.8	-4.5	-10.4	85	81	83	83	0.5	0.7	0.7	0.6	10✳	10⚠	10⚠	C 0	E 1	E 1
4	120.9	119.1	122.1	120.7	-5.9	0.5	-3.1	-2.9	1.4	-6.3	81	63	88	77	0.7	2.3	0.6	1.2	10	9	10	C 0	SSW 2	W 3
5	120.3	113.2	111.9	115.1	-9.4	-1.5	-0.7	-3.1	1.6	-11.0	76	68	77	74	0.7	1.8	1.3	1.3	1	10	10✳	NW 2	W 1	SW 2
6	117.9	119.3	121.8	119.7	-3.3	-2.1	-2.7	-2.7	-0.7	-3.3	81	83	82	82	0.9	0.9	0.9	0.9	10✳	9✳	10✳	WSW 5	W 4	W 6
7	121.4	120.3	117.5	119.7	-3.5	1.4	-7.0	-4.0	2.3	-7.9	83	58	88	76	0.8	2.9	0.4	1.4	10	1⊙	1	S 2	SW 2	C 0
8	115.2	116.0	118.1	116.4	-10.0	1.1	-5.7	-5.1	1.2	-10.6	94	70	87	80	0.4	2.0	0.5	1.0	9	9	3	C 0	ENE 1	SW 1
9	121.0	125.1	129.6	125.2	-2.9	0.6	-1.6	-1.4	0.8	-6.6	91	83	88	87	0.4	1.1	0.6	0.7	10⚠	10	10✳	C 0	SSE 1	NW 3
10	132.2	131.3	130.7	131.4	-4.4	0.0	-6.9	-4.6	1.3	-8.8	86	54	77	72	0.6	2.8	0.8	1.4	9	2⊙	9	C 0	C 0	C 0
11	127.3	125.6	129.8	127.6	-3.5	0.4	-2.5	-2.0	1.0	-7.2	65	47	82	65	1.6	3.4	0.9	2.0	10	10✳	10⚠✳	SE 2	SW 4	ENE 3
12	121.6	110.4	101.1	111.0	-10.5	5.4	4.7	1.1	6.9	-11.7	80	49	64	64	0.5	4.6	3.0	2.7	8	9	10●	ESE 1	WSW 8	W 10
13	95.3	90.7	91.3	92.4	0.3	0.2	-1.6	-0.7	5.4	-1.6	94	90	86	90	0.3	0.6	0.7	0.5	10	10✳	10	WNW 6	W 6	C 0
14	93.0	94.1	98.6	95.2	-3.2	-4.7	-6.3	-5.1	-1.6	-6.3	86	83	83	84	0.7	0.7	0.6	0.7	10	10✳	10✳	NE 2	NE 3	NE 1
15	106.3	110.8	118.9	112.0	-7.3	-6.5	-8.6	-7.8	-6.1	-8.8	82	78	80	80	0.6	0.8	0.6	0.7	10✳	10✳	9✳	NNE 3	NE 2	E 2
16	115.9	106.6	100.4	107.6	-12.0	-3.0	2.0	-2.8	2.3	-15.6	63	77	74	71	0.9	1.1	1.9	1.3	9	10✳	10✳	SW 3	C 0	W 8
17	97.2	97.9	104.4	99.8	-2.7	-2.7	-4.3	-3.5	2.0	-4.4	91	89	91	90	0.5	0.6	0.4	0.5	10✳	10✳	10✳	W 7	W 8	W 8
18	108.7	114.0	120.6	114.4	-5.5	-7.2	-7.2	-6.8	-4.3	-7.6	87	82	82	84	0.5	0.6	0.6	0.6	10✳	10✳	10✳	WNW 6	WSW 6	W 6
19	120.1	118.9	120.8	119.9	-7.3	-2.7	-0.3	-2.6	-0.3	-8.9	88	89	92	90	0.4	0.6	0.5	0.5	10✳	10✳	10●⚠	ESE 1	SW 1	SW 3
20	122.0	122.3	121.0	121.8	-0.7	-0.6	-0.3	-0.5	0.0	-1.2	85	81	78	81	0.9	1.1	1.4	1.1	10⚠	9✳	10	SW 2	W 3	SW 2
21	119.8	120.6	122.9	121.1	-3.0	-4.7	-5.3	-4.6	-0.2	-5.6	81	86	85	84	0.9	0.6	0.6	0.7	10✳	10✳	10✳	WSW 4	SW 4	NW 1
22	126.6	126.8	129.5	127.6	-8.2	-7.6	-10.5	-9.2	-5.3	-10.8	81	67	84	77	0.6	1.1	0.4	0.7	10✳	9	9	C 0	NE 3	C 0
23	129.1	126.4	122.6	126.0	-11.7	-6.3	-9.1	-9.0	-6.2	-13.0	82	55	79	72	0.4	1.7	0.6	0.9	10	10✳	10✳	C 0	ENE 1	SE 1
24	118.2	115.7	116.7	116.9	-10.9	-7.4	-12.2	-10.7	-7.5	-12.2	80	65	85	77	0.5	1.2	0.4	0.7	10✳	10✳	6✳	ESE 1	SE 1	C 0
25	117.5	118.5	119.3	118.4	-20.5	-8.9	-15.7	-15.2	-7.7	-21.4	82	64	77	74	0.2	1.1	0.4	0.6	5	10	5	C 0	NW 1	C 0
26	119.8	119.5	119.0	119.4	-19.6	-5.4	-9.3	-10.9	-5.4	-21.1	83	62	79	75	0.2	1.5	0.6	0.8	6	3⊙	8	C 0	E 1	SW 1
27	118.0	116.5	116.0	116.9	-9.3	-1.1	-2.6	-3.9	-0.3	-10.1	79	73	83	78	0.6	1.6	0.9	1.0	9	9	10	C 0	ENE 2	C 0
28	114.0	112.5	111.6	112.7	-4.4	0.4	-2.3	-2.2	0.9	-4.6	86	72	85	81	0.6	1.8	0.8	1.1	9✳	9	8	C 0	C 0	C 0
29																								
30																								
31																								
M	116.9	116.0	117.0	116.6	-7.5	-2.7	-5.0	-5.0	-1.0	-9.5	82	72	82	79	0.6	1.5	0.8	1.0	9.0	8.3	8.7	1.7	2.4	2.2

Zakopane $H_s = 844\,m$ $H_b = 838{,}2\,m$ $h_w = 17{,}7\,m$ Styczeń - Janvier 1962

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	1.6	24	•°9^07-39 ⁂°-10^01 *^0-1-10^52 *°13^45-15^40
2	7	1.0	18	*°3^45...4^20 ⊽°6^05-7^45, 8^30-9^25 ♎°-11^40 *°-12^10 ♎°-13^40, 14^55-15^10, ~°6^05-9^25
3	9	·	19	
4	7	·	18	=8^20-48 ≡°-10^35; v°8^48-10^35
5	9	·	18	⌴°19-24
6	8	0.5	18	⌴°0-9
7	6	1.7	18	*°0^35...1^40, 6^32...8^30-15^40, 19^00-20^15, 20^30-24
8	9	0.0	21	⚥°0^00-20 *°16^45...18^10
9	6	·	20	=0^30-3^35 ≡-7^50 =-8^20 ≡'-8^50 =-16^15; v3^35-8^50; ⌴°19-24
10	8	·	20	⌴°0-7
11	8	·	20	⌴'1-8
12	6	2.0	18	•°7^05...8^15-9^12 ⁂°-11^22 ♎°18^38-20^45, =8^15-16^45 ≡'-18^40 =21^50
13	9	2.0	17	•°9^15-45 ♎°19^20-20^25 *°...21^45 *°-1 22^40-24, ≫0^20-3^30
14	9	·	24	*°-1 0^00-1^15 *°2^10...4^15
15	9	·	25	
16	8	·	25	⌴°21-24
17	9	·	25	⌴°0-9 ⌴°-1 20-24, ⚲°-1 18^40-24
18	7	·	22	⌴'0-10, ⚲'0^00-5^30
19	8	0.0	22	
20	9	0.0	21	•°3^45...4^20 ⚥°18^50-19^20, 20^35-21^30
21	8	0.0	18	•°16^25...38
22	8	·	14	⚶°0^10-2^20
23	9	·	13	⌴°1-9, ⚶°1-7 ⚲°20^45-23^10
24	9	0.3	13	*°23^05-24; ⌴°2-8
25	8	3.0	12	*°0^00...1^40 •°6^05...45 7^10-9^10 ⚥°10^07-25 •°22^40-23^40
26	6	6.5	8	•°3^10-7^35 *°-10^50, 11^45...12^15-15^55, 23^10-24
27	6	9.2	15	*°-1 0^00-3^30 ♎°⚥°-4^10 ⚥°-1-7^20 *°-1-12^20 ⚥°12^30-16^40 ♎°-19^20 ⚥°-1-24; =na, a-p
28	9	8.8	55	⚥'0^00-30 *'-0-11^43 *°13^45-14^50...15^30-16^45, 17^20-20^15 ⚥°-1 20^35-22^10, 22^30-24
29	6	5.4	55	⚥°0^00-10 *'-0 0^20-24; =1-24
30	6	0.6	60	*°0^00-5^40, 6^10-21^15; =0^00-5^40, 8^15-18^30
31	6	0.5	50	⚥'-0 9^25-13^30 *°-16^45; =16^30-24
Σ	—	43.4	—	UWAGI:

Luty - Février

1	8	0.4	50	*°20^15...24
2	8	1.0	48	*°0^00-3^20 ↔-5^35; =5^35-9^30, 17^30-18^45
3	7	2.2	49	*°3^15-11^30 ♎°-23^10
4	8	0.0	46	*°1^20-2^13 ⚲°20^42-22^35; =4^30-9^40
5	8	6.8	44	*°15^50-18^40, 20^30-21^20 ♎°-22^15 *°-1-23^25 ⚥°23^40-24
6	6	2.8	53	⚥°-2 0^00-23^35; =8^10-24
7	9	·	55	⚥°0^00-3^40; =0^00-3^10; ⌴°20-24
8	7	0.0	53	⌴°0^00-8; ∩ 10^20-12^35, ⊕°10^30-14^15
9	7	2.4	50	♎°-1 6^28-11^40 *°18^40-19^20 •°...20^10 *°...22^40; =a ≡2-0 17^50-19^40 =p, np
10	8	·	47	⚲°0^25-3^30; =0^00-7^15; ~°0^25-3^30
11	8	0.3	44	*°9^32...10^40, 12^36-13^10 ⚥°15^35-16^15 ⚥°-17^42 ⚥°19^45-20^30 ♎ ⚥°-22^06
12	9	3.3	45	•°17^30...24; ≫-⊘ p-np; ⌴°1-8
13	6	5.4	50	•°0^00-4^45 *°-6^45 ♎-7^25 *°-17^40 ⚥°18^25-19^25 ♎°21^20-24; ≫0^00-4^30; =6^30-17^40
14	5	10.0	40	♎°0^00-35, 5^40-6^10 ⚥°-2 7^10-14^35 ♎² 9^35-40 *² 14^35-15^35 *°-24; =6^30-24
15	5	4.3	60	*°0^00-5^40 ⚥°5^50-11^20 *°-1-21^30 ⚥°-24; =na, a-np, np
16	6	4.2	70	⚥°0^00-20, 1^35-2^10 *°8^50...9^30 ♎°-11^45 *°-14^50, 18^35...19^40, ⚹ 15^35-17^15; ≫p, np; =na
17	5	13.6	60	*°-1 0^00-1^35, 5^40-10^40...11^35-16^40...17^20-24; ⚹ 11^35-17^10, 17^40-19^20, por wiatru do 14m/s 0-15^15; =6^15-24
18	6	7.7	80	*'-0 0^00-9^30 ⚥°-3-18^35 *'-24; ⚹°9^30-18^35
19	5	10.8	92	*°0^00...1^30 *°-1 5^40...7^10-20^35 ⚲°-2 ♎°-22^35 ♎°-24; =na-a, p, np
20	7	2.1	86	♎°0^00-30 ♎°-2^16 4^28-5^18 5^45-7^15 ♎'-7^40 ⚥°-10^30 ♎°-10^50 ⚥°12^03-13^15, 15^26-16^28; =na
21	6	9.1	82	⚥°0^30-1^15, 2^15-4^35 ⚥°-1 6^00-10^40, 11^05-14^45 *°-1-24; =na-a, a-np
22	7	0.7	105	⚥°-1 0^00-10^10 ⚥°11^12-40, 13^45-17^40 *°-22^40; =11^40-12^10, 14^45-18^30
23	7	1.3	103	⚥°7^10-8^25 *°12^15-14^10, 16^00-24; =7^30-9^15, 20^30-24
24	6	0.5	96	*°0^00-9^20, 12^40...13^15, 19^40-50, 20^00-21^15; =0^00-13^30, 15^30-24
25	7	·	87	=0^00-6^15; ⌴°1^30-8; ⌴'21-24
26	7	·	85	=9^40-12^30; ⌴'0^00-10 ⌴°18-24
27	8	0.2	82	=19^15-20^30; ⌴'0^00-9
28	7	0.0	77	*°5^35-6^35...11^45; =5^35-12^30, 16^30-24
29				
30				
31				
Σ	—	89.1	—	UWAGI:

Zakopane φ=49°18' λ=19°57' Marzec - Mars 1962

DNI	CIŚNIENIE P-800+ I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	109.1	107.3	106.8	107.7	-4.9	-0.1	-3.2	-2.6	0.5	-7.5	88	80	90	86	0.5	1.2	0.5	0.7	10	10	10	C 0	E 2	E 2
2	105.9	105.4	106.8	106.0	-4.4	-2.0	-4.2	-3.7	-1.6	-4.6	81	70	79	77	0.8	1.6	0.9	1.1	10	10	4	C 0	C 0	C 0
3	107.3	107.7	107.1	107.4	-5.3	0.7	-0.1	-1.2	0.7	-7.5	85	62	71	73	0.6	2.5	1.8	1.6	10	10	6	SW 1	E 2	C 0
4	101.9	99.4	98.5	99.9	3.3	7.0	8.9	7.0	9.4	-1.2	63	59	64	62	2.9	4.1	4.2	3.7	8	10	10 ●	NE 4	SSW 6	S 3
5	100.0	101.2	99.5	100.5	8.0	12.1	10.8	10.4	13.0	6.6	62	55	57	58	4.0	6.3	5.6	5.3	9	7 ⊙	8 ●	ESE 2	SW 8	S 10
6	98.2	106.0	112.9	105.7	5.6	2.7	-3.6	0.3	11.6	-3.6	87	73	85	82	1.2	2.0	0.7	1.3	10 ●	7 ⊙	10 ✳	E 1	WSW 3	W 2
7	116.9	118.7	122.6	119.4	-6.5	-6.3	-7.3	-6.8	-3.5	-7.7	78	83	79	80	0.8	0.6	0.7	0.7	10 ✳	10 ✳	10 ✳	E 1	NE 3	ENE 1
8	124.8	126.2	126.6	125.9	-12.6	-4.2	-13.5	-11.0	-3.2	-13.7	81	60	80	74	0.4	1.8	0.4	0.9	5	6 ⊙	0	E 1	E 1	C 0
9	125.9	124.8	121.9	124.2	-16.2	-0.7	-9.2	-8.8	0.8	-17.1	81	62	85	76	0.3	2.2	0.4	1.0	1 ⊙	2 ⊙	1	C 0	C 0	C 0
10	116.9	115.3	115.6	115.9	-6.1	3.4	-3.3	-2.3	5.7	-10.6	71	46	81	66	1.1	4.2	0.9	2.1	7 ⊙	10	5	NE 2	ENE 3	C 0
11	113.6	112.2	109.1	111.6	-3.8	3.1	0.8	0.2	3.8	-6.2	87	70	94	84	0.6	2.2	0.4	1.1	10	10 ●	10 ●	C 0	E 1	C 0
12	103.4	100.0	97.7	100.4	0.4	1.1	0.0	0.4	2.0	0.0	94	92	98	95	0.4	0.5	0.1	0.3	10 ● ═	10 ✳	10	C 0	E 1	SW 3
13	103.6	108.0	113.7	108.4	-5.9	-6.3	-9.0	-7.6	0.0	-9.5	76	70	70	72	0.9	1.1	0.9	1.0	10 ✳	9 ⊙	8	W 4	WSW 4	W 2
14	116.9	118.9	119.7	118.5	-11.0	-7.1	-9.7	-9.4	-6.6	-14.0	76	42	72	63	0.6	2.1	0.8	1.2	10 ✳	10	10	SW 1	WNW 2	C 0
15	116.4	114.3	113.4	114.7	-10.3	-9.4	-10.7	-10.3	-9.3	-11.7	68	79	80	76	0.9	0.6	0.5	0.7	10	10 ✳ ♙	10 ♙	ENE 4	ENE 4	ENE 3
16	111.3	112.5	113.6	112.5	-10.4	-9.4	-11.5	-10.7	-9.0	-11.6	84	79	79	81	0.4	0.6	0.5	0.5	10 ✳	10 ✳	10 ✳	E 4	E 4	E 3
17	110.5	109.3	111.7	110.5	-12.2	-9.3	-10.5	-10.6	-8.2	-12.5	78	70	77	75	0.5	0.9	0.6	0.7	10 ✳	10 ✳	10 ✳	NE 1	N 1	C 0
18	113.1	116.5	118.7	116.1	-8.9	-6.7	-8.1	-8.0	-6.0	-10.7	76	59	75	70	0.7	1.5	0.8	1.0	10 ✳	9	10 ✳	C 0	NE 1	C 0
19	119.3	119.4	120.2	119.6	-11.7	-4.4	-7.6	-7.8	-3.6	-12.1	82	55	73	70	0.4	2.0	0.9	1.1	8	7 ⊙	9	W 1	NE 2	C 0
20	120.0	120.2	119.3	119.8	-10.3	-3.8	-11.7	-9.4	-3.0	-12.0	74	62	82	73	0.7	1.8	0.4	1.0	8	8	1	C 0	ENE 2	C 0
21	115.2	113.3	111.2	113.2	-14.9	-2.5	-6.3	-7.5	-2.2	-17.0	73	65	83	74	0.5	1.8	0.6	1.0	0 ⊙	3 ⊙	10	C 0	C 0	C 0
22	108.3	107.2	106.7	107.4	-5.7	-1.8	-5.2	-4.5	-1.6	-6.7	87	79	88	85	0.5	1.1	0.5	0.7	10 ✳	10 ♙	10 ✳	C 0	NE 1	C 0
23	105.9	106.9	109.5	107.4	-6.6	-3.1	-4.7	-4.8	-2.7	-7.0	80	77	86	81	0.7	1.1	0.6	0.8	10 ✳	10 ♙	10 ✳	C 0	ENE 2	C 0
24	113.2	116.0	119.7	116.3	-5.7	-1.9	-4.5	-4.2	-1.2	-6.3	82	67	86	78	0.7	1.8	0.6	1.0	10 ✳	9	10 ✳	SE 1	NE 1	NE 1
25	120.6	119.8	118.0	119.5	-7.5	-2.1	-6.9	-5.8	-1.8	-7.6	82	70	74	75	0.6	1.5	0.9	1.0	9	10	7	C 0	NNE 1	NE 2
26	115.3	113.5	112.2	113.7	-15.7	-2.4	-7.7	-8.4	-2.1	-18.1	72	57	76	68	0.5	2.2	0.8	1.2	6 ⊙	2 ⊙	6	C 0	NE 3	NE 2
27	108.4	107.3	107.9	107.9	-9.7	0.2	-5.2	-5.0	2.9	-18.5	81	60	75	72	0.5	2.5	1.0	1.3	10	9 ⊙	0	C 0	E 2	ESE 1
28	106.8	107.0	109.9	107.9	-4.6	0.7	-0.4	-1.2	3.5	-5.8	86	88	80	85	0.6	0.8	1.2	0.9	7	10 ✳	10 ♙	SE 1	C 0	NW 2
29	111.6	110.5	107.2	109.8	-1.4	4.1	-0.6	0.4	5.0	-1.8	80	43	73	65	1.1	4.7	1.5	2.4	9	9 ⊙	5	W 1	W 2	C 0
30	104.8	105.0	102.4	104.1	1.1	10.3	8.7	7.2	10.6	-1.1	81	47	58	62	1.3	6.6	4.7	4.2	9 ●	5 ⊙	8	C 0	W 3	SW 5
31	99.7	100.6	101.7	100.7	4.2	9.5	3.2	5.0	10.7	3.1	78	62	84	75	1.7	4.6	1.2	2.5	9	9	2	E 1	E 2	ESE 1
M	111.1	111.3	111.7	111.4	-6.1	-0.9	-4.3	-3.9	0.5	-8.2	79	66	79	75	0.9	2.2	1.1	1.4	8.5	8.4	7.4	1.0	2.2	1.4

Kwiecień - Avril

1	107.9	111.6	115.1	111.5	0.7	0.5	0.4	0.5	5.1	0.1	92	92	65	83	0.5	0.5	2.3	1.1	10 ♙ ●	7 ✳	1	ESE 2	SW 2	W 3
2	114.6	115.4	118.6	116.2	1.2	4.6	1.8	2.2	5.5	-2.3	60	49	72	60	2.8	4.3	2.0	3.0	9 ⊙	9 ⊙	4	W 2	SW 6	W 1
3	120.1	118.0	114.0	117.4	-1.9	7.9	4.7	3.8	9.7	-4.2	71	52	55	59	1.6	5.1	3.8	3.5	1 ⊙	5 ⊙	2	C 0	ENE 2	C 0
4	107.3	107.2	104.3	106.3	7.5	9.1	7.4	7.8	10.4	1.7	32	41	56	43	7.1	6.9	4.5	6.2	3 ⊙	9	5 ●	SSE 10	S 8	SSW 6
5	92.6	94.4	96.8	94.6	8.1	5.3	2.6	4.6	9.9	2.4	60	85	89	78	4.4	1.3	0.9	2.2	10 ●	10 ●	9	SSW 7	NE 2	C 0
6	97.6	99.8	103.6	100.3	0.3	1.0	0.5	0.6	2.6	-0.2	94	92	94	93	0.3	0.5	0.3	0.4	10 ✳	10 ✳	10 ✳	C 0	C 0	WSW 2
7	108.4	113.9	115.6	112.6	0.6	-1.2	-3.3	-1.8	0.9	-3.9	90	84	83	86	0.7	0.9	0.8	0.8	10 ✳	9 ✳	5	WSW 4	SW 5	SW 3
8	114.5	115.9	114.8	115.1	1.4	4.8	3.2	3.2	7.5	-3.8	78	72	79	76	1.6	2.4	1.6	1.9	10	9	3	W 3	SW 2	ESE 2
9	115.7	116.6	119.4	117.2	1.6	9.2	2.6	4.0	11.2	-0.5	73	50	91	71	1.8	5.8	0.7	2.8	3 ⊙	6 ⊙	10	ESE 1	E 1	C 0
10	120.5	121.0	122.3	121.3	1.8	5.4	2.5	3.0	5.7	1.5	91	73	93	86	0.7	2.4	0.5	1.2	10	10	10	C 0	NE 2	SE 1
11	122.1	121.4	122.3	121.9	2.0	4.3	2.4	2.8	4.8	2.0	94	93	96	96	0.4	0.5	0.3	0.4	10 ═	10	10 ═	C 0	ENE 1	C 0
12	121.5	120.3	119.5	120.4	2.2	8.1	2.7	3.9	9.7	1.5	93	77	93	88	0.6	2.4	0.5	1.2	10	8 ⊙	6	C 0	C 0	ESE 2
13	117.1	114.5	113.3	115.0	2.7	9.8	4.4	5.3	10.1	0.0	90	59	91	80	0.7	4.8	0.8	2.1	4 ⊙	9	10 ●	ESE 1	NE 1	SE 4
14	115.6	117.9	121.7	118.4	0.2	3.6	1.9	1.9	4.4	0.1	92	76	93	87	0.5	1.9	0.5	1.0	10 ♙	10	10	W 2	W 1	E 1
15	121.6	121.4	121.8	121.6	2.0	5.7	6.9	5.4	8.4	1.0	94	89	94	92	0.4	1.1	0.5	0.7	10 ●	9	10	E 2	ENE 3	NE 1
16	121.2	122.8	125.6	123.2	5.6	13.8	6.9	8.3	14.8	2.1	82	48	73	68	1.6	8.3	2.6	4.2	9 ⊙	8	3	SE 1	E 1	ENE 2
17	126.8	126.9	124.7	126.1	8.2	15.0	14.0	12.8	15.6	2.7	58	35	24	39	4.7	11.0	12.2	9.3	5 ⊙	9	9	ENE 5	SE 4	S 6
18	123.3	123.1	122.8	123.1	13.5	16.2	8.5	11.7	17.0	7.8	34	32	63	43	10.3	12.6	4.1	9.0	10	10	8	S 7	S 7	SE 2
19	122.8	123.7	124.0	123.5	7.6	17.8	8.6	10.6	19.0	5.1	66	27	67	53	3.5	14.8	3.7	7.3	8	10	1	C 0	NE 2	C 0
20	124.9	124.1	124.5	124.5	6.9	19.7	9.8	11.6	19.9	3.1	76	33	66	58	2.3	15.2	4.1	7.2	1 ⊙	3 ⊙	8	C 0	E 2	C 0
21	126.0	125.4	125.1	125.5	8.3	19.9	10.9	12.5	21.3	4.2	72	30	57	53	3.1	16.3	5.6	8.3	8 ⊙	5 ⊙	1	SE 1	SE 2	ESE 2
22	125.4	125.0	125.3	125.2	10.0	19.9	10.9	12.9	21.3	3.7	61	34	62	52	4.9	15.3	5.0	8.4	0 ⊙	3 ⊙	2	SSE 2	NE 2	SE 1
23	125.6	125.4	125.8	125.6	12.4	21.5	10.0	13.5	22.2	5.2	54	33	72	53	6.5	17.1	3.5	9.0	0 ⊙	3 ⊙	2	C 0	NE 2	C 0
24	127.1	127.8	128.9	127.9	10.3	21.2	10.6	13.2	22.0	6.2	72	29	69	57	3.5	18.0	4.1	8.5	1 ⊙	2 ⊙	0	C 0	E 3	SE 1
25	130.1	129.7	129.7	129.8	10.4	20.7	10.1	12.8	21.5	5.4	73	33	76	61	3.4	16.4	3.1	7.6	1 ⊙	4 ⊙	0	C 0	E 3	C 0
26	127.9	124.9	120.2	124.3	11.0	18.7	8.9	11.9	19.9	6.0	66	26	68	53	4.6	16.1	3.7	8.1	0 ⊙	1 ⊙	0	SW 2	NE 3	C 0
27	113.6	113.9	115.0	114.2	11.4	8.5	2.6	6.3	12.9	2.3	71	75	90	79	4.0	2.8	0.7	2.5	9	10	10 ●	C 0	SE 2	C 0
28	108.9	107.9	108.1	108.3	2.8	1.4	1.1	1.6	5.1	-0.5	77	91	90	86	1.8	0.7	0.6	1.0	10	8 ✳	10 ✳	SW 3	W 5	NNW 2
29	109.4	110.5	110.8	110.2	0.0	0.6	-0.8	-0.2	2.8	-0.8	84	90	87	87	1.0	0.7	0.8	0.8	10 ♙	10 ✳	1	ESE 1	NE 3	W 2
30	109.0	109.6	112.9	110.5	-1.3	3.2	-0.3	0.3	3.5	-3.5	84	57	94	78	0.9	3.3	0.4	1.5	9 ♙	8	9	E 2	NE 2	NE 3
31																								
M	117.3	117.7	118.2	117.7	4.9	9.9	5.1	6.2	11.5	1.5	74	59	77	70	2.7	7.0	2.5	4.1	6.7	7.5	5.6	1.9	2.6	1.6

Zakopane $H_s = 844\,m$ $H_a = 838{,}2\,m$ $h_w = 17{,}7\,m$ Marzec - Mars 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	·	72	$=0^{00}-9^{30}, 20^{10}-24$
2	7	0.0	70	$\triangle^{\circ}8^{07}-11^{15}, =0^{00}-9^{30}$
3	7	0.0	70	$*^{\circ}1^{40}-3^{15}, 8^{45}\ldots 9^{20}$
4	9	0.2	68	$\overset{\bullet}{\nabla}{}^{\circ}0^{25}-2^{13} *^{\circ}3^{30}-5^{40} \overset{\bullet}{\nabla}{}^{\circ}14^{48}-16^{30} \bullet^{\circ}-21^{35}, = na$
5	9	1.6	48	$\overset{\bullet}{\nabla}{}^{\circ}20^{15}-21^{25}, 22^{50}-24; \gg p, np$
6	8	5.1	50	$\overset{\bullet}{\nabla}{}^{\circ}0^{00-10}, 1^{40}-2^{45} \bullet^{\circ}-7^{50} *^{\circ}14^{35}\ldots 15^{10}-16^{40}, 20^{40}\ldots 24; = p-24$
7	5	8.1	54	$*^{\circ}0^{00}-12^{15} *'-16^{25} *^{\circ}-22^{30}\ldots 23^{10}-24, = 0^{00}-20^{20}, np$
8	8	·	44	$*^{\circ}0^{00}-3^{30}\ldots 5^{15}, = 0^{00}-3^{30}, \sqcup' 19-24$
9	9	·	40	$\sqcup' 0^{00}-8$
10	9	·	37	
11	6	0.3	32	$*^{\circ}11^{01}\ldots 12^{15} \bullet^{\circ}13^{42}\ldots 14^{23}, 16^{35}-18^{30} \bullet_{\bullet}{}^{\circ}-19^{40} \bullet_{\bullet}{}^{\circ}-21^{15}, = 12^{30}-19^{50} \equiv^{\circ}-20^{30} = -23^{30} \equiv^{\circ}-24, \sqcup^{\circ} na-8; \oplus^{\circ} a$
12	5	6.7	29	$\bullet_{\bullet}{}^{\circ}6^{05}-7^{25} 9^{20}-10^{15} *^{\circ}-14^{30} *^{\circ-1}-24; \equiv^{\circ\prime} 0^{00}-7^{30} = -24$
13	8	1.5	34	$*^{\circ}0^{00}-4^{45}, 6^{18}-9^{30} \overset{\bullet}{\nabla}{}^{\circ-1}\ldots 17^{35}, = 0^{00}-3^{20}$
14	9	0.0	38	$*^{\circ}6^{10}\ldots 7^{40} \overset{\bullet}{\nabla}{}^{\circ}14^{20-35}; \oplus' 9^{30}\ldots 19^{30}$
15	5	7.2	34	$*^{\circ}9^{43}\ldots 11^{15} \triangle' -12^{30} *^{\circ} \triangle' -14^{15} *^{\circ}-15^{10} \triangle' -24, = 11^{25}-24$
16	5	10.2	47	$\triangle' 0^{00-10} *^{1-0}-24, = 0^{00}-24$
17	6	5.0	55	$*^{\circ}0^{00}-9^{40} \overset{\bullet}{\nabla}{}^{\circ}-10^{10} *^{\circ}-24, = 0^{00}-24$
18	9	0.3	66	$*^{\circ}0^{00}-11^{15}\ldots 12^{10}, 19^{35}\ldots 20^{45} \overset{\bullet}{\nabla}{}^{\circ}21^{30}-22^{15} *^{\circ}22^{45}\ldots 24, = 0^{00}-11^{15}; \oplus^{\circ}15^{15}-16^{40}$
19	9	·	62	$*^{\circ}0^{00-40}$
20	7	·	54	$\sqcup^{\circ} 23-24$
21	9	0.5	52	$\sqcup^{\circ} 0^{00}-9$
22	6	3.1	50	$*^{\circ}4^{40}-12^{15} \triangle^{\circ}-19^{20} *^{\circ}-24, = 5^{30}-24$
23	7	4.1	55	$*^{\circ}0^{00}-9^{15} \triangle^{\circ}-16^{25} *^{\circ}-24, = 0^{00}-8^{30}, 15^{30}-24$
24	6	0.2	60	$*^{\circ}0^{00}-2^{30} *'-4^{15} *^{\circ}-7^{30}\ldots 8^{45}, 15^{40}-18^{50}, 20^{35}\ldots 22^{40}, = 0^{00}-24$
25	7	·	58	$=0^{00}-5^{30}, \sqcup^{\circ} 21-24$
26	9	·	55	$\sqcup^{\circ} 0^{00}-9$
27	8	0.1	55	$\sqcup' 0^{00}-8 \sqcup^{\circ} 19-24; \oplus^{\circ} 8-11^{30} \oplus' -14^{15} \oplus^{\circ}-15^{10}$
28	6	2.9	51	$\overset{\bullet}{\nabla}{}^{\circ}0^{25}-1^{13}, 11^{30}-12^{15} *^{2-0}-15^{35} \overset{\bullet}{\nabla}{}^{\circ}20^{32}-21^{07} \overset{\bullet}{\nabla}{}^{\circ}21^{25}-22^{15}$
29	8	0.0	50	$\overset{\bullet}{\nabla}{}^{\circ}0^{35}-1^{16}, 7^{14-43}; \oplus^{\circ}12^{30}-13^{20}$
30	9	0.0	49	$\bullet^{\circ}6^{15}\ldots 7^{10}, = 3^{30}-4^{40}$
31	8	4.7	55	
Σ	—	61.8	—	UWAGI

Kwiecień - Avril

1	8	0.6	25	$\overset{\bullet}{\nabla}{}^{\circ-2}1^{02}-2^{20} \bullet_{\bullet}{}^{\circ}3^{30}\ldots 5^{50} \triangle^{\circ} \bullet_{\bullet}{}^{\circ}6^{10}-7^{16} \overset{\bullet}{\nabla}{}^{\circ}10^{05-30}, 11^{25}-12^{45}, \gg 1^{02-30}$
2	8	1.5	25	$\overset{\bullet}{\nabla}{}^{\circ}13^{10-18} \overset{\bullet}{\nabla}{}' 21^{15-35} \overset{\bullet}{\nabla}{}' \triangle' -21^{40} \overset{\bullet}{\nabla}{}^{1-0}-22^{10}$
3	9	·	25	
4	9	1.1	15	$\overset{\bullet}{\nabla}{}^{\circ}17^{35-51} 18^{41}-19^{25}, 20^{10-20}, 22^{23-38}; \nwarrow na, a \gg a, p, np$
5	7	5.6	pł.	$\bullet^{\circ}4^{10}-5^{10} \overset{\bullet}{\nabla}{}^{\circ-1}-7^{35} \overset{\bullet}{\nabla}{}^{\circ}9^{50}\ldots 11^{20} \bullet^{\circ}11^{35}\ldots 13^{50}, 15^{15}-17^{20}, \frown' 7^{15-35}$
6	5	21.2	2	$\bullet^{\circ}4^{48}\ldots 5^{01} *^{\circ-1}-24, = 6^{15}-24$
7	7	2.3	27	$*^{1-0}0^{00}-9^{30} \triangle -10^{37} *^{\circ}-12^{15} \overset{\bullet}{\nabla}-13^{20} \overset{\bullet}{\nabla}{}^{\circ}14^{45}-15^{15} \overset{\bullet}{\nabla}{}^{\circ}-15^{45} *^{\circ}-18^{32} = 0^{00}-12^{15}$
8	8	·	30	$\overset{\bullet}{\nabla}{}^{\circ}3^{15}-4^{10}$
9	8	·	13	
10	7	4.3	9	$*^{\circ}8^{05-14} \bullet^{\circ}5^{55}\ldots 10^{10} \overset{\bullet}{\nabla}{}^{\circ}13^{50}\ldots 14^{10} \bullet^{\circ}14^{20}-18^{20}, 21^{40}\ldots 24; = a, np$
11	6	·	pł.	$\bullet^{\circ}0^{00-05}, 4^{15}-5^{45}; \equiv' 6^{15}-7^{40} = \equiv^{\circ}-17^{30} \equiv^{1-2}-24$
12	6	·	pł.	$\equiv^{2} 0^{00}-3^{25} = -13^{30}$
13	7	4.9	pł.	$\bullet^{\circ}19^{05\ldots 30}, 20^{21}-21^{15} \bullet_{\bullet}{}^{\circ}-22^{15} \bullet^{\circ}-24, = 18^{30}-24$
14	8	1.0	pł.	$\bullet^{\circ}0^{00}-2^{45} *^{\circ}4^{10}\ldots 5^{20} \triangle^{\circ}6^{23}-7^{15}, = 0^{00}-7^{30}, 16^{40}-21^{30} \equiv^{\circ}-24$
15	6	0.7	pł.	$\bullet_{\bullet}{}^{\circ}2^{20}-3^{35}, 4^{15}\ldots 5^{10}-10^{25}, 10^{40}-11^{13}; \equiv 0^{00-40} = -9^{30}, 12^{30}-13^{15}$
16	8	·	pł.	
17	9	·	·	$\gg np\ldots$
18	9	·	·	$\gg na, a\ldots$
19	9	·	·	
20	9	·	·	$\triangle' na-a \triangle^{\circ}22-24, \varnothing^{\circ}20^{50}-24$
21	8	·	·	$\triangle^{\circ}0^{00}-7, \cup^{\circ}0^{00}-3^{30}$
22	9	·	·	$\triangle^{\circ}0^{00}-7, 23-24$
23	9	·	·	$\triangle^{\circ}0^{00}-9^{00}\ p-n$
24	9	·	·	$\triangle^{\circ} na-7 \triangle^{\circ-1} 19-24$
25	9	·	·	$\triangle' 0-9, 20-24$
26	9	0.2	·	$\triangle' 0-9$
27	7	11.5	·	$\bullet^{\circ}2^{35}\ldots 3^{10} \overset{\bullet}{\nabla}{}^{\circ-1} 8^{25}-10^{43}, 13^{03}\ldots 19^{33} \overset{\bullet}{\nabla}{}' -20^{40}$
28	8	8.7	·	$\overset{\bullet}{\nabla}{}^{\circ}8^{00}\ldots 10^{16} \overset{\bullet}{\nabla}{}^{\circ}\ldots 11^{17} \overset{\bullet}{\nabla}{}^{\circ}\ldots 11^{24} \overset{\bullet}{\nabla}{}' -11^{52} \overset{\bullet}{\nabla}{}^{\circ}\ldots 14^{02} \overset{\bullet}{\nabla}{}^{\circ} 14^{25-38} \overset{\bullet}{\nabla}{}^{\circ} 15^{03}\ldots 18^{06} \overset{\bullet}{\nabla}{}^{1-0}-18^{42}\ 20^{35}\ldots 22^{10}; \nwarrow' 11^{16-42}\ NW-SE$
29	7	3.8	2	$*^{\circ}2^{03}-5^{30} \triangle^{\circ}-7^{03} \overset{\bullet}{\nabla}{}^{\circ} 7^{15-32} \overset{\bullet}{\nabla}{}^{\circ-1} 8^{25}-9^{50} \overset{\bullet}{\nabla}{}^{\circ-1} 10^{45}\ldots 15^{30}, = 3^{30}-5^{30}, \sqcup^{\circ} 20-24$
30	2	6.5	·	$\triangle^{\circ}6^{15}-7^{25} \overset{\bullet}{\nabla}{}^{\circ}7^{51}-8^{45} \overset{\bullet}{\nabla}{}^{\circ}13^{05-50}, 14^{35}-16^{15}\ldots 16^{40} \overset{\bullet}{\nabla}{}^{1-0}-19^{40}, \sqcup^{1-0} 0^{00}-7$
31				
Σ	—	103.9	—	UWAGI.

Zakopane — φ = 49°18' — λ = 19°57' — Maj – Mai 1962

DNI	CIŚNIENIE P = 800 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	113.7	113.3	112.7	113.2	-2.6	0.4	-2.3	-1.7	2.3	-2.9	95	81	89	85	0.8	1.2	0.6	0.9	9 ✳	9 ✳	2	E 1	SSW 2	C 0
2	109.5	109.0	111.2	109.9	-2.6	3.8	0.0	0.3	4.5	-4.9	87	53	100	80	0.7	3.7	0.0	1.5	8 ⊙	10	10 ✳	C 0	W 4	NNE 2
3	113.4	113.4	113.6	113.5	-1.2	4.5	0.4	1.0	6.4	-4.4	80	61	86	76	1.1	3.2	0.9	1.7	1 ⊙	8 ⊙	6	C 0	SSW 3	C 0
4	109.8	110.2	112.5	110.8	2.0	6.1	3.0	3.5	7.4	0.0	90	61	72	74	0.7	4.1	2.1	2.3	9	9	9	SSW 3	SSW 6	C 0
5	114.0	116.0	118.5	116.2	2.7	6.2	4.5	4.5	7.8	-1.4	76	70	83	76	1.7	2.9	1.4	2.0	8	10 ●	10 ●	E 1	C 0	C 0
6	121.1	121.9	122.3	121.8	3.4	8.9	3.2	4.7	11.1	1.8	87	54	84	75	1.0	5.3	1.2	2.5	10	8	0	C 0	NE 3	ESE 1
7	121.1	120.8	121.7	121.2	8.1	11.2	9.2	9.4	13.8	1.2	56	67	86	70	4.8	4.5	1.6	3.6	9	9	9	E 1	SE 2	SW 2
8	121.6	121.1	118.6	120.4	12.5	16.4	13.8	14.1	18.4	8.7	75	53	63	64	3.6	8.8	5.9	6.1	6 ⊙	10 ● R	10 ●	SW 2	WNW 4	SE 2
9	119.0	119.1	117.0	118.4	11.2	16.0	10.7	12.2	17.5	10.0	87	55	82	75	1.7	8.3	2.4	4.1	9	4 ⊙	8	NW 3	NNW 4	C 0
10	112.7	116.3	117.3	115.4	9.5	9.2	8.6	9.0	11.2	8.5	96	89	83	89	0.5	1.3	1.9	1.2	10 ●	10 ●	10	SE 1	WSW 4	WSW 3
11	116.9	117.2	117.3	117.1	6.6	7.6	4.4	5.8	8.7	4.4	91	69	90	83	0.9	3.2	1.1	1.7	10 ●	10 ●	1	E 1	C 0	C 0
12	118.6	118.5	119.6	118.9	7.6	12.2	7.1	8.5	12.5	0.5	73	56	91	73	2.8	6.2	0.9	3.3	5 ⊙	10	9	C 0	SE 2	C 0
13	120.3	120.8	117.7	119.6	8.5	9.9	10.0	9.6	12.4	1.9	71	83	84	79	3.2	2.1	2.0	2.4	3 ⊙	10 ●	10	C 0	NE 2	C 0
14	109.3	105.2	110.4	108.3	11.3	13.6	3.8	8.1	17.3	3.6	85	51	83	73	2.1	7.7	1.4	3.7	8	8	10 ●	SW 1	S 7	WSW 3
15	111.3	111.9	114.6	112.6	5.0	6.3	3.6	4.6	6.9	3.4	67	68	87	74	2.9	3.0	1.0	2.3	10	9	10 ●	WSW 4	SW 4	W 2
16	116.8	119.2	120.9	119.0	4.2	4.9	4.4	4.5	6.7	3.1	83	83	70	79	1.3	1.5	2.5	1.8	10 ●	10 ●	7	WSW 4	SW 3	NW 1
17	120.9	120.0	119.4	120.1	6.5	13.4	8.9	9.4	13.7	0.7	60	47	69	59	3.9	8.2	3.5	5.2	9	8 ⊙	10	WNW 2	WSW 6	NE 2
18	119.7	121.2	124.3	121.7	8.2	12.3	6.2	8.2	13.2	6.0	82	56	76	71	2.0	6.2	2.3	3.5	10 ●	8 ●	1	SE 1	W 5	C 0
19	122.7	119.8	116.1	119.5	7.7	17.1	17.1	14.8	18.3	2.0	68	45	45	53	3.4	10.7	10.7	8.3	4 ⊙	8 ⊙	8	ENE 1	S 5	S 6
20	113.9	114.4	116.9	115.0	15.3	8.8	5.9	9.0	17.6	5.6	59	82	92	78	7.2	2.0	0.8	3.3	9	10 ●	10 ●	E 2	E 1	NW 1
21	118.1	117.9	118.3	118.1	4.1	5.0	3.4	4.0	5.9	3.3	93	87	91	90	0.6	1.1	0.7	0.8	10 ●	10 ●	10 ●	C 0	ENE 1	C 0
22	118.5	119.1	122.5	120.0	6.4	14.6	9.5	10.0	14.6	0.5	80	45	72	66	1.9	9.0	3.3	4.7	1 ⊙	6 ⊙	10	SW 1	E 2	ESE 1
23	124.0	122.9	122.9	123.3	11.2	16.8	10.3	12.2	18.8	5.1	58	41	77	59	5.6	11.2	2.9	6.6	4 ⊙	4 ⊙	2	NW 3	NW 3	C 0
24	122.3	121.8	118.9	121.0	10.7	9.5	8.3	9.2	11.5	6.3	77	93	96	89	3.0	0.8	0.5	1.4	9	10 ●	10	C 0	SW 1	C 0
25	117.2	117.3	116.2	116.9	6.6	8.5	7.1	7.3	8.9	6.2	94	90	96	93	0.5	1.1	0.5	0.7	10 ●	10	10	C 0	NE 1	NE 1
26	114.2	113.5	116.8	114.8	7.7	14.7	10.8	11.0	16.8	6.7	96	80	92	89	0.5	3.3	1.1	1.6	10	9	10	E 1	ENE 3	C 0
27	118.4	119.8	120.5	119.6	8.6	11.5	11.5	10.8	13.5	8.1	93	89	92	91	0.8	1.6	1.7	1.4	10	10	10	C 0	E 1	E 1
28	120.6	119.7	119.5	119.9	9.9	15.3	11.7	12.2	19.8	8.2	93	62	85	80	0.9	6.7	2.0	3.2	9	9	6	C 0	SW 2	C 0
29	121.7	122.3	121.3	121.8	10.4	12.1	10.9	11.1	15.4	8.4	86	87	92	88	1.8	1.9	1.0	1.6	10	10	7	E 1	C 0	C 0
30	122.3	123.6	123.9	123.3	6.9	7.4	6.0	6.6	11.5	5.4	92	88	86	89	0.7	1.2	1.4	1.1	10 ●	10 ●	0	NE 2	NNW 2	SE 1
31	122.8	120.0	117.1	120.0	8.7	16.0	15.4	13.9	18.8	1.0	65	44	45	51	3.9	10.1	9.6	7.9	0 ⊙	2 ⊙	2	C 0	SE 3	SW 4
M	117.6	117.7	118.1	117.8	6.9	10.3	7.3	8.0	12.4	3.5	80	67	82	76	2.1	4.6	2.2	3.0	7.7	8.6	7.3	1.2	2.8	1.1

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1	118.5	120.4	117.4	118.8	6.8	4.6	1.6	3.6	16.6	1.5	94	82	91	89	0.6	1.6	0.7	1.0	10 ●	10 ●	10 ● R	C 0	N 1	E 2
2	115.9	121.0	123.1	120.0	2.2	3.7	3.8	3.4	4.0	0.7	95	83	88	89	0.4	1.4	1.0	0.9	10	10	10	C 0	ENE 1	C 0
3	124.2	125.7	126.6	125.5	0.8	3.3	2.8	2.4	4.3	0.5	92	91	91	91	0.5	0.6	0.7	0.6	10 ✳ ●	10 ●	10 ●	C 0	SW 1	SE 1
4	125.3	125.8	124.7	125.3	0.5	0.9	0.6	0.6	4.4	0.5	96	96	96	96	0.2	0.2	0.3	0.2	10 ✳	10 ✳ ●	10 ✳ ●	C 0	C 0	SW 3
5	123.4	123.7	123.9	123.7	1.0	1.1	3.7	2.4	3.7	0.4	94	94	92	93	0.4	0.4	0.7	0.5	10 ✳ ●	10 ●	10 ●	C 0	NNW 3	NE 2
6	123.2	124.9	126.1	124.7	1.9	1.0	1.5	1.5	5.3	1.0	86	90	88	88	0.9	0.7	0.8	0.8	10 ●	10 ✳	10 ✳	NNE 2	E 1	E 2
7	125.0	128.3	129.9	127.7	0.6	1.3	0.4	0.7	1.8	0.0	88	91	96	92	0.8	0.7	0.3	0.6	10	10 ✳	10 ✳ ●	N 1	C 0	C 0
8	129.4	130.3	129.6	129.8	3.9	9.8	5.4	6.1	10.6	0.4	88	64	88	80	1.0	4.4	1.1	2.2	9	9	9	C 0	E 1	C 0
9	126.1	123.7	121.0	123.6	8.2	14.0	8.6	9.8	15.4	0.6	74	54	71	66	2.9	7.4	3.2	4.5	7	8 ⊙	7	S 2	W 2	SSE 2
10	118.5	118.0	117.2	117.9	8.0	13.3	9.3	10.0	17.3	5.1	83	69	79	77	1.8	4.8	2.5	3.0	10	6 ⊙	6	C 0	S 2	SE 2
11	115.4	114.0	115.4	114.9	10.6	12.8	9.0	10.4	17.0	4.2	72	86	93	84	3.6	2.2	0.9	2.2	8	10 ● R	10 ●	ESE 1	SW 2	W 1
12	117.2	117.8	119.7	118.2	6.2	7.7	6.7	6.8	9.6	6.0	92	80	83	85	0.8	2.1	1.6	1.5	10 ●	9	9	C 0	SE 1	SE 1
13	121.6	122.5	123.1	122.4	6.6	10.8	5.6	7.2	12.5	3.4	73	58	86	72	2.6	5.4	1.3	3.1	9	8	1	C 0	NE 2	C 0
14	122.3	121.8	123.4	122.5	10.6	17.7	11.3	12.7	19.3	1.1	61	50	78	63	5.0	8.1	3.0	5.4	7	7 ⊙	0	WNW 1	SE 2	S 1
15	125.6	126.6	127.3	126.5	14.8	21.9	14.1	16.2	23.9	7.8	69	48	61	66	5.1	13.7	3.1	7.3	0 ⊙	6 ⊙	1	C 0	NNE 3	C 0
16	126.9	126.2	126.0	126.4	17.4	25.1	15.6	18.4	25.2	9.3	74	48	82	68	5.1	16.4	3.3	8.3	0 ⊙	5 ⊙	3	C 0	E 2	C 0
17	126.3	126.1	125.7	126.0	17.2	15.2	14.7	15.4	17.7	10.8	84	91	91	89	3.3	1.6	1.5	2.1	9(R)	9(R)	9	C 0	C 0	C 0
18	125.0	124.3	124.1	124.5	13.2	18.4	12.2	14.0	19.0	12.2	94	67	90	84	0.9	6.9	1.4	3.1	10 ●	7 ⊙	0	C 0	NE 3	C 0
19	122.9	121.6	120.8	121.8	14.0	21.9	17.5	17.7	22.9	6.4	76	56	73	68	4.0	11.6	5.5	7.0	0 ⊙	3 ⊙	4	C 0	E 2	ESE 1
20	122.0	123.0	124.3	123.1	17.5	19.0	15.2	16.7	21.3	10.0	74	76	92	81	5.1	5.1	1.4	3.9	5 ⊙	8 ⊙	9	ENE 2	E 1	C 0
21	125.4	126.3	127.4	126.4	15.1	16.4	12.6	14.2	17.2	10.7	85	88	90	88	2.7	2.4	1.5	2.2	8 ⊙	10 ●	3	E 1	C 0	SE 1
22	128.9	128.7	128.9	128.8	14.6	20.6	15.3	16.4	22.1	8.7	85	58	89	77	2.6	10.2	2.0	4.9	2 ⊙	7	2	C 0	E 2	C 0
23	128.3	127.5	126.9	127.6	17.0	24.5	15.6	18.2	25.7	9.8	78	45	78	67	4.4	16.9	4.0	8.4	1 ⊙	4 ⊙	1	C 0	NE 2	C 0
24	125.7	124.4	123.7	124.6	20.1	25.1	17.8	20.2	27.0	11.6	59	39	71	56	9.4	19.3	5.9	11.5	6 ⊙	7 ⊙(R)	3	SE 2	NW 4	C 0
25	122.0	122.3	123.3	123.2	21.7	20.0	14.4	17.8	24.1	14.3	48	66	63	59	13.7	8.2	6.1	9.3	4 ⊙	8	10	SW 3	NNE 3	ESE 2
26	123.3	120.6	118.6	120.8	9.5	15.0	12.1	12.2	15.6	6.8	74	53	75	67	3.2	7.9	3.6	4.9	8	8	9	ENE 2	NE 3	C 0
27	117.2	117.4	119.1	117.9	10.3	15.4	10.5	11.7	16.5	5.0	78	49	60	62	2.7	9.0	5.1	5.6	9 ⊙	6 ⊙	10	C 0	WNW 3	SW 2
28	118.8	118.2	117.0	118.0	7.0	8.1	7.2	7.4	10.8	6.6	71	63	70	68	2.9	4.1	3.1	3.4	8 ⊙	9	10	NE 3	NW 5	WNW 4
29	117.1	118.4	119.3	118.3	6.6	9.4	7.0	7.5	10.5	4.7	65	58	74	66	3.4	5.0	2.6	3.7	7 ⊙	7 ⊙	8	SW 4	W 7	SW 1
30	118.6	119.3	121.1	119.7	6.6	9.4	6.6	7.3	10.4	3.0	73	58	91	74	2.6	5.0	0.9	2.8	10	9	10 ●	SW 1	SE 2	SE 1
31																								
M	122.7	123.0	123.2	123.0	9.7	12.9	9.3	10.3	15.1	5.4	79	68	83	77	3.1	6.1	2.3	3.8	7.2	8.0	6.8	0.8	2.0	1.0

Zakopane $H_s = 844m$ $H_k = 838{,}2m$ $h_w = 17{,}7m$ Maj - Mai 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	POGODA
1	7	0.4	3	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}5^{45}-6^{55}$ 7^{35-50} $8^{10}-12^{30}$ $12^{38}-13^{17}$ $15^{25}...18^{55}$
2	8	9.2	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}13^{36}...14^{20}$ $\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}16^{47}-17^{06}$ $19^{45}-20^{10}$ $\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{1-0}-24$; $= 20^{10}-24$
3	9	2.5	8	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}0^{00-35}$ $2^{20}-3^{30}$ $16^{50}-17^{05}$ $17^{45}-18^{15}$; $= 0^{00-30}$
4	8	0.0	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}3^{48}...4^{10}-5^{55}$ $\bullet^{\circ}...6^{20}$ $\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}11^{37-48}$; $\triangle^{\circ}20-24$
5	7	0.5	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}11^{47}-13^{01}$; $13^{50}-14^{13}$, $15^{34}-16^{07}$; $19^{35}...23^{20}$; $\sqcup^{\circ}0^{00}-6$
6	8	•	•	$= 5^{30}-7^{40}$; $\triangle^{0-1}19-24$
7	7	0.4	•	$\bullet^{\circ}13^{50}...14^{55}$; $21^{42}-22^{10}$; $\triangle^{2}0^{00}-1$ $\sqcup^{0-1}-4$
8	7	3.4	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}$ R $12^{40}-13^{02}$ WSW-ENE; $\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{2}15^{01-16}\bullet^{\circ}20^{35}...21^{10}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-2}-23^{20}$
9	8	10.3	•	
10	6	3.1	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}1^{09-16}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}'$ R$^{\circ}$- 2^{10} W $\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-1}$- 9^{20} $\bullet^{\circ}9^{48}-10^{15}...16^{10}$ 19^{18-35}
11	8	5.1	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}5^{32}-6^{04}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-1}6^{14}-7^{15}$; $10^{20}-11^{05}$; $11^{35}-14^{30}\bullet^{\circ}-16^{10}$; $= 6^{30}-7^{30}$
12	9	0.6	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}16^{25}-17^{35}\bullet^{\circ}19^{05}...20^{20}$
13	8	11.4	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-2}11^{07}-13^{23}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}13^{45-56}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-1}17^{06}...22^{40}\bullet^{\circ}23^{30}-24$
14	9	10.9	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}0^{00}...6^{25}$ $9^{42}-10^{05}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-2}10^{43}-11^{41}$; $13^{41}-15^{48}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-1}18^{20}-21^{13}$; R$'13^{46}-14^{45}$ SW-E; $\gg a,p$; $= na$; $\frown 6^{34-39}\frown^{\circ}7^{00-08}$
15	7	2.4	•	$\bullet^{\circ}17^{35}...20^{15}-22^{40}...24$
16	6	3.0	•	$\bullet^{\circ}0^{00}...2^{30}$; $4^{18}-7^{05}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}9^{33}...12^{45}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{2-0}-14^{20}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}-16^{37-42}$
17	9	0.3	•	$\bullet^{\circ}17^{36}...18^{06}$
18	9	0.7	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}1^{35}-3^{00}$; $5^{50}-8^{15}$; 12^{35-44}; $\triangle^{\circ}20-24$
19	9	0.0	•	$\triangle^{0-1}0^{00}-3$ $\gg 21^{15}-24$
20	6	38.3	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}1^{22-28}$ 3^{05-15} 8^{26-35}; $10^{52}-13^{30}\bullet^{0-2}$-24; $\gg 0^{00}-2^{15}$ $\nearrow -3^{30}$
21	6	14.2	•	$\bullet^{\circ}0^{00}-2^{55}$; $3^{05}-14^{28}\bullet'-15^{22}\bullet^{\circ}-23^{20}$; $= 0^{00}-19^{15}$
22	9	0.0	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}15^{42}-15^{50}$
23	9	•	•	$\triangle^{\circ}2-8$, $21-24$
24	6	19.6	•	$\bullet^{\circ}7^{41}...10^{20}$ $\bullet^{\circ}11^{25}-12^{10}\bullet'-12^{40}\bullet^{\circ}-18^{35}$; $= 10^{30}-24$; $\triangle^{\circ}0-5$
25	6	11.4	•	$\bullet^{\circ}3^{30}-4^{05}\bullet^{0-1}-11^{14}\bullet^{\circ}...11^{35}$; $13^{45}-15^{06}\bullet^{0-1}16^{40}-18^{55}\bullet^{\circ}19^{02}...20^{35}$; $= 0^{00}-24$
26	8	5.4	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}4^{15}...8^{10}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{2-0}13^{48}-14^{17}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0}14^{41-52}$ $16^{49}-17^{03}\bullet^{\circ}21^{40}...22^{07}-23^{49}$; $= 0^{00}-4^{40}$; $18^{15}-24$
27	6	0.3	•	$\bullet^{\circ}3^{23}-7^{05}...7^{25}$; $8^{05}-9^{12}$; $13^{57}...14^{40}$; $= 0^{00}-7^{30}$; $20^{30}-24$
28	9	0.4	•	$\bullet^{\circ}10^{10-25}$; $10^{30}-13^{30}$; $= 0^{00}-6^{02}$ $\equiv^{\circ}-6^{45} = -8^{50}$
29	6	3.3	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}4^{00-15}$ 9^{15-24}; 18^{11-55}; $= 7^{20}-14^{30}$
30	6	2.0	•	$\bullet^{\circ}4^{25}...5^{15}\bullet'-6^{20}\bullet^{\circ}7^{40}...8^{15}-9^{35}$ $\bullet^{1-0}-11^{10}$ $\bullet^{0-2}13^{32}-14^{45}$; $= 4^{30}-15^{30}$
31	8	8.9	•	$\triangle^{\circ}0^{00}-2$ $\sqcup^{\circ}-6$
Σ	—	171.0	—	UWAGI.

Czerwiec - Juin

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	POGODA
1	6	30.6	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}'4^{18}-5^{10}\bullet^{0-1}19^{48}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-1}20^{43}-22^{02}...24$; R$'20^{53}-22^{03}$ NW-NE; $= 6^{20}-12^{50}$
2	7	6.6	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-1}0^{00}-1^{19}\blacktriangle^{2}-1^{20}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-2}-4^{15}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}6^{50}-7^{30}$ $\bullet^{\circ}8^{00}-10^{15}...10^{35}-11^{15}\bullet^{\circ}15^{11-25}$; R$'1^{10}-2^{05}$ W-SW R$2^{47}-3^{10}$ SW; $\gg 0^{40}-2^{45}$; $= na-a$
3	7	12.9	•	$\bullet^{0-1}2^{15}-6^{40}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}-9^{15}\bullet^{\circ}-10^{30}...16^{35}$; $17^{33}-22^{12}\bullet^{\circ}22^{40}-23^{35}...24$; $= 2^{30}-11^{15}$, np
4	5	38.5	1	$\bullet^{\circ}0^{00}...0^{15}-3^{35}$; $4^{05}-6^{20}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-1}$; $\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-1}-14^{35}\bullet^{\circ}17^{02-11}\blacktriangle'-17^{15}\bullet^{0-1}-21^{12}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}'$; $\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}'-24$; $= na-p$, np
5	6	42.8	3	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-1}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}0^{00}-24$; $= 0^{00}-24$
6	5	8.7	pł.	$\bullet\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-1}0^{00}-5^{33}$; $6^{25}...7^{01}-8^{15}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-1}...8^{35}-10^{02}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}-10^{15}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}-11^{40}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-1}-12^{50}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}...24$; $= 0^{00}-p$
7	6	10.2	3	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}0^{00}-7^{40}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}-8^{15}$; $8^{38}-12^{15}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}-14^{40}$ $\bullet^{\circ}15^{35}-16^{39}\blacktriangle^{\circ}-17^{12}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}-24$; $= 4^{15}-24$
8	8	•	pł.	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-1}0^{00}-3^{40}$; $= 0^{00}-3^{40}$
9	8	0.0	•	$\sqcup^{\circ}0^{00}-6$
10	8	0.5	•	$\bullet^{\circ}6^{45}...7^{10}\bullet^{\circ}10^{33}...11^{40}$; 12^{22-28}
11	7	32.4	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-2}13^{13}-14^{45}$; $16^{48}-17^{05}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{2-0}20^{48}-23^{25}$; R$^{\circ}13^{13}-14^{47}$ W-SE (R)$^{\circ}15^{35-50}$ N R$^{\circ}21^{06-45}$ W-SE
12	8	6.8	•	$\bullet^{\circ}1^{22}...43$ $\bullet^{0-2}3^{05}-11^{43}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}12^{02}...19^{05}$; $= 4^{30}-11^{40}$
13	8	•	•	$\triangle^{\circ}22^{00}-24$
14	8	•	•	$\triangle^{1-2}0^{00}-3^{00}\sqcup^{\circ}-5$ $\triangle^{\circ}21-24$
15	8	0.0	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}16^{46-52}$; $\triangle'0^{00}-9$ $\triangle^{0-1}19-24$
16	8	3.2	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-2}14^{14-42}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}16^{44}-17^{08}$; R$'14^{35}-15^{45}$ S-E R$^{\circ}16^{39}-17^{43}$ N-E; $\triangle^{1-2}0-8$
17	7	6.1	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-2}8^{07-35}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-1}9^{55}...17^{05}\bullet^{\circ}22^{43}...23^{10}$; (R)' 7^{25} - R' 8^{07-51} W-SE (R)' S 10^{10} - R$^{\circ}11^{03}-13^{15}$ - (R)$^{\circ}14^{25}$ SW; $= na-a$
18	8	0.0	•	$\bullet^{\circ}4^{13}...5^{38}$; $6^{15}-7^{01}\bullet'-7^{04}\bullet^{\circ}...8^{27}$; $= 3^{30}-10^{30}$; $\triangle'$ np
19	8	•	•	$\triangle^{1-2}0^{00}-9$ $\triangle^{\circ}21-24$; $\omega^{\circ}na$
20	8	8.4	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}11^{15}-12^{38}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-2}15^{02}-16^{18}$; R$^{\circ}10^{42}$ - R$^{\circ}11^{15}-12^{35}$ SW-SE (R)' 14^{20} - R' $15^{02}-16^{15}$ W-NE; $= np$; $\triangle^{0-1}0^{00}-9$; $\omega^{\circ}na$
21	7	2.6	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}11^{13}-12^{45}\bullet^{\circ}13^{10}...14^{35}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{0-1}-15^{58}$; $17^{46}-18^{37}$; $= 0^{00}-a,p$.
22	7	•	•	$\triangle^{0-1}np$
23	8	•	•	$\triangle^{1-2}0^{00}-10$ $\triangle'22-24$
24	9	•	•	(R)$^{\circ}13^{38}-15^{02}$ N; $\triangle'0^{00}-10$, $21-24$
25	7	0.0	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}14^{49-53}$; 16^{08-16}; $\triangle'0^{00}-9$
26	8	•	•	$\triangle^{\circ}4-7$
27	9	0.7	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{1-0}10^{01-27}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}18^{29-31}$ 18^{43-55}; $\triangle'2-10$
28	8	3.4	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}9^{12-17}$; 11^{03-08} 12^{25-29}; 15^{19-23}; $16^{49}-17^{02}$; $20^{53}-21^{20}$; $23^{06}-24$
29	9	•	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}0^{00-23}\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{1-0}2^{03}-3^{40}$
30	8	0.9	•	$\overset{\bullet}{\bar{\bar{\bar{\bullet}}}}{}^{\circ}18^{06-14}\bullet^{\circ}19^{07}-20^{45}$; $21^{35}-22^{10}\bullet^{\circ}-24$; $\triangle^{\circ}2-8$
31				
Σ	—	215.3	—	UWAGI.

Zakopane φ = 49°18' λ = 19°57' Lipiec – Juillet 1962

DNI	CIŚNIENIE P – 800 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	121.0	121.1	121.8	121.3	7.6	12.0	8.5	9.2	13.8	6.1	90	68	95	84	1.1	4.4	0.8	2.1	9	9	10	SE 2	NE 2	C 0
2	119.9	119.1	118.1	119.0	7.9	10.4	7.9	8.5	12.0	5.3	73	71	79	74	2.8	3.7	2.2	2.9	8⊙	10●	10	SE 5	NW 5	W 1
3	112.2	111.0	109.7	111.0	8.8	10.4	8.1	8.8	12.3	5.7	82	67	83	77	2.0	4.2	1.9	2.7	9	10●	9	W 2	WSW 4	W 4
4	108.0	108.8	111.0	109.3	7.6	11.6	6.9	8.2	13.9	5.8	72	50	65	62	2.9	6.8	3.4	4.4	3⊙	4⊙	8	WNW 4	W 5	SW 4
5	112.2	113.2	116.2	113.9	8.2	11.7	7.3	8.6	13.0	0.9	63	60	93	72	4.1	5.5	0.7	3.4	8⊙	10	10●	E 1	W 2	C 0
6	119.7	120.6	121.9	120.7	8.2	14.3	9.2	10.2	14.9	2.5	74	51	89	71	2.9	7.9	1.3	4.0	1⊙	9	7	SW 2	ENE 1	SW 1
7	121.5	121.0	122.2	121.6	10.0	13.7	9.8	10.8	13.6	4.3	79	67	73	73	2.6	5.2	3.3	3.7	9	10	10	SW 1	NW 3	C 0
8	123.0	124.2	125.0	124.1	7.8	11.1	7.3	8.4	13.1	5.2	79	66	89	78	2.3	4.6	1.1	2.7	7⊙	9	9	SE 3	W 3	C 0
9	125.2	124.8	123.7	124.6	9.7	14.9	10.5	11.4	16.7	5.7	81	45	77	68	2.2	9.2	2.9	4.8	7	5⊙	8	C 0	NE 3	SW 2
10	121.7	121.2	120.3	121.1	11.6	17.3	12.5	13.5	18.4	4.9	73	52	78	68	3.6	9.6	3.3	5.5	1⊙	8⊙	9●	NE 1	WNW 5	C 0
11	119.2	118.3	117.5	118.3	15.6	22.1	15.0	16.9	22.5	7.1	61	48	92	67	6.9	13.8	1.4	7.4	8⊙	8⊙	8	C 0	WNW 3	C 0
12	116.8	116.8	116.0	116.5	15.1	16.1	13.3	14.4	20.5	10.9	79	71	69	73	3.8	5.2	4.8	4.6	10	8	8	SE 1	NW 3	SE 2
13	115.0	115.0	116.3	115.4	12.3	14.5	9.9	11.7	16.4	9.5	84	59	82	73	2.3	6.8	2.3	3.8	8	9	4	SE 2	W 6	SE 1
14	115.8	115.5	115.2	115.5	11.2	13.1	11.7	11.9	13.7	6.0	74	62	70	69	3.5	5.8	4.0	4.4	9	9	10	NE 1	W 4	C 0
15	114.1	113.2	112.9	113.4	10.9	15.2	13.3	13.2	17.7	10.7	87	74	77	79	1.7	4.5	3.6	3.3	10	10●	9	SW 1	ESE 1	C 0
16	113.5	113.6	115.6	114.2	13.0	17.9	11.9	13.7	19.8	8.6	72	56	91	73	4.2	9.0	1.2	4.8	7	5⊙	7	E 2	W 2	ESE 1
17	116.1	117.3	118.3	117.2	13.4	11.9	12.2	12.4	17.6	7.1	77	91	91	86	3.6	1.2	1.3	2.0	7⊙	9●K	4	C 0	SE 2	C 0
18	117.4	117.6	118.5	117.8	11.9	11.3	11.3	11.4	12.3	9.8	94	95	94	94	0.8	0.7	0.9	0.8	10●	10●	10●	C 0	C 0	NNE 2
19	118.6	119.9	122.1	120.2	10.9	12.1	12.5	12.0	12.6	9.8	94	92	93	93	0.8	1.1	1.1	1.0	10●	10●	10●	ENE 2	N 1	C 0
20	123.7	123.9	124.6	124.1	14.5	19.1	13.0	14.9	20.1	11.1	86	56	86	76	2.4	9.7	2.2	4.8	7⊙	8⊙	1	E 1	NE 1	C 0
21	124.7	122.6	122.9	123.4	13.3	22.5	15.0	16.4	23.6	6.6	76	50	82	69	3.7	13.6	3.2	6.8	0⊙	3⊙	0	C 0	ENE 2	C 0
22	123.7	123.3	123.0	123.3	16.5	23.2	15.3	17.6	24.4	9.2	75	50	96	74	4.8	14.0	0.8	6.5	1⊙	6⊙	9	C 0	SW 1	C 0
23	124.3	125.1	126.6	125.4	14.7	18.3	15.4	16.0	20.1	13.9	94	75	88	86	1.0	5.2	2.2	2.8	10●	9	10	C 0	NE 1	SW 2
24	128.3	128.6	129.2	128.7	14.5	16.4	11.7	13.6	17.3	11.5	72	59	83	71	4.6	7.5	2.4	4.8	10	9	6	C 0	ENE 1	WSW 1
25	129.1	128.4	127.8	128.4	12.0	19.9	12.7	14.3	21.6	4.7	75	43	81	66	3.5	13.3	2.8	6.5	0⊙	1⊙	0	C 0	NE 3	C 0
26	126.9	125.5	125.4	125.9	15.4	25.3	16.5	18.4	26.8	7.8	77	48	80	68	4.2	16.6	4.0	8.3	0⊙	1⊙	3	C 0	ENE 3	S 1
27	124.6	123.4	123.6	123.9	17.6	25.8	18.5	20.1	26.4	10.9	69	52	76	66	6.2	15.8	5.1	9.0	8	7⊙	10	C 0	ENE 1	SW 1
28	124.0	124.5	124.4	124.3	13.3	15.1	9.5	11.8	18.5	9.3	86	63	85	78	2.2	6.4	1.8	3.5	10	9	5	NE 2	NW 2	SE 1
29	124.3	123.6	124.7	124.2	10.6	15.0	9.1	11.0	15.8	5.6	80	49	78	69	2.7	8.7	2.6	4.7	6⊙	9⊙	0	ENE 2	NE 3	C 0
30	124.6	124.4	124.5	124.5	9.5	14.8	11.7	11.9	15.8	2.8	71	46	83	67	3.5	9.1	2.4	5.0	8⊙	10	10	C 0	ENE 3	C 0
31	125.4	125.4	126.3	125.7	9.8	16.5	9.0	11.1	18.2	5.4	85	50	82	72	1.8	9.4	2.1	4.4	7⊙	6⊙	1	SW 1	NE 3	ENE 1
M	120.5	120.4	120.5	120.5	11.7	15.9	11.5	12.6	17.6	7.2	79	61	83	74	3.1	7.7	2.4	4.4	6.7	7.7	6.9	1.1	2.5	0.8

Sierpień – Août

1	125.5	124.5	124.3	124.8	14.2	19.5	14.9	15.9	20.6	7.1	63	44	74	60	5.9	12.7	4.4	7.7	1⊙	8⊙	4	SE 1	WNW 8	C 0
2	123.5	123.0	122.3	122.9	13.3	21.0	13.7	15.4	22.4	9.2	82	41	72	65	2.9	14.8	4.4	7.4	4⊙	5⊙	0	C 0	N 3	WSW 1
3	120.9	120.8	122.1	121.3	15.4	20.6	15.3	16.8	22.3	9.4	81	68	95	81	3.4	7.6	0.9	4.0	9	9	7	C 0	C 0	C 0
4	122.4	122.7	123.2	122.8	15.3	25.0	16.5	18.3	25.7	10.4	88	47	80	72	2.2	16.7	4.0	7.6	0⊙	3⊙	2	C 0	W 3	C 0
5	121.9	118.9	117.8	119.5	16.4	25.2	14.5	17.6	25.5	11.2	85	50	97	77	2.7	14.8	0.6	6.0	3⊙	6⊙	10	C 0	ENE 3	C 0
6	118.9	119.2	119.9	119.3	17.1	23.5	14.6	17.4	24.1	11.2	80	45	83	69	4.0	15.9	2.8	7.6	3⊙	4⊙	0	C 0	NW 5	C 0
7	116.2	114.0	116.5	115.6	22.4	26.0	20.5	22.4	26.3	10.7	43	30	76	50	15.5	23.6	5.9	15.0	1⊙	1⊙	8	S 7	S 9	SSW 3
8	122.6	122.9	123.2	123.6	11.7	19.9	15.9	15.8	21.2	10.8	88	55	69	71	1.7	10.3	5.6	5.9	10	4⊙	10	SW 1	ENE 2	C 0
9	127.4	127.4	128.2	127.7	13.4	17.9	14.4	15.0	18.6	12.6	82	54	73	70	2.9	9.3	4.4	5.5	10	8	8	C 0	NE 2	C 0
10	126.7	125.0	124.1	125.3	11.6	19.9	13.0	14.4	21.0	7.0	84	56	87	76	2.2	10.1	2.0	4.8	7⊙	6⊙	2	C 0	NE 2	SW 1
11	124.4	123.6	124.6	124.2	14.9	22.1	14.5	16.5	22.5	9.1	68	45	75	63	5.3	14.8	4.2	8.1	0⊙	7⊙	2	C 0	N 3	SE 2
12	125.1	125.0	125.5	125.2	15.2	22.2	15.0	16.4	24.6	8.6	87	55	81	74	2.0	12.1	3.3	5.8	4⊙	7⊙	6	C 0	NE 2	C 0
13	125.8	125.3	125.4	125.6	14.9	24.2	15.7	17.6	25.4	10.4	78	46	83	69	3.7	16.2	3.1	7.7	8⊙	9	3	C 0	SW 2	C 0
14	124.7	124.6	122.9	124.1	15.8	22.6	15.8	17.5	25.0	11.2	83	68	84	78	3.1	8.9	2.9	5.0	0⊙	5⊙	8	C 0	NE 1	C 0
15	121.5	119.5	117.3	119.4	15.0	27.6	24.1	22.7	28.3	11.4	90	43	40	58	1.7	21.4	18.0	13.7	10⊙	9⊙	6	C 0	S 3	S 3
16	118.4	119.3	120.9	119.6	14.5	14.7	13.3	14.0	24.1	13.2	97	91	93	94	0.6	1.3	1.2	1.1	10●K	10	1	C 0	C 0	S 2
17	121.0	120.4	118.6	120.0	12.9	20.3	13.3	15.0	21.1	8.8	90	59	87	79	1.3	9.7	2.0	4.4	8⊙	9	8	C 0	NE 2	C 0
18	117.7	118.4	121.9	119.3	13.7	18.9	11.3	13.8	20.9	11.2	87	56	91	78	2.1	9.4	1.2	4.2	9⊙	7⊙	10●	C 0	NW 3	C 0
19	121.8	121.3	122.2	121.8	10.9	12.3	8.3	10.0	13.7	6.6	70	55	93	73	3.9	6.4	0.8	3.7	4⊙	10	10●	NW 4	NW 6	NW 2
20	121.0	122.3	121.6	121.6	9.1	11.2	10.2	10.2	11.6	8.3	89	81	93	88	1.3	2.5	0.8	1.3	10●	9●	10●	W 3	NW 4	SE 1
21	120.6	120.2	120.3	120.4	9.1	13.3	10.4	11.3	16.2	7.7	93	66	93	84	0.8	6.0	0.8	2.5	10	9	4	C 0	NE 2	C 0
22	121.1	122.3	123.4	122.3	12.5	13.3	10.3	11.6	15.5	8.2	84	88	93	89	2.3	1.9	0.6	1.6	6	10	6	C 0	SW 1	C 0
23	123.4	124.3	124.9	124.2	11.3	17.2	11.3	12.8	17.9	7.3	72	44	71	62	3.9	11.0	4.0	6.3	9⊙	5⊙	10	C 0	WNW 5	C 0
24	122.8	121.0	118.9	120.9	13.5	19.3	20.3	19.0	21.7	10.4	62	39	38	46	6.7	13.9	15.0	11.9	9	9	0	SW 3	SW 6	SW 8
25	120.4	121.3	124.3	122.1	17.6	19.1	12.3	13.3	20.9	12.3	64	55	76	65	7.2	9.9	3.4	6.8	9	9	9	SW 4	W 6	SW 3
26	127.1	127.0	125.8	126.6	10.4	17.8	8.3	11.2	19.1	5.4	70	46	85	67	3.8	10.9	1.6	5.4	1⊙	3⊙	3	SW 2	NW 3	C 0
27	123.3	121.1	121.9	122.1	8.5	24.4	17.4	16.9	25.1	4.7	89	38	58	62	1.3	18.9	8.5	9.6	1⊙	1⊙	7	C 0	SW 3	SW 1
28	125.4	126.0	126.4	125.9	12.6	17.3	9.4	12.2	20.1	8.9	74	37	73	62	3.8	12.6	3.0	6.3	3⊙	8⊙	0	W 1	WSW 6	C 0
29	124.9	123.9	123.4	124.1	10.0	20.1	16.3	15.8	21.4	5.1	78	44	60	61	2.8	13.2	7.3	7.8	1⊙	1⊙	8	C 0	WSW 3	W 3
30	125.1	126.2	126.2	125.8	10.1	13.3	6.9	9.4	16.3	6.8	82	52	86	73	2.3	7.3	1.3	3.7	10	7⊙	3	SW 1	NW 3	C 0
31	122.3	120.6	121.7	121.6	5.8	16.9	9.7	10.3	17.4	2.2	71	41	70	61	2.7	11.4	3.7	5.9	3⊙	4⊙	8	C 0	WSW 6	NNE 3
M	122.7	122.4	122.6	122.6	13.2	19.7	13.8	15.1	21.2	8.9	79	53	78	70	3.4	11.5	3.9	6.3	3.6	6.3	3.6	0.9	3.3	1.2

Zakopane $H_s = 844\,m$ $H_b = 838{,}2\,m$ $h_w = 17{,}7\,m$ Liniec - Juillet 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	POGODA
1	8	7.0	•	•°0^00-32 ⚲°-2 15^25-40 ⚲°16^37-17^00 ⚲°-2 18^49-20^20 ⚲°22^01-23^17, = na-a,p-24
2	7	1.[illegible]	•	⚲°12^27 13^37 ▲°-13^39 ⚲°-2-14^20 ⚲°-1 15^34-16^05, = na
3	8	2.4	•	⚲°1^35-2^20 •°5^15 6^20 ⚲°-1 8^35 18^10 •°22^46 23^22
4	9	0.0	•	•°6^47 7^10
5	8	5.1	•	•°15^48 16^17 •°-1 16^41-20^04 •°20^25-22^15, ⌓°0^00-4 ⌣'-6
6	8	1.1	•	⚲°14^18-25 ⚲°-1 15^19-46 18^40-19^03 19^18-20
7	8	2.6	•	⚲°8^25...36 9^18-12^10, 17^10-25 ⚲°-2 22^25-23^18
8	8	3.7	•	⚲°8^33-47 ⚲°-1 10^04 20^48
9	9	•	•	⌓² na-a
10	8	0.2	•	⚲°11^05-17 14^52 15^44, 21^30 22^06, = 20^15-22^10, ⌓-2 0^00-8
11	8	3.6	•	⚲°15^52-21 ⚲°-1 16^01 17^46 19^42-20^15 ⚟°17^00-45 SW-S ⌓° na-a
12	8	5.4	•	⚲'13^21-26 ⚲°-13^33, ⌓° na, ⊗°21^00-23^00
13	8	3.5	•	⚲°-1 0^34 4^41 ⚲°15^10-20 ⚲°-2 15^58-16^28, ⚟°0^32-1^00 W-SW (⚟)°-2^15 WSW-SSW ⚟°-1-3^30 SSW
14	8	0.0	•	⚲°11^46 13^03, 15^43-16^11, 17^03-10
15	8	2.5	•	⚲6^10-15 •°-1 7^10 8^10-9^02 ⚲°-1-9^11 •°-9^19, 12^02-20 ⚲°-1-0 14^25
16	9	0.1	•	⚲°16^28-40, ⌓° 2^00-8 ⌓°-1 20-24
17	7	10.8	•	⚲°-2 12^14-13^46 ⚲°19^17-22, ⚟'12^24-45 ⚟°-1-14^15 W-S-E, = 12^45-13^30, ⌓°-2 0^00-9, ⊕°na-a,p
18	6	108.2	•	•°4^40 5^15-8^48 ⚲°-2-14^35 •'-24, = na,p-24
19	6	45.7	•	•°-1 0^00-20^40 •°-2 21^10-24, = 0^00-24
20	8	•	•	•°0^00-03 = na
21	8	•	•	⌓² na ⌓°-1 20^30-24
22	8	31.3	•	⚲°-2 18^05-19^50 ⚲°20^20-28, 21^08-29, ⚟'18^25-20^05
23	8	1.4	•	⚲°-2 0^25-4^40 •°4^55-5^40 •°6^21-7^25 •°-7^50 ⚲°14^03-07, 20^18-40, ⚟'0^50-2^15 SW-NE (⚟)°-2^30 NE-NW, = na,a
24	8	•	•	⌓° 20-24
25	8	•	•	⌓-2 0^00-8, 19-24
26	9	•	•	⌓² 0^00-9
27	9	0.0	•	•°8^39-42 ⚲°22^20...46, ⌓² na-9 ⌓° np
28	8	•	•	⚲°6^51-7^05, = 7^30-8^30, ⌓° 0^00-6^30, 20-24
29	8	•	•	⌓-2 0^00-9, ⊕°a..p
30	9	•	•	⌓² na-9
31	9	•	•	⌓°-1 1^00-9 ⌓-2 19-24
Σ	—	336.5	—	UWAGI

Sierpień - Août

1	8	0.0	•	⚲°16^26-29, ⌓² 0^00-9^00
2	8	•	•	⌓² 0^00-10 ⌓°-1 21^00-24
3	7	0.5	•	⚲°14^17 15^50 ⚲°18^05-45, ⚟°18^20-19^30 S-SE, = np, ⌓°-2 0^00-8^00
4	9	•	•	= 0^00-2^15, ⌓' na-8, 21-24
5	8	7.4	•	⚲°15^24-16^02 ⚲°-2 18^50-20^05, (⚟)°15^10-45 E-SE ⚟'18^31-40 NW-W ⚟°-21^30 SW-E, ⌓-2 0^00-8; ∩'19^55-20^10
6	9	•	•	⌓² na-9 ⌓° np
7	9	1.6	•	⌓°-1 0^00-7^00, ⚲ na,a,p
8	9	•	•	•°1^10-2^20 •°-4^30 •-5^05 •°22^56-59
9	8	•	•	⌓° 22-24
10	8	•	•	⌓°-2 0^00-8^00
11	9	•	•	⌓-2 2-9 ⌓° np
12	9	•	•	⌓°-2 0^00-8 ⌓° 21-24; ⊕°a,p
13	9	•	•	⌓°-1 0^00-9, 21-24
14	7	4.0	•	⚲°-2 17^30-55, (⚟)°17^17-⚟'17^30-55 (⚟)°-18^30 S-E, ⌓°-2 0^00-8^00
15	8	15.7	•	⚲°1^18-3^25, 23^20-26, ⚟°1^43-3^00 NW-W ⚟°23^23-26 (⚟)°-24 W-SE
16	8	9.7	•	⚲'0^35-38 ⚲°-2 2^45 13^35, (⚟)° 0^00-⚟°0^35-38 (⚟)°-2^15 W-E ⚟°2^30-4^30 6^40-9^40 W-E, ⌣-2 20-24
17	8	•	•	⌓-2 0^00-10
18	8	3.7	•	⚲°12^54-13^02, 15^10-21 ⚲°-2 16^22-18^10 ⚲°20^20-22^03, ⌓°-2 0^00-9
19	9	2.4	•	⚲°15^42-45, 18^21-30, 20^10...23^10
20	7	0.8	•	⚲°0^20-42 •°-1 1^15 3^40 •°6^04 9^05 •°13^36...15^35 •°-17^10 •°18^07-20^45, 21^20-22^25
21	7	•	•	•°0^10-35 •°1^10-3^45, ⌓' np
22	8	0.1	•	⚲°9^00-18, 12^24-29, 15^55-16^15 •°-17^20, = 16^30-22^30, ⌓-2 0^00-9
23	9	•	•	
24	9	0.0	•	•°8^58...9^05, 10^58-11^06, ⚲ 20^15-45, ⌓° 0^00-7
25	9	0.0	•	⚲°14^25-29, 16^31...17^12, ⌓°-1 np
26	8	•	•	⌓°-2 0^00-10^00
27	9	•	•	⌓°-2 0^00-10 ⌓° 21-24
28	9	•	•	⌓° 0^00-8, np
29	9	0.6	•	⌓-2 0^00-10
30	8	•	•	⚲°0^13-1^20, 2^22-3^20, ⌓' 21-24
31	9	1.0	•	⌓² 0^00-9
Σ	—	47.5	—	UWAGI

Zakopane φ = 49°18' λ = 19°57' Wrzesień - Septembre 1962

DNI	CIŚNIENIE P = 800 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D.v I	II	III
1	122.5	125.3	127.7	125.2	6.6	8.7	7.5	7.6	10.4	5.4	89	81	85	85	1.0	2.1	1.6	1.6	10	10 ●	10 ●	S 2	WSW 3	C 0
2	129.6	129.1	128.1	128.9	5.6	16.1	7.6	9.2	17.2	2.5	86	55	91	77	1.3	8.3	0.9	3.5	0 ⊙	4 ⊙	3	C 0	NE 1	C 0
3	126.9	125.9	125.0	125.9	6.3	20.1	9.4	11.3	21.6	2.3	85	47	88	73	1.4	12.4	1.5	5.1	0 ⊙	0 ⊙	0	C 0	ENE 2	C 0
4	122.9	121.0	118.3	120.7	8.9	23.0	15.2	14.6	24.4	5.0	85	40	75	67	1.7	16.9	3.9	7.5	1 ⊙	4 ⊙	0	C 0	WNW 1	S 1
5	113.9	115.0	116.7	115.2	20.8	22.3	11.6	16.6	23.5	11.5	44	55	89	63	13.9	12.3	1.5	9.2	1 ⊙	8 (⚿)	1	S 8	W 1	SW 2
6	116.7	116.3	115.6	116.2	9.9	18.8	18.1	16.2	19.3	7.5	84	47	60	64	2.0	11.5	8.1	7.2	9	7 ⊙	8	C 0	WSW 4	WNW 3
7	113.1	112.4	114.6	113.4	17.5	14.9	11.9	14.0	20.0	11.6	65	79	73	72	6.9	3.5	3.8	4.7	10	10 ●	9	SW 3	WSW 6	W 1
8	117.0	117.4	120.0	118.1	10.0	15.2	5.4	9.0	16.4	5.3	80	55	92	76	2.4	7.9	0.8	3.7	9	10	2	C 0	W 5	SSW 1
9	123.9	127.2	129.0	126.7	6.3	7.7	3.2	5.1	9.4	3.2	90	78	93	87	0.9	2.3	0.5	1.2	10 ●	9	2	WNW 2	NW 3	C 0
10	127.9	126.4	125.5	126.6	1.6	16.6	7.2	8.2	18.9	-0.2	93	48	88	76	0.6	9.9	1.3	3.9	1 ⊙	1 ⊙	0	C 0	NNE 1	C 0
11	124.1	122.7	125.6	124.1	7.7	21.9	13.2	14.0	23.6	2.7	78	35	93	69	2.3	17.0	1.2	6.8	3 ⊙	8 ⊙	10 ●	C 0	WNW 4	WSW 1
12	124.4	121.4	117.4	121.1	12.2	22.8	22.4	20.0	24.9	8.7	76	45	47	56	3.4	15.1	14.6	11.0	9	6 ⊙	4	C 0	SW 6	S 8
13	120.6	122.5	125.7	122.9	13.9	13.0	8.3	10.9	23.2	7.5	64	78	70	71	5.8	3.4	3.4	4.2	6	10	10	WNW 5	NW 3	N 1
14	128.2	128.4	127.7	128.1	5.2	11.8	2.8	5.6	13.4	2.7	85	53	91	76	1.3	6.4	0.7	2.8	4	2 ⊙	1	SW 2	NNW 2	C 0
15	125.6	124.3	122.1	124.0	2.2	17.0	6.0	7.8	18.1	-0.3	90	38	77	68	0.7	12.0	2.2	5.0	1 ⊙	1 ⊙	0	C 0	NE 2	C 0
16	120.4	118.3	117.1	118.6	3.0	22.1	8.2	10.4	22.4	0.9	91	37	82	70	0.7	16.7	2.0	6.5	1 ⊙	1 ⊙	0	C 0	E 2	SSE 2
17	115.3	114.1	113.3	114.2	9.1	18.0	11.7	12.6	19.4	4.4	81	57	96	78	2.3	8.8	0.5	3.9	8	10	10 ●	NE 1	SW 3	C 0
18	112.9	109.8	111.5	111.4	7.8	9.1	8.3	8.4	11.8	7.4	99	95	93	96	0.2	0.7	0.9	0.6	10 ≡	10 ●	7	C 0	C 0	W 3
19	116.2	117.9	119.8	118.0	4.9	11.5	6.8	7.5	12.3	3.9	77	54	75	69	2.0	6.3	2.5	3.6	4 ⊙	1 ⊙	10	W 2	NNE 2	C 0
20	121.8	122.2	123.1	122.4	1.4	11.4	4.7	5.6	11.9	0.5	91	48	77	72	0.7	7.0	1.9	3.2	0 ⊙	5 ⊙	2	C 0	N 3	SE 2
21	123.4	123.7	122.9	123.3	3.8	7.3	5.4	5.5	9.4	2.3	83	68	79	77	1.4	3.2	1.9	2.2	9	9	10	ENE 2	WNW 4	C 0
22	121.5	123.0	124.8	123.1	4.1	4.9	4.6	4.6	5.5	1.8	91	87	88	89	0.7	1.2	1.0	1.0	10 ●	10 ●	9	NW 3	N 1	NW 2
23	123.1	122.4	121.2	122.2	4.3	5.2	3.8	4.3	6.1	3.8	91	88	93	91	0.7	1.0	0.5	0.7	10 ●	10	10 ●	NW 1	NW 1	C 0
24	124.0	126.7	128.9	126.5	4.3	4.7	1.6	3.0	6.1	1.6	92	90	96	93	0.7	0.8	0.3	0.6	10	10 ●	0	C 0	C 0	C 0
25	130.3	130.1	129.5	130.0	-1.1	8.8	2.0	2.9	11.5	-2.5	91	77	93	87	0.4	2.6	0.6	1.2	0 ⊙	6 ⊙	0	C 0	C 0	C 0
26	127.2	125.2	124.1	125.5	0.0	14.1	3.3	5.2	14.9	-1.1	96	53	93	81	0.2	7.5	0.5	2.7	1 ⊙	3 ⊙	1	C 0	C 0	C 0
27	121.3	119.4	119.1	119.9	0.7	13.6	6.1	6.6	14.0	-1.1	94	63	92	83	0.4	5.9	0.7	2.3	7	10	9	C 0	NE 2	C 0
28	117.9	117.4	117.8	117.7	3.8	13.4	8.7	8.6	14.5	3.8	95	62	97	85	0.4	5.9	0.3	2.2	4 ⊙	8	6	C 0	C 0	C 0
29	118.4	118.8	121.8	119.7	5.5	14.6	7.7	8.9	15.1	4.1	95	59	93	82	0.4	6.9	0.7	2.7	5	8	2	C 0	C 0	C 0
30	123.9	124.1	126.1	124.7	3.2	16.1	5.3	7.5	16.2	2.5	97	52	92	80	0.3	8.9	0.7	3.3	4 ⊙	8 ⊙	0	C 0	NE 1	C 0
31																								
M	121.8	121.6	122.0	121.8	6.3	14.2	7.9	9.1	15.8	3.6	85	61	85	77	1.9	7.5	2.0	3.8	5.2	6.6	4.5	1.0	2.1	0.9

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1	127.2	127.4	128.9	127.8	5.8	17.7	6.9	8.8	17.9	2.3	95	48	92	78	0.5	8.4	0.7	3.2	0 ⊙	1 ⊙	0	C 0	NE 2	C 0
2	129.5	129.3	129.8	129.5	4.1	18.5	7.2	9.2	19.2	3.3	95	49	96	80	0.4	10.8	0.5	3.9	0 ⊙	1 ⊙	0	C 0	NE 2	C 0
3	129.3	128.9	129.4	129.2	4.8	18.8	6.8	9.3	19.1	3.9	95	53	91	80	0.4	10.1	0.9	3.8	1 ⊙	1 ⊙	0	C 0	E 1	C 0
4	128.8	128.6	127.8	128.4	5.6	18.9	8.4	10.3	18.9	4.3	90	52	93	78	0.9	10.3	0.7	4.0	0 ⊙	1 ⊙	3	C 0	SSE 1	C 0
5	126.5	126.2	127.8	126.8	8.0	17.4	10.7	11.7	17.5	6.3	91	58	94	81	0.9	8.4	0.9	3.4	9	8 ⊙	9	C 0	NNW 1	C 0
6	127.4	128.1	130.1	128.5	6.9	9.4	8.4	8.3	10.9	6.2	94	93	96	94	0.5	0.8	0.4	0.6	10	10 ●	10	C 0	C 0	C 0
7	131.5	132.8	134.4	132.9	7.7	10.3	7.2	8.1	10.5	7.2	94	72	91	86	0.6	3.5	1.0	1.7	9	10	0	C 0	C 0	C 0
8	135.4	135.5	136.2	135.7	2.5	16.6	3.5	6.5	16.9	1.6	96	30	93	73	0.3	13.2	0.5	4.7	0 ⊙	1 ⊙	0	C 0	NE 2	C 0
9	135.1	133.9	132.9	134.0	0.0	16.2	3.4	5.8	17.1	-0.6	94	46	89	76	0.4	9.9	0.8	3.7	2 ⊙	2 ⊙	0	C 0	C 0	C 0
10	130.1	127.8	127.1	128.3	0.9	17.5	4.9	7.0	17.6	0.1	90	36	82	69	0.6	12.8	1.6	5.0	0 ⊙	1 ⊙	0	C 0	NE 2	C 0
11	125.5	124.0	122.3	123.9	2.1	17.3	4.8	7.2	17.6	1.3	86	41	88	72	0.9	11.7	1.0	4.5	1	0 ⊙	0	C 0	NE 1	C 0
12	121.1	121.1	122.8	121.7	0.7	15.2	3.9	5.9	15.7	0.3	90	52	92	78	0.6	8.4	0.7	3.2	0 ⊙	1 ⊙	1	C 0	NE 2	C 0
13	123.8	123.1	122.1	123.0	0.5	14.7	4.3	6.0	14.8	0.0	98	61	92	84	0.1	6.6	0.7	2.5	2 ⊙	1 ⊙	1	C 0	NE 1	SW 2
14	117.1	117.1	120.7	118.3	5.7	11.9	5.4	7.1	12.8	1.5	83	70	92	82	1.6	4.1	0.8	2.2	9	9	10	C 0	WSW 3	SW 3
15	123.3	125.5	128.3	125.7	3.1	6.4	3.1	3.9	6.4	2.8	89	80	89	86	0.8	1.9	0.8	1.2	10	10	10	C 0	C 0	WNW 1
16	126.9	125.2	125.7	125.9	-1.5	6.9	2.7	2.7	7.4	-2.1	100	76	91	89	0.0	2.3	0.6	1.0	10 ≡	10	4	C 0	W 1	C 0
17	127.3	127.7	128.7	127.9	-2.3	10.1	1.9	2.9	11.3	-2.9	89	59	88	79	0.6	5.1	1.8	2.5	0	4 ⊙	0	C 0	NE 2	C 0
18	126.9	126.1	122.6	125.2	2.0	9.4	1.7	3.7	10.8	0.5	86	72	92	83	1.0	3.3	0.5	1.6	3	5	1	C 0	N 2	C 0
19	118.1	118.8	120.3	119.1	7.8	8.7	6.1	7.2	9.7	1.4	73	78	84	78	2.9	2.4	1.5	2.3	8	10	8	SW 2	WSW 3	NW 2
20	121.1	124.1	128.3	124.5	4.1	4.5	4.6	4.4	6.1	3.9	89	88	83	87	0.9	1.0	1.4	1.1	10	10 ●	10	SW 1	C 0	C 0
21	131.7	132.2	132.8	132.2	-0.2	7.1	-0.5	1.5	8.4	-0.7	94	58	92	81	0.4	4.2	0.5	1.7	1	1 ⊙	0	C 0	N 2	C 0
22	132.2	131.1	131.1	131.5	-2.3	11.1	0.7	2.6	12.0	-2.5	91	57	92	80	0.5	5.8	0.5	2.3	0	0 ⊙	0	C 0	C 0	C 0
23	129.4	128.4	127.5	128.4	-2.0	13.5	1.3	3.5	13.5	-2.7	91	43	87	74	0.5	8.8	0.9	3.4	0	0 ⊙	0	C 0	NE 1	C 0
24	125.9	124.8	125.7	125.5	-2.1	12.6	0.2	2.7	12.7	-2.6	98	47	96	80	0.1	7.7	0.3	2.7	0	0 ⊙	0	C 0	C 0	C 0
25	124.6	123.5	123.7	123.9	-2.1	9.3	0.5	2.0	9.8	-2.8	94	67	94	85	0.3	3.9	0.3	1.5	0	0	0	C 0	WNW 1	C 0
26	122.8	122.1	120.9	121.9	-1.7	9.6	1.8	2.9	10.6	-2.2	96	60	90	82	0.2	4.9	0.7	1.9	0	2 ⊙	2	C 0	NE 1	C 0
27	118.4	119.0	120.7	119.4	-0.3	12.8	2.0	4.1	13.3	-1.1	86	43	91	73	0.9	8.6	0.7	3.4	0	3 ⊙	2	C 0	C 0	C 0
28	118.1	116.0	114.1	116.1	-0.2	10.9	4.1	4.7	11.0	-1.6	92	54	86	77	0.5	5.9	1.1	2.3	7	9	9	C 0	ENE 2	C 0
29	112.8	113.3	118.2	114.8	2.8	7.7	2.8	4.0	7.7	2.6	93	77	95	88	0.6	2.4	0.4	1.1	9	8	10 ●	C 0	NE 1	C 0
30	119.9	119.6	117.3	119.0	2.0	3.5	1.5	2.1	4.0	1.5	93	91	96	93	0.6	0.7	0.3	0.5	10 ≡	10	10 ≡	C 0	C 0	C 0
31	114.2	112.8	111.9	113.0	3.3	9.2	8.1	7.2	11.0	0.7	93	75	92	87	0.5	2.9	0.8	1.4	9 ●	7 ⊙	10	C 0	NE 1	NE 3
M	125.2	125.0	125.5	125.2	2.1	12.1	4.1	5.6	12.7	1.0	91	61	91	81	0.6	6.2	0.8	2.5	3.9	4.4	3.3	0.1	1.1	0.4

Zakopane $H_s = 844\,m$ $H_b = 838{,}2\,m$ $h_w = 17{,}7\,m$ Wrzesień - Septembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	1.3	·	$\overset{*}{\bullet}{}^{0-1}6^{30}\ldots12^{30}\bullet^{\circ}13^{25}\ldots14^{12}\overset{*}{\bullet}{}^{\circ}16^{26}-17^{05};21^{40}-22^{05}$
2	9	·	·	$\triangle^{2}0^{00}-11$
3	9	·	·	$\triangle^{2}0^{00}-11\triangle^{0-1}19-24$
4	9	·	·	$\triangle^{2}0^{00}-8\triangle^{\circ}21-23;\ \gg23^{15}-24$
5	8	4.4	·	$\overset{*}{\bullet}{}^{0-1}13^{00}\ldots15^{00}\bullet^{0-2}15^{27-35}\overset{*}{\bullet}{}^{\circ}15^{45-50}\bullet^{0-0}16^{40}-17^{00};\ \mathrm{R}\,14^{08}-15^{10}\,NW-E\ \mathrm{R}^{\circ}16^{48}-17^{15}\,SW-E;\ \gg0^{00}-6$
6	9	0.9	·	$\overset{*}{\bullet}{}^{\circ}16^{01-05}16^{10}-17^{45};\ \triangle^{2}0^{00}-10^{00}$
7	7	1.9	·	$\overset{*}{\bullet}{}^{\circ}5^{35}-7^{10};13^{25}-14^{15}\bullet^{\circ}14^{40}\ldots18^{10}$
8	8	4.6	·	$\overset{*}{\bullet}{}^{0-2}17^{33}-18^{28}$
9	7	3.3	·	$\bullet^{0-1}6^{50}-7^{15}\overset{*}{\bullet}{}^{0-2}-8^{05}\bullet^{0-2}-9^{48}\bullet^{\circ}10^{15-45}\overset{*}{\bullet}{}^{\circ}11^{05-36};12^{03-40};13^{15-30}$
10	9	·	·	$\sqcup^{\circ2}0^{00}-10\triangle'21-24$
11	9	0.8	·	$\overset{*}{\bullet}{}^{\circ}15^{30}\ldots17^{20};19^{40}-21^{30}\bullet^{\circ}\ldots22^{05};=21^{30}-23^{30};\triangle^{1-2}2-5\sqcup'-7$
12	9	·	·	$\gg p,np$
13	8	0.0	·	$\overset{*}{\bullet}{}^{\circ}12^{50-55};13^{50}-14^{02}$
14	9	·	·	$\triangle^{\circ}2-8\triangle^{0-2}19-24;\cup1^{30}-3^{20}$
15	9	·	·	$\triangle^{2}0^{00}-1\sqcup'-8$
16	9	·	·	$\triangle^{2}0^{00}-1\sqcup'-8$
17	7	10.4	·	$\overset{*}{\bullet}{}^{0-1}13^{41}-16^{10};16^{25}-18^{15}\bullet^{0-1}-22^{20}\bullet\ldots24$
18	5	19.0	·	$\bullet^{\circ}0^{00}\ldots1^{10}\bullet^{2}\ldots2^{20}\bullet^{\circ}3^{20}-4^{10}\bullet^{\circ}\ldots4^{50}\bullet^{\circ}\ldots5^{15}\bullet^{\circ}6^{05}\ldots7^{10}\bullet^{0-1}9^{44}-18^{15};\equiv^{\circ}-12^{45}=-17^{30}$
19	9	·	·	
20	8	·	·	$\triangle^{\circ}0^{00}-2\sqcup^{\circ\pm}8$
21	8	2.1	·	$\overset{*}{\bullet}{}^{1-2}12^{15}\ldots13^{55};16^{05}-17^{02}$
22	6	10.2	·	$\bullet^{0-1}1^{43}\ldots6^{00}-9^{15};9^{40}-10^{40}\overset{*}{\bullet}{}^{\circ}-11^{20}\bullet^{\circ}\ldots20^{18}$
23	7	8.9	·	$\bullet^{\circ}2^{10}-3^{45}4^{30-45}7^{40}\ 13^{25};14^{45}-24$
24	6	4.6	·	$\bullet^{0-1}0^{00}\ldots4^{45}\bullet^{\circ}7^{50}-8^{20}\overset{*}{\bullet}{}^{0-1}10^{56}-11^{40};12^{22}-13^{15}\bullet^{0-1}-15^{35}\bullet^{\circ}16^{35}\ldots19^{05};=7^{30}-20^{50}$
25	7	·	·	$=8^{30}-12^{20};\triangle'19-22\sqcup'-24$
26	9	·	·	$\sqcup'0^{00}-8\triangle'19-23\sqcup'-24$
27	9	·	·	$=0^{30}-5^{40};\sqcup'0^{00}-6\triangle^{\circ}-9,20-24;\oplus12^{30}-14^{00}$
28	8	2.7	·	$\overset{*}{\bullet}{}^{2-0}17^{10}-18^{15}\bullet^{\circ}\ldots20^{30};\triangle^{\circ}0^{00}-10$
29	8	·	·	$\triangle^{0-1}20-24$
30	8	·	·	$\triangle'0^{00}-9\triangle^{0-1}20-24$
31				
Σ	—	74.1	—	UWAGI

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1	8	·	·	$\triangle^{1-2}0^{00}-5\sqcup'-6\triangle'20-24$
2	9	·	·	$\triangle^{2}na-a\triangle^{1-2}20-24$
3	7	·	·	$\triangle^{2}0^{00}-5\sqcup^{\circ}-6\triangle^{1-2}19-24$
4	9	·	·	$\triangle^{2}0^{00}-8\triangle'20-24$
5	7	·	·	$=16^{30}-24;\triangle'0^{00}-11$
6	6	5.6	·	$\bullet^{\circ}9^{45}\ldots10^{20}\bullet^{\circ}-11^{15}\bullet^{\circ}12^{10-43}\bullet^{0-1}-13^{15}\bullet^{\circ}-14^{10}\bullet^{\circ}-15^{20}\bullet^{0-1}23^{12}-24;=0^{00}-24;\triangle^{\circ}0^{00}-1$
7	8	·	·	$\bullet^{\circ}0^{00-25};=0^{00}-9^{30};\triangle'20-24$
8	9	·	·	$\triangle^{1-2}0^{00}-4\sqcup^{\circ}-7\triangle^{\circ}20^{30}-24$
9	9	·	·	$\sqcup^{\circ2}0^{00}-7\triangle^{0-1}18-24$
10	9	·	·	$\sqcup^{1-2}0^{00}-7^{30}\triangle^{0-1}19-24$
11	9	·	·	$\triangle^{1-2}0^{00}-4\sqcup'-7\triangle^{\circ}19-24;\cup23^{30}-24$
12	8	·	·	$\triangle^{\circ}0^{00}-2\sqcup^{\circ}-7^{30}\triangle^{0-1}18-24;\cup^{\circ}0^{00}-2^{15}$
13	8	·	·	$=9^{30}-10^{30};\sqcup^{\circ}0^{00}-8^{30}\triangle'20-24;\cup^{\circ}0^{00}-5$
14	8	2.3	·	$\bullet^{\circ}8^{38\ldots48};10^{07-30};11^{54}-12^{06}\bullet^{\circ}17^{07-30}\bullet^{\circ}-18^{35}\bullet^{\circ}23^{40}\ldots24;=p-24;\sqcup'0^{00}-8$
15	7	0.0	·	$\bullet^{\circ}0^{00}-1^{15}8^{45}\ldots9^{10}\overset{*}{\bullet}{}^{\circ}16^{02-15};=0^{00}-7^{40}18^{50}-24$
16	6	·	·	$=0^{00}-5^{50}\equiv^{1-2}-7^{45}=-16^{20};20^{30}-24;\sqcup^{\circ}3-8\triangle'20-24$
17	9	·	·	$=0^{00}-3^{40};\sqcup'0^{00}-9\sqcup^{\circ}22-24$
18	7	·	·	$=18^{10}-21^{15};\sqcup'0-9\sqcup^{\circ}20-24$
19	8	0.9	·	$\bullet^{\circ}13^{50}\ldots15^{15};\sqcup^{\circ}0^{00}-3$
20	7	2.3	·	$\bullet^{\circ}6^{10\ldots20}\bullet^{0-1}7^{05}\ldots8^{22}-10^{05}\bullet^{\circ}12^{25}\ldots15^{05}\bullet^{\circ}15^{28}-16^{02}\bullet^{\circ}-16^{10};=a,p\triangle^{\circ}0^{00}-6$
21	8	·	·	$\sqcup^{\circ}0^{00}-7^{30}\sqcup^{0-1}20-24$
22	9	·	·	$\sqcup^{\circ2}0^{00}-8\sqcup^{0-1}20-24$
23	9	·	·	$\sqcup^{2}0^{00}-11\sqcup^{\circ}20-24$
24	8	·	·	$\sqcup^{\circ2}0^{00}-1\sqcup^{0-1}20-24$
25	6	·	·	$=6^{20}-15^{40}20^{30}-24;\sqcup^{1-2}0^{00}-8\sqcup^{0-1}19-24$
26	7	·	·	$=na,a;\sqcup^{1-2}0^{00}-11\sqcup^{\circ}np$
27	7	·	·	$\sqcup^{1-2}0^{00}-10\sqcup^{\circ}22-24$
28	8	·	·	$=21^{15}-24;\sqcup^{0-1}0^{00}-8$
29	6	0.5	·	$\bullet^{\circ}18^{10}-24;=0^{00}-17^{45}\equiv^{\circ}-24$
30	5	0.3	·	$\bullet^{\circ}0^{00}-6^{10};\equiv^{\circ}0^{00}-9^{40}=-18^{50}\equiv^{\circ}-24$
31	8	2.7	·	$\bullet^{\circ}3^{25}\ldots6^{10}\overset{*}{\bullet}{}^{\circ}\ldots11^{00};17^{50}\ldots22^{10};\equiv^{\circ}0^{00-45}=-1^{40};na,a,p-24$
Σ	—	14.6	—	UWAGI.

Zakopane φ = 49°18' λ = 19°57' Listopad - Novembre 1962

DNI	CIŚNIENIE P = 800 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	108.6	109.0	110.9	109.5	9.3	10.9	8.8	9.4	13.0	7.8	95	93	96	95	0.6	0.9	0.4	0.6	9	10 ●	10 ●	NE 1	C 0	S 1
2	114.6	116.1	118.9	116.5	6.0	8.6	6.3	6.8	10.7	5.7	94	89	97	93	0.6	1.3	0.2	0.7	10	9 ⊙	10 ≡	C 0	E 2	C 0
3	119.6	119.3	121.2	120.0	4.0	10.5	3.9	5.6	12.0	3.9	95	77	93	88	0.4	2.9	0.6	1.3	10 ≡	6 ⊙	1	C 0	C 0	C 0
4	121.4	121.3	120.3	121.0	1.2	11.2	9.3	7.8	13.5	0.5	96	72	56	75	0.3	3.8	5.2	3.1	10 ≡	2 ⊙	1	C 0	ENE 1	SE 3
5	119.6	118.3	117.2	118.4	10.3	14.1	5.3	8.8	14.7	4.7	54	41	82	59	5.7	9.5	1.6	5.6	2	1 ⊙	2	SE 5	SE 4	SE 2
6	114.6	115.6	117.9	116.0	11.3	10.7	10.7	10.8	12.4	4.5	45	60	64	56	7.4	5.2	4.7	5.8	9	9	9	SW 4	SSE 5	S 5
7	121.5	122.9	124.9	123.1	3.8	15.0	4.7	7.0	15.2	3.8	92	58	91	80	0.7	7.1	0.7	2.8	4	4 ⊙	2	NE 1	NE 3	C 0
8	122.9	120.7	119.9	121.2	2.2	14.2	5.2	6.7	15.0	1.9	96	56	87	80	0.3	7.1	1.1	2.8	1	5 ⊙	8	C 0	NE 2	ESE 2
9	118.0	116.7	116.7	117.1	3.6	12.0	7.1	7.4	12.1	3.0	91	61	89	80	0.7	5.3	1.1	2.4	9	9 ⊙	10 ●	C 0	NE 2	C 0
10	113.2	113.2	116.2	114.2	6.3	3.8	0.0	2.5	7.1	0.0	94	92	98	95	0.5	0.7	0.1	0.4	10	10	10 △	C 0	NE 2	NE 1
11	118.0	118.2	118.2	118.1	-0.9	1.2	1.0	0.6	2.0	-1.0	93	87	96	92	0.4	1.0	0.3	0.6	10 *	10	10 ≡	NE 1	C 0	C 0
12	115.5	116.7	120.0	117.4	2.3	6.1	4.5	4.4	6.6	1.0	96	92	93	94	0.3	0.7	0.5	0.5	10 ●	10 ●	6	C 0	NNE 1	C 0
13	121.4	121.3	121.1	121.3	3.7	7.6	3.8	4.7	7.6	3.6	92	77	95	88	0.7	2.4	0.4	1.2	10	9	9 ●	C 0	NE 2	C 0
14	119.9	119.6	120.6	120.0	3.9	7.2	3.5	4.5	7.2	3.5	95	91	93	93	0.4	1.0	0.5	0.6	10 ●	10 ●	6	C 0	C 0	C 0
15	117.8	112.3	108.9	113.0	1.2	8.0	4.8	4.7	9.7	0.8	94	79	91	88	0.4	2.3	0.7	1.1	10	8 ⊙	10 ●	C 0	SW 6	C 0
16	111.0	112.2	114.8	112.7	-0.6	-1.8	-2.7	-2.0	4.8	-3.3	93	86	86	88	0.4	0.8	0.7	0.6	10	10 △	10	C 0	NE 1	C 0
17	116.9	116.0	113.5	115.5	-4.8	-1.8	-4.0	-5.6	-1.2	-6.7	91	75	75	80	0.4	1.3	1.1	0.9	10	4 ⊙	4	C 0	NE 1	SE 2
18	108.9	106.6	104.3	106.6	-2.0	5.8	3.6	2.8	6.2	-5.5	75	45	82	67	1.4	5.0	1.4	2.6	5	8	10 ●	NE 3	NE 3	S 7
19	106.9	109.8	106.4	107.7	3.6	6.6	8.5	6.8	9.2	3.3	56	43	69	56	3.5	5.5	3.5	4.2	8	10	10 ●	SW 3	SW 8	Ś 9
20	106.3	105.7	111.7	108.0	10.5	6.0	-0.8	3.7	10.8	-0.9	57	92	91	80	5.5	0.8	0.5	2.3	10	10 ●	10 *	SW 5	ENE 3	WSW 1
21	112.9	111.5	110.4	111.6	-1.8	-0.8	-1.1	-1.2	-0.6	-2.4	90	89	89	89	0.5	0.6	0.6	0.6	10	10	10	ENE 1	NE 2	C 0
22	110.0	114.2	117.8	114.0	-3.3	1.5	-0.4	-0.6	2.1	-3.4	90	73	94	86	0.5	1.8	0.3	0.9	6	8	10 △	C 0	C 0	C 0
23	121.3	121.1	122.9	121.8	-2.8	-2.8	-4.3	-3.6	-0.4	-4.4	93	88	89	90	0.4	0.6	0.5	0.5	10 *	10 *	10 △	C 0	ENE 1	NE 1
24	124.7	125.4	127.6	125.9	-4.8	-3.0	-3.8	-3.8	-2.9	-5.0	88	81	87	85	0.5	0.9	0.6	0.7	10 *	10 *	10 △	NE 1	NE 1	C 0
25	128.3	127.6	128.1	128.0	-5.3	-2.3	-2.5	-2.6	-1.6	-4.9	92	96	91	93	0.4	0.3	0.5	0.4	10	10 △ ≡	10 *	C 0	NE 1	C 0
26	129.2	129.0	130.1	129.4	-2.6	-1.5	-2.0	-2.0	-1.3	-3.2	91	94	94	93	0.5	0.3	0.4	0.4	10	10 ● △	10 *	C 0	C 0	C 0
27	130.9	130.8	129.7	130.5	-1.9	-0.2	-1.8	-1.4	-0.2	-2.2	94	84	83	87	0.3	0.9	0.9	0.7	10	10	10	C 0	C 0	C 0
28	127.2	126.4	126.6	126.7	-3.8	-3.3	-4.5	-4.0	-1.8	-5.1	89	83	91	88	0.5	0.8	0.4	0.6	10	10	10	C 0	C 0	C 0
29	126.4	126.1	124.5	125.7	-3.6	-0.5	-0.1	-1.1	1.0	-4.9	85	82	88	85	0.7	1.1	0.8	0.9	10	9	10	C 0	SW 1	SW 2
30	120.8	119.5	120.1	120.1	-4.5	1.5	-0.1	-0.8	1.9	-4.8	91	75	86	84	0.4	1.7	0.9	1.0	6	10	10 △	SW 1	WSW 1	NW 3
31																								
M	118.3	118.1	118.7	118.4	1.4	4.8	2.1	2.6	6.2	-0.3	87	77	87	84	1.2	2.5	1.0	1.6	8.6	8.4	8.3	0.9	1.8	1.3

Grudzień - Décembre

1	125.8	132.2	136.6	131.5	-2.6	-5.6	-5.1	-4.6	0.2	-5.6	87	77	83	82	0.7	0.9	0.7	0.8	10 *	5	10	NE 2	NE 3	NNE 4
2	139.7	140.7	140.9	140.4	-6.0	-4.6	-14.8	-10.0	-4.3	-15.3	87	69	82	79	0.5	1.3	0.3	0.7	8 ·	8 ⊙	0	C 0	ENE 1	C 0
3	136.9	134.8	133.0	134.9	-16.5	-3.5	-10.7	-10.4	-3.5	-17.6	80	67	80	76	0.3	1.5	0.5	0.8	0	3 ⊙	0	C 0	C 0	C 0
4	129.9	128.8	128.3	129.0	-10.1	-0.3	-5.4	-5.3	0.0	-12.1	84	61	75	73	0.4	2.4	1.0	1.3	3	1 ⊙	2	C 0	C 0	C 0
5	126.4	125.5	129.7	127.2	-2.0	-0.2	-2.6	-1.8	1.0	-9.1	64	63	81	69	1.9	2.2	1.0	1.7	8	10	10	SW 1	WSW 3	C 0
6	130.7	130.6	130.4	130.6	-2.6	-2.4	-8.7	-5.6	-1.1	-9.6	87	85	83	85	0.7	0.8	0.5	0.7	10	10	0	C 0	C 0	C 0
7	129.4	129.1	130.1	129.5	-6.4	3.4	-5.5	-5.5	4.2	-9.5	89	64	90	81	0.4	2.8	0.4	1.2	3	1 ⊙	0	ESE 1	C 0	C 0
8	131.1	131.4	131.0	131.2	-6.6	2.7	-7.0	-4.5	3.5	-8.1	88	61	85	78	0.4	2.8	0.5	1.2	0	0 ⊙	0	C 0	E 1	C 0
9	124.4	118.0	112.6	118.3	-9.1	6.9	-5.9	-3.5	7.4	-10.2	82	28	74	61	0.5	7.1	1.0	2.9	4	9 ⊙	10	S 1	SW 4	NE 1
10	109.4	109.3	109.3	109.3	0.9	-0.1	-1.6	-0.6	4.6	-6.2	70	71	73	71	2.0	1.8	1.4	1.7	10	10	9	SW 2	SW 1	W 2
11	112.0	112.0	110.1	111.4	-1.5	0.1	-5.5	-3.1	0.3	-5.6	82	79	85	82	1.0	1.4	0.6	1.0	10	9	4	W 2	NW 2	WNW 2
12	105.3	102.6	102.1	103.3	-4.3	3.2	-2.9	-1.7	3.7	-7.8	82	39	70	64	0.8	4.7	1.4	2.3	9	9	7	C 0	NE 5	NE 2
13	102.4	101.7	102.7	102.3	3.3	4.0	6.5	5.1	6.5	-3.2	56	40	53	50	3.4	4.9	4.6	4.3	8	8	9	WSW 5	S 6	S 5
14	103.8	105.8	109.1	106.2	0.4	-0.5	-3.3	-1.7	6.5	-3.3	92	96	85	91	0.5	0.3	0.7	0.5	10 *	10 *	10 △	C 0	C 0	NNE 2
15	104.3	94.8	93.5	97.5	-6.9	-1.1	-1.8	-2.9	-0.4	-8.9	72	69	77	73	1.0	1.8	1.2	1.3	6	10 *	10	SW 1	WSW 5	W 3
16	81.6	82.4	84.9	83.0	-4.1	1.5	1.0	-0.2	2.8	-5.1	91	81	82	85	0.4	1.3	1.2	1.0	10 *	9 *	10	C 0	W 4	WSW 3
17	92.6	97.5	101.4	97.2	-3.0	-3.3	-2.7	-2.9	1.0	-3.7	88	85	82	85	0.6	0.7	0.9	0.7	10 *	10 *	9 *	WNW 3	WNW 2	WSW 2
18	100.8	100.5	101.8	101.0	-3.3	-1.8	-8.6	-5.6	-1.2	-10.1	81	77	86	81	0.9	1.2	0.4	0.8	9	8	9	SW 2	WSW 4	C 0
19	102.3	104.3	108.9	105.3	-5.7	-4.2	-6.5	-5.7	-4.2	-8.5	84	79	89	84	0.6	0.9	0.4	0.6	9 *	9	10	C 0	ENE 1	WNW 1
20	114.5	117.2	120.2	117.3	-9.0	-9.0	-10.6	-9.8	-6.4	-10.6	82	67	77	75	0.5	1.0	0.6	0.7	10 *	10	10 *	W 1	C 0	ENE 1
21	117.0	114.2	115.6	115.6	-22.5	-11.3	-18.8	-17.8	-10.6	-23.2	81	66	78	75	0.2	0.9	0.3	0.5	7	8 ⊙	0	C 0	NE 1	C 0
22	119.5	123.3	127.8	123.5	-22.8	-15.5	-17.1	-18.1	-15.0	-25.5	80	77	74	77	0.2	0.4	0.4	0.3	1	10	10 △	C 0	E 1	E 2
23	130.1	131.8	132.7	131.5	-18.8	-16.4	-19.3	-18.4	-15.6	-22.2	78	66	71	72	0.3	0.6	0.4	0.4	10 △	8	0	E 1	ENE 1	C 0
24	131.8	132.3	131.9	131.7	-15.3	-11.8	-15.6	-14.6	-11.8	-20.9	72	64	77	71	0.5	0.9	0.4	0.6	10 *	8 *	10	NE 2	NE 5	C 0
25	129.0	126.2	122.0	125.7	-18.1	-8.6	-10.7	-12.0	-7.9	-19.2	73	74	83	77	0.4	0.8	0.4	0.5	8	10 *	10 *	C 0	C 0	C 0
26	116.3	113.8	112.3	114.1	-14.6	-8.9	-17.6	-14.7	-8.9	-18.4	83	70	79	77	0.3	0.9	0.3	0.5	8	10	6	C 0	C 0	C 0
27	109.0	108.0	109.8	108.9	-11.1	-8.6	-11.2	-10.5	-8.5	-18.4	83	71	79	78	0.4	0.9	0.3	0.6	10	9	10	C 0	NE 1	SW 1
28	111.2	112.9	115.1	113.1	-16.5	-8.4	-17.0	-14.7	-8.0	-18.0	75	66	80	74	0.4	1.1	0.3	0.6	8	6 ⊙	0 ←	C 0	W 2	C 0
29	112.3	109.7	108.7	110.2	-16.6	-0.2	-0.4	-4.4	2.1	-18.9	75	65	76	72	0.4	2.1	1.4	1.3	2	8 *	7	NNE 2	S 6	SSW 2
30	109.5	108.8	109.6	109.3	-8.6	-2.1	-4.0	-4.7	-0.4	-9.0	86	83	89	86	0.4	0.9	0.5	0.6	6	10	10 *	C 0	C 0	C 0
31	111.0	113.2	115.6	113.3	-7.9	-9.0	-13.7	-11.1	-5.9	-14.5	87	79	79	82	0.4	0.6	0.4	0.5	10 *	10 *	1	NE 1	NE 2	NE 1
M	116.1	115.9	116.7	116.2	-8.6	-3.7	-8.0	-7.1	-2.2	-12.2	81	69	79	76	0.7	1.7	0.8	1.1	7.3	7.9	6.2	0.9	2.0	1.1

Zakopane $H_s = 844\,m$ $H_b = 838{,}2\,m$ $h_w = 17{,}7\,m$ Listopad - Novembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	6	10.2	•	•°3^30...6^10 ⚥°7^45...9^05 ⚥°-1 9^10-12^10 •°-17^15 ⚥°-1 -21^50 •°-22^20; =0^00-5^20; a-p
2	6	•	•	=8^35-18^50 ≡°-24
3	8	•	•	≡°0^00-35 =-1^45 ≡°-3^35 =-4^45 ≡°-1 -7^02 =20^15-24; ⌓' 20-24
4	9	•	•	=0^00-30 ≡°5^50-7^45; ⌓' 0^00-2 ⌣' -7
5	9	•	•	
6	9	0.0	•	⚥°10^02-50; 15^40-16^06
7	9	•	•	⌓' 20-24
8	9	•	•	⌓' 0^00-3 ⌣°-7; ⊕°14^30-45 ⚲°18^45-24
9	8	1.4	•	•°20^02...15; 20^35-24; =9^20-10^45; ⌓° na -I
10	5	3.4	•	•°0^00...2^18 ⚥°4^12-5^12 ⚲°10^55-12^10; 13^15...14^45 •°-15^05 •°-17^30 •°-18^20 *°-20^25 ♎°-22^35; =1^30-24
11	6	2.2	1	♎°0^42-1^25 *°6^28...7^25; =0^00-15^50; p ≡°18^25-24
12	6	1.8	•	•°0^50...8^35 ⚥°...13^06; ≡°0^00-40 =-24
13	6	2.7	•	⚥°11^42...14^45 20^35...22^38 ⚥°-1 -23^24; =0^00-18^45 ≡°-1 -20^25
14	6	1.2	•	•°6^32...7^21; 11^02-12^25; 13^25...19^10; ≡°4^45-5^45 =6^30-9^30; 10^15-20^15
15	8	13.0	•	•°10^45-11^40; 12^00...50 ⚥°14^25-35; 15^40-16^30 •°...20^05; 20^15-24; =6^10-9^30
16	6	5.3	14	•°0^00-1^45 ⚥°-2^10 *°-4^35; 7^20-12^15 ♎°-16^30 *°-18^10...19^05 ♎°-21^30 *°-24; =na-24
17	8	0.0	15	*°0^00-6^15; 21^38...23^13; =0^00-6
18	9	13.0	11	•°14^45...15^10; 18^40...20^15 •°-1 -23^10; ⚶°0^35-3^35
19	9	28.4	•	•°1^40...2^25 13^47...14^30 16^30...18^20 •'-24
20	6	17.1	•	•°-1 0^00-2^40 7^02-15^28 ⚥'-17^10 *'-17^43...18^33-21^35; ⚳ na, p, np; =8^30-23^10
21	6	•	2	♎°0^18-2^40; =0^20-24
22	8	21.1	1	*°18^30...20^20 ♎°-22^10 *°-24; =0^00-3^15
23	5	17.3	20	*°-1 0^00-20^02 ♎°-22^35 *°-24; =0^00-24
24	6	1.5	37	*°-1 0^00-10^15...13^40-19^10 ♎°-21^15; =0^00-2^30, 6^15-24
25	2	11.8	37	♎°12^24-14^18 *°-1 -23^10; =0^00-8^48 ≡°-1 -13^50 =14^15-24; V° 9^30-13^50
26	5	16.1	38	*°11^07-20 ♎°-12^10 ♊°♎°-15^05 ♋°-15^35 *'-0 -24; =0^00-24; ∼ 12^10-15^35
27	6	•	43	*°0^00-2^38; =0^00-24
28	6	0.1	40	=0^00-19^45 ≡°-20^20 =-24
29	7	•	35	♋°0^35-3^40; =0^00-11^40; 17^15-20^10; ∼° 0^35-3^40
30	7	4.9	33	♎°15^25-18^15; 20^15-21^10 ⚥°-0 -23^40
31				
Σ	—	172.5	—	UWAGI:

Grudzień - Décembre

1	8	1.8	39	⚥°-1 0^26...2^42 ⚲°-1 5^07-7^45...8^10 ⚥°-1 8^18...23^45; =4^10-8^10; 21^30-24
2	7	•	44	⚥°0^50-3^10 *°3^30-6^15; =0^00-7^20
3	8	•	40	⌣'1-24
4	9	•	39	⌣' 0^00-9
5	9	•	37	=15^30-17^30
6	6	•	35	=11^30-13^40; 14^20-17^30 ≡°-19^45 =-20^20; ⌣°-1 19^00-24; ⚶' 21-22 ⚲' -23 ⚶' -24
7	9	•	34	⌣°-2 0^00-9 ⌣°20-24; ⚶' 0^00-3^30
8	9	•	32	=0^30-6^10; ⌣°20-24
9	9	0.0	30	⌣°0^00-10^00; ⚲°20-21^30
10	8	0.8	29	*°3^15...40; 5^45-6^07; 14^08-50
11	7	0.0	30	*°2^45-3^30 ♎°-5^20 ⚥°8^08-9^40 *°-10^23 ⚥13^15-42; 14^05-16^13; =8^15-10^30
12	9	•	27	⚶°19^00-20^10
13	9	4.0	25	•°21^15...22^20; ⚶°9^40-11^15 ⚥°-13^45; ⚳ a, p; ⚶°6^10-7^10
14	6	21.9	25	•°3^45-4^10 •°-4^40 *°-1 -20^00 ♎°-1 -24
15	6	1.4	42	♎°0^00-1^40 *°10^35...11^05-13^15...14^20-15^18; =12^30-15^30; ⚶°22^40-23^20 ⚲ 23^45-24
16	8	3.0	42	*°6^05-9^25 •*°-11^15 ⚥°12^20-13^45; 19^50-20^13; 22^45-24; ⚲°0^00-1^15
17	6	1.5	41	⚥°0^00...5^40 ⚥°-1 -8^40 *°-2 -14^38; 19^50-21^45; =6^30-14^15
18	9	0.0	43	⚥°11^58-12^10 *°21^50...22^20; ⌣° p-np
19	9	2.8	41	*°-1 0^48...1^25; 6^07-11^45...12^10 ⚥12^50-15^40 *°-16^15; 17^30...19^10; =7^20-24
20	9	0.3	47	*°0^45...1^20; 14^42...16^25; 17^10-24; ⌓° 0^00-12^30; 15^40-24
21	7	•	49	*°0^00...10; =0^00-30; 6^30-24; ⌣°-1 1-9 ⌣' 20-24
22	6	1.8	42	↔°9^45-10^20 *°15^40...18^30-20^20 ♎°-23^15; =9^30-15^20; 18^30-24; ⌣' 0^00-16^00
23	8	1.3	43	♎°1^12-7^15 *°-1 10^08 ↔°2 18^10-24; =0^00-11^30; 18^10-24
24	7	0.0	45	↔' 0^00-16 *°3^20-12^10; 12^30...16^10; =0^00-12^30; 20^10-24
25	6	0.9	44	*°7^20...13^15-17^30...18^25; 20^25...22^10; =0^00-16; 7^20-24; ⌣°0^00-7; np
26	6	0.0	42	•°9^45-11^10; =0^00-5^30; 9^20-13^20; ⌣°0^00-8
27	7	0.0	40	*°8^15...9^10-10^15...12^30; =0^40-12^30
28	7	0.0	40	↔°20^30-22^10; =17^30-20^30
29	8	0.0	39	⚥°12^27-13^15; ⚶°10^20...12^15 ⚥°...17^43; ⚳ a, p; ⌣°-2 0^00-9
30	8	11.9	37	*'20^10-23^40 *°-24; =10^45-24
31	6	3.7	32	*°-1 0^00-9^30 ♎°-10^10 *°-1 -14^25; =0^00-14^25
Σ	—	57.1	—	UWAGI:

Kasprowy Wierch φ=49°14' λ=19°59' Styczeń-Janvier 1962

DNI	CIŚNIENIE P-700 I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	92.1	91.9	90.1	91.4	-0.6	-5.9	-6.5	-4.9	2.0	-7.8	89	79	86	85	0.6	0.8	0.5	0.6	10	10✳	10△	WNW 5	N 3	ESE 2
2	85.9	86.7	88.4	87.0	-7.6	-10.1	-13.0	-10.9	-5.9	-13.3	96	94	92	94	0.1	0.2	0.2	0.2	10≡	10△≡	10△≡	SW 2	N 3	NNE 5
3	91.2	94.2	96.4	93.9	-14.9	-11.1	-9.8	-11.4	-9.7	-15.3	100	39	94	78	0.0	1.6	0.2	0.6	0	1⊙	7	NNE 10	NNE 5	NNE 7
4	99.4	100.5	100.3	100.1	-5.4	-0.8	-1.7	-2.4	0.1	-10.6	22	9	18	16	3.2	5.2	4.4	4.3	0	0⊙	0	NE 4	E 2	NE 2
5	99.8	99.3	97.9	99.0	-4.2	-0.7	0.2	-1.1	0.6	-4.7	0	19	22	14	4.5	4.7	4.8	4.7	3	9⊙	4	NNE 3	NNW 1	W 4
6	94.7	93.7	91.8	93.4	-2.3	-2.5	-5.7	-4.0	0.7	-6.2	41	52	97	63	3.1	2.5	0.1	1.9	1	2⊙	4	SW 6	W 5	WNW14
7	91.4	94.2	97.4	94.3	-10.7	-10.2	-12.1	-11.3	-5.5	-12.4	94	94	96	95	0.2	0.2	0.1	0.2	10✳△≡	10✳△≡	10✳≡	NNW 7	N 8	NNE 9
8	99.6	101.1	101.4	100.7	-8.6	-4.9	-5.8	-6.3	-4.6	-13.8	36	45	97	59	2.0	2.3	0.1	1.5	1	1⊙	9	NE 7	NNE 4	C 0
9	98.6	97.0	96.3	97.3	-5.1	-4.8	-3.2	-4.1	-2.5	-7.9	28	27	17	24	3.0	3.1	4.0	3.4	3	2⊙	2	S 10	SSW11	SSW12
10	91.0	86.9	90.1	89.3	-4.8	-8.1	-7.1	-6.8	-2.1	-10.0	32	95	96	74	2.9	0.2	0.1	1.1	8	10≡	10	S 18	S 20	SSW11
11	91.0	88.7	88.0	89.2	-5.0	-5.7	-4.1	-4.7	-3.6	-8.6	73	97	96	89	1.1	0.1	0.2	0.5	1	10≡	10△≡	S 12	S 16	S 17
12	86.3	86.4	83.4	85.4	-3.8	-4.0	-4.5	-4.2	-3.0	-5.4	96	96	98	97	0.2	0.2	0.1	0.2	10✳≡	10△≡	10△≡	SSW13	SW 6	SSW11
13	75.9	79.2	80.2	78.4	-5.2	-4.5	-5.3	-5.1	-3.8	-7.6	95	98	98	97	0.2	0.1	0.1	0.1	10△≡	9	10✳≡	SSW14	SW 6	S 7
14	81.5	83.8	86.9	84.1	-7.6	-10.0	-9.8	-9.3	-4.6	-11.1	96	72	79	82	0.1	0.8	0.6	0.5	10✳≡	3⊙	2	NW 4	WNW 8	W 11
15	89.5	92.0	94.4	92.0	-9.8	-10.2	-11.7	-10.8	-9.4	-12.4	69	78	86	78	0.9	0.6	0.3	0.6	1	2⊙	0	W 11	W 7	NNE 1
16	97.1	98.6	98.8	98.2	-10.0	-7.0	-4.1	-6.3	-5.6	-13.2	43	40	16	33	1.6	2.2	3.8	2.5	0	3⊙	7	N 3	SSW 5	SSW12
17	97.6	96.6	96.3	96.8	-3.2	-4.7	-1.6	-2.8	0.2	-10.0	26	59	23	36	3.5	1.7	4.1	3.1	8	6	6	SSW15	SSW18	SSW12
18	93.4	95.0	96.7	95.0	-3.7	1.0	-1.4	-1.4	2.5	-6.0	33	33	48	38	3.1	4.4	2.9	3.5	10	9⊙	5	SSW18	SSW 7	NW 4
19	97.6	98.0	97.1	97.6	-3.8	-1.5	-2.9	-2.8	-0.6	-4.5	87	76	88	84	0.6	1.4	0.6	0.9	7	8⊙	6	W 2	WNW 6	SW 11
20	97.1	98.4	100.6	98.7	-4.1	-4.0	-4.0	-4.0	-0.5	-6.1	98	55	96	83	0.1	2.1	0.2	0.8	9✳	4⊙	10✳≡	WNW13	WNW13	NW 11
21	101.2	100.9	100.4	100.8	-4.4	-2.8	-2.3	-3.0	-1.3	-7.0	98	97	98	98	0.1	0.1	0.1	0.1	10✳	8	9	WNW 8	SW 5	WSW 7
22	95.1	92.2	93.0	93.4	-3.4	-2.2	-5.4	-4.1	-0.2	-5.9	97	64	65	75	0.2	1.9	1.4	1.2	9	9⊙	9	SSW12	SW 14	WNW11
23	93.2	94.3	95.4	94.3	-6.6	-6.9	-8.8	-7.8	-5.4	-10.0	44	50	71	55	2.1	1.8	0.9	1.6	8	7⊙	9	WSW 8	W 6	WSW 5
24	95.1	94.6	92.0	93.9	-11.6	-9.5	-9.2	-9.9	-8.0	-12.2	97	83	95	92	0.1	0.5	0.2	0.3	6✳	8	10✳△≡	W 3	W 8	SSW13
25	92.5	91.2	90.8	91.5	-3.0	-3.6	-5.0	-4.2	-2.0	-10.0	97	97	98	97	0.1	0.2	0.1	0.1	10✳△≡	10✳≡	10✳≡	WNW 8	SW 7	WNW 8
26	89.9	91.2	91.5	90.9	-5.6	-8.6	-10.1	-8.6	-4.5	-12.0	97	95	94	95	0.1	0.2	0.2	0.2	10✳≡	10✳△≡	8	N 9	N 6	NNW 9
27	89.8	90.6	91.3	90.6	-6.6	-9.4	-10.6	-9.3	-5.7	-11.4	97	98	97	97	0.1	0.1	0.1	0.1	10✳△≡	10△≡	10✳≡	NNW 8	NNW13	NNW12
28	87.7	86.8	84.6	86.4	-10.9	-11.3	-15.9	-13.5	-10.3	-16.2	97	97	95	96	0.1	0.1	0.1	0.1	10✳≡	10✳	10✳△≡	N 13	NNW 8	N 8
29	84.3	86.5	89.9	86.9	-19.4	-20.5	-21.8	-20.9	-15.9	-21.8	95	96	96	96	0.1	0.1	0.0	0.1	10✳△≡	10✳≡	9✳	N 11	N 10	NE 9
30	94.1	96.5	97.7	96.1	-16.3	-14.5	-16.5	-16.0	-13.9	-21.8	95	96	95	95	0.1	0.1	0.1	0.1	9✳	10✳≡	3	ENE 9	NE 8	ENE11
31	96.5	95.7	94.6	95.6	-17.0	-11.0	-10.2	-12.1	-8.9	-18.3	95	93	91	93	0.1	0.2	0.3	0.2	8	8✳⊙	0	E 14	ESE 4	ENE 2
M	92.6	93.0	93.3	93.0	-7.3	-6.8	-7.4	-7.2	-4.2	-10.8	73	72	79	75	1.1	1.3	1.0	1.1	6.8	7.1	7.1	9.0	7.8	8.3

Luty-Février

1	89.9	89.7	89.9	89.8	-11.9	-8.4	-8.8	-9.5	-6.4	-13.0	97	92	95	95	0.1	0.3	0.2	0.2	9✳	3⊙	10✳△	SSW 7	SSE 7	SE 4
2	89.1	91.3	92.0	90.8	-11.6	-8.0	-11.3	-10.6	-6.6	-12.0	93	93	90	92	0.2	0.2	0.3	0.2	10	5⊙	10	S 4	SW 1	ENE 4
3	92.1	93.8	95.6	93.8	-11.0	-9.3	-7.0	-8.6	-6.5	-11.8	93	95	96	95	0.2	0.2	0.1	0.2	10✳≡	10△≡	10△≡	NE 8	NNE 8	ENE 7
4	94.6	93.8	94.2	94.2	-4.8	-6.4	-10.3	-8.0	-3.6	-10.6	93	73	97	88	0.3	1.0	0.1	0.5	5	9	10△≡	S 4	NW 3	N 2
5	92.5	87.5	86.6	88.9	-12.7	-10.5	-8.5	-10.0	-6.1	-13.7	81	94	95	90	0.4	0.2	0.2	0.3	1	10≡	10✳≡	SSW 8	SSW16	NNW 6
6	89.9	91.7	94.0	91.9	-11.6	-11.1	-11.1	-11.2	-8.4	-12.1	93	93	97	94	0.2	0.2	0.1	0.2	10✳≡	10✳≡	10✳≡	NNW16	NNW11	NNW15
7	94.0	94.3	92.5	93.6	-11.7	-6.7	-6.6	-7.9	-5.2	-12.3	97	91	75	88	0.1	0.3	0.9	0.4	10≡	1⊙	1	N 7	NE 3	S 3
8	90.6	91.0	92.3	91.3	-5.5	-1.7	-7.7	-5.6	-1.1	-8.0	92	98	96	95	0.3	0.1	0.1	0.2	9	9⊙	6	W 1	C 0	C 0
9	94.9	98.4	101.5	98.3	-6.5	-6.2	-8.8	-7.6	-4.8	-9.0	97	97	95	96	0.1	0.1	0.2	0.1	10△	10△≡	10✳≡	WNW 1	NNE 4	NNW 1
10	102.1	102.8	102.6	102.5	-13.4	-11.1	-10.4	-11.3	-8.8	-13.7	80	59	39	59	0.4	1.1	1.7	1.1	0	2⊙	9	NNE 4	ENE 3	NE 3
11	100.0	99.6	100.5	100.0	-7.2	-6.6	-11.2	-9.0	-5.2	-11.9	17	51	93	54	2.9	1.8	0.2	1.6	9	9✳△	10✳△≡	W 3	WNW 5	N 8
12	94.8	86.8	79.3	87.0	-12.4	-8.0	-4.2	-7.2	-2.6	-14.3	63	96	96	85	0.9	0.1	0.2	0.4	8	10≡	10✳≡	SSW18	WSW24	WSW23
13	73.1	68.6	68.6	70.1	-5.9	-6.1	-9.6	-7.8	-3.6	-9.6	97	97	94	96	0.1	0.1	0.2	0.1	10✳△≡	10✳≡	10△≡	W 14	SW 8	W 4
14	68.1	68.2	71.3	69.2	-11.4	-12.8	-14.6	-13.4	-9.5	-14.6	93	96	96	95	0.2	0.1	0.1	0.1	10△≡	10✳≡	10✳△≡	N 7	N 11	N 12
15	77.2	80.5	87.8	81.8	-15.3	-15.4	-17.3	-16.3	-14.6	-17.6	95	95	95	95	0.1	0.1	0.1	0.1	10✳≡	10✳≡	10✳≡	N 12	NNE17	NNE14
16	88.0	80.7	77.5	82.1	-16.3	-8.4	-6.6	-9.5	-5.2	-20.5	77	98	97	91	0.4	0.1	0.1	0.2	9	10✳≡	10✳	W 11	WSW19	WNW23
17	72.0	72.7	77.4	74.0	-10.4	-10.9	-12.0	-11.3	-6.6	-12.2	97	94	93	95	0.1	0.2	0.2	0.2	10✳≡	10✳≡	10✳≡	NW 24	NW 23	NNW19
18	79.9	83.9	90.1	84.6	-14.8	-16.3	-16.0	-15.8	-12.0	-16.9	96	95	95	95	0.1	0.1	0.1	0.1	10✳≡	10✳≡	10✳≡	N 22	N 21	N 17
19	91.0	92.1	93.9	92.3	-16.0	-9.6	-7.7	-10.2	-7.5	-16.9	95	94	96	95	0.1	0.2	0.1	0.1	10✳≡	10✳≡	10✳≡	N 9	NNW12	NNW12
20	95.0	95.3	95.1	95.1	-8.9	-8.4	-7.5	-8.1	-7.2	-9.8	95	95	96	95	0.2	0.2	0.1	0.2	10≡	10≡	10≡	N 8	NW 6	NNW11
21	91.5	91.4	93.1	92.0	-11.5	-13.6	-13.8	-13.2	-7.3	-14.1	95	96	96	95	0.2	0.1	0.1	0.1	10✳≡	10✳≡	10✳≡	N 10	N 9	N 11
22	95.0	95.8	97.0	95.9	-16.5	-13.6	-18.5	-16.8	-12.6	-18.6	95	92	95	94	0.1	0.2	0.1	0.1	10✳≡	9	6	N 10	NE 12	NE 7
23	96.6	95.7	92.2	94.8	-17.7	-14.0	-16.5	-16.2	-13.2	-18.6	95	96	95	95	0.1	0.1	0.1	0.1	3	10✳△	10✳≡	NE 8	NNE 8	N 8
24	87.6	86.2	86.5	86.8	-16.3	-11.7	-16.7	-15.4	-10.9	-17.2	95	93	95	94	0.1	0.2	0.1	0.1	10✳≡	9✳△	3△	NNE 7	S 1	S 1
25	87.1	88.6	89.8	88.5	-17.4	-13.0	-15.1	-15.2	-12.4	-17.9	95	92	96	94	0.1	0.2	0.1	0.1	6	10✳≡	4△	ESE 1	SSW 3	SE 4
26	89.8	90.6	92.0	90.8	-15.8	-12.4	-10.6	-12.4	-9.3	-16.7	95	89	84	89	0.1	0.3	0.4	0.3	8	3⊙	9	SSE 5	SSW10	S 6
27	92.1	91.7	91.0	91.6	-6.5	-5.6	-4.8	-5.4	-3.6	-11.0	91	76	88	85	0.3	0.9	0.5	0.6	9	9⊙	10✳	S 3	S 6	SE 2
28	88.8	87.3	86.6	87.6	-7.7	-7.0	-7.5	-7.4	-4.7	-8.8	96	96	96	96	0.1	0.1	0.1	0.1	10✳△≡	9✳	10✳≡	S 6	SSW10	S 8
29																								
30																								
31																								
M	89.2	88.9	89.7	89.3	-11.7	-9.7	-10.7	-10.7	-7.3	-13.7	89	90	92	90	0.3	0.3	0.2	0.3	8.4	8.5	8.9	8.5	9.3	8.4

Kasprowy Wierch H_s=1991m H_b=1988,8m h_w=15,4m Styczeń - Janvier 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	7	5.3	105	∗▲^0-1 7^55-8^30 ∗^0-9^15 ∗^1-11^00 ∗^0-11^40 ▲^0-11^45 ∗^0-16^50 17^20 20^15 ▲^0-24; ≡^1 9^00-30 ≡^2-11^00 ⪢ 0^00-5^40 (por. 22) ⌓^0 2^30-5^10
2	0	2.2	115	▲^0 0^00-1^50 ∗^0 2^15-5^50 ▲^0 8^45-10^15 11^45-13^35 20^35-24; v^0-2 5^50-13^40 14^50-24; ≡^2 5^50-13^40 14^50-24
3	9	0.3	116	▲^0 0^00-4^30 ∗ ▲^0 17^10-19^10 ∗^0 20^00 v^2 0^00-6^10 v^0 16^12 21^30; ≡^2 0^00-5^30 ⩸-6^10 (∞)-8^00 ⩸ 16^12-35 ≡^2-20^20 ⩸-21^25 ∞ 21^00-24. ⪢ 6^00-7^20 8^40-9^05; ⫲^0 6^00-24, () 6^10-15^20
4	9	•	114	∞ 0^00-6^00 (∞)-10^40; ⫲^0 0^00-4^30; () 6^10-24, zielony promień 15^47 (niebieski)
5	9	•	105	() 0^00-24
6	9	2.5	103	v^1 22^20-24, ⩸ 15^35-16^30 ≡^2 22^20-24; ⪢ 17^30-24 (por. 24), ⫲^0-1 11^45-12^10 16^15-24
7	0	8.0	105	∗▲^0-1 1^30-20^15 ∗^0-24; v^1-2 0^00-24; ≡^2 0^00-24; ⪢ 0^00-45 (por. 17) 9^40-11^45 (por. 15) 19^30-20^20; ⫲^1 0^00-1^10 ⫲^0-1 8^15-24
8	9	0.1	111	∗^0 0^00-1^45 ∗ ▲^0 16^40-18^50; v^2 0^00-1^40 v^0 16^50-19^50 20^30-21^15; ≡^2 0^00-1^35 ⩸-1^40 ∞ 1^35-na (∞)-9^20 ⩸ 16^50-18^15 ≡^2-19^30 ⩸-19^50 (∞)-21^10 ⩸ 20^30-21^15; ⫲^0 0^00-6^00 ⫲^0-7^30; () 4^40-16^20
9	9	•	106	(∞) 3^30-7^10 ∞-11^30 (∞)-13^40, ⪢ 4^45-24 (por. 20); ⫲^0 6^50-8^30 ⫲^0-9^30 ⫲^1-24; () 5^30-24
10	0	•	100	v^0 9^35-21^40; ≡^2 9^35-18^10 ⩸-19^30 ≡^2-20^26 ⩸-21^40, ⪢ 0^00-4^45 ⇘-18^30 (por. 36) ⪢-22^50 (por. 21); ⫲^1 0^00-6^00 ⫲^2-18^30 ⫲^0-1-24, () 0^00-9^35
11	0	10.0	97	▲^0 10^08 12^10 15^50-21^50; v^0 7^45 14^00 v^1-2-24; ⩸ 7^45-9^15 ≡^2-24, ⪢ 4^30-12^10 (por. 21) ⇘-24 (por. 30) ⫲^0-1 0^00-24, () 0^30-8^15
12	0	9.4	97	∗^0-1 3^15-7^40 ∗▲^0-1-11^30 ▲^0-1 11^30-24; v^2 0^00-5^10 v^1-2-24; ≡^2 0^00-24; ⇘ 0^00-3^10 (por. 26) ⪢-8^30 (por. 26), 14^25-18^35 (por. 16), 20^20-24 (por. 24); ⫲^0-1 0^00-24
13	9	4.7	95	▲^0-1 0^00-3^20 ∗▲^0-1-6^10 ▲^0-1-8^30 ∗▲^0-10^40 ∗^0-11^40 18^25-24; v^0 0^00-9^30 v^1-11^15 v^0-11^40 17^00...35 19^25 24; ≡ 0^00-7^05 ⩸-8^20 ≡^2-11^15 ⩸-11^40 17^05-35 ≡^2 19^25 24; ⪢ 0^00-8^30 (por. 28) 16^35-18^20; ⫲^0-1 0^00-8^30 ⫲^0...
14	9	0.0	100	∗^0 0^00-5^15 ▲^0-7^20; v^0 0^00-0^30 1^15 4^40-6^00 v^1-8^35 v^0 22^30-24; ≡^2 0^00-30 ⩸-1^15 ≡^2 4^40-8^35 ⩸-22^30-24; ⪢ 10^50-12^30 14^20-22^15 (por. 18); ⫲^0-1 0^00-40 10^10-24; () 12^20-16^30
15	9	0.0	98	v^0 0^00-40 ⊔^0 18^00-24; ⩸ 0^00-40 (∞) 7^30-a, 11^00-n, ⪢ 0^20-10^05, ⫲^1-0 0^00-10^15 (por. 20), ⊘ a.. () 9^30-13^40 [13.1: 14^20 20^30-24
16	9	•	97	∗^0 1^50 2^15; ⊔^0-1 0^00-25 v^0-1^45 ⊔^0 2^30-8^00; ⩸ 0^25-35 ≡^2-1^40, ⪢ 14^15-24; ⫲ 15^10-24; () 7^15-24
17	9	•	92	⪢ 0^00-4^30 ⇘-5^10 ⪢-9^05 ⇘-14^40 (por. 24) ⪢-16^40 17^30 19^00 ⇘-19^55 (por. 21) ⪢-24 (por. 16), ⫲^0 0^00-15 ⫲^0-1 0^15 11^30 ⫲^2-13^30 ⫲^1-16^40 ⫲^0-22^30; ⌓^0 18^40-n, () 0^00-24
18	9	•	90	⪢ 0^00-3^20 (por. 18) ⇘-8^00 (por. 24) ⪢-11^20; ⌓^0 0^00-3^30; () 0^00-24
19	9	0.1	87	v^0 22^30...50; ⩸ 22^30-50; ⪢ 19^35...21^40 (por. 20) ⇘-24 (por. 26); ⫲^0-1 22^00-24; ⊘ a-p; ⌒ p-np; () 0^00-15^30, 16^20-20^00
20	8	1.4	84	∗^0 2^40 7^15 ▲^0-9^30 18^53 19^10 ∗▲^0-24; v^0 6^15 9^20 16^20-24, ⩸ 6^15-9^20 16^20 18^30 ≡^2-24. ⇘ 0^00-1^40 (por. 24) ⪢ 11^40 (por. 29), 12^05 15^10 (por. 28) ⇘-17^15 (por. 28) ⪢ 21^30; ⫲^0-1 0^00 2^40 ⫲^0-1 10^30, 15^10-24; ⌒^0 na.. 2^30
21	8	0.3	81	∗▲^0 0^00-2^35 ∗^0-1 5^50-9^15 15^50-18^40, v^0 0^00-3^40 4^40 11^40; ≡^2 0^00-30 ⩸-3^40 4^40-11^40 12^00-18^30, 20^20-21^30; ⪢ 0^45-2^20 (por. 20), 13^50...20^10 (por. 20); ⫲^0 0^00-2^35 5^50-8^00 15^50-20^15
22	9	•	81	v^0 1^20 2^30 v^0-1 8^30; ⩸ 1^20-2^30 ≡^2-6^15 ⩸-8^30; ⪢ 3^00-9^20 ⇘-9^35 (por. 22) ⪢-10^50 (por. 18) ⇘-11^00 ⪢-11^45 ⇘-11^55 ⪢ 13^20, 18^20-21^20 (por. 23); ⫲^0-1 8^20-14^30; () 8^30-24
23	9	0.0	79	⊔^0 22^00-24, ⊕^0-1 7^30-11^30 14^40-15^55 ⌒^0-1 1^40-4^20 ⌓^0 20^00 21^00 ⌓^1-24; () 0^00-7^20, 11^30-15^45
24	8	3.1	78	∗^0 6^09 9^10 17^40-20^10 ∗▲^0-24; ⊔^0-1 0^00-6^05 v^1... 9^20 v^0 16^05-24; ⩸ 6^10-9^20 16^05-17^15 ≡^2-24; ⪢ 19^30-24 (por. 23); ⫲^0-1 17^40-24; ⌓^1 0^00-1^25 ⊕ 8^07-9^20
25	0	6.4	82	∗▲^0-1 0^00-3^40 5^15-8^30 ∗^0-10^50 12^20 14^50 20^25-22^30 ∗^1-23^20, v^0-1 0^00-10^40 v^1... 24; ≡^2 0^00-10^40 ⩸-11^30 ≡^2 12^20-14^15 ⩸-19^30 ≡^2 20^20-21^30 22^30-23^40 ⩸-24; ⪢ 0^00-5^30 (por. 25), 8^50-11^50 (por. 19); ⫲^0-1 0^00-24
26	0	11.9	90	▲^0 1^15-20 2^50 3^10 ∗^0 5^50-6^30 ∗^1-8^45 ∗^0-11^40 ▲^0-12^30 ∗▲^0-16^40 ▲^0-17^40; v^1 0^00-17^40 v^0 23^15-24; ⩸ 0^00-20 ≡^2-17^40 ⩸ 21^40 23^15 ≡^2-24; ⫲^0-1 0^00-9^30 ⫲^1 20^30-21^40 ⫲^0-24
27	0	16.6	105	∗^0 0^10-40 ∗^1 3^10 ▲^0 5^20 ▲^0 6^10 ∗▲^0-7^30 ∗^1-8^15 ▲^0 9^00 ∗▲^0-1 11^15 ▲^0-1 14^05 ▲^0-1 18^10 ∗^1-21^40 ∗^0-22^25 ∗^0-1-24; v^0 0^00-9^30 v^1-2 21^40 v^2...24; ≡^2 0^00-21^40 ⩸-23^20 ≡^2-24; ⪢ 2^40 3^30 (por. 16), 8^30-9^20 (por. 17), 10^10-24 (por. 21);
28	5	17.9	143	∗^0-1 0^00-30 ∗^1-2 1^40 ∗^0-1 4^30 ∗^1-8^10 ∗▲^1-10^35 ∗^1-0 17^45 ∗^2-19^25 ∗▲^0-21^25 ∗^2-23^30 ∗^1-0-24, v^2 0^00-9^10 v^1-10^10 v^0-24; ≡^2 0^00-12^20 ⩸-13^40 ≡^2-24; ⪢ 0^00-9^10 (por. 23); ⫲^1-2 0^00-3^45 ⫲-9^15 ⫲^1-0-24; ʃ^2 16^20 19^10, 21^30 23^40
29	0	14.7	190	∗^1-0 0^00-3^10 ∗▲^0-9^30 ∗^1-16^15 ∗^0-22^45 23^20-24, v^0 0^00-19^40 24; ≡^2 0^00-19^40 ⩸-23^40 ≡^2-24; ⪢ 0^30-13^20; ⫲^1-0 0^00-24 [27.1: ⫲^0 0^00-6^30 ⫲^1-2-21^30 ⫲^0-2-24; ʃ^1 20^00 21^00
30	1	1.7	205	∗^0 0^00-1^46 6^30-16^30 ∗▲^0-18^30 ∗^0-19^30, v^0 0^00-1^40 8^45-18^45; ≡^2 0^00-1^40 ⩸-2^30 7^15-8^45 ≡^2-18^45, ⪢ 9^15-11^40 (por. 20), 13^15-24 (por. 20); ⫲^0-1 0^00-24; ⌂^0 2^50-4^00
31	6	0.9	207	∗▲^0 8^28-9^45 ∗^0-13^15 ... 16^25, v^0 8^36 ... 13^30; ⩸ 8^36-9^10 ≡^2-10^20 ⩸-13^30 (∞) p-24, ⪢ 0^00-7^15 (por. 24); ⫲^1 0^00-7^15 ⫲^0-9^15
Σ	—	117.5	—	UWAGI.

Luty - Février

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	9	3.5	205	∗^0 4^51 7^40-8^35 ... 9^50 ▲^0 18^50 19^20 ∗▲^0-1-20^45 ∗^1-2-24, v^0 4^40...12^45, (∞) 0^00-5^15 ⩸ 4^40 5^15 ≡^2-6^10 ⩸-6^50 ≡^2-7^46 ⩸-12^45 ∞ 6^10...8^30, ⪢ 7^10-9^20; ⫲^0 6^20-16^15; ⊛^0 7^45...10^20
2	9	0.3	191	∗^0-1 0^00-2^52 ∗▲^0 7^40-8^30 ∗^0-9^50; v^0 3^30-10^40; ⩸ 3^30-7^10 ≡^2-9^40 ⩸-10^40 (∞) 9^40-11^30 ∞ 14^35-15^20 (∞) 23^30-24, ⫲^2 2^40-4^40 9^40-12^10, ⊕^2 13^30-16^00, ⌂^0-1 0^20...2^10; () 10^00-24
3	0̈	3.1	192	∗^0 2^45-6^00 ▲^0-8^30 ∗▲^0-1-12^20 ▲^0-22^35, v^0 3^20-22^40; ≡^2 3^20-22^40 (∞) 0^00-3^20, 22^40-24. ⪢ 3^50-4^05, 8^40-11^30 (por. 15), 14^15-45; ⫲^0 2^00-21^30; () 0^00-2^00
4	9	0.3	195	▲^0 15^49 18^05 ∗^0... 20^05 ▲^0... 24; v^0 10^30...11^10, 17^20-24; (∞) 0^00-a ∞ a-9^30 (∞)-10^30 ⩸ 10^18-11^10, 17^15-30 ≡^2-24. ⊛^0 8^00-9^00; ⊕^0 8^10...10^10; () 8^00-10^20, 11^10-14^30
5	0	2.8	192	▲^0 0^00...15 ∗^0 2^20 ▲^0 17^40-20^20 ∗^0-24; v^1 0^00-2^30 v^0 12^30-24, ≡^2 0^00-2^15 ⩸-2^40 ∞ 2^15-4^00 (∞)-6^00 ⩸ 10^05-12^30; ⪢ 8^40-12^40 ⇘-15^15 (por. 22) ⪢-20^30 (por. 22), 22^40-24 (por. 21); ⫲^0 6^00-8^30 ⫲^0-12^20 ⫲^1-24; () 7^30-11^30
6	0	4.4	195	∗^0 0^00-12^45 ∗^0-1-23^40; v^1 0^00-p v^2-24, ≡^2 0^00-24; ⪢ 3^40-5^20 (por. 28) ⇘-6^30 (por. 24) ⪢-16^30 (por. 21) ⇘-19^45 (por. 31) ⪢-24 (por. 16); ⫲^1 0^00-3^40 ⫲^2-7^30 ⫲^1-16^30 ⫲^2-22^00 ⫲^1-24
7	9	•	210	∗^0 0^50-2^30, v^2 0^00-8^25, ≡^2 0^00-8^25 ⩸-8^45; ⪢ 0^00-2^30 (por. 15), ⫲^1 0^00-2^00 ⫲^0 3^15, ⊛^1 8^25-45, () 9^30-24
8	8	0.6	205	⊔^0 17^30-20^15 ⊔ v^0-22^40 v^0-1-24, ∞ a-np ⩸ 20^15-22^40 ≡^2-24, ⊕^0 8^20-14^30, () 0^00-9^15
9	0	1.4	201	▲^0-1 5^05-9^30 ∗^0-11^15 ▲^1-13^15 ▲^0-15^40 ∗^0 20^15-21^20, v^0-1 0^00-na v^1... 8^20-24, ≡^2 0^00-3^50 ⩸-8^20 ≡^2-18^10 ⩸-18^30 ≡^2-24
10	9	•	205	∗^0 1^50-4^20, v^1 0^00-5^30, ≡^2 0^00-5^30 ∞-7^30 (∞)-a; ⌒^1-2 18^35-20^10, () 5^30-24
11	9	3.2	199	▲^0 7^41-8^30 ∗▲^0-9^45 ∗^1-10^45 ∗^0-10^50 ∗▲^0 12^30-24; v^0-1 15^35-24, ≡^2 15^35-24; ⪢ 14^10-20^30 (por. 17); ⫲^0-1 14^10-24; () 0^00-9^15, 10^50-14^30
12	1	4.4	201	∗▲^0 0^00-45 ∗^0 13^45 14^30-24, v^1 0^00-1^50 v^0 10^15-23^00 v^1-24, ≡^2 0^00-50 ⩸-1^50, 10^10-25 ≡^2-24, ⪢ 5^10-20 ⇘-24 (por. 41); ⫲^0 0^00-30 ⫲^1 4^45-5^20 ⫲^2-24; () 6^20-9^30
13	0	7.3	202	∗^0 0^00-6^05 ∗▲^0-1 7^40 ∗^0-18^30 19^50-20^30 ▲^0-21^20 ▲^0-24; v^1 0^00-24, ≡^2 0^00-16^40 ⩸-17^10 ≡^2-24; ⇘ 0^00-6^10 (por. 33) ⪢-7^00 (por. 19); ⫲^2 0^00-7^00 ⫲^1-8^30 ⫲^0-18^10
14	0	31.8	205	▲^0 0^00-1^40 ∗^0 2^40-4^50 ▲^0-6^40 ▲^0-8^40 ∗^0-1-17^40 ∗▲^1-21^30 ∗^1-24, v^1 0^00-a v^2-24, ≡^2 0^00-24, ⪢ 12^15-24 (por. 21); ⫲^0 5^30-12^15 ⫲^1-24
15	0	17.6	250	∗^1 0^00-3^00 ∗^0-17^30 ∗^1-22^15 ∗^0-24, v^2 0^00-8^00 v^0-1-24, ≡^2 0^00-24, ⪢ 0^00-11^20 (por. 21) ⇘-16^50 (por. 25) ⪢-24 (por. 23); ⫲^1-2 0^00-22^30 ⫲^1-24
16	0	3.0	262	∗^0 0^00 2^30 ∗▲^0 8^45-11^35 ∗^0-1-24, v^1 0^00 2^45 v^2 9^20 24; ≡^2 0^00-2^45 ⩸ 9^20-11^14 ≡^2-13^51 ⩸-15^10 ≡^2-18^30 ⩸-21^40 ≡^2-24; ⪢ 0^00-45 (por. 16), 6^30-7^40 (por. 23), 8^30-10^45 (por. 20) ⇘-24 (por. 40); ⫲^1 0^00-1^00 3^40-10^45 ⫲^1-2 11^30 ⫲^2-24; () 6^20 7^30
17	0	5.8	268	∗^1 0^00-2^20 ∗^0-7^30 ∗^1-8^20 ∗^0-15^40 ∗^1-24; v^0 0^00...24; ≡^2 0^00-3^40 ⩸-5^50 ≡^2-24; ⇘ 0^00-24 (por. 38); ⫲^2 0^00-24
18	0	14.2	270	∗^1 0^00-40 ∗^0-5^40 ∗^1-8^30 ∗^0-1-24, v^0 0^00-24, ≡^2 0^00-24, ⇘ 0^00-24 (por. 36); ⫲^2 0^00-24
19	0	16.6	282	∗^1 0^00-1^45 ∗^0-2^30 5^45-13^10 ∗^1-16^15 ∗▲^0-19^10 ∗^0-23^10 ▲^0-24; v^0-1 0^00-24, ≡^2 0^00-24, ⇘ 0^00-1^30 (por. 23) ⪢-5^40 (por. 19), 7^15-8^30 (por. 17), 9^30-24 (por. 22), ⫲^2 0^00-1^30 ⫲^0-1-24
20	0	10.2	285	▲^0 0^00-40 ∗^0-3^45 8^45-10^40 ∗▲^0-11^30 ▲^0-16^30, v^1 0^00-na v^2 na-16^30 v^1-17^40 v^2-24, ≡^2 0^00-16^30 ⩸-17^40 ≡^2-24. ⪢ 0^00-5^40 (por. 22), 19^30-24 (por. 18); ⫲^1 0^00-5^40 ⫲^2-10^20, 17^10-19^30 ⫲^1-24; ⊛^2 16^20-45
21	0	25.8	290	▲^0 1^50-5^20 ∗^0-9^20 ∗^1-10^30 ∗^0-13^15 ∗^1-17^30 ∗^0-2-24; v^2 0^00-24, ≡^2 0^00-24; ⪢ 0^00-7^40 (por. 22), 8^30-9^15 (por. 15), 14^35-24 (por. 18); ⫲^1 0^00-40 ⫲^2-6^30 ⫲^1-10^20 ⫲^0-1 11^40-16^00 ⫲^1-24
22	7	1.1	305	∗^1-2 0^00-1^30 ∗^1-3^10 ∗^0-1-8^40 13^30 16^45, v^2 0^00 24; ≡^2 0^00-8^30 ⩸-10^15 ≡^2-12^20 ⩸-13^30 ≡^2-16^45 ⩸ ∞-21^25 ≡^2-22^15 ⩸ ∞-24; ⪢ 0^00-7^30 (por. 15), 10^40 13^30; ⫲^1 0^00-5^30 ⫲^0-1-21^30 ⫲^0... 24, ⊛^0 np-24
23	8	6.9	300	∗▲^0 12^15-13^30 ∗^0-1-24, v^2 0^00...45 v^0 13^10-24, ⩸ 0^00-45 ∞ 0^00-8^45 ≡^2 13^10-15^45 ⩸-16^10 ≡^2-24; ⫲^0 0^00-7^45 ⫲^0-11^30 ⫲^1-24, ⊛^0 0^00...40 7^10-8^00, ⊕ 10^45-11^30; () 8^30-11^30
24	5	0.5	304	∗^0 0^00-8^40 ▲^0 9^30 ... 12^10 ∗▲^0... 13^40 ∗^0... 14^15 ▲^0-18^42 20^21-21^15, v^0 0^00-7^45 15^00...17^30 ⊔^0 19^00-24, ≡^2 0^00-7^45 ⩸-12^05-17^30 ∞ p-22^30 (∞)-24, ⫲^0 0^00-7^30, ⊕ 14^20-16^15
25	1	1.5	299	▲^0 9^40-11^40 ∗^0-15^40 ∗▲^0-16^20 ▲^0-21^40, ⊔^0 0^00-7^30 v^0 11^40...16^40, (∞) 0^00-na ≡^2 11^40-15^30 ≡^1-16^40 ⩸-17^30, ⊕^0-1 7^25-9^30
26	9	0.3	297	∗^0 22^40-23^20; ⩸ 5^30-6^47 ∞-8^45 ⩸ 11^16-45, 15^40-18^15; ⪢ 11^20-13^00; ⫲^0 11^15-13^00 ⫲^0-15^30 ⫲^0 18^15-19^40
27	9	0.9	290	∗^0 0^15-2^45, 20^20-21^30, 22^45-24
28	5	1.0	282	∗^0 0^00-1^45, 2^30-6^30 ∗▲^0-7^30 ∗^0-1-8^30 ▲^0-9^15 ∗^0-19^40...21^52; v^0 5^45-16^00 v^1-2-21^40; ≡^2 5^45-12^13 ⩸-13^10 ≡^2-21^35 ⩸-21^42 ∞ 21^40-24; ⪢ 8^20-13^05; ⫲^0 7^30-14^00, 19^50...23^15 ⫲^0-24
29				
30				
31				
Σ	—	168.5	—	UWAGI.

Kasprowy Wierch φ=49°14' λ=19°59' Marzec - Mars 1962

Dni	Ciśnienie P=700 I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność względna U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	84.3	85.3	82.0	83.2	-8.0	-4.0	-8.0	-7.0	-3.1	-8.9	96	91	96	94	0.1	0.4	0.1	0.2	3	4 ⊙	9	SSW 4	C 0	C 0
2	80.2	80.2	81.1	80.5	-10.3	-8.9	-10.5	-10.1	-5.6	-11.2	87	95	87	90	0.4	0.2	0.4	0.3	1	3 ⊙	1	NE 3	SSW 4	WSW 5
3	81.9	82.8	82.5	82.4	-11.0	-9.3	-8.8	-9.5	-8.3	-12.2	93	95	95	94	0.2	0.2	0.2	0.2	10 ✳	10 ✳=	10✳△=	W 4	SW 8	S 11
4	79.3	77.0	78.4	78.2	-5.4	-3.2	-0.2	-2.2	0.0	-6.8	98	97	100	98	0.1	0.1	0.0	0.1	10 ✳△=	10 △=	10 △=	S 17	S 19	SSW12
5	81.3	80.5	78.6	80.1	0.4	1.2	0.9	0.8	1.9	-0.2	100	100	100	100	0.0	0.0	0.0	0.0	10 ●=	10 ●=	10 ●	SSW12	SW 18	S 19
6	77.7	83.4	86.2	82.4	-0.4	-2.7	-4.8	-3.2	1.0	-5.7	100	93	100	98	0.0	0.3	0.0	0.1	10△=	8 ⊙	10 ✳	WSW10	SSW 6	SSW 3
7	87.5	88.4	91.2	89.0	-14.8	-14.6	-16.4	-15.6	-4.4	-16.8	100	100	100	100	0.0	0.0	0.0	0.0	10✳=	10 ✳=	10✳=	NNE 8	N 12	NNE11
8	93.1	95.6	97.4	95.4	-18.1	-14.5	-12.1	-14.2	-12.1	-18.2	95	96	55	75	0.1	0.1	1.6	0.6	7	8 △	1	NNE14	NNE 6	NE 8
9	97.3	98.1	96.0	97.1	-9.6	-8.3	-7.8	-8.4	-7.2	-12.4	20	32	20	24	2.4	2.2	2.7	2.4	3 ⊙	4 ⊙	3	NE 3	SSW 6	SSW11
10	91.7	90.7	91.5	91.3	-7.6	-7.8	-6.5	-7.1	-5.2	-10.0	33	62	97	64	2.3	1.3	0.1	1.2	8	9	4	S 16	S 18	SSW12
11	90.3	89.2	86.8	88.8	-3.8	-4.1	-3.0	-3.5	-2.6	-6.5	96	96	97	96	0.2	0.2	0.1	0.2	10	10✳△=	9✳	SSW 7	SSW 9	SSE 2
12	81.7	78.4	75.6	78.6	-3.1	-1.6	-6.7	-4.5	-1.2	-7.0	97	98	96	97	0.1	0.1	0.1	0.1	10✳△=	10 ✳	10△=	SSE 5	SSE 1	WNW 4
13	76.8	79.0	83.7	79.8	-14.9	-15.6	-19.0	-17.1	-6.7	-19.1	96	100	95	97	0.1	0.0	0.1	0.1	10△=	9 ✳	10✳=	WNW11	NNW 9	NW 6
14	85.6	88.5	88.7	87.6	-19.1	-17.4	-18.9	-18.6	-15.8	-20.2	95	95	95	95	0.1	0.1	0.1	0.1	9	9 ⊙	10✳=	W 9	N 3	NNE 7
15	85.7	82.9	81.9	83.5	-19.6	-19.1	-20.2	-19.8	-18.9	-20.6	77	95	96	89	0.3	0.1	0.1	0.2	10	10✳△=	10✳△=	ENE15	ENE16	NE 17
16	79.7	81.0	81.1	80.6	-19.9	-19.0	-21.0	-20.2	-18.1	-21.2	95	95	96	95	0.1	0.1	0.0	0.1	10✳△=	10✳=	10✳=	NE 19	NNE19	NNE17
17	79.2	79.2	81.0	79.8	-21.7	-17.9	-19.7	-19.8	-16.9	-21.8	96	95	95	95	0.0	0.1	0.1	0.1	10✳=	10✳△=	10✳=	N 13	NNE10	NNE12
18	82.0	85.5	88.7	85.4	-18.3	-17.4	-16.5	-17.2	-16.2	-19.7	95	95	95	95	0.1	0.1	0.1	0.1	10✳=	8	10△	N 17	NNE17	NNE11
19	89.4	90.5	90.8	90.2	-17.9	-12.9	-15.1	-15.2	-11.9	-18.7	95	81	96	91	0.1	0.4	0.1	0.2	6 ⊙	8 ✳	10✳=	E 1	SSW 2	C 0
20	90.6	91.4	90.6	90.9	-16.9	-11.0	-15.1	-14.5	-10.9	-17.2	95	86	96	92	0.1	0.4	0.1	0.2	9	9 ✳	7✳	C 0	SW 2	SW 3
21	87.6	86.5	85.5	86.5	-10.6	-10.3	-9.8	-10.1	-6.9	-16.2	55	75	56	62	1.3	0.7	1.3	1.1	1 ⊙	7 ⊙	10	S 2	SSW 8	C 0
22	82.3	82.1	81.3	81.9	-9.2	-6.9	-8.3	-8.2	-5.2	-10.5	95	96	95	95	0.2	0.1	0.2	0.2	10 ✳	10✳△=	10✳△	SSE 4	C 0	C 0
23	80.5	81.1	82.7	81.4	-6.9	-7.7	-9.2	-8.2	-5.3	-9.9	96	99	95	97	0.1	0.0	0.2	0.1	10 ✳	10✳△=	10✳=	C 0	SSW 6	SSW 3
24	85.5	88.4	91.3	88.4	-10.6	-9.2	-11.3	-10.6	-8.2	-11.6	94	95	93	94	0.2	0.2	0.2	0.2	10✳=	9	10✳=	SSW 4	WSW 6	SW 4
25	92.2	91.8	89.4	91.1	-12.6	-11.4	-13.7	-12.8	-10.6	-14.0	58	93	67	73	1.0	0.2	0.7	0.6	9	9	7	NNE 5	NNE 7	NNE10
26	86.8	86.6	85.3	86.2	-13.5	-11.5	-11.5	-12.0	-10.0	-15.6	45	93	93	77	1.2	0.2	0.2	0.5	5 ⊙	3 ⊙	1	NE 7	ENE 2	C 0
27	82.4	82.5	82.8	82.6	-12.1	-9.4	-9.5	-10.1	-7.7	-13.3	93	72	98	88	0.2	1.2	0.1	0.5	9 ⊙	9 ⊙	8	NNE 1	WNW 4	SSW 8
28	82.4	83.0	85.0	83.5	-9.0	-7.0	-8.8	-8.4	-6.3	-9.8	95	96	95	95	0.2	0.1	0.2	0.2	7 ⊙	10 ✳=	10✳=	SSW 5	WSW 4	WNW 2
29	86.1	86.4	84.0	85.5	-10.3	-7.7	-6.6	-7.8	-6.3	-10.7	94	90	97	94	0.2	0.3	0.1	0.2	9 ✳	9	10=	NW 3	SW 7	SSW14
30	83.1	84.6	81.8	83.2	-3.1	-1.1	-0.8	-1.4	-0.5	-6.6	97	99	99	98	0.1	0.1	0.0	0.1	10△=	8	10=	SW 11	SW 13	S 16
31	80.0	81.2	82.2	81.1	-0.3	0.3	-0.1	0.0	0.8	-0.9	100	98	100	99	0.0	0.1	0.0	0.0	9	9	10	SW 12	SW 9	SSW 7
M	84.7	85.2	85.3	85.3	-10.9	-9.4	-10.3	-10.2	-7.4	-12.8	86	90	90	89	0.4	0.3	0.3	0.3	8.2	8.5	8.4	7.7	8.2	7.5

Kwiecień - Avril

1	83.6	86.9	89.9	86.8	-5.9	-7.4	-9.2	-7.9	0.1	-9.3	97	96	95	96	0.1	0.1	0.2	0.1	10✳=	10✳	4	N 8	WNW 8	WNW 8
2	90.0	91.3	93.4	91.6	-8.4	-6.8	-7.2	-7.4	-5.9	-9.6	86	96	88	90	0.4	0.1	0.4	0.3	7 ⊙	7✳⊙	4	WSW 7	WSW 6	W 8
3	94.8	94.5	92.1	93.8	-7.1	-4.6	-5.0	-5.4	-3.6	-10.3	88	91	98	92	0.4	0.4	0.1	0.3	2 ⊙	4 ⊙	1	WSW 5	SSW13	S 16
4	86.1	85.3	81.3	84.2	-4.0	-2.5	-2.6	-2.9	-1.5	-6.3	79	89	98	89	0.9	0.6	0.1	0.5	4 ⊙	10	10✳△=	S 19	SSE16	SSE19
5	73.0	73.8	75.6	74.1	-1.5	-2.5	-4.1	-3.0	-0.8	-4.4	99	98	96	98	0.1	0.1	0.2	0.1	10✳△=	10✳=	10✳=	SSE15	SSW 4	C 0
6	75.4	76.9	79.9	77.4	-4.7	-5.4	-6.3	-5.7	-4.0	-6.6	98	98	97	98	0.1	0.1	0.1	0.1	10✳=	10✳=	10✳=	NNE 6	NNE 5	N 6
7	83.2	86.9	89.8	86.6	-6.6	-9.4	-10.1	-9.0	-5.5	-10.8	97	95	94	95	0.1	0.2	0.2	0.2	10✳=	10✳△=9		N 11	N 11	NNW10
8	90.3	92.5	92.5	91.8	-4.6	-2.6	-3.0	-3.3	-1.8	-11.0	96	98	97	97	0.2	0.1	0.1	0.1	10	10	10=	N 10	W 9	SSW14
9	93.2	94.4	94.9	94.2	-3.2	-0.1	-3.1	-2.4	0.6	-4.0	83	88	97	89	0.8	0.3	0.1	0.6	2 ⊙	8	10=	S 5	SSW 1	SSW 4
10	95.8	97.1	98.3	97.1	-3.7	-2.3	-2.3	-2.6	-1.1	-4.6	97	100	96	98	0.2	0.0	0.3	0.2	10 ✳	10 ✳=	10	S 2	S 3	SE 3
11	98.0	98.1	98.9	98.3	-1.2	-0.2	-0.8	-0.8	0.7	-2.7	95	84	85	88	0.3	1.0	0.9	0.7	9	9	9	SE 4	SSE 8	C 0
12	97.8	97.6	97.0	97.5	-0.6	2.2	-0.7	0.0	3.4	-1.7	76	87	87	83	1.5	1.0	0.8	1.1	4 ⊙	9	7	ENE 1	C 0	SW 1
13	94.3	92.7	90.4	92.5	-0.5	-0.7	-2.5	-1.6	1.4	-2.9	78	99	98	92	1.4	0.0	0.1	0.5	4 ⊙	10=	10◑△=	SE 1	NNE 2	N 3
14	90.4	93.6	96.4	93.5	-6.2	-1.8	-4.3	-4.2	-0.8	-6.5	97	100	98	98	0.1	0.0	0.1	0.1	10△=	10=	10=	NNE 4	C 0	NNE 5
15	96.7	98.0	99.0	97.9	-2.9	-0.1	0.5	-0.5	1.0	-4.9	99	100	92	97	0.0	0.0	0.5	0.2	10✳=	10△=	7	ENE 6	ESE 3	E 13
16	98.7	101.0	103.3	101.0	1.4	1.7	2.0	1.8	3.3	-0.7	79	88	68	78	1.5	0.8	2.3	1.5	8 ⊙	9	5	SSE 7	SE 9	SSE 9
17	104.2	105.2	103.9	104.4	1.7	2.8	2.6	2.4	3.4	-0.1	73	68	61	67	1.8	2.4	3.0	2.4	5 ⊙	8 ⊙	8	SSE 9	SSE 8	SSE14
18	103.3	102.8	102.7	102.9	1.6	2.7	3.0	2.6	4.2	1.4	79	78	71	76	1.5	1.6	2.2	1.8	10	10	10	S 16	SSW16	S 14
19	102.5	103.7	103.8	103.3	2.0	4.4	4.5	3.8	6.3	1.3	81	73	68	74	1.4	2.3	2.7	2.1	9 ⊙	9 ⊙	3	SSW12	SSW 9	S 3
20	103.8	105.0	104.7	104.5	5.8	6.9	6.5	6.4	8.1	3.3	74	50	61	62	2.4	5.0	3.8	3.7	2 ⊙	5 ⊙	9	C 0	SSE 3	S 1
21	105.0	105.9	105.9	105.6	5.7	9.3	7.6	7.6	11.8	3.1	66	54	50	57	3.1	5.4	5.2	4.6	8 ⊙	5 ⊙	3	ENE 1	C 0	C 0
22	105.1	105.9	106.0	105.7	6.7	9.2	8.7	8.3	12.6	5.2	46	39	45	43	5.2	7.1	6.2	6.2	3 ⊙	5 ⊙	3	ESE 1	SSE 1	WNW 1
23	105.7	106.5	106.2	106.1	8.5	11.8	9.0	9.6	14.2	6.9	52	50	50	51	5.4	6.9	5.8	6.0	0 ⊙	2 ⊙	1	C 0	NNE 3	S 3
24	107.0	108.4	108.7	108.0	6.9	9.9	6.6	7.5	12.2	5.8	63	48	61	57	3.7	6.4	3.8	4.6	2 ⊙	5 ⊙	2	NNE 3	ENE 3	ESE 4
25	109.1	110.2	109.2	109.5	7.2	11.2	6.6	7.9	12.3	5.7	54	43	72	56	4.7	7.5	2.6	4.9	1 ⊙	4 ⊙	2	ENE 5	ENE 4	ENE 2
26	106.9	105.0	101.0	104.3	4.6	7.9	6.5	6.4	9.5	3.9	79	42	47	56	1.7	6.2	3.1	4.3	1 ⊙	1 ⊙	1	NNE 4	N 3	SW 4
27	93.7	92.1	90.5	92.1	3.4	-1.0	-4.7	-1.8	7.3	-4.8	86	99	98	94	1.1	0.1	0.1	0.4	9	10=	10△=	SW 5	N 6	N 9
28	86.3	84.0	83.9	84.7	-6.3	-6.7	-6.3	-6.4	-4.6	-7.6	97	96	97	97	0.1	0.1	0.1	0.1	10	9	10✳△=	WSW 8	WNW 8	N 4
29	84.4	85.5	86.7	85.5	-8.0	-4.8	-8.3	-7.4	-4.2	-8.5	96	98	95	96	0.1	0.1	0.2	0.1	10✳=	10✳△=	4	NNE 6	N 3	NW 2
30	84.6	85.5	87.2	85.8	-7.5	-6.0	-7.8	-7.3	-4.1	-9.0	93	97	96	95	0.2	0.1	0.1	0.1	7 ⊙	10✳△=	10△=	NNE 1	N 4	NNW 7
31																								
M	94.8	95.5	95.8	95.4	-0.9	0.5	-0.8	-0.5	2.5	-2.9	83	81	82	82	1.4	1.9	1.6	1.6	6.6	8.0	6.7	6.1	5.6	6.3

Kasprowy Wierch $H_s = 1991m$ $H_n = 1988{,}8m$ $h_w = 15{,}4m$ Marzec - Mars 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBŚNIEGU h	POGODA
1	9	.	273	v°13¹⁰ 18⁴⁰; ♏ 0⁰⁰⁻³⁰(♏)-3³⁰ ♏ -12¹⁰ = -12³⁰ ♏ -13¹⁰ = -16²⁰ ♏ -16⁴⁵ = -18⁴⁰ ♏ -24; ⚸°0⁰⁰-1⁴⁰; ()6¹⁰-8³⁰ ⦶ 10⁴⁰-11²⁰; ☠' 16⁰⁵⁻⁴⁵
2	9	0.4	268	v°2³⁰ 3⁴⁰ 13¹⁵ 20¹⁵; ♏ 0⁰⁰-2²⁰ = -3⁴⁰ ♏ -13¹⁵ = 11¹⁵-13¹⁵ ≡² -13⁴⁵ = -14¹⁵ ≡² 16²⁰ = -20¹⁵ ♏ 16²⁰-19³⁰; ()5³⁰-13¹⁵ 16²⁰-24
3	1	5.7	265	*°1²⁰-6¹⁵ 6³⁰-13³⁰ *♎°-24, v°0¹⁵-6¹⁰ 8³⁰-24, = 0¹⁰-2¹⁵ = -6¹⁰ = 7⁴⁰-8⁴⁵ ≡² -24; ≫14³⁵-15⁴⁵ (por.15) 16¹⁵-24 (por.20); ⚸°10³⁰-19¹⁵ ⚸⁻¹-24; ()0⁰⁰⁻³⁰
4	0	17.3	262	*♎°0⁰⁰-12¹⁰ ♎°-22⁴⁰ ✱°-23¹⁰ •°-24, v°0⁰⁰-1³⁰ v'-13²⁰ v°-22⁵⁰ ≡² 0⁰⁰-24; ≫0⁰⁰-6²⁰ (por.26) ⚹-19³⁰ (por.34) ≫-23⁴⁰ (por.33) ⚹-24 (por.32); ⚸°0⁰⁰-6²⁰ ⚸² -20¹⁰ ⚸⁻¹-22²⁰
5	0	10.9	253	•°0⁰⁰-5¹⁰ 8¹⁰-14¹⁵ 20⁰⁰-24, ≡² 0⁰⁰-13¹⁰ = -13⁴⁴ ≡² -20¹⁰ = -21⁰⁰ ≡² -24; ⚹ 0⁰⁰-2²⁰ (por.38) ≫-5⁴⁰ (por.26) 6²⁰-8³⁰ (por.29) ⚹-24 (por.36)
6	9	4.4	204	•°0⁰⁰-1⁰⁵ ✱°-1⁴⁰ *♎°⁻¹-3¹⁰ ✱°-5⁴⁵ ♎°-8⁴⁴ *°14⁵⁰-16⁴⁰ ♎°20²⁰-21¹⁵ 23¹⁵-24, v°3⁰⁰ 11²⁰ 15²⁵-24, ≡°0⁰⁰-10²⁰ ♏ -15²⁵ = -11²⁰ ≡² 15²⁵-16⁴⁰ = ♏ -18³⁰ ≡² -24; ⚹ 0⁰⁰⁻⁴⁰ (por.26) ≫-8¹⁵ (por.24); ()
7	0	24.9	205	♎°0⁰⁰⁻¹⁵ *°11⁰-6¹⁰ *-6⁴⁰ *°-7¹⁵ *'-14⁴⁰ *°⁻¹-24, v°0⁰⁰-na v°⁻¹-24; ≡² 0⁰⁰-24; ≫11³⁰-24, ⚸°-1 6⁰⁰-24 [6.III: 10²⁰-15²⁵
8	6	1.2	213	*°'0⁰⁰-3⁴⁰ ♎°11⁵³ 13²⁰ *♎° 14⁵⁰ v°⁻¹0⁰⁰-2⁴⁵ 11⁴⁰-15¹⁰; ≫0⁰⁰-11³⁰ (por.21) 17⁵⁰-19⁴⁰ ⚸°0⁰⁰-9³⁰ ⚸°-24, ☠°⁻¹ a. 14⁴⁰; ()16⁵⁰-24
9	9	.	201	≫19³⁰-24 (por.21); ⚸°0⁰⁰ 5¹⁰ ⚸² 12¹⁰ 13¹⁵ ⚸°-24; ⦶ 14³⁵-15²⁰ ⚲ 20⁰⁰-21¹⁵; ()0⁰⁰-18³⁰; 20¹⁰-24
10	9	.	195	v°16²⁰ 19¹⁵, ≡² 16²⁰-18³⁰ = -19¹⁵, ≫0⁰⁰-20 (por.23) ⚹-19³⁰ (por.39) ≫-24; ⚸°⁻¹0⁰⁰-1⁰⁰ ⚸'-6⁰⁰ ⚸⁻² 20³⁰ ⚸°-22³⁰; ()0⁰⁰-2³⁰; 5⁰⁰-12³⁰
11	0	3.6	190	*♎°10³⁵-20¹⁵, *° 24, v°⁻¹8⁴⁵-22⁴⁰ = 7⁴⁰-8⁴⁵ ≡² -20³⁵ = -22⁴⁰ 23¹⁵-24; ≫0⁰⁰-4¹⁰ 14¹⁵-15³⁰ ⚸°10³⁵-17³⁰
12	5	8.3	192	*°0⁰⁰⁻⁴⁰ 1¹⁵-5²⁰ *♎°-9¹⁰ *°⁻¹14²⁵ *♎°-17³⁰ ♎°-24, v°⁻¹1⁰⁰-9²⁰ v°15¹⁵-24; = 0⁰⁰-1¹⁰ ≡² -6⁵⁰ = -11¹⁵; 15¹⁵-²⁵ ≡² -24; ≫21¹⁵-24 (por.23); ⚸°⁻¹20⁵⁰-24
13	5	7.0	193	♎°0⁰⁰-6⁵⁰ *♎°-10²⁰ *°⁻¹23³⁵ v°0⁰⁰-23⁴⁰, ≡² 0⁰⁰-7⁴⁰ = -19¹⁵ ≡² -23²⁰ = -23⁴⁰ ♏ -24, ≫0⁰⁰-2⁴⁰ (por.23) 6¹⁵-8¹⁵ (por.17); 11⁰⁵-12¹⁰ (por.15); ⚸°⁻¹0⁰⁰-21⁴⁵
14	9	0.0	196	*°15³⁵-16⁵⁰ 20¹⁵-21³⁰, v°15³⁰-23³⁰, ♏ 0⁰⁰-1³⁰ (♏) -5⁰⁰ ♏ -8²⁵ = 15¹⁰⁻⁴⁰ ≡² -23¹⁰ = -23³⁰; ≫2¹⁰-6³⁰ (por.17) 23⁴⁰-24; ⦶ °7¹⁵ p
15	1	2.6	191	*♎°9⁴⁵-24; v°10²⁰-24, ≡² 10²⁰-24; ≫0⁰⁰-11¹⁰ (por.24) ⚹-16³⁰ ≫-17¹⁰ ⚹-24 (por.25); ⚸°⁻¹0⁰⁰ 11¹⁰ ⚸² -24; ()8⁰⁰-9³⁰
16	1	17.0	198	*♎°0⁰⁰-11³⁰ *°-24, v°0⁰⁰-24, ≡² 0⁰⁰-24; ⚹ 0⁰⁰-24 (por.30); ⚸² 0⁰⁰-24
17	1	18.6	200	*°0⁰⁰-10¹⁵ *♎°-13²⁰ *°⁻¹-24; v°0⁰⁰-24, ≡² 0⁰⁰-24; ⚹ 0⁰⁰-5⁴⁰ ≫-11⁴⁵ 12²⁰-13⁰⁵ 16⁴⁰-24; ⚸² 0⁰⁰-5³⁰ ⚸'-10⁴⁰ ⚸°⁻¹-24
18	8	6.3	209	*°⁻¹0⁰⁰-10²⁰ *♎°-11⁵⁰ ♎°16⁵⁰-24; v°0⁰⁰-11⁴⁵ 15⁴⁰-24, ≡² 0⁰⁰-11¹⁵ = -11⁴⁵ 15⁴⁰-21⁴⁰ ≡² -22²⁰ = -24; ≫0⁰⁰-6⁰⁵ ⚹-11³⁰ ≫-12²⁵ ⚹-13²⁰ ≫-22⁴⁵; ⚸°⁻¹0⁰⁰-5⁰⁰ ⚸'⁻²-23⁴⁵
19	8	0.5	213	♎°0⁰⁰-1⁵⁵ *°11³⁵⁻⁴⁵; 12²⁵-14³⁰ *°⁻¹16³⁵ *°18⁴⁰-24, v°0⁰⁰-5⁴⁰; 6¹⁰⁻³⁰ 17³⁵-23³⁰, = 0⁰⁰-5⁴⁰; 6¹⁰⁻³⁰ ♏ 5¹⁰-8⁰⁰ = 12⁴⁵-17³⁵ ≡² -21⁴⁵ = -23³⁰
20	6	0.2	212	*°0⁰⁰-4³⁰; 10³⁰ 16¹⁰-19³⁰ 20³⁰-24, v°1⁴⁵-3³⁰ 18¹⁰-19³⁵ = 1⁴⁵-2⁴⁰ ≡² 3⁴⁵ = -5³⁰; 18¹⁰-19³⁵ ⦶ 6⁵⁰-7³⁵
21	9	1.4	210	*°0⁰⁰-1¹⁰ 23⁵⁰-24; ≫9²⁰⁻⁴⁵; ⚸°8⁴⁵-10⁴⁵ ⦶ 10⁰⁰-p, () 11⁰⁰-14⁰⁰
22	0	4.1	210	*°0⁰⁰-9⁴⁰ *♎°-15³⁰ ♎°-17³⁰ ♎♎°-21¹⁵ *°⁻¹-24; v°7⁰⁰⁻⁴⁵ = 7⁰⁰⁻⁴⁵ ≡² 12²⁰-16⁰⁷; 18¹⁵-19¹⁰ 21⁴⁵-23⁴⁰
23	0	4.1	214	*°⁻¹0⁰⁰-8³⁰ ♎°-12¹⁵ *♎°-16²⁰ *°-24; v°10⁰⁰ 12¹⁵-24, = 9¹⁰-10²⁰ ≡² -1¹⁰ = -12¹⁵ ≡² -24; ⚸°22⁴⁰-24 ⦶ °1⁸³⁵-10²⁰
24	4	0.1	216	*°0⁰⁰-8⁵⁰ 12⁵⁰-13⁵⁰ 17²⁰-20⁵⁰ v°0⁰⁰-5⁰⁰ v'-7³⁰ v°9³⁰ 23²⁰, ≡² 0⁰⁰-7¹⁵ = ♏ -9³⁰ ≡² -11²⁰ = -14³⁰ ≡² -23²⁰ = ♏ -24; ⚸°0⁰⁰ 6²⁰
25	9	0.8	215	♎°8⁵⁵ 12⁰⁰ v°11⁴⁰-12¹⁵ 14⁴⁰-15⁰⁵, = 0⁰⁰-2¹⁵ ♏ 0⁰⁰-5¹⁵ (♏) -11⁴⁰ = -12¹⁵, 14⁴⁰-15⁰⁵; ≫18⁰⁵-23³⁵ (por.15); ⚸°16³⁰-24; ⦶ °16²⁰-17³⁰ ⚲ '22⁵⁰-24; ()8⁵⁰-11³⁰; 12¹⁵-20¹⁰
26	9	1.0	209	♏ 15⁴⁰-20³⁰; ⚸°0⁰⁰-7⁴⁰, ⚲ 0⁰⁰-2¹⁰ ⦶ °7⁴⁰-8²⁰ ☠ 15⁴⁰-16³⁵; ()5³⁰-13⁴⁰
27	9	0.5	205	*°4⁴⁵-6³⁰, 21³⁵-24; ⌣ 18³⁰-22⁰⁰ ⌣ v°-24, ⦶ °1⁻²6²⁰-15²⁵
28	0	2.3	203	*°0⁰⁰ 5⁴⁵ *♎°10⁴⁰-11¹⁵ *°-13¹⁰ *♎°⁻¹-16³⁵ *°19⁵⁰-23⁴⁰ ♎°24, ⌣ v°0⁰⁰; 1¹⁰ v°4³⁰, 7⁴⁶-24; = 1¹⁰-4³⁰, 7⁴⁶-12²⁵ ≡² 16⁴⁵ = -19⁵ ≡² -24; ⚸°10²⁰-11²⁰ 12²⁰-4⁵; 17⁴⁵-18¹⁰; ☠°⁻¹ 7⁴⁶-9⁴⁰
29	7	0.2	205	♎°0⁰⁰⁻¹⁵ *°3⁴⁰ 6¹⁵ 11⁴⁰ 13⁵⁰ 14²⁰, v°0⁰⁰-5⁵⁰, 17⁴⁰-24; ≡² 0⁰⁰-2⁴⁰ = -5⁵⁰ 8³⁰-12¹⁰ ≡² 17⁴⁰-24; ≫15⁰⁰-24 (por.19); ⚸'-1 5⁰⁰-24; ⦶ 11³⁰ p
30	8	2.0	202	♎°⁻²6³⁶-7⁰⁵ ♎°10⁴⁰-12²⁰; v°0⁰⁰-na v'-8⁰⁰ 9¹⁵, 12¹⁰ 15³⁰-24; ≡² 0⁴⁰-7⁴⁵ = -9¹⁵ ≡² -12¹⁰ 15³⁰-24; ≫0⁰⁰-17³⁰ ⚹-21⁴⁰ ≫-24; ⚸'0⁰⁰-6⁰⁰ ⚸°⁻¹ 9³⁰ 10⁴⁰-24
31	9	1.7	198	♎°2²⁵-5³⁵ ✱°10⁴⁴-11⁵⁴, v'0⁰⁰-5³⁰ 7⁵⁰-a; ≡² 0⁰⁰-5³⁰ = -7⁵⁰ ≡² -8¹⁵ = -9³⁰ ≡² -11¹² = -11²⁰ 13¹⁵-17⁴⁰ ≡² -18¹⁰ = -18⁴⁰; 20²¹-21²⁰ ≡² 24; ≫0⁰⁰ 14²⁶ (por.22), 21¹⁰-24 (por.19); ⚸°0⁰⁰-9³⁰
Σ	—	146.1	—	UWAGI

Kwiecień - Avril

1	6	1.8	191	*°0¹⁵-1¹⁴ ♎°⁻¹2²² *°-2⁴⁵ *°3⁴⁰-6⁰⁵ ♎°⁻¹-7⁴⁶ ♎°9⁴⁰-10³⁰ *♎°11⁴⁰-12⁰⁰-13⁴⁰, v°1⁰-2⁴⁰ 3⁴⁵-4¹⁵ v°⁻¹13⁴⁵ ≡² 0⁰⁰-2²⁰ = -2⁴⁰ 3⁴⁵-4¹⁵ ≡² 11⁴⁵ = -13⁴⁵ ≡² 0⁰⁰-2²⁰ 3⁴⁵-4¹⁵ ≡² -11⁴⁵ = -13⁴⁵ ⚸°⁻¹1¹⁰-4⁵⁰ 12³⁰-13⁵⁰ 15²⁰-24, ≫0⁰⁰⁻⁴⁰
2	9	1.6	188	♎°⁻²9⁰⁵ 16²⁰ ♎°22⁵⁵-3⁵ *°-23¹⁵, v°21²⁰ 23¹⁵, = 12⁰⁰ 15⁴⁵ ≡² 21²⁰ 22²⁰ = -23¹⁵; ≫0⁰⁰-4⁰⁵ (por.22) 21²⁵-22⁰⁰ ⚸°0⁰⁰-5¹⁵ 7⁵⁰ 9¹⁵ 21²⁰ 22¹⁵ 23³⁰-24; ()6¹⁰-12⁰⁰
3	9	.	188	= 17²⁰ 20²⁰ ≫10³⁰-18³⁰ ⚹-24 (por.30); ⚸°0⁰⁰-3⁰⁰ 10¹⁵-12¹⁰ ⚸'⁻²-24; ()8³⁰-17¹⁵ [1.IV. (por.15) 1¹²-4³⁵ (por.23) 18¹⁰⁻³⁰ (por.20) 19²⁰-20¹⁵ (por.25) 21¹⁰-24 (por.22); ☠ 1'' na
4	9	4.4	182	♎°16⁵³-17²⁰ *♎°23¹⁵ ♎°24, v°3⁴⁵-4²⁰ 15¹⁵⁻⁴⁰ 16³⁰-24, ≡² 3⁴⁵-4²⁰ = 15¹⁵⁻⁴⁰ 16³⁰-18¹⁰ ≡² -22⁴⁰ = -24; ⚹ 0⁰⁰-14³⁰ (por.36) ≫-18³⁰ (por.31) ⚹-19⁰⁵ (por.28) ≫20¹⁰ ⚹-22³⁵ (por.34) ≫-24 (por.35); ⚸°0⁰⁰-24 () 4²⁰-13⁴⁰
5	1	19.3	170	♎°0⁰⁰-2¹⁰ 4¹⁵ ♎°⁻¹5³⁰ ♎°⁻¹11³⁰ *°13⁴⁰ *♎°14¹⁵ ♎°16²⁰ *°17⁵⁰ 19⁴⁹ 21³⁵ 23³⁰ 24, v°0⁰⁰-2³⁰ 4¹⁵ 24, = 0⁰⁰-1²⁰ 4¹⁵-3⁵ ≡² -5³⁰ = -6¹⁵ ≡² -17⁴⁴ = -19²⁵ ♏ 17⁴⁴ p = 20¹²⁻²⁷ ≡² -21²⁰ = 22⁴⁰-23⁴⁰ ≡² -24 ♏ np.
6	0	70.5	175	*°0⁰⁰ 2¹⁰ 4²⁰-5²⁰ *°-8³⁰ *°-12⁰⁰ *'-24; v°⁻¹0⁰⁰ 24, = 0⁰⁰-1⁵ = -1⁴⁰ ♏ 0⁰⁰ 1⁴⁰ ≡² -24; ⚸°7⁰⁰-8³⁰ 22³⁰-23⁰⁰ ⚸'-24
7	0	23.0	220	*'0⁰⁰-8¹⁵ *°-11³⁰ *♎°⁻¹-17¹⁰ *°-20²⁵ 22⁴⁵ 23³⁰, v'0⁰⁰-17¹⁰, ≡² 0⁰⁰-17¹⁰ = -24; ≫0⁴⁵-24 (por.19); ⚸°0⁰⁰-24 [5.IV: 24; ≫0⁰⁰⁻³⁰ (por.37) ⚹-6⁰⁵ (por.37) ≫-11¹⁵; ⚸°⁻¹0⁰⁰-12¹⁰; ☠°⁻¹ 12¹⁹⁻⁴³
8	7	.	232	*°0⁻⁴⁰ 1³⁰; 2⁴⁵-4³⁰, v°0³⁰ 5¹⁰ a. 13¹⁵ 14³⁸ 24; = 0⁰⁰-3⁰ ≡² 1¹⁵ = -4³⁰ ≡² 5³⁰ = -7³⁰ 9¹⁰ 13¹⁵ ♏ 14⁰⁰⁻⁴⁴ = 14³⁸ 15¹⁰ ≡² 16²⁵ = -20⁰⁰ ≡² -22³⁰ = -24; ≫0⁰⁰ 10⁰⁰ (por.18) 12¹⁵ (por.15) 16⁴⁰-18⁰⁴ (por.21) ⚹-
9	9	0.2	229	♎°16¹⁵ 18³⁰, v°0⁰⁰⁻⁴⁰ 15²⁰⁻⁴⁵ 16³⁰-17⁴⁰ 18⁴⁰-24, = 0⁰⁰-4⁰ 15²⁰⁻⁴⁵; 16³⁰-17⁴⁰ 18⁴⁰-20¹⁰ ≡² -23³⁰ = ♏ -24; ≫0⁰⁰-5³⁰ (por.21); ⚸°⁻¹0⁶⁰-4¹⁵; ()7²⁰-11³⁰
10	0	7.5	221	*°5⁵⁰ 6¹⁰ *♎° 8³⁰ *°18²⁰ 21⁵⁰ 23⁴⁰ *♎°24, v°0⁰⁰-1⁵ 5¹⁰ a. 21⁴⁵-24, = 0⁰⁰-1⁵ ♏ 0⁰⁰-7¹⁵ ≡² 5³⁰-8⁵⁰ ≡² -17¹⁵ ≡² 21⁴⁵-24 ♏ 17¹⁵-21⁴⁵
11	8	0.0	225	*♎°0⁰⁰-2⁰ 1⁵⁵ 2¹⁰ 4⁵⁰ 5²⁰ *°7⁰⁰⁻¹⁶ 11⁴³-12¹⁵, v°0⁰⁰ 5²⁰ ≡² 0⁰⁰-2¹⁵ = -4³⁰ ≡² 5²⁰ ♏ 21⁵-24, ☠'0⁰⁰-2¹⁵ [8.IV: 20¹⁵ ≫-24 (por.22); ⚸°0⁰⁰-9¹⁵ ⚸²-13⁴⁰; 16²⁵-17²⁰ ⚸°⁻¹-24; ⦶ °14¹⁰⁻⁴⁴
12	7	0.0	215	♎°16⁴⁴-17²⁵ ⌣ 19⁴⁰-24, ♏ 0⁰⁰-13⁴⁰ = 12¹¹-13⁴⁰ ≡² -16²⁵ = -18³⁵ ⦶ °12⁰⁹ 13¹⁵
13	0	6.3	207	*°11⁵³ 12¹⁰ 16⁵⁰-17⁰⁵ ♎°17¹⁰ 18⁴⁰-19⁴⁰ ♎°20³⁰ *♎°-21²⁰ ⚹ ♎°23⁴⁰ ♎°24, ⌣ 0⁰⁰-6⁰⁰ v°11¹⁵-12¹⁵ 17⁴⁰-24; ~°⁻¹20³⁰-24⁴⁰, = 9⁴⁵-11¹⁵ ≡² -13¹⁰ = -13⁴⁰ ≡² -24
14	0	3.4	203	♎°0⁰⁰-1⁴⁵ *♎°-4¹⁰ ♎°-8¹⁵; v°⁻¹0⁰⁰-10⁰⁰ 18³⁰-24; ≡² 0⁰⁰-10⁰⁰ = -10⁴⁵ ≡² -14⁴⁰ = -15³⁰ ≡² -16³⁰ ♏ -18³⁰ ≡² -24
15	0	0.2	201	*°3¹⁵ 11³⁵ ♎°-13¹⁵; v'0⁰⁰-9⁵⁰, ≡² 0⁰⁰-9⁵⁰ 11³⁰-13¹⁵ = -14⁴⁰ ≡² -15²⁵ = -16¹⁰, 17²⁰-20¹⁵; ≫18¹⁰-21⁴⁵ (por.20), 23³⁰-24
16	8	0.0	192	♎°16¹⁷⁻⁴³; = 7³⁵-8⁴⁰ 9²⁰⁻³⁵; ≫0⁰⁰⁻⁴⁵ (por.16), 14⁴⁰...24 (por. do 22)
17	9	.	187	≫0⁰⁰ 8²⁰ (por. do 21), 9⁴⁰-12¹⁰ (por.23), 16¹⁰-24 (por.28); ⚲°2¹⁰-3³⁰ ⌣ °20²⁰-23¹⁰, () 3³⁰-12³⁰
18	9	.	169	≫0⁰⁰-1¹⁰ (por.25) ⚹-8¹⁰ (por.27) ≫-11¹⁵ (por.24) ⚹...13¹⁰ (por.23) ≫-22²⁰ (por.22) ⚹-24 (por.20); ⌣ °0³⁰-2¹⁰ ⦶ °12¹⁰-13¹⁵ ⌣ °-°20⁰⁰-24
19	9	.	155	⚹ 0⁰⁰-5⁰⁵ (por.22) ≫-9³⁰; ⌣ °⁻¹0⁰⁰-2³⁰; () 8³⁰-13⁴⁵
20	9	.	148	⦶' p ⚲² p -23⁰⁰
21	8	.	140	
22	9	.	131	
23	9	.	123	
24	8	.	115	
25	8	0.0	105	•°14³⁰⁻⁵⁶; ☠°20²⁵-22¹⁵ SSW
26	8	0.6	99	⌣ °2³⁰-5²⁰
27	0	12.9	92	•°2⁵⁰ 3¹⁰ 8⁴⁵-9²⁰ *°9⁴⁰ *♎°-10¹⁵ *°-2 11⁰⁶ *°-11³⁵ ♎° 13⁴⁰ 14¹⁵ *♎°-15³⁰ ♎°⁻¹-16⁴⁵ 18⁴⁰ 24, = 8⁰⁰-3⁰ ≡² -24; ⚸°19³⁰-24; ☠°9¹⁵-10³⁰
28	7	15.3	96	♎°0⁰⁰ 2³⁰ *°-7³⁵ 9⁵⁰ 10²² 11¹⁶ *♎°-11³⁹ *°-12³⁰ *°13¹⁰ 14⁴³ 15²¹ 18³⁰ ♎° 20¹⁰ *°21²⁰ ♎° 22³⁰ *°23⁴⁵ ♎° 24, v°0⁰⁰-3⁴⁰ ⚹°7¹⁰ 12³⁴ 13³⁵ 15³⁵ ⚹°21⁰⁰ ⚹' 24, = 0⁰⁰-2⁴⁵ = -3⁴⁰ 7³⁰ 8⁴⁰ 9¹⁰ 11¹⁵ ≡² 12²⁰ = -12²⁴ ≡² 13¹⁵ 14³⁵ = -15³⁵ ≡² 24
29	1	7.0	107	♎°0⁰⁰-1⁴⁵ *♎°2¹⁵ *°4⁰⁵ *♎°6⁰⁰ *♎°6¹⁰ *°7¹⁵ *♎°8³⁰ *°12³⁰ *♎°-13³⁰ *°16⁵⁰; v°0⁰⁰ 2⁰⁰ ⚹°7³⁰ ⚹°18³⁰ ⌣ °22³⁰ 24, = 0⁰⁰-14³⁰ = -15³⁰ ≡² -17³⁰ = -18³⁰; ⚸°4⁰⁰ 6³⁰, ☠°9³⁰ 10²⁰
30	0	25.3	120	♎°4⁴⁵ 5⁴⁰ ♎°6⁴⁰ 9⁴⁰ *°10⁴⁰ *♎°12²⁰ *°15⁴⁰ *°16⁴⁰ *°17⁴⁰ *♎°20⁴⁰ ♎°22⁴⁰ 24, ⌣ °0⁴⁰ 4³⁰ v°6³⁰ 7⁵⁰ 8³⁰ 21⁴⁰ v'24, ♏ 5³⁰ 6³⁰ = 7²⁵ ♎°8³⁰ 9¹⁵ = 9⁴⁵ ≡² 24; ⚸°13²⁰ 15⁴⁰ ⚸°18⁴⁵ ⚸°20⁰⁰ ⚸°23³⁰ ☠°6³⁰-a. ☠'14⁵⁰-15⁵⁵
31				[28.IV: ≫11²⁵⁻³⁰ (por.15) 14⁴⁵ 54 (por.16) 15²⁵...17⁴⁰ (por.17); ☠°0⁰⁰...1'...7³⁵ ...19³⁰; ☠°11⁴⁰...50; [☠°11⁴⁵⁻⁴⁵ NW
Σ	—	195.5	—	UWAGI

Kasprowy Wierch φ=49°14' λ=19°59' Maj-Mai 1962

DNI	CIŚNIENIE P=700+ I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI d I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	86.4	87.1	87.5	87.0	-11.0	-7.1	-10.7	-9.9	-5.7	-11.9	93	96	90	93	0.2	0.1	0.3	0.2	10 * =	9 *	2	N 7	NNW 3	WNW 5
2	84.5	84.9	86.2	85.2	-10.6	-7.6	-7.2	-8.2	-6.5	-11.0	90	93	96	93	0.3	0.2	0.1	0.2	8 ⊙	9 *	10 *	SSW 5	S 4	C 0
3	87.7	89.1	89.5	88.8	-9.8	-6.6	-7.5	-7.8	-3.9	-10.6	94	91	71	85	0.2	0.3	1.0	0.5	1 ⊙	9 *	8	N 3	WNW 1	NW 1
4	87.1	87.2	88.8	87.7	-4.8	-4.2	-5.6	-5.0	-3.4	-7.5	98	94	95	96	0.1	0.3	0.2	0.2	10 *△ =	9 *	9	WNW 11	W 8	NW 3
5	89.8	92.5	94.5	92.3	-4.9	-3.3	-3.7	-3.9	-2.0	-7.0	69	97	97	88	1.3	0.1	0.2	0.5	8 ⊙	10 * =	8 △	W 6	SSW 3	SW 3
6	96.2	98.4	99.1	97.9	-4.3	0.3	-1.0	-1.5	1.6	-5.2	96	87	85	89	0.2	0.8	0.9	0.6	10 △ =	10	1	N 1	C 0	SSW 6
7	99.0	99.6	100.4	99.7	0.8	1.4	2.8	2.0	3.3	-1.6	92	96	100	96	0.6	0.3	0.0	0.3	9	10 ●	10	NNW 4	SSW 4	NNE 7
8	100.7	101.3	99.6	100.5	3.2	5.6	6.0	5.2	7.2	1.9	100	90	78	89	0.0	0.9	2.1	1.0	9	10 ●(K)	10	N 6	NW 5	WSW 7
9	97.9	99.3	97.6	98.3	3.2	4.7	6.9	5.4	8.5	1.8	100	76	65	80	0.0	2.1	3.4	1.8	10 =	7 ⊙	6	NW 7	C 0	SW 6
10	92.4	94.6	96.1	94.4	3.4	1.5	0.5	1.5	7.0	0.3	100	100	100	100	0.0	0.0	0.0	0.0	10 ●, =	10 ●, =	9	NNE 3	N 9	NNW 2
11	94.7	94.4	95.0	94.7	-0.4	-1.5	-1.8	-1.4	1.0	-2.1	100	99	94	98	0.0	0.1	0.3	0.1	10 =	10 *	2	NW 1	NNE 1	NNW 3
12	95.9	97.1	96.9	96.6	-1.3	2.1	-1.1	-0.4	3.2	-2.7	84	94	99	92	0.9	0.4	0.1	0.5	6 ⊙	10	10 * =	C 0	C 0	SSW 4
13	97.9	98.7	97.1	97.9	-0.2	-0.3	3.3	1.5	4.2	-1.6	78	100	100	93	1.3	0.0	0.0	0.4	5 ⊙	10 * =	10 ● =	SSE 3	SSE 6	S 11
14	89.5	85.7	87.3	87.5	3.7	1.9	-3.8	-0.5	5.0	-4.0	100	96	96	97	0.0	0.3	0.2	0.2	10 ●	10 (K)	10 * =	S 16	SSW 19	NW 12
15	88.2	89.4	90.6	89.4	-4.0	-2.6	-3.3	-3.3	-2.3	-4.2	96	98	97	97	0.2	0.1	0.1	0.1	10 △ =	10 =	10 △ =	WNW 13	WNW 7	NNW 9
16	92.6	94.9	96.6	94.7	-3.7	-3.3	-4.7	-4.1	-2.8	-5.0	97	97	96	97	0.2	0.1	0.2	0.2	10 △ =	10 * =	8	NNW 9	WNW 11	W 8
17	97.0	98.6	98.2	97.9	-2.7	-0.1	1.4	0.0	1.7	-5.9	93	96	93	94	0.4	0.3	0.6	0.4	10	8 ⊙	8	W 12	SSW 8	SSW 13
18	97.1	99.1	101.5	99.2	0.5	1.8	-0.1	0.5	2.5	-0.3	100	85	70	85	0.0	1.1	1.9	1.0	10 * =	9 ⊙	1	WNW 5	W 9	WNW 4
19	100.7	99.3	95.7	98.6	1.4	3.6	5.9	4.2	6.5	-0.5	77	88	81	82	1.6	0.9	1.8	1.4	8 ⊙	7	7	S 6	SSE 16	SSE 16
20	94.9	93.4	94.0	94.1	4.4	4.9	-1.2	1.7	7.2	-1.4	100	96	99	98	0.0	0.4	0.1	0.2	9	10 ●	10 ● =	SSE 11	SE 8	N 2
21	94.1	94.2	94.3	94.2	-2.8	-2.3	-2.7	-2.6	-1.1	-2.9	97	98	97	97	0.1	0.1	0.1	0.1	10 * =	10 *△ =	10 *△ =	NNE 7	ENE 5	NE 4
22	96.0	97.9	100.4	98.1	-2.4	1.0	0.5	-0.1	1.7	-3.2	84	86	92	87	0.8	1.0	0.5	0.8	1 ⊙	6 ⊙	8	WNW 3	S 5	WNW 5
23	101.7	102.6	102.4	102.2	0.7	4.8	4.2	3.5	7.4	-0.2	84	69	82	78	0.9	2.7	1.4	1.7	4 ⊙	5 ⊙	4	WSW 4	SSE 3	S 4
24	101.4	100.5	97.9	99.9	4.0	3.1	3.4	3.5	5.9	2.5	93	100	100	98	0.5	0.0	0.0	0.2	9	10 ● =	9	SSE 4	SSW 2	S 5
25	95.6	95.9	95.3	95.6	2.1	4.5	3.9	3.6	6.0	0.5	100	96	96	97	0.0	0.3	0.3	0.2	10 ● =	10	10 (K)	S 6	S 6	SSW 5
26	94.1	94.3	96.2	94.9	3.9	5.4	4.6	4.6	6.5	3.4	91	97	100	96	0.7	0.3	0.0	0.3	9 ●	9	10 =	SSE 7	SSW 7	S 9
27	97.3	99.1	100.2	98.9	4.2	5.5	5.3	5.1	6.3	3.0	100	97	100	99	0.0	0.3	0.0	0.1	9	10 ●	8	S 5	SSW 9	S 7
28	100.4	100.1	100.1	100.2	6.2	4.8	5.9	5.7	7.7	4.1	88	98	100	95	1.1	0.1	0.0	0.4	6 ⊙	9	7	SSE 6	SSW 10	SSW 7
29	100.5	101.4	101.1	101.0	5.3	5.8	4.8	5.2	6.7	4.7	100	100	98	99	0.0	0.0	0.1	0.0	10 =	10 =	8	S 4	SSW 5	SSW 6
30	99.4	100.4	101.4	100.4	3.0	1.0	-0.2	0.9	4.9	-0.5	98	100	98	99	0.2	0.0	0.1	0.1	10 =	10 ●, =	7	SSW 6	NNE 4	NNW 3
31	100.5	99.8	98.0	99.4	0.2	6.7	3.9	3.7	7.9	-0.7	78	53	100	77	1.3	4.6	0.0	2.0	1 ⊙	4 ⊙	10	SSE 4	SW 7	S 11
M	95.2	95.8	96.1	95.7	-0.4	1.0	0.3	0.3	3.0	-2.2	93	92	92	92	0.4	0.6	0.5	0.5	8.1	9.0	7.7	6.0	6.0	6.1

Czerwiec-Juin

1	95.9	96.8	95.0	95.2	4.1	2.6	4.9	4.1	8.7	-2.5	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 ●, =	10 ● =	SW 10	SSW 8	S 14
2	92.6	96.1	98.2	95.6	4.0	-3.1	-4.3	-1.9	7.5	-4.5	100	97	96	98	0.0	0.1	0.2	0.1	10 =	10 =	10 =	SSW 8	WNW 2	NNE 6
3	98.4	100.1	100.9	99.8	-4.5	-3.3	-4.0	-4.0	-2.5	-4.7	98	97	96	97	0.1	0.1	0.2	0.1	10 *△ =	10 △ =	10 *△ =	NNE 7	NNE 5	NNE 6
4	99.6	100.2	99.2	99.7	-4.5	-4.1	-4.7	-4.5	-3.6	-4.9	98	96	96	97	0.1	0.2	0.1	0.1	10 *△ =	10 △ =	10 △ =	NNE 5	N 4	NNW 7
5	97.7	98.0	97.6	97.8	-4.9	-4.6	-5.4	-4.1	-3.0	-6.0	98	98	97	98	0.1	0.1	0.2	0.1	10 △ =	10 * =	10 * =	NNW 9	N 8	NNW 14
6	95.9	97.6	98.2	97.2	-5.7	-6.0	-6.1	-6.0	-2.5	-6.7	95	97	97	96	0.2	0.1	0.1	0.1	10 * =	10 *△ =	10 * =	NE 14	N 14	NNE 16
7	97.7	101.0	102.7	100.5	-6.9	-3.8	-5.1	-5.2	-2.9	-7.5	96	99	98	98	0.1	0.1	0.1	0.1	10 *△ =	10 △ =	10 △ =	NNE 11	NNE 7	NE 9
8	103.4	106.2	106.0	105.2	-2.7	-0.5	-0.6	-1.1	0.1	-5.2	97	100	99	99	0.1	0.0	0.0	0.0	10 △ =	10 =	9	NE 9	N 5	C 0
9	103.1	102.1	99.9	101.7	-0.9	1.4	1.8	1.0	3.5	-2.0	99	91	100	97	0.0	0.7	0.0	0.2	9	6 ⊙	10	W 1	C 0	NNW 2
10	97.5	97.6	97.1	97.4	2.0	2.7	3.1	2.7	5.3	1.0	98	94	89	94	0.2	0.4	0.8	0.5	10 ●	9	8	N 1	W 2	N 3
11	95.5	94.4	94.2	94.7	3.5	4.5	1.0	2.5	6.7	0.9	78	84	100	87	1.6	1.3	0.0	1.0	7 ⊙	9 ●(K)	10 * =	W 3	SW 3	NW 3
12	94.3	95.4	96.4	95.4	-1.2	-0.5	-1.5	-1.2	2.1	-1.8	99	100	99	99	0.1	0.0	0.1	0.1	10 * =	10 =	10 =	NNE 3	N 2	NNE 5
13	97.8	99.9	101.0	99.6	-2.3	0.1	0.3	-0.4	1.7	-4.0	98	96	83	92	0.1	0.3	1.0	0.5	10 =	9	1	NNE 4	C 0	SW 3
14	100.7	101.9	103.5	102.0	1.8	5.4	6.0	4.8	7.6	-0.5	92	83	79	85	0.6	1.5	2.0	1.4	6	6 ⊙	3	SSW 8	SSW 7	W 2
15	106.1	108.0	108.4	107.5	7.5	10.6	10.1	9.6	13.2	5.6	84	69	78	77	1.8	3.9	2.7	2.8	3 ⊙	7	3	WNW 1	NW 1	W 2
16	108.2	108.7	108.0	108.3	9.7	13.5	10.2	10.9	14.5	9.0	75	58	92	74	3.1	6.5	1.0	3.5	2 ⊙	6 ⊙	7	SSW 5	WSW 3	S 8
17	107.2	106.6	105.9	106.6	10.5	8.3	8.0	8.7	11.4	6.5	86	73	91	83	1.9	3.0	1.0	2.0	9(K)	9 ●	8	S 1	SSE 9	NE 2
18	104.6	104.9	104.5	104.7	6.9	8.2	7.0	7.3	9.5	6.4	100	99	86	95	0.0	0.2	1.4	0.5	10 ● =	10 =	1	NE 2	NNE 1	NE 2
19	103.5	103.5	102.7	103.2	7.9	11.7	9.5	9.6	14.5	6.3	75	82	94	84	2.6	2.6	0.7	2.0	0 ⊙	6	5	N 1	NE 1	SW 4
20	103.2	104.4	105.0	104.2	9.1	10.4	8.7	9.2	11.9	7.4	85	77	100	87	1.8	2.9	0.0	1.6	3 ⊙	7(K)	10 =	NNW 1	SW 3	C 0
21	105.8	106.7	107.4	106.6	8.4	7.8	6.6	7.4	10.4	6.2	95	100	88	94	0.5	0.0	1.2	0.6	8 ⊙	10 ● =	7	SW 2	SE 2	NNE 4
22	108.5	109.6	109.6	109.2	7.2	9.4	9.3	8.8	12.3	5.8	100	97	96	98	0.0	0.3	0.5	0.3	10 =	9	4	NE 3	C 0	SSW 6
23	109.4	109.9	109.1	109.5	9.4	13.3	12.1	11.7	16.5	8.4	85	77	65	76	1.8	3.5	5.0	3.4	2 ⊙	5	2	WSW 1	NNE 1	NNW 4
24	107.9	107.8	106.6	107.4	11.2	15.3	12.6	12.9	17.1	10.6	79	45	72	65	2.8	9.6	4.2	5.5	3 ⊙	5(K)	6	WNW 5	SW 3	WSW 3
25	104.7	104.6	104.3	104.5	11.3	13.1	4.2	8.2	15.4	4.1	69	59	100	76	4.2	6.3	0.0	3.5	6 ⊙	9	10 =	W 8	NNW 5	NNE 5
26	100.9	100.4	98.5	99.9	3.1	7.0	4.1	4.6	8.8	0.4	34	77	94	68	5.0	2.2	0.5	2.6	7	8	9	NE 1	N 1	SW 6
27	97.0	97.3	97.5	97.3	3.7	5.3	0.5	2.5	7.4	0.5	55	69	96	73	3.6	2.7	0.2	2.2	9 ⊙	6	10	C 0	NNW 5	N 3
28	95.6	95.7	94.4	95.2	-2.6	-0.8	-1.8	-1.8	0.6	-2.7	98	95	98	97	0.1	0.3	0.1	0.2	10 =	10 △	10 *△	N 4	WNW 1	WSW 5
29	93.6	95.7	96.6	95.3	-3.7	-1.6	-1.6	-2.1	0.0	-4.0	97	96	98	97	0.2	0.2	0.1	0.2	9	10	7	W 7	NW 8	WNW 5
30	95.2	96.8	98.0	96.7	-2.6	-1.0	-1.2	-1.5	0.9	-3.3	95	99	99	98	0.2	0.1	0.1	0.1	10 △ =	10 =	10 △ =	N 4	NNW 1	N 3
31																								
M	100.7	101.6	101.5	101.3	2.6	4.0	2.9	3.1	6.4	0.6	89	87	95	90	1.1	1.6	0.8	1.2	7.8	8.5	7.7	4.6	3.7	3.1

Kasprowy Wierch $H_s = 1991m$ $H_b = 1988,8m$ $h_w = 15,4m$ Maj - Mai 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	0.7	140	⩶°0^00-1^40 *°5^30-14^35 *°⁻¹15^20-17^18 17^30-19^10 V'0^00-10^05, ≡²0^00-10^10 ⩶-11^15 ≡²-12^20 ⩶-14^30 ≡²15^40-16^35
2	7	13.7	141	*°9^20 17^35 *'20^20-24, V°17^30-18^30, 19^40-24, ⩶ 13^30-14^50 ≡²-15^40 ⩶-16^20 ≡²-18^30 ⩶-19^40 ≡²-24
3	7	1.4	155	*'0^00-30 *°-2^00 10^15-13^10, 13^35-14^30, 17^25-18^30, V°0^00-4^35, 17^30-50, 18^10-30, ≡²0^00-4^35 ⩶-5^30, 17^30-50, 18^10-30, Ⓢ a...p, ()6^00-9^20
4	6	0.6	157	*°2^55 4^10 *°⁻¹-6^45 ⩶°7^50 *°8^45 18^15, V°3^45-7^10 10^25 11^40 ⊔°19^30-21^15 V° 22^40 ⊔°-24, ⩶ 3^45-55 ≡²-6^45 ⩶-7^10 10^25-11^40 21^15-30 ≡²-22^40, ≫6^10-7^10(pot.17), 16^40-18^40(pot 19), ╪°4^10-16^30 ╪°⁻¹-19^45, 23^40-24
5	0	0.6	154	*°⁻¹9^35-13^45 ⩶°17^35-21^40, ⊔°0^00-5^00 V°11^45-12^50, p..., ⩶ 9^30-11^45 ≡²-12^50 ⩶-14^30, 15^10-24, ╪°0^00-3^15, ⊕²4^51-5^41 ⊕⁰⁻¹-7^20
6	6	0.0	152	⩶°5^35-8^40 ⩶°11^11 12^23, V°3^30-8^10, a... ⊔°19^20-24, ⩶ 0^00-40 ≡²3^30-8^10 ⩶-8^40, 9^15-35, 10^25-40 ≡²-11^15 ⩶-12^43
7	7	1.3	148	●°10^55 13^15-19^50 21^50 24, ⊔°0^00-15, ⩶ 14^10-30 ≡²-24
8	7	2.5	140	●°0^00 1^50, 12^35-13^20 21^12-23^35, (ꓘ)°W 12^20-ꓘ°12^35-13^15, ≡²0^00-4^40 ⩶-7^15, 21^35-24, ≫23^35-24; ⊕°18^05-20, ꓘ'12^30-13^10
9	8	17.6	152	⩶ 0^00-45 ≡²2^40-8^15 ⩶... 12^00; ≫0^00-4^30(pot 19), 23^35-24
10	0	8.3	110	●°⁻²0^50-2^45 3^50-6^00 ●●'-7^30 ●'-9^00 ●●°-13^30 ●°-14^50 ●°15^40 16^50, (ꓘ)°10^8-30W ≡²2^30-16^35 ⩶-16^45, 17^20-20^10, 21^10-21^30 ≡²-24, ≫0^00-10, 10^30-11^30(pot 17)
11	5	11.7	101	⩶°4^50-5^05 *°⁻¹9^28 16^45, V°12^00 16^35 ⊔°20^00-24, ≡²0^00-15 ⩶-0^30, 1^30-46 2^10-3^30 4^20-5^15 ≡²-6^45 ⩶-8^30 ≡²-12^15 ⩶-13^25 ≡²-16^35 ⩶-16^45 18^43-19^02, ꓘ⁰⁻¹9^35-12^00
12	8	1.7	104	⩶°12^50-14^20 *°15^00-40 ⩶'-17^30 *⩶'-18^20 *°-21^45, (ꓘ)'16^44-17^30 SSW, 18^36 N, ⊔°0^00-5^00 V°17^50 21^20, (m) na -12^30 ⩶-14^20 17^15-50 ≡²-18^10 ⩶-19^15 ≡²-20^45 ⩶-21^20, ⊕°5^20-12^00
13	0	17.1	102	*°⁻¹10^50-16^35 ●°17^35-18^40, 19^25-21^45 22^07-40 ●°⁻¹23^27-24, (m) 4^00 -na ⩶ 11^30-12^20 ≡²-15^05 ⩶-15^35 ≡²-22^10 ⩶-23^30, ≫15^05-45(pot 17), 18^10-22^30(pot 19), 23^23-24, ⊕°7^00 -a
14	9	12.7	88	●°⁻¹0^00-7^40 9^45-11^38 *⩶°⁻¹13^44-14^20 *°-15^45 ●°16^40 17^10 *°18^44 22^10, (ꓘ)°NNE 12^10-ꓘ¹⁻⁰13^35-14^45, ≡²1^15-3^40 ⩶-4^10 ≡²-6^25 ⩶-10^40 ≡²-11^26 ⩶-11^40 12^21-13^35 ≡²-14^20 ⩶-15^30 ≡²-24, ≫0^00-3^35
15	0	3.1	84	⩶°6^03-7^40 17^53-24, V°0^00-3^00 V¹⁻²-9^30 V°-24, ≡²0^00-24, ≫0^00-8^30(pot 23) [14.V: (pot 26)↘-11^15(pot 30)≫-12^15(pot 25)↘-15^15(pot 27)≫-18^25(pot 25) 19^30-24(pot 27); () 11^40-13^35, ꓘ'13^10-14^45
16	1	3.0	86	⩶°0^00-3^30 4^30-8^50 ⩶°11^40-14^30, V°0^00-2^10 V¹⁻²-15^35, ≡²0^00-15^35, ⩶-18^30, ≫0^20-3^30(pot 23), 4^40-6^30 10^45-20^10(pot 15), 21^15-22^30(pot 15), ╪°0^30-3^50, 4^30-6^30 ╪°16^40-20^15
17	8	0.9	87	*°16^35-17^30 ⩶°-18^40 ●°23^35-24, ⩶ 9^45-10^25 16^30-19^45 23^30-24, ≫2^40-6^30 10^40-11^25, 13^50-24(pot 20), ⊕'12^05-30
18	8	0.5	83	●°0^00-15 5^40-6^20 *°-7^15 ⩶°8^44-10^13, ⩶ 0^00-1^40 ≡²-4^45, 5^05-7^50 ⩶-8^07 ≡²-8^25 ⩶-10^30, 14^35-15^28, 17^35-18^15, ≫0^00-1^40(pot 16), 2^40-3^30, ⌓'21^25-22^45 ⌓°-23^05, Ⓢ 17^35-18^15
19	8	2.1	80	≫0^05-35(pot 16), 8^20-12^10(pot 23)↘-13^05(pot 25)≫-16^30(pot 28)↘-17^20(pot 26)≫-19^40(pot 28)↘-22^30(pot 36)≫-24(pot 34), () 3^15-4^30
20	8	52.9	69	●°1^55 3^30-4^40 5^45 6^50-7^30 10^22-13^00 ●'-15^00 ●°-15^20 ●°-16^50 ●'17^20-18^15 ⩶°-21^15 *'-22^15 *°-24, ⌣⁰⁻¹18^15-21^15 V°-24, ⩶ 3^15-35 ≡²5^13 ⩶-5^35, 11^06-14^30 ≡²-24, ≫0^00-2^25(pot 35), 6^30-7^35(pot 18)
21	0	10.2	70	*°0^00-15 ⩶°-1^10 *°⁻¹-12^30 *Δ°-14^35 *°⁻¹-20^15 *Δ°-23^15, V°⁻¹0^00-15 ~0^15-1^10 V⁰⁻¹1^10-23^50, ≡²0^00-23^50 ⩶-24 [20.V: 8^15-10^05(pot 23), 13^10-14^15(pot 21), () 5^30-8^00
22	9	0.1	78	*°23^35-24, ⩶ 0^00-40 (m) -2^30 (m) -a ⩶ 14^17-16^40, 23^20-40 ≡²-24, ╪°10^20-11^20, ()0^00-1^00, 4^30-8^15, ⦶°a..., ⌒'16^01-25
23	8	•	74	*°0^00-45 ≡²0^00-15 ⩶-0^30, ⌣⁰⁻¹1^10-2^00, ()8^30-10^40
24	0	22.9	68	●°11^20-40 ●'-14^00 ●°-14^25 15^25-16^00 ●Δ°-16^05 ●'-18^25 ●°-18^50, ≡²7^25-16^25 ⩶-22^15 (m) -24, ⌣⁰⁻¹1^20 na, ꓘ 12^00-13^30
25	7	18.0	60	●°4^50 7^45, 8^15-11^40 16^30-58 ●Δ'-17^01 ●'-17^40 ●°-18^20 18^40 20^15, (ꓘ)°16^55-18^00 S-SE, 20^25-21^15 NE-ENE, (m) 0^00-1^30 (m) -3^30 ⩶-4^50 ≡²-10^30 ⩶-11^15 (m) -13^40 ⩶-14^40 (m) -16^05 ⩶-16^40 ≡²-17^30 ⩶
26	8	9.3	54	●°5^10 6^45 7^40 8^20 13^46-59 ●Δ⁰⁻¹-14^04 ●⁰⁻¹-15^41 16^35-17^15 ●°-21^42 22^15-24, (ꓘ)°13^10-30 SW, ≡²0^00-2^30 ⩶-5^20 ≡²-6^05 ⩶-6^30, 8^35-45 ≡²-9^15 ⩶-12^15 13^50-14^14 ≡²-15^25 ⩶-16^30 ≡²-18^08 ⩶-19^10 ≡²-20^00 ⩶
27	7	1.2	47	●°0^00-0^20 3^15 ●⁰⁻¹7^24 ●°8^40-9^20 10^50 13^05-15^35, (ꓘ)°14^19-45 S, ≡²0^00-30 ⩶-2^20 (m) 0^30-3^20 ⩶ 3^15-30 ≡²-7^08 ⩶-9^40, 15^40-20^10 (m) 7^08-24, ≫8^40-9^15(pot 19), 11^05-12^05(pot 17), 14^45-15^05(pot 20)
28	9	5.4	40	●°9^40-13^15, (m) ⩶ 0^00-1^20 ≡-3^10 ⩶-3^30 (m) -22^30 ⩶ 10^45-12^45 ≡²-13^10 ⩶-13^30, 14^10-22^30 ≡²-24, ≫12^35-15^00(pot 20); () 3^30-9^00, 13^45-16^00
29	0	1.3	pł.	●°4^56-5^15, 16^45-17^12, (ꓘ)°11^27-45 E, ≡²0^00-10^25 ⩶-11^42 ≡²-13^50 ⩶-15^35 16^15-22^20 ≡²-23^30 ⩶-24 [25.V: -19^50 (m) ⩶-20^30 (m) 22^30 ≡²-24, ≫8^30-9^10(pot 17), 19^50-20^25(pot 22), 23^15-24(pot 19);
30	0	0.9	pł.	●°4^25-6^40 ●●°9^40-11^50 *°11^55-12^20 ●●°13^35-15^50, ⊔°22^20-24, ⩶ 0^00-40 ≡²-11^40 ⩶-12^30 ≡²-16^05 ⩶-17^25 ≡ 20^20-22^10 [25.V: ꓘ⁰⁻¹16^55 24
31	8	9.5	pł.	⊔°0^00-6^00, ⩶ 20^35-23^40, ≫19^45-24(pot 19) [26.V: -20^15 ≡²-24, ≫0^00-50(pot 18), 7^30 11^30(pot 20); ꓘ⁰⁻¹0^00-40
Σ	—	211.2	—	UWAGI

Czerwiec - Juin

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	0	29.5	pł.	●°2^51 3^25 ●⁰⁻¹4^25-6^45 ●°8^50-10^40 ⩶°-12^15 ●°-13^15 ●●°-13^45 ●'-17^40 18^35-54 20^10-25 20^46-51 ●Δ'-20^58 ●°⁻² ●Δ⁻²-23^15 ●°-24, (ꓘ)°SW 20^46-ꓘ'20^51, 21^07, (ꓘ)²21^30 NE ꓘ'22^26-45, ⩶ 1^30-2^40 ≡²-24, ≫0^00-3^20(pot 24)↘-
2	0	4.5	pł.	●°0^00-20 ⩶°-1^16 ●⁰⁻¹ ⩶⁰⁻¹ ●Δ⁻²1^16 2^10 ●°2^45-3^10 6^40-7^10, ꓘ'1^10-2^00 W-E, 2^46-3^00 NE, ~'0^20-1^40, V⁰⁻¹15^10-24, ≡²0^00-11^07 ⩶-11^35 ≡²-17^42 ⩶-18^35 ≡²-24, ≫1^15 7^15(pot 20)
3	0	17.6	4	⩶°0^35-2^30 ⩶°-3^45 Δ ⩶⁰⁻¹-5^30 ⩶°-6^45 *⩶⁰⁻¹-10^30 ⩶°-19^30 *⩶°-23^40 *'-24, V⁰⁻¹0^00-24, ≡²0^00-24
4	0	38.8	21	*'0^00-10 *⩶⁰⁻¹-1^30 ⩶'-2^30 *⩶°-3^20 *⩶⁰⁻¹-12^10 ⩶⁰⁻¹-24, V'0^00-8^30 V°-24, ≡²0^00-24, ╪°19^10-24, ꓘ 13^40-14^05
5	0	69.4	75	⩶⁰⁻¹0^00-9^30 *⩶°-10^15 *°-14^00 *'-15^00 *°-22^15 ⩶*°-24, V°0^00 -na V'na -p V²p -24, ≡²0^00-24, ≫19^20-24(pot 16), ╪°0^00 na ╪⁰⁻¹-24
6	0	60.8	120	*⩶°0^00-45 *°-5^15 *⩶°-6^30 *°-9^30 *⩶°16^30 ⩶°-18^30 19^15-20^45 *⩶⁰⁻¹24, V²0^00-24, ≡²0^00-18^45 ⩶-19^10 ≡²-24, ≫0^00-8^30↘-10^45(pot 21)≫-15^10(pot 21)↘-24(pot 25); ╪'0^00-24
7	0	15.9	180	*⩶⁰⁻¹0^00-4^40 ⩶'-6^30 *⩶'-7^20 *⩶°-8^30 ⩶°-14^40 *°15^20 ⩶°-18^35 *⩶°-20^35 ⩶°-24, V²0^00-24, ≡²0^00-24↘0^00-2^45(pot 22)≫-9^20(pot 20), 22^25-23^40, ╪'0^00-9^20 ╪°-10^30 ╪°22^25-24
8	0	0.4	200	⩶°0^00-7^40 *⩶°-8^15, V²0^00-6^40 V°-11^15, ≡²0^00-14^15 ⩶-14^30 ≡²-15^10 ⩶-18^25, ≫2^15-5^40, 9^50-11^20, ╪°0^00-1^30 ╪'-3^15 ╪°-5^40
9	8	0.7	178	⩶ 5^10-8^20 22^00-24 [1.VI: 4^10(pot 25)≫-8^05(pot 19), 17^10-19^25(pot 23)↘-20^44(pot 28)≫-21^44(pot 26)↘-21^55(pot 29)≫-22^00(pot 19), 22^05-40(pot 17)↘-23^10(pot 25)≫-23^45(pot 25)
10	8	0.4	160	●°5^50-8^10 10^45-12^10, ⩶ 0^00-30, 6^15-30 ≡²-7^20, 10^20-11^15 ⩶ 19^40-20^15
11	7	15.5	135	●°13^07-15^15, 17^28-18^25 ●⁰⁻¹19^30-21^00 Δ°-21^10 ⩶°-22^10 ●°-24, (ꓘ)°10^40-11^30 E, 13^10-15^15 NW-N, 21^10-15 S, ⩶ 0^20-2^45, 11^10-40, 15^25-17^10, 20^15-35 ≡²-22^25, ꓘ°21^35-22^30
12	0	6.7	105	●°0^00-05 2^45-4^50 ⩶°-5^10 *⁰⁻¹-10^30 *⩶⁰⁻¹-11^20 ⩶°-13^15, 18^40-19^35, ~°5^50-8^30, V⁰⁻¹6^30-11^00, 18^00-24, ⩶ 0^15-1^20 ≡²-24
13	7	0.0	103	⩶°8^45-9^30 10^40-11^15, V°0^00-11^30 ⊔'23^30-24, ≡²0^00-11^30 ⩶-11^40
14	8	•	90	⊔'0^00-4^30, ≫11^40-12^40, ⊕ 20^00-30
15	8	0.2	72	●°17^01-20
16	7	•	56	(ꓘ)°13^15 S, 14^40-17^00 NNE-NE, NW-N, ꓘ⁰⁻¹14^45-15^10
17	7	25.2	56	●°8^17-30 ●⁰⁻¹9^38 10^20 ●Δ⁰⁻¹10^22 ●⁰⁻¹12^20 ●¹⁻²12^45 ●⁰⁻¹14^10 ●°-15^15, (ꓘ)°6^40-7^45 SW-W (ꓘ)'-8^30 NW-NE (ꓘ)°10^10 NE ꓘ¹⁻²10^30 (ꓘ)°12^10 E ꓘ¹⁻⁰12^45, 13^45-14^15, ⩶ 7^45 8^05 ≡²-8^20 ⩶-8^30, 10^10-45, 11^30-40, 16^15-30 ≡-17^20 ⩶-
18	0	0.1	pł.	●°4^40-8^35, ≡²5^30-8^30 ⩶-9^30 ≡²-10^45 ⩶-12^40 ≡²-16^45 ⩶-19^30 [17.VI: 18^30, ꓘ'10^10-14^30
19	7	•	pł.	⌂°0^30-8^20, ⩶ 21^05-20
20	8	19.0	pł.	●°11^05-20 ●Δ²-11^25 ●⁰⁻¹-11^40 15^05-45, (ꓘ)°10^21-11^05 NE SW-W ꓘ'-11^15 ꓘ²-11^40 ꓘ'12^05 (ꓘ)°-13^50 NE, 15^40-17^15 SW-NE, ⩶ 7^55-8^15, 9^20-12^05, 14^10-16^30, 17^15-18^10, 19^10-25 ≡²-22^05 ⩶-23^10, ꓘ²10^30-12^10, 15^10-17^00
21	1	29.2	pł.	●¹⁻²11^00-30 12^40-15^09 ●°-16^10 18^50-19^40, ꓘ°13^08-15, ⩶ 3^30-4^10 ≡²-5^50 ⩶-6^50 7^30-9^15 ≡²-14^30 ⩶-15^45, 17^15-18^30 ≡²-19^20 ⩶-20^40
22	7	•	pł.	≡²0^30-4^30 ⩶-7^15 ≡²-8^00 ⩶-9^45 ≡²-10^30 ⩶-11^40 ≡²-12^30 ⩶-14^30, 23^45-24, Ⓢ na...
23	7	•	pł.	⌂'2^30-8^40, ⩶ 0^00-45 2^00-45
24	8	•	pł.	(ꓘ)°13^40-14^30 NNE-NE, ⌓ 20^30-45
25	8	0.0	pł.	●°16^50-17^05, ⩶ 14^15 20^30 ≡²-22^15 ⩶-22^40
26	8	•	pł.	⌂'0^30-8^30, ⩶ 0^30-45 ≡²-4^10 ⩶-4^20 (m) 4^10-8^40 ⩶ 21^30-22^45
27	8	0.2	pł.	●°10^15-30 ●Δ°-10^38, ⌂'0^00-4^50, ⩶ 12^40-13^15, 23^30-24
28	8	2.2	pł.	⩶°8^30-35 9^55, 11^20 ⩶°11^55-12^20 13^08 14^10 15^15-16^10 *°16^45-17^30 ⩶°17^45-18^35, 20^45-21^10 *⩶°-22^15 ⩶⁰⁻¹-24, V°6^15-9^15, 21^02-24, ⩶ 0^00-1^30 ≡²-8^20 ⩶-9^15, 21^02-24, ≫22^00-50
29	8	0.0	5	⩶⁰⁻¹0^00-1^10, 2^55-3^10 *⩶°-4^30 ⩶°7^50 10^20, 17^45-18^10, V°0^00-4^40, ⩶ 0^00-4^40, 12^20-30, ≫2^02-6^05(pot 20), 9^50-11^05(pot 21); ╪°3^50-8^10
30	1	2.2	pł.	*°6^50-7^15 ⩶°-9^30, 10^45-11^35 *°12^05-25, 17^50-20^30 ⩶°-24, V°4^05-8^40, 20^30-24, ⩶ 3^40-4^05 ≡²-7^10 ⩶-7^25 ≡²-8^40 ⩶ 9^35-13^10 ≡²-13^50 ⩶-16^40 ≡²-24
31	[illegible]	[illegible]	[illegible]	[illegible]
Σ	—	338.5	—	UWAGI

Kasprowy Wierch φ=49°14' λ=19°59' Lipiec-Juillet 1962

DNI	CIŚNIENIE P=700+ I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	98.2	99.4	99.1	98.9	-0.5	2.6	1.0	1.0	3.4	-1.2	100	98	100	99	0.0	0.2	0.0	0.1	10 ≡	9	10 ≡	N 1	W 1	W 5
2	97.0	97.0	96.4	96.8	-1.0	1.1	-0.1	0.0	2.1	-2.2	91	84	96	90	0.6	1.0	0.3	0.6	3⊙	9	9	NE 2	NW 3	W 5
3	91.5	90.5	88.9	90.3	0.2	0.3	0.0	0.1	1.4	-2.1	100	100	100	100	0.0	0.0	0.0	0.0	10	10 ✳	10 ✳ ≡	WSW 9	W 8	SSW 6
4	87.0	88.5	89.8	88.4	-1.6	0.0	-1.3	-1.0	2.8	-2.3	98	90	86	91	0.1	0.6	0.8	0.5	10 ≡	8	7	WSW 5	SSW 5	SSE 10
5	90.4	92.1	93.8	92.1	-0.8	2.0	-0.3	0.2	3.1	-2.8	83	92	100	92	1.0	0.6	0.0	0.5	8⊙	10	10 ✳ ≡	C 0	N 1	C 0
6	97.2	99.6	100.5	99.1	-0.1	3.6	2.7	2.2	5.7	-1.5	94	96	84	91	0.4	0.3	1.2	0.6	2⊙	9	0 ●	WNW 1	SW 3	SW 3
7	100.1	100.2	100.3	100.2	3.1	4.5	1.2	2.5	5.2	1.1	82	86	91	86	1.4	1.1	0.7	1.1	8	10	10	S 1	NW 3	WNW 5
8	99.9	101.5	102.7	101.4	-1.5	0.0	0.5	-0.1	2.5	-2.0	99	100	100	100	0.1	0.0	0.0	0.0	10 ≡	10 ✳	10 ≡	W 5	NW 4	N 3
9	102.6	103.3	103.0	103.0	0.1	5.4	4.0	3.4	7.0	-0.7	100	74	82	85	0.0	2.4	1.4	1.3	10	6 ◉	9	NE 2	NW 4	W 3
10	101.5	101.9	100.8	101.4	4.4	6.0	5.9	5.6	8.4	3.0	80	97	90	89	1.7	0.3	0.9	1.0	3⊙	10 ●	9	WNW 8	WNW 6	NW 5
11	100.3	101.0	99.8	100.4	7.2	11.5	9.6	9.5	12.6	4.3	56	65	76	66	4.6	4.8	2.9	4.1	7⊙	9	7	WNW 9	NW 6	W 8
12	98.0	98.3	97.9	98.1	6.5	8.4	7.7	7.6	11.3	6.4	92	81	62	78	5.0	2.0	4.0	3.7	10	9	9	WNW 5	NW 6	WSW 5
13	95.5	95.1	95.4	95.3	4.4	5.1	1.8	3.3	7.8	1.6	82	75	96	84	1.5	2.2	0.3	1.3	8⊙	8⊙	10	W 9	NW 5	WNW 7
14	94.9	95.2	95.2	95.1	1.6	3.3	3.2	2.8	4.1	0.7	95	88	87	90	0.5	0.8	1.0	0.8	7⊙	9	9 ●	NW 5	WSW 7	W 10
15	94.7	94.1	94.0	94.3	3.1	4.3	4.5	4.1	6.1	3.0	97	100	100	99	0.2	0.0	0.0	0.1	10 ●	10 ●	9	SW 6	SSW 8	SSW 8
16	94.0	95.3	96.3	95.2	4.9	8.1	5.9	6.2	10.3	3.4	93	85	90	89	0.6	1.6	1.0	1.1	8	8	5	C 0	C 0	W 1
17	96.4	97.7	98.4	97.5	6.4	5.2	5.1	5.4	8.7	4.9	95	95	96	95	0.5	0.4	0.3	0.4	8⊙	10 ●(R)	4	E 1	NNE 3	NE 2
18	97.2	97.3	97.5	97.3	5.5	5.3	4.6	5.0	6.0	4.5	100	100	100	100	0.0	0.0	0.0	0.0	10 ●◉ ≡	10 ● ≡	10 ● ≡	NNE 4	NNE 3	N 11
19	97.6	98.4	101.1	99.0	4.4	4.9	5.1	4.9	5.7	3.4	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	10 ● ≡	10 ● ≡	NNE 10	N 15	NNE 11
20	102.6	104.4	105.3	104.1	5.3	8.1	7.7	7.2	11.9	4.9	100	89	85	91	0.0	1.2	1.6	0.9	10 ≡	8⊙	3	NNW 8	NNE 2	NNW 2
21	105.1	104.9	104.9	105.0	7.2	12.8	9.3	9.6	13.9	6.0	85	69	90	81	1.6	4.6	1.2	2.5	1⊙	5◉	0	SSW 2	SW 4	SSW 6
22	105.3	105.6	104.9	105.3	10.9	13.1	11.2	11.6	15.4	8.5	85	80	76	80	2.0	3.0	3.1	2.7	1⊙	8	9	ENE 2	C 0	SW 3
23	104.6	105.7	106.6	105.6	7.9	10.2	8.0	8.5	12.1	7.2	100	94	100	98	0.0	0.7	0.0	0.2	10 ● ≡	9	10 ● ≡	NNE 4	NNE 2	NNE 7
24	106.8	107.5	108.2	107.5	5.1	5.2	4.1	4.6	8.1	3.9	100	98	91	96	0.0	0.1	0.7	0.3	10 ≡	10 ≡	5	NNE 3	N 1	NNE 3
25	107.9	108.7	108.4	108.3	4.9	10.7	8.3	8.0	13.3	3.0	67	70	94	77	2.9	3.9	0.7	2.5	0⊙	2⊙	1	W 3	N 1	SSW 8
26	107.9	108.8	108.4	108.4	10.9	15.5	12.5	12.8	16.3	8.1	56	57	73	62	5.8	7.5	4.0	5.8	0⊙	1⊙	2	SSW 6	SW 5	SSW 5
27	107.7	107.1	105.9	106.9	14.5	16.3	11.4	13.4	17.2	11.3	47	72	87	69	8.8	5.3	1.8	5.3	9	7	9	WNW 1	E 3	WNW 3
28	103.1	103.7	103.2	103.3	5.6	5.3	3.0	4.2	11.5	2.7	100	98	96	98	0.0	0.1	0.3	0.1	10 ● ≡	10 ≡	3	NNW 7	N 4	N 4
29	102.2	102.5	102.7	102.5	2.5	5.1	1.9	2.8	7.4	1.3	98	86	98	94	0.1	1.2	0.1	0.5	9	9 ◉	1	NE 4	NNE 1	NE 3
30	102.4	103.1	103.2	102.9	2.5	4.4	3.3	3.4	5.8	1.3	87	84	100	90	1.0	1.3	0.0	0.8	5⊙	9	10	ENE 3	NE 1	NE 2
31	103.6	104.8	105.3	104.6	3.1	6.6	5.0	4.9	8.8	2.1	100	71	63	78	0.0	2.8	3.3	2.0	10 ≡	7	3	NNE 3	NNW 3	NNW 3
M	99.8	100.4	100.6	100.3	4.1	6.3	4.7	5.0	8.3	2.6	89	86	90	88	1.3	1.6	1.0	1.3	7.3	8.4	7.1	4.2	3.8	5.1

Sierpień-Août

1	105.3	105.6	105.0	105.3	5.3	9.4	7.1	7.2	11.5	4.5	83	58	97	79	1.5	5.0	0.4	2.3	2◉	7	8	W 4	W 6	WNW 6
2	103.4	104.3	104.2	104.0	6.3	12.1	9.8	9.5	14.6	6.0	86	56	62	68	1.3	6.2	4.6	4.0	7	4⊙	1	W 7	NNW 3	SSW 7
3	103.3	103.4	104.0	103.6	10.3	13.0	11.0	11.3	14.0	8.2	78	76	92	82	2.7	3.7	1.0	2.5	9⊙	9	8	SSW 8	WSW 6	SW 3
4	104.2	105.7	105.7	105.2	9.5	12.0	11.9	11.3	15.5	9.2	78	81	73	77	2.5	2.6	3.7	2.9	1⊙	8	6	W 3	N 2	W 4
5	104.1	102.8	100.7	102.5	11.4	14.6	10.1	11.6	16.0	8.2	77	75	84	79	3.2	4.1	2.1	3.1	5⊙	8(R)	6	W 1	NNE 1	SW 11
6	101.2	102.1	102.4	101.9	9.6	14.9	10.9	11.6	15.6	8.1	72	57	76	68	3.4	7.2	3.1	4.6	2⊙	5⊙	1	W 6	NW 4	WSW 5
7	100.5	98.1	99.6	99.4	11.2	14.4	13.4	13.1	15.7	10.6	76	63	83	74	3.1	6.0	2.6	3.9	1⊙	3⊙	8	SE 12	S 15	WSW 9
8	101.8	104.1	105.2	103.7	7.8	11.1	8.3	8.9	13.4	3.9	100	80	100	93	0.0	2.6	0.0	0.9	10 ≡	6	10 ≡	SSW 8	SW 5	WSW 1
9	106.2	107.3	107.4	107.0	4.8	7.7	5.6	5.9	9.9	4.3	100	92	100	97	0.0	0.8	0.0	0.3	10 ≡	9	5	ENE 3	NE 1	C 0
10	106.3	106.2	105.3	105.9	8.2	11.7	8.9	9.4	13.0	5.3	64	82	78	75	3.9	2.6	2.6	3.0	7◉	9	1	C 0	SE 1	SSW 2
11	104.6	105.3	105.7	105.2	7.9	11.9	9.0	9.4	13.7	6.9	81	66	83	77	2.0	4.7	2.0	2.9	1◉		4	C 0	N 1	C 0
12	106.0	107.3	107.5	106.9	10.3	14.4	11.7	12.0	16.6	8.5	62	60	75	66	4.8	6.5	3.3	4.9	6⊙		6	S 2	SW 4	S 2
13	107.3	108.4	108.1	107.9	10.9	14.6	12.0	12.4	15.4	10.2	74	70	81	75	3.3	5.0	2.6	3.6	9⊙		3	SSW 8	C 0	N 2
14	106.7	107.1	106.0	106.6	11.8	14.0	12.5	12.7	16.6	10.8	74	90	66	77	3.5	1.6	4.9	3.3	1⊙		8	NNE 3	NNW 1	NNW 5
15	104.1	104.1	100.6	102.9	12.7	16.0	13.7	14.0	17.5	9.9	70	69	67	69	4.6	5.5	5.3	5.1	10⊙		8	SSW 6	SSW 6	SW 10
16	99.6	100.1	101.9	100.5	8.5	8.8	7.4	8.0	13.7	7.2	100	100	100	100	0.0	0.0	0.0	0.0	10 ●R	10 ● ≡	10 ≡	SSW 10	S 2	NW 2
17	102.0	102.4	100.7	102.0	7.7	10.5	7.8	8.4	12.4	6.3	75	74	94	81	2.6	3.3	0.7	2.2	8⊙	9	5	C 0	WSW 1	SSE 6
18	99.4	100.0	100.6	100.0	8.7	8.9	3.6	6.2	11.2	2.7	65	87	100	84	3.8	1.5	0.0	1.8	7	8⊙	10 ● ≡	W 3	WSW 3	N 6
19	99.7	100.0	99.8	99.8	0.9	2.1	0.8	1.2	3.6	0.1	88	80	100	89	0.8	1.5	0.0	0.8	3⊙	10	10 ● ≡	WNW 9	WNW 12	NW 8
20	99.0	100.1	100.1	99.7	1.6	2.5	3.2	2.6	3.7	0.4	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	10 ● ≡	10 ● ≡	N 9	NNE 7	N 6
21	99.4	100.2	100.7	100.1	4.1	6.5	5.9	5.6	9.0	2.4	94	97	98	96	0.5	0.3	0.2	0.3	3⊙	10 ≡	5	NE 2	SSW 1	SW 2
22	101.1	102.2	102.6	102.0	4.9	6.3	5.0	5.3	7.2	4.4	100	98	100	99	0.0	0.1	0.0	0.0	9	10 ≡	3	WNW 1	C 0	SSW 2
23	102.3	103.9	104.5	103.6	3.4	6.7	5.1	5.1	8.7	2.9	88	68	70	75	0.9	3.1	2.6	2.2	9◉	7⊙	9	WNW 4	W 7	NW 8
24	103.1	101.7	101.1	102.0	5.5	7.7	9.2	7.9	9.6	4.3	93	76	74	81	0.6	2.5	3.0	2.0	9	8	1	WSW 6	SSW 19	S 16
25	101.7	102.8	103.5	102.7	8.7	9.8	5.6	7.4	10.8	5.3	86	75	59	73	1.6	3.0	3.8	2.8	9	9	2	WSW 12	W 7	WNW 9
26	104.4	106.7	105.4	105.5	1.2	8.4	5.3	5.0	11.2	0.6	82	54	71	69	1.2	5.1	2.6	3.0	3◉	3⊙	1	NW 7	WNW 2	SSW 8
27	103.3	103.8	103.9	103.7	8.3	12.7	10.3	10.4	14.1	5.3	89	72	62	74	1.2	4.2	4.8	3.4	1◉	4◉	6	SSW 13	S 8	WSW 9
28	104.2	105.4	105.8	105.1	4.9	9.1	6.3	6.6	10.9	3.8	66	42	37	48	3.0	6.7	5.9	5.2	6◉	7⊙	1	W 9	WNW 5	W 7
29	104.3	105.1	104.1	104.5	5.5	11.1	7.8	8.0	12.6	4.4	85	53	82	73	1.3	6.2	1.9	3.1	1⊙	3⊙	9	SW 8	WSW 5	W 11
30	102.7	103.9	103.4	103.3	1.4	1.7	0.0	0.8	7.9	0.0	100	96	98	98	0.0	0.3	0.1	0.1	10 ≡	9⊙	1	N 8	W 4	NNW 1
31	101.0	100.6	99.7	100.4	3.0	7.9	1.6	3.5	8.8	-0.9	25	52	100	59	5.7	5.2	0.0	3.6	7	7⊙	10	WNW 9	WNW 3	WNW 4
M	103.0	103.6	103.4	103.3	7.0	10.1	7.8	8.2	12.1	5.3	81	74	83	79	2.0	3.5	2.1	2.5	6.0	7.6	5.7	5.8	4.6	5.6

Kasprowy Wierch H_s=1991m H_L=1988,8m h_w=15,4m Lipiec - Juillet 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	7	6.9	pł.	⚠°0^00-50 ⚹°-1^15 25-16^10 ⚹°16^50 17^45 18^15...50 ⚹°-1^19 19 ⚹°-1^19 32 22^43-23^25, v°0^00-9^50, ≡²0^00-8^45 ≡-10^25 ≡²-12^40 ≡-14^25 ≡²-15^10 ≡-21^20 ≡²-24 ▭ 20^40-21^20, ⊓ 16^15-40, ⚹°-1^15 58-16^10 19^15-50
2	7	2.5	pł.	⚹°-1^11 55-12^15 13^02-25 13^45-14^15 ⚹°14^50-15^10 ⚹°15^20-45 ⚹²-16^10 ⚹°-16^15 ⚹°21^05-30, (⚹)°11^30-45, ∾°2^50-7^10, ≡²0^00-2^20 3^40-4^45 ≡-5^20 8^30-11^05 12^50-13^10 13^45-15^30 ≡²-16^10 ≡-18^20, 21^35-22^10
3	8	3.4	1	⚹°1^55-5^00 5^50-6^40 8^10-15 8^50 10^05 ⚹⚠°11^50 12^45 ⚹°13^30 ⚹°-16^20 ⚹°-17^30 ⚹⚹°18^30 ⚹°19^50 21^15-23^50, v°2^30-6^30, ≡1^15-30 ≡²-2^40 ≡-3^10 ≡²-4^45 ≡-9^45 12^15-14^10 ≡²-17^45 ≡-18^25 ≡²21^30-24, ≫10^20
4	8	0.0	1	⚹°1^45-3^20 4^15-5^30 ⚠°6^20-7^15 ⚹°8^15, v°na-8^15, ≡²0^00-4^30 ≡-6^30 ≡²-8^05 ≡-8^20 8^45-10^30 ≡11^05-40, ≫20^40-22^30 [3.VII: -13^00 (por.25), 15^30 19^30 (por.22)
5	7	6.7	pł.	⚹°15^35 17^40 ⚹⚠°-1^19 30 ⚹°-22^30, ⊔ 0^50-8^30 v°22^00...24, ≡10^35-12^10 13^20-45 14^30 17^20 ≡²-24
6	7	0.0	1	⚹°14^27-37 ⚹°15^05-10 15^50-16^05 21^25-35, (⚹)°19^50-20^15 NE, 20^51-21^30 SE-E, v°0^00...2^30, ≡²0^00-30 ≡-1^15 ≡²-2^30 4^20-5^25 ≡9^30-12^50 21^10-30
7	7	2.0	pł.	⚹°9^40 10^45 11^40-12^20 14^10...35 ⚹°15^05 ⚹▲°-15^20-25 15^45 16^02 ⚹°16^15-25 ⚹°22^50-23^20, (⚹)°15^10-30 16^50, ⊔ 1^00-5^10 v°23^00-24, ≡9^05 12^30 13^30-18^00 20^40-21^00 23^15-24
8	7	7.1	1	⚹°8^40-9^10 ⚹°11^15-30 ⚹°12^50 13^05 ⚹⚹°13^35 ⚹°-13^45 ⚹°-13^50 ⚹°-16^48 17^20 ⚹°-19^50 20^50 ⚹°-21^05, v°0^00-12^10, ≡0^00-10 1^50-2^10 ≡²-5^05 ≡-6^10 ≡²-7^45 ≡-9^10 ≡²-12^10 ≡-16^00 ≡²-17^20 ≡19^20 20^10 ≡²-20^45
9	8	.	pł.	≡²0^00-3^30 ≡...7^50, 10^30-11^50 [8.VII: ≡-21^15 ≡²-24, ⚹°-1^16 48 17^15, 20^30-40
10	7	0.0	pł.	⚹⚠°13^24-27 ⚹°-14^10, 17^40...18^10 21^41-44, ⌓°1^00-8^30, ≡19^30-21^30
11	8	4.9	pł.	⚹°14^35 15^10 15^50 16^30 ⚹°-17^30 ⚹°19^10 20^30, (⚹)°16^23-18^00 WNW-SW-SE, 19^50-20^30 S ⚹°21^50 WNW, 22^55 23^35-24, ⌓°4^00-5^50, ≡0^40-2^30, ≫4^50-6^50 (por.17), ⊕°-10^50-12^15, ⚹°19^45-20^30
12	8	5.0	pł.	⚹°0^00-2^15 W-SW, 22^20-24 NE-W, ≡5^50-7^05, 10^30-11^15, ≫1^30-2^00
13	8	0.8	pł.	⚹⚠°0^45-48 ⚹°1^10 2^55-3^30 4^05-30 10^07-30 ⚹°-16^06-45 ⚹°18^08...30, ⚹°2^55-3^45 W-N-NE, ≡²2^40-3^50 16^15-40 ≡-17^15 ≡²20^30-21^30 ≡...24, ≫3^05-30 17^50-18^15 18^30-19^10 (por.16), ⚹°0^45-3^30 16^23-35
14	7	0.7	pł.	⚹°11^40-12^20 15^45-17^05 21^35-42 21^55-23^10, ≡0^00-40 ≡²1^30-2^40 ≡-3^30 5^20-6^45 16^05-17^20, ≫18^30-19^20 20^15-23^30 (por.19)
15	8	4.7	pł.	⚹°3^55...6^30-9^40 11^50-15^05, ≡8^50-9^25 ≡²-11^50 ≡-13^05 ≡²13^45-16^05 ≡-22^05 23^45-24, ≫19^20...23 (por.15)
16	8	5.8	pł.	⚹°15^45-50 ⚹▲°-1^16 11 ⚹°-16^17 ⚹▲°-16^20 ⚹°-16^35, ⚹°16^05, ⌓°3^45-8^30, ≡0^00-30 5^30-6^40 7^45-8^40 ≡²-9^05 ≡-9^30 ≡²-9^45 ≡-12^30 ≡²15^30-16^05 16^40-17^45
17	7	17.1	pł.	⚹°12^35-53 ⚹▲°-13^01 ⚹°-14^03 17^50-18^40 19^50-20^10, (⚹)°12^28-16^00 NW-N-NE ⚹°21^27-45 NW, ⌓°0^45-8^40, ≡8^25-10^35 ≡²-10^50 ≡-12^30 ≡²-12^45 ≡-14^05 16^10-25 17^15-18^35 ≡²-19^10 ≡-21^05 ▭-21^25 ≡21^50...
18	0	143.8	pł.	⚹°3^20-4^00 ⚹°-4^20 ⚹⚹°-8^05 ⚹°-1^17 10 ⚹°-2^24, (⚹)°6^50-7^15 E, ⌓°1^10-3^20, ≡²1^20-40 ≡-2^30 ≡²-24, ≫18^05-24, ⚹°7^15...30 [17.VII: 23^10, ()4^30-8^20 19^45-20^40
19	0	40.1	pł.	⚹°-2^00-16^15 ⚹°-1^24, ≡²0^00-24, ≫0^00-10 2^30...14^30 ⚹-20^30 (por.23) ≫-24 (por.19)
20	8	.	.	⚹°0^00-35 1^05...3^35, ≡²0^00-10^50 ≡...11^50, ≫0^00-3^40
21	8	.	.	⌓°4^50-8^30
22	8	18.0	.	⚹°18^00-05 ⚹°18^30-40 ⚹°-1^19 50-20^20, (⚹)°-1^17 25-19^45 NW, NE-E-SE ⚹°-20^30 SE-S ⚹°21^20-22^00 N, ⌓°0^30-8^30, ⚹°-1^19 45-20^10
23	6	28.1	.	⚹°2^-1^25-5^50 ⚹°6^45 7^45 ⚹°-8^35 ⚹°13^55-14^15 ⚹°16^50-18^05 ⚹°-18^30 ⚹°-19^10 ⚹°20^02-55 ⚹°-22^10 ⚹°-1^23 05 ⚹°-24, (⚹)°0^56-2^30 NW, NE (⚹)°18^12-19^15 NNE-NE ⚹°20^36-21^30 S-E-N, ≡0^40-45 ≡²-4^30 6^30-
24	1	.	.	⚹°0^00-20 1^10-30 ⚹°2^02-45, ⌓°22^30-24, ≡²0^00-13^50 ≡-16^30 20^20-21^25 [23.VII: 9^45 ≡-10^05 ≡²-11^55 ≡-12^15 ≡²-13^35 ≡-16^10 ≡²-17^35 ≡-18^30 ≡²-24
25	8	.	.	⌓°0^00-9^20
26	8	.	.	
27	9	0.1	.	⚹°8^45-9^05 15^20-30, (⚹)°14^51-16^30 NE-NE, E, 18^55-19^00 SW ⚹°22^50-24 S-E, ≫2^00-3^10 23^15-24 (por.16); ()6^20-10^15
28	1	0.0	.	⚹°6^30-8^15, ⌓°21^30-24, ⚹°0^00-2^00 S-E, ≡1^30-2^10 ≡²-3^30 ≡-5^20 ≡²-9^50 ≡-13^15 ≡²-13^55 ≡-15^10 ≡²-16^15 ≡-17^30 18^20-19^15, ≫0^00-30
29	8	.	.	⌓°0^00-7^00, ≡²0^40-2^30 ≡-3^05 ≡²6^30 ≡-8^45 ≡²-9^35 ≡-11^30 19^45...20^20, ⊕13^50-14^35, ()18^50-19^30
30	9	.	.	⌓°4^30-7^30, ≡19^45-21^05 21^20-45 ≡²-23^40 ≡-23^50, ⊕7^50-8^10, ()4^40-20^30 21^05-20
31	9	.	.	⌓°-1^4 00-5^00 21^30-24, ≡0^30-4^30 5^40-6^15 ≡²-8^20 ≡-9^10 ≡²-11^30, ()11^30-17^00 20^30-24
Σ	—	297.7	—	UWAGI

Sierpień - Août

1	8	0.0	.	⚹°16^33-17^10, ⌓°0^00-4^00
2	7	.	.	(▭)4^30-6^50
3	8	6.4	.	⚹°17^50-18^05 18^21-35 ⚹°-1^2-19^05 ⚹°-19^20, ⚹°-1^18 30-19^30 W-N-NE ⚹°21^20-22^30 W, ≡14^12...18^15 ≡²-18^40 ≡20^40-21^10, ≫18^35-50 (por.18)
4	8	.	.	⚹23^50 N
5	8	10.5	.	⚹°15^01-02 15^40-16^03 ⚹°-1^18 29-19^35 ⚹▲°-1^2-19^40 ⚹°-1^21 15, (⚹)°13^20-14^30 W, 15^12-40 NE ⚹°16^15 ⚹°-1^18 35-20^30, ⌓°0^00-1^50 ⌓°-8^00, ≡18^50-19^00 ≡²-20^30 ≡-21^40, ≫19^02-20 19^35-22^30, ⌒²20^05-14, ()
6	9	.	.	⌓°5^00-8^00 ⌓°21^00-24, (▭)8^30-9^30, ()9^00-17^00 [5.VIII: 19^45-20^10, ⚹°15^30-16^00
7	9	0.9	.	⌓°0^00-4^00, (▭)4^30-8^30 ≡22^10-40 ≡²-24, ≫0^45-9^30 (por.19) ⚹-11^40 (por.33) ≫-21^20 (29), ()4^30-9^30 13^30-14^10
8	9	.	.	⚹°3^00-7^20, ≡²0^00-7^50 ≡-9^40 ▭8^40-9^20 ≡10^45-11^15 19^30-21^15 ≡²-24, ≫1^40-2^20 (por.18); ()9^40-20^30
9	8	.	.	≡²0^00-1^40 ▭1^45-4^15 ≡²-9^40 ≡-11^20 17^35-19^40 ≡²-21^30 ≡-22^20 ▭-23^15
10	8	.	.	
11	8	.	.	⌓°22^30-24, ⊕°23^40-24 ⊔°22^50-24
12	8	.	.	⌓°0^00-2^00, ⊕°0^00-50 ⊔°0^00-1^20, ⊕°8^40-13^45 15^40-17^50, ()18^40-20^50
13	8	.	.	
14	4	6.7	.	⚹°17^42-45 ⚹▲°-1^17 51 ⚹°-18^2, (⚹)°16^43-17^00 NW, 17^35-18^30 NW-E, ⌓°1^00-8^30, ≡11^45-55 ≡²-12^40 ≡-13^45 18^07-27, ⌒°17^57-18^07, ⚹°-1^17 35-18^06, ()19^30-21^20
15	8	18.8	.	⚹°-1^46-3^07 ⚹°23^55-24, (⚹)°0^50-2^30 NW-W, 23^22-45 NW-N ⚹°23^45-24, ≫20^25-22^40 (por.23), ⚹°1^58-2^05 23^22-24
16	0	14.9	.	⚹°0^00-03 3^30-4^10 ⚹▲°6^40-45 ⚹°7^05 ⚹°-9^20 ⚹°10^07-14^15, ⚹°0^00-10 NE (⚹)°-4^30 NE-N, NW ⚹°6^42-50 ⚹°-9^30, ≡3^40-50 ≡²-4^30 ≡-4^40 5^50-9^35 ≡²-17^35 ≡-18^45 21^10-35 ≡²-22^30, ≫7^00-8^00
17	8	.	.	(⚹)°15^40-17^30 S-SE, ⌓²0^30-8^50, ≡13^45-14^30 19^50-20^30 21^30-22^00, ()8^30-12^30 [16.VIII: ⚹°-0^00-1^40 2^50-4^40 ⚹²6^40-7^10
18	8	1.4	.	⚹°12^48-13^30 15^15-19^05 ⚹°-20^30-22^45, ≡-3^40-4^30 15^17-16^20 ≡²-18^50 ≡-20^05 ≡²-22^40 ≡-24, ()7^15-9^40
19	8	5.5	.	⚹⚠°17^01-10 ⚹°-17^40 ⚹°-18^05 ⚹°-18^45 ⚹°-19^45 20^05-30 21^20-24, ≡0^00-20 ≡²-3^20 ≡-4^40 5^20-6^05 17^30-18^10 ≡²-24, ≫13^30-45 15^50...17^40 (por.17)
20	0	5.2	.	⚹°0^00-1^10 1^55...2^10-5^20...7^25 ⚹⚠°...7^30 ⚹°...16^50 ⚹°-19^50 ⚹⚹°-21^25 ⚹°-22^35 ⚹°-24, ≡²0^00-24, ≫1^30-2^30 (por.17)
21	0	.	.	⚹°0^00-2^30, ≡²0^00-3^40 ≡-4^15 10^40-11^30 ≡²-15^40 ≡-24 (▭)5^50-7^15 ▭-11^30
22	0	0.5	.	⚹°9^20-10^30 13^57-14^30, ⌓°0^40-2^30 4^10-5^30 ⌓°22^40-24, ≡0^00-40 10^10-12^20 ≡²-19^30 ≡-19^50 ≡²-20^20 ≡-20^45 21^20-40
23	8	.	.	⌓°0^00-8^20
24	9	0.2	.	⚹°8^25...11^25 15^25-40, ≡7^35-9^20, ≫9^35-11^20 (por.20) ⚹-24 (por.30); ()11^00-24
25	9	0.6	.	⚹°6^30-7^00 ⚹°14^15-15^05 15^50-17^10, ⌓²22^30-24, ≡10^30-45 12^10-40 23^35-24, ⚹0^00-2^00 (por.30) ≫-9^40 (por.18), 16^30-19^30 (por.22); ⌒°19^32-37; ()0^00-1^50 9^00...23^30
26	8	.	.	⌓°0^00-9^00 21^30-24, ≡0^00-1^40 2^30-4^20, ≫23^30-24
27	8	.	.	⌓°0^00-1^10 5^40-7^50, ≫0^00...12^20 14^00-25 (por.21), 15^30-16^40 (por.20)
28	8	.	.	⌓°7^00-8^30, ≫1^25-3^30 (por.21); ()14^30-21^30
29	8	1.7	.	⌓°2^30-7^40, ≡²23^40-24, ≫21^20-24 (por.19); ()6^00-45
30	8	.	.	⚹°1^07-3^15, ≡²0^00-8^50 ≡-9^10 ≡²...12^10 ≡-12^50 18^30-45 ≡²-19^40 ≡-20^45 ≡²-21^03, ≫0^00-40 (por.17)
31	8	1.1	.	≡19^30-21^50 ≡²-24; ()5^40-11^30
Σ	—	74.0	—	UWAGI.

Kasprowy Wierch φ=49°14' λ=19°59' Wrzesień - Septembre 1962

DNI	CIŚNIENIE P=700 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	98.9	101.9	104.4	101.7	-1.0	-0.2	0.0	-0.3	1.6	-1.6	99	98	100	99	0.1	0.1	0.0	0.1	10 ≡	10 ≡	10 ≡	N 6	N 5	N 4
2	105.9	107.8	107.4	107.0	0.7	6.9	4.8	4.3	9.0	-1.3	86	83	69	79	0.9	1.6	2.7	1.7	1 ⊙	5 ⊙	1	SW 2	SSE 2	SSW 4
3	106.1	106.7	105.8	106.2	8.4	12.3	8.3	9.3	13.0	4.3	35	56	60	50	7.1	6.2	4.3	5.9	1 ⊙	1 ⊙	1	C 0	SW 1	SSW 4
4	103.7	104.0	101.6	103.1	9.1	13.9	9.2	10.4	15.3	7.6	61	56	79	65	4.4	7.0	2.4	4.6	1 ⊙	4 ⊙	0	SSW 6	SW 5	S 9
5	96.7	98.0	97.7	97.5	9.5	12.2	6.0	8.4	13.8	5.2	81	71	62	71	2.3	4.1	3.6	3.3	1 ⊙	7 ⊙ (R)	2	S 15	WSW 13	W 10
6	96.7	97.7	97.2	97.2	4.6	7.4	7.9	7.0	8.3	3.5	91	92	100	94	0.7	0.8	0.0	0.5	9	7 ⊙	9	SW 11	WSW 12	WSW 12
7	95.4	94.4	94.7	94.8	8.0	7.0	4.0	5.8	9.6	3.6	97	100	68	88	0.3	0.0	2.6	1.0	9	10 ●	9	SW 6	W 8	WNW 4
8	96.3	97.4	98.9	97.5	3.2	3.5	2.2	2.8	4.4	1.4	86	94	68	83	1.1	0.4	2.3	1.3	9	9	1	SSW 6	SW 6	W 11
9	100.1	102.8	105.0	102.6	-1.2	-1.2	-1.8	-1.5	2.7	-2.4	99	99	98	99	0.1	0.1	0.1	0.1	10 ✳ ≡	10 ✳ ≡	1	N 6	NNE 4	NNE 1
10	105.3	106.2	105.8	105.8	5.4	7.8	10.7	8.6	11.2	-2.2	25	49	3	26	6.8	5.4	12.5	8.2	8 ⊙	1 ⊙	0	SSW 7	SW 6	S 6
11	104.9	105.6	104.8	105.1	8.9	12.2	6.8	8.7	13.1	6.5	45	50	100	65	6.2	7.2	0.0	4.5	2 ⊙	8	10 ● ≡	WSW 5	W 8	WNW 11
12	104.1	104.3	101.1	103.2	6.0	11.9	12.4	10.7	14.1	4.1	82	69	73	75	1.7	4.4	4.0	3.4	8	4 ⊙	3	W 8	WSW 8	SSW 14
13	100.3	101.3	101.8	101.1	4.2	4.3	-1.1	1.6	12.6	-1.3	94	100	99	98	0.4	0.0	0.1	0.2	9	9 ●	10 ≡	WNW 13	WNW 8	N 9
14	103.6	105.3	105.1	104.7	-2.8	1.9	1.7	0.6	4.4	-3.2	95	71	50	72	0.2	2.0	3.5	1.9	9	1 ⊙	1	N 2	W 1	SSW 5
15	103.4	103.9	102.1	103.1	2.9	7.9	5.9	5.6	9.1	0.8	23	33	44	33	5.8	7.1	5.1	6.0	1 ⊙	1 ⊙	1	SSW 4	SW 4	SSW 7
16	101.1	101.1	98.6	100.3	9.2	12.3	5.1	7.9	13.0	4.4	21	38	63	41	9.2	8.8	3.3	7.1	1 ⊙	1 ⊙	1	SW 6	SSW 6	SSW 10
17	96.2	94.9	94.0	95.0	6.9	6.3	6.2	6.4	7.9	3.5	93	100	100	98	0.6	0.0	0.0	0.2	7	10 ● ≡	10 ● ≡	SW 10	WSW 12	SW 6
18	92.6	90.1	90.4	91.0	4.0	4.2	1.0	2.6	6.3	1.0	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ● ≡	10 ≡	SSW 3	S 11	SW 8
19	92.9	96.0	96.9	95.3	-2.9	1.6	-2.4	-1.5	3.2	-5.4	93	77	96	89	0.3	1.6	0.2	0.7	5 ⊙	4 ⊙	10	S 7	SSW 2	N 1
20	97.8	99.6	100.0	99.1	-3.5	-0.2	-1.6	-1.7	2.5	-4.1	83	98	94	92	0.8	0.1	0.3	0.4	0 ⊙	9	4	WNW 1	C 0	NW 3
21	99.7	99.7	99.3	99.6	-3.1	-2.0	-3.4	-3.0	-1.6	-5.5	97	98	97	97	0.1	0.1	0.2	0.1	10 ≡	10 ✳ ≡	10	N 4	WNW 6	N 3
22	96.9	98.4	100.1	98.5	-3.1	-2.8	-3.0	-3.0	-2.2	-4.2	97	95	97	96	0.1	0.2	0.1	0.1	10 △ ≡	10 △ ≡	10 ≡	NNW 4	N 2	W 4
23	98.9	98.4	97.3	98.2	-3.3	-3.2	-2.7	-3.0	-2.4	-3.5	95	97	97	96	0.3	0.1	0.1	0.2	10 △	10 ✳ △ ≡	10 ✳ △ ≡	NNW 3	WNW 6	NW 5
24	99.5	101.7	103.8	101.7	-3.1	-1.1	-3.4	-2.8	-0.8	-3.5	97	99	97	98	0.1	0.1	0.2	0.1	10 △ ≡	10 ✳ △ ≡	2	N 4	C 0	NNE 1
25	104.7	106.4	106.1	105.7	-2.8	-0.3	-0.7	-1.1	0.7	-4.4	90	86	87	88	0.5	0.9	0.8	0.7	1 ⊙	7 ⊙	0	SE 4	ESE 5	C 0
26	105.0	103.9	102.3	103.7	3.8	6.4	4.7	4.9	8.4	-0.9	45	76	32	51	4.2	2.3	5.8	4.1	2 ⊙	4 ⊙	0	C 0	SSE 1	ENE 3
27	99.3	98.9	98.2	98.8	5.5	4.5	4.0	4.5	6.2	2.4	24	67	71	54	6.8	2.8	2.3	4.0	7 ⊙	9 ⊙	6	C 0	WSW 5	S 1
28	96.7	97.2	96.9	96.9	2.9	3.5	2.6	2.9	6.0	1.7	80	98	96	91	1.5	0.1	0.3	0.6	2 ⊙	9	1	SSW 1	SW 2	S 2
29	97.1	98.6	100.5	98.7	2.3	4.5	2.9	3.2	5.6	1.5	80	83	96	86	1.5	1.4	0.3	1.1	7 ⊙	8	0	C 0	WSW 2	SSW 3
30	101.8	103.3	104.6	103.2	3.2	7.9	4.2	4.9	8.5	1.9	59	78	87	75	3.1	2.3	1.0	2.1	4 ⊙	9 ⊙	0	SSW 1	ESE 2	WSW 1
31																								
M	100.1	100.8	100.7	100.5	2.7	5.0	3.0	3.4	6.8	0.5	75	80	79	78	2.2	2.2	1.9	2.1	5.8	6.9	4.4	4.8	5.1	5.4

Październik - Octobre

1	105.6	107.1	108.1	106.9	4.2	9.5	5.4	6.1	10.8	3.3	75	69	88	77	2.1	3.6	1.1	2.3	0 ⊙	2 ⊙	1	N 2	ESE 1	NNW 2
2	108.2	109.1	109.1	108.8	6.5	11.1	6.7	7.8	11.8	4.9	19	67	65	50	7.8	4.4	3.4	5.2	1 ⊙	1 ⊙	0	NE 2	SSW 1	SSW 1
3	108.4	108.8	108.7	108.6	7.3	11.5	7.0	8.2	12.7	5.4	27	71	77	58	7.4	4.0	2.2	4.5	1 ⊙	2 ⊙	0	NE 3	C 0	W 1
4	107.7	108.6	107.6	108.0	7.1	9.8	6.3	7.4	11.6	6.0	27	75	92	65	7.4	3.0	0.7	3.7	1 ⊙	2 ⊙	1	ENE 3	ENE 1	NNE 2
5	105.5	105.9	105.7	105.7	4.4	8.0	2.4	4.3	8.4	2.1	100	67	96	88	0.0	3.5	0.3	1.3	10 ≡	8 ⊙	2	NNE 3	NNE 2	NNE 4
6	104.7	105.3	106.0	105.3	1.8	2.1	0.5	1.2	3.6	0.4	85	100	100	95	1.1	0.0	0.0	0.4	9	10 ● ≡	10 ≡	NNE 5	N 5	NNE 8
7	107.4	108.9	110.9	109.1	0.3	0.4	1.2	0.8	1.6	-0.5	100	100	92	97	0.0	0.0	0.6	0.2	10 ≡	10 △	1	ENE 8	NE 6	E 2
8	112.4	113.8	113.5	113.2	5.0	8.4	4.3	5.5	8.8	1.0	55	55	36	49	3.8	4.9	5.3	4.7	1 ⊙	1 ⊙	0	E 4	C 0	NE 4
9	112.8	112.6	110.9	112.1	6.9	9.7	7.0	7.6	10.3	4.1	27	57	28	37	7.3	5.1	7.2	6.5	1 ⊙	1 ⊙	1	NE 1	ENE 2	ENE 2
10	108.4	107.7	106.4	107.5	6.4	10.9	7.0	7.8	11.5	6.1	26	46	39	37	7.2	7.0	6.1	6.8	1 ⊙	1 ⊙	1	C 0	C 0	C 0
11	104.6	103.9	102.0	103.5	6.1	8.3	6.0	6.6	9.1	4.7	36	50	35	40	6.1	5.6	6.1	5.9	1 ⊙	1 ⊙	1	C 0	SSW 2	SSW 3
12	100.1	100.7	101.2	100.7	5.1	6.0	3.2	4.4	8.0	2.6	18	70	78	55	7.2	2.9	1.8	4.0	2 ⊙	1 ⊙	1	SW 3	W 2	SSW 4
13	101.7	102.5	100.5	101.6	3.4	6.0	1.3	3.0	7.2	1.2	55	76	100	77	3.5	2.3	0.0	1.9	1 ⊙	2 ⊙	3	S 1	SW 3	SSW 10
14	96.8	96.6	97.2	96.9	1.7	2.0	-1.4	0.2	2.8	-1.7	96	100	99	98	0.3	0.0	0.1	0.1	9	10 ●	10 ● ≡	SSE 11	SSW 3	NNW 3
15	98.3	100.7	102.6	100.5	-3.6	-2.9	-4.1	-3.7	-1.4	-4.9	97	97	96	97	0.2	0.1	0.2	0.2	10 ≡	10 △ ≡	10 ≡	NNE 5	N 5	NNE 1
16	101.4	101.1	100.9	101.1	-3.9	-1.7	-2.7	-2.8	-0.9	-4.8	91	96	49	79	0.4	0.2	2.5	1.0	4 ⊙	10 ≡	0	S 5	NW 1	WNW 2
17	102.1	104.0	104.7	103.6	-2.2	1.3	-0.3	-0.6	1.8	-4.7	9	80	89	59	4.8	1.4	0.6	2.3	0 ⊙	4 ⊙	1	NE 3	C 0	SSW 2
18	104.0	103.2	101.5	102.9	3.0	3.6	5.0	4.2	6.7	-1.2	70	67	63	67	2.3	2.6	3.3	2.7	2 ⊙	9 ⊙	1	W 5	SW 8	W 6
19	96.9	96.7	96.8	96.8	2.4	0.3	-2.0	-0.3	5.6	-2.5	100	100	98	99	0.0	0.0	0.1	0.0	10 ≡	10 ● ≡	10 ≡	W 13	N 6	N 4
20	96.4	98.8	102.3	99.2	-3.3	-3.7	-4.2	-3.8	-2.0	-5.1	97	97	96	97	0.1	0.2	0.2	0.2	10 ✳ ≡	10 △ ≡	10 △ ≡	N 6	NNE 7	NNE 6
21	105.1	107.3	108.4	106.9	-4.6	2.4	4.3	1.6	4.3	-7.2	42	66	42	50	2.5	2.6	4.8	3.3	1 ⊙	1 ⊙	0	NE 5	ENE 1	ENE 2
22	108.0	108.6	108.3	108.3	3.9	7.0	4.1	4.8	8.3	2.6	46	50	42	46	4.4	5.0	4.8	4.7	0 ⊙	1 ⊙	0	SE 1	C 0	C 0
23	106.5	106.7	105.5	106.2	3.5	6.6	5.7	5.4	8.4	2.7	36	39	41	39	5.0	5.9	5.4	5.4	1 ⊙	0 ⊙	0	C 0	SW 3	C 0
24	103.4	103.3	102.6	103.1	4.4	5.7	2.9	4.0	6.3	1.2	17	31	52	33	6.9	6.4	3.6	5.6	0	0 ⊙	0	SSW 6	SSW 6	S 10
25	101.5	101.7	101.3	101.6	1.6	4.1	2.8	2.8	4.4	0.5	36	45	39	40	4.3	4.3	4.6	4.3	1	0 ⊙	0	SE 6	WSW 7	SSE 7
26	99.8	100.1	98.6	99.5	0.4	3.7	-0.3	0.9	4.6	-0.8	64	54	77	65	2.3	3.7	1.4	2.5	0	2 ⊙	4	S 10	S 9	SSW 10
27	96.8	98.5	98.6	98.0	-1.7	4.6	3.2	2.3	5.4	-2.3	84	57	17	53	0.9	3.7	6.3	3.6	1	2 ⊙	2	SSW 11	SSW 4	SSW 7
28	96.1	94.7	92.3	94.4	0.8	2.5	0.3	1.0	3.5	-1.4	49	64	100	71	3.4	2.7	0.0	2.0	7	8 ⊙	10 ● ≡	S 12	SW 9	SSW 10
29	90.5	91.5	94.4	92.1	-1.6	-0.1	-1.2	-1.0	1.2	-2.4	98	100	80	95	0.1	0.0	1.1	0.4	2	9	10	SSE 1	SE 1	SSE 4
30	96.2	96.2	94.9	95.8	-0.7	-0.6	-0.2	-0.4	0.4	-2.3	81	99	90	90	1.1	0.0	0.6	0.6	9	9	7	SW 4	SW 4	S 10
31	92.3	92.3	91.0	91.9	0.8	1.7	4.1	2.7	4.6	-2.3	100	100	100	100	0.0	0.0	0.0	0.0	10 ✳	10 ≡	10	SE 6	S 7	SE 13
M	102.6	103.1	103.0	102.9	2.1	4.3	2.4	2.8	5.8	0.2	60	72	71	68	3.2	2.8	2.4	2.8	3.7	4.7	3.3	4.7	3.4	4.3

Kasprowy Wierch H_s=1991m H_c=1988,8m h_w=15,4m Wrzesień - Septembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	0	2.7	1	♎°6^50-7^00 * ♎°-7^20 ♎°-7^45 8^20-9^15 10^10-25 11^35-13^10 13^45-14^10 ♎°17^05-35 21^50-22^00 v°4^30-10^00 ≡² 0^00-45 ≡ -2^40 3^15-30 ≡² -18^45 ≡ -19^05 ≡² 19^40-24
2	9	·	pł.	≡² 0^00-1^25 ≡ -4^20 ⊕² 18^38-19^15 () 7^40-24
3	8	·	·	() 0^00-8^50
4	8	·	·	≫ 23^30-24 (por 17)
5	8	3.9	·	•°12^35-40 15^05-17 16^40-17^10 18^35-19^25 (K)°13^35-15^00 NW 15^20-16^40 SE E (K)°17^30 ≡ 14^30-16^40 ≡² -19^40 ≫ 0^00-1^45 (por 18) ♋-7^30 (por 34) ≫ -9^30 (por 22) 13^15-15^40 (por 20) 17^40-18^20 (por 17) 21^20
6	8	3.9	·	•°9^50-10^05 15^45-18^20 18^50 21^10 ≡ 8^25-9^20 ≡² -10^03 ≡ -13^07 15^40-17^40 ≡² -20^10 ≡ -22^30 ≫ 5^20-13^50 (por 20) 14^00-10 16^00 17^45 18^15-22^05 (por 22) 22^20-24 (por 20) () 0^00-8^30
7	8	2.4	·	•°4^45-6^10 •°-6^25-7^25 •°12^45-14^10 14^35-17^10 •°-18^20 ≡ 5^55-6^20 ≡² -7^05 ≡ -7^45 8^25-9^40 10^15-12^30 15^00-16^30 17^20 18^10 ≫ 0^00-5^05 (por 23) 12^30-13^10 (por 16) 15^35-16^05 (por 23) ♋ 16^05-17^30
8	8	2.5	·	•°16^50-17^02 17^48-18^20 ≡ 8^15-12^40 16^30-17^45 ≫ 0^00-20 19^20-24 (por 18) () 0^00-11^30 18^30-24
9	0	9.1	1	* °°6^45-8^05 * ♎'-8^45 * °-10^05 * ♎°10^25-51 12^45-13^02 * °13^30-14^15 (K)°8^10-45 E v°5^45-11^25 12^05 15^33 16^20-17^10 18^25-19^30 ≡ 2^40-3^20 ≡² 5^40-11^25 ≡ -12^05 ≡² -15^33 ≡ -16^20 ≡² -17^10 ≡ -18^25 ≡²
10	9	·	3	() 5^50-20^00 23^30-24
11	9	2.4	pł.	•°15^35-17^25 20^40-21^45 ≡² 20^25-23^40 ≫ 3^45-4^30 5^30-6^45 (por 16) 19^10-22^40 (por 18) () 0^00-4^00 6^30-15^40 [5.IX: -22^30 ⌒°13^10-15 () 19^40-24
12	9	·	·	≫ 8^50-9^00 (por 16) 10^10-11^15 (por 18) 12^35-45 (por 16) 16^45-18^30 (por 18) ♋-19^30 (por 24) ≫ -24 (por 21)
13	8	0.4	·	•°°12^55-13^45 •°17^45-18^20 v°20^30 24 ≡ 12^05-14^30 ≡² -18^36 ≡ -20^30 ≡² 22^40 ≡ -23^30 ≡ -24 ≫ 0^00-12^45 (por 26)
14	8	·	·	v°0^00 1^00 ≡² 0^00-6^30 ≡ -9^20 ≡² -11^05 ≡ -11^30 () 22^30-24 [7.IX (por 24) ≫ -19^45 (por 19) ♋-20^30 (por 23) ≫ 21^30 23^15-24 (por 18) K°°6^35-45 () 18^30-24
15	9	·	·	≫ 17^50-19^30 ♨ 4^30-5^10 ⊕ 12^05-30 () 0^00-19^45
16	9	·	·	≫ 1^50-2^20 21^15-24 (por 19) () 5^30-24 [9.IX: 19^30 ≡ -20^15 ≫ 0^00-1^30 ⊥°9^27-10^05 K° 9^17-21 () 0^00-30
17	0	21.5	·	•°12^50-13^05 •°°13^34-22^30 23^35-24 ♎° 4^00-8^00 ≡ 12^30-13^10 ≡² -24 ≫ 0^00-3^30 7^10-15^30 (por 19) () 0^00-4^30
18	0	29.7	·	•°0^00-1^30 °5^35-7^15 •°°9^15-18^45 ≡² 0^00-9^15 ≡ -9^50 ≡² -11^20 ≡ -12^50 ≡² 14^05 ≡ -15^20 ≡² -18^45 ≡ -19^06 ≡² 19^25 22^05 ≡ -22^20 ≡² 23^20-24 ≫ 13^15-40 (por 15) 20^50 22^30 (por 16)
19	9	·	·	v°0^00-5^40 ⌒°2^50-7^45 ≡² 0^00-5^40 ≡ -6^10 ♎ 6^50 ≡ -7^50 8^07-11^10 ≡ 14^20-15^10 16^45-18^15 21^05-23^05 ≡² 24 () 12^30-17^30
20	8	·	·	v°1^30-4^10 ⌣ 22^30-24 ≡ ² 0^00-4^10 ≡ 12^05-13^45
21	0	2.5	·	* °11^05-10 ♎° 11^25 11^50-14^10 16^20-50 ♎°°-17^45 ♎° 19^05-55 23^50-24 ⌣ 0^00-1^30 v°8^30 13^25-45 14^05-20 16^20-17^15 18^50-21^15 22^30-24 ≡² 1^30-8^30 ≡ -9^20 11^03-40 12^07-25 ≡² 13^25-45 ≡ -14^05 ≡² 14^20 ≡ -14^30 ≡² -16^20-
22	0	15.2	2	♎° 0^00-7^45 * ♎'-7^52 ♎° 8^40-9^45-10^15 * °-12^40 * ♎°-13^10 ♎° 21^10 v°0^00-24 ≡ 0^00-24 [21.IX: -17^15 ≡ -17^30 18^40-50 ≡² -21^15 22^30-24
23	0	10.8	11	♎° 3^30-6^45 7^20-8^30 * ♎°-15^30 ♎°-16^20 * ♎°-24 v°0^00-24 ≡² 0^00-7^05 ≡ -8^15 ≡² -24
24	0	0.7	21	* ♎°-0^00-4^30 ♎° 5^40 7^25 – 9^07 * °-11^20 ♎° 11^51-13^25 * ♎°-13^50 ♎°-14^40 * °-15^30 * ♎° 18^15-19^20 * °20^30 v°0^00-9^02 9^27-17^35 17^50-20^30 ≡² 0^00-9^02 ≡ -9^27 ≡² -17^35 ≡ -17^50 ≡² -20^30 ≡ -21^45
25	9	·	22	(♎) 4^30-13^00 () 6^50-17^30
26	9	·	18	(♎) 4^30-8^30 () 5^30-14^45 17^30-24
27	9	·	9	≡ -16^20-17^25 ⊕ °11^45-13^15 13^50-14^45 () 0^00-14^15
28	8	0.2	5	•°16^20-18^30 ≡ 12^10-14^30 16^10-20^30 21^40-22^30 ≡² -23^40 ≡ -24
29	8	·	3	⌒°5^50-7^45 ⌓' 21^00-24 ≡ 0^00-30 5^30-50 6^20-45 14^20-18^30
30	7	·	pł.	⌓' 0^00-2^30 ⌣' -8^30 ⌓° 19^50-23^15 ⌣° 24 ⊕ 8^35-9^40 () 8^50-9^40
31				
Σ	—	107.9	—	UWAGI

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1	8	·	pł.	⌣° 0^00-7^25 ⌓° 19^30-24
2	9	·	pł.	⌓° 0^00-5^30 23^30-24 () 8^30-13^30
3	9	·	pł.	⌓° 0^00-5^50 () 9^00-17^00
4	8	·	·	⌓' 20^30-22^40 ≡ 22^40-23^45 ≡² 24 () 6^00-12^30
5	8	·	·	≡² 0^00-45 ≡ -1^10 ≡² 5^40-9^05 ≡ -9^20 ≡² 14^30-18^20 19^40-20^15 ≡ 21^20-22^15
6	0	8.5	·	♎° 8^25-9^30 ♎'-10^15 ♎°-14^30 ♎'-16^20 ♎° 22^30-24 ≡ 7^21-9^30 ≡² -24
7	5	0.0	·	•°0^00-15 ♎° 12^20 13^10 ⌓° 20^30-24 ≡² 0^00-8^25 ≡ -10^40 11^30-12^45 ≡² -19^30 ≡ -20^20
8	9	·	·	⌓° 0^00-5^00 (♎) 4^00-8^30 () 5^30-24
9	9	·	·	(♎) 4^30-10^00 np 24 () 0^00-24
10	9	·	·	(♎) 0^00-10^00 () 0^00-24
11	9	·	·	♨² 23^30-24 () 0^00-14^30
12	8	·	·	⌓° 4^00-6^00 ⌣' 23^30-24 ♨² 0^00-3^00 () 1^30-12^30
13	9	·	·	⌣' 0^00-8^30 ⌓° 19^00-30 ≡ 19^30-24 ≫ 19^45-21^40
14	8	0.6	·	•° 8^20-12^45 17^10-18^20 20^15-21^40 ♎° 23^45-24 ⌒° 20^45-21^45 23^50-24 ≡ 0^00-6^15 8^20-16^15 ≡² -24 ≫ 1^15-8^00 (por 16)
15	0	1.3	·	♎° 0^00-3^40 ♎° 7^50-8^02 8^35-10^40 12^35-14^08 ⌒° 0^00-3^50 v°'-7^50 8^10-22^35 ≡² 0^00-7^50 ≡ -8^10 ≡² -22^35 (♎) -24
16	0	·	1	(♎) 0^00-11^40 ≡ 9^40-11^40 ≡² -14^15 ≡ -16^30 ≡² -19^30 ♎ -20^15 (♎) -24
17	9	·	pł.	(♎) 0^00-10^00 ≡ -7^45-8^15 14^20-15^30 ♎ 16^15-18^00 ♋' 14^00-16^00 () 8^30-13^00
18	9	·	·	(♎) 5^00-18^30 ♨° 22^00-30 () 8^30-24
19	0	0.2	·	♎♎° 11^40-13^15 ♎°-15^15 ⌓° 1^00-3^30 v°18^00 24 ≡² 5^35-6^55 ≡ -9^20 10^15-40 ≡² -16^50 ≡ -17^30 ≡² -24 ≫ 2^25-8^15 () 0^00-5^35
20	0	6.0	·	♗° 6^30-50 * ♎° 7^40-8^30 * ♗'-10^20 ♎° 12^15-13^30 15^50-17^40 18^05-20^45 v° 0^00-na v'-24 ≡² 0^00-22^30 ≡ -24
21	9	·	3	v'-° 0^00-4^30 ≡ 0^00-2^30 ≡² -4^30 ≡ -5^15 ♎ -10^50 ⌀ 15^00 zielony promień °16^37 () 8^30-24
22	9	·	1	() 0^00-24
23	9	·	pł.	() 0^00-24
24	9	·	pł.	≫ 19^30-24 () 0^00-24
25	9	·	pł.	≫ 0^00-2^50 23^50-24 () 0^00-10^30
26	8	·	pł.	≫ 0^00-1^30 4^45-8^30 (por 17) 11^20-12^10 (por 17) 18^20-19^20 (por 19) 20^20-24 (por 23)
27	9	·	pł.	≫ 0^00-8^10 (por 27) () 6^10-13^30
28	9	0.9	pł.	♎° 19^20-24 ≡ 15^35-18^30 ≡² -24 ≫ 2^50-10^45 (por 16) 12^00-30 20^00-22^15 (por 14) () 5^30-14^15
29	7	·	pł.	♎° 0^00-2^30 v°4^00 6^15 9^30-10^20 ≡² 0^00-4^15 ≡ -6^15 ♎ 4^15-7^25 (♎) -15^30 ≡ 7^50-10^20 11^30-17^30 ♎ 15^30-24
30	6	0.9	pł.	⌣° 19^30-21^50 ⌓° -24 ≡ 1^10-30 9^40-11^40 12^10-17^15 ♎ 0^00-18^30 ≫ 20^20-45 (por 15) 22^40-23^10 (por 18)
31	0	4.2	pł.	* 2^45-3^40 ♎° 4^45 ♎° 5^10 ♎° 6^25 * 7^15 ♎° 11^45 17^50-19^50 ⌓° 0^00-1^50 n° 4^45-5^50 ≡ 5^40-8^05 ≡² 15^15 ≡ -15^30 ≡² 18^20-20^15 ≡ -21^20 ≫ 7^00-15 (por 19) 8^30-12^00 (por 20) 18^40-24 (por 30)
Σ	—	22.6	—	UWAGI

Kasprowy Wierch φ=49°14' λ=19°59' Listopad-Novembre 1962

DNI	CIŚNIENIE P=700+ I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	89.6	89.7	90.6	90.0	4.9	3.3	3.3	3.7	5.7	2.4	93	100	100	98	0.6	0.0	0.0	0.2	9	10●	10●	SSE 8	SSE 5	SSE10
2	95.4	95.5	96.9	95.2	2.5	4.1	2.2	2.7	4.8	1.1	67	68	81	72	2.4	2.7	1.4	2.2	8	7⊙	2	SSE 7	SSW 7	SE 5
3	97.5	98.4	99.3	98.4	2.1	2.9	2.3	2.4	3.7	0.7	98	92	87	92	0.1	0.5	1.0	0.5	9	9	3	S 4	SSW 8	SSE 6
4	99.8	99.8	99.1	99.6	2.0	3.9	1.0	2.0	4.7	0.6	88	78	88	85	0.9	1.8	0.8	1.2	2	2⊙	1	S 10	SW 11	SSW 9
5	97.1	96.8	95.6	96.5	0.1	2.9	1.9	1.7	2.9	-0.3	96	75	71	81	0.3	2.0	2.0	1.4	4	3⊙	2	SSE 8	S 14	SSE10
6	92.6	93.9	96.4	94.3	0.9	0.4	0.3	0.5	2.4	0.0	86	100	100	95	0.9	0.0	0.0	0.3	7	10● =	10●△=	SSE16	SSE14	SSW14
7	100.3	102.2	103.7	102.1	2.8	3.9	2.5	2.9	4.8	0.3	98	100	100	99	0.2	0.0	0.0	0.1	5	8	10 =	S 9	SSW11	S 5
8	102.0	100.6	99.4	100.7	2.4	4.3	2.9	3.1	5.2	2.0	100	86	75	87	0.0	1.2	2.0	1.1	1	8⊙	7	S 12	SSW13	S 11
9	97.2	96.3	95.6	96.4	1.2	3.4	1.8	2.0	3.5	0.0	96	88	100	95	0.3	0.9	0.0	0.4	8	9⊙	10●	S 9	SSW 8	S 5
10	92.0	90.7	91.1	91.3	2.1	0.0	-3.0	-1.0	2.4	-3.9	98	100	97	98	0.1	0.0	0.1	0.1	10●	10●✳ =	10✳=	SE 2	NE 2	NE 4
11	95.1	94.2	94.9	94.1	-3.9	-2.3	-1.8	-2.4	-1.8	-4.0	96	98	98	97	0.2	0.1	0.1	0.1	10✳ =	10 =	10	SSE 4	S 3	SE 3
12	92.5	93.9	96.4	94.3	-0.7	-0.5	-1.9	-1.2	-0.2	-2.0	99	98	98	98	0.0	0.2	0.1	0.1	10△ =	10△ =	10 =	SSE 6	S 7	SSE 5
13	98.0	98.5	98.5	98.3	-0.9	-0.5	-0.2	-0.4	-0.2	-2.9	99	100	100	100	0.0	0.0	0.0	0.0	10 =	10✳ =	10✳△=	S 4	S 5	SSE 3
14	97.1	97.0	96.8	97.0	-0.9	-0.5	-2.7	-1.7	-0.1	-2.9	99	100	97	99	0.0	0.0	0.1	0.0	10 X =	10△ =	9	SSE 1	SSW 4	S 5
15	94.4	89.8	86.6	90.3	-5.1	-1.6	-1.8	-2.1	-1.1	-4.8	97	98	98	98	0.1	0.1	0.1	0.1	9	10△ =	10△ =	SSW11	S 14	SSW 5
16	85.7	85.9	87.8	86.5	-7.9	-9.5	-11.5	-10.1	-1.8	-12.0	96	94	93	94	0.1	0.2	0.2	0.2	10✳ =	10✳ =	10✳ =	N 4	NNW 5	NNW 5
17	89.3	88.6	87.1	88.4	-12.0	-11.3	-11.3	-11.5	-10.3	-12.4	93	97	93	94	0.2	0.1	0.2	0.2	10✳ =	7	10	C 0	SSW11	SSW12
18	83.7	82.2	81.7	82.5	-9.3	-5.5	-5.6	-5.5	-3.6	-11.9	95	95	97	96	0.2	0.2	0.2	0.2	10△	7⊙	10△=	SSE16	SW 18	SSE14
19	84.1	87.0	84.2	85.1	-6.2	-4.6	-0.2	-2.8	-0.1	-7.3	94	96	100	97	0.2	0.2	0.0	0.1	10	9	10✳=	SW 14	SSE15	SSE16
20	85.0	84.9	86.3	85.4	0.0	0.1	-6.6	-3.3	0.6	-6.9	100	100	99	100	0.0	0.0	0.0	0.0	10 =	10●✳ =	10✳=	S 18	SSE10	S 1
21	87.1	86.9	86.4	86.8	-6.0	-6.1	-4.0	-5.0	-4.0	-8.0	97	97	39	78	0.1	0.1	2.8	1.0	2	8	6	SSW 3	S 5	S 7
22	85.4	89.6	92.3	89.1	-8.0	-5.6	-4.7	-5.8	-4.0	-8.7	96	97	98	97	0.1	0.1	0.1	0.1	10	8	10✳=	S 16	SSW 7	SW 10
23	95.8	93.9	94.6	94.1	-6.6	-5.6	-7.2	-6.6	-4.1	-7.6	99	95	96	97	0.0	0.2	0.1	0.1	10✳=	10✳=	10✳=	SSW 6	S 5	SSW 1
24	96.5	98.5	100.6	98.5	-4.6	-2.7	-1.2	-2.4	-1.2	-7.3	96	97	99	97	0.2	0.1	0.1	0.1	10✳=	10✳	10△	S 3	SSE 1	SE 5
25	101.5	100.9	100.3	100.9	-2.0	-3.3	-7.6	-5.1	-1.2	-7.8	85	97	96	93	0.8	0.1	0.1	0.3	8	10✳ =	10X△=	ENE 3	ENE 7	NNE 4
26	101.7	102.0	103.0	102.2	-5.6	-3.1	-3.8	-4.1	-2.8	-7.6	97	97	96	97	0.1	0.1	0.2	0.1	10△ =	10 =	10✳ =	NE 5	ENE 8	ENE 7
27	103.7	103.9	102.8	103.5	-5.8	-3.0	-4.6	-4.5	-1.7	-6.4	97	66	53	72	0.1	1.7	2.0	1.3	3	0⊙	0	S 1	C 0	SSE 8
28	100.5	100.4	100.6	100.5	-4.5	-2.8	-1.3	-2.5	-1.3	-5.8	53	79	27	53	2.1	1.0	4.1	2.4	1	0⊙	1	SSW12	SSW 6	NNW 2
29	99.4	99.6	98.6	99.2	-5.6	-5.0	-3.2	-3.8	-0.4	-6.1	22	98	81	67	3.6	0.1	0.9	1.5	6	1⊙	0	N 1	ENE 5	SW 6
30	95.6	94.7	93.9	94.7	-3.4	-4.7	-7.5	-5.8	-2.0	-8.0	90	98	96	95	0.5	0.1	0.1	0.2	4	10 =	10✳△=	WNW 9	NNE 7	NW 8
31																								
M	94.3	94.5	94.7	94.5	-2.5	-1.6	-2.4	-2.2	0.0	-4.6	91	93	88	91	0.5	0.5	0.6	0.5	7.5	7.9	7.7	7.4	7.9	6.9

Grudzień-Décembre

1	96.4	100.5	104.4	100.5	-10.6	-13.9	-13.8	-13.0	-7.4	-14.6	94	100	100	98	0.2	0.0	0.0	0.1	10△ =	10✳=	10✳ =	NNE10	NNE 7	NNE 9
2	107.3	109.1	109.7	108.7	-15.2	-14.4	-8.9	-11.8	-7.8	-15.6	100	100	47	82	0.0	0.0	1.7	0.6	10✳ =	6⊙	0	ENE 7	NE 4	ENE 3
3	108.2	107.4	105.6	107.1	-5.4	-3.8	-4.6	-4.6	-2.0	-9.8	41	33	40	38	2.4	3.1	2.6	2.7	1	2⊙	0	S 3	ENE 2	NE 3
4	103.3	103.0	102.6	103.0	-5.3	-4.0	-4.1	-4.4	-3.1	-6.1	32	32	18	27	2.8	3.1	3.7	3.2	2	1⊙	1	NE 4	NE 4	NE 6
5	100.9	100.0	102.1	101.0	-3.2	-3.4	-4.0	-3.6	-3.2	-7.4	20	97	61	59	3.8	0.2	1.8	1.9	6	10△ =	1	NNE 8	N 7	NE 8
6	103.7	104.4	104.8	104.3	-3.4	-0.9	-3.0	-2.6	0.2	-5.1	47	34	42	41	2.5	3.8	2.8	3.0	1	9⊙	0	NE 2	NE 3	NE 4
7	104.1	104.3	104.4	104.3	-2.2	-0.9	-1.5	-1.5	0.3	-3.4	57	51	17	42	2.2	2.8	4.5	3.2	1	1⊙	0	NE 4	NE 2	NE 1
8	104.6	106.0	106.1	105.6	-5.0	-2.2	-1.7	-2.2	-1.3	-4.9	29	32	29	30	3.4	3.5	3.8	3.6	1	0⊙	1	NE 4	NNE 3	NE 3
9	99.6	95.1	89.3	94.7	-3.4	-3.7	-6.7	-5.1	-1.4	-7.1	30	39	69	46	3.3	2.8	1.1	2.4	9	9⊙	9	S 16	S 18	SW 13
10	85.1	84.2	84.3	84.5	-8.2	-0.4	-10.2	-9.2	-4.4	-10.8	95	75	94	88	0.2	0.8	0.2	0.4	10	9	10✳ =	SSW10	SW 6	W 6
11	86.1	86.8	84.6	85.8	-9.6	-8.9	-10.1	-9.7	-7.8	-10.4	94	95	94	94	0.2	0.2	0.2	0.2	10△ =	10✳	8	NNW 7	NW 6	SSW 8
12	82.2	79.9	78.0	80.0	-8.6	-10.0	-7.8	-8.6	-7.4	-10.4	95	87	96	93	0.2	0.4	0.1	0.2	9	9	10 =	S 14	S 21	S 18
13	78.7	78.1	79.9	78.9	-6.0	-6.3	-5.7	-4.9	-5.6	-9.1	97	94	97	96	0.1	0.2	0.2	0.2	10△ =	9	10△=	S 15	S 23	S 20
14	81.1	81.9	82.6	81.9	-4.2	-6.7	-10.7	-8.1	-2.6	-10.7	98	99	97	98	0.1	0.0	0.1	0.1	10✳△ =	10✳ =	10△=	SSW10	NNE 2	N 5
15	79.0	70.3	70.2	73.2	-13.7	-11.2	-10.3	-11.4	-9.6	-14.3	96	93	94	94	0.1	0.2	0.2	0.2	7	10✳ =	10 =	SW 5	SSE23	NW 11
16	60.6	62.2	63.6	62.1	-6.6	-6.3	-7.3	-6.9	-4.0	-11.8	97	97	96	97	0.1	0.1	0.1	0.1	10✳ =	10△	10△	SW 13	WNW 9	W 7
17	68.1	71.9	76.4	72.1	-11.0	-11.4	-11.3	-11.2	-7.2	-11.7	93	93	93	93	0.2	0.2	0.2	0.2	10✳ =	10✳ =	10✳=	NW 7	N 7	NW 3
18	76.6	76.0	76.1	76.2	-11.4	-11.1	-12.4	-11.8	-10.8	-12.5	93	97	96	95	0.2	0.1	0.1	0.1	10✳	7	9	SW 7	SW 5	SSW 4
19	76.8	77.8	81.0	78.5	-13.6	-10.0	-14.3	-13.0	-9.9	-14.4	96	94	100	97	0.1	0.2	0.0	0.1	6✳	10✳=	10	C 0	C 0	C 0
20	84.3	86.2	89.0	86.5	-16.9	-18.6	-18.3	-18.0	-14.3	-19.0	100	95	95	97	0.0	0.1	0.1	0.1	10✳ =	10✳=	10✳=	NNE 4	NNE 6	NNE 5
21	87.6	86.1	86.7	86.8	-14.8	-12.1	-13.4	-13.4	-11.7	-18.6	61	60	50	57	0.8	1.0	1.1	1.0	1	7⊙	0	C 0	S 2	C 0
22	87.9	89.6	91.9	89.8	-16.8	-19.5	-22.8	-20.5	-13.2	-24.1	56	71	96	74	0.7	0.4	0.0	0.4	1	4⊙	10△=	NE 8	NNE11	NE 12
23	94.4	97.8	99.0	97.1	-20.4	-16.6	-16.8	-17.6	-15.4	-24.0	96	85	75	85	0.1	0.2	0.4	0.2	10△	8	0	ENE 5	NE 11	E 16
24	98.1	98.9	100.7	99.2	-17.2	-11.7	-7.9	-11.2	-7.0	-19.0	95	93	87	92	0.1	0.2	0.4	0.2	10✳ =	7✳	7✳	NE 6	E 4	SE 8
25	99.1	96.7	92.9	96.2	-9.4	-13.1	-12.4	-11.8	-7.7	-14.0	91	92	93	92	0.3	0.2	0.2	0.2	9✳	10△	7✳	SSE 1	S 4	C 0
26	88.1	86.3	84.7	86.4	-11.4	-9.3	-10.4	-10.4	-8.0	-13.0	93	63	55	70	0.2	1.1	1.3	0.9	2	1⊙	1	SW 4	C 0	SW 4
27	82.0	81.5	82.4	82.0	-9.4	-9.5	-10.1	-9.7	-8.4	-10.9	39	46	40	42	1.8	1.6	1.7	1.7	9	5⊙	10	NE 2	NE 2	E 2
28	83.8	85.6	87.1	85.5	-11.3	-10.8	-13.3	-12.2	-10.0	-13.8	70	74	64	69	0.8	0.7	0.8	0.8	6	7⊙	0	C 0	SSW 3	SSW11
29	86.0	83.1	84.8	84.6	-11.5	-11.0	-7.4	-9.3	-7.2	-15.2	93	93	96	94	0.2	0.2	0.1	0.2	10 =	10✳ =	10✳=	S 17	S 25	SSW13
30	85.8	85.7	85.2	85.6	-4.7	-2.3	-2.0	-2.8	-1.5	-7.9	98	98	98	98	0.1	0.1	0.1	0.1	10 =	10△ =	10✳△=	SSW10	SW 5	SSW 5
31	84.7	84.6	87.3	85.6	-5.2	-11.3	-7.3	-7.9	-1.6	-13.0	98	93	93	95	0.1	0.2	0.2	0.2	10✳△	10✳△ =	1	C 0	ENE 6	ENE 3
M	89.2	89.1	89.6	89.3	-9.5	-9.1	-9.3	-9.3	-6.4	-12.3	77	78	75	77	0.9	0.9	1.0	0.9	7.1	7.5	6.0	6.5	7.5	6.8

Kasprowy Wierch H_s=1991m H_b=1988,8m h_w=15,4m Listopad - Novembre 1962

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	7	20.5	.	●°4^50-6^00 7^50-55 8^35 10^40 △° 11^05 ●°-21^40 23^40-24, ⩧ 8^42-9^30 ≡²-10^10 ⩧ -22^30 ≡²-24; ⋙ 0^00-6^35 (por. 26), 8^29-9^15 (por 24), 20^20-21^30 (por 20)
2	9	.	.	●°0^00-30, ≡²0^00-1^20 ⩧ -1^40 (ꝏ) 5^45-24, ⋙ 1^02-40 (por 21), 2^40-4^30 (por 20), 10^15 12^05 (por 16), () 5^45-18^50
3	9	.	.	⌂' 20^00-24, (ꝏ) 0^00-12^00 ⩧ 4^05-10^30, () 14^20-17^00
4	9	.	.	⌂^2-1 0^00-6^00 (ꝏ) 3^00-11^30 ⩧ 9^00-11^30, ⋙ 0^00-15^40 (por 19), 17^40-18^30 (por 19), 21^35-24 (por 20), () 7^00-24
5	9	.	.	(ꝏ) na ⩧ 6^20 7^20, ⋙ 0^00-6^25 (por 26), 9^00-21^40 (por 30) ⋙-24 (por 32), () 0^00-24
6	0	5.0	.	●°8^50 17^20 ● △° 18^40-20^45 ●°-24; ⩧ 8^30-55 ≡²-15^20 ⩧ -17^10 ≡²-24, ⋙ 0^00-40 (por 26) ⋙ -5^45 (por 30) ⋙ -8^20 (por 34) ⋙ -15^30 ⋙ -16^45 (por 35) ⋙ -17^30 (por 24), 19^40-24 (por 21)
7	8	.	.	●°0^00-1^30, ≡²0^00-4^10 ⩧ -7^45 ≡²-10^40 ⩧ -18^20 ≡²-22^40 ⩧ -24, ⋙ 0^00-5^40 7^30-11^15 (por 16), 12^15-16^25 (por 16), 21^40-24 (por 16); () 6^15-7^45
8	9	.	.	⩧ 0^00-30 1^40-5^30 6^30-11^30 22^30-23^40, ⋙ 0^00 24 (por 17), ⌓° 18^20-20^10 ⌣' 20^20 24; () 8^25-22^30
9	9	3.1	.	●° 18^40-24; ⩧ 1^30-2^20 ꝏ -7^40 ⩧ 6^10-11^40, 13^05-14^30 ꝏ -15^10 ⩧ -16^40, 18^30-23^30, ⋙ 0^00-3^15, 7^50-10^30, ⌣^1-0 0^00 3^30, () 5^40-7^40, 9^30-16^30
10	0	2.3	.	●°0^00-5^30, 6^35-8^40 ●' 10^20-11^30 ● ∗° 14^05 ∗°-21^15, V° 14^15-20^40, ꝏ 4^00-6^50 ⩧ -8^30 ≡²-20^40 ⩧ -21^15 ꝏ -24
11	0	4.4	2	∗°0^15 4^50 6^20-7^05 △° 13^50-15^10 ∗° 22^55-24, V° 3^30 15^20 16^30 18^30 21^10 24, ꝏ 0^00-3^30 ≡²-5^10 ꝏ -6^20 ≡²-7^05 ꝏ -7^45 ≡²-9^30 ⩧ ꝏ -10^15 ≡²-15^10 ⩧ -15^20 ꝏ -17^20 ⩧ 16^30-17^20 ≡²-18^15 ⩧ -18^30 ꝏ 18^15-
12	0	4.7	4	∗^0-1 0^00-6^20 △°-7^30 ∗^0-1-9^30 △°-10^40, 11^45 14^40, 16^25-18^45, V° 0^00-21^30 V' 23^30-24; ⩧ (ꝏ) 0^00-1^40 ≡²-2^30 ⩧ -3^10 ≡²-21^30 ⩧ -23^30 ≡²-24, ✢° 5^00-9^00
13	0	9.1	6	△° 7^05-35 ∗° 8^05-20 ∗'-9^50 △° 11^10-45 △°-12^10 ∗^0-1-15^50 ∗△° 20^15-22^15 ∗'-23^20, V' 0^00 24, ≡²0^00-30 ⩧ -3^40 ≡²-21^20, 22^20-24 [11.XI: 24 ⩧ 21^10 24
14	0	7.4	12	∗° 5^15-8^10 △° 10^50-11^10 ∗△°-12^20 △°-14^45 ∗^0-1-15^30 △^0-1-17^30 ∗△^0-1-19^55, V^1-0 0^00 12^30 13^40-24, ≡²0^00-5^20 (ꝏ)-6^30 ≡²-8^25 ⩧ -8^50 ≡²-9^05 ⩧ -10^30 ≡²-19^50 ⩧ -22^15 ≡²-24, ✢° 18^50 19^55
15	0	20.6	16	△° 9^40-22^30 ∗°-24, V° 0^00-45 8^45-11^00 V' 24, ≡²0^00-30 ⩧ -0^45 ꝏ -3^40 (ꝏ) 5^40-7^05 ⩧ -8^30 ≡²-24, ⋙ 2^45-10^30 (por 21) ⋙ -12^15 (por 23) ⋙ -16^30 (por 22), 17^30-19^10 (por 16), ✢° 4^10 22^30, ⌓' 3^30-5^40 ⌣'
16	0	17.7	30	∗°0^00-1^30 ∗²-5^40 ∗'-7^00 ∗ ⁂'-7^25 ∗'-16^30 ∗°-24, V' 0^00 - a V²-24, ≡²0^00-24 . [15.XI 4^40-6^00
17	8	2.2	45	∗°0^00-2^35 ∗ ⁂°-3^20 ∗°-7^05 △° 18^55-19^20, V² 0^00-7^00 V° 11^40 19^30, 20^10 24, ≡²0^00-7^00 ⩧ -7^05, 11^40-24, ⋙ 9^25-24 (por 19), ✢° 8^20-10^10 ✢' 24
18	8	4.6	35	△° 5^50-10^45, 14^40-19^30 △^1-0 24, V° 0^00 1^30 5^40 24, ⩧ 0^00-1^30 5^40-6^45 ≡²-7^30 ⩧ -16^30 ≡²-24, ⋙ 0^00-24, 4^30-6^15 (por 17) ⋙ -19^20 (por 23) ⋙ -24 (por 28), ✢^0-1 0^00-5^30 ✢' -16^00 ✢² -24
19	9	20.8	40	△^0-1 0^00-5^40 ∗° 13^40-22^10 ∗'-24; V^0-1 0^00 8^00, 13^45-24, ≡²0^00-4^10 ⩧ -8^30 ≡² 13^45-24, ⋙ 0^00-11^45 (por 20) ⋙ -12^25 (por 25) ⋙ -14^00, 17^05-30 (por 18) ⋙ -18^35 (por 30) ⋙ -19^10 (por 28) ⋙ -21^00
20	0	18.6	35	∗' 0^00-1^15 ∗°-4^50 7^50-10^30 ⁂°-12^45 ∗°-13^50 ⁂°-14^15 ⁂'-15^50 △°-16^30 ∗△^1-0-17^15 △^0-1-19^20 △°-20^25 ∗'-21^10 ∗°-22^30, 23^50-24, V^1-0 0^00-6^40, 16^10-20^05 V°-22^30, ≡²0^00-7^15 ⩧ -10^30 ≡²-22^30 ⩧ -24, ⋙ 4^20-6^20 (por 20)
21	8	.	43	∗°0^00-30 2^50-3^30 V° 1^20-3^40 5^15-35 9^04-30 18^35-19^30, 23^40-24, ⩧ 0^00-1^20 ≡²-3^40 ⩧ -5^15 ≡²-5^35 ꝏ -24 ⩧ 9^04-30, 18^35-19^30, 23^40-24, ⊛^1-2 p , () 16^30-18^35
22	9	7.9	41	△° 8^40-10^05 ∗° 17^50-24, V° 0^00-1^20 5^50-8^30 V' -10^08 V° 14^30-24, ⩧ 0^00-1^20 ꝏ 0^00-6^10 ⩧ 5^50-6^50 ≡²-10^08 ⩧ -16^16, 12^10-14^30 ≡²-24, ⋙ 0^05-5^15 (por 21) ⋙ -6^45 (por 25) ⋙ -11^00 (por 21), 18^40-
23	1	23.0	59	∗°0^00-5^00 ∗'-6^20 ∗°-7^15 ∗'-8^50 ∗^0-1-15^40 ∗△°-17^35 ∗°-24, V° 0^00- na V' -8^45 V°-24, ≡²0^00-8^45 ⩧ -11^30 ≡²-12^45 ⩧ -18^25 ≡²-22^40 ⩧ -24, ⋙ 0^00-3^00 (por 20), ✢° 0^00-5^00
24	5	5.4	90	∗^0-1 0^00-19^30 △°-21^53, V° 0^00 7^30, ⩧ 0^00-2^50 ≡²-4^30 ⩧ -6^20 ≡²-7^30 ⩧ -8^30 (ꝏ) 16^30-24, ✢° 17^30-18^30
25	0	9.2	91	∗° 10^50-14^10 △° 14^50 ∗°-17^50 ∗^1-0-19^30 ∗△°-22^25, V° 10^45-16^30 V'-20^10 V°-21^20, (ꝏ) 0^00-3^40 ꝏ -10^45 ⩧ 9^20-10^45 ≡²-21^20 ⩧ -24, ✢° 13^40-20^10
26	0	13.9	98	△° 4^50-7^30 ∗° 9^50 13^40-24, V^0-1 2^15-24 ∼° 3^50-4^50, ⩧ 0^00-2^15 ≡²-24, ✢° 11^45-21^30 [20.XI: ⋙ -9^15 (por 35) ⋙ 14^15 (por 27); ✢° 0^00-6^20 ✢^1-0-9^15
27	9	.	105	∗°0^00-50, V' 0^00 5^20 ≡²0^00-3^00 ⩧ -4^30 ≡²-5^20 ⩧ -5^30, 6^30-7^30 ꝏ 5^20-24, ✢° 21^30-24, () 7^30-24 [22.XI: 24 (por 22) ✢° 3^30-8^40 ✢' -10^00 ✢° -12^00, 18^40-24
28	9	.	100	ꝏ 0^00-24, ⋙ 2^30-9^00, ✢° 0^00-30, 1^40-10^45, () 0^00-24
29	9	.	98	ꝏ 0^00-24 ⩧ 11^30-12^50 ⊕° 9^30-10^20, ⊛ 14^40-15^15, () 0^00-24
30	0	11.8	96	△° 10^50-11^15, 13^45-14^30, 15^45-19^30 ∗△° 20^35-22^30 ∗ ⁂^0-1-24, V^0-1 9^07-24, ꝏ 0^00-5^40 (ꝏ)-9^07 ≡²-24; ✢° 20^50 22^30, () 0^00-7^30
31				[19.XI: (por 35) ⋙ -23^25 (por 25), ✢² 0^00-7^30 ✢° -11^45 ✢' -12^40 ✢° -14^15, 17^00-30 ✢² -18^35 ✢' -23^25 ✢° -24; () 8^15-12^00
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Grudzień - Décembre

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	0	21.4	110	∗ △^0-1 0^00-3^30 ∗°-6^30 △°-9^15 ∗^0-1-24, V^0-1 0^00-24, ≡²0^00-24, ⋙ 6^20-7^00, ✢^0-1 4^30-24
2	9	0.8	130	∗°0^00-7^15, V' 0^00- na V²-7^15, ≡²0^00-7^15 ⩧ -9^20 (ꝏ) 15^00-18^00, ✢° 0^00-10^30, () 10^30-15^00
3	9	.	126	(ꝏ) 3^00-8^30, () 6^15-24
4	9	.	122	() 0^00-24
5	0	0.0	118	△° 12^30-13^30, V° 11^30-14^30, ⩧ 10^45-11^30 ≡²-14^30 ꝏ -24, ✢° 16^20-23^20, () 0^00-1^30, 6^00-10^30, 14^30-24
6	9	.	114	ꝏ 0^00-19^30 (ꝏ)-24, ⊛ 7^50-8^40, 15^03-15, () 0^00-24
7	9	.	110	(ꝏ) 0^00-8^30, 21^30-24, () 0^00-24
8	9	.	107	(ꝏ) 0^00-24, () 0^00-24
9	9	1.8	104	△° 23^50-24, (ꝏ) 0^00-9^30 ⩧ 22^30-23^20, ⋙ 4^30-6^30 (por 19) ⋙ -19^40 (por 31) ⋙ -21^15 (por 21), 22^25 24 (por 21), ✢^0-1 6^00-10^30 ✢^1-2-20^50 ✢^1-0-21^15, ⌓' 20^50-21^30, () 0^00-22^30
10	9	3.1	90	△° 0^00-6^15 ∗° 14^40-15^30, 19^50-21^00, V° 0^30-3^30 V' 4^20-6^15 V° 13^15 24, ≡²0^30-3^30 4^20-6^15 ⩧ 7^35-9^15, 13^00-15 ≡²-14^40 ⩧ -14^50, 15^20-30 ≡²-16^30 ⩧ -18^15 ≡² 19^45-21^00 ⩧ -21^15 ≡² 23^15-24.
11	6	1.8	95	∗° 1^50-3^40 ⁂° ∗ ⁂°-4^30 ∗°-6^15 ⁂°-7^35 ∗^0-2 8^15-10^30 ∗^0-1-17^15, V° 0^00 24, ≡²0^00-40 ⩧ -1^40 ≡²-8^10 ⩧ -8^30 ≡²-11^45 ⩧ -15^50 ≡² 20^30 ⩧ -21^20 ≡²-24, ⋙ 22^15-24, ✢° 2^40-3^30 ✢' 17^30-24
12	9	2.0	96	V^1-2 0^00-3^20, 19^30-24, ≡²0^00-2^30 ⩧ -3^20 7^45-12^50 ≡² 19^30-24, ⋙ 0^00-6^10 ⋙ -6^30 ⋙ -8^30 (por 23) ⋙ -23^05 (por 35) ⋙ -24, ✢' 0^00-8^30 ✢² -24; () 10^30-19^15
13	9	10.8	92	△° 2^50-6^50 20^25-23^30 ∗△°-24, V² 0^00-7^10 15^20-17^30 19^30-24, ≡²0^00-8^10 15^20-17^30 ⩧ 18^45-19^30 ≡² 24, ⋙ 0^00 7^10 (por 26) ⋙ -21^45 (por 34) ⋙ -24 (por 20), ✢' 0^00 5^10 ✢^1-2-24, () 7^30-14^50
14	0	23.8	101	∗△^0-1 0^00-8^30 △°-11^30 △'-12^10 ∗^1-2-14^10 ∗△^0-1-15^30 △^0-1-24, V' 0^00-9^10 V°-24, ≡²0^00-10^40 ⩧ -11^15 ≡²-24, ⋙ 0^00-7^30 (por 19), ✢' 0^00-6^10 ✢° -8^15, ⚡' 12^10-14^10
15	1	0.8	110	△^0-1 0^00-4^00 ∗° 12^30-18^35, V° 0^00 24, ≡²0^00-5^30 ⩧ -6^40 9^40-11^15 ≡²-18^15 ⩧ -19^30 ≡²-21^15 ⩧ 24, ⋙ 4^10-5^40 7^20-10^35 (por 20) ⋙ 10^35-18^00 (por 32) ⋙ -21^45 (por 18), ✢° 3^45-4^10 ✢' -5^40 ✢° -7^30 ✢' -11^00 ✢² -18^00
16	5	6.4	110	∗° 5^00-10^30 △°-11^15 12^15-13^00 ∗° 16^53-18^50 △°-21^50 V° 0^00 18^30 20^30 23^30 24, ⩧ 0^00-3^30 ≡²-10^15 ⩧ -10^30 ≡² 11^15 ⩧ 20^45 ≡²-21^45 ⩧ -24, ⋙ 2^45-4^00 (por 16) ⋙ -5^35 (por 27) ⋙ -11^30 (por 20), 13^30-15^10 (por 20), ✢° 0^00-
17	0	9.9	112	∗^0-1 0^55-22^40 ∗° 23^30 24, V^0-1 0^00 22^30, ⩧ 0^00-1^30 ≡²-22^30, ✢° 0^00-19^30, 21^30-24
18	7	0.9	125	∗°0^00 3^30, 4^50 10^15, 13^25-40 ∗ 19^40-20^30 ∗° 21^30-24, V' 5^15-6^30, 18^30 23^30, ≡² 5^15-6^30 ≡ 8^45-16^30, 18^30-23^30, ✢° 0^00 8^30
19	0	2.7	125	∗°0^00-1^15, 5^50-9^10 ∗^0-1-18^10 ∗° 21^50-24, ≡² 12^30-13^45 ⩧ -16^40 ≡²-18^30 ⩧ -21^30 ≡²-24 ꝏ 18^30-21^30
20	0	3.1	132	∗°0^00 2^50, 6^30-21^40, V^0-1 3^45-21^45 ≡²0^00-21^45 ꝏ -24 [10.XII ⋙ 0^00-20 (por 19), 6^20 9^15 (por 20), ✢° 0^00 2^50 ✢^1-0 4^20-8^05 ✢^3-1-8^30 ✢° -11^10, () 8^15-13^00
21	9	.	135	ꝏ 0^00 - a; () 16^30-24
22	9	4.4	130	△° 17^50-24, V° 15^10 23^30, (ꝏ) na ꝏ 9^30-15^10 ⩧ -16^40 ≡²-22^40 ⩧ -23^30, ⋙ 10^40-24 (por 24), ✢° 6^00-24; () 0^00-15^10
23	9	6.0	128	△^0-1 0^00 8^30 ∗°-12^20, V° 1^40 12^45 (ꝏ) 1^10-3^30 ⩧ 1^40-6^50 ≡²-12^15 ⩧ -12^45 ⋙ 0^00-1^30 (por 17), 12^05-14^30 (por 30) ⋙ -22^15 (por 30) ⋙ -24 (por 24), ✢° 0^00-3^40, 4^35-6^45 ✢^0-1 9^00-24
24	7	1.8	125	∗° 4^20-12^10 22^20-24, V° 0^30 12^50, ≡²0^30-8^30 ⩧ -12^50, ⋙ 0^00-5^10 (por 26), ✢' 0^00-4^30 ✢° 4^50-6^30
25	7	0.8	124	∗°0^00-2^50 5^35-9^40 △° 10^15-12^35 ∗° 19^45-22^30 V° 7^20-50, 10^30-17^30, ⩧ 7^20-50, 10^30-17^30 (ꝏ) 23^30-24
26	9	.	125	(ꝏ) 0^00-8^40 ꝏ -14^00 (ꝏ)-24, () 17^30-24 [15.XII: ✢^1-0-24, ⌣' 2^30 5^50
27	9	.	125	(ꝏ) 0^00-3^30 ꝏ -5^00 (ꝏ)-18^30, () 0^00 24 [16.XII: 4^00 ✢^1-2-10^20 ✢^0-1-24
28	9	.	121	(ꝏ) 2^30-8^30, ⋙ 19^40-24, ✢^0-1 19^40-24, zielony promień 15^53, () 0^00-24
29	1	2.0	115	∗△° 10^50-12^30 ∗°-21^30, V° 5^30-22^00 V'-24, ≡² 5^30-24, ⋙ 0^00-4^20 ⋙ -18^30 (por 41) ⋙ -24 (por 22), ✢^0-3 0^00-24; () 0^00-4^30
30	0	16.5	114	∗° 9^10-40 △° 12^30-16^50 ∗ ⁂°-17^05 ∗△°-17^40 ∗△'-18^30 ∗^1-0-20^25 ∗△^0-1-23^05 △°-24; V' 0^00 24, ≡²0^00-5^30 ⩧ -6^15 ≡²-7^20 ⩧ -8^30 ≡²-22^50 ⩧ -23^50 ≡'-24, ⋙ 0^00 10^40, ✢' 0^00-10^40 ✢° -12^40
31	0	2.7	130	△° 0^00-30 ∗△^0-1-7^40 ∗△° 9^30-10^45 ∗△'-11^30 ∗△° 12^20-14^45, V' 0^00-4^30 V° 10^30-14^30, ≡' 0^00-1^50 ≡²-4^30, 10^30-14^30 ⩧ 15^35-16^20, ✢° 13^20-14^30, 15^15-30, () 16^30-24
Σ	—	125.5	—	UWAGI

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1962

TABLICA II

WYNIKI MIESIĘCZNE I ROCZNE SPOSTRZEŻEŃ METEOROLOGICZNYCH

RÉSULTATS MENSUELS ET ANNUELS
DES OBSERVATIONS MÉTÉOROLOGIQUES

Rozewie $\varphi = 54°50'$ $\lambda = 18°20'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																					
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.1	-0.4	8.2	22	-12.1	31	1.5	1.9	0.9	1.3	6.0	5.8	5.7	5.8	87	81	85	84	0.9	1.4	1.0	1.1	8.5	7.7	7.9	8.0
II	–	–	–	–	1.3	-2.6	4.8	12	-12.1	1	-1.2	-0.1	-0.4	-0.5	4.9	5.1	5.0	5.0	85	83	82	83	0.8	1.0	1.1	1.0	8.3	8.3	7.2	7.9
III	–	–	–	–	0.9	-4.2	7.0	31	-9.6	15	-2.8	0.1	-1.6	-1.5	4.1	4.8	4.4	4.4	81	76	80	79	0.9	1.5	1.1	1.2	6.4	6.5	5.5	6.1
IV	–	–	–	–	9.7	2.9	19.3	18	-0.1	2,30	5.2	7.1	5.3	5.7	7.7	8.2	7.6	7.8	86	81	85	84	1.3	2.1	1.6	1.7	5.7	6.7	5.9	6.1
V	–	–	–	–	11.3	5.0	18.9	23	-0.3	1	7.5	9.4	7.0	7.7	9.1	9.6	8.7	9.1	87	82	86	85	1.4	2.4	1.5	1.8	7.4	6.9	5.8	6.7
VI	–	–	–	–	15.8	8.8	24.0	15	3.4	1	12.5	14.1	11.5	12.4	11.6	12.2	11.4	11.7	79	75	83	79	3.2	4.3	2.5	3.3	4.7	4.4	4.9	4.7
VII	–	–	–	–	17.6	11.1	25.0	20	6.2	4	14.1	16.2	13.8	14.5	14.0	14.5	13.9	14.1	87	78	87	84	2.2	4.2	2.1	2.8	6.0	5.6	6.2	5.9
VIII	–	–	–	–	17.7	11.8	27.5	12	8.0	15	14.0	16.5	13.8	14.8	13.9	14.2	13.9	14.0	87	76	88	84	2.1	4.7	1.9	2.9	6.1	6.6	5.8	6.2
IX	–	–	–	–	15.4	9.1	26.5	4	6.0	25	11.3	14.4	11.4	12.1	12.0	12.5	11.6	12.0	89	77	86	84	1.5	4.1	1.9	2.5	6.3	5.9	5.3	5.8
X	–	–	–	–	12.7	6.5	20.6	4	0.5	28	7.9	11.6	8.8	9.3	9.6	10.7	10.0	10.1	88	76	85	83	1.2	3.2	1.6	2.0	6.2	5.8	5.3	5.8
XI	–	–	–	–	5.4	2.0	10.7	2	-3.9	24	3.4	4.6	3.7	3.8	7.1	7.3	7.1	7.2	8.9	8.5	8.7	8.7	0.9	1.3	1.1	1.1	7.8	7.7	7.5	7.7
XII	–	–	–	–	0.5	-3.9	6.1	5	-16.1	21	-2.2	-4.0	-1.5	-1.6	4.7	5.0	4.7	4.8	8.3	8.2	8.2	8.2	0.8	1.0	1.0	0.9	8.1	8.3	7.5	8.0
Rok	–	–	–	–	9.3	3.8	27.5	12.VIII	-16.1	21.XII	5.9	7.9	6.1	6.5	8.7	9.2	8.7	8.9	8.6	7.9	8.5	8.3	1.4	2.6	1.5	1.8	6.8	6.7	6.2	6.6

Łeba $\varphi = 54°46'$ $\lambda = 17°34'$

I	–	–	–	–	3.5	-0.3	8.4	22	-11.4	31	1.7	2.3	1.3	1.6	6.4	6.2	5.9	6.2	91	84	86	87	0.6	1.2	1.0	0.9	9.1	8.7	8.2	8.7
II	–	–	–	–	1.8	-2.8	5.9	12	-12.0	1	-1.0	0.3	-0.1	-0.2	4.9	5.2	5.1	5.1	84	81	83	83	0.9	1.1	1.0	1.0	9.3	8.3	7.7	8.4
III	–	–	–	–	2.2	-4.7	7.5	31	-10.8	2,15	-2.9	1.3	-1.5	-1.2	4.3	4.8	4.6	4.6	86	72	82	80	0.7	1.9	1.0	1.2	7.5	7.3	5.5	6.8
IV	–	–	–	–	10.1	3.1	21.0	18	-0.1	30	5.5	8.1	5.6	6.2	8.0	8.2	8.0	8.1	87	76	87	83	1.3	3.0	1.4	1.9	6.3	7.3	6.5	6.7
V	–	–	–	–	11.9	5.5	19.9	19	-0.2	3	8.3	10.2	7.5	8.4	9.7	9.8	9.3	9.6	88	79	89	85	1.4	2.9	1.3	1.9	7.7	8.3	6.6	7.5
VI	–	–	–	–	16.6	9.1	28.2	19	2.6	8	12.6	15.0	12.3	13.0	12.4	12.6	12.2	12.4	84	74	84	81	2.5	5.2	2.4	3.4	5.4	5.6	6.2	5.7
VII	–	–	–	–	18.2	10.6	27.5	21	6.2	4	13.9	16.9	13.8	14.6	14.4	14.9	14.5	14.6	90	73	92	87	1.7	4.8	1.5	2.7	6.1	6.2	6.3	6.2
VIII	–	–	–	–	18.5	11.9	27.2	12	7.0	15	14.1	17.3	14.4	15.0	14.5	14.9	14.8	14.7	90	76	90	85	1.7	5.1	1.7	2.8	7.5	7.3	6.3	7.0
IX	–	–	–	–	16.5	9.0	27.4	4	1.9	25	11.3	15.5	11.3	12.4	11.8	12.6	11.8	12.1	88	72	87	82	1.7	5.3	1.8	2.9	6.7	6.6	5.4	6.2
X	–	–	–	–	13.6	5.6	22.2	3	-1.6	28	7.7	12.4	8.5	9.3	9.6	10.9	10.2	10.2	90	74	89	84	1.1	4.0	1.3	2.1	6.1	6.4	5.5	6.0
XI	–	–	–	–	6.0	1.9	13.2	5	-4.6	22	3.3	5.0	3.8	4.0	7.2	7.5	7.4	7.4	92	85	90	89	0.7	1.5	0.8	1.0	8.2	8.4	8.3	8.3
XII	–	–	–	–	0.3	-4.9	6.8	5	-16.4	21	-2.5	-4.3	-2.4	-2.2	4.9	5.1	5.0	5.0	89	88	90	89	0.6	0.7	0.5	0.6	8.3	7.9	7.7	8.0
Rok	–	–	–	–	9.9	3.7	28.2	19.VI	-16.4	21.XII	6.0	8.6	6.2	6.8	9.0	9.4	9.1	9.2	88	78	87	84	1.2	3.1	1.3	1.9	7.4	7.4	6.7	7.2

Puck $\varphi = 54°43'$ $\lambda = 18°25'$

I	–	–	–	–	3.5	-0.1	8.4	22	-12.6	31	1.9	2.4	1.3	1.7	6.0	5.8	5.7	5.8	83	78	82	81	1.2	1.6	1.2	1.3	9.3	8.6	8.1	8.7
II	–	–	–	–	1.7	-2.4	5.6	20	-12.4	1	-1.0	0.2	-0.1	-0.2	4.9	5.2	5.1	5.1	84	81	82	82	0.9	1.2	1.1	1.1	9.2	8.8	7.7	8.6
III	–	–	–	–	1.3	-4.7	8.0	31	-13.1	15	-2.7	0.4	-1.3	-1.2	4.2	5.1	4.6	4.6	80	80	82	81	1.0	1.2	1.0	1.1	7.0	8.1	7.0	7.4
IV	–	–	–	–	10.7	3.5	19.5	17	-0.4	30	6.5	8.5	6.3	6.9	7.9	8.2	7.8	8.0	81	74	81	79	1.9	3.3	2.0	2.4	5.6	6.8	8.1	6.8
V	–	–	–	–	12.8	5.7	17.9	23	-0.4	1	8.6	10.9	8.4	9.1	9.3	9.5	9.0	9.3	83	74	80	79	2.0	3.8	2.3	2.7	7.5	8.2	8.5	8.1
VI	–	–	–	–	17.4	9.3	26.7	15	2.8	3	13.5	15.6	12.8	13.7	11.6	11.6	11.5	11.6	74	65	77	72	4.4	6.7	3.6	4.9	5.7	5.8	6.5	6.0
VII	–	–	–	–	18.4	10.6	25.9	20	7.7	4	15.0	17.0	14.6	15.3	13.8	13.8	14.0	13.9	81	72	84	79	3.3	5.8	2.7	3.9	6.2	6.7	7.7	6.9
VIII	–	–	–	–	19.1	12.2	27.9	12	8.8	10	14.8	17.4	15.0	15.6	14.1	14.0	13.9	14.0	83	71	81	78	2.9	6.1	3.3	4.1	7.1	7.7	7.5	7.4
IX	–	–	–	–	16.2	9.1	27.7	4	4.3	25	11.0	15.1	12.2	12.6	11.6	12.9	12.2	12.2	88	79	85	84	1.6	4.6	2.2	2.8	6.6	6.9	7.6	7.0
X	–	–	–	–	12.8	6.4	20.2	4	-1.0	28	8.2	11.8	9.8	9.9	9.6	10.7	10.3	10.2	86	76	83	82	1.5	3.4	2.1	2.3	7.4	7.3	7.6	7.4
XI	–	–	–	–	5.8	2.6	11.7	5	-2.9	24	3.8	5.0	4.4	4.4	7.1	7.3	7.0	7.1	86	82	82	83	1.2	1.6	1.6	1.5	8.1	7.8	8.1	8.0
XII	–	–	–	–	0.4	-4.7	6.7	5	-15.4	21	-2.1	-0.6	-1.4	-1.4	4.6	4.9	4.6	4.7	81	80	77	79	0.9	1.2	1.1	1.1	9.1	8.5	7.8	8.5
Rok	–	–	–	–	10.0	4.0	27.9	12.VIII	-15.4	21.XII	6.5	8.6	6.8	7.2	8.7	9.1	8.8	8.9	82	76	81	80	1.9	3.4	2.0	2.4	7.4	7.6	7.7	7.6

Hel $\varphi = 54°36'$ $\lambda = 18°49'$

I	1011.3	1042.3	982.5	1011.6	2.8	-0.1	6.4	22	-10.2	31	1.5	2.0	1.1	1.4	6.1	6.0	5.9	6.0	89	83	87	86	0.8	1.2	0.9	1.0	9.6	8.7	8.3	8.9
II	1013.1	1039.1	968.9	1013.4	1.4	-2.3	5.1	20	-10.6	1	-1.0	0.2	-0.3	-0.4	5.0	5.1	5.0	5.0	86	81	83	83	0.8	1.2	1.0	1.0	9.2	8.4	7.9	8.5
III	1011.6	1028.1	982.7	1011.9	1.7	-4.2	6.1	26	-11.8	16	-2.6	1.0	-1.4	-1.1	4.5	4.6	4.6	4.6	87	70	82	80	0.7	2.0	1.0	1.2	6.6	6.3	5.7	6.2
IV	1013.4	1030.1	987.5	1013.7	10.9	2.8	20.2	21	-0.1	30	5.1	9.2	5.0	6.1	8.2	8.4	8.0	8.2	91	71	90	84	0.8	3.7	0.9	1.8	6.1	7.0	6.7	6.6
V	1011.8	1019.5	993.3	1012.1	12.5	4.9	17.5	30	-1.2	6	8.1	11.0	7.3	8.4	9.9	10.0	9.1	9.7	90	77	89	85	1.1	3.3	1.2	1.9	7.3	7.8	6.7	7.3
VI	1016.7	1032.3	1002.9	1017.0	17.8	8.9	25.4	19	0.2	3	12.8	16.4	11.7	13.2	12.0	12.5	11.6	12.0	80	66	83	76	3.0	6.7	2.5	4.1	5.6	5.7	5.6	5.6
VII	1013.1	1023.0	995.9	1013.4	19.3	10.9	25.4	20	5.5	18	14.5	18.0	13.6	14.9	14.5	14.8	14.0	14.4	87	72	89	83	2.1	6.2	1.7	3.3	6.0	6.5	6.6	6.4
VIII	1012.4	1022.3	999.4	1012.7	19.2	12.5	27.6	12	6.9	4	14.4	18.1	14.8	15.5	14.5	15.2	14.5	14.7	89	73	86	83	1.9	5.8	2.4	3.4	6.2	6.9	5.8	6.3
IX	1013.7	1031.4	990.4	1014.0	16.1	10.1	23.5	4	3.0	25	11.3	15.4	12.2	12.8	12.2	13.0	12.4	12.5	90	74	87	84	1.4	4.8	1.9	2.7	5.9	6.8	5.8	6.2
X	1020.7	1037.1	1004.3	1021.0	12.6	6.8	19.0	3	-1.6	28	8.7	12.1	9.2	9.8	10.3	11.1	10.4	10.6	90	77	87	85	1.2	3.2	1.4	1.9	7.1	6.7	6.2	6.7
XI	1017.3	1031.6	998.4	1017.6	6.1	3.1	11.3	5	-1.6	24	4.3	5.4	4.7	4.7	7.7	7.7	7.6	7.7	90	85	88	88	0.8	1.4	1.1	1.1	8.3	8.0	8.1	8.1
XII	1015.3	1050.9	972.5	1015.6	0.4	-3.1	7.2	5	-12.5	20	-1.2	-0.6	-1.2	-1.0	5.1	5.1	5.1	5.1	88	83	87	86	0.7	1.0	0.7	0.8	8.6	8.2	8.6	8.5
Rok	1014.2	1050.9	968.9	1014.5	10.1	4.2	27.6	12.VIII	-12.5	20.XII	6.3	9.0	6.4	7.0	9.2	9.5	9.0	9.2	88	76	86	83	1.3	3.4	1.4	2.0	7.2	7.2	6.8	7.1

Rozewie $H_s = 54\,m$ $h_w = 19\,m$ 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v > 15	◔	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	⩋
I	3.5	9.9	5.5	9.5	3.5	3.6	1.5	4.3	13.5	6.7	33.5	7.3	23.5	10.8	8.5	7.9	·	8.2	28	3.8	28	1	3	15	·	16	9	·	17	21	12	·	6	5	·
II	8.5	14.4	15	9.1	9	6.2	1	6.0	8.5	5.4	19	8.3	14.5	11.7	8.5	12.7	·	9.6	25	7.8	12	2	8	25	·	13	9	1	17	17	6	·	2	11	·
III	6.5	8.8	17	7.2	3.5	1.3	18	5.2	17	4.3	10.5	3.1	7.5	6.1	7	6.2	6	5.1	47	40.8	12	·	9	30	·	8	3	2	8	13	10	1	6	17	·
IV	8	4.6	11.5	5.9	6.5	4.2	10	3.4	7.5	4.2	19.5	4.3	13	5.0	10	4.6	4	4.4	24	9.0	5	·	·	2	·	2	·	2	9	14	5	·	8	1	·
V	6	5.2	11.5	2.6	6	1.8	8.5	3.9	3	3.3	14	3.0	16	4.6	15	4.2	13	3.2	62	14.1	14	·	·	2	·	3	1	·	10	18	13	1	13	·	2
VI	9	4.9	7	5.6	1.5	2.0	4.5	3.0	6.5	2.1	12.5	4.4	26	6.3	21	5.0	2	4.8	83	30.3	16	·	·	·	·	4	2	3	4	13	9	3	2	·	3
VII	14	1.6	3.5	1.7	2	3.5	2.5	2.8	8	2.2	16	4.2	15	4.8	21	4.4	11	3.1	43	14.0	27	·	·	·	·	·	·	1	7	15	10	1	2	·	2
VIII	2.5	2.6	2.5	2.6	·	·	11	2.0	5	3.7	26.5	5.3	29.5	5.9	16	6.2	·	5.0	66	9.2	7	·	·	·	1	4	1	1	7	19	13	·	·	·	4
IX	4	6.9	4.5	3.7	6.5	2.5	8	3.8	6	4.2	20	6.0	18	6.0	16	8.8	7	5.4	64	40.1	19	·	·	·	1	7	3	3	6	14	11	2	2	·	3
X	7	5.5	3	2.7	·	·	2	4.7	17	3.5	25.5	4.7	20	4.4	11.5	5.5	7	4.2	11	3.3	26	·	·	·	·	2	2	5	12	9	4	·	7	·	·
XI	2	2.5	10	6.8	6.5	10.1	19	8.1	10	2.6	29.5	3.2	8	6.9	1	6.0	4	5.3	56	16.7	1	·	·	7	·	7	2	3	18	13	11	1	7	2	·
XII	2.5	5.4	15	4.0	8	3.9	4.5	3.0	15	3.4	24	5.2	20	7.6	1	3.0	3	4.8	24	10.2	17	5	13	21	·	7	1	1	17	12	6	1	4	14	·
Rok	73.5	6.0	106	5.1	53	3.3	90.5	4.2	117	3.8	250.5	4.9	211	6.7	136.5	6.2	57	5.3	533	30.3	16.VI	8	33	102	2	73	33	22	132	178	110	10	59	50	14

Łeba $H_s = 2\,m$ $h_w = 21\,m$

I	5.5	5.4	1.5	8.0	2.5	4.0	3.5	2.4	17	4.1	39.5	4.7	17.5	5.5	6	4.9	·	4.8	50	5.2	19	1	3	14	·	7	·	·	23	22	16	·	2	6	·
II	9.5	7.8	5	8.2	13.5	4.7	1	1.5	14	3.7	19	4.9	13.5	6.7	8.5	7.1	·	5.7	44	12.9	12	2	8	23	·	10	·	1	19	19	8	1	·	15?	·
III	13.5	4.0	12	4.6	1.5	3.0	11	3.2	25	2.1	15	2.0	5	3.5	5	4.2	5	2.9	39	9.8	12	2	5	30	·	2	·	2	11	13	9	·	1	16?	·
IV	7.5	2.5	14.5	3.2	8.5	3.9	4	3.2	12.5	1.9	18.5	3.0	15.5	2.9	3	3.5	6	2.7	32	7.6	8	·	·	1	·	·	·	3	10	13	10	·	7	·	·
V	12	2.8	9	2.7	2	2.0	3	4.3	7	1.6	31.5	2.4	16	2.7	9.5	1.9	3	2.4	94	18.0	3	·	·	1	·	2	·	·	17	22	15	4	5	·	4
VI	12	4.3	8	4.1	·	·	0.5	5.0	8.5	2.8	23.5	4.0	26.5	4.2	7	2.9	4	3.7	54	8.9	27	·	·	·	2	4	·	2	5	11	9	·	·	·	2
VII	14.5	4.9	3	2.5	·	·	1.5	3.0	11.5	2.5	27.5	2.5	18.5	2.8	14.5	2.3	2	2.4	103	23.2	4	·	·	·	1	·	·	3	10	14	12	3	4	·	1
VIII	7	2.6	1	3.0	1.5	4.0	3	3.3	11	2.8	31	4.4	31	5.0	7.5	3.7	·	4.2	107	23.1	5	·	·	·	1	3	·	1	9	19	15	3	·	·	4
IX	5	2.7	1	2.0	4.5	2.0	9.5	1.6	7	2.2	25	4.3	17	4.5	15	4.0	6	3.3	58	9.2	23	·	·	·	1	6	·	2	11	12	11	·	1	·	3
X	7.5	2.7	1	1.0	·	·	1.5	2.7	24	2.9	24.5	2.3	14.5	3.4	10	4.2	10	2.6	21	9.7	4	·	·	3	·	·	·	5	11	8	4	·	4	·	1
XI	5.5	2.7	2	6.0	14	6.0	14.5	4.9	17	2.2	32.5	3.0	2.5	3.8	1	2.0	1	3.7	58	22.3	1	·	·	7	·	·	·	2	18	13	9	2	3	1	·
XII	4	3.2	8	3.1	7.5	2.3	9.5	2.0	18.5	2.7	32	4.4	9	4.3	2.5	3.2	2	3.3	41	8.9	17	9	14	23	·	1	·	1	20	18	10	·	3	15	·
Rok	103.5	3.6	66	4.0	55.5	2.7	62.5	3.1	173	2.6	319.5	3.5	186.5	4.1	89.5	3.7	39	3.5	701	23.2	4.VII	14	30	102	5	35	·	22	164	184	128	13	30	53?	15

Puck $H_s = 1\,m$ $h_w = 14\,m$

I	4	1.6	5	7.8	2	5.0	7	2.1	5	4.4	36	7.2	23	7.2	6	3.3	5	6.4	34	6.6	27	1	3	13	·	13	7	·	20	16	10	·	·	7	–
II	2	1.1	10	13.2	10	8.4	4	7.0	8	3.6	19	6.7	12	1.1	12	1.3	7	8.5	47	17.0	12	2	9	23	·	17	8	1	21	14	7	2	·	10	–
III	7	5.0	12	8.3	1	4.0	23	3.7	3	3.0	6	3.7	6	4.0	5	6.2	30	3.3	38	10.5	12	3	9	29	·	6	3	3	16	11	9	1	5	22	–
IV	9	6.0	14	4.4	4	1.5	6	2.3	2	2.5	20	2.4	8	3.8	9	3.6	18	2.8	28	11.2	5	·	·	2	·	2	·	1	12	10	7	1	5	·	–
V	3	1.3	20	3.4	10	1.8	10	3.4	·	·	10	3.4	17	3.0	9	4.2	14	3.0	53	21.5	14	·	·	1	·	5	·	·	16	12	8	2	7	·	–
VI	13	8.0	6	3.8	5	2.0	2	4.5	1	5.0	13	3.3	28	5.1	6	4.0	16	4.0	63	18.0	29	·	·	·	2	6	1	1	13	8	7	3	·	·	–
VII	4	2.5	11	2.5	3	2.0	4	3.8	·	·	18	2.6	20	3.0	15	3.3	18	2.3	59	15.3	13	·	·	·	1	2	·	3	15	10	9	3	·	·	–
VIII	4	3.5	1	3.0	5	1.6	3	2.7	5	5.8	24	4.7	30	5.2	5	3.8	16	3.8	82	14.6	7	·	·	·	1	7	2	3	16	16	12	2	·	·	–
IX	3	4.0	3	3.3	2	2.5	14	3.4	1	1.0	20	4.6	16	6.4	11	5.0	20	3.6	68	13.0	19	·	·	·	1	4	2	1	10	13	13	1	1	·	–
X	4	4.0	3	3.7	·	·	6	2.0	3	4.7	18	2.7	14	6.3	7	4.7	38	2.4	13	3.9	14	·	·	1	·	4	2	2	16	9	4	·	5	·	–
XI	2	4.0	5	7.8	5	1.5	25	7.7	1	2.0	12	2.4	5	5.2	1	5.0	34	4.2	60	15.5	1	·	·	6	·	10	4	3	20	12	10	1	3	1	–
XII	1	2.0	10	4.2	15	3.3	5	3.0	2	2.0	21	2.8	12	6.0	1	5.0	26	2.7	30	11.2	17	8	13	22	·	3	·	·	21	9	6	1	·	14	–
Rok.	56	3.6	100	5.4	62	2.8	109	3.8	31	2.8	217	3.9	191	4.7	87	4.1	242	3.9	575	21.5	14.V	14	34	97	5	79	29	18	196	140	102	17	26	54	–

Hel $H_s = 1\,m$ $H_b = 2{,}6\,m$ $h_w = 24\,m$

I	1	3.5	6.5	8.5	3	2.7	1	5.0	19.5	7.0	26	7.0	25.5	7.3	9.5	6.5	1	6.9	26	5.0	28	1	3	12	·	18	·	·	23	17	9	·	1	6	·
II	5	9.0	8	8.2	11.5	7.0	1.5	4.7	11.5	6.6	18	8.6	12.5	8.4	15	9.9	1	8.2	39	7.4	12	1	9	23	·	19	3	·	19	22	10	·	1	22	·
III	9.5	5.5	14	6.2	2.5	1.8	18	5.1	16	3.9	6	2.8	8	4.8	9	3.8	10	4.2	62	17.6	12	2	5	29	·	10	·	3	12	13	11	2	3	27	·
IV	15	5.1	9	4.6	6.5	4.2	10.5	3.0	11.5	3.9	13	4.3	4	2.9	15.5	4.1	5	3.9	20	8.7	5	·	·	1	·	3	·	3	13	11	6	·	5	1	1
V	14	3.6	10	3.3	9.5	2.9	5	3.3	9	3.0	14	3.4	10.5	3.0	13	4.6	8	3.2	83	20.0	14	·	·	4	·	3	·	·	13	23	14	2	6	·	2
VI	21	5.6	3.5	3.6	3	2.0	6	3.1	6.5	3.2	9.5	4.6	26	5.4	10.5	3.8	4	4.5	63	49.2	16	·	·	·	1	5	·	·	7	10	8	2	·	·	3
VII	18	2.5	6	2.5	4	3.1	3	3.8	11	4.7	5.5	4.8	16	4.3	18.5	4.3	11	3.3	53	7.9	7	·	·	·	1	3	·	4	11	14	12	·	1	·	3
VIII	3	2.3	2.5	2.0	8.5	2.4	2	4.0	9	3.4	19	6.7	34	5.9	12	3.7	3	4.8	133	73.2	7	·	·	·	1	10	·	4	8	19	14	3	·	·	2
IX	2.5	4.2	2.5	4.4	10.5	3.3	6.5	4.0	12	4.1	11.5	6.1	24	6.0	16.5	5.8	4	5.0	80	21.0	18	·	·	·	·	4	·	3	9	14	12	2	1	·	1
X	4.5	4.1	1	2.8	·	·	4.5	3.3	18.5	4.6	12	4.4	25.5	5.0	15	5.2	12	4.1	8	2.4	5	·	·	2	·	4	·	1	12	8	2	·	3	·	·
XI	2	1.5	4	5.0	10	8.8	18	7.2	15.5	4.7	21	3.9	10.5	5.5	3	2.8	6	5.1	59	21.7	1	·	·	4	·	11	·	2	23	12	11	1	1	·	·
XII	1.5	3.3	8	3.9	13.5	4.4	8	3.5	14	4.8	17.5	6.2	22	6.0	6.5	3.7	2	4.9	42	15.3	17	2	14	20	·	9	·	·	22	15	7	1	·	16	·
Rok	97	4.2	75	4.5	82.5	3.6	84	4.2	154	4.5	173	5.2	218.5	5.4	144	4.8	67	4.8	668	73.2	7.VIII	6	31	95	3	99	3	20	172	178	116	13	22	72	12

UWAGA. Kierunki i prędkości wiatru – wg anemometru.

Ustka $\varphi = 54°35'$ $\lambda = 16°52'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0,m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1010.6	1041.5	981.3	1011.7	3.4	0.1	8.2	22	-12.2	31	1.5	2.3	1.6	1.8	6.4	6.2	6.0	6.2	91	85	86	87	0.6	1.1	1.0	0.9	8.7	8.4	7.9	8.3
II	1013.0	1039.6	969.6	1014.1	1.7	-2.4	5.9	12	-12.4	1	-1.0	0.5	-0.1	-0.2	5.1	5.4	5.3	5.3	87	84	85	85	0.7	1.0	0.9	0.9	8.8	7.9	7.5	8.1
III	1010.7	1027.0	982.0	1011.8	2.2	-4.0	7.8	31	-9.9	20	-2.5	1.3	-1.0	-0.8	4.5	4.9	4.7	4.7	86	73	81	80	0.7	1.9	1.1	1.2	7.4	7.2	4.8	6.5
IV	1012.5	1029.9	987.4	1013.5	10.0	3.4	22.7	17	0.5	1,2	5.3	7.6	5.9	6.2	7.8	8.0	8.1	8.0	87	78	86	84	1.2	2.8	1.4	1.8	5.8	7.0	5.3	6.0
V	1011.1	1017.9	1001.9	1012.1	11.7	5.8	20.3	19	-0.1	3	8.2	9.9	8.4	8.7	9.5	9.6	9.2	9.4	87	79	83	83	1.5	3.0	2.0	2.2	7.2	8.1	6.8	7.4
VI	1016.6	1033.2	1002.3	1017.6	16.5	9.7	28.3	19	3.7	8	12.6	14.3	12.9	13.2	11.8	12.2	11.9	12.0	80	75	79	78	3.0	4.7	3.3	3.7	5.9	5.3	5.1	5.4
VII	1012.4	1022.7	993.4	1013.4	17.8	10.9	27.5	21	6.6	4	14.1	16.7	14.2	14.8	14.2	14.5	14.2	14.3	89	77	87	84	1.9	4.9	2.2	3.0	5.5	6.0	5.5	5.7
VIII	1011.8	1021.5	999.7	1012.8	17.8	12.2	28.2	12	8.0	15	14.1	17.0	14.6	15.1	14.3	14.6	14.8	14.6	88	75	89	84	1.9	5.0	1.9	2.9	6.9	7.5	5.5	6.6
IX	1013.2	1029.3	989.5	1014.2	16.0	9.2	27.0	4	4.5	18	11.0	15.3	11.8	12.5	11.7	12.4	11.8	12.0	89	71	85	82	1.6	5.3	2.1	3.0	6.3	6.6	4.2	5.7
X	1019.9	1036.2	1005.1	1020.9	13.3	5.8	22.1	3	-0.6	28	7.7	12.5	8.9	9.5	9.6	11.0	10.4	10.3	90	75	89	85	1.2	3.9	1.3	2.1	7.7	6.1	4.9	6.2
XI	1015.8	1031.1	997.3	1016.9	5.8	2.2	13.1	5	-2.6	18	3.3	5.1	3.8	4.0	7.3	7.5	7.3	7.4	92	85	89	89	0.7	1.6	0.9	1.1	7.8	8.1	7.9	7.9
XII	1014.7	1050.3	971.1	1015.8	0.0	-5.3	6.0	5	-16.8	24	-3.2	-1.4	-2.6	-2.4	4.6	5.1	4.8	4.8	88	87	88	88	0.6	0.6	0.6	0.6	7.3	8.4	7.0	7.6
Rok	1013.5	1050.3	969.6	1014.5	9.7	4.0	28.3	19 VI	-16.8	24 XII	5.9	8.4	6.5	6.8	8.9	9.3	9.0	9.1	88	79	86	84	1.3	3.0	1.6	2.0	7.1	7.2	6.0	6.8

Ustka-Wydma $\varphi = 54°35'$ $\lambda = 16°52'$

I	-	-	-	-	3.3	0.1	7.9	22	-12.0	31	1.6	2.3	1.6	1.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	1.7	-2.2	6.2	12	-12.1	1	-0.9	0.5	0.0	-0.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	2.0	-3.6	7.7	31	-9.9	20	-2.4	1.1	-0.9	-0.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	9.6	3.3	22.6	17	0.3	1	5.1	7.2	5.7	5.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	11.7	5.9	21.2	19	0.5	6	8.2	9.7	8.3	8.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	-	-	-	16.2	9.9	29.3	19	4.0	8	12.6	14.4	12.8	13.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	-	-	-	17.5	11.0	28.4	21	6.5	4	14.1	16.8	14.3	14.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	-	-	-	17.9	12.3	28.3	12	8.1	15	14.3	17.1	14.5	15.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	-	-	-	16.0	9.5	27.2	4	4.6	18,25	11.1	15.3	11.9	12.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	-	-	-	13.3	5.9	22.9	3	-0.6	28	7.8	12.4	8.8	9.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	5.8	2.2	13.1	5	-2.6	18	3.3	5.1	3.7	4.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-	-	-	-0.3	-5.2	5.7	5	-17.5	24	-3.1	-1.6	-2.7	-2.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Rok	-	-	-	-	9.6	4.1	29.3	19 VI	-17.5	24 XII	6.0	8.4	6.5	6.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Lębork $\varphi = 54°33'$ $\lambda = 17°45'$

I	1008.8	1039.6	980.0	1011.5	3.3	-0.6	8.6	22	-13.1	30	1.6	2.2	1.1	1.5	6.1	5.9	5.7	5.9	87	81	84	84	0.9	1.4	1.1	1.1	9.4	8.8	8.5	8.9
II	1010.9	1037.2	967.1	1013.6	1.5	-3.4	5.6	12	-11.9	1	-1.5	0.1	-0.6	-0.6	4.6	4.8	4.7	4.7	82	76	78	79	1.0	1.4	1.3	1.2	8.6	8.8	8.3	8.6
III	1008.8	1025.2	981.3	1011.5	2.2	-6.6	8.9	31	-13.6	2	-4.8	1.2	-2.3	-2.0	3.8	4.3	4.2	4.1	85	64	79	76	0.7	2.4	1.1	1.4	7.4	7.8	5.1	6.8
IV	1010.6	1027.5	985.2	1013.3	13.1	3.6	26.5	21	-1.2	14	5.9	11.2	7.2	7.9	8.0	8.3	8.4	8.2	84	64	82	77	1.6	6.1	2.3	3.3	7.1	7.4	6.1	6.9
V	1009.1	1016.2	998.2	1011.8	13.6	5.4	20.2	19	-1.4	1	8.5	12.1	8.3	9.3	9.6	9.4	9.3	9.4	85	67	84	79	1.7	5.1	1.9	2.9	7.7	8.8	6.8	7.8
VI	1014.4	1029.9	1000.6	1017.1	18.2	7.8	27.9	16	0.2	7	12.5	16.8	12.4	13.5	11.8	10.8	11.3	11.3	80	57	77	71	3.0	9.2	3.5	5.2	6.9	6.7	6.6	6.7
VII	1010.5	1020.7	992.4	1013.2	19.1	9.4	27.4	21	5.9	30	13.2	17.7	13.8	14.6	13.7	13.5	13.8	13.7	90	68	87	82	1.6	7.2	2.2	3.7	7.0	7.7	6.1	6.9
VIII	1010.0	1019.8	998.6	1012.7	19.1	11.1	28.3	12	5.0	14	13.5	17.6	13.8	14.7	14.2	14.0	14.3	14.2	91	70	90	84	1.5	6.4	1.6	3.2	8.0	8.2	6.8	7.7
IX	1011.3	1027.9	988.2	1014.0	16.4	7.7	27.4	4	-0.1	25	10.1	15.5	10.6	11.7	11.4	11.8	11.6	11.6	91	68	90	83	1.2	6.1	1.3	2.9	6.9	7.1	5.9	6.6
X	1018.1	1034.2	1002.9	1020.8	13.6	4.3	22.4	4	-3.1	15	6.5	12.6	8.2	8.9	9.1	10.5	9.9	9.8	92	71	88	84	0.9	4.5	1.5	2.3	7.7	6.4	5.9	6.7
XI	1014.2	1029.4	995.1	1016.9	5.6	1.9	13.2	5	-5.7	22	3.2	4.8	3.8	3.9	7.0	7.3	7.1	7.1	89	83	86	86	0.9	1.6	1.2	1.2	8.4	8.2	8.3	8.3
XII	1012.8	1048.6	969.6	1015.5	-1.1	-6.6	5.6	12	-20.1	24	-3.8	-1.9	-3.9	-3.4	4.4	4.9	4.5	4.6	90	88	90	89	0.6	0.7	0.5	0.6	7.9	8.1	7.7	7.9
Rok	1011.6	1048.6	967.1	1014.3	10.4	2.8	28.3	12 VIII	-20.1	24 XII	5.4	9.2	6.0	6.6	8.6	8.8	8.7	8.7	87	71	85	81	1.3	4.3	1.6	2.4	7.8	7.8	6.8	7.5

Gdynia $\varphi = 54°31'$ $\lambda = 18°34'$

I	1009.3	1039.6	980.7	1011.2	3.5	0.1	8.4	22	-11.4	31	1.9	2.3	1.5	1.8	6.0	5.8	5.7	5.8	85	79	83	82	1.1	1.6	1.2	1.3	9.0	8.5	8.2	8.6
II	1011.1	1037.3	968.6	1013.0	1.6	-2.4	5.8	20	-11.8	1	-1.0	0.1	0.0	-0.2	4.8	5.1	5.0	5.0	83	81	81	82	1.0	1.2	1.2	1.1	8.6	8.6	7.7	8.3
III	1009.5	1026.5	981.5	1011.4	1.2	-3.9	7.7	31	-8.8	15	-2.5	0.3	-1.1	-1.1	4.4	4.8	4.6	4.6	84	76	82	81	0.8	1.5	1.1	1.1	7.3	7.7	6.6	7.2
IV	1011.4	1028.2	986.0	1013.2	10.9	4.2	19.6	21	0.3	30	5.9	8.6	6.1	6.7	8.0	8.2	8.2	8.1	85	74	86	82	1.4	3.4	1.4	2.1	7.1	7.9	6.2	7.1
V	1009.8	1017.0	994.7	1011.6	11.9	6.4	17.2	23	0.2	1	8.4	10.2	8.2	8.8	9.3	9.5	9.2	9.3	84	77	84	82	1.8	3.2	1.8	2.3	7.7	8.6	6.7	7.7
VI	1014.8	1030.3	1001.4	1016.6	17.2	10.4	27.6	15	3.9	3	13.1	14.7	12.6	13.2	11.2	11.7	11.6	11.5	73	69	78	73	4.3	5.5	3.3	4.4	6.1	6.6	6.9	6.5
VII	1011.2	1021.0	994.0	1012.9	18.5	12.0	25.6	20	8.1	4	14.8	17.1	14.7	15.3	13.5	13.6	14.1	13.7	80	70	84	78	3.5	6.2	2.8	4.2	6.1	7.0	6.6	6.6
VIII	1010.5	1020.3	998.8	1012.2	18.9	12.8	26.6	12	9.4	31	14.6	17.6	15.3	15.7	13.6	14.0	13.9	13.8	82	70	80	77	3.1	6.4	3.5	4.3	6.4	7.9	6.1	6.8
IX	1011.9	1029.0	989.5	1013.7	16.1	10.0	24.7	4	5.6	25	11.5	15.1	12.5	12.9	11.8	11.9	12.3	12.0	86	70	84	80	1.9	5.5	2.3	3.2	6.2	7.3	6.2	6.6
X	1018.6	1034.7	1002.1	1020.4	12.6	7.0	17.8	3	-0.1	21	8.3	11.7	9.5	9.8	9.8	10.5	10.1	10.1	87	75	83	82	1.3	3.4	2.0	2.2	7.0	6.5	5.8	6.4
XI	1015.2	1029.3	996.5	1017.1	5.9	2.9	11.3	2	-2.9	24	4.0	4.9	4.5	4.5	7.4	7.3	7.4	7.4	88	83	86	86	1.0	1.5	1.2	1.2	8.2	8.2	8.2	8.2
XII	1013.2	1048.5	971.6	1015.1	0.7	-3.6	7.3	4	-14.3	21	-1.6	-0.7	-1.5	-1.3	4.8	4.8	4.7	4.8	84	78	82	81	0.9	1.4	1.0	1.1	9.0	8.2	7.5	8.2
Rok	1012.2	1048.5	968.6	1014.0	9.9	4.7	27.6	15 VI	-14.3	21 XII	6.4	8.5	6.9	7.2	8.7	8.9	8.9	8.8	83	75	83	80	1.2	3.4	1.9	2.4	7.4	7.8	6.9	7.4

UWAGA. W ciągu całego roku ciśnienie powietrza jest za niskie przeciętnie o około 0,5 mb.

Ustka $H_s = 6 m$ $H_b = 8,1 m$ h_w = 19,8 m anemometr / 18,0 m wiatromierz Wilda 1962

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	◉	●	Opad R ≥ 0,1	R ≥ 1,0	R ≥ 10,0	═	⊞	R
I	2	11.0	2	6.5	2	8.5	5.5	4.3	17	5.9	39	6.7	12.5	8.1	13	6.0	·	6.6	61	7.4	6	1	3	12	·	6	·	·	19	26	18	·	3	6	·
II	9.5	9.6	12.5	8.2	9.5	4.3	0.5	3.0	8.5	5.8	21	6.8	15.5	8.5	7	9.3	·	7.4	38	7.6	5	2	8	22	·	12	4	1	17	17	11	·	3	18	·
III	10.5	5.7	13	5.5	1	1.0	15	3.7	18.5	4.2	15	2.2	4.5	5.7	8.5	3.9	7	3.8	49	14.1	12	·	6	29	·	4	·	2	12	16	12	1	7	24	·
IV	4	5.1	23	4.6	3.5	3.9	4.5	3.8	5.5	5.0	21	4.8	19	4.1	8.5	5.3	1	4.5	22	6.2	8	·	·	·	·	1	·	3	8	13	7	·	8	·	·
V	8	4.5	14	2.8	1	3.0	2	3.0	6.5	4.9	23	3.1	20.5	5.0	18	3.7	·	3.8	51	9.2	26	·	·	1	2	·	·	·	16	20	14	·	9	·	1
VI	11.5	5.4	4.5	3.1	·	·	·	·	3.5	2.6	12.5	3.8	34	6.3	23	4.4	1	5.0	56	18.0	28	·	·	·	1	2	·	3	6	12	9	1	1	·	1
VII	12	2.0	11.5	2.8	1.5	2.3	1	2.0	5	3.0	21	3.6	22	4.7	17	3.8	2	3.5	104	24.2	4	·	·	·	1	1	·	4	9	15	12	4	4	·	1
VIII	5	2.2	2	1.0	1	2.0	2	5.5	4.5	3.1	32.5	4.5	27	6.1	18	5.5	1	4.8	122	28.3	7	·	·	·	1	3	·	2	8	25	20	4	3	·	1
IX	4	2.5	1	2.0	2	3.5	13	2.7	5.5	2.8	25.5	4.1	13	5.7	24	6.2	2	4.4	63	11.1	8	·	·	·	·	·	·	7	6	13	12	1	2	·	5
X	6	3.8	4	3.5	1	4.0	2	1.5	20	2.4	37	3.5	9	5.3	11	5.3	3	3.5	29	10.3	4	·	·	1	·	1	·	3	11	14	7	1	10	·	·
XI	2.5	2.8	5.5	5.3	7	6.5	24	3.8	12.5	3.5	30.5	3.2	4	8.2	4	7.0	·	4.2	62	10.7	29	·	·	8	·	1	·	3	22	17	12	1	9	9	·
XII	6	4.0	3	3.7	9	1.8	13	3.2	14	3.2	39	4.8	5	5.4	4	4.8	·	4.0	45	8.4	9	8	14	24	·	2	·	2	15	16	10	·	7	17	·
Rok	81	4.9	96	4.1	38.5	3.4	82.5	3.0	121	3.9	317	4.3	186	6.1	156	5.4	17	4.6	702	28.3	7.VIII	11	31	97	5	33	4	30	149	204	144	13	66	74	9

UWAGA. Kierunki i prędkości wiatru – wg anemometru.

Ustka-Wydma $H_s = 7 m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Lębork $H_s = 18 m$ $H_b = 21,8 m$ $h_w = 12 m$

I	1.5	5.7	5	2.3	4.5	1.3	6	1.6	11.5	3.2	28.5	3.8	28.5	3.7	7.5	3.1	·	3.3	54	9.7	28	2	3	13	·	2	·	·	26	22	14	·	·	6	
II	5.5	4.5	8	3.1	13.5	2.3	3.5	1.9	7	2.3	15	3.1	22	5.3	9.5	6.3	·	3.9	50	20.1	12	2	9	24	·	5	2	1	20	20	6	1	·	25	1
III	9	2.8	10.5	2.0	6	1.5	22	1.8	19	1.6	5.5	1.5	12	2.0	9	2.1	·	1.9	37	13.4	12	10	6	29	·	·	·	1	11	12	10	1	1	25	·
IV	7.5	2.5	11.5	2.1	10.5	2.0	8	1.6	10	2.2	11.5	3.1	18	2.0	11	2.4	2	2.2	26	5.7	5	·	·	3	2	·	·	2	13	12	8	·	1	·	·
V	4	1.3	9	1.4	13	2.0	7.5	2.0	3.5	2.4	25	1.9	20.5	1.7	10.5	2.5	·	1.8	100	17.8	14	·	·	3	·	·	·	·	15	24	17	2	·	·	4
VI	7.5	2.4	7.5	2.6	0.5	1.0	3	1.7	3	2.0	16.5	2.5	36	2.7	16	1.8	·	2.4	48	11.2	29	·	·	·	3	1	·	1	9	12	8	1	·	·	3
VII	3.5	1.4	14.5	1.3	5	1.3	6.5	1.6	6	1.7	18.5	2.3	20	1.9	18	1.7	1	1.7	78	17.6	27	·	·	·	2	·	·	·	15	16	11	1	1	·	3
VIII	2.5	1.2	1	1.0	1.5	1.3	6	2.2	7.5	2.1	19	3.1	42	2.9	13.5	1.7	·	2.6	89	11.5	18	·	·		1	·	·	·	14	21	17	2	1	·	5
IX	1	1.0	3.5	1.3	10.5	1.2	10	1.5	4	2.9	18.5	2.2	24.5	2.7	14	2.1	4	2.0	73	15.0	23	·	·	1	1	1	1	3	10	15	12	2	1	·	3
X	4.5	1.4	4	1.0	·	·	7.5	1.6	12	1.7	19	1.9	25	2.3	12	1.6	9	1.7	21	5.9	4	·	·	7	·	·	·	5	14	9	5	·	6	·	
XI	0.5	1.0	4.5	1.7	20	2.9	13	2.1	17.5	1.3	17.5	1.9	11	2.2	3	1.7	3	2.0	68	29.0	1	·	·	8	·	·	·	·	20	13	10	2	·	5	·
XII	3	1.0	3.5	1.1	14.5	1.2	6	1.5	6.5	2.9	25	2.3	17	2.6	5.5	1.5	12	1.7	22	4.9	11	11	15	25	·	·	·	1	19	17	8	·	4	20	
Rok	50	2.2	82.5	1.7	99.5	1.5	99	1.8	107.5	2.2	219.5	2.5	276.5	2.7	129.5	2.4	31	2.3	666	29.0	1.XI	25	33	113	9	9	3	14	186	193	126	12	15	81	19

Gdynia $H_s = 2 m$ $H_b = 14,5 m$ h_w = 25 m anemograf / 12,5 m wiatromierz Wilda

I	2.5	8.4	3.5	10.1	4	5.9	2	8.2	12.5	7.2	29.5	6.7	29	6.7	10	6.0	·	6.9	40	6.4	28	1	3	11	·	18	1	·	20	19	11			4	·
II	5	10.0	8.5	8.2	7.5	8.3	4.5	7.4	11.5	7.3	17.5	6.5	17	7.2	12.5	9.0	·	7.7	44	17.2	12	1	8	21	·	17	·	1	20	18	6	1	2	14	1
III	9.5	7.2	7	7.3	3.5	5.4	9	6.9	25	6.4	7.5	3.7	9.5	3.5	12	4.5	10	5.1	33	9.2	13	·	10	29	·	9	·	3	14	11	8	-	6	17	
IV	13.5	5.6	7	4.5	1.5	4.7	3.5	4.0	18.5	4.0	15.5	5.4	10.5	4.0	14	4.9	6	4.4	30	14.2	5	·	·	·	·	5	·	2	14	11	8	1	7	·	
V	9	5.0	4	4.6	4	4.1	3.5	5.0	15	4.9	18	2.9	16	4.0	18.5	4.2	5	3.9	108	31.5	14	·	·	·	·	3	·	·	16	18	15	4	8	·	
VI	12.5	7.7	3.5	5.0	2	3.0	3.5	4.1	8	3.8	10.5	3.9	24	4.4	18	4.3	8	4.3	66	19.2	16	·	·	·	1	4	·	1	6	12	11	2	·	·	3
VII	12.5	3.4	5	3.3	2.5	5.0	3	4.3	7	4.2	13.5	5.3	20	3.7	19.5	4.3	10	3.7	53	10.5	27	·	·	·	1	·	·	3	8	16	10	1	·	·	4
VIII	3	5.2	1	2.5	3	3.5	6	4.7	10	3.4	29	5.3	26	5.0	11	4.1	4	4.5	130	65.4	7	·	·	·	1	12	·	2	10	16	10	4	1	·	3
IX	3.5	5.3	·	·	3.5	4.0	10	5.8	11.5	4.8	16	5.0	34	4.4	9.5	5.0	2	4.7	53	13.0	18	·	·	·	·	10	·	2	12	15	10	1	2	·	1
X	3.5	5.9	1.5	3.0	·	·	4.5	3.9	18.5	5.9	15.5	3.8	30	3.5	13.5	3.4	6	3.9	12	5.7	5	·	·	1	·	2	·	2	10	9	3	·	8	·	·
XI	1	3.0			7.5	11.2	16	10.8	16	6.5	24.5	3.8	16	3.3	5	3.1	4	5.8	66	24.3	1	·	·	5	·	10	3	1	21	13	12	2	6	·	
XII	1.5	2.7	3.5	4.9	9.5	5.0	4	5.6	12.5	4.2	23.5	4.0	25	3.7	10.5	3.4	3	3.9	68	29.9	18	4	13	20	·	3	·	·	19	15	8	2	6	18	·
Rok	77	5.8	44.5	4.4	48.5	5.0	69.5	5.9	166	5.2	220.5	4.7	257	4.4	154	4.7	58	4.9	703	65.4	7.VIII	6	34	87	3	93	4	17	170	173	112	18	46	53	12

UWAGA. Obserwacji nad wiatrem w terminach klimatologicznych dokonywano za pomocą wiatromierza Wilde, w czasie między terminami – za pomocą anemografu.

Słupsk $\varphi = 54°28'$ $\lambda = 17°01'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnio I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.5	-0.4	8.5	22	-14.4	31	1.6	2.5	1.4	1.7	6.1	6.0	5.7	5.9	87	80	81	83	0.9	1.5	1.3	1.2	9.1	8.3	8.4	8.6
II	–	–	–	–	1.9	-3.0	6.1	12	-13.8	1,2	-1.2	0.6	-0.3	-0.3	4.9	5.2	5.0	5.0	84	80	81	82	0.9	1.2	1.2	1.1	9.0	7.4	6.1	7.5
III	–	–	–	–	2.7	-5.2	8.6	31	-13.7	15	-3.6	1.7	-1.3	-1.1	4.2	4.8	4.5	4.5	84	70	80	78	0.7	2.2	1.2	1.4	6.5	7.5	5.3	6.4
IV	–	–	–	–	13.0	4.1	26.7	25	-0.5	1	6.0	11.1	7.4	8.0	8.0	8.6	8.4	8.3	84	65	81	77	1.6	5.6	2.3	3.2	5.8	5.8	6.4	6.0
V	–	–	–	–	13.7	5.8	20.1	19	-0.7	2,6	8.6	12.2	8.7	9.6	9.6	9.3	9.6	9.5	85	66	84	78	1.7	5.2	1.9	2.9	7.1	8.5	6.1	7.2
VI	–	–	–	–	18.3	8.7	27.7	19	2.2	8	12.8	17.1	12.9	13.9	11.8	11.2	11.9	11.6	79	58	79	72	3.3	9.1	3.4	5.3	6.2	6.4	5.8	6.1
VII	–	–	–	–	19.4	10.0	27.3	21	6.5	4	13.5	18.3	13.9	14.9	13.5	14.0	13.9	13.8	87	67	87	80	2.1	7.5	2.2	3.9	6.5	6.6	5.3	6.1
VIII	–	–	–	–	19.0	11.6	28.7	12	6.1	10,15	13.8	18.0	14.3	15.1	13.8	13.9	14.1	13.9	87	68	86	80	2.1	7.0	2.3	3.0	7.2	7.8	6.7	7.2
IX	–	–	–	–	16.7	8.1	27.8	4	1.7	25	10.4	15.9	10.7	11.9	11.3	12.0	11.5	11.6	89	66	88	81	1.5	6.5	1.5	3.2	6.8	6.4	5.1	6.1
X	–	–	–	–	13.6	4.8	22.7	3	-2.3	28	6.5	13.0	8.1	8.9	9.3	10.7	9.9	10.0	93	71	89	84	0.7	4.8	1.3	2.3	7.4	5.1	6.0	6.2
XI	–	–	–	–	5.8	2.2	13.4	8	-2.8	18	3.2	5.2	3.6	3.9	7.0	7.4	7.1	7.2	89	83	88	87	0.9	1.8	1.0	1.2	8.4	8.1	8.6	8.4
XII	–	–	–	–	-0.9	-6.0	5.6	12	-18.6	24	-3.9	-1.8	-3.9	-3.4	4.3	4.7	4.3	4.4	86	82	85	84	0.6	0.9	0.7	0.7	8.0	7.2	7.4	7.5
Rok	–	–	–	–	10.6	3.4	28.7	12 VIII	-18.6	24 XII	5.6	9.5	6.3	6.9	8.6	9.0	8.8	8.8	86	71	84	80	1.4	4.4	1.7	2.5	7.3	7.1	6.4	6.9

Darłowo $\varphi = 54°27'$ $\lambda = 16°23'$

I	–	–	–	–	3.6	0.2	8.4	22	-14.4	31	1.2	2.3	1.7	1.7	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.2	9.0	8.6
II	–	–	–	–	1.5	-2.2	5.2	8,12	-13.0	1	-0.7	0.4	-0.2	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	9.1	7.3	7.1	7.8
III	–	–	–	–	2.3	-3.8	9.3	30	-9.2	16	-2.1	1.2	-1.1	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.1	5.5	6.4
IV	–	–	–	–	9.5	3.5	20.6	17	0.6	30	5.3	7.4	5.6	6.0	8.0	8.5	8.4	8.3	89	83	90	87	1.0	2.2	1.0	1.4	7.0	5.1	7.1	6.4
V	–	–	–	–	11.8	6.0	20.5	19	-0.2	3	8.2	9.9	8.0	8.5	9.8	9.8	9.8	9.8	90	81	90	87	1.2	2.7	1.1	1.7	7.4	7.0	7.6	7.3
VI	–	–	–	–	16.0	9.7	28.1	19	3.3	8	12.5	14.3	12.6	13.0	12.4	12.7	12.7	12.6	84	78	85	82	2.3	4.2	2.2	2.9	5.9	4.7	5.5	5.4
VII	–	–	–	–	17.6	11.1	27.2	21	6.3	4	14.0	16.3	13.9	14.5	14.3	15.0	14.5	14.6	89	81	91	87	1.8	4.0	1.5	2.4	5.6	5.8	5.5	5.6
VIII	–	–	–	–	18.0	12.3	25.7	12	7.5	15	14.3	16.8	14.8	15.2	14.3	15.0	14.8	14.7	87	78	88	84	2.1	4.4	2.0	2.8	7.3	6.6	7.1	7.0
IX	–	–	–	–	15.9	9.5	26.4	4	4.2	18,25	11.4	15.0	11.6	12.4	12.0	13.0	12.1	12.4	89	77	89	85	1.7	4.2	1.6	2.5	6.2	4.7	5.3	5.4
X	–	–	–	–	13.1	5.6	22.3	2	-0.4	28	8.1	12.0	8.4	9.2	9.9	11.4	10.6	10.6	90	80	93	88	1.1	3.0	0.9	1.7	6.9	5.8	5.8	6.2
XI	–	–	–	–	6.0	2.0	13.2	5,8	-3.3	18	3.3	5.1	3.5	3.8	7.4	7.8	7.4	7.5	93	88	92	91	0.6	1.3	0.7	0.9	8.5	7.7	7.5	7.9
XII	–	–	–	–	-0.3	-4.8	5.7	5	-16.2	22	-3.0	-1.4	-2.8	-2.5	4.7	5.2	4.7	4.9	86	88	86	87	0.6	0.6	0.6	0.6	7.3	7.3	7.1	7.2
Rok	–	–	–	–	9.6	4.1	28.1	19 VI	-16.2	22 XII	6.0	8.3	6.3	6.7	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.4	6.7	6.8

Gdańsk-Nowy Port $\varphi = 54°24'$ $\lambda = 18°40'$

I	–	–	–	–	3.1	-0.5	8.5	22	-15.5	31	1.5	2.3	1.0	1.4	5.9	5.8	5.6	5.8	84	78	83	82	1.1	1.6	1.1	1.3	7.7	7.3	7.9	7.6
II	–	–	–	–	1.4	-3.1	5.6	20	-15.0	1	-1.5	0.2	-0.3	-0.5	4.8	5.1	5.2	5.0	85	81	85	84	0.8	1.2	0.9	1.0	7.3	7.9	6.5	7.2
III	–	–	–	–	1.3	-4.6	7.6	31	-13.3	15	-3.4	0.7	-1.5	-1.4	4.0	4.8	4.6	4.5	82	75	83	80	0.8	1.7	0.9	1.1	6.3	6.3	5.4	6.0
IV	–	–	–	–	11.6	4.3	21.9	17	0.4	30	6.2	9.9	6.9	7.5	8.2	8.4	8.2	8.3	85	70	82	79	1.4	4.6	2.3	2.8	5.5	6.5	6.1	6.0
V	–	–	–	–	12.7	6.2	18.7	19	-0.3	1	8.6	11.5	8.7	9.4	9.6	9.6	9.6	9.6	86	72	84	81	1.7	4.3	1.9	2.6	7.5	7.7	6.9	7.4
VI	–	–	–	–	17.7	10.0	28.0	15	3.3	3	13.5	16.1	13.0	13.9	11.3	11.8	11.5	11.5	72	64	76	71	4.6	7.3	3.9	5.3	5.2	5.7	5.6	5.5
VII	–	–	–	–	18.9	11.3	26.8	21	7.4	5	14.9	17.6	14.7	15.5	13.6	13.5	13.7	13.6	80	68	81	76	3.4	7.0	3.2	4.5	5.2	5.9	6.3	5.8
VIII	–	–	–	–	19.2	12.3	28.0	12	8.3	10	14.5	17.9	15.0	15.6	13.4	14.1	13.7	13.7	81	69	80	77	3.2	6.7	3.4	4.4	5.9	6.9	4.6	5.8
IX	–	–	–	–	16.4	9.2	26.3	4	4.7	25	11.1	15.6	11.7	12.5	11.3	11.8	11.5	11.5	85	67	84	79	2.0	6.3	2.3	3.5	6.0	7.0	6.2	6.4
X	–	–	–	–	12.8	5.8	20.5	3	-1.5	28	7.3	12.3	8.9	9.4	9.1	10.3	9.7	9.7	87	71	82	80	1.3	4.2	2.1	2.5	7.0	6.5	6.5	6.7
XI	–	–	–	–	5.5	2.2	11.0	2,5	-3.1	24	3.3	4.9	3.9	4.0	6.9	7.2	7.0	7.0	87	81	86	85	1.1	1.7	1.2	1.3	7.7	7.6	7.8	7.7
XII	–	–	–	–	-0.1	-5.1	6.3	5	-17.7	21	-2.5	-1.3	-2.7	-2.3	4.5	4.7	4.5	4.6	82	80	81	81	0.9	1.2	0.9	1.0	8.0	6.9	7.0	7.3
Rok	–	–	–	–	10.0	4.0	28.0	15 VI, 12 VIII	-17.7	21 XII	6.1	9.0	6.6	7.1	8.6	8.9	8.7	8.7	83	73	82	79	1.9	4.0	2.0	2.6	6.6	6.8	6.4	6.6

Gdańsk-Wrzeszcz $\varphi = 54°23'$ $\lambda = 18°36'$

I	1010.3	1040.7	981.9	1011.9	3.3	-1.0	8.6	22	-15.9	31	1.5	2.1	1.1	1.4	5.9	5.8	5.7	5.8	84	80	83	82	1.1	1.5	1.1	1.2	8.5	8.5	8.0	8.3
II	1012.1	1037.6	969.5	1013.7	1.5	-3.6	5.6	20	-14.5	1	-1.7	0.0	-0.5	-0.7	4.6	5.0	4.8	4.8	83	80	80	81	1.0	1.2	1.2	1.1	8.0	8.4	7.7	8.0
III	1010.3	1027.3	982.3	1011.9	1.3	-5.7	7.6	31	-13.2	15	-3.5	0.5	-1.8	-1.6	4.0	4.6	4.3	4.3	83	71	80	78	0.8	1.9	1.1	1.3	6.8	6.8	5.6	6.4
IV	1012.2	1028.9	986.6	1013.7	12.5	4.0	25.1	21	-0.7	30	6.3	10.3	6.8	7.6	8.2	8.4	8.3	8.2	84	67	83	78	1.6	5.0	1.9	2.8	6.8	7.5	6.5	6.9
V	1010.6	1018.1	995.1	1012.1	13.1	5.8	19.3	19	-1.1	1	8.6	11.7	8.6	9.4	9.5	9.6	9.3	9.5	84	70	83	79	1.8	4.5	2.1	2.8	7.7	8.1	6.6	7.5
VI	1015.7	1031.0	1002.3	1017.2	18.3	9.6	28.0	15	3.4	3	13.3	16.3	12.8	13.8	11.0	11.1	11.2	11.1	71	60	75	69	4.6	8.2	4.0	5.6	6.0	6.5	5.8	6.1
VII	1011.9	1022.0	994.7	1013.4	19.3	10.8	28.0	21	7.4	5	14.5	17.7	14.2	15.2	13.3	12.8	13.5	13.2	80	65	83	76	3.4	7.9	2.9	4.7	5.4	6.7	6.2	6.1
VIII	1011.5	1021.3	999.6	1013.0	19.6	12.0	28.4	12	8.8	31	14.3	18.0	14.8	15.5	13.4	13.8	13.8	13.7	82	67	82	77	2.9	7.2	3.1	4.4	6.4	7.7	5.7	6.6
IX	1012.7	1029.8	990.2	1014.2	16.8	8.6	27.2	4	3.7	27	10.6	15.8	11.6	12.4	11.4	11.6	11.6	11.5	89	65	84	79	1.6	6.7	2.2	3.5	5.8	7.1	5.6	6.2
X	1019.6	1035.4	1003.6	1021.1	13.2	5.7	20.7	2,3	-2.0	28	7.2	12.3	8.9	9.3	9.3	10.3	9.8	9.8	89	71	84	81	1.1	4.3	1.9	2.4	6.0	6.8	5.3	6.0
XI	1016.1	1030.3	997.0	1017.7	5.6	1.7	12.2	4	-5.2	17	3.0	4.7	3.7	3.8	7.0	7.3	7.2	7.2	90	84	88	87	0.7	1.5	1.0	1.1	8.1	8.2	8.2	8.2
XII	1014.2	1049.4	971.7	1015.8	-0.1	-5.4	6.6	7	-18.6	21	-2.8	-1.5	-2.9	-2.5	4.6	4.7	4.5	4.6	86	81	85	84	0.7	1.1	0.8	0.9	8.5	7.1	7.6	7.7
Rok	1013.1	1049.4	969.5	1014.6	10.4	3.5	28.4	12 VIII	-18.6	21 XII	5.9	9.0	6.4	6.9	8.5	8.8	8.7	8.7	84	72	82	79	1.8	4.2	1.9	2.6	7.0	7.4	6.6	7.0

Słupsk $H_s = 16\,m$ $h_w = 17\,m$ 1962

Miesiąc	Rozkład wiatru (°D, °mD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr > 16	> 15	●	●	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	■	▦	≋
I	5	4.4	4	2.0	1	1.0	4	2.2	21.5	2.2	31.5	5.2	13	5.0	3	2.7	10	3.5	69	9.3	28	2	3	11	·	5	2	·	21	24	19	·	·	9?	·
II	14.5	4.5	15.5	2.0	·		2.5	2.0	8.5	2.3	19	5.8	12.5	7.1	3.5	7.8	8	4.1	74	21.8	12	2	8	23	·	8	2	1	16	21	13	4	·	21	·
III	7.5	2.7	6	2.6	5	2.5	10.5	2.4	11	1.7	5	3.8	1	6.0	5	3.5	42	1.5	46	17.8	12	4	4	28	·	1	·	4	9	15	10	1	1	22	·
IV	8.5	2.2	11	2.7	2.5	1.0	4.5	3.4	10	2.0	11.5	3.1	7.5	2.5	6.5	3.0	28	1.8	29	7.4	8	·	·	1	1	1	·	3	9	13	9	·	·	·	1
V	7.5	2.3	3	1.0	1	1.0	3	3.7	9	1.7	13.5	2.1	12.5	2.4	9.5	1.6	34	1.3	101	12.3	28	·	·	2	·	·	·	·	12	23	17	3	2	·	2
VI	10	2.9	1.5	1.7		·	1	3.0	9.5	1.7	20	3.1	16.5	3.3	5.5	2.9	26	2.0	54	11.7	19	·	·	·	3	1	1	1	6	11	6	2	·	·	4
VII	8.5	2.2	1.5	2.3	0.5	2.0	3.5	2.0	6.5	2.4	14	2.6	8.5	2.5	5	2.6	45	1.2	116	19.3	22	·	·	·	2	·	·	2	11	15	11	6	1	·	2
VIII		·	1	3.0	1.5	1.7	3.5	1.7	10	2.4	30.5	3.3	16	3.6	5.5	1.5	25	2.2	138	25.2	25	·	·	·	1	2	1	1	12	19	17	3	2	·	2
IX	1.5	2.3	1	2.0	2.5	1.4	2.5	2.6	8.5	1.9	18	2.9	14	4.5	7	1.9	3.5	1.8	68	12.8	23	·	·	·	1	1	1	7	9	14	13	2	1	·	1
X	0.5	3.0	·	·	1	1.0	5.5	1.6	11.5	1.7	18.5	2.2	7.5	1.9	4.5	1.9	44	1.0	30	11.3	4	·	·	5	·	·	·	3	12	11	8	1	5	·	·
XI	2.5	1.2	7	3.2	15.5	2.9	7	2.1	13.5	1.3	14	1.6	0.5	0.6	·	·	30	1.4	78	16.6	29	·	·	7	·	·	·	1	23	13	12	3	2	9	·
XII	2	1.8	5.5	1.2	2.5	1.0	·	·	25.5	1.6	19	1.8	2.5	1.8	2	1.8	34	1.0	43	8.9	14	8	15	23	·	1	·	2	17	16	9	·	5	17	·
Rok	68	2.5	57	2.0	33	1.3	47.5	2.2	14.5	1.9	21.45	3.1	11.2	3.4	57	2.6	361	1.9	846	25.2	25.VIII	16	30	100	8	20	7	25	157	195	144	25	19	78	12

Darłowo $H_s = 3\,m$ $h_w = 2.3\,m$

I	4	1.6	3	6.3	4	2.5	5	1.6	24	4.7	32.5	7.9	12	9.6	7.5	5.5	1	6.7	52	10.5	6	1	2	9	·	11	3	1	23	17	15	1	–	2	·
II	10.5	1.13	13.5	5.0	7.5	4.9	3	2.7	10	2.8	16	10.0	14	8.7	9.5	9.4	·	7.5	45	13.5	5	2	8	22	·	11	4	·	16	15	10	1	–	8	·
III	10	3.5	13.5	6.3	7.5	2.9	16.5	2.4	13	1.9	7	3.1	7	3.9	9.5	6.1	9	3.4	50	18.3	12	·	5	27	·	3	·	1	12	16	13	1	4	13	·
IV	11.5	5.5	22	3.5	6.5	3.4	3.5	1.6	10	4.0	20.5	4.5	10.5	3.5	3.5	5.0	2	3.9	27	6.4	16	·	·	·	·	2	·	1	5	11	9	·	7	·	·
V	11.5	5.2	7	3.9	4.5	1.3	2	3.0	15.5	2.5	31.5	2.9	9.5	5.8	3.5	6.7	8	3.3	75	19.8	13	·	·	1	·	·	·	·	13	18	14	1	7	·	·
VI	11	4.6	6	6.8	2	3.0	1	3.0	6	1.8	17	4.2	3.5	6.2	5	5.0	7	4.7	66	20.3	28	·	·	·	2	4	1	4	6	10	8	2	2	·	4
VII	7	3.6	9	3.1	2	1.0	7	1.7	9.5	2.5	16	4.3	2.6	4.6	8.5	2.9	8	3.3	83	16.2	2	·	·	·	1	·	·	6	9	14	12	3	4	·	2
VIII	4	5.1	1	2.0	7.5	1.5	4.5	1.7	10	3.4	29	7.3	28	6.7	3	6.2	6	5.3	105	18.2	24	·	·	·	1	6	1	1	10	19	16	4	·	·	1
IX	7.5	5.5	2	1.5	17.5	1.7	4.5	2.4	10	3.6	13	5.3	27	8.0	6.5	6.0	2	5.0	43	8.2	4	·		·	1	7	1	5	6	11	11	·	1	·	1
X	7.5	4.2	3.5	5.0	8	1.9	14.5	1.8	14.5	3.0	16	4.4	18	6.3	5	7.3	6	3.8	26	13.7	4	·		1	·	3	1	7	13	10	5	1	9	·	1
XI	3.5	7.3	5	6.7	23.5	4.0	11	2.5	2.6	3.0	7.5	4.5	8.5	7.4	1	6.0	4	4.0	41	9.2	29		·	9	·	4	·	2	20	11	10	·	4	1	·
XII	5	5.0	8.5	2.8	11	1.4	10	1.5	20.5	3.1	19	6.0	7	9.6	1	3.0	11	3.6	43	9.2	9	6	14	22		4	·	3	16	14	11	·	–	15	·
Rok	93	5.2	94	4.4	101.5	2.5	82.5	2.2	16.9	3.0	22.5	5.4	202.5	6.7	63.5	5.8	64	4.5	656	20.3	28.VI	9	29	91	5	55	11	31	149	166	134	14	–	39	9

Gdańsk - Nowy Port $H_s = 7\,m$ $h_w = 1.3\,m$

I	2.5	8.4	2	13.2	4	3.8	10	3.4	14	4.6	2.6	4.7	21	7.6	10.5	6.3	3	5.5	21	3.2	28	1	3	15	·	11	6?	1	16	15	9	·	2	8	·
II	8	11.9	7.5	8.4	5	7.9	7.5	5.1	12.5	4.8	10.5	6.0	16.5	8.0	10.5	10.6	6	7.2	24	9.2	12	2	8	23	·	17	9?	1	11	15	7	·	·	16?	1
III	8	6.1	10.5	5.9	2.5	3.2	20	2.7	13.5	3.2	3.5	2.3	6	6.1	11	4.3	18	3.3	23	3.8	6	1	9	30	·	4	3	3	9	9	8	·	3	17	·
IV	19.5	5.2	6	4.6	2.5	2.4	9	2.8	10	3.0	13	4.8	6	3.5	10	5.8	14	3.7	28	12.5	5	·	·	·	·	8	·	5	13	9	6	1	8	·	1
V	12.5	4.6	14	2.8	2.5	1.8	8	2.5	10.5	3.5	9	3.4	15	3.5	12.5	4.9	9	3.2	13.5	37.5	14	·	·	1	·	3	2	·	13	19	14	3	7	·	2
VI	16	8.3	7.5	3.4	1	5.0	4	3.1	6	3.6	3	3.7	24	4.7	11.5	5.0	17	4.2	42	12.2	16,29	·	·	·	2	6	2	3	4	10	7	2	·	·	3
VII	17	4.1	5.5	1.9	4.5	2.3	3	2.3	6	4.2	11	3.6	18.5	3.2	12.5	2.8	15	2.8	53	19.8	22	·	·	·	2	·	·	3	4	16	12	2	1	·	6
VIII	6	3.0	1.5	3.7	2.5	3.4	2.5	1.8	5.5	2.8	22.5	4.2	26.5	3.7	7	3.9	19	2.9	99	43.0	7	·	·	·	1	2	1	3	5	17	9	3	1	·	3
IX	3.5	5.6	4	1.8	8.5	1.4	6.5	2.2	9.5	3.2	16.5	4.7	23.5	4.1	11	3.5	7	3.3	74	24.7	18	·	·	·	1	7	2	2	9	15	13	2	2	·	1
X	6.5	5.2	2	1.7			12	2.3	19.5	2.4	6	3.0	25	3.6	12	3.7	10	2.8	11	4.8	5	·	·	1	·	3	1	2	12	7	3	·	6	·	·
XI	1.5	5.3	2.5	3.8	14.5	5.6	18.5	3.5	17.5	3.0	13	2.3	11.5	4.1	2	4.8	9	3.4	81	36.2	1	·	·	6	·	8	2	3	19	15	10	2	·	·	·
XII	1.5	3.0	2.5	3.4	6	3.7	16	2.7	19	3.6	15.5	3.8	18.5	3.8	6	4.7	8	3.3	37	14.2	17	8	15	22	·	9	1	1	16	15	8	1	1	17	·
Rok	102.5	5.9	65.5	4.6	53.5	3.4	117	2.9	143.5	3.5	149.5	3.9	212	4.7	116.5	5.0	135	3.8	628	43.0	7.VIII	12	35	98	6	78	29?	27	131	162	106	16	31	58?	17

Gdańsk - Wrzeszcz $H_s = 13\,m$ $H_b = 12.4\,m$ $h_w = 15.5\,m$

I	2.5	9.0	6.5	7.3	1.5	3.3	7	3.7	23	4.7	32.5	6.9	11.5	7.8	7.5	7.9	1	6.3	29	8.0	28	1	3	16	·	14	·	1	20	16	8	·	1	8	·
II	10	12.2	12	7.1	6	5.8	4.5	3.6	14	4.2	16	6.9	12.5	9.2	8	10.2	1	7.4	33	13.4	12	2	9	22	·	12	10	·	16	17	5	1	·	16	·
III	12	7.6	13	6.5	0.5	4.0	11	2.8	18	3.6	7.5	2.5	9	4.7	3	5.0	19	3.8	30	8.3	12	3	9	29		4	4	3	11	10	7	·	4	23	·
IV	17	6.0	17.5	4.6	2	3.5	4.5	3.8	11	4.1	14	5.2	2	4.0	5	5.6	17	4.0	25	12.4	5	·	·	1	1	3	·	2	13	10	6	1	6	·	·
V	15	5.5	17.5	4.3	1	2.0	5.5	3.2	12.5	3.5	16	3.8	9	4.2	5.5	6.4	11	3.8	97	29.7	14	·	·	1	·	2	2	·	12	19	11	3	7	·	2
VI	15	6.0	11	5.8	2.5	3.2	2.5	3.8	8	3.4	10.5	6.0	18.5	5.9	9	5.3	13	4.7	47	15.3	16	·	·	·	3	2	·	1	6	13	8	2	·	·	3
VII	9.5	4.7	17	4.7	1	5.0	2	2.2	13.5	3.6	12.5	5.6	12	5.8	12.5	4.1	13	4.1	59	24.0	22	·	·	·	2	1	1	2	6	17	13	1	·	·	2
VIII	5	5.0	5.5	3.3	4.5	3.1	2	3.5	8	3.9	27.5	5.4	22.5	5.8	10	5.0	8	4.6	108	53.8	7	·	·	·	1	2	1	1	11	14	10	3	·	·	3
IX	3.5	6.6	4.5	4.8	2.0	2.8	5.5	3.4	11	3.5	19	5.7	20	6.2	12.5	5.6	12	4.5	45	17.5	18	·	·	·	1	3	·	2	7	12	9	1	1	·	1
X	7	6.2	2.5	4.8	0.5	2.0	6	3.3	17.5	3.6	18	4.0	16	6.2	8.5	5.1	17	3.8	10	3.7	5	·	·	1	·	2	·	5	10	9	3	·	4	·	·
XI	3.5	4.1	1.5	6.0	1.0	7.0	18.5	3.1	21	3.2	16.5	4.0	5.5	5.3	1.5	5.7	12	3.6	64	23.7	1	·	·	5	·	2	·	1	18	12	10	2	3	1	·
XII	3	3.0	5	2.3	1	4.5	4	2.0	14.5	3.1	15	5.6	13	5.4	5.5	4.6	32	2.8	37	13.8	17	8	15	23	·	1	·	·	16	15	7	1	2	19	·
Rok	103	6.3	113.5	5.1	32.5	3.8	73	3.2	172	3.7	205	5.1	151.5	5.9	88.5	5.9	156	4.4	584	53.8	7.VIII	14	36	98	8	48	18	18	146	164	97	15	28	67	11

UWAGA. *Kierunki i prędkości wiatru - wg anemometru.*

Gdańsk-Siedlce $\varphi = 54°21'$ $\lambda = 18°36'$ 1962

Miesiąc	Ciśnienie p: P_m	Max	Min	$P_{o.m}$	Temperatura T: — Max	— Min	Max abs.	Data	Min abs.	Data	Średnia: I	II	III	Dies	Średnia prężność pary e_m: I	II	III	Dies	Średnia wilgotność względna U_m: I	II	III	Dies	Średni niedosyt wilgotności Δ_m: I	II	III	Dies	Średnie zachmurzenie N_m: I	II	III	Dies
I	-	-	-	-	2.6	-1.3	8.1	22	-17.7	31	0.9	1.7	0.4	0.8	6.0	5.9	5.7	5.9	88	83	88	86	0.8	1.2	0.8	0.9	9.0	8.8	7.8	8.5
II	-	-	-	-	1.1	-4.3	4.9	21	-16.3	1	-2.2	-0.3	-1.0	-1.1	4.6	4.9	4.8	4.8	85	80	82	82	0.8	1.2	1.0	1.0	8.2	8.8	7.5	8.2
III	-	-	-	-	1.4	-5.6	7.2	31	-14.2	15	-3.8	0.6	-2.2	-1.9	4.0	4.6	4.4	4.3	83	71	83	79	0.7	1.9	0.9	1.2	7.4	7.1	5.5	6.7
IV	-	-	-	-	12.7	4.3	27.8	21	-0.6	1	6.3	11.1	6.6	7.6	8.4	8.8	8.5	8.6	87	68	86	80	1.4	5.4	1.6	2.8	6.7	7.6	6.1	6.8
V	-	-	-	-	13.4	5.9	19.2	19	-0.8	1	8.9	12.1	8.4	9.4	10.0	9.8	9.7	9.8	86	71	87	81	1.6	4.6	1.5	2.6	8.0	8.9	7.0	8.0
VI	-	-	-	-	18.8	9.1	29.1	16	2.9	3	13.2	17.0	12.2	13.6	11.5	11.6	11.6	11.6	75	59	80	71	3.9	8.7	3.0	5.2	6.9	6.9	6.9	6.9
VII	-	-	-	-	19.7	10.7	27.4	20	6.7	5	14.5	18.2	13.5	14.9	13.8	13.9	13.8	13.8	83	67	88	79	2.8	7.4	1.9	4.0	6.1	8.1	7.4	7.2
VIII	-	-	-	-	19.5	11.6	27.6	12	7.9	10	14.0	18.1	13.9	15.0	13.8	14.5	14.1	14.1	86	70	88	81	2.3	6.6	1.9	3.6	7.9	8.7	5.8	7.5
IX	-	-	-	-	16.5	8.6	26.1	4	4.6	27	10.4	15.5	10.7	11.8	11.6	12.2	11.7	11.8	92	69	90	84	1.1	5.8	1.3	2.7	6.7	7.9	5.1	6.6
X	-	-	-	-	12.9	5.3	20.4	4	-1.4	28	6.6	12.1	8.2	8.8	9.3	10.6	9.9	9.9	93	74	89	85	0.7	3.9	1.3	2.0	6.4	7.4	5.6	6.5
XI	-	-	-	-	5.0	1.4	11.1	2	-3.8	24	2.6	4.3	3.1	3.3	7.0	7.4	7.1	7.2	92	88	90	90	0.5	1.1	0.7	0.8	8.8	8.3	7.8	8.3
XII	-	-	-	-	-0.7	-6.4	5.7	5	-20.2	21	-3.6	-2.0	-3.8	-3.3	4.5	4.7	4.5	4.6	88	83	87	86	0.6	0.9	0.6	0.7	8.7	7.6	6.5	7.6
Rok	-	-	-	-	10.2	3.3	29.1	16.VI	-20.2	21.XII	5.6	9.0	5.8	6.6	8.7	9.1	8.8	8.9	86	74	86	82	1.4	4.1	1.4	2.3	7.6	8.0	6.6	7.4

Kamienica Królewska $\varphi = 54°23'$ $\lambda = 17°54'$

I	-	-	-	-	1.9	-1.9	7.1	22	-14.8	31	0.1	0.6	-0.5	-0.1	-	-	-	-	-	-	-	-	-	-	-	-	9.7	9.2	8.9	9.3
II	-	-	-	-	-0.2	-4.8	3.6	20	-13.4	1	-2.9	-1.1	-2.3	-2.1	-	-	-	-	-	-	-	-	-	-	-	-	9.1	8.2	5.9	7.7
III	-	-	-	-	1.3	-8.7	6.1	31	-16.4	23	-5.9	0.0	-4.6	-3.8	-	-	-	-	-	-	-	-	-	-	-	-	6.7	7.0	6.0	6.6
IV	-	-	-	-	12.7	3.3	28.1	22	-1.9	1	5.9	11.0	6.5	7.5	-	-	-	-	-	-	-	-	-	-	-	-	6.9	6.8	6.1	6.6
V	-	-	-	-	13.0	4.5	18.5	19	-1.7	1,2	7.7	11.1	7.3	8.4	-	-	-	-	-	-	-	-	-	-	-	-	7.9	8.3	7.7	8.0
VI	-	-	-	-	17.9	6.8	28.4	16	0.1	8	11.6	16.4	11.0	12.5	-	-	-	-	-	-	-	-	-	-	-	-	6.8	6.0	6.5	6.5
VII	-	-	-	-	19.2	9.1	25.6	20	5.2	4	13.1	17.6	12.7	14.0	-	-	-	-	-	-	-	-	-	-	-	-	7.3	7.3	6.8	7.1
VIII	-	-	-	-	18.7	10.2	27.2	12	4.5	15	12.9	17.3	12.7	13.9	-	-	-	-	-	-	-	-	-	-	-	-	7.3	7.3	6.9	7.2
IX	-	-	-	-	15.7	7.4	26.0	4	2.1	18,25	9.8	14.4	9.9	11.0	-	-	-	-	-	-	-	-	-	-	-	-	6.5	6.5	5.7	6.2
X	-	-	-	-	12.5	4.2	22.1	4	-2.5	28	6.1	11.4	7.0	7.9	-	-	-	-	-	-	-	-	-	-	-	-	6.9	5.9	5.6	6.5
XI	-	-	-	-	4.7	0.8	11.7	8	-5.9	24	1.9	3.6	2.6	2.7	-	-	-	-	-	-	-	-	-	-	-	-	8.8	8.5	7.8	8.4
XII	-	-	-	-	-1.5	-7.7	4.6	12	-21.0	24	-4.7	-2.7	-5.1	-4.4	-	-	-	-	-	-	-	-	-	-	-	-	8.3	7.4	6.7	7.5
Rok	-	-	-	-	9.7	1.9	28.4	16.VI	-21.0	24.XII	4.6	8.3	4.8	5.6	-	-	-	-	-	-	-	-	-	-	-	-	7.7	7.4	6.5	7.3

Krynica Morska $\varphi = 54°23'$ $\lambda = 19°27'$

I	-	-	-	-	2.2	-1.2	6.2	22	-14.5	31	0.2	1.4	0.3	0.6		-	-	-	-	-	-	-	-	-	-	-	9.0	8.7	9.0	8.9
II	-	-	-	-	0.4	-3.1	3.5	20	-11.9	1	-2.1	-0.5	-1.4	-1.4	-	-	-	-	-	-	-	-	-	-	-	-	8.1	8.4	8.8	8.4
III	-	-	-	-	1.0	-5.1	7.2	31	-14.6	15	-4.0	0.0	-1.8	-1.9	-	-	-	-	-	-	-	-	-	-	-	-	6.9	6.6	6.1	6.5
IV	-	-	-	-	11.4	4.1	23.4	21	-0.4	8,11	6.0	10.2	6.4	7.2	-	-	-	-	-	-	-	-	-	-	-	-	7.0	6.5	6.8	6.8
V	-	-	-	-	13.4	6.6	18.4	13,19	0.5	1	9.0	11.9	8.9	9.7	-	-	-	-	-	-	-	-	-	-	-	-	8.4	7.5	7.3	7.7
VI	-	-	-	-	17.6	9.7	25.9	16	3.6	2	13.0	15.8	12.7	13.6	-	-	-	-	-	-	-	-	-	-	-	-	6.2	4.8	5.4	5.5
VII	-	-	-	-	19.3	12.2	28.6	21	9.3	4	14.5	18.0	14.6	15.4	-	-	-	-	-	-	-	-	-	-	-	-	7.1	5.1	6.3	6.2
VIII	-	-	-	-	19.7	12.5	25.2	12	9.8	31	14.9	18.7	15.3	16.0	-	-	-	-	-	-	-	-	-	-	-	-	6.7	6.5	7.5	6.9
IX	-	-	-	-	16.4	8.7	22.9	4	4.5	25	11.5	15.1	11.9	12.6	-	-	-	-	-	-	-	-	-	-	-	-	6.6	6.4	6.1	6.4
X	-	-	-	-	12.9	6.9	19.4	2,3	-0.6	28	0.6	11.8	9.3	9.8	-	-	-	-	-	-	-	-	-	-	-	-	7.7	6.0	5.2	6.3
XI	-	-	-	-	5.8	1.8	11.4	4	-4.0	22	2.8	4.5	3.5	3.6	-	-	-	-	-	-	-	-	-	-	-	-	9.2	9.1	8.0	8.8
XII	-	-	-	-	-1.3	-5.8	7.4	5	-17.6	23	-4.0	-2.9	-3.8	-3.6	-	-	-	-	-	-	-	-	-	-	-	-	7.5	7.1	6.5	7.0
Rok	-	-	-	-	9.9	3.9	28.6	21.VII	-17.6	23.XII	5.9	8.7	6.3	6.8	-	-	-	-	-	-	-	-	-	-	-	-	7.5	6.9	6.9	7.1

Czarna Dąbrówka $\varphi = 54°21'$ $\lambda = 17°34'$

I	-	-	-	-	2.1	-1.2	7.4	2.2	-12.1	31	0.7	1.3	0.8	0.6	-	-	-	-	-	-	-	-	-	-	-	-	10.0	8.9	8.2	9.0
II	-	-	-	-	0.4	-4.3	4.2	12,13	-14.9	1	-2.5	-0.6	-1.5	-1.5	-	-	-	-	-	-	-	-	-	-	-	-	9.6	8.7	8.1	8.8
III	-	-	-	-	0.9	-9.2	7.2	31	-16.9	24	-6.1	0.6	-4.0	-3.4	-	-	-	-	-	-	-	-	-	-	-	-	7.1	7.0	6.5	6.9
IV	-	-	-	-	12.3	3.6	25.6	21	-4.2	30	5.8	11.4	6.7	7.6	-	-	-	-	-	-	-	-	-	-	-	-	7.0	5.3	5.6	6.0
V	-	-	-	-	12.5	5.0	17.8	19	-2.5	1	8.0	11.7	7.8	8.8	-	-	-	-	-	-	-	-	-	-	-	-	7.7	8.2	6.6	7.5
VI	-	-	-	-	17.6	7.6	27.1	16	1.6	3,4	11.7	16.6	11.9	13.0	-	-	-	-	-	-	-	-	-	-	-	-	6.4	5.6	5.5	5.8
VII	-	-	-	-	18.5	9.0	25.4	26	6.1	5,9	13.0	17.6	13.2	14.2	-	-	-	-	-	-	-	-	-	-	-	-	6.3	7.0	5.8	6.4
VIII	-	-	-	-	17.9	10.8	26.6	12	4.8	15	13.3	17.2	13.4	14.3	-	-	-	-	-	-	-	-	-	-	-	-	7.7	7.7	6.1	7.2
IX	-	-	-	-	15.4	7.7	25.4	4	1.8	18,25	10.1	14.9	10.1	11.3	-	-	-	-	-	-	-	-	-	-	-	-	6.7	6.0	5.6	6.1
X	-	-	-	-	12.2	4.6	21.0	4	-2.4	15	5.9	11.8	7.6	8.2	-	-	-	-	-	-	-	-	-	-	-	-	8.6	5.9	6.6	7.0
XI	-	-	-	-	4.7	1.4	11.6	5	-6.2	24	2.6	4.2	3.2	3.3	-	-	-	-	-	-	-	-	-	-	-	-	9.1	7.8	8.2	8.4
XII	-	-	-	-	-1.8	-7.4	4.8	12	-19.9	24	-4.9	-2.4	-4.8	-4.2	-	-	-	-	-	-	-	-	-	-	-	-	8.3	7.1	7.0	7.5
Rok	-	-	-	-	9.4	2.3	27.1	16.VI	-19.9	24.XII	4.8	8.7	5.3	6.0	-	-	-	-	-	-	-	-	-	-	-	-	7.9	7.1	6.6	7.2

Gdańsk-Siedlce $H_s = 72\,m$ $h_w = 10\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU (%D, %mD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	≥ 15	◐	●	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	≡	⊞	R ≥ 0
I	5	8.0	4	6.8	·	·	4	4.2	15	5.0	20.5	6.9	22	7.9	14.5	8.1	8	6.4	35	10.2	28	2	3	16	·	10	·	1	23	18	8	1	·	13	·
II	13	11.9	6	9.3	10	6.5	3	8.0	13	5.0	12.5	7.1	14.5	9.5	12	8.6	·	8.1	43	12.8	12	2	8	24	·	12	4	1	18	19	6	1	·	19	·
III	16.5	8.2	5.5	6.7	8	5.9	10.5	4.6	26.5	4.9	4.5	4.4	6.5	5.1	10	7.2	5	5.6	49	17.0	12	2	9	29	·	4	1	5	15	10	9	1	2	22	·
IV	2.0	5.4	6	6.7	·	·	4	4.0	12	4.7	17.5	4.8	4.5	5.3	11	5.0	15	4.3	29	14.6	5	·	·	2	1	·	·	2	13	9	5	1	·	·	·
V	21.5	5.4	8.5	3.6	3	4.0	1	4.0	11	4.1	14	4.5	8.5	3.2	13.5	4.8	12	3.9	96	28.0	14	·	·	1	·	2	1	·	17	18	11	2	4	·	2
VI	21	8.3	8	4.3	3	4.0	·	·	8	4.0	13.5	7.1	13	6.2	17.5	5.2	6	5.8	52	15.1	29	·	·	·	4	5	1	·	12	11	9	2	·	·	4
VII	21	3.4	3	4.0	2	4.5	0.5	3.0	9.5	4.2	12.5	3.7	10.5	4.9	16	4.8	18	3.3	67	27.2	22	·	·	·	2	1	·	2	17	18	12	2	·	·	4
VIII	4	3.0	3	3.0	3	4.0	2	2.0	6	3.0	15	4.7	28.5	5.5	11.5	5.7	20	3.8	100	50.0	7	·	·	·	2	3	1	1	16	18	10	2	·	·	3
IX	2	3.5	·	·	3	2.0	3	4.7	8	4.2	10	4.9	16.5	5.7	22.5	4.4	25	3.4	67	22.4	18	·	·	·	1	2	1	2	10	14	11	2	1	·	1
X	8	3.5	2	2.5	0.5	2.0	1.5	1.3	18	3.7	8.5	4.2	14.5	5.8	17	4.0	23	3.1	11	2.6	19	·	·	1	·	1	1	3	13	11	4	·	4	·	·
XI	4	4.0	·	·	9.5	5.8	18.5	4.2	15.5	3.8	18.5	3.4	10.5	4.6	2.5	4.6	11	3.7	76	28.7	1	·	·	7	·	·	·	2	19	14	10	2	1	3	·
XII	4	2.2	1	3.0	6	2.5	3	2.7	9	3.0	19	4.5	17.5	4.4	12.5	5.4	21	3.1	35	13.6	17	9	15	24	·	1	·	1	17	18	8	1	·	20	·
Rok	140	5.6	4.7	4.0	4.8	3.4	5.1	3.6	145	4.1	166	5.0	167	5.7	160.5	5.6	164	4.5	660	500	7.VIII	15	35	104	10	41	10	20	190	178	103	17	12	77	14

Kamienica Królewska $H_s = 160\,m$ $h_w = 11\,m$

I	8	6.1	2	3.5	1	2.0	3	7.7	27	6.4	21	6.9	24	4.0	2	3.5	5	5.3	52	16.2	28	1	3	17	·	10	3	·	26	16	9	1	5	–	–
II	17	7.2	10	3.0	3	3.3	1	2.0	22	6.5	11	9.2	13	6.5	2	2.5	5	5.9	67	14.0	5	3	11	23	·	10	5	·	21	16	14	2	5	–	–
III	11	6.7	6	6.5	6	2.0	1	10.0	34	6.2	2	2.5	3	2.3	2	4.0	28	3.9	46	17.2	12	13	7	30	·	7	2	2	13	11	7	2	3	–	–
IV	18	2.9	7	5.3	4	5.0	·	·	23	4.9	12	4.0	3	2.3	10	3.2	13	3.4	28	6.9	27	·	·	5	2	3	·	2	11	11	9	·	2	·	–
V	9	3.9	4	3.0	6	2.0	2	5.0	21	4.1	14	3.0	7	2.7	5	1.8	25	2.4	89	23.4	14	·	·	4	·	1	·	·	14	21	17	1	5	·	–
VI	11	3.5	4	6.2	4	5.0	2	6.0	7	5.4	12	6.4	19	3.4	9	2.4	22	3.3	52	8.5	16	·	·	·	3	4	1	1	9	13	11	·	·	·	–
VII	20	2.9	5	3.0	6	3.0	1	2.0	18	4.3	15	4.8	12	3.2	6	3.2	10	3.2	57	14.8	14	·	·	·	2	1	·	·	15	17	16	1	3	·	–
VIII	4	2.8	·	·	1	3.0	5	3.6	24	6.2	17	6.7	19	6.0	8	4.2	15	4.8	85	12.5	24	·	·	·	1	8	2	1	14	17	13	3	3	·	–
IX	12	2.8	·	·	3	2.3	4	3.0	19	4.7	12	6.9	14	4.1	6	2.2	20	3.3	63	12.0	18	·	·	·	1	3	·	3	9	14	12	1	5	·	–
X	6	1.8	·	·	·	·	·	·	33	4.7	7	5.1	17	3.5	5	2.4	25	2.9	23	6.0	18	·	·	7	·	2	·	4	13	12	7	·	11	·	–
XI	2	2.5	3	8.3	10	5.3	1.7	7.4	26	3.6	14	4.6	4	2.5	·	·	14	4.2	52	22.5	1	·	1	14	·	5	·	·	22	8	7	2	12	–	–
XII	4	3.0	5	1.4	7	2.1	3	2.3	29	5.4	13	4.9	7	3.0	3	3.7	22	3.2	32	14.0	11	12	15	28	·	5	1	2	16	15	6	1	8	–	–
Rok	122	3.8	4.6	3.4	5.1	2.9	3.9	4.1	283	5.2	150	5.4	142	3.6	58	2.8	204	3.8	646	23.4	14.V	29	37	128	9	59	14	15	183	171	128	14	62	–	–

Krynica Morska $H_s = 4\,m$ $h_w = 17\,m$

I		·	5	6.9	5	5.3	2	3.5	12	5.4	3.9	5.6	20	8.2	7	4.8	3	5.9	21	4.1	6	2	3	15	·	5	1	2	27	15	7	·	2	6	–
II	9	8.0	5	9.0	14.5	5.6	4.5	4.7	5.5	6.9	20.5	8.2	11.5	7.8	11.5	11.2	2	7.9	14.3	4.6	5	1	9	22	·	12	5	2	23	14	5	·	1	22	–
III	8	5.6	1.6	8.2	8.5	3.6	13.5	4.9	9	4.6	10	3.2	7.5	5.2	8.5	5.8	12	4.7	24	8.3	13	4	6	28	·	7	1	5	15	9	4	·	1	27	–
IV	11	4.6	6.5	5.6	8.5	4.7	7	6.2	3	3.2	22	4.2	8.5	3.4	10.5	4.1	13	3.8	10.3	4.1	5	·	·	2	·	1	·	2	13	8	3	·	5	·	–
V	8	6.4	3.5	3.3	10.5	3.0	2	4.0	4.5	5.2	27.5	4.1	7	3.6	13	5.3	17	3.6	16.0	39.6	14	·	·	·	·	3	·	1	19	20	16	7	1	·	–
VI	9	4.7	12.5	8.5	0.5	12.0	3	3.0	4	2.6	28.5	3.9	20.5	7.1	8	4.3	4	5.2	61	17.4	16	·	·	·	3	6	2	4	5	12	7	3	·	·	–
VII	1.5	2.0	9	2.1	1.5	2.6	2.5	2.2	1.5	2.3	19	4.8	18.5	4.7	18.5	4.6	21	3.2	61	11.7	2	·	·	·	2	1	·	5	10	17	13	1	·	·	–
VIII	2	4.5	·	·	·	·	0.5	3.0	4	2.4	49.5	5.0	21.5	5.3	7.5	6.5	8	4.6	94	19.8	18	·	·	·	1	3	·	3	14	18	13	3	·	·	–
IX	5	5.4	·	·	9	3.4	2	1.0	12	4.8	19.5	6.4	13.5	6.7	23	7.5	6	5.6	83	20.6	18	·	·	·	·	11	·	4	12	14	12	2	1	·	–
X	5	5.2	6	3.3	1.5	6.0	1.5	3.3	16	2.7	32.5	5.1	18.5	5.0	5	5.0	7	4.1	14	3.7	31	·	·	1	·	·	·	2	10	8	5	·	5	·	–
XI	1	10.0	2.5	10.4	8	4.3	20.5	8.2	14	2.5	24	3.4	16	3.2	4	2.0	2	4.5	39	7.2	20	·	·	6	·	7	·	·	23	12	10	·	6	·	–
XII	4	3.4	4	2.5	18	2.8	3	2.5	4.5	6.2	32	4.4	12	6.7	6.5	4.7	9	3.9	16	7.4	1	9	15	26	·	3	·	5	16	11	3	·	2	18	–
Rok	63.5	5.0	7.0	5.0	83.5	4.4	6.2	3.9	9.0	4.1	324	4.9	17.5	5.6	123	5.5	104	4.7	597.2	39.6	14.V	16	33	100	6	59	9	35	187	158	98	16	24	73	–

Czarna Dąbrówka $H_s = 120\,m$ $h_w = 12\,m$

I	2	13.0	3	3.0	3	2.7	7	5.9	10	8.3	3.9	7.7	15	5.7	14	6.1	·	6.9	51	8.0	28	2	4	15	·	9	4	·	25	25	13	·	–	–	·
II	14	7.6	·	·	13	3.1	2	5.0	11	6.0	20	6.2	12	11.5	12	10.0	·	7.2	53	13.6	12	3	12	23	·	12	7	·	19	22	10	2	–	–	·
III	11	6.4	3	3.7	4	3.0	1.5	4.7	22	4.6	11	2.7	19	3.5	8	5.5	·	4.3	44	9.2	12	17	9	30	·	5	1	1	11	13	11	·	–	–	·
IV	10	3.4	1	6.0	5	2.8	2	7.0	24	3.9	20	4.3	12	4.2	16	3.9	·	4.0	22	5.8	27	·	·	4	1	·	·	4	7	12	6	·	–	·	1
V	4	3.2	·	·	1	3.0	8	3.4	15	4.8	26	4.0	24	3.4	15	4.9	·	4.0	112	20.4	13	·	·	3	·	2	·	·	12	27	21	2	–	·	4
VI	12	5.5	1	2.0	·	·	·	·	6	6.3	16	4.8	39	4.8	16	3.7	·	4.7	54	9.3	29	·	·	·	4	1	·	4	5	12	10	·	1	·	3
VII	8	2.9	1	3.0	·	·	·	·	11	3.9	20	4.0	26	3.7	27	3.4	·	3.6	92	14.1	22	·	·	·	2	·	·	1	7	16	14	3	–	·	5
VIII	1	5.0	·	·	·	·	·	·	14	4.1	30	5.5	36	5.6	12	3.0	·	5.0	106	12.6	24	·	·	·	1	5	1	1	7	19	17	4	–	·	2
IX	2	4.0	·	·	2	2.0	1.3	3.6	16	4.1	17	5.2	24	4.8	15	4.3	1	4.4	63	14.9	20	·	·	·	1	4	·	5	8	15	11	1	1	·	3
X	7	3.3	·	·	·	·	2	6.0	17	5.0	39	3.3	17	4.6	8	2.0	3	3.7	27	5.0	26	·	·	5	·	1	·	2	16	14	8	·	5	·	1
XI	3	2.7	2	7.0	9	4.0	2.1	5.7	18	4.1	31	3.6	3	6.7	3	3.3	·	4.4	74	27.1	1	·	·	12	·	2	·	1	20	12	10	2	·	–	·
XII	5	2.6	3	2.3	1.5	2.2	5	4.0	23	4.7	29	5.2	8	3.9	5	3.6	·	4.1	26	5.8	9	11	16	27	·	1		2	14	14	7	·	1	–	·
Rok	79	5.0	1.4	2.2	52	1.9	7.5	3.8	187	5.0	298	4.7	235	5.2	151	4.5	4	4.7	724	27.1	4.XI	33	41	119	9	42	13	21	151	201	138	14	–	–	19

Świbno $\varphi = 54°20'$ $\lambda = 18°56'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA t												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{m.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.9	-1.2	8.0	22	-15.5	31	0.7	1.7	0.4	0.8	5.9	5.9	5.6	5.8	9.0	8.3	8.7	8.7	0.7	1.2	0.9	0.9	9.2	8.5	8.0	8.6
II	–	–	–	–	1.2	-3.7	5.6	20	-13.3	1	-2.1	-0.4	-1.0	-1.1	4.7	5.1	4.9	4.9	8.8	8.4	8.6	8.6	0.7	0.9	0.8	0.8	7.9	8.4	8.0	8.1
III	–	–	–	–	1.1	-4.8	7.0	31	-15.1	15	-4.0	0.1	-1.9	-1.9	4.0	4.8	4.5	4.4	8.3	7.8	8.2	8.1	0.7	1.4	0.9	1.0	7.2	7.0	5.4	6.5
IV	–	–	–	–	12.0	4.4	26.8	21	-0.2	6	5.9	9.9	6.6	7.2	8.5	8.8	8.6	8.6	8.9	7.2	8.6	8.2	1.1	4.2	1.4	2.2	7.1	7.0	6.9	7.0
V	–	–	–	–	13.2	6.5	18.5	19	0.7	1,2	8.7	11.2	9.0	9.5	10.1	10.2	10.0	10.1	8.8	7.6	8.6	8.3	1.4	3.5	1.6	2.2	7.7	8.1	7.2	7.7
VI	–	–	–	–	17.7	9.3	26.1	18	4.0	6	12.8	15.4	12.8	13.4	11.8	11.7	12.2	11.9	7.8	6.7	8.2	7.6	3.2	6.5	2.9	4.2	5.9	6.2	6.3	6.1
VII	–	–	–	–	19.0	11.0	27.2	21	6.9	6	14.3	17.5	14.6	15.2	13.9	13.6	14.3	13.9	8.4	6.9	8.5	7.9	2.6	6.7	2.5	3.9	6.6	6.4	7.3	6.8
VIII	–	–	–	–	19.1	11.5	27.6	12	7.4	10	14.0	17.8	14.8	15.4	14.1	15.4	14.7	14.7	8.8	7.6	8.7	8.4	2.0	5.3	2.2	3.2	6.8	7.3	6.6	6.9
IX	–	–	–	–	16.2	8.8	24.8	4	4.4	25	10.8	15.4	11.7	12.4	11.6	13.3	12.0	12.3	8.9	7.6	8.6	8.4	1.4	4.5	1.9	2.6	6.4	7.2	6.0	6.5
X	–	–	–	–	12.1	5.0	19.4	4	-2.2	28	7.0	11.5	8.6	8.9	9.2	10.6	10.0	9.9	9.0	7.6	8.8	8.6	1.2	3.4	1.5	2.0	7.8	7.2	5.8	6.9
XI	–	–	–	–	5.4	1.5	11.4	4	-3.5	25	2.8	4.6	3.6	3.6	7.0	7.4	7.1	7.2	9.1	8.6	8.8	8.8	0.7	1.3	1.0	1.0	8.3	8.4	7.4	8.0
XII	–	–	–	–	-0.6	-6.1	6.4	5	-17.8	21	-3.4	-2.4	-3.7	-3.3	4.6	4.7	4.5	4.6	8.9	8.6	8.8	8.8	0.5	0.7	0.6	0.6	8.1	7.5	6.3	7.3
Rok	–	–	–	–	9.9	3.5	27.6	12.VIII	-17.8	21.XII	5.6	8.5	6.3	6.7	8.8	9.3	9.0	9.0	8.7	7.7	8.6	8.3	1.4	3.3	1.5	2.1	7.4	7.4	6.8	7.2

Kartuzy $\varphi = 54°20'$ $\lambda = 18°12'$

I	–	–	–	–	1.4	-1.9	6.6	22	-14.9	31	-0.2	0.3	-0.5	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	9.6	9.2	8.8	9.2
II	–	–	–	–	-0.4	-4.8	3.2	12,20	-14.7	1	-3.5	-1.7	-2.2	-2.4	–	–	–	–	–	–	–	–	–	–	–	–	8.8	9.2	8.5	8.8
III	–	–	–	–	0.7	-7.1	6.2	31	-13.8	2	-5.4	-0.4	-3.8	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.4	4.4	6.1
IV	–	–	–	–	12.1	3.3	25.9	21	-1.4	1.30	5.8	10.7	6.2	7.2	8.2	8.2	8.3	8.2	8.7	6.5	8.6	7.9	1.4	5.9	1.7	3.0	6.4	6.6	5.3	6.1
V	–	–	–	–	12.6	5.1	18.7	19	-1.8	1	7.7	11.0	7.5	8.4	9.4	9.6	9.2	9.4	8.8	7.4	8.8	8.3	1.3	3.8	1.3	2.1	7.3	9.2	6.8	7.8
VI	–	–	–	–	17.2	8.2	27.5	16	2.8	2	11.5	15.5	11.7	12.6	10.9	11.4	11.3	11.2	7.9	6.4	8.0	7.4	3.1	7.0	3.0	4.4	5.4	6.2	5.0	5.5
VII	–	–	–	–	18.4	10.0	26.3	26	6.2	4	13.0	16.9	12.8	13.9	13.4	14.2	13.7	13.8	8.9	7.4	9.2	8.5	1.8	5.5	1.3	2.9	6.4	8.3	6.6	7.1
VIII	–	–	–	–	18.0	11.0	27.0	12	7.0	15	12.8	16.7	13.2	14.0	13.1	13.5	13.7	13.4	8.8	7.2	9.0	8.3	1.8	5.8	1.6	3.1	8.0	7.9	7.4	7.8
IX	–	–	–	–	14.9	7.9	26.5	4	3.0	25	9.4	14.0	10.0	10.8	11.2	11.7	11.4	11.4	9.4	7.3	9.2	8.6	0.8	4.7	1.0	2.2	8.1	8.0	5.1	7.1
X	–	–	–	–	12.0	4.8	20.6	4	-2.0	28	6.2	11.1	7.3	8.0	9.2	10.1	9.6	9.6	9.5	7.5	9.1	8.7	0.6	3.6	1.0	1.7	8.3	6.7	5.6	6.9
XI	–	–	–	–	3.8	0.8	9.9	2,4	-4.5	22,24	1.7	3.0	2.3	2.3	6.9	7.1	7.0	7.0	9.7	9.2	9.5	9.5	0.2	0.7	0.4	0.4	9.3	9.0	8.3	8.9
XII	–	–	–	–	-2.2	-6.9	4.1	5	-18.8	21	-4.7	-3.3	-4.9	-4.4	4.4	4.7	4.4	4.5	9.4	9.1	9.4	9.3	0.2	0.4	0.2	0.3	8.2	7.5	7.1	7.6
Rok	–	–	–	–	9.0	2.5	27.5	16.VI	-18.8	21.XII	4.5	7.8	5.0	5.6	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.9	6.6	7.4

Tolkmicko $\varphi = 54°19'$ $\lambda = 19°32'$

I	–	–	–	–	2.7	-0.8	8.4	22	-15.6	31	0.8	1.8	0.5	0.9	5.9	6.0	5.7	5.9	8.8	8.4	8.6	8.6	0.8	1.1	0.9	0.9	8.7	7.8	8.4	8.3
II	–	–	–	–	-0.7	-3.4	4.1	12	-13.0	1	-2.3	-0.4	-1.3	-1.3	4.5	4.8	4.7	4.7	8.5	8.0	8.3	8.3	0.8	1.2	0.9	1.0	8.4	7.6	7.9	8.0
III	–	–	–	–	0.9	-5.6	8.8	31	-15.6	15	-4.3	0.2	-1.8	-1.9	4.0	4.7	4.3	4.3	8.6	7.4	7.9	8.0	0.6	1.6	1.1	1.1	6.6	7.2	6.3	6.7
IV	–	–	–	–	12.5	5.1	24.3	21	0.5	7,30	6.9	10.4	7.6	8.1	8.7	9.3	8.7	8.9	8.6	7.3	8.3	8.1	1.6	4.1	2.1	2.6	7.1	7.1	6.9	7.0
V	–	–	–	–	13.7	6.7	18.9	13,19	0.6	1	9.4	11.9	9.3	10.0	10.1	10.6	10.1	10.3	8.5	7.6	8.5	8.2	1.8	3.6	1.8	2.4	7.7	7.3	7.5	7.5
VI	–	–	–	–	17.6	10.2	25.8	15,19	3.6	2	13.0	15.2	13.2	13.6	12.1	12.4	12.6	12.4	8.0	7.2	8.2	7.8	3.2	5.6	3.0	4.0	5.9	5.4	6.4	5.9
VII	–	–	–	–	19.0	12.5	27.5	21	8.1	4	14.7	17.5	14.9	15.5	14.4	14.7	14.5	14.5	8.6	7.4	8.5	8.2	2.4	5.5	2.6	3.5	6.3	6.0	6.9	6.4
VIII	–	–	–	–	19.4	12.9	26.9	12	8.1	15	14.6	18.0	15.2	15.8	14.1	15.0	14.5	14.5	8.5	7.3	8.3	8.0	2.6	6.0	3.0	3.9	6.8	6.5	6.8	6.7
IX	–	–	–	–	16.2	9.5	26.3	4	5.5	25	10.9	15.1	11.9	12.4	11.9	13.6	12.5	12.7	9.1	7.9	8.9	8.6	1.3	3.9	1.6	2.3	6.5	6.9	6.8	6.7
X	–	–	–	–	12.7	6.6	20.5	1,2,4	0.0	28	7.9	11.8	8.9	9.4	9.8	11.3	10.2	10.4	9.0	8.0	8.7	8.6	1.1	2.9	1.6	1.9	6.9	6.4	6.9	6.7
XI	–	–	–	–	5.7	1.9	13.3	4	-4.7	25	2.6	4.8	3.6	3.6	6.9	7.5	7.1	7.2	9.1	8.6	8.8	8.8	0.7	1.3	1.0	1.0	7.6	7.7	7.4	7.6
XII	–	–	–	–	-1.4	-5.7	5.2	12	-19.6	23	-3.9	-2.7	-3.9	-3.6	4.4	4.5	4.3	4.4	8.6	8.4	8.6	8.5	0.7	0.8	0.7	0.7	7.6	6.9	7.0	7.2
Rok	–	–	–	–	9.9	4.2	27.5	21.VII	-19.6	23.XII	5.9	8.6	6.5	6.9	8.9	9.5	9.1	9.2	8.7	7.8	8.5	8.3	1.5	3.1	1.7	2.1	7.2	6.9	7.1	7.1

Gołdap $\varphi = 54°19'$ $\lambda = 22°19'$

I	–	–	–	–	0.8	-3.2	5.4	22	-22.8	31	-1.6	-0.3	-1.2	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	8.9	9.1	8.2	8.7
II	–	–	–	–	-1.0	-7.7	3.0	12	-20.0	28	-5.0	-2.6	-4.3	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.8	6.3	7.5
III	–	–	–	–	-0.2	-9.5	6.0	31	-19.7	1,2	-7.1	-4.2	-4.5	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.5	6.7	5.8	7.0
IV	–	–	–	–	13.0	3.9	26.7	23	-1.6	8	6.0	11.6	7.5	8.2	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.8	6.0	6.4
V	–	–	–	–	14.2	5.0	19.8	27	-1.9	1	8.6	12.6	8.6	9.6	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.2	7.2	7.8
VI	–	–	–	–	18.3	7.3	27.6	16	2.1	2,8	12.1	16.8	11.8	13.1	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.8	6.2	6.4
VII	–	–	–	–	19.5	9.8	26.8	21	5.5	8,30	13.5	17.7	13.4	14.5	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.7	6.7	7.5
VIII	–	–	–	–	19.4	10.6	25.3	12	2.1	15	13.7	18.0	13.8	14.8	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.9	6.5	7.5
IX	–	–	–	–	15.2	6.1	24.6	5	0.3	25,27	9.5	14.2	10.3	11.1	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.3	5.1	7.2
X	–	–	–	–	11.4	4.1	18.8	1,4	-2.4	15	6.1	10.5	6.8	7.6	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.5	7.3	7.9
XI	–	–	–	–	4.8	0.7	12.4	2	-7.2	26	1.8	3.8	2.5	2.6	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.7	8.1	8.7
XII	–	–	–	–	-2.9	-8.5	3.2	5,6	-23.9	23	-6.1	-4.5	-6.1	-5.7	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.6	7.2	8.0
Rok	–	–	–	–	9.4	1.6	27.6	16.VI	-23.9	23.XII	4.3	8.0	4.9	5.5	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.8	6.7	7.5

Świbno $H_s = 3\,m$ $h_w = 10\,m$ 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R (?)
	ROZKŁAD WIATRU nD, vmD																		OPAD R			LICZBA DNI (n) Temperatura T				Wiatr v				Opad R					
I	1	5.0	6	7.2	3	4.3	9.5	5.0	25	4.8	19	6.1	17.5	4.9	8	7.7	4	5.3	18	3.8	25	1	3	14	·	5	1	1	24	11	7	·	·	9?	·
II	8.5	10.5	9.5	7.3	8.5	5.7	6.5	5.2	17	5.5	10	6.8	10.5	6.0	10.5	9.2	3	6.7	25	7.6	12	1	8	23	·	11	1	·	17	13	8	·	·	15?	1
III	14.5	8.4	8	6.9	7	5.6	17.5	5.7	13	3.3	3	2.3	8.5	2.8	5.5	6.3	16	4.6	26	4.1	13	4	9	30	·	5	·	4	12	11	9	·	5	18?	·
IV	20	5.8	10.5	4.9	4	4.6	9	5.2	11	3.6	8	5.9	5	3.0	14.5	5.3	8	4.6	30	11.0	5	·	·	1	1	6	·	1	14	13	6	1	6	·	·
V	12.5	5.4	14.5	4.1	5	3.2	6	5.4	14	3.6	10.5	3.8	11.5	2.6	16	5.3	3	4.1	126	42.6	14	·	·	·	·	2	·	·	15	17	15	4	3	·	7
VI	19	7.0	7.5	2.7	2	1.5	1	3.0	6	2.4	10.5	4.8	23	3.4	15	3.7	6	4.0	74	19.8	11	·	·	·	3	6	1	1	8	12	9	3	·	·	4
VII	22.5	4.7	6.5	4.5	2.5	2.6	5.5	6.2	8.5	4.3	13.5	4.0	13.5	3.7	14.5	3.9	6	4.0	92?	31.7?	1	·	·	·	2	2	·	3	12	15	10	3	·	·	4
VIII	6.5	2.9	2	4.5	2.5	3.6	4.5	4.9	11	4.2	20	5.0	24.5	4.2	10	5.2	12	3.9	82	22.6	5	·	·	·	1	4	·	1	14	14	13	2	·	·	2
IX	5.5	3.7	3.5	3.6	5	2.8	4	4.8	12	3.8	18	4.7	14	4.2	13	4.6	15	3.5	83	21.6	18	·	·	·	·	4	·	1	10	13	11	4	2	·	1
X	9.5	4.6	1	4.0		·	10	3.3	16	3.5	14.5	3.3	10.5	3.3	8.5	5.4	23	2.8	9	3.0	31	·	·	4	·	1	·	·	13	9	3	·	6	·	
XI	3	4.7	5	8.6	16.5	6.1	13.5	3.9	16	3.0	16.5	3.5	3.5	3.6	3	2.7	13	3.7	52	13.7	1	·	·	7	·	3	·	2	17	15	11	1	8	·	·
XII	2	4.5	7.5	3.2	13.5	2.4	5.5	4.5	22	4.2	15.5	4.0	6	3.2	5	5.4	16	3.1	17	5.2	13	9	15	25	·	1	·	2	14	11	7	·	1	18?	·
Rok	124.5	5.6	81.5	4.9	69.5	3.5	92.5	4.8	171.5	3.8	159	4.5	148	3.7	123.5	5.4	125	4.2	634?	42.6	14.V	15	35	104	7	50	3	16	170	154	109	18	31	60?	19

Kartuzy $H_s = 220\,m$ $h_w = 10\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R (?)
I	3	7.0	4	3.0	2	3.0	1	1.0	3	2.3	55	3.4	17	2.8	6	4.3	2	3.3	61	10.5	28	2	4	18	·	1	·	·	26	16	16	1	9	22	–
II	8	6.1	8	3.8	5	4.2	6	2.7	2	3.0	30	3.3	15	6.1	8	7.2	2	4.4	52	12.3	12	2	12	24	·	4	·	1	21	15	10	1	4	28	–
III	7	5.0	6	3.0	2	5.0	4	3.5	7	2.1	18	1.4	9	2.1	7	2.7	33	1.7	40	13.6	12	11	12	30	·	·	·	4	11	9	7	1	7	31	–
IV	10	3.2	4	3.0	2	3.0	7	3.3	7	2.1	26	2.4	12	1.7	9	2.8	13	2.2	34	9.1	5	·	·	6	1	·	·	3	12	10	9	·	4	3	–
V	3	5.0	3	5.0	1	3.0	3	2.3	4	2.0	33	2.1	19	1.8	12	4.2	15	2.2	101	29.0	14	·	·	2	·	·	·	·	14	21	14	4	6	·	–
VI	9	5.7	2	5.0	·	·	1	3.0	1	3.0	23	2.3	30	3.0	16	3.9	8	3.0	58	10.0	26	·	·	·	3	·	·	3	6	15	12	1	·	·	–
VII	4	2.0	3	3.0	1	1.0	·	·	1	1.0	36	2.4	23	2.0	14	2.1	11	1.9	94	19.2	13	·	·	·	3	·	·	1	11	18	14	2	1	·	–
VIII	1	3.0	1	1.0	·	·	1	3.0		·	48	3.5	18	2.3	19	3.0	5	3.0	132	42.4	7	·	·	·	1	1	1	1	17	21	14	4	·	·	–
IX	1	1.0	·	·	·	·	4	1.0	1	1.0	39	2.7	16	2.4	17	2.6	12	2.2	64	10.0	19	·	·	·	1	·	·	·	9	15	14	1	6	·	–
X	2	2.0	·	·	·	·	1	1.0	3	2.3	34	1.5	26	2.5	7	3.9	20	1.6	15	4.0	18	·	·	4	·	·	·	2	12	11	7	·	14	·	–
XI	1	3.0	4	3.0	3	4.0	16	2.8	9	2.6	36	1.8	10	1.8	5	2.2	6	2.1	61	18.2	1	·	2	14			·	2	25	11	10	3	6	7	–
XII	1	1.0	2	1.0	1	1.0	7	1.3	2	1.0	34	2.6	10	2.4	13	3.8	23	1.9	48	14.4	18	11	17	26	·	1	·	2	17	11	9	1	9	20	–
Rok	50	3.7	37	2.6	17	2.0	51	2.1	40	1.9	412	2.4	205	2.6	133	3.6	150	2.5	760	42.4	7.VIII	26	47	124	9	7	1	19	181	173	136	19	66	111	–

Tolkmicko $H_s = 1\,m$ $h_w = 19\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R (?)
I	0.5	8.0	7	8.6	3	3.7	4	4.8	13.5	8.7	54	8.9	5.5	7.6	4.5	10.7	1	8.4	38	5.8	27	2	3	14	·	–	–	2	23	20	9	·	·	13	·
II	5	11.2	8.5	7.0	11.5	6.6	6.5	5.0	6.5	9.0	30	8.3	10	10.2	6	13.8	·	8.5	40	9.3	16	1	10	23	·	–	–	1	20	16	9	·	·	23	·
III	3	5.3	11.5	7.7	9.5	4.2	22.5	5.4	12	5.1	18	4.0	5.5	5.6	5	7.6	6	5.0	51	13.8	12	6	9	30	·	–	–	4	16	13	8	2	2	30	·
IV	13.5	5.6	11.5	6.2	2.5	6.8	13	5.0	11.5	5.3	20.5	5.8	7	4.6	9.5	5.5	1	5.4	15	4.1	12	·	·	·	·	–	–	2	10	16	6	·	5	·	1
V	3.5	4.3	11	5.4	4	3.0	8	5.0	5	4.4	29.5	4.1	13.5	3.7	12.5	8.4	6	4.6	149	37.3	14	·	·	·	·	–	–	·	14	20	17	4	1	·	4
VI	12	7.6	8	6.8	1	3.0	5.5	2.3	3.5	4.4	26.5	5.4	13.5	5.7	17	4.3	3	5.2	61	17.3	16	·	·	·	1	–	–	2	6	14	12	1	·	·	3
VII	5.5	3.8	14	4.0	1	3.0	2	2.5	4.5	3.3	21.5	4.7	13	5.4	29.5	5.4	2	4.6	74	21.6	22	·	·	·	2	–	–	2	9	19	13	1	·	·	4
VIII	·	·	1	2.0	·	·	6	4.0	4.5	3.2	44.5	7.0	22	5.9	12	4.9	3	5.8	92	21.9	7	·	·	·	1	–	–	2	7	18	14	4	·	·	5
IX	1	4.0	1.5	6.3	3.5	3.3	10.5	4.7	8	5.0	26	7.9	22	7.0	12.5	7.5	5	6.3	119	30.4	18	·	·	·	1	–	–	3	12	14	13	3	1	·	1
X	·	·	3	2.7	1	1.0	7.5	4.7	9.5	4.3	35.5	5.5	9	3.9	16.5	5.2	11	4.3	16	3.6	31	·	·	·	·	–	–	1	12	8	5	·	5	·	
XI	·	·	·	·	12	8.6	24.5	6.6	12	3.7	29.5	4.7	4	5.6	2	3.0	6	5.3	38	8.5	20	·	·	6	·	–	–	·	16	12	10	·	5	·	·
XII	2	4.0	7	3.7	12	3.2	13	3.8	8	6.8	40	7.2	1	1.0	4	2.5	6	5.1	19	6.3	1	9	15	23	·	–	–	3	15	10	5	·	·	21	·
Rok	46	4.5	84	5.0	61	3.9	123	4.5	98.5	5.3	375.5	6.1	126	5.5	131	6.6	50	5.7	712	37.3	14.V	18	37	96	5	–	–	22	160	180	121	15	19	87	18

Gołdap $H_s = 150\,m$ $h_w = 15.5\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R (?)
I	3.5	6.8	4	2.8	2	3.0	4	3.5	9.5	3.7	33	4.0	20	4.6	5	2.8	12	3.5	36	5.8	20	3	4	21	·	2	·	2	25	22	16	·	1	24	–
II	6	4.2	3	6.0	9	3.7	3	2.3	14	4.5	9	4.4	14	6.8	8	5.6	18	3.9	43	6.0	17	8	14	27	·	3	1	2	15	16	15	·	3	28	–
III	15.5	3.7	15	2.3	9	2.2	17	3.3	6	3.2	2	5.5	4	3.1	8	3.9	30	2.3	35	8.7	6	12	16	29	·	1	·	2	13	13	6	·	7	31	–
IV	15	4.3	4.5	3.8	9	4.1	9.5	3.2	15.5	4.0	4.5	2.0	12	2.8	16.5	2.6	17	2.6	30	6.5	8	·	·	6	2	·	·	3	11	13	12	·	2	3	–
V	15	4.3	4	1.2	4	3.5	3.5	2.6	7.5	2.1	13	2.3	16	2.6	18.5	3.0	25	1.9	86	41.6	20	·	·	4	·	·	·	·	15	20	15	3	6	·	–
VI	11	4.7	3	4.3	·	·	2.5	3.4	9.5	2.0	12.5	2.4	19.5	3.3	14	2.8	18	2.5	37	14.4	23	·	·	·	1	1	·	·	10	10	9	1	·	·	–
VII	6.5	1.7	2	2.0	·	·	2	2.5	8	2.5	11.5	3.0	27.5	2.9	18.5	2.8	17	2.2	75	15.7	28	·	·	·	2	·	·	1	17	16	14	2	2	·	–
VIII	3.5	2.6	3	2.0	2	1.5	1.5	2.7	11	4.2	21.5	4.2	24	3.2	5.5	2.4	21	2.7	99	22.6	17	·	·	·	1	2	·	1	16	17	16	3	4	·	–
IX	3.5	2.9	1.5	1.7	7.5	1.9	5	2.4	11	3.5	20	4.1	15.5	3.4	7	3.7	19	2.6	130?	36.0?	21	·	·	·	·	·	·	2	13	18	18	5	4	·	–
X	1.5	2.3	1	1.0	1	4.0	3	2.0	6.5	3.4	12.5	3.2	17.5	2.9	14	2.1	36	1.7	20	4.7	28	·	·	8	·	·	·	2	19	11	7	·	13	·	–
XI	1	3.0	6	3.8	15.5	4.2	19.5	4.4	5	3.2	11.5	2.9	7.5	1.7	4	2.8	20	2.8	48	10.6	20	·	1	16	·	·	·	2	24	14	8	1	14	1	–
XII	10	1.8	5	3.0	5.5	1.2	6.5	2.0	14	3.3	17	4.2	15.5	3.3	4.5	2.8	15	2.5	46	2.3	12	12	16	25	·	·	·	1	20	19	7	·	4	16	–
Rok	65	3.3	38.5	2.8	64.5	2.4	77	2.9	117.5	3.3	168	3.5	193	3.4	123.5	3.1	248	2.6	655?	36.0?	21.IX?	35	51	136	6	9	1	18	198	189	143	15	60	103	–

Hopowo $\varphi = 54°16'$ $\lambda = 18°14'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.1	-2.3	6.5	22	-18.8	31	-0.9	0.0	-1.0	-0.7	–	–	–	–	–	–	–	–	–	–	–	–	9.8	8.7	8.1	8.9
II	–	–	–	–	-0.4	-5.5	3.5	12	-17.4	2	-4.4	-1.9	-2.7	-2.9	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.7	8.9	8.8
III	–	–	–	–	0.1	-8.2	6.5	31	-13.8	2	-5.9	-0.9	-3.9	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.3	5.9	6.8
IV	–	–	–	–	11.8	3.4	25.3	21	-0.5	30	5.6	10.3	6.3	7.1	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.0	6.5	6.7
V	–	–	–	–	12.3	4.4	17.3	19	-1.7	2	7.4	11.0	7.2	8.2	–	–	–	–	–	–	–	–	–	–	–	–	7.4	8.3	6.7	7.5
VI	–	–	–	–	17.2	7.6	26.8	16	1.4	3	11.3	15.5	11.2	12.3	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.5	6.1	6.4
VII	–	–	–	–	18.6	9.4	25.8	21	5.9	4	12.8	16.8	12.5	13.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	7.4	6.0	6.5
VIII	–	–	–	–	18.2	10.3	26.1	12	5.5	15	12.6	16.7	12.4	13.5	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.4	7.0	7.1
IX	–	–	–	–	14.8	7.4	25.6	4	3.0	25	9.3	13.9	9.3	10.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.5	5.6	6.9
X	–	–	–	–	11.5	4.1	20.3	3	-2.3	28	6.0	11.0	5.9	7.2	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.8	5.8	6.5
XI	–	–	–	–	3.4	-0.1	10.0	5	-5.1	22	1.2	2.8	1.2	1.6	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.4	8.7	8.7
XII	–	–	–	–	-2.8	-7.4	3.5	5,12	-20.0	22	-5.8	-3.8	-5.6	-5.2	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.5	8.2	8.1
Rok	–	–	–	–	8.8	1.9	26.8	16.VI	-20.0	22.XII	4.1	7.6	4.4	5.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.6	7.0	7.4

Bartoszyce $\varphi = 54°15'$ $\lambda = 20°48'$

I	–	–	–	–	2.0	-2.0	8.0	22	-18.0	31	-0.1	0.9	-0.1	0.2	5.5	5.7	5.4	5.6	86	84	85	85	0.9	1.0	1.0	1.0	8.9	7.8	7.6	8.1
II	–	–	–	–	-0.2	-5.6	4.1	12	-15.8	1	-3.6	-1.5	-2.4	-2.5	4.1	4.7	4.5	4.4	80	83	85	83	0.8	0.9	0.8	0.8	7.9	8.1	7.1	7.7
III	–	–	–	–	0.5	-8.3	7.0	31	-22.3	15	-6.4	-0.6	-3.7	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.3	4.7	6.1
IV	–	–	–	–	13.5	3.7	26.8	23	-0.9	11,30	5.9	11.9	7.5	8.2	8.5	9.4	9.4	9.1	92	67	88	82	1.0	5.9	1.4	2.8	8.2	6.3	4.6	6.4
V	–	–	–	–	14.0	5.2	18.8	13	-2.4	6	8.3	12.4	9.3	9.8	9.9	9.9	10.4	10.0	89	69	88	82	1.2	4.8	1.5	2.5	7.8	8.1	7.9	8.0
VI	–	–	–	–	18.7	7.9	28.2	16	1.0	2	12.5	17.3	12.8	13.8	11.7	11.1	11.9	11.6	78	56	79	71	3.2	9.0	3.3	5.2	5.8	5.9	7.4	6.4
VII	–	–	–	–	19.7	10.1	26.9	21	6.3	7	13.7	18.3	13.9	15.0	14.1	13.6	13.9	13.9	90	65	87	81	1.6	7.8	2.2	3.9	7.1	7.1	7.4	7.2
VIII	–	–	–	–	19.7	10.4	29.9	12	4.1	15	13.6	17.9	14.3	15.0	14.0	14.3	14.5	14.3	90	70	89	83	1.6	6.5	1.9	3.3	7.5	7.3	6.9	7.2
IX	–	–	–	–	15.9	6.7	25.2	4	0.1	27	9.3	14.6	10.4	11.2	11.1	12.2	11.7	11.7	94	73	92	86	0.8	4.8	1.2	2.3	7.1	7.2	5.6	6.6
X	–	–	–	–	12.5	4.0	19.8	1,2	-3.4	28	5.7	11.5	7.3	8.0	8.9	10.5	9.5	9.6	94	76	91	87	0.5	3.4	1.0	1.6	8.0	6.6	5.2	6.6
XI	–	–	–	–	5.5	1.4	13.3	4	-2.6	22	2.4	4.5	3.4	3.4	6.8	7.4	7.1	7.1	92	86	88	89	0.6	1.3	1.0	1.0	8.8	8.3	7.5	8.2
XII	–	–	–	–	-2.4	-7.5	4.7	5	-20.9	23,31	-4.9	-3.5	-5.2	-4.7	4.2	4.4	4.1	4.2	86	82	85	84	0.6	0.8	0.6	0.7	8.1	7.1	7.1	7.4
Rok	–	–	–	–	10.0	2.2	29.9	12.VIII	-20.9	15.III	4.7	8.6	5.6	6.1	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.2	6.6	7.2

Nowy Dwór Gdański $\varphi = 54°13'$ $\lambda = 19°08'$

I	–	–	–	–	2.6	-1.6	8.3	22	-16.5	31	0.5	2.1	0.2	0.8	6.0	6.1	5.8	6.0	90	85	89	88	0.5	1.1	0.6	0.7	8.4	7.2	7.7	7.8
II	–	–	–	–	1.5	-3.9	5.2	11	-14.1	1	-2.0	0.2	-1.4	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.8	7.8	7.8
III	–	–	–	–	1.6	-5.8	7.9	31	-15.2	15	-3.8	0.9	-2.4	-1.9	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.7	5.5	6.1
IV	–	–	–	–	13.5	4.4	27.0	21	0.0	30	6.8	12.6	6.9	8.3	9.1	9.9	9.0	9.3	90	69	89	83	1.1	5.8	1.3	2.7	6.0	6.1	6.7	6.3
V	–	–	–	–	14.5	5.8	20.4	19	-0.9	1	9.4	12.9	8.7	9.9	10.6	11.1	10.1	10.6	89	78	88	85	1.4	4.1	1.3	2.3	6.8	7.5	7.3	7.2
VI	–	–	–	–	19.2	9.1	28.8	16	2.8	2	13.6	17.8	12.7	14.2	12.2	12.5	12.1	12.3	78	61	82	74	3.6	8.6	3.0	5.1	5.3	5.9	6.7	6.0
VII	–	–	–	–	20.4	10.4	28.0	21	7.0	5	15.1	19.1	14.0	15.6	14.6	14.9	14.4	14.6	85	68	89	81	2.7	7.6	1.8	4.0	6.4	6.7	6.9	6.7
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Koszalin $\varphi = 54°12'$ $\lambda = 16°10'$

I	1007.7	1037.6	978.5	1012.0	3.4	-0.8	8.6	22	-18.2	31	0.9	1.9	1.0	1.2	6.1	6.2	6.0	6.1	91	86	87	88	0.6	1.0	0.9	0.8	8.0	8.6	7.8	8.1
II	1010.1	1036.4	969.4	1014.4	1.9	-3.2	6.9	12	-12.7	1	-1.2	0.5	-0.6	-0.5	5.0	5.4	5.0	5.1	86	82	84	84	0.8	1.1	0.9	0.9	8.9	7.8	7.1	7.9
III	1007.0	1023.1	977.5	1011.3	2.4	-4.2	10.5	30	-8.4	15	-2.8	1.2	-1.2	-1.0	4.4	4.8	4.7	4.6	87	71	83	80	0.7	2.0	1.0	1.2	7.7	7.6	6.3	7.2
IV	1008.9	1025.3	983.1	1013.0	12.3	3.2	24.6	22	-0.5	1	5.1	10.3	6.7	7.2	8.0	8.8	8.4	8.4	90	70	85	82	1.0	4.5	1.9	2.5	7.5	6.8	6.3	6.9
V	1007.8	1013.8	1000.4	1011.9	12.6	5.1	19.9	19	-2.1	2	7.9	10.9	8.3	8.8	9.8	9.5	9.6	9.6	90	73	88	84	1.0	3.8	1.5	2.1	7.7	8.4	7.5	7.9
VI	1013.5	1029.4	999.3	1017.6	17.0	7.9	27.8	19	2.0	3	12.2	15.4	11.6	12.7	11.7	12.2	11.7	11.9	81	70	84	78	2.7	6.0	2.3	3.7	6.4	6.9	6.2	6.5
VII	1009.2	1020.1	988.8	1013.3	18.5	9.3	25.9	21	5.8	5	13.2	17.2	13.0	14.1	13.7	14.0	13.7	13.8	90	72	91	84	1.6	6.0	1.4	3.0	6.3	6.9	5.9	6.4
VIII	1008.9	1018.1	997.0	1013.0	18.5	11.0	27.7	12	5.8	15	13.4	17.1	13.5	14.4	13.8	14.2	14.2	14.1	89	73	91	84	1.7	5.5	1.5	2.9	7.9	7.8	6.5	7.4
IX	1010.1	1025.3	986.8	1014.2	16.2	8.2	25.6	4	3.9	25	10.4	15.1	10.9	11.8	11.4	12.1	11.6	11.7	90	71	88	83	1.3	5.4	1.6	2.8	6.9	6.8	4.9	6.2
X	1016.7	1032.4	1002.9	1020.5	12.9	5.0	22.1	2	-0.7	15	6.7	12.0	8.2	8.8	9.5	10.8	10.1	10.1	95	76	91	87	0.6	3.7	1.1	1.8	7.4	7.0	5.9	6.8
XI	1012.1	1028.1	992.9	1016.3	5.6	1.5	15.3	8	-3.1	25	2.7	4.9	3.1	3.4	7.0	7.4	7.1	7.2	92	85	91	89	0.6	1.6	0.8	1.0	8.2	7.9	7.6	7.9
XII	1011.4	1045.7	966.7	1015.8	-0.7	-5.9	5.5	12	-16.5	22.	-4.1	-2.2	-3.7	-3.4	4.4	4.8	4.5	4.6	91	87	91	90	0.4	0.6	0.4	0.5	7.2	8.0	5.6	6.9
Rok	1010.3	1045.7	966.7	1014.5	10.0	3.1	27.8	19.VI	-18.2	31.I	5.4	8.7	5.9	6.5	8.7	9.2	8.9	8.9	89	76	88	84	1.1	3.4	1.3	1.9	7.5	7.5	6.5	7.2

Hopowo $H_s = 220 m$ $h_w = 12 m$ 1962

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v>10	v>15	◷	●	Opad R ≥0.1	R ≥1.0	R ≥10.0	≡	⊠	R
I	0.5	3.0	2	5.5	2	5.5	1	3.0	11.5	7.5	44	6.6	12.5	7.0	9.5	6.0	10	5.9	29	8.1	28	2	6	23	·	6	2	·	26	22	7	·	–	19	·
II	4.5	7.9	10	5.8	3.5	3.7	2.5	3.4	40	6.6	25	7.7	5	8.7	15.5	10.2	8	6.8	48	13.2	12	4	12	27	·	7	4	·	23	21	11	1	–	28	·
III	7	6.0	8	4.6	1	4.0	7	4.1	11.5	4.7	13	4.3	4.5	4.6	8	7.2	33	3.2	28	11.8	6	12	16	30	·	2	·	3	12	11	6	1	16	31	·
IV	4	5.8	7	4.6	1.5	3.7	3	3.7	11.5	5.3	28	4.7	5.5	3.9	12.5	4.9	17	3.8	18	2.6	28	·	·	5	1	2	·	1	12	12	7	·	12	6	·
V	1.5	3.6	5.5	3.4	·	·	2.5	3.4	40	4.4	27	4.0	9.5	3.4	12	4.7	25	2.9	70	13.6	17	·	·	4	·	·	·	·	12	21	15	2	14	·	6
VI	8	6.0	3	5.3	0.5	3.0	1	5.0	5.5	5.0	23.5	4.7	16.5	3.9	16	5.0	16	3.9	41	11.2	16	·	·	·	2	2	·	2	6	15	10	1	3	·	5
VII	4.5	2.6	4.5	1.9	1.5	2.3	1.5	3.0	8.5	4.8	26	3.6	13.5	3.2	13	3.9	20	2.8	86	32.2	22	·	·	·	1	·	·	1	9	19	14	1	5	·	4
VIII	0.5	5.0	·	·	0.5	3.0	4	2.5	6.5	5.8	34	5.7	19.5	4.8	9	4.2	19	4.1	99	26.3	7	·	·	·	1	4	1	1	10	20	15	2	4	·	4
IX	·	·	1	3.0	0.5	3.0	1.5	5.0	9.5	5.9	26	6.0	10	5.3	9.5	5.4	32	3.6	75	19.1	12	·	·	·	1	2	·	·	11	16	13	2	6	·	4
X	0.5	3.0	0.5	3.0	·	·	0.5	3.0	18.5	5.4	22.5	4.4	11	4.3	6.5	4.1	33	3.0	19	8.3	31	·	·	4	·	2	·	4	14	10	5	·	10	·	
XI	3	2.7	3.5	3.4	7	3.8	12.5	3.1	15.5	3.7	22.5	4.0	6.5	2.9	3.5	3.7	16	2.9	47	16.3	1	·	6	15	·	·	·	1	21	9	6	2	9	6	·
XII	1.5	1.7	6	2.8	1	3.5	2	3.0	8.5	5.9	29.5	6.2	9	4.9	4.5	3.0	31	3.4	15	3.1	10	10	19	29	·	3	·	2	20	13	8	·	9	14	·
Rok	35.5	3.9	51	3.6	19	3.0	39	3.5	127	5.4	321	5.2	123	4.7	119.5	5.2	260	3.9	575	32.2	22 VII	28	59	137	6	30	7	15	176	189	117	12	–	104	23

Bartoszyce $H_s = 60 m$ $h_w = 13 m$ I–VII, $11 m$ VIII–XII

I	3.5	4.7	4.5	2.3	2	3.0	0.5	3.0	14	2.6	41	3.1	18	2.9	4.5	2.0	5	2.9	20	4.5	20	3	3	18			·	1	19	23	4	·		8	–
II	6.5	3.8	5.5	2.6	10	2.2	4.5	2.1	5	2.9	22.5	3.6	12.5	3.6	8.5	5.8	9	3.1	24	4.3	12	5	13	26	·	·	·	·	16	20	8	·	·	22	–
III	10.5	3.7	2	1.5	10.5	1.6	11.5	1.9	6.5	2.0	4.5	2.0	5	2.7	15.5	2.9	27	1.7	32	7.3	12	11	13	31	·		·	2	11	13	8	·	2	31	–
IV	7.5	2.1	7	3.3	7.5	2.5	8	2.1	8.5	2.9	13	3.0	6.5	2.8	17	2.9	15	2.3	19	3.4	27	·	·	5	2	·	·	1	9	15	7	·	2	·	–
V	6.5	1.8	9	2.3	3.5	2.4	12	2.1	4	2.4	12.5	3.3	17	2.5	17.5	2.3	11	2.2	88	15.4	14	·	·	2	·	·	·	·	17	26	13	3	2	·	–
VI	11	3.4	1.5	4.7	0.5	1.0	4.5	2.3	4	3.1	18	3.6	19.5	3.2	19	2.6	15	2.6	23	5.8	29	·	·	·	1	·	·	·	9	13	8	·	·	·	–
VII	7.5	2.0	1	3.0	·	·	1.5	4.0	4	2.1	10.5	2.8	28	2.4	25.5	2.3	15	1.9	79	20.6	27	·	·	·	3	·	·	·	10	15	13	3	·	·	–
VIII	4	2.0	1	2.0	1	1.0	1.5	2.0	8.5	2.9	29.5	3.3	18.5	2.5	11	1.7	18	2.2	130	42.0	7	·		·	1	·	·	·	15	19	14	3	·	·	–
IX	4	2.4	4	1.0	3	2.0	3	2.0	8.5	2.9	23	2.8	14.5	2.8	8	2.6	22	2.0	79	22.4	18	·	·	·	1	·	·	2	12	16	14	2	3	·	–
X	3.5	2.1	1.5	4.0	2	1.0	6.5	1.9	7.5	2.3	24.5	2.3	13	2.8	5.5	2.4	29	1.6	11	4.0	28	·	·	6	·	·	·	2	11	12	3	·	8	·	–
XI	3	1.8	8.5	2.9	19.5	2.9	13	2.9	9	2.0	20.5	2.3	6.5	2.8	6	1.4	4	2.4	24	5.4	20	·	1	9		·	·	1	18	13	7	·	·	·	–
XII	4	1.5	16	1.5	4.5	1.4	9	1.6	13.5	3.0	20.5	3.6	10	2.4	3.5	2.0	12	2.1	17	4.0	13	11	15	25		·	·	3	18	12	8	·	2	14	–
Rok	71.5	2.6	61.5	2.1	64	1.8	72.5	2.1	93	2.6	240	3.0	169	2.8	141.5	2.6	182	2.2	546	42.0	7.VIII	30	45	122	8	·	·	12	165	197	107	11	19	75	–

Nowy Dwór Gdański $H_s = 0 m$ $h_w = 13 m$

I	2.5	3.0	9.5	2.6	4	2.5	14	2.6	10.5	2.7	31	3.0	10.5	2.3	11	3.3	·	2.8	32	6.1	27	3	3	16	·	·	·	2	18	17	11	·	·	–	
II	6.5	5.5	15	4.2	6.5	4.5	9	2.3	8	4.9	14.5	4.7	8.5	5.0	15	4.5	1	4.3	42	9.3	12	1	9	23	·	4	·	1	18	19	9	·	2	–	·
III	13.5	5.3	12	3.0	13	2.2	20	2.3	8	1.7	4	1.1	7.5	2.1	5	5.5	10	2.6	46	11.2	12	5	7	30	·	1	·	4	8	10	8	1	3	–	·
IV	15.5	3.1	14	2.0	9	2.3	14	2.6	9.5	3.2	5	1.4	3	2.7	14	2.8	6	2.4	24	7.3	5	·	·	·	1	·	·	2	10	14	5	·	5	·	1
V	9.5	3.4	17.5	2.8	8.5	2.1	5.5	2.6	9	1.6	9.5	2.1	10	2.1	12.5	2.0	11	2.1	128	42.8	14	·	·	2	·	1	·	1	12	19	16	3	·	·	4
VI	13	4.3	11.5	1.4	1	1.0	2	1.5	7	1.7	3	1.8	24.5	2.1	26	1.7	2	2.1	67	19.8	16	·	·	·	4	·	·	2	6	13	11	2	·	·	5
VII	16.5	1.7	9	3.0	2	2.5	4	2.2	8.5	2.1	13.5	2.0	11	1.7	17.5	2.1	11	1.7	72	10.1	29	·	·	·	3	·	·	1	9	21	17	1	·	·	5
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Koszalin $H_s = 33 m$ $H_b = 33,9 m$ $h_w = 13,5 m$

I	2	6.5	4	4.4	3.5	1.3	7	4.3	23.5	7.2	33.5	7.4	9	8.4	9.5	4.8	1	6.4	56	8.9	25	2	3	12	·	14	4	2	22	28	14		2	4	
II	9	7.4	14.5	4.3	5.5	4.0	2	5.5	14.5	6.2	15.5	7.2	15	8.2	8	6.8	·	6.5	31	10.4	12	2	8	24	·	8	4	1	16	13	8	1	3	10	·
III	13	4.5	12.5	3.4	4.5	1.9	28.5	4.2	11.5	3.0	4	4.2	7.5	4.4	5.5	3.3	6	3.6	20	3.5	12	·	6	28	·	3	·	1	15	15	8	·	6	13	·
IV	12	3.2	11	5.5	6	1.9	11.5	3.3	11.5	5.1	12	5.0	14	3.7	11	3.5	1	4.0	32	5.6	16	·	·	2	·	1	·	2	13	14	11	·	8	·	1
V	15	3.3	2.5	3.0	3	2.3	12	4.2	12.5	4.2	9	5.0	16.5	4.0	17.5	3.3	5	3.6	112	12.2	13	·	·	4	·	·	·	·	16	21	19	2	6	·	6
VI	12.5	4.6	5.5	3.8	·	·	6	2.5	3.5	4.4	17	4.9	26	5.1	13.5	4.3	6	4.3	48	10.8	27	·	·	·	3	2	·	1	7	12	10	1	·	·	2
VII	12.5	3.3	3	3.0	4.5	2.3	4	2.8	8	3.8	22.5	4.4	14.5	3.4	17	2.9	7	3.2	78	15.2	7	·	·	·	1	1	1	2	10	15	14	2	7	·	6
VIII	4	2.1	2	1.5	2.5	4.2	9.5	3.2	14.5	4.3	29	5.6	22	4.9	6.5	3.6	3	4.4	121	23.5	18	·	·	·	1	6	1	1	15	21	15	4	4	·	3
IX	4	1.8	0.5	1.0	7	2.0	14	3.8	11.5	3.4	23	5.1	14	6.5	12	4.0	4	4.1	56	11.6	7	·	·	·	1	4	1	4	10	15	11	1	2	·	4
X	3.5	2.7	2.5	2.2	0.5	4.0	20.5	3.0	24.5	3.7	15.5	3.5	11	5.0	8	3.0	7	3.2	29	13.6	4	·	·	2	·	2	·	5	15	10	4	1	9	·	1
XI	4	3.1	6.5	4.5	15.5	3.2	22	4.0	17	3.7	14	4.8	8	5.6	1	1.0	2	4.0	40	8.2	12	·	·	11	·	1	·	1	19	12	10	·	9	7	·
XII	3	4.3	7.5	1.5	8.5	2.6	16.5	2.6	19	5.2	25	4.8	4.5	3.9	2	3.2	7	3.6	31	7.4	11	7	17	26	·	3	·	3	15	13	7	·	8	15	·
Rok	94.5	3.9	72	3.2	61	2.2	153.5	3.6	171.5	4.5	220	5.1	162	5.3	111.5	3.6	49	4.2	654	23.5	18 VIII	11	34	109	6	45	11	23	173	189	131	12	64	49	23

Kołobrzeg-Wydma $\varphi = 54°11'$ $\lambda = 15°33'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	P_{0m}	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.4	0.0	8.6	22	-14.3	31	1.4	2.3	1.7	1.8	–	–	–				–			–		–	8.5	8.7	8.5	8.6
II	–	–	–	–	4.9	-2.3	6.6	12	-12.6	1	-0.5	0.8	0.0	0.1	–		–		–	–		–		–	–	–	8.4	8.0	6.8	7.7
III	–	–	–	–	2.7	-2.5	12.5	30	-6.5	16	-1.3	1.9	-0.1	0.1			–	–				–		–	–	–	8.0	7.5	6.9	7.5
IV	–	–	–	–	9.7	3.4	20.7	18	0.9	2,11	5.1	7.3	6.0	6.1					–					–	–		8.2	7.2	7.2	7.5
V	–	–	–	–	12.0	6.2	20.9	19	0.1	3	8.6	10.4	8.7	9.1			–		–	–			–	–	–	–	7.9	7.9	8.2	8.0
VI	–	–	–	–	16.7	10.6	28.5	19	4.8	1,8	13.0	14.8	13.2	13.6		–		–	–	–	–	–	–	–	–	–	6.8	7.0	6.7	6.8
VII	–	–	–	–	17.6	11.0	26.5	21	7.1	5	14.1	16.3	14.1	14.6	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.7	6.4	6.8
VIII	–	–	–	–	18.4	12.6	28.0	12	9.0	10	14.4	17.1	14.7	15.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.7	7.5	7.7
IX	–	–	–	–	16.1	9.5	24.3	4	5.2	25	11.2	15.1	12.2	12.7	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.1	5.8	6.8
X	–	–	–	–	13.0	6.2	23.4	3	0.6	28	7.7	12.1	9.2	9.6	–	–	–	–	–	–	–	–	–		–	–	7.7	7.1	6.4	7.1
XI	–	–	–	–	5.7	2.0	13.6	8	-3.1	24	3.1	5.0	3.5	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.5	8.5	8.4
XII	–	–	–	–	0.0	-4.6	5.5	12	-15.5	22	-3.0	1.5	-2.4	-2.3	–	–	–	–	–	–	–	–	–	–		–	8.1	8.0	6.8	7.6
Rok	–	–	–	–	9.8	4.3	28.5	19.VI	-15.5	22.XII	6.2	8.5	6.7	7.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.6	7.1	7.5

Kołobrzeg $\varphi = 54°11'$ $\lambda = 15°35'$

I	1011.2	1041.9	981.1	1011.9	3.7	-0.2	8.5	22	-15.7	31	1.4	2.5	1.6	1.8	6.0	6.2	6.0	6.1	87	83	86	85	0.9	1.3	1.0	1.1	8.4	8.6	8.5	8.5
II	1014.0	1040.2	973.6	1014.7	2.4	-2.3	7.5	8	-12.8	1	-0.6	1.1	0.0	0.1	5.0	5.4	5.1	5.2	83	79	81	81	1.0	1.4	1.2	1.2	8.3	8.0	7.1	7.8
III	1010.7	1027.2	980.6	1011.4	3.1	-3.0	12.7	30	-6.5	2,16	-1.6	1.9	-0.3	-0.1	4.6	4.9	4.9	4.8	83	7.0	8.0	7.8	0.9	2.2	1.2	1.4	7.9	7.4	6.7	7.3
IV	1012.6	1029.7	986.4	1013.2	10.2	3.2	20.8	25	0.6	14	5.1	8.1	5.9	6.2	7.8	8.1	7.9	7.9	88	75	84	82	1.2	3.1	1.6	2.0	8.1	7.2	7.1	7.5
V	1011.4	1017.4	1004.7	1012.0	12.2	5.7	20.1	19	-0.5	5	8.5	10.6	8.7	9.1	9.7	9.6	9.5	9.6	86	76	84	82	1.5	3.4	1.9	2.3	7.8	8.2	8.1	8.0
VI	1017.3	1034.3	1002.8	1017.9	16.9	9.7	28.1	19	3.1	8	13.0	15.1	12.9	13.5	11.9	12.3	12.2	12.1	78	71	80	76	3.3	5.5	3.0	3.9	6.6	7.2	6.6	6.8
VII	1012.8	1023.5	991.4	1013.4	17.7	10.4	26.4	21	7.2	5	14.0	16.6	13.9	14.6	14.1	14.4	14.3	14.3	88	76	90	85	2.0	4.8	1.7	2.8	7.3	6.8	6.2	6.8
VIII	1012.4	1021.9	1000.5	1013.0	18.6	11.8	28.2	12	6.6	15	14.1	17.3	14.4	15.0	13.8	14.6	14.3	14.2	86	74	87	82	2.3	5.4	2.2	3.3	7.8	7.8	7.5	7.7
IX	1013.7	1028.8	99.0.0	1014.3	16.3	9.0	24.7	4	3.0	25	11.0	15.3	11.6	12.4	11.7	12.6	11.7	12.0	88	73	85	82	1.6	5.0	2.1	2.9	7.3	7.3	5.8	6.8
X	1020.4	1036.2	1005.9	1021.0	13.2	5.2	23.1	3	-1.5	28	7.2	12.2	8.6	9.2	9.6	11.2	10.2	10.3	93	77	89	86	0.8	3.6	1.3	1.9	7.6	7.1	6.4	7.0
XI	1015.6	1032.2	996.5	1016.3	5.8	1.7	14.4	8	-3.2	24	3.0	5.1	3.3	3.7	7.1	7.6	7.2	7.3	92	85	91	89	0.6	1.5	0.8	1.0	8.2	8.7	8.6	8.5
XII	1015.0	1050.3	969.3	1015.7	-0.1	-5.0	5.7	5	-15.9	22	-3.2	-1.5	-2.6	-2.5	4.6	5.0	4.8	4.8	89	86	89	88	0.5	0.8	0.5	0.6	8.1	8.0	6.8	7.6
Rok	1013.9	1050.3	969.3	1014.6	10.0	3.8	28.2	12.VIII	-15.9	22.XII	6.0	8.7	6.5	6.9	8.8	9.3	9.0	9.0	87	77	86	83	1.4	3.2	1.5	2.0	7.8	7.7	7.1	7.5

Kmiecin $\varphi = 54°11'$ $\lambda = 19°10$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	20.0	10.1	26.9	21	6.3	5	14.2	18.2	13.8	15.0	14.6	13.2	13.7	13.8	89	64	86	80	1.8	8.1	2.3	4.1	5.9	6.4	6.5	6.3
VIII	–	–	–	–	19.6	11.0	26.9	12	5.9	15	14.0	18.3	14.1	15.1	–	–	–	–		–	–				–	–	7.2	7.2	6.5	7.0
IX	–	–	–	–	16.5	8.1	25.9	4	3.3	15	10.1	15.5	10.8	11.8	11.6	12.9	11.9	12.1	93	73	91	86	0.9	5.0	1.2	2.4	7.5	7.0	7.2	7.2
X	–	–	–	–	12.4	4.8	20.8	3	-3.3	28	6.6	11.8	7.9	8.6	9.3	10.6	9.7	9.9	9.3	76	89	86	0.8	3.6	1.3	1.9	8.2	7.6	7.5	7.8
XI	–	–	–	–	5.2	1.3	12.5	4	-5.2	25	2.5	4.6	3.3	3.4	6.9	7.3	7.1	7.1	92	85	90	89	0.6	1.4	0.8	0.9	8.5	8.5	7.9	8.3
XII	–	–	–	–	-1.8	-7.3	4.7	12	-18.5	23,31	-4.4	-3.3	-4.7	-4.3	4.3	4.4	4.2	4.3	89	85	88	87	0.5	0.7	0.5	0.6	8.0	7.0	7.7	7.6
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Żelisławki $\varphi = 54°10$ $\lambda = 18°39'$

I	–	–	–	–	2.1	-1.8	7.7	22	-16.5	31	0.3	1.1	0.0	0.4			–	–		–	–	–	–	–	–	–	9.3	8.1	8.7	8.7
II	–	–	–	–	0.6	-4.4	4.4	20	-17.0	1	-2.8	-0.8	-1.6	-1.7	–		–	–	–	–	–	–		–	–	–	8.3	7.9	7.4	7.9
III	–	–	–	–	0.9	-6.5	7.7	31	-13.7	15	-4.6	-0.1	-2.8	-2.6			–	–	–	–	–		–	–	–	–	5.9	5.9	5.1	5.6
IV	–	–	–	–	12.8	3.8	27.1	21	-0.8	30	6.0	11.2	6.8	7.7	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.7	6.2	6.2
V	–	–	–	–	13.9	5.3	19.4	23	-2.5	1	8.5	12.3	8.1	9.2	–	–	–	–	–	–	–	–		–	–	–	7.1	8.3	7.4	7.6
VI	–	–	–	–	18.8	8.5	28.5	16	2.2	3	12.8	17.2	11.9	13.4	–	–	–	–	–	–	–	–	–	–	–	–	4.1	6.2	6.3	5.5
VII	–	–	–	–	20.0	10.3	27.5	21	6.7	4	13.9	18.3	13.5	14.8	–	–	–	–	–	–	–	–	–	–	–	–	4.8	6.2	6.3	5.8
VIII	–	–	–	–	19.9	11.2	27.7	12	5.8	31	13.7	18.4	14.1	15.1	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.7	5.5	5.9
IX	–	–	–	–	16.6	7.7	26.5	4	2.9	16	9.9	15.5	10.8	11.8	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.8	4.7	5.7
X	–	–	–	–	12.7	4.5	20.5	2	-2.1	28	6.3	11.8	7.7	8.4	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.5	6.2	5.9
XI	–	–	–	–	4.9	0.8	10.9	4	-4.1	24	2.1	3.8	2.8	2.9	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.1	8.0	8.0
XII	–	–	–	–	-1.6	-7.2	5.5	5,7	-20.5	21	-4.4	-3.2	-4.6	-4.2	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.0	6.3	6.7
Rok	–	–	–	–	10.1	2.7	28.5	16.VI	-20.5	21.XII	5.1	8.8	5.6	6.3	–	–	–	–		–	–	–	–	–	–	–	6.5	7.0	6.4	6.6

Kołobrzeg-Wydma $H_s = 5\,m$ $h_w = 11\,m$ 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	◐	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R 10
I	3.5	4.2	3	6.3	2.5	2.4	10	4.6	31	6.9	31.5	7.2	4.5	6.6	7	6.1	·	6.8	42	8.0	25	1	2	11	·	–	–	1	26	22	12	·	–	7	–
II	9	11.1	13	9.2	5.5	5.9	3.5	4.3	18	6.0	17	7.7	11.5	9.0	6.5	12	·	8.1	38	11.8	12	2	6	19	·	–	–	1	16	14	7	1	–	12	–
III	9.5	5.2	14.5	7.0	4.5	3.7	23.5	3.7	18.5	3.1	6	4.3	8.5	4.8	8	5.6	·	4.5	29	7.9	27	·	5	27	·	–	–	·	14	11	9		–	14	–
IV	7	6.8	20	6.3	4	3.4	8	3.5	12	4.2	18	5.3	13	3.9	8	5.1	·	5.0	52	22.6	16	·	·	·	·	–	–	1	13	13	10	1	–	·	–
V	14.5	5.5	8	3.4	2.5	2.2	7.5	2.9	15.5	3.3	16.5	3.9	20.5	4.0	7	5.1	1	4.0	103	16.1	9	·	·	·	·	–	–	·	19	21	18	3	–	·	–
VI	11	6.7	5.5	4.8	1.5	1.3	5	3.4	5	1.9	13	5.7	38	5.7	9	4.9	2	5.2	49	16.5	27	·	·	·	2	–	–	1	9	12	10	2	–	·	–
VII	6.5	3.6	11.5	4.3	3.5	1.4	6.5	2.9	8	4.4	17.5	5.0	23	4.5	16.5	3.7	·	4.1	93	15.0	12	·	·	·	1	–	–	·	12	16	13	5	–	·	–
VIII	5.5	3.8	2	1.5	3	3.3	6.5	1.8	19.5	4.4	28.5	6.3	15	5.7	10	4.0	3	4.7	121	38.8	7	·	·	·	1	–	–	·	16	20	14	4	–	·	–
IX	2	3.2	6	2.9	13.5	3.6	8	2.2	15.5	3.9	12	6.0	24	6.9	7	6.5	2	4.8	46	11.5	8	·	·	·	·	–	–	1	9	12	8	2	–	·	–
X	5	3.6	6.5	3.2	3	2.3	16	2.2	27	3.6	17	3.8	8	5.4	5.5	5.1	5	3.4	17	8.9	4	·	·	·	·	–	–	2	15	8	3	·	–	·	–
XI	1.5	5.0	9	7.3	24	4.9	7	3.3	23	3.6	16	5.2	3.5	4.7	1	9.0	5	4.5	24	4.5	22	·	·	9	·	–	–	·	20	13	7	·	–	6	–
XII	2	6.0	5	1.9	16.5	3.4	10	2.6	24	4.1	27	5.4	1.5	0.7	4	4.5	3	4.1	30	6.8	11	7	15	24	·	–	–	2	18	12	9	·	–	15	–
Rok	77	5.1	104	4.8	84	3.2	111.5	3.1	217	4.1	220	5.5	171	5.2	89.5	5.1	21	4.9	644	38.8	7.VIII	10	28	90	4	–	–	9	187	174	120	18	–	54	–

Kołobrzeg $H_s = 3\,m$ $H_b = 5{,}4\,m$ $h_w = 22\,m$ anemometr, $17\,m$ wiatromierz Wilda

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	◐	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R 10
I	4.5	9.0	2	5.8	4	3.4	9	3.9	24.5	6.0	36.5	6.8	9.5	6.4	3	4.7	·	6.2	44	8.0	25	2	2	11	·	7	·	1	25	26	15	·	3	7	·
II	7.5	8.1	13	7.5	7.5	5.5	3.5	4.3	14.5	5.3	18	7.1	13.5	7.9	6.5	7.6	·	6.9	42	13.0	12	2	5	21	·	10	·	1	16	15	8	1	4	12	
III	14	4.7	12.5	5.4	5	3.4	27.5	3.7	10.5	2.8	7.5	3.1	9	4.2	6	3.9	1	4.0	36	6.5	27	·	3	27	·	5	·	·	12	15	9		5	14	
IV	11.5	4.2	20	5.0	3.5	3.6	8.5	3.0	10.5	4.3	18.5	4.9	13	4.0	4.5	3.0	·	4.3	42	11.3	16	·	·	·	·	2	·	1	13	13	10	1	8	·	2
V	16	3.7	8.5	3.4	2.5	2.0	9.5	3.1	10	2.6	24	3.4	16.5	4.1	5	5.0	1	3.5	105	15.2	9	·	·	2	·	1	·	·	18	23	20	2	7	·	3
VI	15	4.3	5.5	4.0	1.5	1.3	4	3.5	5.5	1.8	15	5.4	34	4.8	8.5	3.6	1	4.3	54	18.6	27	·	·	·	2	2	·	1	10	13	10	2	2		3
VII	7	3.1	13	3.5	5	2.7	5.5	2.3	4	3.1	24	3.4	24	3.7	10.5	3.2	·	3.3	85	13.3	12	·	·	·	1	1	·	1	10	17	12	4	2	·	5
VIII	5	3.1	1.5	2.0	6.5	2.5	4	2.0	13.5	3.6	36	4.9	15	5.5	8.5	3.9	3	4.1	109	30.3	7	·	·	·	1	2	·	·	16	22	16	2	2	·	3
IX	2	2.5	5	2.2	13.5	3.5	8	2.4	11.5	3.0	21	5.0	21	6.0	6	4.5	2	4.2	40	9.9	8	·	·	·	·	3	·	·	9	13	8	·	1	·	3
X	4.5	3.6	7	2.9	4.5	1.3	16	1.9	26	3.4	19	2.8	10.5	5.2	4.5	2.8	1	3.0	18	9.6	4	·	·	3	·	·	·	3	15	9	3	·	10	·	1
XI	1	4.0	12	5.4	23	4.5	6.5	3.7	21	3.2	20	4.0	3.5	5.6	·	·	3	4.0	29	7.4	30	·	·	9	·	1	·	·	20	13	7	·	7	6	·
XII	3.5	3.7	7	2.2	16.5	2.4	9	1.8	21.5	4.3	26	4.7	4	7.0	2.5	2.8	3	3.6	29	6.4	11	7	15	24	·	2	·	2	18	13	10	·	9	15	·
Rok	91.5	4.5	107	4.1	93	3.0	111	3.0	173	3.6	265.5	4.6	173.5	5.4	65.5	3.8	15	4.3	633	30.3	7.VIII	11	25	97	4	36	·	10	182	192	128	12	60	54	20

UWAGA. Kierunki wiatru – wg wiatromierza Wilda, prędkości – wg anemometru.

Kmiecin $H_s = 0\,m$ $h_w = 8\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	◐	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R 10
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	15	3.1	7.5	2.5	1.5	3.7	1.5	3.0	12.5	3.7	11.5	2.2	17	2.7	12.5	3.6	14	2.6	90	16.4	22	·	·	·	2	1	·	2	10	21	17	3	2	·	3
VIII	6	2.5	4	2.5	3.5	3.4	7	2.7	7	3.7	25.5	4.0	22	4.0	9	3.4	9	3.3	70.2	16.3	7	·	·	·	1	1	·	1	13	17	13	1	5	·	1
IX	7	2.6	1	2.0	8.5	2.4	9	2.9	10.5	4.4	17	4.3	21.5	3.9	11.5	3.6	4	3.5	60	13.6	18	·	·	·	1	2	·	1	16	16	12	2	8	·	·
X	7.5	3.6	0.5	4.0	·		7.5	3.4	25	3.6	16	3.3	19	3.7	8.5	3.1	9	3.1	16	5.6	5	·	·	4	·	2	·	·	16	12	4	·	7	·	·
XI	1.5	2.0	4.5	5.6	17.5	4.5	14.5	5.0	24	3.5	11.5	3.7	8.5	3.4	1	3.5	7	3.8	39	8.3	30	·	·	11	·	·	·	1	20	16	8	·	4	·	·
XII	1	2.0	18.5	2.3	4	3.5	3	2.3	21	5.1	20.5	4.0	9	3.3	2	5.0	14	3.2	21	8.4	1	11	16	26	·	·	·	2	18	11	5	·	1	18	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Żelisławki $H_s = 68\,m$ $h_w = 12\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	◐	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R 10
I	2	3.0	1.5	3.0	5.5	1.5	1.5	3.0	16.5	4.5	36.5	6.0	17.5	7.3	9	5.5	3	5.3	24	10.0	28	3	3	16	·	8	1	·	23	10	5	1	1	9	–
II	5.5	9.0	6	4.3	11	4.5			13	4.3	16.5	7.2	10.5	8.8	12.5	10.0	9	6.1	29	9.8	12	3	10	24	·	11	4	·	17	10	7	·	1	25	–
III	11.5	5.0	8.5	3.9	3	3.7	10.5	3.7	11	3.4	10	2.8	16.5	4.7	4	7.2	18	3.4	43	15.3	12	4	11	31	·	4	·	7	10	9	8	2	5	28	–
IV	12	3.4	4.5	2.9	2	2.5	4.5	3.7	9	4.1	20	3.4	6	5.8	13	5.3	19	3.2	32	12.9	5	·	·	3	2	1	·	2	10	10	8	1	4		–
V	13.5	3.4	7.5	2.3	1	2.0	4	2.5	7	3.8	17	3.5	14	2.6	9	5.3	20	2.6	98	31.2	14	·	·	4	·	1	·	1	17	12	10	4	2	·	–
VI	13	3.9	4.5	3.4	2.5	3.0	3.5	3.0	2	3.3	7.5	4.7	31.5	5.7	12.5	4.0	13	4.0	61	21.3	16	·	·	·	4	2	1	4	5	10	9	1	·	·	–
VII	5.5	2.0	5	1.6	1.5	2.3	1.5	1.0	6.5	2.2	10.5	2.2	19	4.1	12.5	3.9	31	2.0	52	15.4	22	·	·		2	·	·	3	6	20	13	1	·	·	–
VIII	4.5	2.7	4	1.1	3	2.7	2.5	2.2	4	3.4	22	4.6	31.5	5.5	11.5	3.8	10	3.9	61	21.4	7	·	·		1	4	·	2	9	15	11	2	1	·	–
IX	4	1.9	1	1.0	4.5	1.6	8.5	1.3	9.5	2.8	19.5	4.2	21	6.9	11	4.3	11	3.6	71	41.6	18	·	·	·	1	3	1	4	7	10	9	1	5	·	–
X	2	2.5	·		0.5	2.0	5.5	3.5	13.5	2.3	21	3.1	23	5.3	11.5	3.5	16	3.1	8	4.3	31	·	·	5	·	2	·	4	11	5	2	·	5	·	–
XI	4.5	1.7	2.5	3.4	11	3.5	13.5	2.9	14	2.9	19	3.7	8	3.6	0.5	1.0	17	2.6	49	13.4	1.		·	15		1		2	19	11	10	1	4	·	–
XII	2.5	1.0	2.5	1.0	4.5	1.4	2.5	2.8	12.5	3.1	24.5	5.4	10.5	5.2	7.5	4.7	26	3.0	17	6.0	17	11	15	26	·	5	·	4	15	7	6		·	23	–
Rok	80.5	3.3	47.5	2.3	50	2.6	58	2.5	118.5	3.3	224	4.2	209	5.5	114.5	4.9	193	3.6	545	41.6	18 IX	21	39	124	10	42	7	33	149	129	98	14	28	85	–

Elbląg $\varphi = 54°10'$ $\lambda = 19°26'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1007.0	1037.0	979.1	1012.5	2.0	-2.0	7.5	22	-18.3	31	-0.1	1.2	-0.1	0.2	5.5	5.6	5.3	5.5	88	81	84	84	0.8	1.3	1.0	1.0	9.2	8.0	8.5	8.6
II	1008.2	1033.2	967.2	1013.7	0.4	-4.6	4.2	20	-14.7	1	-2.8	-0.8	-1.7	-1.8	4.4	4.7	4.6	4.6	85	80	83	83	0.7	1.2	0.9	0.9	8.4	8.4	7.9	8.2
III	1006.1	1023.3	979.1	1011.6	0.8	-5.5	8.0	31	-12.9	15	-4.0	-0.1	-2.0	-2.0	3.8	4.5	4.2	4.2	81	74	78	78	0.8	1.6	1.1	1.2	7.4	7.5	6.2	7.0
IV	1008.1	1024.0	982.5	1013.4	13.4	5.1	27.0	21	-0.3	2	6.7	12.0	7.8	8.6	8.3	8.8	8.4	8.5	83	77	78	79	1.8	6.7	2.7	3.7	7.9	7.5	6.3	7.2
V	1006.3	1014.4	988.0	1011.6	13.7	6.1	18.4	19	-1.4	1	8.7	12.2	9.2	9.8	9.7	9.9	9.7	9.8	85	70	83	80	1.7	4.6	2.1	2.8	8.1	8.5	7.5	8.0
VI	1011.5	1025.7	998.4	1016.7	18.0	9.1	28.0	16	3.7	3	12.5	16.2	13.0	13.7	11.7	11.2	11.8	11.6	79	60	78	72	3.0	8.0	3.7	4.9	7.3	6.9	7.6	7.3
VII	1007.9	1017.8	992.0	1013.1	19.3	10.6	27.0	21,26	7.2	4	13.5	18.1	14.0	14.9	13.8	13.2	14.0	13.7	89	64	87	80	1.8	7.8	2.3	4.0	7.2	7.1	7.1	7.1
VIII	1007.8	1018.0	995.2	1013.0	19.2	11.6	26.2	12	7.0	15	13.8	18.0	14.5	15.2	13.8	14.0	14.3	14.0	87	68	86	80	2.1	6.9	2.4	3.8	7.5	7.7	7.0	7.4
IX	1008.9	1026.0	987.1	1014.2	16.1	8.4	25.5	4	4.5	24	10.3	15.1	11.3	12.0	11.5	12.4	11.9	11.9	91	72	88	84	1.2	5.1	1.7	2.7	6.9	7.5	5.6	6.7
X	1015.9	1031.8	1000.4	1021.3	12.3	5.4	20.6	1	-1.5	28	7.0	11.5	8.3	8.8	9.3	10.2	9.7	9.7	91	74	86	84	1.0	3.8	1.6	2.1	7.5	7.6	6.7	7.3
XI	1012.3	1027.0	994.8	1017.7	5.3	1.8	12.8	4	-4.2	25	2.7	4.4	3.5	3.5	6.7	7.1	6.7	6.8	89	82	84	85	0.8	1.6	1.4	1.3	8.5	8.6	8.0	8.4
XII	1010.6	1044.9	968.4	1016.2	-1.9	-6.5	5.0	5	-18.2	23	-4.7	-3.1	-4.2	-4.0	4.2	4.4	4.2	4.3	87	83	85	85	0.6	0.8	0.7	0.7	8.3	7.3	7.3	7.6
Rok	1009.2	1044.9	967.2	1014.6	9.9	3.3	28.0	16.VI	-18.3	31.I	5.3	8.7	6.1	6.6	8.6	8.8	8.7	8.7	86	74	83	81	1.4	4.1	1.8	2.4	7.8	7.7	7.1	7.5

Płocko $\varphi = 54°09'$ $\lambda = 16°50'$

I	–	–	–	–	2.2	-1.3	7.3	22	-11.1	31	0.3	1.2	0.7	0.7	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.7	8.7	8.8
II	–	–	–	–	0.2	-4.1	4.7	12	-15.6	1	-2.0	-0.2	-1.2	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.3	7.5	8.3
III	–	–	–	–	1.6	-7.2	7.9	31	-13.9	15,20	-4.0	0.3	-2.3	-2.1	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.2	6.9	7.1
IV	–	–	–	–	12.9	2.9	26.0	19	-0.8	10	5.8	11.6	6.9	7.8	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.2	6.3	6.5
V	–	–	–	–	12.9	4.7	18.9	19	-1.2	1	7.8	11.8	7.5	8.6	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.9	7.4	7.8
VI	–	–	–	–	17.8	7.8	27.0	15	2.2	8	11.9	16.6	11.6	12.9	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.8	6.8	6.7
VII	–	–	–	–	19.0	9.0	25.8	22	5.6	9,10,30,31	13.3	17.7	13.5	14.5	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.9	7.2	6.9
VIII	–	–	–	–	18.4	9.9	28.2	12	5.2	10,15	13.1	17.2	13.6	14.4	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.5	8.7	7.6
IX	–	–	–	–	16.4	7.0	26.4	4	1.7	18	10.3	15.3	10.7	11.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.7	6.0	6.4
X	–	–	–	–	13.3	4.4	21.8	2,4	-2.3	28	7.6	12.3	8.4	9.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.9	7.4	7.4
XI	–	–	–	–	5.0	1.3	13.1	8	-6.5	24	2.4	3.9	3.2	3.2	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.4	8.3	8.6
XII	–	–	–	–	-2.0	-7.1	4.6	13	-19.6	22	-5.1	-3.5	-4.7	-4.5	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.0	7.6	8.1
Rok	–	–	–	–	9.8	2.3	28.2	12.VIII	-19.6	22.XII	5.1	8.7	5.7	6.3	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.5	7.4	7.5

Kościerzyna $\varphi = 54°08'$ $\lambda = 17°58'$

I	–	–	–	–	1.4	-2.0	6.9	22	-16.3	31	0.0	0.6	-0.5	-0.1	5.6	5.6	5.4	5.5	89	85	88	87	0.6	1.0	0.8	0.8	10.0	9.3	8.5	9.3
II	–	–	–	–	-0.1	-5.2	3.7	12	-17.9	1	-3.3	-1.3	-2.2	-2.2	4.2	4.8	4.6	4.5	85	83	85	84	0.7	0.9	0.8	0.8	8.8	8.4	8.4	8.5
III	–	–	–	–	0.7	-8.3	7.0	31	-16.9	9	-5.9	0.1	-3.5	-3.2	3.7	4.8	4.2	4.2	88	77	86	84	0.5	1.4	0.6	0.8	7.0	6.9	5.1	6.3
IV	–	–	–	–	12.6	3.6	25.3	21	-1.8	30	5.8	11.1	6.9	7.7	8.0	8.1	8.2	8.1	85	61	81	76	1.5	6.4	2.2	3.4	7.4	7.0	5.0	6.5
V	–	–	–	–	13.2	4.6	18.0	8,19	-3.7	1	7.7	11.3	7.7	8.6	9.4	9.1	9.2	9.2	88	70	86	81	1.3	4.6	1.5	2.5	7.6	8.8	6.7	7.7
VI	–	–	–	–	17.7	7.4	27.0	16	1.2	3	11.5	16.0	11.7	12.7	11.0	10.4	11.0	10.8	80	58	78	72	2.9	8.5	3.3	4.9	7.3	6.7	6.6	6.9
VII	–	–	–	–	18.7	9.1	26.0	21	5.4	5,18	13.0	17.0	12.7	13.8	13.2	12.8	13.1	13.0	88	67	88	81	1.9	7.1	1.8	3.6	6.7	7.8	6.1	6.9
VIII	–	–	–	–	18.3	10.2	25.8	12	5.7	10,15	12.7	17.0	13.3	14.1	13.1	13.5	13.6	13.4	89	70	88	82	1.6	6.1	1.9	3.2	7.6	8.0	6.6	7.4
IX	–	–	–	–	15.3	7.1	25.3	4	1.6	25	9.2	14.1	9.8	10.7	10.8	11.6	11.2	11.2	93	72	92	86	0.9	4.9	1.1	2.3	7.7	8.2	4.9	6.9
X	–	–	–	–	11.7	3.8	20.1	3	-2.8	28	5.4	10.9	7.1	7.6	8.9	10.0	9.5	9.5	97	76	92	88	0.3	3.5	0.9	1.6	8.5	7.2	5.9	7.2
XI	–	–	–	–	4.1	0.7	10.4	5	-4.6	24	1.7	3.2	2.3	2.4	6.7	7.1	6.9	6.9	95	91	94	93	0.4	0.8	0.5	0.6	8.6	8.0	8.4	8.3
XII	–	–	–	–	-2.2	-7.9	4.6	1	-20.3	22	-5.1	-3.5	-5.5	-4.9	4.3	4.5	4.2	4.3	93	90	94	92	0.3	0.5	0.2	0.3	8.3	7.5	6.6	7.5
Rok	–	–	–	–	9.3	1.9	27.0	16.VI	-20.3	22.XII	4.4	8.0	5.0	5.6	8.2	8.5	8.4	8.4	89	75	88	84	1.1	3.8	1.3	2.1	8.0	7.8	6.6	7.5

Lidzbark Warmiński $\varphi = 54°08'$ $\lambda = 20°36'$

I	–	–	–	–	1.7	-2.4	9.5	23	-19.5	31	-0.6	0.7	-0.6	-0.3	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.0	7.5	8.2
II	–	–	–	–	-0.6	-6.0	3.5	12	-20.0	1	-4.0	-1.6	-3.2	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.4	8.0	8.3
III	–	–	–	–	-0.2	-7.4	7.6	31	-15.0	1	-6.1	-1.0	-3.8	-3.7	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.7	6.2	6.7
IV	–	–	–	–	13.8	4.0	28.1	23	-1.3	8	6.2	12.5	7.9	8.6	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.3	6.2	6.9
V	–	–	–	–	14.0	5.5	18.9	13	-2.9	6	8.3	12.6	8.9	9.7	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.0	7.8	8.2
VI	–	–	–	–	19.2	8.2	29.1	16	1.6	3	11.6	17.7	12.6	13.6	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.2	5.6	5.7
VII	–	–	–	–	20.3	10.4	27.1	21	6.6	30	13.4	18.4	13.6	14.8	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.0	6.9	6.5
VIII	–	–	–	–	20.0	11.3	26.1	12	4.6	15	13.4	18.4	14.5	15.2	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.2	7.7	7.6
IX	–	–	–	–	16.1	7.7	25.7	4	1.9	27	9.0	14.9	10.9	11.4	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.1	6.8	7.3
X	–	–	–	–	12.7	4.4	19.9	1,3	-1.7	30	6.0	11.1	7.9	8.2	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.3	7.3	7.6
XI	–	–	–	–	5.2	1.1	13.4	4	-2.7	22	2.3	4.3	3.0	3.2	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.8	8.9	8.9
XII	–	–	–	–	-2.6	-7.6	4.8	5	-21.5	23	-5.6	-3.9	-5.5	-5.1	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.3	7.7	7.7
Rok	–	–	–	–	10.0	2.4	29.1	16.VI	-21.5	23.XII	4.5	8.7	5.5	6.0	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.2	7.2	7.5

Elbląg $H_s = 38 m$ $H_b = 42,8 m$ $h_w = 14,5 m$ anemometr, $14,0 m$ wiatromierz Wilda — 1962

MIESIĄC	ROZKŁAD WIATRU (nD, vmD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	◎	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R ro
I	2.5	5.6	7	5.5	2	4.5	13.5	4.9	24	5.6	21.5	5.4	12	4.2	10.5	3.5	·	5.0	28	7.1	27	3	3	17	·	3	1	2	26	14	8	·	1	24	·
II	10	9.2	10	5.5	9	6.8	6.5	6.5	15	4.8	11	5.6	10	3.6	12.5	6.4	·	6.0	27	4.4	12	3	10	24	·	12	·	1	21	13	9	·	2	27	·
III	14	6.6	15.5	4.6	5.5	3.7	27	5.1	14	3.7	3.5	2.9	5	2.1	8.5	4.0	·	4.6	30	6.0	12	6	11	30	·	7	·	3	16	9	8	·	4	22	·
IV	13.5	6.0	6.5	7.3	6	5.0	14	4.8	16	4.8	12.5	3.2	4	2.8	17.5	3.4	·	4.6	22	8.8	27	·	·	1	1	6	·	1	12	15	7	·	5	·	·
V	15.5	4.1	13	3.8	5	3.0	8.5	4.0	19	3.5	8.5	3.9	8	3.2	13.5	3.1	2	3.5	155	34.8	15	·	·	1	·	3	·	·	14	23	14	5	3	·	7
VI	22.5	6.1	5	3.8	4.5	2.0	6.5	2.9	7	2.8	14	3.9	13.5	3.4	15	3.6	2	4.0	99	44.4	16	·	·	·	1	4	1	·	10	13	10	3	1	·	3
VII	19.5	3.3	6	3.9	4	2.0	9.5	2.7	11.5	4.7	10.5	3.4	9	3.6	22	3.3	1	3.4	84	26.0	12	·	·	·	3	·	·	1	12	21	13	1	3	·	7
VIII	11.5	3.0	2.5	2.6	7.5	2.7	7	3.1	12.5	3.8	19.5	4.5	18.5	2.9	11	3.1	3	3.2	87	12.4	31	·	·	·	1	1	·	1	16	17	15	4	2	·	6
IX	7	3.6	6.5	3.1	8.5	4.0	7	4.1	13	3.7	14	3.8	12	3.9	17	3.2	5	3.4	106	29.7	18	·	·	·	1	1	·	3	13	13	13	5	5	·	4
X	9.5	3.2	3	1.5	3.5	1.6	19.5	3.4	16.5	3.3	10.5	4.0	10	2.0	10.5	3.1	10	2.7	12	4.7	31	·	·	4	·	·	·	1	13	5	3	·	7	·	·
XI	2	2.5	7	6.5	13	7.3	20.5	6.0	23.5	3.0	12	2.8	6	3.5	3	3.3	3	4.5	44	8.8	20	·	·	9	·	5	·	2	21	13	11	·	5	·	·
XII	1.5	2.0	10	3.2	17.5	2.6	13.5	3.3	20.5	4.6	18	3.9	5.5	2.3	2.5	2.0	4	3.3	47	5.6	13	10	16	25	·	1	·	3	18	10	5	·	5	21	·
Rok	129	4.6	92	4.3	86	3.8	153	4.2	192.5	4.0	155.5	3.9	113.5	3.1	143.5	3.5	30	4.0	711	44.4	16.VI	22	40	111	7	43	2	18	192	166	116	18	43	94	27

UWAGA. Kierunki wiatru – wg wiatromierza Wilda, prędkości – wg anemometru

Płocko $H_s = 125 m$ $h_w = 14 m$ I–VIII, $15 m$ IX–XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◎	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R ro
I	9	5.4	4	6.7	·	·	3	4.0	17.5	4.9	39.5	7.7	11	6.6	9	4.6	·	6.3	64	9.8	6	1	4	17	·	6	2	–	–	19	15	·	·	–	–
II	10	4.4	14	3.9	3	3.3	·	·	11	4.2	16	6.6	17	6.4	13	5.8	·	5.3	72	13.8	16	2	11	24	·	5	3	–	–	18	10	2	·	–	–
III	12	3.2	9	2.8	2	3.0	10	3.9	24	2.6	9	2.8	11	2.4	16	3.4	·	3.0	53	22.4	12	10	9	29	·	·	·	–	–	10	9	1	3	–	–
IV	12	3.3	7	4.1	2	3.5	4	3.0	18	3.9	15	4.4	18	3.9	12	3.4	2	3.8	20?	5.2	1	·	·	4	2	·	·	–	–	9	6	·	4	–	–
V	8	2.4	4	3.2	1	2.0	6	3.2	9.5	3.5	14.5	4.0	26	3.2	21	3.9	3	3.3	97	17.4	12	·	·	4	·	·	·	–	–	20	18	1	3	·	–
VI	15	4.6	·	·	1	2.0	2	7.0	2	3.8	20	5.0	31	3.8	18	2.8	1	4.0	67	20.2	27	·	·	·	4	2	·	–	–	10	10	1	·	·	–
VII	14.5	2.8	·	·	·	·	·	·	7	3.1	31	4.2	23	3.3	17.5	3.1	·	3.5	61	13.8	4	·	·	·	3	·	·	–	–	11	11	2	1	·	–
VIII	·	·	·	·	3	3.0	3	2.3	9.5	4.4	41	4.9	25.5	3.6	8	2.8	3	4.0	100	9.4	25	·	·	·	1	1	·	–	–	20	20	·	·	·	–
IX	2	2.0		·	·	·	7	3.3	11.5	2.8	36.5	4.0	22	3.8	6	4.0	5	3.5	40	8.6	23	·	·	·	1	·	·	–	–	8	7	·	3	·	–
X	1	2.0	·	·	·	·	·	·	38	2.4	34	2.9	13	3.5	3	2.7	4	2.6	27	6.7	4	·	·	3	·	·	·	–	–	8	7	·	9	·	–
XI	3	1.3	3	2.7	6	3.3	20	3.2	22	2.6	21	4.0	5	4.8	3	3.3	7	3.0	36	10.6	29	·	·	12	·	·	·	–	–	11	9	1	3	–	–
XII	·	·	1	1.0	10	2.7	14	3.1	28.5	3.2	31.5	4.0	4	2.5	·	·	4	3.2	31	13.6	11	9	16	25	·	·	·	–	–	7	5	1	4	–	–
Rok	86.5	2.6	42	2.0	28	1.9	69	2.8	198.5	3.4	309	4.5	206.5	4.0	126.5	3.3	29	3.8	668?	22.4	12.III	22	40	118	11	14	5	–	–	151	127	9	30	–	–

Kościerzyna $H_s = 180 m$ $h_w = 12 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◎	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R ro
I	4	3.5	5	3.0	1	1.0	1	3.0	2	6.0	29	6.0	32	3.1	15	3.9	4	4.0	51	6.0	20	2	5	17		1	·	·	27	23	17	·	5	12	·
II	7	5.8	14	5.7	1	7.0	·	·	1	7.0	18	6.3	19	3.4	22	5.7	2	5.2	47	10.7	12	3	12	24		5	·	1	22	21	12	1	2	21	1
III	7.5	2.9	6	5.0	·	·	4	3.0	8	4.0	10	3.0	14	4.1	26.5	2.3	17	2.2	45	14.4	12	13	14	30		·	·	3	12	13	10	1	7	29	·
IV	7	2.4	8	5.5	1	7.0	2	5.0	1	7.0	17	4.2	24	1.8	23	2.0	7	2.7	28	5.6	5,6	·	·	5	1	·	·	3	10	14	9	·	3	·	1
V	9	1.7	3	3.0	·	·	1	3.0	2	2.0	14	3.6	32	1.3	29	1.8	3	1.9	83	24.0	14	·	·	4	·	·	·	1	13	25	15	1	1	·	3
VI	11	4.6	·	·	·	·	·	·	·	·	9	4.3	27.5	2.7	38.5	1.6	4	2.5	97	30.4	16	·	·	·	3	·	·	1	10	15	14	1	1	·	5
VII	3	1.7	2	3.0	·	·	·	·	·	·	9.5	3.7	27.5	2.2	36	1.4	15	1.7	61	26.4	22	·	·	·	2	·	·	3	10	18	11	1	4	·	7
VIII	·	·	1	3.0	·	·	·	·	·	·	10	5.1	45	2.7	27	1.6	10	2.3	112	40.6	7	·	·	·	1	1	·	2	14	20	13	3	1	·	5
IX	3	1.0	0.5	1.0	2	4.0	·	·	·	·	9	3.9	33.5	2.7	32	1.4	10	2.0	89	16.2	18	·	·	·	1	·	·	2	15	16	13	4	4	·	5
X	1.5	3.0	·	·	·	·	·	·	·	·	15.5	2.7	32.5	1.8	20.5	1.6	23	1.5	47	4.2	5	·	·	6	·	·	·	2	14	15	5	·	12	·	·
XI	3	1.0	8	4.0	16	4.1	5	4.6	1	5.0	12	3.2	14	1.4	7	1.7	24	2.2	60	15.5	1	·	2	14	·	·	·	2	20	16	8	2	7	4	·
XII	7	1.6	14	3.2	0.5	1.0	0.5	4.0	·	·	15	5.4	27.5	2.0	9.5	1.8	19	2.3	27	5.4	13	10	15	28	·	·	·	3	17	13	10	·	3	20	·
Rok	63	2.4	61.5	3.0	21.5	2.0	13.5	1.6	15	2.6	168	4.3	328.5	2.2	286	2.2	138	2.5	717	40.6	7.VIII	28	48	128	8	7	·	23	184	209	137	14	50	86	27

Lidzbark Warmiński $H_s = 90 m$ $h_w = 13 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◎	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R ro
I	3	10.0	5	4.4	4.5	2.9	3	5.7	28.5	5.5	34	8.1	9.5	4.1	4.5	4.2	1	6.1	36	6.7	17	3	3	18	·	7	1	1	18	12	11	·	·	15	–
II	7.5	5.9	12.5	3.2	5	4.8	3.5	3.6	19	4.6	19	8.2	4.5	9.7	13	7.3	·	6.0	33	6.9	12	5	14	26	·	8	2	·	19	13	10	·	·	19	–
III	17	3.7	11	2.8	4	3.0	23	3.6	15.5	2.0	10.5	2.0	2	1.5	8	5.8	2	3.1	31	14.2	6	8	15	30	·	2	·	1	14	8	7	1	3	30	–
IV	6.5	2.8	16.5	3.5	6	2.2	11.5	4.9	15	3.8	3.5	3.7	9	2.6	10	5.2	12	3.2	16	7.6	5	·	·	4	2	1	·	·	11	8	6	·	–	·	–
V	11	2.2	10.5	2.0	3	3.5	12.5	4.2	5	3.3	20	3.2	19.5	3.2	9.5	2.4	2	2.9	88	20.5	14	·	·	2	·	·	·	·	16	20	13	2	3	·	–
VI	13	5.1	2.5	3.0	·	·	4	2.5	6	2.3	29	4.0	8.5	4.1	23	2.8	·	3.4	42	20.2	29	·	·	·	2	1	·	5	7	9	6	1	1	·	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	71	18.7	26	·	·	·	3	–	–	1	8	11	11	2	·	·	–
VIII	9	1.9	2	2.0	1	1.0	3	2.3	11	3.9	21	6.6	27.5	4.3	11.5	2.8	7	3.9	120	19.2	7	·	·	·	1	2	·	·	15	16	15	5	·	·	–
IX	7	1.6	10	1.7	2	2.0	1.5	3.3	3	4.3	23	4.4	33.5	3.6	4	2.2	6	3.1	82	27.3	18	·	·	·	1	·	·	2	16	15	13	2	3	·	–
X	5	1.6	·	·	·	·	4	3.2	17	2.4	23	3.2	16	3.4	8	2.0	20	2.2	20	6.9	5	·	·	7	·	·	·	·	14	9	6	·	6	·	–
XI	9.5	1.2	7	5.7	16.5	4.9	14.5	4.6	10.5	2.6	12.5	3.0	14.5	3.4	·	·	5	3.5	44	17.1	20	·	·	11	·	1	·	1	24	8	7	2	2	·	–
XII	14	1.1	17	1.6	·	·	3	3.7	16	3.9	19	4.1	20	3.2	3	1.7	1	2.8	14	6.2	13	10	15	27	·	·	·	3	18	4	4	·	·	16	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	597	27.3	18.IX	26	47	125	9	–	–	14	180	133	109	15	–	80	–

Orneta $\varphi = 54°07'$ $\lambda = 20°07'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{0,m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–		1.7	-2.2	7.8	22	-20.1	31	-0.4	0.7	-0.4	-0.1	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.7	7.5	8.1
II	–	–	–	–	-0.4	-5.6	4.5	13	-15.9	1	-3.3	-1.4	-2.6	-2.5	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.8	7.8	8.0
III	–	–	–	–	0.2	-7.8	6.5	31	-19.0	15	-5.9	-0.7	-3.2	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.3	6.1	6.6
IV	–	–	–	–	13.6	4.1	27.5	23	-1.8	30	6.5	12.2	7.4	8.4	–	–	–	–	–	–	–	–	–	–	–	–	7.9	6.2	6.4	6.8
V	–	–	–	–	13.5	5.5	18.1	19	-2.2	1	8.4	12.2	9.0	9.6	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.6	8.0	7.5
VI	–	–	–	–	18.6	8.2	29.3	16	1.4	3	12.4	16.7	12.8	13.7	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.4	6.2	5.7
VII	–	–	–	–	19.6	10.0	28.0	21	5.5	30	13.3	18.4	13.9	14.9	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.2	6.4	6.5
VIII	–	–	–	–	19.5	11.3	26.4	12	4.0	15	13.5	18.2	14.4	15.1	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.1	6.5	6.5
IX	–	–	–	–	15.7	7.5	25.8	4	2.8	25	9.7	14.6	11.0	11.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.0	6.1	6.6
X	–	–	–	–	12.1	4.2	19.6	1	-1.5	13	5.9	11.5	7.7	8.2	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.2	7.0	6.7
XI	–	–	–	–	5.2	1.3	13.1	4	-3.1	25	2.6	4.3	3.1	3.3	–	–	–	–	–	–	–	–	–	–	–	–	9.5	8.3	8.9	8.9
XII	–		–	–	-2.3	-7.3	5.2	5	-21.6	23	-5.2	-3.8	-5.0	-4.8	–	–	–	–	–	–		–	–	–	–	–	8.5	8.0	8.2	8.2
Rok	–	–	–	–	9.8	2.4	29.3	16.VI	-21.6	23.XII	4.8	8.6	5.7	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.9	7.1	7.2

Kętrzyn $\varphi = 54°06'$ $\lambda = 21°21'$

I	999.3	1028.2	973.8	1012.8	1.3	-2.5	6.6	22	-18.4	31	-1.1	0.3	-0.9	-0.6	5.3	5.6	5.1	5.3	89	86	85	87	0.6	0.9	0.9	0.8	8.7	8.3	7.5	8.2
II	1000.0	1024.1	959.0	1013.7	-0.7	-6.2	3.8	12	-15.7	1	-4.3	-2.3	-3.2	-3.2	4.0	4.4	4.2	4.2	87	82	85	85	0.6	0.9	0.7	0.7	7.5	7.6	6.8	7.3
III	998.2	1016.2	974.6	1011.9	-0.1	-7.1	7.0	31	-14.3	1	-5.7	-1.1	-3.5	-3.4	3.6	4.3	4.0	4.0	86	75	81	81	0.6	1.4	0.8	0.9	7.7	6.1	5.7	6.5
IV	1000.7	1017.5	976.8	1013.8	13.4	4.1	26.5	23	-1.4	8	5.9	11.9	7.8	8.4	8.6	9.5	9.2	9.1	90	68	85	81	1.1	5.5	2.0	2.9	7.8	6.6	5.4	6.6
V	998.9	1007.5	978.1	1011.9	13.9	5.5	19.1	13	-3.5	1	8.3	12.5	9.2	9.8	9.9	10.2	10.3	10.1	88	70	87	82	1.3	4.7	1.6	2.5	8.5	8.5	7.8	8.3
VI	1003.6	1016.2	990.4	1016.4	18.6	8.3	28.0	16	3.4	10	12.4	16.7	12.7	13.6	11.9	14.7	11.4	11.7	81	62	77	73	2.9	8.3	3.7	5.0	6.1	6.6	6.0	6.2
VII	1000.2	1010.1	985.6	1013.0	19.5	10.5	26.5	21	6.6	4	13.5	18.0	13.9	14.8	14.1	14.3	14.1	14.2	91	70	88	83	1.5	6.6	2.0	3.4	7.1	7.3	6.1	6.8
VIII	1000.4	1010.3	988.4	1013.2	19.8	11.3	25.8	12	5.0	15	13.7	18.2	14.3	15.1	14.2	14.9	14.5	14.5	90	71	88	83	1.5	6.4	2.0	3.3	7.1	7.2	6.1	6.8
IX	1001.3	1018.7	981.1	1014.2	15.8	7.8	24.9	4	3.3	25,27	9.3	14.5	10.7	11.3	11.1	12.4	12.0	11.8	94	75	92	87	0.8	4.5	1.1	2.1	6.3	7.5	4.3	6.0
X	1008.1	1023.4	991.7	1021.3	12.0	5.0	19.5	2	-1.0	15	6.3	11.1	7.8	8.2	9.2	10.4	9.8	9.8	93	77	91	87	0.6	3.2	1.0	1.6	7.6	6.9	5.5	6.7
XI	–	–	–	–	5.0	1.2	12.0	4	-4.3	26	2.2	4.1	2.8	3.0	6.9	7.4	7.0	7.1	93	88	91	91	0.5	1.1	0.7	0.8	8.8	9.1	7.7	8.5
XII	–	–		–	-3.0	-8.0	3.9	5	-23.9	23	-5.9	-4.5	-5.8	-5.5	4.0	4.2	4.0	4.1	87	85	87	86	0.5	0.6	0.5	0.5	6.9	7.2	7.3	7.1
Rok	–	–		–	9.6	2.5	28.0	16.VI	-23.9	23.XII	4.6	8.3	5.5	6.0	8.6	9.1	8.8	8.8	89	76	86	84	1.0	3.7	1.4	2.0	7.5	7.4	6.4	7.1

Suwałki $\varphi = 54°06'$ $\lambda = 22°57'$

I	991.4	1020.0	967.7	1012.8	0.3	-3.3	4.6	22	-19.6	31	-1.7	-0.7	-1.8	-1.5	5.1	5.3	5.0	5.1	90	87	89	89	0.5	0.7	0.6	0.6	8.5	8.3	7.7	8.2
II	991.6	1013.6	950.5	1013.2	-1.7	-8.4	2.1	12,16	-18.6	28	-5.9	-3.3	-4.9	-4.8	3.8	4.2	4.0	4.0	92	85	88	88	0.3	0.7	0.5	0.5	8.7	8.1	7.5	8.1
III	990.2	1008.5	969.0	1011.7	-0.5	-8.5	5.3	31	-19.2	1	-6.9	-1.8	-4.5	-4.4	3.5	4.1	3.8	3.8	90	75	84	83	0.4	1.3	0.7	0.8	7.1	7.1	6.0	6.7
IV	992.9	1010.3	971.6	1013.5	13.3	4.1	25.7	23	-1.6	8	5.9	11.7	7.8	8.3	8.5	9.0	9.1	8.9	89	67	84	80	1.1	6.0	2.0	3.0	8.0	8.1	7.1	7.7
V	990.8	999.9	970.3	1011.2	14.2	5.4	20.4	27	-2.4	3	8.6	12.5	9.4	10.0	10.1	9.8	10.3	10.1	88	67	85	80	1.4	5.0	1.8	2.7	8.5	9.1	7.4	8.3
VI	995.3	1007.1	982.5	1015.6	18.3	8.3	26.8	16	2.2	3	12.2	16.5	12.4	13.4	11.0	10.6	11.3	11.0	76	56	77	70	3.5	8.7	3.3	5.2	7.5	8.2	6.7	7.5
VII	992.1	1001.9	978.2	1012.0	19.7	9.7	27.2	21	5.3	4	13.8	18.2	13.9	15.0	13.4	13.4	13.6	13.5	85	64	85	78	2.6	7.9	2.5	4.3	7.7	8.3	6.1	7.4
VIII	992.7	1003.2	981.3	1012.6	19.8	10.7	25.8	7	2.9	15	13.7	18.4	14.2	15.1	14.0	13.8	14.4	14.1	89	55	88	81	1.8	7.8	2.1	3.9	7.5	7.8	5.8	7.0
IX	993.5	1011.7	974.3	1014.0	15.2	7.2	25.4	5	0.3	25	8.8	14.1	10.4	10.9	10.5	11.2	11.3	11.0	92	70	88	83	1.0	5.3	1.5	2.6	7.8	8.0	5.1	7.0
X	1000.2	1015.3	982.1	1020.9	11.4	3.8	18.8	1	-2.0	16	5.4	10.5	6.6	7.3	8.4	9.4	9.0	8.9	92	73	90	85	0.7	3.6	0.9	1.7	8.4	8.2	6.2	7.6
XI	998.1	1010.6	980.9	1019.3	5.2	0.8	11.9	2	-5.1	25	1.8	4.1	2.7	2.8	6.7	6.9	6.8	6.8	92	82	88	87	0.5	1.6	0.9	1.0	8.7	8.3	7.9	8.3
XII	994.5	1027.5	955.7	1016.3	-3.4	-8.1	3.1	5,7	-21.8	23	-5.7	-4.5	-6.0	-5.6	3.9	4.0	3.9	3.9	87	82	87	85	0.5	0.8	0.5	0.6	8.4	7.6	7.6	7.9
Rok	993.6	1027.5	950.5	1014.4	9.3	1.8	27.2	21.VII	-21.8	23.XII	4.2	8.0	5.0	5.6	8.2	8.5	8.5	8.4	88	73	86	82	1.2	4.1	1.4	2.2	8.1	8.1	6.8	7.7

Sejny $\varphi = 54°06'$ $\lambda = 23°21'$

I		–		–	0.6	-3.3	5.1	22,23	-20.9	31	-1.6	-0.3	-1.7	-1.3	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.5	7.5	7.9
II	–	–	–	–	-1.5	-8.5	2.1	12,13,16	-20.6	28	-5.9	-2.9	-5.0	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.6	6.1	7.3
III	–	–	–	–	0.2	-9.4	5.9	31	-22.7	1	-7.5	-1.1	-4.7	-4.5	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.7	5.6	5.8
IV	–	–	–	–	13.3	3.7	25.9	23	-2.7	8	6.1	12.0	7.8	8.4	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.6	6.3	6.3
V	–	–	–	–	14.7	4.6	21.8	27	-2.8	1,4	8.6	13.1	9.1	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.9	6.6	7.1
VI	–	–	–	–	18.8	7.2	27.1	16	2.5	3	12.3	17.0	11.8	13.2	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.7	5.2	5.8
VII	–	–	–	–	20.4	8.9	26.9	21	4.8	8,17	13.7	19.2	13.8	15.1	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.7	6.2	6.3
VIII	–	–	–	–	20.4	9.8	27.3	13	2.3	15	13.5	18.7	13.7	14.9	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.6	5.8	6.3
IX		–	–	–	15.7	6.7	26.1	5	-0.6	25	8.8	14.5	10.1	10.9	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.7	5.1	6.1
X	–	–	–	–	11.9	3.1	19.2	1,2	-4.5	16	5.2	10.9	6.1	7.1	–	–	–	–	–	–	–	–	–	–	–		7.3	6.8	5.6	6.6
XI	–		–	–	5.4	0.4	13.4	1	-5.7	25	2.0	4.1	2.8	2.9	–	–	–	–		–	–	–	–	–	–	–	8.4	7.2	6.7	7.4
XII	–	–	–	–	-3.0	-8.0	3.9	8	-21.6	23	-5.6	-4.4	-6.0	-5.5	–	–	–	–	–	–	–	–	–	–	–	–	7.9	6.6	6.6	7.0
Rok	–	–	–	–	9.7	1.3	27.3	13.VIII	-22.7	4.III	4.1	8.4	4.8	5.5		–	–	–	–	–	–	–	–	–	–	–	7.0	6.9	6.1	6.7

Orneta $H_s = 70\,m$ $h_w = 14\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU (%D, %mD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -18°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	> 15	◐	●	Opad R ≥ 0,1	≥ 1,0	≥ 10,0	▬	▦	∂R
I	2,5	7,0	3,5	4,9	1	1,0	3	5,7	27	3,5	36,5	6,0	13,5	4,5	2	3,5	4	4,7	28	5,3	20	3	4	19	·	2	1	1	17	15	10	·	·	14	–
II	7	7,5	13,5	3,4	6	2,3	9,5	2,7	11	3,6	19	5,8	10,5	4,7	5,5	1,1	2	4,7	28	8,3	5	4	12	23	·	6	2	·	18	16	8	·	·	16	–
III	15	4,3	6	3,2	10	2,7	22	3,0	15	2,8	0,5	3,0	6,5	2,8	8	3,5	10	2,9	34	9,7	5	10	13	30	·	1	·	2	14	11	8	·	6	25	–
IV	14	3,6	8	2,1	7	3,3	12,5	3,6	17,5	2,7	12	2,6	1,5	1,7	9,5	4,0	8	2,8	21	5,7	27	·	·	3	2	1	·	·	9	15	6	·	2	·	–
V	9,5	2,7	6	3,1	9,5	2,1	11	2,6	11	2,9	14,5	3,7	17	2,7	11,5	4,7	3	3,0	130	24,9	14	·	·	2	·	2	·	·	17	22	18	4	·	·	–
VI	18	4,8	1,5	2,3	0,5	1,0	4,5	2,6	6	1,9	12,5	5,2	27	3,5	15	3,6	5	3,6	44	10,5	23	·	·	·	3	1	·	2	8	14	10	2	·	·	–
VII	8	2,4	1,5	2,0	2,5	1,2	2	2,0	11,5	2,2	11,5	3,0	25,5	2,7	26,5	2,7	4	2,5	71	16,7	26	·	·	·	3	·	·	1	8	14	13	1	1	·	–
VIII	5	2,3	3,5	2,6	6,5	1,3	3	2,2	18	2,9	24	5,1	16,5	3,7	11,5	2,1	5	3,2	68	12,8	24	·	·	·	1	·	·	1	11	16	14	1	·	·	–
IX	1	3,0	4	1,8	9	2,2	4,5	2,0	10,5	3,0	22	4,0	18	4,0	10	3,0	11	2,9	105	23,2	18	·	·	·	1	1	·	2	11	14	13	4	3	·	–
X	2,5	1,6	0,5	2,0	3,5	1,0	15,5	2,4	13	2,2	11,5	4,3	8,5	2,5	11	2,5	27	1,8	15	3,9	14	·	·	5	·	1	1	·	13	10	5	·	11	·	–
XI	4,5	1,7	6,5	3,2	23	3,7	11	2,6	11,5	2,1	18,5	2,2	5	2,4	1	1,0	9	2,5	41	10,1	20	·	·	8	·	·	·	·	20	12	11	1	16	·	–
XII	5	1,2	15,5	1,2	10	1,4	7	1,3	15,5	1,6	14,5	3,1	15,5	1,7	2	1,0	8	1,6	8,3	4,3	13	10	17	26	·	·	·	·	21	8	2	·	1	15	–
Rok	92	3,5	70	2,6	88,5	1,9	105,5	2,7	167,5	2,6	197	4,0	16,5	3,1	113,5	2,7	96	3,0	593,3	24,9	14.V	27	46	116	10	15	4	9	167	167	118	13	40	70	–

Kętrzyn $H_s = 110\,m$ $H_b = 107{,}4\,m$ $h_w = 11\,m$

I	3	5,5	5	4,5	3	2,0	3	2,7	2,3	4,3	37,5	5,4	14	4,0	2,5	2,6	2	4,5	20	3,5	6	3	4	20	·	2	·	2	20	17	7	·	1	18	·
II	2,5	5,0	7,5	4,3	8	4,0	10,5	4,1	15	4,0	16	4,9	9,5	5,1	13	5,7	2	4,5	32	6,8	12	5	12	27	·	5	·	2	14	15	9	·	3	28	·
III	5	5,9	7	3,6	4	1,6	3,4	3,6	10,5	2,0	3,5	2,9	4,5	3,8	11,5	3,6	13	2,9	29	9,5	12	7	15	29	·	4	·	3	14	10	5	·	2	30	·
IV	3,5	4,1	9,5	4,5	6	5,0	1,5	3,4	13	3,3	10,5	2,9	4,5	1,3	2,2	2,7	6	3,1	20	5,5	27	·	·	4	2	·	·	1	12	10	8	·	5	·	1
V	4	2,0	8	3,8	2	3,3	5	3,6	12,5	2,5	17	2,6	16	3,0	19,5	3,0	9	2,6	91	14,5	15	·	·	3	·	·	·	·	22	22	16	4	5	·	2
VI	9,5	4,8	4,5	6,1	1	3,0	5	2,6	6,5	2,5	12	3,0	17,5	4,3	24	2,4	10	3,0	33	10,3	29	·	·	·	2	·	·	·	8	12	7	1	·	·	4
VII	9	2,3	2	1,5	·	·	2	2,0	8,5	2,5	12	2,8	24	2,7	24,5	3,2	11	2,4	96	21,8	13	·	·	·	3	·	·	·	11	16	12	3	3	·	6
VIII	4	3,8	·	·	3	1,3	4	3,8	7	4,0	21	3,8	27	3,9	13	2,1	14	2,9	100	22,3	17	·	·	·	2	·	·	3	13	17	16	2	2	·	6
IX	5,5	3,5	0,5	1,0	6,5	2,0	6,5	2,4	9,5	3,0	14	2,9	28	4,7	7,5	2,6	12	2,9	73	31,1	18	·	·	·	·	·	·	2	10	16	13	1	3	·	2
X	4,5	1,9	·	·	·	·	9	2,1	16,5	2,3	19	2,6	16,5	3,3	12,5	2,6	15	2,2	18	5,1	19	·	·	5	·	·	·	3	13	13	5	·	5	·	·
XI	1,5	1,3	3	4,2	8,5	4,9	29,5	4,8	13	2,3	12	2,7	7	2,3	3,5	1,4	12	3,1	41	15,7	20	·	1	10	·	·	·	1	20	11	6	1	2	2	·
XII	2	1,0	1,5	1,8	3	2,0	4	3,5	18,5	2,7	14,5	3,0	13	2,8	7	1,6	16	2,1	13	4,3	11	10	14	25	·	·	·	5	18	13	5	·	1	15	·
Rok	54	3,4	62	2,9	4,5	2,4	127,5	3,2	153,5	3,0	189	3,3	181,5	3,4	160,5	2,8	122	3,0	566	31,1	18.IX	25	46	123	9	8	·	22	175	172	109	12	32	93	21

Suwałki $H_s = 165\,m$ $H_b = 169{,}6$ $h_w = 13\,m$

I	2,5	6,0	7,5	4,4	·	·	2	5,5	20,5	6,1	38	5,7	13	6,4	7,5	4,5	2	5,6	30	7,7	6	3	8	22	·	9	·	2	22	19	9	·	8	24	·
II	9	7,0	5,5	5,9	8,5	4,8	4,5	6,9	16,5	5,5	15,5	7,5	7	5,7	9,5	7,1	8	5,7	51	10,4	12	11	16	28	·	10	2	·	18	19	11	2	4	28	·
III	8,5	7,3	11	4,6	7	3,3	15,5	5,6	8	4,4	15,5	3,1	5	4,7	7,5	5,7	15	4,0	32	9,7	6	12	17	29	·	8	1	4	13	13	6	·	4	31	·
IV	7	3,9	10	5,0	8,5	3,9	11,5	5,4	12,5	5,5	11	4,7	9	4,6	8,5	5,0	12	4,2	37	11,4	13	·	·	3	1	4	·	2	15	13	8	1	3	1	4
V	4,5	2,3	5,5	3,2	3	6,0	8,5	4,0	4	4,8	15	4,3	14,5	3,5	19	4,7	19	3,3	105	16,9	20	·	·	5	·	4	·	·	16	17	15	3	4	·	3
VI	10	6,2	3,5	7,3	2,5	4,6	1	2,0	7,5	3,2	23	4,8	16,5	5,2	13	4,5	13	4,2	52	15,4	23	·	·	·	1	7	·	·	13	14	10	2	1	·	4
VII	6	3,7	3	4,2	2,5	2,6	·	·	10,5	3,9	13	4,2	23	5,3	21	4,2	14	3,8	40	9,0	3	·	·	·	4	5	·	·	12	14	8	·	7	·	5
VIII	6	4,3	2	3,0	0,5	4,0	4	5,8	9	4,2	29,5	4,9	27	4,9	6	1,9	9	4,1	101	16,9	15	·	·	·	2	7	·	·	13	18	16	2	4	·	6
IX	3	3,8	5,5	2,9	7	3,7	3,5	4,3	11,5	4,5	21,5	6,2	19	5,4	7	5,4	12	4,3	77	23,9	18	·	·	·	1	10	1	1	13	18	12	1	6	·	4
X	6	3,3	·	·	0,5	4,0	5	3,3	9,5	4,1	18,5	4,1	19	4,6	11,5	3,1	23	3,0	12	7,2	28	·	·	5	·	4	·	1	17	10	3	·	12	·	·
XI	3,5	4,4	·	·	1,0	8,4	3,9	5,9	5	4,0	16	3,2	8	3,0	3,5	2,7	5	4,8	52	13,3	15	·	2	15	·	10	1	2	22	18	10	2	13	1	·
XII	8,5	2,8	14,5	2,6	1,5	3,0	3	3,0	17,5	4,4	18,5	5,6	9	4,6	6,5	3,9	14	3,5	17	3,4	14	12	17	29	·	2	1	2	19	17	4	·	3	20	·
Rok	74,5	4,6	68	3,6	51,5	4,0	97,5	4,3	132	4,6	235	4,9	170	4,8	120,5	4,4	146	4,2	606	23,9	18.IX	38	60	136	9	80	6	14	193	188	112	13	69	105	26

UWAGA. [1]) Kierunki i prędkości – wg anemometru.

[2]) Ciśnienie powietrza jest za niskie przeciętnie o około 0,3 mb.

Sejny $H_s = 130\,m$ $h_w = 12\,m$

I	6	7,0	4,5	4,3	2	3,0	3	4,8	2,3	4,8	2,3	6,9	17,5	5,4	7	3,1	7	5,0	21	5,4	6	3	7	20	·	6	·	2	17	12	9	·	1	–	·
II	9	8,5	3,5	7,6	9,6	5,1	5,5	3,5	9,5	4,7	10,5	7,6	6	11,5	9,5	5,4	21	4,9	35	8,8	17	11	16	28	·	6	1	·	11	12	9	·	2	–	·
III	11,5	4,8	1,5	4,0	13,5	4,3	14	5,7	7,5	2,6	0,5	4,0	4,5	4,2	11	5,0	29	3,2	26	5,5	5	13	16	29	·	·	·	6	10	11	8	·	3	–	·
IV	10	4,0	7,5	5,1	9	4,5	1,5	3,7	14	4,5	3,5	5,0	8	3,6	6	3,2	17	3,4	37	11,5	13	·	·	5	1	1	·	3	7	11	9	1	·	–	2
V	6,5	4,5	0,5	4,0	12	4,3	2	5,2	10,5	3,5	5,5	4,5	10	3,9	14	3,8	32	2,7	114	21,0	27	·	·	4	·	2	·	·	12	18	14	1	2	·	2
VI	11,5	6,1	2,5	3,0	4	5,0	1	3,0	6,5	4,2	9,5	4,5	2,6	4,3	11	3,1	18	3,5	53	13,3	4	·	·	·	2	3	·	·	3	12	8	1	·	·	2
VII	8,5	3,4	·	·	·	·	·	·	11,5	3,9	6	4,2	2,7	4,8	10	3,8	30	2,9	38	7,8	27	·	·	·	3	1	·	1	8	11	8	·	3	·	3
VIII	6,5	5,4	0,5	3,0	1	4,5	2,5	6,4	1,6	4,3	14,5	5,4	20,5	4,7	8,5	2,8	23	3,5	104	19,3	7	·	·	·	3	2	·	1	4	15	15	3	7	·	3
IX	2	3,0	6	4,0	4	3,6	5	3,1	8,5	5,3	16,5	6,3	2,1	5,9	6	3,7	21	3,9	68	18,0	18	·	·	1	1	4	·	2	7	14	11	2	6	·	2
X	2	1,0	·	·	2,5	1,6	10,5	2,4	7,5	4,1	6,5	6,6	1,4	4,7	1,7	3,4	3,3	2,5	6	2,5	2,8	·	·	8	·	1	·	2	13	9	2	·	1,8	·	·
XI	3	4,0	1,5	10,1	1,6	8,0	23,5	5,2	1	3,0	7	4,6	5	3,5	6	2,9	27	3,9	48	11,0	14	·	1	1,7	·	6	·	4	16	12	8	2	1,1	–	·
XII	12,5	3,6	6,5	3,7	7	3,1	4	3,0	1,0	6,0	1,1	5,7	10,5	5,7	3,5	3,4	2,8	3,2	12	5,0	14	11	16	27	·	1	·	3	15	10	4	·	1	–	·
Rok	8,9	4,6	3,4,5	4,1	8,0,6	3,9	8,6	3,8	12,5,5	4,2	1,1,4	5,4	1,7,0	5,2	10,9,5	3,6	28,6	3,6	56,2	21,0	27.V	38	56	139	10	33	1	24	123	1,4,7	105	1,0	5,4	–	1,4

Tczew $\varphi = 54°05'$ $\lambda = 18°48'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA t										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.8	-1.0	8.2	22	-16.3	31	0.7	1.6	0.5	0.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	1.2	-3.4	4.9	20	-14.5	1	-2.2	0.0	-1.1	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.2	7.0	6.7
III	–	–	–	–	1.8	-4.9	9.2	31	-12.6	15	-3.5	0.9	-1.9	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.0	4.4	5.0
IV	–	–	–	–	13.5	4.8	27.2	21	-0.3	30	6.8	12.4	7.5	8.6	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.7	4.0	5.1
V	–	–	–	–	14.7	6.3	19.8	19	-0.6	1	9.1	13.0	9.0	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.8	5.7	6.6
VI	–	–	–	–	19.1	10.1	27.7	16	4.5	2	12.6	17.6	13.1	14.1	–	–	–	–	–	–	–	–	–	–	–	–	4.3	5.2	4.9	4.8
VII	–	–	–	–	20.5	11.4	27.3	26	7.3	5	14.1	19.1	14.9	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.4	5.6	5.4
VIII	–	–	–	–	20.5	12.3	28.3	12	8.3	10	13.7	19.3	15.5	16.0	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.3	6.3	6.3
IX	–	–	–	–	17.2	8.8	27.5	4	4.6	27	9.9	16.3	11.9	12.5	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.0	4.2	5.3
X	–	–	–	–	13.1	5.7	20.7	3	-0.9	28	7.1	12.4	8.5	9.1	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.7	5.5	5.9
XI	–	–	–	–	5.5	1.8	12.4	4	-3.3	25	2.7	4.6	3.3	3.5	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.3	7.3	7.9
XII	–	–	–	–	-0.9	-5.8	5.6	5	-18.3	22	-4.2	-2.7	-3.8	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.9	5.7	5.9
Rok	–	–	–	–	10.8	3.8	28.3	12.VIII	-18.3	22.XII	5.6	9.5	6.4	7.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Rosnowo $\varphi = 54°04'$ $\lambda = 16°18'$

I	–	–	–	–	3.2	-0.8	8.2	22	-20.2	31	0.9	2.3	1.0	1.3	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.1	8.2	8.2
II	–	–	–	–	1.8	-3.1	5.9	8	-12.6	1	-1.3	0.8	-0.6	-0.4	–	–	–	–	–	–	–	–	–	–	–	–	9.2	7.6	5.9	7.6
III	–	–	–	–	2.8	-6.0	10.5	30	-13.6	24	-4.5	1.9	-1.9	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.0	6.0	6.1
IV	–	–	–	–	13.2	3.3	27.0	25	-1.3	1	5.3	11.9	6.6	7.6	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.1	5.0	5.9
V	–	–	–	–	13.6	5.2	19.8	19	-1.8	2,5	8.2	11.9	8.6	9.3	–	–	–	–	–	–	–	–	–	–	–	–	6.8	8.4	6.0	7.1
VI	–	–	–	–	18.2	7.8	28.2	15	0.0	4	12.0	16.9	12.0	13.2	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.7	4.0	5.2
VII	–	–	–	–	19.6	9.4	27.0	21	5.7	5,10	12.9	18.4	13.6	14.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.2	4.4	6.3
VIII	–	–	–	–	19.0	11.0	28.0	12	4.6	14	12.9	17.8	13.8	14.6	–	–	–	–	–	–	–	–	–	–	–	–	7.7	8.2	6.1	7.3
IX	–	–	–	–	16.7	7.6	26.7	4	1.6	18	9.6	15.5	10.3	11.4	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.7	3.6	5.1
X	–	–	–	–	13.3	4.4	22.1	4	-2.7	28	6.6	12.6	7.8	8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.0	4.2	5.3
XI	–	–	–	–	5.6	2.1	13.6	8	-2.3	22,25	2.9	5.1	3.4	3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.3	7.0	7.7
XII	–	–	–	–	-1.3	-6.6	5.1	12	-18.9	23	-4.4	-1.9	-4.6	-3.9	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.6	5.3	6.2
Rok	–	–	–	–	10.5	2.9	28.2	15.VI	-20.2	31.I	5.1	9.4	5.8	6.5	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.8	5.5	6.5

Stare Pole $\varphi = 54°04'$ $\lambda = 19°13'$

I	–	–	–	–	2.3	-1.3	8.3	22	-16.3	31	0.4	1.5	0.2	0.6	–	–	–	–	–	–	–	–	–	–	–	–	9.3	7.8	7.6	8.2
II	–	–	–	–	0.7	-4.3	4.6	12	-14.3	1	-2.5	-0.4	-1.5	-1.5	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.6	7.0	7.6
III	–	–	–	–	0.8	-6.6	8.2	31	-18.6	15	-4.7	0.1	-2.8	-2.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.2	4.3	6.0
IV	–	–	–	–	13.3	4.3	26.8	21	-0.4	30	6.3	12.1	7.1	8.2	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.3	6.1	6.3
V	–	–	–	–	14.2	5.5	19.2	8	-2.4	1	8.5	12.6	9.0	9.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.8	7.3	7.6
VI	–	–	–	–	18.4	8.8	28.1	16	2.6	3	12.7	16.9	12.7	13.8	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.3	6.4	5.6
VII	–	–	–	–	19.8	10.4	27.3	21	7.6	17,18	13.9	18.6	14.0	15.1	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.9	7.4	6.6
VIII	–	–	–	–	19.8	11.6	27.0	12	6.1	10	14.2	18.6	14.6	15.5	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.1	6.1	6.6
IX	–	–	–	–	16.6	8.3	26.4	4	3.3	25	10.1	15.4	11.2	12.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.9	5.5	6.5
X	–	–	–	–	12.5	5.0	20.8	1	-3.2	28	6.5	11.7	8.2	8.6	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.2	6.4	7.4
XI	–	–	–	–	5.3	1.4	13.3	4	-4.9	25	2.7	4.6	3.3	3.5	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.0	7.0	7.9
XII	–	–	–	–	-2.0	-7.0	4.7	12	-18.6	23	-4.7	-3.2	-4.6	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.6	6.6	7.0
Rok	–	–	–	–	10.1	3.0	28.1	16.VI	-18.6	15.III, 23.XII	5.3	9.0	6.0	6.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.9	6.5	7.0

Giżycko $\varphi = 54°03'$ $\lambda = 21°46'$

I	–	–	–	–	0.9	-2.9	6.0	23	-18.7	31	-1.3	0.0	-1.0	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.6	8.0	8.7
II	–	–	–	–	-1.3	-6.8	3.1	13	-15.9	1	-4.9	-2.7	-3.6	-3.7	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.2	6.8	7.7
III	–	–	–	–	-0.4	-7.4	7.0	31	-16.7	1	-6.1	-1.4	-3.6	-3.7	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.2	5.4	6.2
IV	–	–	–	–	12.8	4.2	26.3	23	-1.5	8	5.8	11.3	7.9	8.2	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.2	4.6	5.9
V	–	–	–	–	13.8	6.0	18.7	13	-1.5	1	8.1	12.4	9.3	9.8	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.7	7.9	8.2
VI	–	–	–	–	18.0	9.0	27.5	16	4.3	2	12.2	16.5	12.8	13.6	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.2	6.2	6.0
VII	–	–	–	–	19.1	11.1	26.0	21	7.0	4	13.4	17.6	14.2	14.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.0	6.2	6.8
VIII	–	–	–	–	19.3	11.9	25.3	12	5.7	15	13.7	18.0	14.5	15.2	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.3	5.8	6.9
IX	–	–	–	–	15.3	8.3	23.5	4	3.1	25	9.6	14.2	11.1	11.5	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.6	4.9	6.5
X	–	–	–	–	11.3	5.3	17.8	2,3	-1.5	28	6.4	10.4	7.8	8.1	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.1	5.8	6.9
XI	–	–	–	–	4.9	1.1	12.1	4	-4.3	26	2.1	4.0	2.8	2.9	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.4	7.3	8.2
XII	–	–	–	–	-3.1	-8.0	4.0	5	-23.4	23	-5.8	-4.2	-5.7	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.6	7.4	7.6
Rok	–	–	–	–	9.2	2.6	27.5	16.VI	-23.4	23.XII	4.4	8.0	5.5	5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.3	6.6	7.1

Tczew — $H_s = 10m$ — $h_w = 16m$ — 1962

Miesiąc	Rozkład wiatru (%) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	> 15	●	●	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	▬	▩	π/10
I	25	5.2	4.5	3.8	5	3.2	2	2.5	23	20	35.5	38	6.5	4.2	13	28	4	3.2	21	39	12	2	3	15		3	·	-	-	13	7	·	2	3	·
II	7	10.6	12	9.1	9	4.2	15	17	15.5	27	17.5	54	6.5	7.3	11	8.1	4	5.9	23	61	12	2	11	22	·	9	5	4	10	15	6	·	1	9	·
III	9.5	9.3	10	5.7	25	16	13.5	3.6	21	2.2	3	18	7.5	3.5	8	5.2	18	3.4	22	43	6	2	7	29	·	5	4	9	10	10	7	·	5	12	·
IV	16.5	4.8	8.5	4.1	5	4.0	3.5	3.7	17	2.0	11.5	3.3	8	2.4	10	3.7	10	3.1	30	116	5	·	·	1	2	2	·	6	7	13	6	1	4	·	1
V	16	5.8	7.5	3.0	1	2.0	8	2.2	6	1.8	12.5	2.7	7	2.5	13	2.3	22	2.5	96	26.5	14	·	·	1	·	2	2	2	11	20	13	3	3	·	4
VI	1.5	6.7	7	3.9	·	·	2	1.0	4.5	2.3	16.5	3.4	17.5	4.1	16.5	3.0	11	3.5	59	19.9	16	·	·	·	4	3	3	7	5	13	10	1	·	·	4
VII	11.5	2.4	13.5	2.3	1.5	2.0	4	2.1	19.5	1.5	13.5	3.1	11.5	2.8	10	2.7	8	2.2	78	16.2	12	·	·	·	3	·	·	5	7	20	15	4	·	·	·
VIII	0.5	1.0	4.5	2.8	4	2.2	8	2.2	10.5	1.9	3.4	3.6	13.5	2.5	6	3.2	12	2.5	57	13.5	7	·	·	·	2	·	·	3	11	16	14	2	·	·	2
IX	3	1.3	·	·	10	1.7	3	2.3	14	1.8	14.5	3.1	25.5	3.5	10	2.8	10	2.4	57	19.8	18	·	·	·	1	·	·	6	9	13	12	1	3	·	1
X	4.5	2.3	1	3.0	2	1.0	2	1.0	21.5	1.5	17.5	2.7	12.5	2.5	10	2.4	22	1.6	15	8.8	31	·	·	1	·	·	·	2	8	9	4	·	3	·	·
XI	4	2.0	2	7.2	9.5	4.6	16.5	4.3	17	1.9	12	1.6	11.5	2.3	3.5	3.3	14	2.5	32	9.5	1	·	·	6	·	1	·	1	18	15	8	·	4	·	·
XII	1.5	1.0	6.5	1.9	4.5	1.0	8.5	1.8	19.5	2.4	1.9	2.6	9.5	2.9	9	2.2	15	1.9	17	5.2	13	9	15	25				5	11	11	5		2	1.6	
Rok	91.5	4.4	7.7	3.9	5.4	2.3	72.5	2.4	189	2.0	207	3.1	13.7	3.4	120	3.5	147	2.9	507	26.5	14.V	15	36	100	12	25	14	-	-	168	107	12	27	40	12

Rosnowo — $H_s = 62m$ — $h_w = 12m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	> 15	●	●	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	▬	▩	π/10
I	4	6.0	4	2.0	1.5	1.7	9	2.6	19	3.4	3.0	5.3	13.5	5.5	3	2.2	9	3.9	6.5	8.1	23	2	3	12		3	·	2	22	25	15		3	11	·
II	5.5	3.5	7.5	4.2	8	3.6	4	1.8	7.5	4.3	12	4.4	18	8.7	9.5	5.5	12	4.5	6.0	17.1	12	2	7	22	·	6	2	1	13	21	10	2	1	18	·
III	6.5	3.7	7	2.4	5	2.0	2.0	4.2	·	·	3	2.3	9	3.0	3.5	3.1	3.9	2.0	3.9	9.9	12	7	4	28	·	1	·	5	13	16	10	·	3	2.0	
IV	4	2.2	7	3.3	8	4.5	5	2.2	4	3.5	9.5	4.3	10.5	4.4	11	2.5	3.1	2.3	4.5	7.8	16		·	4	1	·	·	3	9	14	10	·	4	·	1
V	4	2.2	1	2.0	2	2.5	8	3.1	8	1.5	1.0	2.4	8.5	2.9	15.5	2.5	3.6	1.5	13.3	12.4	14	·	·	4	·	·	·	1	12	24	23	3	2	·	2
VI	9	3.9	·	·	·	·	2	1.5	2	3.5	1.5	3.4	2.7	4.0	3	4.3	3.2	2.4	8.3	20.2	27	·	·	·	3	·	·	6	6	13	10	2	·	·	2
VII	1.5	2.0	2	2.0	1	2.0	2	2.0	3	3.3	20.5	2.5	10.5	2.8	9.5	2.7	4.3	1.4	7.4	8.6	4	·	·	·	2	·	·	3	11	17	17	·	5	·	2
VIII	1	3.0	·	·	2.5	2.2	4	3.0	2.5	2.6	30.5	3.7	12.5	3.8	5	2.6	3.5	2.2	12.9	28.7	7	·	·	·	1	·	·	2	16	20	18	3	3	·	1
IX	1	1.0	·	·	3.5	2.9	6	2.9	7.5	2.3	13.5	4.1	11	5.3	6.5	4.5	4.1	2.1	5.5	12.4	12	·	·	·	1	1	·	7	7	15	12	1	2	·	1
X	1	3.0		·	·	·	1.0	1.8	1.0	1.6	10.5	1.7	8.5	2.0			5.3	0.8	2.7	10.5	4	·	·	5		·	·	7	10	11	6	1	6	·	2
XI	1	1.0	1.5	3.7	25.5	4.8	1.4	2.4	8	1.4	2	2.0	1.0	4.0		·	2.8	2.4	4.3	8.1	1	·	·	7		·	·	2	17	14	8	·	3	5	·
XII	1	1.0	2	1.0	4.5	1.1	2.5	2.0	1.6	2.2	10.5	3.6	5.5	5.1	1	1.0	5.0	1.2	3.0	9.3	11	8	15	27	·	·	·	7	13	14	7	·	4	9	·
Rok	39.5	2.7	3.2	1.7	61.5	2.3	86.5	2.5	87.5	2.5	16.7	3.3	144.5	4.3	67.5	2.6	40.9	2.2	78.3	28.7	7.VIII	19	29	109	8	11	2	46	149	204	146	12	36	63	11

Stare Pole — $H_s = 3m$ — $h_w = 11.5m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	> 15	●	●	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	▬	▩	π/10
I	2	4.0	6	6.3	4	1.8	5	2.0	1.8	3.0	3.3	6.8	1.8	5.4	5	5.2	2	5.1	25	5.1	12	2	3	16	·	6	3	2	20	18	7	·	·	2	-
II	5	6.2	9	5.2	11	3.7	3	4.0	12	3.4	18	6.7	13	7.6	13	9.8		6.2	25	5.1	12	2	10	23	·	9	3	1	15	14	9	·	-	-	-
III	1.6	5.8	7	3.7	7	1.9	11	3.1	12	1.7	19	2.4	7	3.3	2	8.0	12	2.9	26	9.7	12	8	12	30	·	3	1	4	10	12	8	·	-	2.3	-
IV	1.5	6.3	5	2.4	8	5.9	5	3.0	12	6.2	13	4.5	3	3.0	13	7.0	16	4.4	19	6.7	5	·	·	1	2	10	1	3	10	14	5		2	·	-
V	11	6.3	10	2.7	5	1.8	2	1.5	16	2.1	15	4.0	13	3.0	12	5.8	9	3.3	120	27.8	14	·	·	3	·	4	2	2	13	20	14	3	4	·	-
VI	2.2	8.0	5	1.6	4	1.0	1	2.0	8	2.6	16	5.0	18	5.4	11	4.2	5	4.8	9.4	40.1	16	·	·	·	4	10	2	6	7	13	11	3	·	·	-
VII	2.2	3.0	4	2.0	3	1.3	1	1.0	11	2.6	15	4.3	15	3.8	12	4.8	10	3.1	77	15.3	26	·	·	·	3	4	·	3	11	16	14	2	4	·	-
VIII	2	2.5	2	1.5	4	1.8	9	1.7	5	3.8	3.9	4.8	1.7	4.4	7	5.0	8	3.7	68	13.0	7		·	·	1	8	2	2	9	15	12	2	1	·	-
IX	3	4.0	5	1.2	11	2.5	2	1.5	15	2.1	17	6.7	21	4.4	8	7.6	8	3.9	76	24.8	18		·	·	1	8	1	3	12	14	11	2	6	·	-
X	9	4.8	·	·	4	1.2	5	1.0	14	2.6	2.4	2.8	1.5	5.3	11	3.6	11	3.0	30	15.0	5		·	1	·	4	1	2	15	11	7	1	1.5		-
XI	7	7.0	9	6.7	12	5.1	11	7.5	19	2.2	22	4.4	5	5.2	3	5.7	2	4.8	41	7.2	20	·	·	10	·	8	1	2	18	15	11		10	·	-
XII	·	·	9	1.1	13	1.7	6	1.0	8	2.9	3.2	3.2	8	3.5	5	2.4	12	2.2	22	11.2	1	11	15	26	·	·	·	3	15	6	5	1	3	1.3	-
Rok	11.4	4.8	7.1	2.9	8.6	2.5	6.1	2.4	15.0	2.9	26.3	4.6	15.3	4.5	10.2	5.8	9.5	4.0	62.3	40.1	16.VI	23	40	110	11	7.4	1.7	33	155	168	114	14	-	-	-

Giżycko — $H_s = 132m$ — $h_w = 12.5m$ I–VII, $13m$ VIII–XII

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	> 15	●	●	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	▬	▩	π/10
I	3	7.7	2	4.0	2	1.5	4	2.5	2.9	3.4	2.7	3.9	1.6	3.1	4	2.7	6	3.3	1.5	3.0	6.20	3	4	20	·	·	·	2	22	17	6	·	1	1.7	
II	4.1	7.5	5	6.2	12	3.0	1.4	2.6	1.5	5.5	7	7.6	10	5.4	7	6.1	3	5.0	20	4.5	12	7	16	27	·	5	3	1	14	15	7		3	2.8	·
III	1.1	5.0	10	2.3	12	2.0	3.2	2.7	3	1.7	4	1.2	2	4.0	10	3.6	9	2.6	2.6	7.6	12	7	17	29	·	·	·	3	11	12	6	·		3.1	
IV	7	3.1	7	3.1	5	3.6	2.1	3.1	8	3.4	8	2.2	4	2.0	2.0	3.4	1.0	2.8	2.4	6.6	1		·	2	1	·	·	3	8	9	6	·	2	2	2
V	8	1.9	4	2.8	2	1.5	1.2	2.1	1.0	2.3	1.3	2.6	7	2.9	2.5	3.8	1.2	2.4	6.9	11.6	14	·	·	2	·	·	·	·	2.0	19	15	2	4	·	2
VI	1.2	6.1	1	1.0	·	·	5	1.0	5	2.0	2.4	2.9	1.3	2.9	1.8	3.8	1.2	2.9	3.7	5.6	12	·	·	·	1	1	·	2	8	13	9	·	·	·	4
VII	1.1	2.3	1	1.0	1	1.0	6	1.7	1.1	2.8	1.1	3.7	1.4	3.4	2.3	2.7	1.5	2.3	9.0	31.0	13	·	·	·	2	·	·	·	11	16	13	3	1	·	8
VIII	3	3.0	·	·	2	1.0	6	1.5	8	2.8	4.0	3.5	1.4	2.0	7	1.1	1.3	2.3	11.2	27.0	17	·	·	·	2	·	·	1	8	18	17	2	·	·	9
IX	4	4.0	4	1.8	4	1.2	8	2.6	7	1.7	2.6	3.7	1.8	3.9	9	4.1	1.0	3.0	7.2	22.8	18	·	·	·	·	·	·	1	11	14	13	1	1	·	3
X	4	2.0	1	1.0	5	1.6	2.1	2.6	8	2.5	1.3	2.8	1.3	2.9	9	2.9	1.9	2.0	1.1	5.0	28	·	·	1	·	·	·	3	16	8	4	·	4	·	·
XI	5	2.2	·	·	2.6	6.6	2.0	3.4	7	2.6	1.0	2.5	1.0	1.5	4	2.0	8	3.5	3.8	14.0	20	·	1	12	·	1	·	2	19	10	6	1	5	1	·
XII	1.2	1.3	1.1	1.9	5	1.4	7	1.6	1.7	3.6	9	3.0	1.7	2.4	6	1.8	9	2.1	9	2.0	11	1.1	1.6	25	·	·	·	4	20	11	5	·	3	1.7	·
Rok	3.1	3.8	4.6	2.1	7.6	2.0	1.5.6	2.3	1.2.8	2.9	1.9.2	3.3	1.3.8	3.0	1.4.2	3.2	1.2.6	2.8	5.2.3	31.0	13.VII	28	54	118	6	7	3	22	168	162	107	9	24	96	28

Olecko $\varphi = 54°03'$ $\lambda = 22°30'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	990.8	1018.9	967.1	1013.2	0.2	-3.4	5.0	22	-19.7	31	-1.8	-0.6	-1.6	-1.4	5.2	5.4	5.1	5.2	9.2	8.9	8.9	9.0	0.5	0.7	0.6	0.6	8.7	8.3	7.6	8.2
II	991.0	1013.2	950.5	1013.7	-1.8	-7.7	2.7	12	-16.7	1	-5.5	-3.4	-4.4	-4.4	4.0	4.2	4.1	4.1	9.5	8.7	8.9	9.0	0.2	0.6	0.5	0.4	8.9	7.4	7.0	7.8
III	988.8	1007.5	968.3	1011.5	-0.9	-8.1	5.7	31	-17.1	1	-6.6	-2.1	-4.1	-4.2	3.6	4.0	4.0	3.9	9.3	7.5	8.2	8.3	0.3	1.3	0.8	0.8	7.8	6.7	6.3	6.9
IV	992.4	1009.6	970.4	1014.1	12.9	4.2	24.7	23	-2.3	8	5.8	11.5	8.0	8.3	8.4	9.1	9.2	8.9	8.9	6.8	8.3	8.0	1.1	5.6	2.2	3.0	7.7	7.1	7.0	7.3
V	990.3	998.8	969.5	1011.8	13.7	5.8	19.1	20	-1.6	1	8.2	12.1	9.3	9.7	9.9	9.6	9.9	9.8	9.0	6.8	8.3	8.0	1.2	4.9	2.1	2.7	8.3	8.5	7.5	8.1
VI	994.9	1006.5	982.3	1016.2	17.7	8.3	25.9	16	3.4	10	12.0	16.0	12.6	13.3	11.0	10.6	10.7	10.8	7.7	5.9	7.2	6.9	3.4	8.0	4.3	5.2	6.7	7.0	6.4	6.7
VII	994.6	1001.4	977.4	1012.7	19.3	9.8	26.7	21	6.2	4	13.3	17.5	13.9	14.6	13.5	13.1	13.4	13.3	8.8	6.7	8.4	8.0	1.9	7.2	2.7	3.9	7.5	7.8	6.4	7.2
VIII	992.2	1002.1	981.2	1013.3	19.2	11.1	25.3	7	5.0	15	13.3	17.7	14.2	14.8	13.9	13.6	14.3	13.9	9.0	6.7	8.7	8.1	1.6	7.1	2.1	3.6	7.6	7.4	7.1	7.4
IX	992.8	1010.9	973.5	1014.2	14.9	7.4	24.3	5	1.0	25	8.9	13.7	10.7	11.0	10.9	11.6	11.7	11.4	9.5	7.4	9.0	8.6	0.6	4.5	1.3	2.1	7.3	7.7	6.6	7.2
X	993.7	1015.1	982.6	1021.6	11.0	4.2	17.5	3	-1.6	16,28	5.6	10.1	7.2	7.5	8.9	10.2	9.6	9.6	9.5	8.1	9.3	9.0	0.4	2.5	0.7	1.2	8.1	7.8	6.7	7.5
XI	997.1	1009.8	979.7	1019.3	5.0	0.9	12.9	2	-5.1	26	2.0	3.9	2.8	2.9	6.9	7.2	7.0	7.0	9.5	8.6	9.0	9.0	0.3	1.2	0.7	0.7	8.9	8.1	8.0	8.3
XII	993.5	1026.2	955.1	1016.4	-3.3	-7.9	3.3	5	-20.6	23	-5.6	-4.3	-5.8	-5.4	4.2	4.3	4.1	4.2	9.3	8.7	9.3	9.1	0.3	0.7	0.3	0.4	8.3	8.1	7.6	8.0
Rok	992.9	1026.2	950.5	1014.7	9.0	2.0	26.7	21.VII	-20.6	23.XII	4.1	7.7	5.2	5.6	8.4	8.6	8.6	8.5	9.1	7.6	8.6	8.4	1.0	3.7	1.5	2.1	8.0	7.7	7.0	7.6

Malbork $\varphi = 54°02'$ $\lambda = 19°02'$

I	-	-	-	-	2.6	-1.8	8.4	22	-19.3	31	0.4	1.4	0.1	0.5	-	-	-	-	-	-	-	-	-	-	-	-	9.2	7.8	7.9	8.3
II	-	-	-	-	0.8	-4.2	4.8	12,20	-14.2	1	-2.7	-0.5	-1.5	-1.6	-	-	-	-	-	-	-	-	-	-	-	-	8.3	7.9	7.8	8.0
III	-	-	-	-	1.2	-6.6	9.4	31	-14.5	2,15	-4.9	0.1	-2.7	-2.6	-	-	-	-	-	-	-	-	-	-	-	-	7.2	7.1	4.1	6.1
IV	-	-	-	-	13.8	4.5	27.0	21	0.1	1,30	6.3	12.3	7.2	8.2	-	-	-	-	-	-	-	-	-	-	-	-	6.4	6.3	5.7	6.1
V	-	-	-	-	14.5	6.1	19.6	8	-0.9	6	8.4	12.8	9.1	9.8	-	-	-	-	-	-	-	-	-	-	-	-	7.1	8.5	6.8	7.5
VI	-	-	-	-	18.9	9.0	28.2	16	3.6	2,3	12.8	16.8	13.0	13.9	-	-	-	-	-	-	-	-	-	-	-	-	5.6	6.5	6.1	6.1
VII	-	-	-	-	20.4	10.5	27.5	21	7.1	30	14.0	19.0	14.2	15.4	-	-	-	-	-	-	-	-	-	-	-	-	6.0	6.9	6.9	6.6
VIII	-	-	-	-	20.3	11.9	27.5	12	7.6	15	13.9	18.7	14.5	15.4	-	-	-	-	-	-	-	-	-	-	-	-	7.1	7.9	6.2	7.1
IX	-	-	-	-	17.0	8.4	26.6	4	3.1	25	10.0	15.6	11.0	11.9	-	-	-	-	-	-	-	-	-	-	-	-	5.8	7.4	5.7	6.3
X	-	-	-	-	12.8	4.8	21.0	1	-2.1	28	6.6	11.7	7.9	8.5	-	-	-	-	-	-	-	-	-	-	-	-	7.4	7.5	6.1	7.0
XI	-	-	-	-	5.5	1.6	12.7	5	-4.4	25	2.7	4.3	3.3	3.4	-	-	-	-	-	-	-	-	-	-	-	-	8.6	8.8	7.0	8.1
XII	-	-	-	-	-1.6	-6.6	5.3	12	-18.3	23,24	-4.7	-3.1	-4.5	-4.2	-	-	-	-	-	-	-	-	-	-	-	-	7.8	7.6	6.7	7.4
Rok	-	-	-	-	10.5	3.1	28.2	16.VI	-19.3	31.I	5.2	9.1	6.0	6.6	-	-	-	-	-	-	-	-	-	-	-	-	7.2	7.5	6.4	7.0

Dziwnów $\varphi = 54°01'$ $\lambda = 14°44'$

I	1010.9	1040.9	980.4	1011.8	3.7	0.2	7.9	22	-13.0	31	1.4	2.4	1.7	1.8	6.3	6.3	6.3	6.3	9.1	8.6	8.8	8.8	0.7	1.1	0.8	0.8	7.7	8.1	6.9	7.6
II	1014.0	1039.6	974.5	1014.9	2.4	-1.9	7.6	12	-11.9	1	-0.4	0.9	0.4	0.3	5.3	5.6	5.4	5.4	8.8	8.5	8.4	8.6	0.7	1.0	1.1	0.9	7.9	7.6	5.7	7.1
III	1010.1	1026.8	979.7	1011.0	2.9	-2.1	12.7	30	-6.2	16	-1.1	1.8	0.4	0.4	5.1	5.3	5.4	5.3	8.7	7.6	8.4	8.2	0.7	1.8	1.0	1.2	7.3	6.9	6.2	6.8
IV	1011.9	1028.3	985.5	1012.7	10.0	3.9	19.1	25	1.3	1	5.4	7.0	6.3	6.2	8.1	8.3	8.4	8.3	9.0	8.3	8.7	8.7	0.9	1.9	1.3	1.4	6.8	6.4	6.7	6.6
V	1010.8	1016.6	1004.1	1011.6	12.6	7.2	20.4	19	1.3	5	9.3	10.9	9.5	9.8	10.1	9.8	10.1	10.0	8.5	7.6	8.4	8.2	1.8	3.5	2.0	2.4	6.5	7.6	7.4	7.2
VI	1016.9	1034.0	1003.2	1017.7	17.3	11.5	28.1	19	5.7	1	13.3	15.6	14.1	14.3	12.2	12.5	12.2	12.3	7.9	7.0	7.4	7.4	3.4	5.9	4.2	4.5	5.4	5.5	5.5	5.5
VII	1012.4	1023.3	990.4	1013.2	18.0	12.6	26.2	21	9.0	5	14.7	16.5	14.7	15.2	14.6	14.2	14.8	14.5	8.7	7.6	8.8	8.4	2.3	4.8	2.0	3.0	6.2	5.9	4.8	5.6
VIII	1012.0	1021.1	1000.1	1012.8	18.7	13.3	28.1	12	10.7	10	14.6	17.4	15.3	15.6	14.1	14.7	14.8	14.5	8.5	7.4	8.5	8.1	2.5	5.4	2.7	3.5	7.5	7.4	6.8	6.9
IX	1013.1	1027.5	990.4	1013.9	16.2	10.2	23.3	4	5.9	25	11.5	15.2	12.8	13.1	12.1	12.6	12.3	12.3	8.9	7.3	8.3	8.2	1.6	4.9	2.6	3.0	6.6	5.8	4.0	5.5
X	1019.6	1034.8	1005.1	1020.4	13.1	7.0	22.8	2	2.2	30	8.3	11.9	9.8	10.0	10.2	11.5	11.1	10.9	9.2	8.1	8.9	8.7	0.9	3.0	1.3	1.7	7.6	6.5	4.5	6.2
XI	1014.7	1031.8	996.3	1015.6	6.1	2.2	13.7	8	-2.7	24,25	3.3	5.0	3.7	3.9	7.2	7.7	7.3	7.4	9.2	8.7	9.0	9.0	0.7	1.4	0.9	1.0	7.9	8.0	6.5	7.5
XII	1014.5	1048.8	967.8	1015.4	0.0	-4.4	5.6	12	-15.0	22	-2.6	-1.6	-2.3	-2.2	4.8	5.0	4.9	4.9	9.0	8.8	9.0	8.9	0.5	0.7	0.5	0.6	8.1	7.3	5.9	7.1
Rok	1013.4	1048.8	967.8	1014.2	10.1	5.0	28.1	19.VI,12.VIII	-15.0	22.XII	6.5	8.6	7.2	7.4	9.2	9.5	9.4	9.4	8.8	8.0	8.6	8.5	1.4	3.0	1.7	2.0	7.1	6.9	5.9	6.6

Piaszczyna $\varphi = 54°01'$ $\lambda = 17°10'$

I	-	-	-	-	1.5	-1.8	7.2	22	-16.5	31	0.0	0.6	-0.2	0.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	-0.1	-4.8	4.1	12	-17.2	1	-3.2	-1.2	-2.0	-2.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	1.0	-7.9	7.7	31	-14.8	15	-5.6	-0.1	-3.3	-3.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	12.8	2.8	25.5	21	-1.7	1,31	5.0	11.5	6.9	7.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	12.8	4.3	18.5	19	-2.6	1	7.1	11.2	7.8	8.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	-	-	-	18.0	7.2	26.5	15,16	0.8	3	11.3	16.1	12.0	12.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	-	-	-	19.2	8.5	26.5	21,26	4.7	9	12.5	17.7	13.6	14.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	-	-	-	18.7	9.9	27.5	12	4.7	14	11.9	17.0	13.6	14.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	-	-	-	15.5	6.3	26.5	4	1.3	18	8.9	14.5	10.0	10.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	-	-	-	11.8	3.1	22.0	3	-2.6	28	5.5	11.0	7.4	7.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	4.4	0.3	10.9	5	-4.6	24	1.9	3.8	2.6	2.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-	-	-	-2.0	-8.6	4.1	4	-19.9	22	-4.9	-3.2	-5.2	-4.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Rok	-	-	-	-	9.5	1.6	27.5	12.VIII	-19.9	22.XII	4.2	8.2	5.3	5.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Olecko $H_s = 181m$ $H_b = 177{,}7m$ $h_w = 13m$ 1962

MIESIĄC	ROZKŁAD WIATRU °D, °mD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>20°	Wiatr v ≥10	≥15	●	●	Opad R ≥0.1	≥1.0	≥10.0	▬	▦	▦
I	1	7.0	6	4.8	2.5	2.8	7	4.1	17.5	5.6	36.5	5.3	16.5	6.2	6	5.3	·	5.4	22	4.3	20	3	9	22	·	4	·	2	24	20	7	·	5	24	·
II	7	7.1	4.5	7.6	9	4.8	10	5.0	17	6.0	12	6.9	11	7.0	12.5	7.8	1	6.4	28	12.5	12	8	16	28	·	10	1	·	15	13	11	1	2	28	·
III	5	8.4	11.5	4.2	13.5	3.3	19.5	4.3	15.5	3.8	6	2.8	10.5	4.1	10.5	7.3	1	4.4	36	8.5	5	11	19	29	·	6	1	1	12	13	7	·	3	31	·
IV	11	3.5	5	7.2	10	4.0	16.5	4.3	14.5	4.5	11	4.4	10	4.4	12	6.2	·	4.6	40	9.7	5	·	·	5	·	5	·	2	13	14	9	·	1	2	2
V	12	2.8	2	5.0	5	2.8	7	3.3	11	3.8	16.5	3.2	21.5	4.0	17	4.1	1	3.5	93	18.6	20	·	·	3	·	1	·	·	17	23	15	3	·	·	2
VI	13	6.4	4	8.5	2	2.0	5	5.9	6	2.8	14	3.9	28	4.3	18	3.8	·	4.4	42	9.7	11	·	·	·	1	4	·	·	7	13	11	·	·	·	4
VII	8	3.5	·	·	1	3.0	2	3.0	13	4.2	10.5	3.6	37.5	3.5	21	3.8	·	3.7	55	10.9	27	·	·	·	2	1	·	·	12	17	10	1	·	·	3
VIII	4.5	3.8	2	2.5	4	1.8	4.5	3.6	8.5	4.5	29	4.9	32.5	4.0	7	2.6	1	4.0	119	16.0	17	·	·	·	1	1	·	·	14	19	16	5	1	·	3
IX	3	4.0	4.5	2.5	8.5	2.5	8	3.2	7	4.4	23	5.6	24.5	4.9	11.5	3.3	·	4.3	89	15.9	18	·	·	·	·	3	·	1	13	20	16	1	4	·	4
X	1.5	3.3	2	2.0	1	1.0	16.5	2.9	10.5	4.1	17.5	4.1	22.5	3.8	19.5	3.7	2	3.7	12	7.0	28	·	·	3	·	2	·	2	18	14	3	·	5	·	·
XI	3	4.7	1	9.0	17	6.0	27	5.0	10.5	3.0	16.5	3.9	9.5	4.0	4.5	3.5	1	4.6	42	14.1	15	·	3	16	·	2	·	1	23	18	8	1	10	·	·
XII	10	3.1	18.5	3.3	3.5	2.7	4	2.8	20	4.6	16	5.9	12.5	5.8	8.5	3.8	·	4.3	15	2.7	11	11	17	28	·	5	·	3	23	17	6	·	1	18	·
Rok	79	4.8	61	4.7	77	3.1	127	4.0	151	4.3	208.5	4.5	236.5	4.7	148	4.6	7	4.4	593	18.6	20.V	33	64	134	4	44	2	12	191	201	119	12	32	103	18

Malbork $H_s = 20m$ $h_w = 11m$

I	4	2.5	2	4.5	2	2.0	9	5.2	44	6.5	1	1.0	18	4.6	2	3.0	11	4.8	22	4.0	12,25,28	2	3	18	·	2	·	2	22	12	7	·	·	–	·
II	10	4.7	2	4.0	11	4.4	3	5.7	23	6.2	2	6.0	14	6.1	6	7.7	13	4.6	29	8.0	15	3	10	23	·	2	·	2	18	9	7	·	·	–	·
III	15	4.1	1	1.0	7	5.1	14	4.6	17	3.4	4	2.8	3	3.0	3	6.0	29	2.8	44	18.0	12	9	7	30	·	·	·	4	8	9	8	1	·	–	·
IV	20	4.4	·	·	8	3.1	8	6.1	25	4.6	·	·	6	5.3	3	4.3	20	3.6	26	9.0	5	·	·	·	2	·	·	3	11	10	8	·	2	–	·
V	14	3.6	4	2.0	4	4.0	8	4.1	18	4.2	4	2.2	9	2.8	6	6.3	26	2.7	141	54.0	14	·	·	2	·	·	·	1	15	20	18	4	2	·	8
VI	12	5.2	2	3.5	1	5.0	5	3.6	12	3.8	6	3.8	15	4.6	12	4.6	25	3.2	109	60.0	16	·	·	·	4	·	·	2	7	10	9	3	·	·	4
VII	7	4.3	2	2.0	4	2.5	2	5.5	15	5.3	2	2.0	14	4.1	5	4.2	42	2.3	77	13.0	26	·	·	·	3	·	·	3	12	17	14	3	·	·	8
VIII	2	4.0	·	·	5	3.2	7	5.6	23	5.0	8	4.6	13	4.8	8	3.8	27	3.3	81	25.0	7	·	·	·	1	1	·	·	15	14	12	2	·	·	5
IX	2	4.0	·	·	7	3.1	6	4.5	18	5.5	5	4.4	15	4.3	5	5.0	32	3.0	68	20.0	18	·	·	·	1	1	·	2	11	14	13	2	·	·	2
X	2	4.0	·	·	·	·	14	4.1	23	3.7	3	3.0	9	4.8	·	·	42	2.2	30	13.0	5	·	·	4	·	·	·	3	14	7	7	1	4	·	·
XI	1	1.0	1	1.0	21	4.9	7	5.3	31	3.9	1	1.0	5	4.4	·	·	23	3.3	53	14.0	30	·	·	7	·	·	·	2	18	12	12	1	4	–	·
XII	1	1.0	3	1.3	3	2.3	7	3.6	25	5.1	3	4.7	8	3.8	·	·	43	2.2	46	6.0	13	9	15	25	·	·	·	3	17	8	8	·	1	–	·
Rok	90	3.6	17	1.6	73	3.3	90	4.8	274	4.8	39	3.0	129	4.4	50	3.7	333	3.2	696	60.0	16.VI	23	35	109	11	6	·	27	168	142	123	17	13	–	27

Dziwnów $H_s = 7m$ $H_b = 7{,}1m$ $h_w = 18m$

I	4.5	11.8	2	9.5	4	2.5	4.5	3.3	34	4.9	29	7.1	9.5	7.5	5.5	7.4	·	6.2	39	7.9	25	1	3	11	·	8	1	2	15	20	13	·	3	2	·
II	7	11.9	10.5	10.0	10.5	6.4	2	4.5	17.5	4.2	10	6.2	18	10.8	8.5	12.5	·	8.3	44	12.4	12	1	6	19	·	16	3	3	13	15	8	1	2	14	·
III	12	5.5	11.5	7.2	10.5	3.7	21.5	3.3	15	3.2	4.5	3.8	9	4.2	8	7.6	1	4.6	24	5.9	31	·	3	27	·	5	·	3	10	11	7	·	2	12	·
IV	8.5	6.0	25.5	7.9	3	4.7	4.5	2.7	17.5	4.4	9.5	5.4	11.5	4.4	10	5.8	·	5.7	39	10.7	16	·	·	·	·	7	2	3	9	18	11	1	8	·	1
V	5.5	8.5	12.5	4.7	3.5	3.0	10	3.6	9.5	4.5	24	3.8	16	4.1	11	7.2	1	4.6	71	14.1	26	·	·	·	·	11	·	3	13	21	16	1	4	·	4
VI	8	6.5	7.5	7.5	2	4.2	3.5	3.7	8	3.2	12.5	4.8	27.5	8.7	17	6.0	4	6.2	71	15.4	15	·	·	·	2	11	3	4	4	14	12	3	·	·	5
VII	3	4.8	13	4.8	4	3.1	4.5	3.0	5.5	3.4	18.5	4.7	19	5.5	18.5	4.7	7	4.3	68	15.3	12	·	·	·	1	4	·	4	8	15	12	2	·	·	4
VIII	6.5	4.2	1	5.0	2.5	3.4	7.5	3.3	18	3.9	28	6.6	16.5	7.4	9	5.5	4	5.3	72	10.8	24	·	·	·	1	8	·	1	12	16	13	1	·	·	3
IX	3.5	3.6	2.5	4.2	8.5	2.9	11.5	3.5	18	4.1	11.5	5.1	16	9.5	14.5	8.5	4	5.5	35	14.2	4	·	·	·	·	11	·	3	1	11	10	1	1	·	2
X	4.5	4.7	4	6.5	3.5	3.0	15	2.8	30	3.9	11.5	4.9	6.5	7.8	11	7.1	7	4.3	16	4.9	26	·	·	·	·	3	·	4	10	6	4	·	7	·	1
XI	2	11.5	6	6.7	2.1	4.7	16.5	3.4	21.5	3.5	10	5.0	9.5	6.3	0.5	0.7	3	4.5	28	6.8	19	·	·	8	·	5	·	1	15	13	7	·	6	3	·
XII	4	6.5	2.5	2.6	14.5	3.4	12.5	2.4	34	4.0	14.5	5.4	6.5	7.5	1.5	5.7	3	4.1	32	6.5	11	5	16	24	·	4	·	1	13	14	8	·	7	16	·
Rok	69	7.1	98.5	6.4	87.5	3.8	113.5	3.3	228.5	3.9	183.5	5.2	165.5	7.0	115	6.6	34	5.3	539	15.4	15.VI	7	28	89	4	93	9	32	123	174	121	10	40	47	20

Piaszczyna $H_s = 175m$ $h_w = 12m$

I	5.5	6.1	3	4.3	1	9.0	4.5	3.7	24	4.9	16	4.2	23	5.4	8	5.7	8	4.6	–	–	–	2	6	14	·	5	1	–	–	–	–	–	–	17	–
II	11	7.4	8	6.4	9	2.8	2	3.0	8	4.6	13	5.1	20	8.2	10	8.0	3	6.1	–	–	–	3	11	26	·	9	4	–	–	–	–	–	6	21	–
III	6	8.8	6	4.7	7	3.1	17	6.0	5	4.0	8	2.9	2	1.5	10	5.4	32	3.3	–	–	–	12	9	30	·	5	1	–	–	–	–	–	4	31	–
IV	9	4.5	4	6.5	11	4.8	9	5.0	8	3.4	13	4.5	6	5.6	11	5.5	19	3.8	–	–	–	·	·	9	1	3	·	–	–	–	–	–	2	2	–
V	10	4.5	8	2.7	1	2.0	10	2.7	7	3.0	13	2.9	22	2.1	15	2.8	7	2.6	60	8.6	14	·	·	4	·	·	·	–	–	17	14	·	·	·	–
VI	10	5.1	3	5.3	·	·	3	5.3	3	2.0	2	2.5	28	4.1	28	3.3	13	3.3	54	7.2	28	·	·	·	3	4	·	–	–	16	14	·	·	·	–
VII	3	3.0	5	2.6	10	1.3	5	3.4	3	1.0	11	3.0	22	2.6	15	3.0	19	2.1	64	6.8	22	·	·	·	3	·	·	–	–	22	17	·	·	·	–
VIII	3	3.0	1	3.0	2	3.5	9	4.8	3	5.3	8	3.6	46	3.1	9	3.1	12	3.0	110	24.8	24	·	·	·	1	2	1	–	–	23	23	1	·	·	–
IX	·	·	5	1.8	5	2.6	20	2.6	6	2.7	13	3.8	20	2.4	13	4.3	8	2.7	64	8.6	6	·	·	·	1	1	·	–	–	18	16	·	5	·	–
X	·	·	2	1.0	·	·	18	2.6	11	2.5	10	3.5	19	1.5	25	2.9	8	2.3	40	8.8	5	·	·	8	·	1	·	–	–	11	11	·	7	·	–
XI	1	4.0	6	3.3	13	4.1	22	4.4	2	5.5	18	2.8	6	2.5	8	3.1	14	3.1	56	12.3	29	·	·	15	·	·	·	–	–	11	11	1	8	7	–
XII	2	2.5	8	1.5	5	2.0	26	2.3	8	3.1	27	2.2	8	3.2	6	2.2	3	2.3	–	–	–	14	17	31	·	·	·	–	–	–	–	–	5	21	–
Rok	60.6	4.1	59	3.6	64	2.9	145.5	3.8	88	3.5	152	3.4	222	3.5	158	4.1	146	3.3	–	–	–	31	43	137	9	30	7	–	–	–	–	–	–	99	–

Siejnik $\varphi = 54°01'$ $\lambda = 22°29'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{a.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.3	-3.4	5.0	22	-19.1	31	-1.9	-0.5	-2.0	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.9	8.6	8.4
II	–	–	–	–	-1.8	-7.5	2.0	12	-17.0	1	-5.2	-3.0	-3.9	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.0	9.2	8.1
III	–	–	–	–	-1.1	-8.5	5.8	31	-16.7	15	-6.4	-1.7	-4.6	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.3	7.5	6.8
IV	–	–	–	–	13.3	4.3	25.0	23	-2.0	8	6.7	12.0	7.9	8.6	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.3	7.0	6.6
V	–	–	–	–	14.3	5.7	19.9	27	-1.4	1	9.0	12.9	9.1	10.0	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.3	7.5	7.4
VI	–	–	–	–	18.5	8.3	27.1	16	3.8	13	12.6	16.8	12.2	13.4	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.5	4.9	5.3
VII	–	–	–	–	20.0	10.2	27.0	21	5.8	4	13.9	18.4	13.4	14.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.4	5.9	6.2
VIII	–	–	–	–	20.0	10.9	25.1	12	4.7	15	14.1	18.8	13.8	15.1	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.5	6.5	6.1
IX	–	–	–	–	15.4	7.4	24.3	5	1.3	25	9.3	14.3	10.6	11.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.8	7.0	6.8
X	–	–	–	–	11.5	4.1	17.9	3	-2.1	28	5.8	10.6	6.9	7.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.4	6.8	6.4
XI	–	–	–	–	5.0	0.8	12.8	2	-3.8	26	1.7	4.2	2.3	2.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.6	8.0	8.1
XII	–	–	–	–	-3.3	-8.0	3.2	5	-20.9	23	-6.1	-4.4	-5.9	-5.6	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.2	7.3	7.3
Rok	–	–	–	–	9.3	2.0	27.1	16.VI	-20.9	23.XII	4.5	8.2	5.0	5.7	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.7	7.2	7.0

Miastko $\varphi = 54°00'$ $\lambda = 16°58'$

I	–	–	–	–	2.0	-1.5	7.0	21,22	-16.1	30	0.4	1.2	0.0	0.4	5.9	5.7	5.7	5.8	91	83	89	88	0.6	1.1	0.6	0.8	9.7	8.7	8.2	8.9
II	–	–	–	–	0.5	-4.4	4.0	20	-16.7	1	-2.5	-0.2	-1.6	-1.5	4.7	5.1	5.0	4.9	88	82	89	86	0.6	1.0	0.6	0.7	9.1	8.0	8.6	8.6
III	–	–	–	–	1.5	-7.6	8.0	30	-15.9	15	-5.9	0.7	-3.6	-3.1	3.6	5.0	4.1	4.2	84	77	84	82	0.6	1.5	0.7	0.9	7.8	6.9	5.5	6.7
IV	–	–	–	–	13.1	3.2	25.5	21	-1.3	1	5.1	12.1	6.6	7.6	7.9	8.9	8.4	8.4	88	63	84	78	1.1	6.4	1.9	3.1	6.6	5.1	6.3	6.0
V	–	–	–	–	13.5	4.6	18.5	19	-4.1	2	7.3	11.6	8.3	8.9	9.4	9.3	9.9	9.5	91	68	89	83	0.9	4.7	1.3	2.3	7.0	8.1	7.2	7.4
VI	–	–	–	–	18.3	7.7	27.5	15	-0.5	3	11.7	16.4	12.4	13.2	11.4	11.1	11.5	11.3	81	60	78	73	2.7	8.3	3.4	4.8	6.5	5.6	5.2	5.8
VII	–	–	–	–	19.6	9.0	26.7	21	4.8	10	13.3	18.1	13.6	14.6	13.1	12.8	13.6	13.2	86	63	87	79	2.3	8.7	2.2	4.4	5.8	6.9	5.2	6.0
VIII	–	–	–	–	18.8	10.5	28.8	12	5.2	14	12.8	17.4	13.7	14.4	13.3	13.7	13.7	13.6	89	70	87	82	1.6	6.5	2.1	3.4	6.4	7.6	7.1	7.0
IX	–	–	–	–	16.1	7.2	26.7	4	1.2	18	9.3	15.0	10.0	11.1	11.0	11.5	11.2	11.2	93	68	90	84	0.8	6.0	1.2	2.7	6.0	6.0	4.6	5.5
X	–	–	–	–	12.3	3.8	21.0	3,4	-2.5	15	5.5	11.4	7.1	7.8	8.8	10.1	9.6	9.5	95	74	92	87	0.4	3.8	0.8	1.7	8.1	6.0	6.9	7.0
XI	–	–	–	–	4.6	0.9	12.0	5	-7.4	24	2.0	3.9	2.8	2.9	6.6	6.9	6.9	6.8	91	83	91	88	0.6	1.5	0.8	1.0	8.6	7.6	9.1	8.4
XII	–	–	–	–	-2.1	-8.0	3.9	12,13	-21.4	24	-5.2	-3.1	-5.5	-4.8	4.0	4.2	3.9	4.0	85	80	86	84	0.5	0.9	0.5	0.6	8.2	7.4	6.8	7.5
Rok	–	–	–	–	9.8	2.1	28.8	12.VIII	-21.4	24.XII	4.5	8.7	5.3	6.0	8.3	8.7	8.6	8.5	88	73	87	83	1.1	4.2	1.3	2.2	7.5	7.0	6.7	7.1

Radostowo $\varphi = 53°59'$ $\lambda = 18°45'$

I	–	–	–	–	2.2	-2.1	7.8	22	-22.7	31	0.0	1.3	0.0	0.3	5.5	5.6	5.3	5.5	86	80	83	83	0.9	1.4	1.1	1.1	8.8	8.1	8.5	8.5
II	–	–	–	–	0.7	-4.7	4.6	12	-19.1	1	-2.6	-0.5	-1.6	-1.6	4.5	4.9	4.7	4.7	86	82	84	84	0.8	1.1	0.9	0.9	8.4	8.0	7.6	8.0
III	–	–	–	–	0.7	-6.5	8.0	31	-17.4	15	-5.1	0.1	-2.9	-2.7	3.8	4.9	4.3	4.3	85	79	86	83	0.6	1.3	0.7	0.9	7.7	7.5	4.4	6.5
IV	–	–	–	–	13.3	3.9	27.2	23	-1.1	7	6.0	12.0	6.9	8.0	8.3	8.8	8.7	8.6	86	64	85	78	1.4	6.6	1.7	3.2	7.9	7.8	6.0	7.2
V	–	–	–	–	14.0	5.0	19.1	8	-2.7	2	8.4	12.8	8.6	9.6	9.9	9.5	9.6	9.7	87	64	85	79	1.3	5.5	1.7	2.8	7.8	9.2	7.5	8.2
VI	–	–	–	–	18.6	8.4	28.0	16	2.9	2	12.8	16.9	12.5	13.7	11.7	11.2	12.0	11.6	77	58	81	72	3.5	8.7	2.9	5.0	6.8	7.3	7.4	7.2
VII	–	–	–	–	20.0	10.0	27.4	21	5.9	5,30	14.0	18.8	13.7	15.0	13.8	13.0	13.7	13.5	86	60	87	78	2.3	9.2	2.1	4.5	6.5	7.0	6.8	6.8
VIII	–	–	–	–	19.9	11.1	26.6	12	6.2	10	13.7	18.7	14.2	15.2	13.9	14.2	14.3	14.1	88	66	88	81	1.9	7.6	1.9	3.8	7.5	7.4	6.5	7.1
IX	–	–	–	–	16.5	7.7	26.4	4	2.2	16,25	9.8	15.6	10.7	11.7	11.2	12.0	11.5	11.6	92	68	89	83	1.1	6.1	1.5	2.9	6.9	7.8	5.6	6.8
X	–	–	–	–	12.4	4.1	19.8	3,4	-3.8	28	6.0	11.5	7.5	8.1	9.0	11.0	9.7	9.9	93	78	91	87	0.7	3.0	1.1	1.6	7.5	7.9	6.3	7.2
XI	–	–	–	–	5.0	1.2	11.7	4	-4.9	25	2.5	4.2	3.2	3.3	6.8	7.2	6.8	6.9	90	86	87	88	0.7	1.3	1.5	1.2	8.6	8.9	7.8	8.4
XII	–	–	–	–	-1.8	-7.7	5.6	5	-20.2	21	-4.7	-3.3	-4.7	-4.4	4.0	4.3	4.0	4.1	84	83	83	83	0.6	0.9	0.7	0.7	8.3	7.5	7.4	7.7
Rok	–	–	–	–	10.1	2.5	28.0	16.VI	-22.7	31.I	5.1	9.0	5.7	6.4	8.5	8.9	8.7	8.7	87	72	86	82	1.3	4.4	1.5	2.4	7.7	7.9	6.8	7.5

Międzyzdroje $\varphi = 53°56'$ $\lambda = 14°27'$

I	–	–	–	–	–	-0.4	–	–	-13.9	31	1.2	2.5	1.4	1.6	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.8	7.6	8.5
II	–	–	–	–	–	-2.0	–	–	-10.5	1	0.1	1.3	0.4	0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.9	7.5	8.1
III	–	–	–	–	3.2	-2.6	12.5	30	-6.9	14	-0.6	2.2	-0.1	0.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.6	6.5	6.8
IV	–	–	–	–	11.8	3.6	21.8	22	-0.2	1	5.8	9.6	6.9	7.3	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.0	6.5	6.9
V	–	–	–	–	13.5	6.5	20.6	19	-0.8	3	9.3	11.9	8.9	9.7	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.4	6.7	6.8
VI	–	–	–	–	18.5	9.9	28.5	15,19	3.9	8	13.4	16.7	13.1	14.1	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.1	5.9	6.1
VII	–	–	–	–	19.1	10.8	25.3	21	6.9	5	14.2	17.2	13.6	14.6	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.3	5.8	6.3
VIII	–	–	–	–	19.1	11.9	28.3	12	8.6	14	14.0	17.5	14.4	15.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.5	6.1	7.1
IX	–	–	–	–	16.7	9.1	23.5	3	4.8	25	10.9	15.7	11.7	12.5	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.3	4.6	5.7
X	–	–	–	–	13.1	6.2	23.2	2	1.4	27	8.0	12.1	9.4	9.7	–	–	–	–	–	–	–	–	–	–	–	–	8.3	6.8	6.3	7.1
XI	–	–	–	–	5.8	1.7	13.7	8	-2.5	24,25	2.9	5.1	3.2	3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.9	7.5	8.1
XII	–	–	–	–	-0.5	-4.9	5.4	12	-15.2	22	-3.1	-1.6	-2.9	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	7.9	6.8	6.0	6.9
Rok	–	–	–	–	–	4.2	–	–	-15.2	22.XII	6.3	9.2	6.7	7.2	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.1	6.4	7.0

Siejnik $H_s = 170 m$ $h_w = 12 m$ 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◔	●	Opad R > 0.1	R > 1.0	R > 10.0	≡	⊠	R K
I	1	120	5	66	·	·	2	3.0	14	44	52	43	11	44	8	55	·	46	32	81	6	3	8	23	·	4	·	2	23	14	9	·	4	27	·
II	1.5	10.3	9.5	64	7	57	45	48	14.5	56	29.5	82	1	120	12.5	11.8	4	74	31	63	12	8	18	28	·	11	3	·	17	16	8	·	4	28	·
III	·	·	20.5	6.1	4.5	4.6	18	44	14	56	8	34	4	62	19	48	5	48	41	83	31	11	19	30	·	6	2	1	12	12	10	·	5	31	·
IV	3	43	8	59	4	62	13	49	15	45	23	42	7	40	11	67	6	46	39	109	5	·	·	5	·	2	1	2	12	13	8	1	12	3?	2
V	1	30	7	30	3	5.0	7	5.0	7	27	30	37	18	40	11	37	9	34	92	184	31	·	·	4	·	·	·	·	12	21	17	4	7	·	2
VI	5	86	1	80	1	14.0	·	·	9	38	23	47	27	44	8	46	16	40	39	11.0	11	·	·	·	2	2	·	2	8	10	9	1	1	·	2
VII	·	·	·	·	·	·	1	3.0	75	46	225	25	35	40	10	27	47	30	70	122	27	·	·	·	3	1	·	2	11	15	11	4	2	·	1
VIII	·	·	·	·	1	3.0	·	·	9	59	48.5	53	13.5	39	8	5.0	13	43	127	198	24		·	·	1	4	·	4	8	18	16	6	2		3
IX	2	30	7	30	2	30	3	27	13	33	38	56	15	60	5	34	5	45	94	182	18		·	·	·	4	1	1	14	22	14	2	6	·	2
X	·	·	·	·	2	25	1	1.0	22	31	34	35	15	33	16	34	3	32	11	24	21	·	·	3	·	·	·	1	12	12	4	·	12	·	
XI	·	·	6	100	14	6.3	29	48	14	37	21	36	·		5	30	1	48	51	170	15	·	1	13	·	3	·	3	22	14	9	1	14	·	
XII	6	22	22	30	·	·	5	34	12	35	31	56	5.5	48	10.5	38	1	40	11	—	—	11	18	27	·	2	·	4	18	18	3	·	4	18	
Rok	19.5	36	86	43	38.5	42	83.5	31	151	42	360.5	46	152	48	124	49	80	44	638	198	24.VIII	33	64	133	6	39	7	22	169	185	118	19	73	107?	12

Miastko $H_s = 145 m$ $h_w = 11 m$

I	5	24	1	20	·	·	1	20	19	26	29	34	25	21	8	28	5	26	77	109	20	2	4	15	·	·	·	·	24	22	15	1	–	11	:
II	4	8.0	8	23	6	18	1	1.0	16	24	10	51	18	41	16	40	5	35	64	142	16	4	12	23	·	3	2	·	18	22	10	3	–	23	·
III	7	26	7	20	2	15	3	30	22	20	7	17	21	17	5	20	19	15	46	161	12	11	9	29	·	·	·	3	11	16	8	1	–	28	·
IV	2	25	3	23	2	4.0	1	20	15	25	15	24	28	19	8	25	16	19	39	60	6	·	·	7	2	·	·	3	7	12	12		–	·	1
V	1	3.0	1	20	·	·	2	3.0	11	20	17	15	40	18	6	25	15	16	94	180	17	·	·	5	·	·	·	·	15	26	18	3	–	·	4
VI	5	36	2	20	·	·	1	4.0	2	25	15	32	48	27	1	3.0	16	24	71	115	19	·	·	1	3	1	·	3	6	15	12	1	–		4
VII	1	20	·	·	·	·	·		2	3.0	12	25	45	19	5	28	28	15	53	98	12	·	·	·	3		·	2	7	16	11	·	–	·	2
VIII	1	3.0	·	·	·	·	1	4.0	·	·	20	31	43	27	1	20	27	20	74	92	15	·	·	·	1	·	·	2	12	22	15	·	–	·	2
IX	1	1.0	·	·	·	·	·	·	5	22	17	25	43	27	1	1.0	23	19	48	126	12	·	·	·	1	·	·	5	6	15	10	1	–	·	2
X	·	·	·	·	·	·	1	1.0	8	1.8	15	21	38	21	2	1.5	29	14	20	42	5	·	·	6	·	·	·	4	14	12	6	·	–		1
XI	·	·	6	27	4	25	13	27	20	18	11	24	19	18	2	25	15	18	51	144	29	·	1	13	·	·	·	2	20	11	8	2	–	6	·
XII	2	15	3	1.0	3	1.0	1	1.0	13	20	16	20	26	15	7	13	22	13	35	85	11	12	17	27	·	·	·	4	18	13	10	·	–	17	·
Rok	29	25	31	14	17	09	25	2.0	133	2.1	184	27	394	22	62	2.3	220	20	672	180	17.V	29	43	126	10	4	2	28	158	202	135	12	–	85	16

Radostowo $H_s = 40 m$ $h_w = 15 m$

I	1.5	5.0	8	56	0.5	60	2	20	12.5	57	43	60	45.5	5.1	8	3.1	2	53	26	58	25	3	3	16	·	7	·	1	21	15	8	·	1	9	·
II	7	89	14.5	60	1.5	57	0.5	6.0	13	59	17.5	66	13.5	64	13.5	47	3	6.0	16	5.0	12	3	11	23	·	11	·	·	19	13	5	·		23	·
III	13.5	5.5	13	5.7	4	1.8	17	36	14.5	32	9	23	10	34	7	24	5	36	30	89	12	8	12	29	·	4	·	2	10	11	7	·	2	30	·
IV	19.5	4.5	13	5.7	1.5	67	6.5	38	17.5	43	16.5	43	7.5	21	7	41	1	43	30	130	5	·	·	4	2	6	·	1	14	12	6	1	2	·	1
V	11	5.0	18	25	1	35	5	34	12.5	27	21	31	12	24	8.5	31	4	29	116	325	14	·	·	3	·	3	·	·	15	20	16	3	2	·	4
VI	20	46	11	34	2.5	14	5	24	25	38	15	44	22	36	11	27	1	37	87	453	16		·	·	3	3	·	1	10	14	9	1	·	·	3
VII	16	27	15.5	25	·	·	3	28	9.5	40	14.5	36	20	32	6.5	21	8	28	85	240	12		·	·	3	·	·	·	12	14	9	3	·	·	2
VIII	5.5	23	6.5	16	1.5	1.0	1.5	1.7	4.5	4.0	31	41	29	32	4.5	27	9	30	61	127	7	·	·	·	1	·	·	·	11	13	12	2	1	·	2
IX	4.5	27	6.5	18	5	20	3.5	23	8	36	21	49	22	34	8.5	35	11	31	52	188	18	·	·		1	2	·	3	11	13	10	1	2	·	·
X	6	34	1.5	33	0.5	20	4.5	28	19	28	22	28	12	35	7.5	27	19	24	8	29	19	·	·	7	·	1	·	3	13	7	3	·	4	·	·
XI	5	32	8	88	9	48	11	40	19	26	19.5	36	4.5	32	1	35	13	35	44	136	1	·	·	9	·	2	·	2	21	12	9	1	3	5	
XII	5	21	13.5	22	3.5	33	3	23	18	46	22	51	8.5	46	2.5	38	17	32	13	55	13	11	15	25	·	3	·	4	20	9	5		2	22	·
Rok	114.5	4.2	129	41	30.5	32	62.5	31	150.5	39	252	4.2	177.5	37	85.5	32	93	36	568	453	16.VI	25	41	116	10	42	·	17	177	153	99	12	19	89	12

Międzyzdroje $H_s = 10 m$ $h_w = 14 m$

I	5.5	10.5	4.5	5.7	4	25	15.5	35	18.5	4.5	18	57	23.5	48	5.5	36	1	48	34	101	24	2	–	12		3	3	2	22	14	8	1	2	–	:
II	5.5	54	15.5	35	6	30	6	37	9	32	14.5	56	10.5	82	16	83	1	54	56	170	12	1	–	21	·	3	2	2	20	18	10	2	2	–	
III	12	45	10	40	30	33	4.5	39	14.5	31	7	36	4	45	11	35	·	36	54	138	5	·	3	27	·	·	·	·	12	14	10	1	1	–	·
IV	12.5	41	23	39	14.5	33	4.5	34	7	43	11	46	11.5	49	6	32	·	40	32	92	16	·	·	1	·		·	2	12	12	12	·	2	·	·
V	10	25	11	22	11	19	7	23	10.5	18	10.5	23	19.5	18	13.5	26	·	22	87	162	9	·	·	2	·	·	·	·	11	20	14	2	2	·	4
VI	19	21	12.5	20	4	12	5	20	6	17	7	21	18.5	45	18	28	·	27	62	180	26	·	·	·	4	1	1	·	7	9	8	2	1		4
VII	17.5	14	12	14	9.5	15	7	16	5.5	18	6	22	17	20	15.5	17	3	16	74	201	12	·	·		1		·	2	11	13	10	2	1	·	3
VIII	9.5	21	6.5	15	10.5	21	7	16	12	23	9	22	28.5	29	9	29	1	24	79	125	24	·	·		1	1	·	1	8	20	15	1	1	·	
IX	6	20	3	18	15	24	7	26	9	24	9.5	27	19.5	30	17	26	4	25	40	157	4	·	·	·	·			2	1	12	10	1	3	·	2
X	4.5	11	7	11	16.5	15	20	18	17	20	7	17	8.5	19	10.5	25	2	18	15	58	26	·	·	·	·		·	·	14	9	5	·	8	·	
XI	3.5	24	4.5	40	35.5	23	11.5	18	16	12	3.5	20	9	22	3.5	11	3	20	29	70	19	·	1	9	·	·	·	·	18	15	10	·	7	3	
XII	3	20	2	20	28	23	15	18	26	19	5	20	8	26	4	22	2	20	34	79	11	6	15	24	·	·	·	1	11	15	7	·	2	16	·
Rok	108.5	33	108.5	28	184.5	23	110	25	151	25	108	31	178	36	129.5	31	17	29	596	201	42.VII	9	–	96	6	8	6	12	147	171	149	12	32	–	13

Świnoujście $\varphi = 53°55'$ $\lambda = 14°14'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.8	0.2	8.2	12	-11.8	31	1.5	2.6	1.9	2.0	6.2	6.2	6.2	6.2	88	83	86	86	0.8	1.3	1.0	1.0	7.6	8.5	7.5	7.9
II	–	–	–	–	2.8	-1.5	7.9	20	-10.7	1	0.1	1.6	0.8	0.8	5.3	5.6	5.2	5.4	84	79	79	81	1.0	1.5	1.4	1.3	7.7	7.9	6.8	7.3
III	–	–	–	–	2.9	-2.1	12.5	30	-7.8	14	-1.1	1.8	0.2	0.3	5.0	5.2	5.1	5.1	86	75	82	81	0.8	1.9	1.2	1.3	7.7	7.3	6.6	7.2
IV	1012.0	1029.4	984.9	1012.6	10.0	3.9	20.4	25	1.0	7	5.4	7.4	6.3	6.4	8.0	8.1	8.1	8.1	88	78	85	84	1.1	2.4	1.6	1.7	7.3	6.6	7.0	7.0
V	1011.4	1016.7	1003.3	1012.0	13.0	6.9	20.4	19	0.4	1,3	9.3	11.5	9.4	9.9	9.9	9.5	9.9	9.8	83	71	83	79	1.9	4.4	2.1	2.8	6.6	7.8	7.2	7.2
VI	1017.5	1035.1	1003.9	1018.1	18.0	10.3	28.5	19	4.6	1	13.1	16.4	13.7	14.2	11.8	11.7	11.3	11.6	77	62	71	70	3.6	7.8	4.7	5.4	5.8	6.0	5.3	5.7
VII	1012.9	1023.7	991.1	1013.5	18.4	11.3	25.4	21	7.7	5,10	14.2	17.0	14.4	15.0	14.2	13.8	14.0	14.0	87	72	85	81	2.2	5.8	2.6	3.5	6.5	7.0	4.9	6.1
VIII	1012.5	1021.7	1000.7	1013.1	19.1	12.2	28.4	12	9.7	30	14.0	17.7	14.9	15.4	13.5	13.9	14.2	13.9	84	69	84	79	2.6	6.6	2.8	4.0	7.6	7.8	5.5	7.0
IX	1013.6	1027.9	994.0	1014.2	16.7	9.2	23.8	12	4.6	25	10.7	15.6	12.2	12.7	11.6	11.7	11.6	11.6	90	66	81	79	1.4	6.3	2.7	3.5	5.9	6.3	4.6	5.6
X	1020.1	1035.1	1004.8	1020.7	12.9	6.7	22.2	2	2.4	28	7.8	11.7	9.6	9.7	10.0	11.1	10.7	10.6	93	80	88	87	0.7	3.0	1.5	1.7	7.4	6.6	5.5	6.5
XI	1015.0	1032.1	997.1	1015.7	5.7	2.4	12.9	5	-2.3	24	3.4	4.9	3.8	4.0	7.3	7.7	7.3	7.4	92	87	89	89	0.7	1.3	0.9	1.0	7.4	8.5	7.0	7.6
XII	1014.9	1048.6	968.8	1015.6	0.0	-4.6	5.6	10	-14.1	22	-2.8	-1.4	-2.6	-2.4	4.7	4.8	4.6	4.7	88	83	87	86	0.5	0.9	0.6	0.7	7.6	7.2	6.0	6.9
Rok	–	1048.6	968.8	–	10.3	4.6	28.5	19.VI	-14.1	22.XII	6.3	8.9	7.0	7.3	9.0	9.1	9.0	9.0	87	75	83	82	1.4	3.6	1.9	2.3	7.1	7.3	6.1	6.8

Gryfice $\varphi = 53°55'$ $\lambda = 15°13'$

I	–	–	–	–	3.1	-0.7	8.2	21	-15.1	31	1.0	2.3	1.1	1.4	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.2	7.9	8.1
II	–	–	–	–	2.1	-2.8	7.1	8	-14.1	1	-0.9	1.4	-0.2	0.0	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.5	7.6	8.0
III	–	–	–	–	3.3	-3.7	12.2	30	-9.8	14	-2.5	2.5	-0.7	-0.3	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.2	6.1	6.5
IV	–	–	–	–	13.3	3.3	27.4	25	-0.1	1	5.6	11.8	6.6	7.6	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.9	7.1	6.6
V	–	–	–	–	14.1	5.7	20.8	19	-2.1	5	8.8	12.4	8.8	9.7	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.9	8.0	7.3
VI	–	–	–	–	18.9	8.7	29.6	15	1.8	4	12.7	17.2	12.3	13.6	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.7	4.6	5.1
VII	–	–	–	–	20.0	10.0	26.9	21	6.2	5	13.6	18.7	13.2	14.7	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.5	5.7	6.0
VIII	–	–	–	–	19.2	11.0	28.3	12	6.7	14	13.5	17.8	13.8	14.7	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.8	6.3	7.0
IX	–	–	–	–	16.6	8.0	24.4	4	3.7	25	9.9	15.8	10.7	11.8	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.0	5.3	5.8
X	–	–	–	–	12.4	5.2	21.9	3	-0.2	28	6.7	11.9	8.2	8.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.2	6.1	6.7
XI	–	–	–	–	5.2	1.3	12.6	8	-3.8	24	2.5	4.7	2.9	3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.2	6.8	7.9
XII	–	–	–	–	-1.1	-5.4	5.1	5	-16.0	22	-3.7	-2.0	-3.6	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.3	5.4	7.1
Rok	–	–	–	–	10.6	3.4	29.6	15.VI	-16.0	22.XII	5.6	9.6	6.1	6.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.0	6.4	6.9

Morąg $\varphi = 53°55'$ $\lambda = 19°56'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	20.0	10.4	27.4	21	6.3	30	13.8	18.8	14.1	15.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	19.8	11.0	26.4	12	5.9	10	13.7	18.1	14.6	15.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	16.1	7.6	25.9	4	3.4	27	9.6	14.7	10.8	11.5	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.9	4.8	5.8
X	–	–	–	–	12.4	4.4	19.8	1,2	-3.5	28	5.9	11.5	7.4	8.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.2	5.7	6.3
XI	–	–	–	–	4.7	1.3	12.8	4	-4.0	24	2.3	4.0	2.8	3.0	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.9	6.8	8.3
XII	–	–	–	–	-2.5	-7.1	4.0	5	-20.3	23	-5.2	-3.8	-5.0	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.2	7.5	7.2
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Nirty $\varphi = 53°54'$ $\lambda = 18°23'$

I	–	–	–	–	1.9	-1.9	7.8	22	-18.2	30	-0.2	1.3	0.2	0.4	5.5	5.9	5.8	5.7	88	85	91	88	0.8	1.1	0.6	0.8	9.6	8.3	8.1	8.7
II	–	–	–	–	-0.3	-4.8	4.7	20	-21.1	1	-3.1	-0.8	-2.0	-2.0	4.5	5.2	4.8	4.8	89	87	90	89	0.6	0.7	0.5	0.6	7.7	8.6	6.5	7.6
III	–	–	–	–	0.4	-6.7	8.8	31	-15.8	2	-5.1	0.0	-2.0	-2.3	3.9	5.3	4.8	4.7	89	85	89	88	0.5	0.9	0.5	0.6	–	–	–	–
IV	–	–	–	–	13.0	2.8	26.9	21	-1.8	1	5.7	11.6	7.3	8.0	8.4	9.2	9.2	8.9	89	69	87	82	1.1	5.8	1.4	2.8	–	–	–	–
V	–	–	–	–	13.6	4.5	18.8	8,19	-2.8	1	8.6	12.4	9.4	10.0	9.9	9.8	10.5	10.1	87	69	88	81	1.4	4.8	1.4	2.5	6.6	7.9	7.6	7.4
VI	–	–	–	–	18.5	8.3	28.4	16	2.7	2,4	12.4	16.9	13.3	14.0	11.3	11.4	12.4	11.7	77	60	79	72	3.5	8.7	3.5	5.2	5.5	5.3	4.9	5.2
VII	–	–	–	–	20.1	9.6	27.4	21	6.3	30	13.7	18.5	13.8	15.0	14.1	13.9	13.5	13.8	89	66	84	80	1.7	7.9	2.5	4.0	5.3	5.9	5.8	5.7
VIII	–	–	–	–	19.5	10.8	27.4	12	6.8	10,14	13.6	18.4	14.5	15.2	13.6	14.5	14.4	14.2	87	69	86	81	2.1	6.9	2.4	3.8	7.3	6.4	6.6	6.8
IX	–	–	–	–	16.6	7.5	26.3	5	1.7	25	9.7	15.7	10.8	11.8	11.2	13.0	11.8	12.0	92	73	91	85	1.0	5.3	1.3	2.5	7.2	6.7	5.0	6.3
X	–	–	–	–	12.6	3.9	20.3	2,3	-3.7	28	6.2	11.9	7.8	8.4	9.1	11.1	9.8	10.0	93	78	90	87	0.7	3.2	1.0	1.6	6.6	5.5	4.4	5.5
XI	–	–	–	–	4.1	0.4	11.3	4	-3.3	23	1.8	3.6	2.6	2.6	6.5	7.0	6.9	6.8	92	87	92	90	0.6	1.2	0.6	0.8	9.0	7.8	7.9	8.2
XII	–	–	–	–	-2.4	-7.2	6.4	12	-20.6	21	-5.0	-3.4	-4.9	-4.6	4.2	4.6	4.3	4.4	89	86	89	88	0.4	0.6	0.5	0.5	8.3	7.4	7.4	7.7
Rok	–	–	–	–	9.8	2.3	28.4	16.VI	-21.1	1.II	4.9	8.8	5.9	6.4	8.5	9.2	9.0	8.9	88	76	88	84	1.2	3.9	1.4	2.2	–	–	–	–

Świnoujście $H_s = 6 m$ $H_b = 5,4 m$ $h_w = 20 m$ 1962

MIESIĄC	ROZKŁAD WIATRU (°D, °mD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v > 15	◑	●	Opad R R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R ro
I	5	87	1	75	35	31	45	32	18	45	40	46	16	49	5	56	·	48	41	82	25	1	3	11	·	2	–	2	17	23	14	·	2	4	
II	8	89	11	83	75	67	·	·	6	45	245	46	17	62	10	88	·	65	55	171	12	1	6	17	·	15	–	3	13	17	10	1	2	16	
III	10	39	14	47	6	20	115	49	105	33	165	19	8	26	155	41	1	35	23	50	31	·	4	26	·	4	·	3	15	13	8	·	5	13	
IV	65	37	285	54	25	26	3	23	5	31	24	36	9	28	115	47	·	41	41	92	16	·	·	·	·	3	·	3	14	16	10	·	8	·	3
V	85	48	14	30	35	27	95	30	65	28	21	29	18	32	7	56	5	32	70	106	1	·	·	·	·	·	·		15	22	15	1	2	·	2
VI	11	45	125	41	05	20	35	36	7	27	15	34	27	41	125	41	1	38	45	120	16	·	·	·	3	·	·	2	5	9	7	1	1	·	4
VII	85	21	16	36	3	25	15	33	5	18	185	26	23	26	125	27	5	27	52	108	3	·	·	·	1	1	·	1	8	15	10	1	·	·	3
VIII	6	22	35	19	1	30	55	24	75	27	375	37	235	38	55	37	3	33	75	128	24	·	·	·	1	·	·	1	7	18	14	2	·		3
IX	35	41	3	20	3	20	135	30	10	24	17	30	275	35	85	46	4	31	24	60	4	·	·	·	·	·	·	1	1	11	7	·	3		1
X	3	35	45	38	45	16	20	22	145	26	19	26	17	31	85	31	2	26	14	62	26	·	·	·	·	·	·	3	12	9	4	·	11		·
XI	1	10	65	54	20	45	17	35	145	28	15	28	125	33	25	62	1	36	22	61	30	·	1	8	·	3	·	1	16	11	7	·	5	3	·
XII	2	55	4	18	11	41	13	32	125	29	325	29	12	31	5	51	1	32	36	83	11	5	15	25	·	1	·	1	14	13	7	·	7	16	
Rok	73	44	1185	43	66	31	1025	29	117	30	2805	32	2105	36	104	49	23	37	498	171	12.II	7	29	87	5	29	–	21	137	177	113	6	46	52	16

Gryfice $H_s = 40 m$ $h_w = 14 m$

I	3	50	25	24	15	26	·	·	105	36	215	39	30	56	4	38	20	35	61	100	6	2	3	12	·	5	·	2	21	21	20	1	2	5	
II	6	73	55	69	165	54		·	4	20	8	32	26	98	7	81	11	61	68	240	12	2	7	21	·	15	5	1	19	16	11	1	2	8	·
III	6	62	4	30	10	42	4	35	12	21	7	23	12	30	4	48	34	22	49	98	12	·	2	28	·	4		2	13	16	10	·	4	10	·
IV	14	30	65	27	9	49	1	10	15	23	11	27	21	40	4	33	22	26	42	128	16	·	·	1	1	5	·	3	12	15	12	1	5	·	2
V	55	42	·	·	3	27	·	·	3	20	12	15	245	34	5	63	40	18	122	132	13	·	·	3	·	3	·	1	17	22	19	3	3	·	2
VI	6	27	4	50	·	·	·	·	05	10	45	26	37	48	8	28	30	28	53	122	27	·	·	·	4	3	·	7	5	10	8	3	·	·	3
VII	45	20	1	10	3	20	·	·	·	·	6	15	225	38	9	33	47	15	98	327	7	·	·	·	1	·	·	3	10	17	14	2	2	·	4
VIII	3	10	·	·	1	10	·	·	1	30	8	39	32	44	5	31	43	21	98	252	24	·	·		1	3	1	2	11	16	12	3	2	·	2
IX	1	10	·	·	2	20	2	15	4	15	4	28	255	37	35	47	48	15	72	160	4	·	·	·	·	1	·	6	10	12	10	3	6	/	2
X	2	20	·	·	1	10	·	·	1	20	5	30	18	29	4	28	62	09	22	112	4	·	·	1		·	·	3	12	6	3	1	14	·	1
XI	2	40	·	·	165	42	45	28	1	20	9	23	6	47	·		51	16	32	65	22	·	2	9	·	·	·	1	19	13	9	·	8	5	·
XII	2	25	·	·	12	21	2	30	·	·	8	18	18	27	1	20	50	11	40	90	11	5	18	25	·	·	·	3	14	13	10		8	7	
Rok	55	34	235	48	755	27	135	40	385	18	404	26	2725	44	545	38	458	23	757	327	7.VII	9	32	100	7	39	6	34	163	177	138	18	56	35	16

Morąg $H_s = 113 m$ $h_w = 12,5 m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	18	20	3	23	·	·	25	44	5	22	15	24	14	24	175	23	18	19	89	180	26	·	·	·	3	1	·	–	–	17	13	2	·	·	4
VIII	3	23	1	15	15	23	·	·	4	48	205	48	185	42	105	24	34	25	100	203	19	·	·	·	1	1	·	–	–	16	15	4	·	·	6
IX	65	20	·	·	35	30	3	27	65	23	175	38	12	38	6	26	35	19	97	263	18	·	·	·	1	·	·	4	9	15	13	2	3	·	3
X	25	30	1	20	25	20	5	13	155	22	14	32	11	30	65	28	35	16	10	28	31	·	·	6	·	1	·	4	14	9	5	·	9	·	·
XI	25	14	45	46	16	56	16	41	85	26	115	23	105	30	45	22	16	30	45	80	20	·	1	9	·	1	·	1	18	14	12	·	4	1	·
XII	5	24	135	24	5	20	25	14	12	28	195	36	105	36	8	19	17	23	14	32	13	10	15	26	·	1	·	4	18	16	4	·	4	19	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Wirty $H_s = 121 m$ $h_w = 13 m$

I	·	·	3	10	·	·	·	·	10	14	48	15	5	26	12	38	15	16	34	98	28	2	4	21	·		·	1	24	13	9	·	2	11	
II	4	36	11	31	9	17	1	10	3	10	26	33	9	50	9	48	12	29	12.2	32	5	3	13	27	·	6	·	2	16	10	4	·	3	24	
III	3	23	16	22	5	14	20	14	4	10	8	11	6	12	5	22	26	11	19.2	68	12	8	17	30	·	·	·	–	–	7	5	·	16	30	
IV	8	16	2	10	8	20	8	12	6	10	14	15	12	16	10	19	22	12	22	51	28		·	7	2	·	·	–	–	11	7	·	7	·	1
V	4	12	4	28	4	10	6	17	5	12	30	14	11	17	4	18	25	11	113	267	14	·	·	5	·		·	2	15	23	13	4	7	·	6
VI	10	24	1	10	·	·	6	13	8	10	24	20	22	15	10	17	9	15	68	243	16	·	·	·	3	·	·	7	6	14	11	1	1	·	3
VII	·	·	7	13	4	10	1	10	6	18	23	13	20	16	4	20	28	10	90	236	13	·	·	·	3	·	·	4	8	17	12	3	2	·	2
VIII	3	13	1	10	2	10	2	10	7	19	36	20	21	14	4	18	17	14	75	198	7	·	·	·	1	·	·	4	13	17	13	3	3	·	4
IX	·	·	·	·	7	10	4	20	4	12	38	19	22	17	·	·	15	14	47	107	19	·	·	·	2	·	·	5	12	14	10	2	7	·	3
X	2	10	·	·	1	10	4	12	10	11	20	15	10	17	13	10	33	08	16	132	31	·	·	8	·	·	·	6	9	15	2	1	16	·	
XI	1	20	8	22	12	17	19	17	7	13	15	11	2	15	·	·	26	11	55	126	29	·	1	13	·	·	·	2	21	18	11	1	13	2	·
XII	4	10	4	12	6	12	4	10	5	12	46	15	1	10	2	10	21	11	22	52	14	11	15	28	·	·	·	4	23	19	6	·	10	21	·
Rok	39	14	57	14	58	11	75	12	75	13	328	17	141	19	73	18	249	14	573	267	14.V	24	50	139	11	6	·	–	–	178	103	15	87	88	19

Jazy $\varphi = 53°53'$ $\lambda = 23°22'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{a.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.7	-3.4	5.0	22	-25.2	31	-1.9	0.0	-1.8	-1.4	5.0	5.6	5.0	5.2	89	88	86	88	0.6	0.7	0.7	0.7	8.7	8.2	7.5	8.1
II	–	–	–	–	-1.2	-8.2	2.6	12,13	-22.9	1	-6.2	-2.7	-4.5	-4.5	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.4	6.8	7.6
III	–	–	–	–	0.2	-9.9	6.6	31	-22.6	2	-7.5	-0.6	-4.7	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.1	6.1	5.9
IV	–	–	–	–	13.8	3.3	25.9	23	-2.6	8	6.5	12.5	7.2	8.4	8.6	9.3	9.0	9.0	87	66	86	80	1.4	6.5	1.6	3.2	6.3	6.3	5.4	6.0
V	–	–	–	–	14.4	4.7	21.5	27	-3.5	4	9.1	12.9	8.6	9.8	10.4	10.2	10.3	10.3	88	69	89	82	1.4	5.1	1.3	2.6	6.8	7.8	6.8	7.1
VI	–	–	–	–	18.6	7.0	27.2	23	0.0	3	12.4	17.1	11.2	13.0	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.1	5.0	6.1
VII	–	–	–	–	20.3	9.2	27.7	21	4.0	4	14.0	18.9	13.7	15.1	13.9	14.0	13.4	13.8	87	65	85	79	2.3	8.2	2.4	4.3	5.5	8.0	5.5	6.3
VIII	–	–	–	–	20.5	10.3	27.2	13	3.1	15	13.6	18.8	14.1	15.2	13.9	13.4	14.0	13.8	89	63	86	79	1.8	8.7	2.4	4.3	6.1	7.0	5.3	6.1
IX	–	–	–	–	15.6	6.7	25.8	5	-0.9	25	8.7	14.4	10.3	10.9	10.6	11.7	11.5	11.3	93	72	90	85	0.9	5.1	1.4	2.5	7.1	6.8	5.9	6.6
X	–	–	–	–	11.7	2.9	19.1	2	-3.9	28	5.0	10.7	6.6	7.2	8.3	9.7	9.0	9.0	94	74	91	86	0.6	3.5	0.9	1.7	7.6	6.3	5.5	6.5
XI	–	–	–	–	5.4	0.9	14.8	1	-4.2	26	2.1	4.4	2.9	3.1	7.0	7.2	6.9	7.1	94	84	90	90	0.4	1.5	0.7	0.9	8.5	7.8	7.5	7.9
XII	–	–	–	–	-3.1	-8.4	3.8	8	-22.6	21	-5.7	-3.9	-6.2	-5.5	3.9	4.0	3.9	3.9	88	81	87	85	0.5	0.9	0.5	0.6	8.0	7.5	7.4	7.6
Rok	–	–	–	–	9.7	1.3	27.7	21.VII	-25.2	31.I	4.2	8.5	4.8	5.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.2	6.2	6.8

Biskupiec $\varphi = 53°52'$ $\lambda = 20°57'$

I	–	–	–	–	0.7	-3.2	6.6	22	-20.9	31	-1.2	0.0	-1.3	-1.0	5.1	5.3	4.9	5.1	86	83	83	84	0.8	1.0	0.9	0.9	9.8	9.0	9.2	9.3
II	–	–	–	–	-1.0	-7.0	2.5	20	-17.0	1	-4.7	-2.0	-3.6	-3.5	3.8	4.2	4.0	4.0	82	78	82	81	0.7	1.1	0.8	0.9	9.5	8.7	8.5	8.7
III	–	–	–	–	0.2	-8.0	6.9	31	-19.3	15	-6.3	-0.6	-4.1	-3.8	3.3	4.1	3.8	3.7	81	69	80	77	0.7	1.9	0.9	1.2	8.6	7.1	6.4	7.4
IV	–	–	–	–	13.8	4.0	27.7	23	-1.5	8	5.8	12.7	7.6	8.4	8.3	8.6	8.8	8.6	88	60	82	77	1.3	7.6	2.2	3.7	8.2	6.8	6.8	7.3
V	–	–	–	–	13.9	5.1	18.4	13	-2.1	6	8.6	12.5	8.7	9.6	9.8	10.1	9.8	9.9	86	69	85	80	1.6	4.8	1.7	2.7	8.4	8.7	8.9	8.7
VI	–	–	–	–	19.1	7.8	28.7	16	2.9	2	12.6	17.7	12.3	13.7	11.3	10.5	11.1	11.0	76	51	76	68	3.7	10.5	3.6	5.9	6.3	7.1	8.1	7.2
VII	–	–	–	–	20.3	10.2	27.9	26	5.4	30	13.7	19.2	13.6	15.0	13.7	13.3	13.5	13.5	87	60	86	77	2.3	9.3	2.3	4.6	–	–	–	–
VIII	–	–	–	–	19.9	10.8	26.3	12	4.0	15	13.6	18.6	14.1	15.1	13.7	14.0	14.2	14.0	87	66	88	80	2.0	7.9	2.0	4.0	–	–	–	–
IX	–	–	–	–	15.7	7.3	25.0	4	1.8	24	9.4	15.0	10.4	11.3	10.8	11.6	11.3	11.2	91	69	89	83	1.2	5.9	1.5	2.9	7.6	7.3	6.9	7.3
X	–	–	–	–	12.1	3.7	19.5	2	-3.2	28	5.8	11.7	6.7	7.7	8.8	10.3	9.0	9.4	92	74	90	85	0.7	3.8	1.0	1.8	–	–	–	–
XI	–	–	–	–	4.6	0.7	11.6	4	-5.9	26	2.0	3.9	2.7	2.8	6.6	7.0	6.7	6.8	90	84	87	87	0.7	1.4	1.0	1.0	9.6	9.4	9.1	9.4
XII	–	–	–	–	-3.3	-7.9	3.6	5	-22.2	23	-5.7	-4.1	-5.7	-5.3	3.7	4.0	3.7	3.8	80	79	79	79	0.7	0.8	0.8	0.8	–	–	–	–
Rok	–	–	–	–	9.7	2.0	28.7	16.VI	-22.2	23.XII	4.5	8.7	5.1	5.8	8.2	8.6	8.4	8.4	86	70	84	80	1.4	4.7	1.6	2.6	–	–	–	–

Mikołajki $\varphi = 53°47'$ $\lambda = 21°35'$

I	996.4	1024.7	971.3	1012.9	1.0	-2.8	6.4	22	-19.1	31	-1.3	0.0	-1.2	-0.9	5.2	5.3	5.0	5.2	89	84	86	86	0.6	1.0	0.8	0.8	8.8	8.1	7.3	8.1
II	996.7	1019.8	956.6	1013.4	-1.1	-6.6	3.1	12	-17.3	1	-4.9	-2.6	-3.6	-3.7	3.8	4.2	4.1	4.0	86	81	84	84	0.5	0.9	0.8	0.7	8.4	7.3	7.2	7.6
III	994.7	1012.4	972.0	1011.3	-0.2	-7.6	8.1	31	-17.5	15	-6.4	-1.3	-3.8	-3.8	3.5	4.1	3.9	3.8	87	72	80	80	0.5	1.5	0.9	1.0	7.2	6.6	5.9	6.6
IV	987.4	1014.4	973.8	1013.4	13.3	3.8	25.6	23	-1.2	8	5.5	11.6	7.6	8.1	8.2	8.6	8.7	8.5	88	64	81	78	1.1	6.1	2.3	3.2	7.0	6.2	4.4	5.9
V	995.5	1004.0	974.4	1011.4	13.7	6.2	18.1	13	-2.0	1	8.3	12.4	9.3	9.8	9.8	9.6	9.9	9.8	87	66	92	82	1.4	5.2	2.1	2.9	8.1	8.8	7.7	8.2
VI	1000.2	1012.3	987.5	1015.9	18.4	9.4	26.9	16	5.2	10	12.3	16.8	12.9	13.7	11.2	10.6	11.5	11.1	76	55	75	69	3.5	9.0	3.7	5.4	6.4	7.0	5.8	6.4
VII	996.8	1006.5	982.6	1012.4	19.6	11.3	26.4	26	7.2	4	13.5	17.9	14.5	15.1	13.4	13.0	13.9	13.4	87	63	83	78	2.2	7.9	2.9	4.3	7.3	7.6	6.2	7.0
VIII	997.4	1007.2	985.2	1013.0	19.8	12.2	26.5	7	7.1	15	14.0	18.4	14.9	15.6	13.8	13.7	14.4	14.0	86	65	84	78	2.3	7.7	2.8	4.2	7.4	7.5	5.8	6.9
IX	998.5	1015.7	978.2	1014.3	15.5	8.5	24.1	4	4.1	27	9.6	14.2	11.4	11.6	10.9	11.4	11.7	11.3	91	70	87	83	1.1	5.2	2.0	2.8	7.2	7.6	4.9	6.6
X	1005.1	1020.5	988.8	1021.2	12.0	5.4	18.3	2	-1.6	28	6.5	10.8	8.0	8.3	9.1	10.6	9.8	9.8	91	80	90	87	0.8	2.7	1.0	1.5	7.1	6.8	5.0	6.3
XI	1001.9	1015.8	984.9	1018.2	5.0	1.3	11.4	4,5	-3.9	25,26	2.2	4.1	3.0	3.1	6.7	7.0	6.9	6.9	91	84	89	88	0.6	1.4	0.8	0.9	8.7	8.5	7.6	8.3
XII	999.3	1031.9	959.3	1016.2	-2.8	-7.9	4.1	5	-21.7	23	-5.4	-4.1	-5.5	-5.1	4.1	4.1	4.0	4.1	88	83	86	86	0.5	0.8	0.6	0.6	7.7	7.5	7.4	7.5
Rok	998.3	1031.9	956.6	1014.4	9.5	2.8	26.9	16.VI	-21.7	23.XII	4.5	8.2	5.6	6.0	8.3	8.5	8.6	8.5	87	72	85	81	1.3	4.1	1.7	2.4	7.6	7.5	6.3	7.1

UWAGA. *Ciśnienie powietrza jest za niskie przeciętnie o około 0,3 mb.*

Resko $\varphi = 53°46'$ $\lambda = 15°25'$

I	1006.3	1035.5	977.0	1013.3	3.3	-1.0	8.4	22	-17.9	31	0.8	2.2	0.9	1.2	5.9	6.1	6.0	6.0	88	83	88	86	0.9	1.3	0.9	1.0	8.3	8.6	7.6	8.2
II	1008.6	1033.6	970.9	1015.7	2.1	-3.1	7.6	8	-13.9	1	-1.1	1.2	-0.4	-0.2	4.9	5.3	5.0	5.1	85	78	80	81	0.9	1.5	1.2	1.2	8.4	7.8	6.5	7.6
III	1004.8	1021.4	975.4	1011.8	3.2	-4.5	13.0	30	-11.3	14	-3.2	2.2	-1.1	-0.8	4.4	4.6	4.6	4.5	86	64	81	77	0.7	2.7	1.2	1.5	7.0	6.5	6.3	6.6
IV	1006.9	1022.5	980.2	1013.8	13.6	3.9	27.2	25	0.0	30	5.4	11.8	7.3	8.0	8.1	8.7	8.7	8.5	88	63	83	78	1.1	6.1	2.0	3.1	7.4	7.0	5.3	6.6
V	1005.9	1011.7	999.1	1012.8	14.0	5.6	20.5	19	-2.9	5	8.3	12.5	9.0	9.7	9.8	9.3	9.7	9.6	88	65	84	79	1.4	5.6	2.0	3.0	6.8	8.6	7.6	7.7
VI	1011.9	1027.4	998.5	1018.7	18.6	7.9	28.7	15	0.7	3	12.4	17.2	12.7	13.8	11.9	12.0	12.1	12.0	81	62	80	74	2.8	8.3	2.9	4.7	6.0	6.8	5.3	6.0
VII	1007.4	1018.3	985.9	1014.2	19.8	9.8	26.2	26	5.5	25	13.3	18.6	13.6	14.8	13.9	13.9	14.2	14.0	91	65	90	82	1.5	8.1	1.6	3.7	6.7	7.4	5.8	6.6
VIII	1007.4	1016.7	995.2	1014.2	19.0	11.1	26.7	12	5.5	14	13.3	17.7	14.0	14.8	14.0	15.0	14.5	14.5	91	74	90	85	1.4	5.6	1.6	2.9	7.5	8.4	5.7	7.2
IX	1008.5	1022.8	986.2	1015.3	16.7	7.9	25.1	4	3.0	18	9.8	15.7	10.5	11.6	11.4	12.4	11.6	11.8	93	70	92	85	0.9	5.7	1.1	2.6	6.8	6.8	3.8	5.8
X	1015.0	1030.0	1000.0	1022.0	12.9	4.8	22.9	3	-1.4	28	6.5	12.1	8.1	8.7	9.4	10.9	10.1	10.1	95	77	91	88	0.6	3.7	1.0	1.8	7.6	7.0	4.9	6.5
XI	1009.8	1026.7	990.6	1016.8	5.4	1.4	14.0	8	-3.4	22,24	2.7	4.8	3.1	3.4	7.0	7.4	7.0	7.1	92	84	90	89	0.6	1.6	0.8	1.0	8.7	8.3	6.8	7.9
XII	1009.4	1042.8	963.3	1016.6	-1.1	-5.8	5.5	12	-17.3	22	-4.1	-2.0	-3.7	-3.4	4.4	4.8	4.4	4.5	89	85	88	87	0.4	0.7	0.5	0.5	7.5	7.6	5.8	7.0
Rok	1008.5	1042.8	963.3	1015.5	10.6	3.2	28.7	15.VI	-17.9	31.I	5.3	9.5	6.2	6.8	8.8	9.2	9.0	9.0	89	72	86	82	1.1	4.2	1.4	2.2	7.4	7.6	6.0	7.0

UWAGA. *Ciśnienie powietrza jest za wysokie przeciętnie o około 0,5 mb.*

Jazy $H_s = 120 m$ $h_w = 15 m$ 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	◐	●	R≥0.1	R≥1.0	R≥10.0	═	■	π ro
I	6.5	4.0	2	2.2	1	1.5	9	2.9	25.5	3.0	22	3.5	15	3.1	3	2.5	9	2.9	28	4.2	6,20	3	8	20	·	·	·	1	22	15	11	·	1	26	·
II	10.5	5.3	7	4.0	3.5	2.3	9.5	4.0	14	3.7	14	3.9	3	4.3	6.5	5.6	16	3.4	51	14.6	12	9	15	28	·	3	1	·	15	14	11	1	1	28	·
III	16	5.2	8.5	2.4	7	2.9	8	3.4	6.5	2.5	3	2.2	4.5	2.6	7.5	3.1	32	2.2	46	7.6	5	12	16	30	·	1	·	4	11	16	10	·	3	31	·
IV	7.5	2.9	9.5	2.8	5.5	1.8	16	2.7	13	2.6	7	2.9	3.5	2.4	7	3.4	21	2.0	51	12.5	13	·	·	7	2	·	·	3	7	12	10	1	1	·	·
V	8.5	4.7	2	1.5	2	2.2	6.5	2.9	7	2.1	14	1.8	13.5	2.9	11.5	2.8	28	1.6	109	14.2	27	·	·	4	·	·	·	·	14	18	16	4	3	·	3
VI	13.5	3.4	4	3.5	1	1.0	2	1.0	6.5	1.9	13	3.1	17.5	2.8	12.5	1.8	20	2.1	58	16.6	4	·	·	·	3	·	·	·	4	13	9	3	·	·	4
VII	10.5	4.7	1	2.5			3	1.5	9.5	1.8	5.5	2.1	32	2.9	13.5	3.3	18	2.0	43	17.4	27	·	·	·	4	1	·	·	6	13	9	1	5	·	3
VIII	2.5	2.6		·	1	3.0	3.5	2.8	12	2.8	19	2.9	26.5	3.0	8.5	3.0	20	2.2	108	19.8	22	·	·	·	4	·	·	1	8	16	15	4	6	·	3
IX	1.5	3.3	3.5	2.1	2.5	2.6	7	2.6	9.5	2.7	16	3.7	20	3.4	9	2.9	21	2.4	67	22.1	18	·	·	1	1	1	·	2	10	17	12	2	5	·	1
X	6	2.2	0.5	1.0	1.5	3.0	7	2.3	7	2.1	14.5	2.7	11.5	3.0	10	2.6	35	1.6	4	1.3	18,28	·	·	8	·	·	·	2	13	8	2	·	9	·	·
XI	2.5	2.8	5	3.5	21	2.8	21	2.4	4	1.9	6.5	2.5	6.5	2.4	2.5	2.4	21	2.0	57	9.8	15	·	1	13	·	·	·	3	22	17	12	·	7	·	·
XII	11.5	2.0	11	1.9	1	2.0	10	2.3	14.5	2.7	17	2.8	7	2.4	5	2.2	16	2.0	19	5.5	14	11	17	28	·	·	·	2	19	12	4	·	·	19	·
Rok	97	3.1	54	2.3	47	2.1	102.5	2.6	129	2.5	151.5	2.8	160.5	2.9	96.5	3.0	257	2.2	641	22.1	18.IX	35	57	139	14	6	1	18	151	171	121	16	41	104	14

Biskupiec $H_s = 160 m$ $h_w = 14 m$

I	5	2.6	2	4.5	4	3.8	2	2.0	14	3.1	37	5.1	19	3.9	7	2.0	3	3.9	32	6.3	6	3	5	22	·	1	·	–	–	14	9	·	1	16	·
II	11	3.5	8	3.2	5	3.6	4	3.8	14	4.2	17	5.9	14	5.2	11	5.5	·	4.6	43	10.9	12	8	14	27	·	4	1	–	–	18	9	1	1	28	·
III	11	2.8	9	2.1	10	3.0	13	3.2	7	2.3	11	2.5	10	4.7	18	2.9	4	2.6	37	11.5	12	9	14	29	·	·	·	–	–	8	8	1	·	23	·
IV	10	1.6	10	2.8	8	3.4	8	3.5	6	3.1	14	4.2	9	2.6	21	3.5	4	3.0	23	4.4	5	·	·	4	2	1	·	–	–	11	8	·	4	·	1
V	5	2.4	11	2.1	6	2.8	6	2.2	5	3.2	9	2.8	22	2.4	22	2.2	7	2.2	84	15.5	20	·	·	2	·	·	·	–	–	22	16	3	2	·	2
VI	9	4.1	2	2.5	·	·	3	2.0	1	3.0	18	4.3	29	2.9	26	2.7	2	3.1	53	21.8	29	·	·	·	2	·	·	–	–	13	9	1	1	·	1
VII	13	2.1	1	3.0	2	2.0	2	1.5	5	3.0	17	3.0	18	2.6	26	2.4	9	2.3	91	18.9	13	·	·	·	3	·	·	–	–	13	11	4	4	·	3
VIII	2	2.5	2	2.0	1	5.0	3	1.7	4	2.5	28	4.3	27	2.7	21	2.2	5	2.9	110	26.3	4	·	·	·	2	·	·	–	–	15	13	5	3	·	6
IX	4	3.0	7	1.7	8	2.6	5	3.0	2	3.0	21	4.3	25	2.2	15	2.7	3	2.8	81	24.8	18	·	·	·	·	·	·	–	–	16	12	1	4	·	·
X	10	1.2	1	2.0	4	1.8	8	1.8	6	2.5	19	2.9	20	2.4	23	1.9	2	2.1	15	5.2	28	·	·	5	·	·	·	–	–	8	4	·	8	·	
XI	5	2.0	4	5.5	18	4.9	15	4.3	8	1.8	19	3.1	13	2.6	6	2.0	2	3.4	44	14.4	19	·	2	10	·	·	·	–	–	11	9	1	8	·	·
XII	16	1.6	16	2.2	1	3.0	6	1.8	9	3.4	27	4.0	11	2.8	7	1.6	·	2.7	14	2.2	11,15	9	17	27	·		·	–	–	13	5	.	1	16	·
Rok	101	2.4	73	2.8	67	3.0	75	2.6	81	2.9	237	3.9	217	2.8	203	2.6	41	3.0	627	26.3	4.VIII	29	52	126	9	6	1	–	–	162	113	17	37	83	13

Mikołajki $H_s = 127 m$ $H_b = 131,1 m$ $h_w = 12 m$

I	4	7.0	4	4.0	2.5	2.2	4.5	3.7	21.5	4.8	34	5.2	14	4.7	6.5	4.2	2	4.7	22	2.9	20	3	4	20	·	7	·	1	18	21	9	·	5	18	·
II	9	5.7	4	8.1	12.5	3.5	5	5.4	18	5.1	11.5	6.4	10	4.5	8	7.5	6	5.0	21	4.8	12	7	16	27	·	6		1	15	21	8	·	3	28	·
III	11.5	5.6	4	2.9	10	2.6	16	4.1	6.5	3.6	5	2.6	8.5	4.3	12.5	4.5	19	3.2	30	8.9	6	8	17	30	·	4		2	12	10	6	·	·	26	·
IV	7.5	4.7	5	2.9	10	3.2	10	3.8	13.5	3.6	7.5	2.9	7.5	3.0	17	3.5	12	3.0	20	4.8	27	·	·	3	1	3	·	2	8	10	7	·	8	·	1
V	3.5	2.0	4	2.0	4.5	2.4	4.5	2.6	18.5	1.9	12.5	4.9	9	2.6	17.5	3.1	19	1.9	83	13.0	14	·	·	1	·	2	·	·	20	21	15	3	5	·	3
VI	7.5	5.0	2.5	5.8	2	2.2	2.5	1.4	7.5	2.4	16.5	3.4	15.5	3.9	25	3.0	11	3.0	28	11.2	23	·	·	·	2	1	·	1	8	11	5	1	·	·	4
VII	5.5	2.8	1	2.5	3	1.8	2.5	3.2	11.5	2.7	12.5	2.8	20.5	4.2	23.5	3.0	13	2.7	108	23.8	26	·	·	·	2	4	2	·	11	18	14	5	3	·	8
VIII	4.5	2.2	2	1.5	2	2.8	4.5	3.3	10	5.0	32.5	3.8	14.5	3.7	11	2.5	12	3.1	82	23.6	17	·	·	·	2	5	·	·	12	15	14	1	4	·	7
IX	5	3.3	3.5	2.1	7	2.6	7	2.3	8.5	4.0	20	3.7	18.5	4.1	11.5	4.8	9	3.3	52	24.0	18	·	·	·	·	3	2	1	13	15	11	1	3	·	1
X	5	1.9	1	1.0	5	1.6	8	2.8	12	4.2	18	3.2	16.5	3.6	10.5	3.9	17	2.7	9	3.7	28	·	·	1	·	2	·	4	10	10	3	·	13	·	·
XI	2	2.8	3.5	3.4	16	6.5	21.5	5.8	11.5	2.8	16	2.8	8.5	2.9	4	3.1	7	4.0	41	14.9	20	·	·	10	·	6	·	1	18	11	5	1	9	·	·
XII	12	2.3	10	2.5	3	2.2	4	2.9	18.5	4.5	21	4.2	8.5	3.2	11	2.3	5	3.2	17	2.7	10,11	11	14	25	·	·	·	4	19	15	8	·	2	16	·
Rok	77	3.8	44.5	3.2	77.5	2.8	90	3.4	157.5	3.7	207	3.6	151.5	3.7	158	3.8	132	3.3	513	24.0	18.IX	29	51	117	7	43	4	17	164	178	105	12	55	88	24

Resko $H_s = 55 m$ $H_b = 56,2 m$ $h_w = 11 m$

I	3.5	3.6	1	2.0	1.5	1.0	2	1.5	23.5	3.6	41	3.9	10.5	2.7	4	2.2	6	3.2	56	9.1	6	2	3	11	·	2	·	2	21	24	17	·	3	7	·
II	6	5.1	11.5	3.0	6	3.1	2.5	3.2	9.5	2.9	15.5	3.1	18	4.6	12	4.9	3	3.7	53	13.6	12	2	6	24	·	5	·	1	15	14	10	1	2	10	1
III	3.5	4.9	7	2.1	6	1.5	17	3.9	13	1.6	2	1.5	10.5	2.1	6	3.2	28	1.9	47	15.8	12	2	4	28	·	·	·	3	13	13	10	1	4	18	·
IV	5.5	2.5	8	2.8	6.5	2.4	8.5	2.4	10	2.9	15.5	3.8	8.5	2.9	12.5	2.2	15	2.3	41	14.3	16	·	·	·	2	·	·	3	11	14	9	1	5	·	3
V	4.5	2.8	3.5	1.4	1	2.0	6	2.8	5	3.1	25.5	2.0	15	2.1	11.5	3.1	21	1.8	122	16.3	12	·	·	5	·	·	·	·	15	21	19	3	4	·	6
VI	6.5	3.8	3	2.3	·	·	3	2.3	3.5	2.0	14	2.5	22	3.2	11	2.5	27	2.0	56	14.6	15	·	·	·	2	1	·	2	8	15	12	1	1	·	5
VII	3.5	4.1	1.5	2.0	3	1.3	5	2.2	4	2.4	22.5	2.2	15.5	2.2	10	2.2	28	1.5	90	32.6	7	·	·	·	2	·	·	1	8	19	14	1	5	·	6
VIII	0.5	3.0	·	·	1	2.0	3.5	2.6	7	2.5	28	2.7	18	3.1	7	1.9	28	1.9	110	14.5	7	·	·	·	1	·	·	1	11	22	15	5	2	·	3
IX	1.5	2.0	·	·	2.5	1.4	11	2.5	7.5	3.0	15	2.8	17.5	3.1	3	3.5	32	1.8	63	11.5	18	·	·	·	1	1	·	3	7	14	11	2	3	·	3
X	1	3.0	1	2.0	1	1.5	7	1.4	17	2.1	11.5	1.8	14.5	2.8	4	2.1	36	1.3	16	5.0	26	·	·	4	·	·	·	4	12	8	3	·	11	·	1
XI	1.5	1.7	3	2.5	14.5	3.3	12.5	3.6	6.5	2.5	10.5	1.7	10	2.2	1.5	3.7	30	1.8	36	12.8	30	·	2	10	·	·	·	1	17	11	7	1	7	5	·
XII	1	1.0	2	1.0	11	2.0	6.5	2.1	16	2.5	20	2.4	9.5	1.9	1	1.0	26	1.6	50	15.2	11	6	18	26	·	·	·	3	14	12	7	1	8	22	·
Rok	38.5	2.9	41.5	1.8	54	1.8	84.5	2.5	122.5	2.6	221	2.5	169.5	2.7	83.5	2.7	280	2.1	740	32.6	7.VII	12	33	108	8	9	·	24	152	187	134	17	55	62	28

Świdwin $\varphi = 53°46'$ $\lambda = 15°46'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA t											ŚREDNIA PREŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{s.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.0	-1.6	7.7	21,22	-19.8	31	0.1	1.4	0.3	0.5	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.9	6.4	7.6
II	–	–	–	–	1.6	-3.7	6.3	8,12	-13.2	1	-1.6	0.1	-1.2	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.1	6.4	7.7
III	–	–	–	–	2.2	-4.9	11.9	30	-12.3	14	-3.2	1.0	-1.8	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.2	5.7	5.9
IV	–	–	–	–	13.3	3.5	26.7	25	-0.5	30	5.8	11.5	7.2	7.9	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.0	5.3	6.0
V	–	–	–	–	13.4	5.2	19.8	19	-3.7	5	8.0	11.7	8.4	9.1	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.7	7.0	7.0
VI	–	–	–	–	18.3	7.8	27.6	15	-0.1	3	12.0	16.4	11.8	13.0	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.9	4.2	5.3
VII	–	–	–	–	19.6	9.3	26.0	26	5.3	5	13.1	18.0	13.0	14.3	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.7	4.9	5.9
VIII	–	–	–	–	18.8	10.5	27.1	12	5.9	14	13.3	17.4	13.6	14.5	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.1	6.1	6.9
IX	–	–	–	–	16.3	7.3	24.9	4	1.5	25	9.5	14.8	10.7	11.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.9	4.2	6.0
X	–	–	–	–	12.6	4.2	22.0	2	-1.5	15	6.2	11.6	7.9	8.4	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.3	4.5	5.9
XI	–	–	–	–	5.3	1.1	12.9	5	-3.6	22	2.3	4.2	2.5	2.9	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.7	7.3	8.0
XII	–	–	–	–	-1.4	-7.0	5.3	12	-19.1	22	-4.8	-3.1	-4.6	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	7.4	8.0	6.8	7.4
Rok	–	–	–	–	10.2	2.6	27.6	15.VI	-19.8	31.I	5.1	8.8	5.6	6.3	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.0	5.7	6.6

Połczyn-Zdrój $\varphi = 53°46'$ $\lambda = 16°06'$

I	–	–	–	–	3.2	-1.1	8.2	21	-17.4	31	0.6	2.2	0.7	1.0	6.2	6.5	6.3	6.3	93	87	92	91	0.4	0.9	0.5	0.6	8.7	7.4	8.4	8.2
II	–	–	–	–	1.7	-3.4	6.3	12	-12.9	1	-1.4	0.5	-0.9	-0.7	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.0	7.7	8.0
III	–	–	–	–	2.9	-5.5	12.0	30	-11.0	14	-3.0	2.0	-1.9	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.5	4.6	5.4
IV	–	–	–	–	13.7	3.6	27.6	25	-0.6	30	6.4	12.5	7.1	8.3	8.5	9.2	9.2	9.0	88	65	90	81	1.3	6.4	1.2	3.0	7.1	5.8	5.9	6.3
V	–	–	–	–	14.3	5.0	20.6	19	-2.2	5	8.7	12.6	8.5	9.6	9.5	9.9	9.9	9.8	83	68	88	80	1.9	5.2	1.5	2.9	7.3	7.5	6.9	7.2
VI	–	–	–	–	18.4	7.3	28.9	15	0.4	3	12.7	17.0	11.8	13.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	19.8	9.0	26.9	26	5.9	30	13.5	18.7	13.1	14.6	13.7	13.1	13.9	13.6	88	62	91	80	1.9	9.2	1.5	4.2	–	–	–	–
VIII	–	–	–	–	19.6	10.7	28.2	12	5.7	14	13.6	18.2	13.6	14.8	13.9	14.4	14.1	14.1	89	69	90	83	1.7	6.9	1.5	3.4	7.8	7.1	5.5	6.8
IX	–	–	–	–	16.9	6.8	26.9	4	1.3	25	10.0	15.7	9.7	11.3	11.2	12.3	11.2	11.6	91	69	92	84	1.2	5.9	1.0	2.7	6.5	5.3	5.5	5.8
X	–	–	–	–	13.1	4.2	22.3	2,3	-2.2	27,28	6.5	12.1	7.6	8.4	9.3	11.0	9.9	10.1	93	77	92	87	0.7	3.6	0.8	1.7	7.6	6.4	5.5	6.5
XI	–	–	–	–	5.5	1.4	12.9	5	-3.8	21	2.6	4.9	3.3	3.5	6.9	7.5	7.1	7.2	92	85	90	89	0.6	1.5	0.8	1.0	7.8	6.7	7.3	7.3
XII	–	–	–	–	-1.2	-6.8	5.2	12	-18.9	22	-4.6	-2.1	-4.4	-3.9	4.2	4.7	4.3	4.4	88	85	88	87	0.5	0.8	0.5	0.6	7.0	7.2	5.6	6.6
Rok	–	–	–	–	10.7	2.6	28.9	15.VI	-18.9	22.XII	5.5	9.5	5.7	6.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Olsztyn-Dajtki $\varphi = 53°46'$ $\lambda = 20°25'$

I	995.8	1024.0	969.3	1012.9	1.3	-2.8	7.2	22	-23.0	31	-1.0	0.3	-0.9	-0.6	5.5	5.6	5.3	5.5	91	87	88	89	0.5	0.8	0.7	0.7	9.1	8.0	7.7	8.3
II	996.5	1020.0	957.4	1013.8	-0.6	-5.8	4.4	12	-17.6	1	-4.0	-1.9	-3.1	-3.0	4.2	4.5	4.4	4.4	88	83	88	86	0.5	0.9	0.6	0.7	9.0	8.5	6.8	8.1
III	994.3	1011.6	970.2	1011.6	0.6	-7.5	8.3	31	-18.4	15	-6.1	-0.6	-3.3	-3.3	3.7	4.3	4.1	4.0	89	72	82	81	0.4	1.6	0.8	0.9	6.9	7.1	4.9	6.3
IV	996.8	1013.2	972.0	1013.5	13.8	3.7	27.1	23	-2.4	30	6.0	12.4	7.8	8.5	8.7	8.6	9.0	8.8	90	62	83	78	1.1	7.5	2.2	3.6	7.9	7.2	4.8	6.6
V	995.2	1003.3	974.7	1011.8	14.0	5.2	18.6	8	-3.5	6	8.2	12.2	9.0	9.6	10.0	9.7	10.1	9.9	90	68	87	82	1.1	5.0	1.6	2.6	8.1	8.7	7.6	8.1
VI	1000.1	1012.6	987.2	1016.5	19.0	8.2	28.9	16	1.1	3	12.6	17.2	13.0	14.0	11.8	11.0	11.6	11.5	79	56	77	71	3.2	9.3	3.9	5.5	6.2	7.2	6.5	6.6
VII	996.8	1006.5	981.4	1013.1	20.2	10.4	27.9	21	5.6	30	13.4	18.4	13.9	14.9	13.8	13.2	13.5	13.5	89	63	84	79	1.7	8.5	2.6	4.3	7.0	6.7	5.5	6.4
VIII	997.0	1006.8	985.9	1013.3	19.8	11.4	26.6	12	5.9	10,15	13.6	18.1	14.5	15.2	14.2	14.4	14.5	14.4	90	69	87	82	1.5	6.7	2.2	3.5	7.2	7.7	6.2	7.0
IX	997.9	1014.4	977.8	1014.4	15.8	8.0	25.7	4	1.7	25	9.5	14.6	10.7	11.4	11.2	11.9	11.7	11.6	94	73	90	86	0.8	5.1	1.4	2.4	6.7	7.5	4.8	6.3
X	1004.6	1020.2	990.0	1021.3	12.2	4.0	19.8	3	-4.7	28	5.6	11.5	7.3	7.9	9.0	10.3	9.5	9.6	96	75	91	87	0.4	3.7	1.0	1.7	6.5	6.6	5.6	6.2
XI	1001.0	1015.6	982.8	1018.1	4.7	0.9	12.8	4	-5.9	26	2.2	3.9	2.8	2.9	6.9	7.2	6.8	7.0	94	87	90	90	0.4	1.1	0.8	0.8	8.6	8.9	8.0	8.5
XII	998.7	1031.5	958.5	1016.2	-2.7	-7.6	4.4	5	-22.0	23	-5.4	-3.8	-5.4	-5.0	4.1	4.4	4.0	4.2	90	87	88	88	0.4	0.6	0.5	0.5	7.5	7.6	7.4	7.5
Rok	997.9	1031.5	957.4	1014.7	9.8	2.3	28.9	16.VI	-23.0	31.I	4.6	8.5	5.5	6.0	8.6	8.8	8.7	8.7	90	74	86	83	1.0	4.2	1.5	2.2	7.6	7.6	6.3	7.2

Kwidzyń $\varphi = 53°44'$ $\lambda = 18°55'$

I	–	–	–	–	2.4	-1.7	8.4	22	-17.8	31	0.3	1.7	0.4	0.7	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.5	8.0	7.6
II	–	–	–	–	1.5	-5.1	4.3	12,13	-14.6	1	-2.1	0.0	-1.0	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.8	7.7	8.0
III	–	–	–	–	2.8	-7.4	9.6	31	-17.0	9	-4.2	0.7	-1.7	-1.7	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.5	6.2	6.7
IV	–	–	–	–	15.1	–	27.0	21,23	–	–	6.4	12.8	8.8	9.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.7	7.1	6.8
V	–	–	–	–	16.1	–	23.1	28	–	–	8.6	13.0	11.0	10.9	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.7	7.5	7.1
VI	–	–	–	–	19.5	8.7	28.0	16	2.0	3	12.5	17.5	14.9	15.0	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.6	6.3	5.8
VII	–	–	–	–	20.6	10.2	27.0	21,26	6.1	30	13.8	19.1	16.2	16.3	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.0	6.5	6.4
VIII	–	–	–	–	20.1	11.2	26.5	12	6.6	10	14.3	18.8	16.4	16.5	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.5	6.7	6.5
IX	–	–	–	–	17.7	8.1	26.0	4	3.6	25	10.3	15.5	13.2	13.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.0	7.1	7.1
X	–	–	–	–	13.8	5.4	20.8	3	-0.6	15	6.7	11.9	8.6	9.0	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.4	5.5	5.8
XI	–	–	–	–	6.4	1.8	13.4	5	-3.5	25	3.1	4.8	3.8	3.9	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.3	8.6	8.6
XII	–	–	–	–	-1.3	-6.4	6.6	12	-18.7	24	-4.7	-3.0	-4.2	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.8	8.0	8.2
Rok	–	–	–	–	11.2	–	28.0	16.VI	-18.7	24.XII	5.4	9.4	7.2	7.3	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.7	7.1	7.0

Świdwin $H_s = 94\,m$ $h_w = 12{,}4\,m$ 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	Wiatr v > 15	◉	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	3	6.5	4.5	2.5	3	1.7	5.5	4.0	16.5	5.0	37.5	6.0	8.5	5.0	12.5	6.6	2	5.2	45	5.6	28	2	3	12	·	5	3	2	17	16	14	·	–	–	·
II	7	10.0	7	6.0	9	5.0	4.5	5.7	12.5	4.3	13.5	6.4	15	10.8	13.5	9.2	2	7.3	28	11.8	12	2	7	26	·	8	8	1	16	11	5	1	–	–	·
III	8	2.8	8	5.9	8	2.8	12.5	4.7	11.5	2.6	8	2.4	9.5	3.1	4.5	2.8	23	2.6	26	10.1	12	1	8	28	·	2	1	4	10	5	5	1	–	–	
IV	6	5.6	11	3.8	5.5	2.6	10	2.0	7	3.0	14	5.5	10.5	3.7	10	2.5	16	3.0	35	5.5	2	·	·	1	1	3	1	5	10	12	9	·	–	·	4
V	6	4.8	4.5	3.0	1	2.0	11.5	2.0	6.5	2.5	15.5	2.9	13	3.2	14	4.4	21	2.5	104	12.7	12	·	·	5	·	1	·	1	13	23	21	2	–	·	3
VI	14.5	4.2	2.5	10.2	1	3.0	2	1.0	4.5	1.7	13.5	3.8	23	5.3	9	2.3	20	3.3	75	16.1	28	·	·	1	2	3	2	5	6	13	13	3	–	·	4
VII	4	2.0	6.5	1.2	3	1.0	4	1.0	2.5	3.0	26.5	3.7	13.5	3.4	7	2.4	26	2.1	80	16.3	14	·	·	·	2	1	1	3	9	18	15	2	–	·	4
VIII	3	2.3	1	1.0	1	3.0	7.5	1.0	5.5	2.8	36.5	4.5	14	5.3	6.5	3.2	18	3.2	84	14.7	21	·	·	·	1	1	·	2	12	18	12	3	–	·	1
IX	1	5.0	7.5	1.0	2.5	1.0	5.5	1.4	7.5	2.5	21	4.8	14	2.4	9	1.7	22	2.1	55	10.9	4	·	·	·	·	1	·	5	9	13	11	1	–	·	2
X	5.5	1.4	4.5	1.0		·	4.5	1.0	20	1.7	5	2.2	13	4.1	6.5	3.5	34	1.5	10	3.7	26	·	·	4	·	·	·	7	12	7	3	·	–	·	1
XI	1	3.0	3	5.0	17.5	5.8	12	3.7	7.5	2.9	17	2.8	8	3.5	2	5.0	22	3.0	36	9.2	22	·	1	11	·	2	·	1	19	9	7	·	–	–	·
XII	1	1.0	2	1.0	14	1.3	5.5	1.7	10.5	2.0	31	3.7	6	3.0	4	2.8	19	2.1	27	7.8	11	8	17	27	·	1	1	3	19	9	6	·	–	–	·
Rok	60	4.0	62	3.5	65.5	2.4	85	2.4	112	2.8	239	4.1	148	4.4	98.5	3.9	225	3.2	605	16.3	14.VII	13	36	115	6	28	17	39	152	154	121	13	–	–	19

Połczyn-Zdrój $H_s = 50\,m$ $h_w = 14{,}5\,m$

I	3	3.0	·	·	·	·	6	3.7	4	2.2	55	3.5	4	2.8	9	2.6	12	2.8	54	7.8	23	2	3	13	·	·	·	·	19	14	13	·	9	3	–
II	5	4.2	12	3.5	1	2.0	4	4.2	8	3.2	28	4.5	3	4.0	20	4.4	3	4.0	49	15.3	12	2	7	24	·	1	·	·	18	13	7	2	6	20	–
III	4	3.0	8	3.4	1	2.0	20	2.4	3	2.0	16	3.2		·	11	3.1	30	1.9	35	13.2	12	3	5	28	·	·	·	2	6	11	8	1	15	15	–
IV	4	4.0	·	·	·	·	11	3.3	4	2.2	22	2.9	6	3.0	21	3.4	22	2.4	32	12.6	16	·	·	1	1	·	·	·	8	8	7	1	9	·	–
V	4	2.8		·	1	4.0	7	3.1	3	2.7	39	2.4	1	5.0	23	3.2	15	2.3	95	10.8	17	·	·	4	·	·	·	·	14	24	22	1	1	·	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	·	·	·	3	–	–	–	–	–	–	–	–	·	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	62	10.0	2	·	·	·	5	–	–	–	–	14	13	1	1	·	–
VIII			·	·			3	2.7	3	2.3	30	2.9	4	2.2	28	3.7	25	2.3	116	21.8	7	·	·	·	1	·	·	1	12	20	16	3	4	·	–
IX	1	1.0			1	3.0	8	3.8	3	2.3	30	3.5	3	4.7	10	4.0	34	2.2	48	6.2	8	·	·	·	1	·	·	3	7	13	13	·	6	·	–
X					2	3.0	9	2.1	13	2.3	32	2.5	1	3.0	5	2.4	31	1.6	47	19.4	5	·	·	5	·	·	·	3	11	8	6	2	13	·	–
XI	2	3.5	6	5.2	3	1.3	27	2.5	7	2.3	20	2.2	4	2.2	7	3.1	14	2.2	35	8.6	29	·	·	10	·	·	·	1	16	13	9	·	7	1	–
XII	4	1.0			2	1.0	9	2.9	4	4.0	30	3.4	3	5.3	9	2.8	32	2.1	35	10.7	11	8	15	25	·	·	·	4	14	10	7	1	5	4	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	15	30	110	11	–	–	–	–	–	–	–	–	43	–

Olsztyn-Dajtki $H_s = 133\,m$ $H_b = 135{,}4\,m$ $h_w = 12\,m$

I	3.5	6.1	4.5	4.3	2.5	3.0	1.5	3.7	19	4.6	39.5	4.5	19.5	5.1	·	·	3	4.5	36	7.4	20	3	4	18	·	1	·	1	20	18	10	·	5	19	·
II	8	6.0	6.5	6.1	9.5	3.8	3	3.5	12.5	5.0	19.5	4.6	15	6.5	9	7.2	1	5.3	37	7.4	16	3	13	27	·	5	·	1	19	18	11	·	3	28	·
III	12.5	5.7	7	3.1	10.5	2.3	16.5	2.5	9.5	2.6	7.5	2.5	7.5	4.0	9	4.6	13	2.9	37	9.8	5	8	13	29	·	·	·	3	11	10	8	·	5	31	·
IV	11.5	1.8	8	2.8	5.5	4.2	9	2.6	12	3.2	16.5	3.2	9.5	2.5	12	4.2	6	3.0	22	5.6	5	·	·	5	2	·	·	1	8	13	7	·	8	2	1
V	4	3.0	7	2.1	6	2.0	4.5	2.7	13.5	1.9	19	2.6	20.5	3.0	15.5	3.1	3	2.5	98	21.2	14	·	·	5	·	·	·	·	18	27	16	3	7	·	5
VI	11.5	4.6	3.5	5.9	-	·	3	1.0	6.5	1.5	15.5	2.4	29	3.9	17	2.7	4	3.1	37	9.0	23	·	·	·	3	·	·	1	9	12	10	·	2	·	2
VII	13	2.5	1.5	2.3	1	3.0	3.5	1.3	6	2.7	18.5	2.6	26	3.8	15.5	2.8	8	2.7	97	26.5	13	·	·	·	3	·	·	·	8	17	11	3	3	·	6
VIII	7	2.3	0.5	1.0	2	2.5	1.5	1.3	7.5	3.1	33	3.7	27.5	3.7	11	2.6	3	3.2	116	19.4	4	·	·	·	3	·	·	2	16	15	14	4	4	·	7
IX	5.5	3.5	1	3.5	12.5	2.2	1.5	1.3	9	3.3	22	3.0	22	4.7	7.5	3.6	9	3.1	77	26.6	18	·	·	·	1	·	·	2	12	18	14	1	3	·	1
X	7	1.5	0.5	1.0	1	1.0	9.5	1.3	12	2.1	25.5	2.8	17	3.4	8.5	4.1	12	2.3	40	3.4	28	·	·	7	·	·	·	5	14	9	4	·	13	·	·
XI	6	2.2	4	5.4	15.5	6.1	18.5	4.0	9.5	2.6	19.5	2.3	9.5	3.4	2.5	2.6	5	3.5	45	12.8	20	·	·	10	·	·	·	1	21	15	10	1	10	8	·
XII	12	2.0	13	3.2	2.5	2.2	4	3.0	13	3.5	27	4.7	14.5	3.5	2	3.0	5	3.4	15	3.1	11	10	15	26	·	·	·	3	18	16	5	·	3	20	·
Rok	101.5	3.4	57	3.4	68.5	2.7	76	2.4	130	3.0	263	3.2	217.5	4.0	109.5	3.4	72	3.3	627	26.6	18.IX	24	45	127	12	6	·	20	174	188	120	12	66	108	22

UWAGA. *Kierunki i prędkości wiatru - wg anemometru.*

Kwidzyń $H_s = 15\,m$ $h_w = 13\,m$

I	1.5	3.7	7	1.7	3	2.0	17.5	3.1	23	3.2	31.5	5.3	6	3.6	3.5	1.1	·	3.7	–	–	–	3	3	15	·	3	·	1	13	–	–	–	·	–	·
II	6	2.5	11	2.9	3.5	2.1	8	1.8	17.5	2.1	9.5	4.8	11	5.3	11.5	5.3	6	3.2	–	–	–	3	5	24	·	3	·	·	17	–	–	–	1	–	·
III	5	1.8	10.5	3.0	7	3.4	21.5	2.1	8.5	2.3	6	2.3	2.5	3.8	8	2.6	24	1.9	25	9.5	6	9	2	31	·	·	·	3	11	5	5	·	3	–	·
IV	12.5	2.1	7	3.7	4.5	2.4	12.5	2.9	11	2.2	16.5	4.1	2.5	1.8	7.5	2.3	16	2.4	23	6.3	5	·	·	–	2	·	·	·	6	11	7	·	2	·	·
V	10.5	2.5	3.5	1.6	3	1.0	8	1.6	13	1.4	20.5	2.1	4.5	2.8	8	3.8	22	1.6	82	17.3	14	·	·	–	·	·	·	·	8	17	14	1	2	·	9
VI	8.5	4.3	5.5	2.5	5.5	2.0	1.5	1.0	14	1.9	15.5	3.4	10	3.0	7.5	2.1	22	2.1	55	9.3	12	·	·	·	1	·	·	·	3	14	10	·	·	·	4
VII	3.5	1.3	7	1.7	3	2.0	4.5	1.0	13	2.4	20.5	2.5	14.5	2.3	6	2.5	21	1.7	69	13.4	13	·	·	·	3	·	·	·	4	16	11	2	·	·	7
VIII	2	1.0	1	1.0	2.5	1.6	4	1.9	15.5	2.2	21.5	2.6	15	2.7	3.5	1.0	28	1.6	57	11.8	24	·	·	·	1	·	·	·	4	16	14	1	·	·	5
IX	3	2.3	1	1.0	4	1.2	8	1.6	18.5	1.1	18.5	3.1	10.5	2.9	6.5	1.9	20	1.8	57	19.7	18	·	·	·	1	·	·	·	9	11	10	1	2	·	4
X	3	3.8	0.5	1.0	1	3.0	9.5	2.2	18	2.5	15	3.1	8.5	3.2	4.5	4.0	33	1.9	11	5.6	31	·	·	3	·	1	·	4	9	3	3	·	8	·	·
XI	4.5	1.4	4.5	1.6	11	3.6	11	4.3	28	3.3	20.5	3.0	3	1.7	0.5	3.0	7	2.9	49	6.2	19,20	·	·	10	·	1	·	1	24	15	15	·	14	–	·
XII	8	2.4	7.5	2.3	9	2.0	3.5	1.3	30	4.2	27	4.6	2.5	3.6	4.5	1.2	1	3.5	15	4.9	13	9	15	25	·	3	·	·	20	7	6	·	8	–	·
Rok	68	2.4	66	2.0	57	2.2	109.5	2.1	210	2.4	222.5	3.4	90.5	3.1	71.5	2.6	200	2.4	–	–	–	24	25	–	8	11	·	9	128	–	–	–	40	–	29

Prabuty $\varphi = 53°44'$ $\lambda = 19°13'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA t										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	P_{0m}	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	-	-	-	-	1.6	-0.5	7.8	22	-19.4	31	-0.4	0.6	-0.6	-0.2	5.4	5.6	5.3	5.4	87	84	86	86	0.8	1.0	0.8	0.9	8.4	8.0	6.9	7.8
II	-	-	-	-	-0.1	-4.8	3.6	12	-16.4	1	-3.1	-1.0	-2.4	-2.2	4.2	4.7	4.3	4.4	82	81	81	81	0.8	1.1	1.0	1.0	7.7	8.0	6.6	7.4
III	-	-	-	-	0.3	-6.8	8.5	31	-15.3	15	-4.8	-0.4	-3.3	-3.0	4.4	4.8	3.9	4.4	82	79	78	80	0.8	1.2	1.0	1.0	6.4	6.4	4.0	5.6
IV	-	-	-	-	14.0	4.2	27.4	23	-0.4	30	6.9	12.4	7.1	8.4	8.6	8.2	8.6	8.5	8.4	5.9	8.4	7.6	1.8	7.5	1.9	3.7	6.5	6.6	4.6	5.9
V	-	-	-	-	14.2	5.2	19.4	8	-3.0	6	8.8	12.4	9.0	9.8	9.8	9.6	10.1	9.8	8.5	6.6	8.6	7.9	1.7	5.0	1.7	2.8	7.5	7.9	5.6	7.0
VI	-	-	-	-	19.0	7.9	28.9	16	0.8	3	12.0	17.1	12.8	13.7	11.2	10.9	12.0	11.4	7.8	5.6	8.0	7.1	3.2	9.5	3.4	5.4	5.6	6.3	5.4	5.8
VII	-	-	-	-	20.1	10.0	27.3	21	6.0	30	13.7	18.7	14.5	15.4	13.7	13.1	13.9	13.6	8.7	6.1	8.4	7.7	2.3	8.9	2.9	4.7	6.1	6.3	5.8	6.1
VIII	-	-	-	-	19.7	10.9	26.5	12	7.5	10,14	13.4	18.0	14.7	15.2	13.5	14.0	14.5	14.0	8.7	6.8	8.6	8.0	2.0	7.1	2.4	3.8	6.4	7.4	5.2	6.3
IX	-	-	-	-	16.2	7.6	26.3	4	3.0	25	10.1	14.8	11.3	11.9	11.2	11.5	11.5	11.4	9.0	6.9	8.6	8.2	1.3	5.7	3.9	3.6	5.5	6.8	4.5	5.6
X	-	-	-	-	12.3	3.8	20.6	1	-3.9	28	6.2	11.4	7.5	8.2	9.1	10.2	9.5	9.6	9.3	7.6	8.9	8.6	0.7	3.7	1.2	1.9	6.4	7.1	5.3	6.3
XI	-	-	-	-	4.8	1.3	12.6	4	-4.4	25	2.7	4.1	3.2	3.3	6.8	7.1	6.6	6.8	9.1	8.8	8.6	8.8	0.9	1.4	1.2	1.2	8.4	8.1	7.1	7.9
XII	-	-	-	-	-2.7	-7.1	4.2	11	-19.0	23	-5.1	-3.6	-5.0	-4.7	4.0	4.2	4.0	4.1	8.7	8.2	8.7	8.5	0.6	0.8	0.5	0.6	7.4	6.9	6.8	6.9
Rok	-	-	-	-	10.0	2.6	28.9	16.VI	-19.4	31.I	5.0	8.7	5.7	6.3	8.5	8.7	8.7	8.6	8.6	7.2	8.4	8.1	1.4	4.4	1.8	2.5	6.9	7.1	5.6	6.5

Szczecinek $\varphi = 53°43'$ $\lambda = 16°41'$

I	995.4	1023.5	967.3	1013.3	2.4	-1.4	7.7	22	-14.5	31	0.3	1.4	0.3	0.6	5.9	6.0	5.7	5.9	9.2	8.7	8.8	8.9	0.6	0.9	0.8	0.8	8.7	8.6	7.9	8.4
II	997.1	1021.3	959.3	1015.1	1.0	-3.9	5.0	20	-13.6	1	-2.2	0.0	-1.3	-1.2	4.7	5.2	4.9	4.9	8.9	8.3	8.6	8.6	0.6	1.0	0.8	0.8	9.0	8.4	8.0	8.5
III	993.8	1000.5	966.1	1011.8	2.1	-5.8	11.4	30	-13.9	16	-4.2	1.3	-2.1	-1.8	4.2	4.6	4.5	4.4	9.1	8.9	8.3	8.1	0.4	2.2	0.9	1.2	8.0	7.0	6.4	7.1
IV	996.1	1011.3	970.4	1013.5	13.5	4.0	25.1	25	-0.8	30	5.8	12.2	7.9	8.4	8.5	9.2	9.1	8.9	9.0	6.5	8.2	7.9	1.0	6.0	2.2	3.1	7.6	7.0	6.2	6.9
V	995.0	1001.5	985.5	1012.2	13.8	5.6	19.3	19	-1.9	5	8.0	12.1	8.9	9.5	9.8	9.5	10.0	9.8	8.9	6.7	8.7	8.1	1.1	5.0	1.6	2.6	7.6	8.2	7.3	7.7
VI	1000.9	1014.7	987.4	1018.0	18.2	8.2	27.8	15	0.9	3	12.3	16.5	12.5	13.4	11.6	11.7	11.9	11.7	7.9	6.3	8.0	7.4	3.0	7.9	3.1	4.7	6.3	6.8	6.1	6.4
VII	996.8	1007.4	976.9	1013.8	19.8	9.7	27.4	26	4.7	29	13.3	18.5	13.8	14.8	13.7	13.6	13.9	13.7	8.9	6.4	8.7	8.0	1.7	8.2	2.2	4.0	7.0	7.5	5.4	6.6
VIII	996.9	1006.1	985.2	1013.9	18.8	11.2	28.2	12	5.2	10,14	13.3	17.5	14.3	14.8	13.9	14.4	14.1	14.1	9.0	7.3	8.6	8.3	1.5	5.9	2.3	3.2	8.1	8.5	6.3	7.6
IX	997.8	1012.9	976.7	1015.0	16.1	7.6	26.2	4	0.6	18,25	9.4	15.1	10.7	11.5	11.1	12.2	11.6	11.6	9.3	7.1	9.0	8.5	1.0	5.4	1.4	2.6	7.4	7.2	5.1	6.6
X	1004.2	1019.4	990.8	1021.7	12.4	4.5	21.2	2	-3.1	28	6.0	11.7	7.7	8.3	9.2	11.0	9.9	10.0	9.6	7.8	9.2	8.9	0.4	3.2	1.0	1.5	8.5	6.8	6.0	7.1
XI	999.2	1015.6	979.8	1017.0	4.9	1.5	12.5	5	-3.1	22	2.4	-4.4	3.1	3.2	6.9	7.4	7.2	7.2	9.3	8.8	9.2	9.1	0.5	1.2	0.6	0.8	8.6	8.4	8.7	8.6
XII	998.2	1031.4	954.2	1016.5	-1.9	-7.2	4.6	12	-18.9	22	-5.0	-3.0	-4.5	-4.2	4.3	4.7	4.3	4.4	9.3	8.8	9.2	9.1	0.3	0.6	0.4	0.4	7.5	7.8	6.4	7.2
Rok	997.6	1031.4	954.2	1015.1	10.1	2.8	28.2	12.VIII	-18.9	22.XII	5.0	9.0	5.9	6.4	8.6	9.1	8.9	8.9	9.0	7.5	8.7	8.4	1.0	4.0	1.4	2.1	7.9	7.7	6.6	7.4

Śliwice $\varphi = 53°43'$ $\lambda = 18°11'$

I	-	-	-	-	2.3	-2.3	8.2	22	-19.0	31	-0.4	1.0	-0.6	-0.2	-	-	-	-	-	-	-	-	-	-	-	-	8.7	8.0	8.5	8.4
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	2.2	-8.1	9.0	31	-18.5	15	-6.1	0.9	-3.4	-3.0	-	-	-	-	-	-	-	-	-	-	-	-	6.4	6.7	4.8	6.0
IV	-	-	-	-	14.6	3.4	29.4	23	-2.0	10	5.9	13.0	7.3	8.4	-	-	-	-	-	-	-	-	-	-	-	-	6.0	6.5	4.7	5.7
V	-	-	-	-	14.8	4.7	20.1	28	-4.3	1	8.2	12.7	8.8	9.6	-	-	-	-	-	-	-	-	-	-	-	-	7.1	8.5	6.9	7.5
VI	-	-	-	-	19.8	8.1	30.2	16	2.5	3	12.2	17.8	13.3	14.2	-	-	-	-	-	-	-	-	-	-	-	-	6.1	6.4	6.0	6.2
VII	-	-	-	-	21.1	9.9	28.8	26	5.3	30	13.7	19.0	14.2	15.3	-	-	-	-	-	-	-	-	-	-	-	-	5.7	7.7	6.2	6.5
VIII	-	-	-	-	20.6	11.3	28.1	12	6.0	10	13.2	18.9	14.7	15.4	-	-	-	-	-	-	-	-	-	-	-	-	7.1	7.4	6.9	7.1
IX	-	-	-	-	16.8	7.3	28.3	4	1.5	25	9.2	15.1	10.6	11.4	-	-	-	-	-	-	-	-	-	-	-	-	6.5	7.3	5.1	6.3
X	-	-	-	-	13.1	3.7	21.2	2,3	-4.4	28	5.4	11.8	7.0	7.8	-	-	-	-	-	-	-	-	-	-	-	-	6.8	6.7	4.9	6.1
XI	-	-	-	-	4.9	0.9	12.2	4	-4.5	24	1.9	3.9	2.7	2.8	-	-	-	-	-	-	-	-	-	-	-	-	8.4	8.3	7.8	8.2
XII	-	-	-	-	-2.0	-7.7	5.4	12	-20.9	21	-5.3	-3.4	-5.7	-5.0	-	-	-	-	-	-	-	-	-	-	-	-	7.9	7.6	6.4	7.3
Rok	-	-	-	-	-	-	30.2	16.VI	-20.9	21.XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Chojnice $\varphi = 53°42'$ $\lambda = 17°33'$

I	994.1	1018.7	963.6	1013.2	1.5	-1.9	7.0	22	-14.6	31	-0.3	0.5	-0.5	-0.2	5.5	5.7	5.4	5.5	8.9	8.7	8.8	8.8	0.7	0.8	0.7	0.7	9.1	8.9	8.6	8.9
II	992.4	1016.3	954.8	1014.7	0.2	-4.3	3.9	20	-14.3	1	-2.9	-0.9	-2.0	-2.0	4.4	4.8	4.5	4.6	8.6	8.2	8.4	8.4	0.7	1.0	0.8	0.8	9.0	8.7	7.7	8.5
III	989.6	1005.1	963.5	1011.9	4.0	-5.8	8.3	31	-11.1	14,16	-4.4	0.2	-2.6	-2.4	4.0	4.5	4.2	4.2	8.6	7.1	8.1	7.9	0.6	1.8	0.9	1.1	7.7	7.8	5.2	6.7
IV	992.1	1007.3	966.3	1013.6	13.2	4.2	26.0	23	-0.7	30	5.7	11.9	7.8	8.3	8.2	8.8	8.6	8.5	8.6	6.4	7.9	7.6	1.4	6.5	2.6	3.5	7.3	7.3	5.1	6.6
V	990.9	998.1	978.9	1012.3	13.5	5.4	18.4	19	-2.9	1	7.9	12.2	8.5	9.3	9.5	9.6	9.7	9.6	8.8	6.7	8.6	8.0	1.3	4.9	1.7	2.6	7.3	9.0	7.0	7.8
VI	996.5	1009.9	983.4	1017.8	18.3	8.2	27.2	16	2.2	4	11.6	16.4	12.5	13.2	11.4	11.4	11.4	11.4	8.1	6.1	7.6	7.3	2.6	8.0	3.6	4.7	6.9	7.2	6.3	6.8
VII	992.7	1003.1	974.1	1013.7	19.6	9.4	26.7	26	5.9	5	13.1	18.2	13.3	14.5	13.6	13.5	13.4	13.5	8.9	6.5	8.7	8.0	1.7	8.1	2.1	4.0	6.1	8.0	5.4	6.5
VIII	992.8	1002.2	982.5	1013.8	19.1	10.8	26.1	12	7.5	9,14	12.9	17.6	13.6	14.4	13.6	14.3	13.7	13.9	9.0	7.1	8.7	8.3	1.4	6.2	2.0	3.2	7.8	8.4	6.6	7.6
IX	993.7	1009.2	973.0	1015.0	15.8	7.4	25.6	4	3.8	24	9.2	14.9	10.5	11.3	10.9	11.7	11.2	11.3	9.3	6.9	8.8	8.3	0.9	5.7	1.7	2.8	7.4	7.5	5.2	6.7
X	1000.1	1015.2	987.0	1021.9	12.0	4.7	20.7	3	-0.1	16,21	5.8	11.1	7.9	8.2	8.9	10.2	9.8	9.6	9.4	7.6	8.9	8.6	0.5	3.5	1.2	1.7	8.1	7.7	5.6	7.1
XI	995.3	1011.0	976.0	1017.4	4.3	1.1	11.9	5	-5.7	24	1.9	3.7	2.7	2.8	6.6	7.1	6.9	6.9	9.1	8.7	9.0	8.9	0.6	1.2	0.7	0.8	8.7	8.7	8.9	8.8
XII	993.9	1026.7	951.6	1016.5	-2.4	-7.3	4.4	12	-19.1	22	-5.2	-3.6	-5.0	-4.7	4.0	4.4	4.0	4.1	8.8	8.7	8.7	8.7	0.5	0.6	0.5	0.5	7.7	7.5	5.8	7.0
Rok	993.4	1026.7	951.6	1015.1	9.7	2.7	27.2	16.VI	-19.1	22.XII	4.6	8.5	5.6	6.1	8.4	8.8	8.6	8.6	8.8	7.4	8.5	8.2	1.1	4.0	1.5	2.2	7.8	8.0	6.4	7.4

Prabuty $H_s = 98\,m$ $h_w = 12\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU nD, vmD: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n) Temperatura T: Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v: v≥10	v≥15	◐	●	Opad R: R≥0.1	R≥1.0	R≥10.0	≡	⊞	R
I	4	5.0	1	12.0	·	·	4	6.0	12	5.8	38	6.7	24	4.2	6	1.8	4	5.3	23	5.1	25	3	3	17	·	8	1	2	15	15	10	·	4	-	·
II	11	8.0	12	5.6	6	6.0	3	8.3	4	5.0	23	5.6	13	5.2	12	5.2	·	5.9	41	7.2	16	3	10	23	·	11	4	1	16	19	10	·	3	-	·
III	20	4.4	5	5.0	1	3.0	6	4.5	17	5.0	11	3.3	15	2.3	11	2.5	7	3.5	40	13.5	12	10	12	29	·	3	1	5	10	10	7	2	5	-	·
IV	17	4.4	8	4.1	4	5.2	4	7.0	10	6.0	17	4.4	11	2.3	10	2.3	9	3.8	25	6.2	27	·	·	1	2	3	1	2	8	10	6	·	2	·	·
V	11	3.0	5	5.0	·	·	4	4.0	7	5.7	19	4.6	24	2.4	15	2.3	8	3.1	143	43.6	14	·	·	3	·	3	·	·	10	17	14	4	3	·	8
VI	17	5.6	3	5.3	·	·	·	·	6	3.0	13	4.3	22	4.7	21	2.3	8	3.8	69	25.8	29	·	·	·	4	4	·	1	9	12	12	1	·	·	3
VII	15	2.4	4	3.2	·	·	1	2.0	6.5	5.0	16.5	3.8	17	2.6	24	1.8	9	2.5	112	26.7	12	·	·	·	3	·	·	·	7	12	10	4	4	·	7
VIII	3	1.7	2	2.0	1	3.0	2	2.5	2	5.0	28	4.4	25	3.4	18	2.2	12	3.0	114	14.6	15	·	·	·	1	1	1	2	8	17	14	7	3	·	6
IX	6	2.3	2	5.5	5	3.0	1	2.0	4	3.2	21	4.9	20	4.1	15	2.4	16	3.1	95	27.2	18	·	·	·	1	3	1	4	9	13	12	4	2	·	3
X	8.5	1.8	·	·	·		1	3.0	14	3.5	25	3.1	21	2.5	9.5	2.9	14	2.4	47	6.5	6	·	·	7	:	·	·	3	10	7	4	·	12	·	·
XI	8	2.5	4	6.8	11.5	4.0	13.5	8.2	10	4.4	15	3.3	16	2.1	8	2.6	4	3.9	31	6.2	20	·	2	10	·	4	·	2	18	12	9	·	7	-	·
XII	10	2.0	8	2.9	6	2.7	1	3.0	8	4.4	25	5.2	15	2.9	7	4.9	13	3.1	24	7.7	13	10	15	26	·	3	·	5	17	15	4	·	6	-	·
Rok	130.5	3.6	54	4.8	34.5	2.2	40.5	4.2	100.5	4.7	251.5	4.5	223	3.2	156.5	2.5	104	3.6	734	43.6	14.V	26	42	116	11	43	9	27	137	159	112	22	51	-	27

Szczecinek $H_s = 137\,m$ $H_b = 142{,}6\,m$ $h_w = 12\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◐	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	R
I	2	7.0	5	3.8	·	·	3.5	2.3	16	4.8	40	4.9	20	4.5	4.5	6.0	2	4.6	47	7.6	12	2	3	15	·	3	·	1	23	22	14	·	5	14	·
II	8.5	8.4	9	5.3	8	3.9	0.5	5.0	10.5	3.7	20	4.2	17.5	5.2	10	8.6	·	5.4	56	17.6	12	2	12	23	·	8	·	1	20	18	8	2	4	20	·
III	6.5	6.2	8	3.2	2.5	1.8	10.5	4.8	18.5	2.8	6	1.5	14	3.0	4	5.1	23	2.6	28	9.6	12	4	7	28	·	·	·	2	16	15	8	·	6	23	·
IV	7	5.2	9	5.0	4	4.6	5	2.8	9.5	3.0	19	4.2	8.5	3.2	12	3.6	16	3.3	34	10.0	27	·	·	1	1	·	·	2	15	15	9	1	5	·	2
V	4	3.8	2	2.5	1	4.0	3.5	2.4	13.5	3.3	22	3.1	16	3.3	11	5.0	20	2.7	79	13.9	19	·	·	3	·	·	·	·	15	25	17	1	3	·	5
VI	8.5	6.3	3	5.0	·	·	1.5	1.0	4.5	3.8	21	4.0	26	3.8	13.5	3.6	12	3.5	72	14.0	19	·	·	·	3	2	·	1	8	16	13	3	·	·	5
VII	5	1.4	7	1.9	2.5	1.8	0.5	3.0	5	4.0	26.5	3.7	19	3.3	8.5	3.8	19	2.6	45	8.7	22	·	·	·	2	·	·	·	8	15	12	·	8	·	2
VIII	1.5	2.3	·	·	2	2.5	2	2.0	9	3.3	33.5	4.3	22	5.2	7	2.7	16	3.5	67	15.5	24	·	·	·	1	·	·	1	16	21	13	1	·	·	2
IX	2.5	3.2	·	·	3	2.3	8.5	3.1	10	3.1	26.5	4.6	21.5	3.4	3	5.8	15	3.2	47	9.3	12	·	·	·	1	1	·	1	8	15	11	·	4	·	3
X	4.5	3.2	1	4.0	·	·	3.5	3.1	20.5	3.1	24.5	3.0	15.5	3.5	6.5	3.5	17	2.6	43	3.9	4	·	·	5	·	·	·	2	15	7	5	·	13	·	2
XI	4	3.0	5.5	5.4	10	4.4	19.5	5.1	11	2.5	20	2.6	8.5	4.3	0.5	6.0	11	3.4	34	9.1	1	·	1	10	·	·	·	1	22	12	7	·	12	7	·
XII	3	1.5	7	2.6	7.5	1.8	4	1.8	13.5	3.5	28.5	3.5	13.5	2.9	4	3.1	12	2.6	29	5.4	11	12	17	26	·	·	·	2	17	14	8	·	10	17	·
Rok	57	4.3	56.5	3.2	40.5	2.0	62.5	3.0	141.5	3.4	287.5	3.6	202	3.8	84.5	4.7	163	3.3	551	17.6	12.II	20	40	111	8	14	·	14	183	195	125	8	70	81	21

Śliwice $H_s = 115\,m$ $h_w = 11\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◐	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	R
I	2	2.5	6	1.8	2	1.0	5	2.2	13	1.8	45	3.8	14	2.8	6	4.0	·	3.1	40	5.8	25	3	3	18	·	3	·	2	24	15	11	·	4	8	·
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	47	12.2	16	-	-	-	·	-	-	-	-	15	10	2	-	-	-
III	10	2.1	12	2.2	4	1.8	24.5	2.2	8.5	1.2	16	1.2	4	3.5	5	4.4	9	1.9	43	16.3	12	12	6	29	·	1	·	3	11	9	8	1	4	26	·
IV	7	3.3	6	2.8	7	2.1	12	2.2	12	2.0	26.5	2.8	4.5	2.7	8	2.1	7	2.3	35	9.2	5	·	·	4	4	·	·	4	6	12	8	·	3	·	2
V	1	3.0	5	3.6	3	1.7	17	1.5	17	1.3	30.5	1.6	7.5	2.0	10	3.2	2	1.8	125	31.3	14	·	·	4		2	·	·	12	22	15	3	2	·	5
VI	12	3.1	5.5	3.1	3.5	1.1	4	1.2	7.5	1.4	30	2.0	18.5	2.6	7	2.4	2	2.2	70	19.4	16	·	·	·	5	2	·	3	8	14	12	2	1	·	5
VII	5.5	1.5	4.5	1.6	6.5	1.5	4	1.5	10.5	2.0	37	1.7	17	2.1	4	2.5	4	1.7	63	18.8	26	·	·	·	5	1	·	·	11	18	11	1	1	·	4
VIII	3	1.3	3	1.3	3	2.3	2	2.0	9.5	1.4	42	2.6	19.5	2.6	1	2.0	10	2.1	112	26.0	7,24	·	·	·	4	·	·	1	13	14	12	3	1	·	4
IX	2	1.5	1.5	1.3	4.5	1.6	10	1.8	8	1.5	35	2.6	16	2.5	4	2.0	9	2.0	70	17.0	18	·	·	·	1	1	·	4	11	14	10	3	3	·	3
X	6	2.0	2	1.0	·	·	9	1.3	20	1.4	32.5	1.9	5.5	1.9	5	2.0	13	1.4	9	3.0	5	·	·	9	·	·	·	5	11	8	3	·	10	·	·
XI	4	2.0	6	3.3	11	2.4	20	3.0	15	1.2	22.5	2.0	2.5	1.4	1	2.0	8	2.0	56	23.7	1	·	1	13	·	·	·	2	19	14	9	1	8	5	·
XII	4	1.0	12	1.4	7	1.4	12	1.2	17.5	2.0	24	2.6	7.5	1.9	2	3.0	7	1.8	24	4.8	13	10	16	28	·	1	·	3	18	12	8	·	4	18	·
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	694	31.3	14.V	-	-	-	19	-	-	-	-	167	117	16	-	-	-

Chojnice $H_s = 172\,m$ $H_b = 177{,}2\,m$ $h_w = 12{,}5\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◐	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	R
I	3	8.2	5.5	3.0	1.5	2.7	5	3.6	11	5.5	35	6.3	21	7.0	11	5.0	·	5.8	36	6.4	25	2	4	17	·	12	2	1	25	22	11	·	5	9	·
II	5.5	7.4	13.5	4.6	5	4.8	3.5	3.7	7.5	5.7	19.5	6.9	15	7.8	14.5	9.1	·	6.8	25	7.2	5	2	12	24	·	10	5	·	19	16	5	·	7	21	·
III	10.5	4.0	12.5	3.0	5.5	2.4	23	3.4	9.5	3.2	3	1.8	7	3.4	11	4.5	11	3.0	30	9.4	12	3	8	29	·	1	·	2	12	11	9	·	7	25	·
IV	6.5	3.2	11	4.2	8.5	3.3	8.5	3.6	9	3.8	20	4.7	3	6.8	17.5	3.6	6	3.8	27	6.6	5	·	·	3	1	2	·	1	10	14	8	·	4	·	2
V	8.5	2.3	7	1.7	1	2.0	8.5	3.4	12	4.3	17.5	3.7	14.5	3.8	17	4.2	7	3.3	89	18.8	14	·	·	3	·	4	·	·	15	24	15	2	3	·	5
VI	10	5.2	5	3.9	·	·	6	2.9	5.5	2.5	19.5	4.8	19	4.4	22	3.8	3	4.1	60	14.9	16	·	·	·	3	5	·	1	10	15	11	1	3	·	5
VII	4.5	1.2	8.5	1.7	3.5	1.0	5.5	2.7	5.5	2.5	20.5	4.1	20	2.9	18	2.9	7	2.7	78	24.1	26	·	·	·	2	2	·	1	9	16	13	3	7	·	2
VIII	4	2.2	1	3.0	4.5	2.2	4.5	1.3	8.5	3.1	21.5	5.3	26.5	4.8	13.5	3.2	9	3.6	106	24.5	24	·	·	·	1	1	·	·	15	16	13	3	3	·	4
IX	·	·	3.5	1.7	8.5	2.8	7.5	2.7	4	3.2	22	4.8	24	4.2	9.5	3.1	11	3.3	75	15.9	19	·	·	·	1	3	·	2	12	16	11	2	7	·	4
X	6.5	1.9	1	2.0	1	1.0	15	2.6	11	2.4	16.5	3.2	15.5	4.5	8.5	4.5	18	2.6	31	22.7	5	·	·	2	·	2	·	3	16	6	4	1	14	·	·
XI	3.5	3.6	9	4.4	21.5	4.6	9	3.7	9	2.4	16.5	3.1	14	4.1	0.5	5.0	7	3.5	41	22.1	1	·	2	13	·	1	·	1	24	13	7	1	14	6	·
XII	3.5	2.9	16.5	1.9	7	1.9	4.5	2.2	9	3.4	16.5	6.1	15.5	4.6	5.5	1.6	15	3.0	22	5.5	13	10	17	28	·	4	·	3	16	16	9	·	9	18	·
Rok	66	3.5	94	2.9	67.5	2.4	100.5	3.0	101.5	3.5	228	4.6	195	4.9	148.5	4.2	94	3.8	620	24.5	24.VIII	17	43	119	8	47	7	15	183	185	116	13	83	79	22

Ostróda $\varphi = 53°42'$ $\lambda = 19°58'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PREŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{s.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.4	-2.6	8.2	22	-20.3	31	-0.7	0.4	-0.9	-0.5	5.3	5.4	5.2	5.3	86	81	85	84	0.9	1.1	0.8	0.9	8.3	7.7	7.0	7.7
II	–	–	–	–	-0.3	-5.3	4.1	12	-17.2	1	-3.4	-1.5	-2.7	-2.6	4.2	4.7	4.4	4.4	84	85	84	84	0.7	0.9	0.8	0.8	8.9	8.3	7.1	8.1
III	–	–	–	–	0.5	-6.8	9.2	31	-19.1	15	-5.2	-0.5	-3.3	-3.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.3	5.2	6.4
IV	–	–	–	–	14.1	4.8	27.6	23	-0.2	30	6.9	12.8	8.0	8.9	8.4	8.7	8.9	8.7	83	60	81	75	2.0	7.7	2.4	4.0	6.3	5.7	5.3	5.8
V	–	–	–	–	14.2	5.8	19.3	8,28	-1.5	6	8.5	12.6	9.3	9.9	9.9	10.3	10.2	10.1	87	70	85	81	1.5	4.7	1.8	2.7	7.5	7.0	6.3	6.9
VI	–	–	–	–	19.0	8.4	29.1	16	2.7	3	12.5	17.3	13.2	14.0	11.6	11.8	12.0	11.8	79	61	78	73	3.4	8.7	3.7	5.3	4.8	5.0	4.7	4.8
VII	–	–	–	–	20.3	10.7	28.4	21,26	6.4	30	13.7	18.7	14.1	15.2	13.8	13.5	13.7	13.7	88	63	85	79	2.0	8.6	2.6	4.4	5.8	5.5	5.3	5.5
VIII	–	–	–	–	19.8	11.3	26.4	12	6.4	10	13.4	18.2	14.6	15.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.5	6.3	6.5
IX	–	–	–	–	16.1	8.0	26.2	4	3.2	25	10.0	14.7	11.2	11.8	11.2	12.8	11.7	11.9	90	77	87	85	1.4	4.3	1.9	2.5	6.5	6.4	5.5	6.1
X	–	–	–	–	12.7	4.5	20.8	1,2,4	-2.5	28	6.1	11.9	7.5	8.2	9.0	10.8	9.5	9.8	92	76	89	86	0.8	3.6	1.2	1.9	7.4	6.5	6.6	6.8
XI	–	–	–	–	4.9	1.6	13.7	4	-2.5	25	2.5	4.2	3.0	3.2	6.8	7.2	6.8	6.9	91	86	88	88	0.7	1.3	1.0	1.0	8.9	8.3	7.5	8.2
XII	–	–	–	–	-2.7	-7.0	3.6	5	-20.6	23	-5.2	-3.8	-5.2	-4.8	4.1	4.3	4.0	4.1	87	85	85	86	0.5	0.7	0.6	0.6	8.0	7.0	7.2	7.4
Rok	–	–	–	–	10.0	2.8	29.1	16.VI	-20.6	23.XII	4.9	8.8	5.7	6.3	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.7	6.2	6.7

Trzebież $\varphi = 53°40'$ $\lambda = 14°31'$

I	–	–	–	–	4.1	-0.1	8.7	25	-13.9	31	1.5	2.9	1.9	2.0	6.3	6.4	6.5	6.4	90	83	89	87	0.7	1.3	0.8	0.9	7.5	8.3	7.4	7.7
II	–	–	–	–	2.9	-2.1	8.5	8	-12.1	1	0.1	1.9	0.6	0.8	5.4	5.8	5.5	5.6	88	80	85	84	0.8	1.4	1.1	1.1	7.9	7.6	6.5	7.3
III	–	–	–	–	3.1	-2.8	12.8	30	-8.7	14	-1.4	2.3	0.2	0.3	5.1	5.1	5.5	5.2	89	71	87	82	0.6	2.2	0.8	1.2	7.0	7.1	6.7	6.9
IV	–	–	–	–	13.0	3.8	27.0	25	0.0	1	6.0	10.8	7.5	8.0	8.5	9.1	8.9	8.8	90	70	85	82	1.0	4.6	1.8	2.5	6.8	6.7	6.4	6.6
V	–	–	–	–	13.8	5.8	20.4	19	-0.6	1	9.2	12.2	9.5	10.1	10.2	9.8	10.3	10.1	86	69	86	80	1.6	4.8	1.7	2.7	6.4	8.2	6.7	7.1
VI	–	–	–	–	18.2	9.0	28.2	19	2.0	8	12.8	16.4	13.2	13.9	12.2	12.9	12.0	12.4	81	68	77	75	2.8	6.5	3.6	4.3	5.2	6.1	3.8	5.0
VII	–	–	–	–	18.9	10.3	25.0	21	5.4	10	13.8	17.6	14.2	15.0	14.3	14.6	14.4	14.4	90	73	88	84	1.6	5.8	2.0	3.1	5.7	6.7	4.4	5.6
VIII	–	–	–	–	19.2	11.2	28.0	12	7.5	14	13.8	17.7	14.2	15.0	14.1	14.9	14.5	14.5	89	74	89	84	1.8	5.6	1.9	3.1	7.0	8.0	4.5	6.5
IX	–	–	–	–	16.6	7.6	24.5	4	2.6	25	10.0	15.6	11.1	12.0	11.7	12.4	12.0	12.0	95	70	90	85	0.7	5.7	1.4	2.6	6.6	6.8	4.4	5.9
X	–	–	–	–	12.9	5.2	22.5	2	0.4	15	7.0	11.7	8.8	9.1	9.8	11.5	10.6	10.6	96	82	92	90	0.4	2.6	1.0	1.3	7.4	6.7	5.4	6.5
XI	–	–	–	–	5.6	1.6	13.6	8	-3.9	24	3.1	4.9	3.4	3.7	7.3	7.6	7.3	7.4	95	87	93	92	0.4	1.3	0.7	0.8	7.9	8.4	6.2	7.5
XII	–	–	–	–	-0.2	-5.3	6.2	12	-15.0	22	-3.1	-1.5	-3.0	-2.6	4.7	4.9	4.8	4.8	92	86	91	90	0.4	0.8	0.4	0.5	8.2	7.4	5.9	7.2
Rok	–	–	–	–	10.7	3.7	28.2	19.VI	-15.0	22.XII	6.1	9.4	6.8	7.3	9.1	9.6	9.4	9.4	90	76	88	85	1.1	3.6	1.4	2.0	7.0	7.3	5.7	6.7

Nowogard $\varphi = 53°40'$ $\lambda = 15°07'$

I	–	–	–	–	3.3	-1.1	8.1	21,22,25	-16.8	31	0.7	2.1	0.7	1.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	2.2	-3.0	7.6	8	-13.0	1	-1.1	1.2	-0.4	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	3.5	-4.1	12.6	30	-10.4	14	-2.6	2.2	-0.8	-0.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	13.5	3.5	26.9	25	-0.7	11	5.5	12.0	7.2	8.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	14.0	5.3	19.9	19	-1.7	3	8.7	12.3	8.9	9.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	19.0	8.1	28.9	15	1.3	4	12.8	17.5	12.6	13.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	19.9	9.5	25.4	21	5.6	10	13.8	18.5	13.1	14.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	19.3	10.8	28.4	12	6.2	14	13.6	18.1	13.7	14.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	17.0	7.3	25.4	4	2.9	25	9.9	15.8	10.3	11.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	12.8	4.5	23.1	2	-0.9	15	6.4	11.9	7.7	8.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	5.4	1.1	13.8	8	-4.1	24	2.4	4.5	2.9	3.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-0.8	-6.4	5.1	12	-16.9	22	-4.4	-2.3	-3.9	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	10.8	3.0	28.9	15.VI	-16.9	22.XII	5.5	9.5	6.0	6.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Biebrza $\varphi = 53°39'$ $\lambda = 22°36'$

I	–	–	–	–	0.7	-3.9	5.0	22	-22.1	31	-1.6	-0.1	-1.7	-1.3	5.1	5.5	5.0	5.2	88	87	87	87	0.6	0.8	0.7	0.7	–	–	–	–
II	–	–	–	–	-1.1	-8.1	2.8	12	-21.9	1	-5.3	-2.6	-4.3	-4.1	3.9	4.3	4.0	4.1	89	83	86	86	0.5	0.9	0.6	0.7	–	–	–	–
III	–	–	–	–	0.2	-8.4	6.7	31	-20.1	2	-6.0	-1.2	-3.7	-3.6	3.7	4.6	4.1	4.1	88	80	84	84	0.4	1.1	0.7	0.7	6.9	5.8	5.5	6.1
IV	–	–	–	–	14.3	3.8	25.7	23	-2.2	8	6.5	12.9	8.2	9.0	8.8	9.6	9.3	9.2	89	66	83	79	1.2	6.4	2.2	3.3	6.1	5.4	4.2	5.2
V	–	–	–	–	14.8	4.5	19.9	27	-3.6	4	8.9	13.2	9.4	10.2	10.6	11.0	10.7	10.8	91	71	89	84	1.1	4.6	1.4	2.4	7.5	7.4	6.1	7.0
VI	–	–	–	–	18.8	6.8	27.2	23	-0.1	3	12.4	17.1	12.1	13.4	12.0	11.8	11.9	11.9	82	60	83	75	2.7	8.4	2.6	4.6	–	–	–	–
VII	–	–	–	–	20.6	8.5	26.8	21	3.4	8	13.7	18.6	13.9	15.0	13.9	14.7	14.1	14.2	88	69	89	82	1.9	7.2	1.9	3.7	5.6	6.3	5.2	5.7
VIII	–	–	–	–	20.5	9.9	26.1	13	1.6	15	13.3	18.9	14.3	15.2	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.7	5.9	6.7
IX	–	–	–	–	16.1	6.2	25.7	5	-1.7	25	8.1	14.7	10.0	10.7	10.3	11.7	11.2	11.1	94	70	90	85	0.7	5.4	1.3	2.5	6.5	6.7	4.9	6.0
X	–	–	–	–	12.0	1.6	18.3	3	-5.6	28	4.9	11.0	5.9	6.9	8.4	9.8	8.8	9.0	94	74	93	87	0.6	3.6	0.7	1.6	8.3	6.1	4.6	6.3
XI	–	–	–	–	6.0	0.6	14.9	1	-5.0	26	2.3	4.9	3.2	3.4	6.9	7.3	7.1	7.1	93	83	90	89	0.5	1.7	0.8	1.0	8.8	7.5	8.1	8.1
XII	–	–	–	–	-2.7	-8.3	3.7	5	-21.4	21	-5.5	-3.9	-5.9	-5.3	4.0	4.2	3.9	4.0	88	84	89	87	0.5	0.8	0.5	0.6	8.0	7.2	6.9	7.4
Rok	–	–	–	–	10.0	1.1	27.2	23.VI	-22.1	31.I	4.3	8.6	5.1	5.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Ostróda — $H_s = 106\,m$ — 1962

MIESIĄC	ROZKŁAD WIATRU (%, m/s) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	≥15	●	●	Opad R ≥0.1	≥1.0	≥10.0	≡	≡	≡
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	28	5.2	25	3	4	17	·	–	–	2	14	15	8	·	2	–	1
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	34	8.8	16	3	12	26	·	–	–	·	17	13	8	·	1	–	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	29	9.8	6	8	10	29	·	–	–	3	13	7	6	·	3	–	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	17	8.2	27	·	·	1	3	–	–	3	7	8	4	·	3	·	·
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	87	30.4	14	·	·	3	·	–	–	1	6	16	11	1	·	·	5
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	43	12.6	23	·	·	·	3	–	–	4	2	10	9	1	2	·	1
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	70	12.4	26	·	·	·	4	–	–	2	3	13	11	2	1	·	5
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	105	14.2	5	·	·	·	3	–	–	1	13	13	13	4	·	·	5
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	57	14.6	18	·	·	·	1	–	–	·	7	13	10	2	4	·	2
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	10	6.2	27	·	·	5	·	–	–	1	13	5	2	·	8	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	20	6.8	20	·	1	10	·	–	–	·	20	9	5	·	5	–	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	9	3.6	11	8	15	27	·	–	–	3	17	6	4	·	3	–	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	509	30.4	14.V	22	42	118	14	–	–	20	132	128	91	10	32	–	19

Trzebież — $H_s = 1\,m$ — $h_w = 18\,m$

I	3	9.0	4.5	8.7	1.5	2.7	3	3.3	15.5	5.3	4.5	6.3	12.5	5.8	7	7.1	1	6.1	39	5.5	25	2	3	11	·	7	2	3	19	21	12	·	6	3	–
II	3.5	11.0	1.0	9.4	13.5	6.9	0.5	8.1	4.5	4.7	16.5	7.1	2.0	8.1	14.5	9.7	1	8.0	42	13.6	12	1	6	22	·	9	6	2	14	14	8	1	3	7	–
III	9	7.4	1.0	6.2	5	4.5	1.1	6.7	17.5	4.1	5	3.2	6	3.6	13.5	5.2	1.6	4.4	25	9.5	27	·	3	26	·	7	·	7	17	12	6	·	1	7	–
IV	10.5	6.8	1.5	6.5	3	6.7	9	2.7	3.5	2.0	20.5	5.0	11.5	4.7	10	5.0	7	4.7	33	8.9	16	·	·	·	2	5	·	3	12	14	11	·	5	·	–
V	13.5	5.7	6.5	5.5	5.5	1.5	4.5	3.6	7	3.4	17.5	4.8	21	3.0	12.5	5.6	5	4.1	89	27.5	3	·	·	2	·	4	1	1	16	20	16	1	·	·	–
VI	11	6.5	10.5	6.5	·	·	1	4.0	7	2.6	9.5	4.6	19.5	5.2	16.5	5.2	1.5	4.4	73	24.9	19	·	·	·	2	4	1	4	4	9	7	2	·	·	–
VII	11.5	3.9	11	2.6	2	4.0	7.5	2.1	2.5	3.2	19.5	3.9	19	3.6	10	4.2	10	3.2	77	19.4	7	·	·	·	·	·	·	4	6	17	12	1	2	·	–
VIII	9	3.7	6	3.0	·	·	3.5	3.4	7.5	3.2	2.4	5.6	2.9	5.4	8	5.7	6	4.6	56	8.9	7	·	·	·	1	5	·	2	6	16	13	·	·	·	–
IX	3	5.0	1	1.0	2.5	2.6	12.5	5.5	6.5	2.1	17.5	5.6	24.5	4.9	12.5	6.4	1.0	4.5	51	18.5	4	·	·	·	·	3	1	4	6	11	9	1	5	·	–
X	1	1.0	3	2.3	1	3.0	8	2.3	1.9	3.2	1.6	4.1	11.5	4.1	12.5	4.7	2.1	2.8	14	6.9	4	·	·	·	·	·	·	3	13	7	2	·	11	·	–
XI	1.5	8.7	2	4.5	1.3	5.9	16.5	5.8	8.5	4.5	14.5	3.7	9	4.9	7	3.8	1.8	4.0	28	6.5	19	·	2	10	·	1	·	1	14	12	11	·	6	6	–
XII	1	5.0	2	4.0	9	4.0	9.5	4.9	6.5	3.1	2.3	4.6	11.5	4.0	7.5	5.2	2.3	3.3	34	8.0	11	7	1.5	24	·	1	·	3	15	12	8	·	7	5	–
Rok	77.5	6.1	81.5	5.0	5.6	3.5	86.5	4.4	105.5	3.4	228.6	4.9	195	4.8	131.5	5.6	133	4.5	561	27.5	3.V	10	29	95	5	46	11	37	142	165	115	6	46	28	–

Nowogard — $H_s = 60\,m$ — $h_w = 11\,m$

I	4	4.0	2	1.0	2	1.0		·	33.5	4.8	27.5	4.8	14.5	3.2	6.5	2.6	3	4.0	56	9.0	6	2	4	13	·	1	·	–	–	21	16		1	–	·
II	9	3.4	1	2.5	1.7	3.1		·	13.5	3.0	9.5	5.2	2.0	3.8	1.4	4.6		3.8	66	18.7	12	2	7	22	·	·	·	–	–	17	11	2	2	–	1
III	15.5	2.5	1.0	1.9	9.5	1.2	1.1	4.7	2.3	2.4	5.5	1.3	8	1.6	9.5	1.8	1	2.3	44	11.0	12	1	4	28	·	·	·	–	–	12	10	1	1	–	·
IV	14.5	2.3	9.5	4.2	8	3.7	3	2.0	21.5	3.9	11.5	4.1	1.0	4.2	1.1	2.0	1	3.4	41	11.0	16	·		1	2	1	·	–	–	13	10	1	5	·	2
V	14.5	3.2	6	1.7	2	2.0	·	·	17.5	3.1	19.5	2.4	2.1	2.7	5.5	3.0	7	2.5	107	10.4	12	·	·	4	·	·	·	–	–	25	22	1	8	·	4
VI	1.4	3.3	4.5	0.4	1	1.0	2.5	1.6	7	2.1	11.5	4.0	2.6	3.7	6.5	1.8	1.7	2.6	49	10.2	28	·	·	·	2	·	·	–	–	10	10	2	·	·	3
VII	1.3	1.2	4.5	1.0	5	1.2	2	1.0	6.5	2.8	2.4.5	3.2	1.9	2.3	4.5	2.0	1.4	1.9	88	31.3	7	·		·	1	·	·	–	–	18	15	2	·	·	5
VIII	7.5	1.3	1.5	1.0	2.5	1.0	1	3.0	1.7	3.8	22	5.7	2.4	2.3	6.5	1.9	1.1	3.0	77	20.0	24	·	·	·	1	2	·	–	–	18	12	3	3	·	2
IX	1.5	1.7	2	1.0	4	1.8	7	1.9	2.4	3.5	2.4	3.6	1.7	1.6	3.5	1.9	7	2.6	68	13.6	18	·	·	·	1	2	·	–	–	15	13	2	4	·	3
X	6.5	1.0	3.5	1.0	2	1.0	6.5	1.0	37.5	2.1	10.5	1.6	18.5	2.6	5	1.0	3	1.8	13	6.3	4	·	·	2	·	1	·	–	–	5	3	·	9	·	1
XI	4	1.5	2	1.0	7	4.4	1.8	4.4	3.6	2.8	8	2.3	12.5	2.9	0.5	5.0	2	3.1	38	9.7	30	·	1	11	·	1	·	–	–	13	8	·	8	5	·
XII	5	1.0	3	1.3	13.5	1.5	4.5	3.4	32.5	3.0	11.5	2.4	15.5	2.4	3.5	1.0	4	2.2	45	10.5	11	7	1.5	28	·	4	·	–	–	11	8	1	7	22	
Rok	1.09	2.2	49.5	1.5	73.5	1.9	55.5	1.9	269.5	3.1	185.5	3.4	206	2.8	76.5	2.4	70	2.8	692	31.3	7.VII	12	31	109	7	12	·	–	–	178	138	1.5	48	–	21

Biebrza — $H_s = 117\,m$ — $h_w = 13\,m$

I	3.5	6.7	2.5	6.4	2	4.0	3	4.0	19.5	4.6	26.5	6.5	21.5	6.9	3.5	8.6	9	5.6	11	17	13	3	8	23	·	7	3	–	–	12	6		1	18	–
II	9	6.1	3	7.0	1.2	6.7	5.5	4.8	11	6.3	18.5	7.1	5	9.4	8	9.1	1.2	6.0	16	3.1	9	11	16	27	·	6	3	–	–	11	6	·	·	28	–
III	8.5	7.6	1.0	5.5	1.0	3.6	15.5	4.4	1.4	4.3	4	2.2	4.5	7.1	4.5	7.3	2.2	3.8	25	7.5	31	1.2	1.3	30	·	3	1	3	11	14	6	·	·	19	–
IV	9	2.7	9	4.2	3.5	5.3	12.5	5.0	16	4.2	9	4.7	8	4.2	9	5.4	1.4	3.7	34	11.6	13	·		6	3	1	·	2	7	11	7	1	·	·	–
V	1.0	2.8	3	5.0	4.5	3.6	6.5	4.5	9.5	3.5	14.5	3.3	13.5	4.4	12.5	5.6	1.9	3.2	89	16.8	20	·	·	6	·	1	·	·	11	16	14	2	1	·	–
VI	9	5.8	8	5.7	·	·	1.5	3.0	10.5	2.7	13	4.8	20	5.0	16	4.5	1.2	4.0	31	9.1	23	·	·	1	2	1	1	–	–	9	6	·	1	·	–
VII	9	3.2	6.5	3.0	4	2.7	7	2.4	9.5	2.3	15.5	2.6	15.5	4.3	13	4.9	1.3	2.9	37	10.1	27	·	·	·	6	·	·	1	2	11	6	1	·	·	–
VIII	4.5	4.3	4	5.0	1.5	3.0	0.5	1.0	1.4	4.9	24.5	5.8	20	5.1	5	4.0	1.9	4.3	121	23.8	15	·	·	·	3	8	1	·	11	17	14	4	2	·	–
IX	5	3.6	2	2.5	6.5	2.4	7.5	2.5	9.5	3.8	22	5.8	17	5.4	8.5	5.6	1.2	4.0	58	16.0	18	·	·	2	1	4	·	2	10	17	7	2	3	·	–
X	7.5	3.7	2	2.2	1	2.0	6.5	1.6	1.2	2.9	12.5	3.9	17.5	4.5	1.0	4.8	2.4	2.7	10	3.8	19	·	·	10	·	3	·	1	8	6	3	·	4	·	–
XI	3.5	2.4	1.5	9.7	13.5	7.9	2.4	5.3	11.5	3.7	9.5	3.9	9	3.2	3.5	2.4	1.4	4.2	40	11.5	15	·	·	13	·	4	·	2	22	14	10	1	3	·	–
XII	7	3.0	2.0	3.5	5	3.6	1	4.0	2.0	4.0	1.8	5.4	13	3.5	6	1.8	3	3.7	13	4.2	14	11	1.5	26	·	1	·	4	18	15	4	·	·	17	–
Rok	8.5.5	4.3	71.5	5.0	63.5	3.7	91	3.5	157	3.9	187.5	4.7	164.5	5.2	101.5	5.3	1.73	4.0	485	23.8	15.VIII	37	52	144	15	39	9	–	–	153	89	11	15	82	–

Pisz $\varphi = 53°38'$ $\lambda = 21°48'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.0	-3.1	6.6	22	-23.4	31	-1.5	0.4	-1.3	-0.9	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.4	7.8	8.5
II	–	–	–	–	-0.6	-7.6	3.1	12	-20.5	1	-4.9	-1.9	-3.6	-3.5	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.1	9.1	8.6
III	–	–	–	–	0.6	-9.0	6.1	31	-21.7	2	-6.1	-0.3	-3.7	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.1	7.4	7.5
IV	–	–	–	–	14.5	4.0	27.3	23	-1.8	8	6.4	13.0	7.9	8.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.7	6.8	7.0
V	–	–	–	–	15.0	5.4	20.6	13	-3.0	1	8.4	13.3	9.4	10.1	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.4	8.0	8.2
VI	–	–	–	–	19.4	8.1	27.4	23	2.0	13	12.4	17.6	12.5	13.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.1	6.8	6.7
VII	–	–	–	–	21.0	9.6	29.3	21	5.0	30	13.6	19.1	13.9	15.1	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.5	6.7	7.2
VIII	–	–	–	–	20.9	10.5	28.1	7	4.0	15	13.7	19.1	14.2	15.3	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.2	6.7	7.1
IX	–	–	–	–	16.6	6.8	25.9	4	0.0	25	9.0	15.2	10.4	11.2	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.4	5.7	6.9
X	–	–	–	–	12.6	2.5	19.6	2.4	-4.4	28	5.5	11.7	6.1	7.4	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.1	7.3	7.7
XI	–	–	–	–	5.6	0.9	12.4	5	-7.1	25	1.9	4.6	3.0	3.1	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.8	9.4	9.2
XII	–	–	–	–	-2.3	-8.0	4.1	5	-21.7	31	-5.7	-3.5	-5.6	-5.1	–	–	–	–	–	–	–	–	–	–	–	–	7.8	8.1	8.6	8.2
Rok	–	–	–	–	10.4	1.7	29.3	21.VII	-23.4	31.I	4.4	9.0	5.3	6.0	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.6	7.5	7.7

Różanystok $\varphi = 53°38'$ $\lambda = 23°24'$

I	–	–	–	–	0.2	-3.5	4.7	22,23	-20.4	31	-1.9	-0.6	-1.7	-1.5	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.2	7.6	8.2
II	–	–	–	–	-1.9	-8.0	2.4	12	-18.4	1	-5.6	-3.4	-4.5	-4.5	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.9	6.9	7.7
III	–	–	–	–	-0.7	-7.9	5.9	31	-17.0	2	-6.3	-1.7	-4.1	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.7	6.5	6.8
IV	–	–	–	–	13.3	4.6	24.9	23	-0.7	8	6.2	12.0	8.2	8.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.0	6.6	7.0
V	–	–	–	–	14.5	6.1	21.0	27	-2.3	1	8.7	12.8	10.1	10.4	–	–	–	–	–	–	–	–	–	–	–	–	7.7	8.0	7.6	7.8
VI	–	–	–	–	18.3	8.4	26.2	23	2.1	3	12.2	16.7	12.4	13.4	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.6	6.4	7.0
VII	–	–	–	–	20.6	9.8	27.3	21	5.3	4	13.6	19.0	14.3	15.3	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.8	7.2	7.5
VIII	–	–	–	–	20.4	10.8	27.8	13	5.3	15	13.9	18.7	14.8	15.6	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.1	6.5	7.0
IX	–	–	–	–	15.8	7.5	25.7	5	2.5	25	8.8	14.1	10.7	11.1	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.6	5.8	6.8
X	–	–	–	–	11.6	3.8	19.2	2	-2.3	28	5.6	10.8	7.0	7.6	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.7	6.4	6.9
XI	–	–	–	–	5.5	1.1	15.5	1	-2.8	26	2.3	4.3	3.0	3.2	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.3	8.4	8.6
XII	–	–	–	–	-3.4	-8.4	2.7	8	-22.0	21	-5.9	-4.9	-6.1	-5.8	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.7	8.0	8.0
Rok	–	–	–	–	9.5	2.0	27.8	13.VIII	-22.0	21.XII	4.3	8.2	5.3	5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.6	7.0	7.5

Szczytno $\varphi = 53°34'$ $\lambda = 21°02'$

I	–	–	–	–	0.9	-3.6	6.9	22	-24.2	31	-1.4	0.1	-1.5	-1.1	5.2	5.3	5.0	5.2	8.9	8.2	8.5	8.5	0.6	1.1	0.8	0.8				
II	–	–	–	–	-0.8	-8.3	3.0	20	-21.3	1	-5.0	-2.0	-4.4	-4.0	3.9	4.4	4.1	4.1	8.7	8.3	8.6	8.5	0.6	0.9	0.6	0.7	8.7	8.5	5.2	7.5
III	–	–	–	–	0.8	-9.1	7.5	31	-22.5	2	-6.1	-0.2	-4.5	-3.8	3.7	4.6	3.9	4.1	8.8	7.5	8.5	8.3	0.4	1.5	0.6	0.8	6.9	6.6	4.6	6.0
IV	–	–	–	–	14.6	3.4	27.8	23	-3.0	8	6.8	13.4	7.2	8.6	8.6	8.8	9.0	8.8	8.5	6.0	8.5	7.7	1.7	8.2	1.7	3.9	–	–	–	–
V	–	–	–	–	14.2	4.4	19.5	13	-2.0	6	9.3	12.9	8.1	9.6	10.2	9.8	9.8	9.9	8.5	6.6	8.8	8.0	1.7	5.5	1.3	2.8	7.1	7.4	6.5	7.0
VI	–	–	–	–	19.2	7.3	27.5	16	2.0	13	13.3	18.1	11.0	13.4	11.9	11.0	11.3	11.4	7.6	5.3	8.4	7.1	3.8	10.6	2.2	5.5	5.5	5.4	4.6	5.2
VII	–	–	–	–	20.6	9.3	28.3	26	4.3	30	14.3	19.3	12.5	14.6	13.7	13.8	13.0	13.5	8.4	6.2	8.9	7.8	2.9	9.2	1.8	4.6	6.5	5.0	5.0	5.5
VIII	–	–	–	–	20.3	9.7	27.4	7	3.6	10	14.1	19.1	13.9	15.2	14.3	14.5	14.6	14.5	8.9	6.6	9.1	8.2	1.9	8.1	1.5	3.8	6.2	5.7	4.8	5.6
IX	–	–	–	–	15.8	6.4	25.3	4	-0.2	15	9.4	14.8	10.1	11.1	11.3	12.2	11.7	11.7	9.3	7.3	9.3	8.6	0.7	5.1	1.0	2.3	5.4	6.1	5.1	5.5
X	–	–	–	–	12.1	2.8	21.5	1	-4.6	28	6.3	11.6	6.2	7.6	9.2	10.7	9.0	9.6	9.4	7.8	9.3	8.8	0.6	3.3	0.8	1.6	6.6	5.3	5.6	5.8
XI	–	–	–	–	4.9	1.0	11.7	1	-6.8	26	2.5	4.4	3.0	3.2	6.8	7.1	6.8	6.9	9.0	8.3	8.8	8.7	0.7	1.5	1.0	1.1	8.6	8.2	6.5	7.8
XII	–	–	–	–	-2.6	-8.2	3.7	5,6	-21.1	21	-5.3	-3.7	-5.9	-5.2	4.0	4.3	3.8	4.0	8.7	8.4	8.4	8.5	0.5	0.7	0.6	0.6	8.0	6.8	6.7	7.2
Rok	–	–	–	–	10.0	1.3	28.3	26.VII	-24.2	31.I	4.8	9.0	4.6	5.8	8.6	8.9	8.5	8.7	8.7	7.2	8.8	8.2	1.3	4.6	1.2	2.4	–	–	–	–

Szczuczyn $\varphi = 53°34'$ $\lambda = 22°17'$

I	–	–	–	–	0.6	-3.7	5.6	22	-21.5	31	-1.5	-0.1	-1.5	-1.2	5.1	5.4	5.1	5.2	8.9	8.6	8.7	8.7	0.6	0.9	0.7	0.7	9.0	8.5	8.1	8.5
II	–	–	–	–	-1.3	-7.9	2.7	12	-19.5	1	-5.2	-2.6	-4.2	-4.0	3.8	4.5	4.1	4.1	8.6	8.3	8.6	8.5	0.6	0.8	0.7	0.7	8.6	8.0	7.1	7.9
III	–	–	–	–	-0.5	-7.7	5.6	31	-18.3	2	-6.0	-1.3	-3.7	-3.7	3.6	4.4	4.0	4.0	8.5	7.8	8.3	8.2	0.5	1.2	0.7	0.8	7.5	6.8	5.8	6.7
IV	–	–	–	–	14.0	4.0	25.8	22	-1.1	2	6.1	12.6	7.9	8.6	8.7	9.5	9.4	9.2	9.0	6.5	8.5	8.0	1.0	6.3	1.8	3.0	7.9	7.4	4.6	6.6
V	–	–	–	–	14.4	5.7	19.6	20	-2.0	1	8.5	13.0	9.6	10.2	9.9	9.7	10.3	10.0	8.8	6.4	8.5	7.9	1.4	5.7	1.8	3.0	8.8	8.9	7.5	8.4
VI	–	–	–	–	18.9	8.1	26.7	23	3.5	3	12.6	16.9	12.4	13.6	11.3	10.5	11.5	11.1	7.6	5.5	7.8	7.0	3.6	9.3	3.2	5.4	7.0	7.3	6.3	6.9
VII	–	–	–	–	20.3	9.9	27.2	21	5.8	4	13.6	18.5	13.8	14.9	13.8	13.0	13.6	13.5	8.8	6.2	8.5	7.8	1.9	8.7	2.4	4.3	7.3	8.0	6.3	7.3
VIII	–	–	–	–	20.6	10.8	27.0	7,13	3.1	15	13.9	19.0	14.1	15.3	14.0	14.1	14.4	14.2	8.8	6.4	8.9	8.0	2.0	8.3	1.8	4.0	7.6	7.8	5.6	7.0
IX	–	–	–	–	16.1	6.8	25.7	5	0.0	25	8.9	14.8	10.5	11.2	10.6	11.2	11.5	11.1	9.2	6.7	8.8	8.2	0.9	6.0	1.4	2.8	6.6	7.8	5.1	6.5
X	–	–	–	–	12.0	3.1	18.5	3	-4.0	28	5.3	11.0	6.3	7.2	8.5	9.8	9.1	9.1	9.4	7.4	9.3	8.7	0.6	3.7	0.7	1.7	7.5	7.3	5.3	6.7
XI	–	–	–	–	5.5	1.0	14.0	1	-3.2	26	2.1	4.6	3.1	3.2	6.8	7.0	7.0	6.9	9.3	8.2	8.9	8.8	0.5	1.7	0.9	1.0	8.5	7.8	8.3	8.2
XII	–	–	–	–	-3.0	-8.0	3.6	5	-21.6	31	-5.5	-4.2	-5.6	-5.2	4.0	4.2	4.0	4.1	8.8	8.5	8.8	8.7	0.5	0.7	0.5	0.6	8.2	8.1	7.7	8.0
Rok	–	–	–	–	9.8	1.8	27.2	21.VII	-21.6	31.XII	4.4	8.5	5.2	5.8	8.3	8.6	8.7	8.5	8.8	7.2	8.6	8.2	1.2	4.4	1.4	2.3	7.9	7.8	6.5	7.4

Pisz $H_s = 118\,m$ $h_w = 14\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU nD, vmD: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n) Temperatura T: Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v: v ≥ 10	v ≥ 15	◔	●	Opad R: R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	K
I	9	1.8	4	2.5	3	1.0	3	1.7	20.5	1.7	18.5	2.4	28	1.9	3	1.0	4	1.8	26	4.2	6	3	6	19	·	·	·	·	19	19	9	·	–	18	·
II	18	3.6	6	2.3	10	2.0	3	1.7	17.5	3.0	4.5	2.7	17	2.9	5	2.0	3	2.7	43	7.6	12	10	15	27	·	1	·	·	19	21	14	·	–	28	·
III	17.5	2.8	15.5	1.2	19	1.4	7.5	1.3	13	2.3	4	2.2	5	3.6	8.5	2.2	3	1.9	41	9.5	5	11	10	29	·	·	·	1	15	15	8	·	–	30	·
IV	23	1.8	9	1.4	16	1.4	9	1.9	14	1.9	3.5	2.0	6.5	1.5	3	1.7	6	1.6	29	9.5	13	·	·	6	2	·	·	1	11	13	6	·	–	·	1
V	29	1.5	7	1.4	16	1.5	2	2.0	12	1.7	4	2.2	10	2.1	9	1.7	4	1.7	115	21.5	15	·	·	4	·	·	·	·	18	23	18	4	–	·	3
VI	33	2.2	4	2.5	10	1.0	3	1.7	7	1.7	3	1.0	20	2.9	10	1.8	·	2.1	38	12.0	23	·	·	·	4	·	·	1	11	43	10	1	–	·	2
VII	26	1.7	12	1.1	4	1.0	5	1.8	13	1.8	2	2.0	15	2.6	13	2.0	3	1.8	80	22.8	13	·	·	·	4	·	·	·	13	17	16	2	–	·	4
VIII	16	1.5	5	1.0	4	1.5	3	1.0	10	1.9	4.5	1.8	39	2.2	10.5	1.7	1	1.8	133	31.2	17	·	·	·	4	·	·	·	11	16	16	5	–	·	5
IX	14.5	1.8	11.5	1.2	7	1.3	6	1.3	11	1.9	7	1.7	25.5	2.4	5.5	1.6	2	1.8	59	28.7	18	·	·	·	2	·	·	·	10	14	12	1	–	·	3
X	19	1.5	4	1.2	10	1.1	6	1.7	12	1.6	15	1.7	21.5	1.9	10	2.1	9	1.5	13	6.2	28	·	·	9	·	·	·	·	13	10	4	·	–	·	·
XI	12	1.3	6	2.3	26	2.7	16.5	2.3	13.5	1.6	4	2.5	9	1.7	·	·	3	2.1	51	12.5	20	·	·	9	·	·	·	·	24	14	9	1	–	1	·
XII	11	1.5	20	1.2	13	1.2	8	1.9	15	2.8	5	2.4	18	2.2	3	1.3	·	1.8	18	5.0	15	10	16	25	·	·	·	2	20	15	6	·	–	17	·
Rok	228	1.9	104	1.6	138	1.4	72	1.7	158.5	2.0	61.5	2.0	214.5	2.3	80.5	1.6	38	1.9	646	31.2	17.VIII	34	47	128	16	1	·	5	184	190	128	14	–	94	18

Różanystok $H_s = 160\,m$ $h_w = 12\,m$

I	2	5.7	7.5	4.1	2.5	1.6	1	3.0	18.5	6.5	47.5	8.5	10	6.8	4	4.4	·	7.1	12	2.1	13	3	10	20	·	14	3	1	20	16	6	·	1	19	·
II	7.5	10.5	7.5	6.1	9	4.0	2.5	4.4	21.5	5.3	19	9.2	8	7.1	7	12.8	2	7.2	10	3.0	16	9	16	28	·	12	4	·	11	9	4	·	·	28	·
III	11	7.8	10	7.2	11	2.6	13.5	3.8	16.5	3.8	11	4.3	8	6.9	9	5.6	3	4.9	23	4.4	5	9	17	29	·	6	2	3	14	14	8	·	3	31	·
IV	6	3.0	9.5	3.8	3	4.5	10	4.3	16	3.5	18.5	5.3	12	3.0	11	5.7	4	4.0	44	8.8	13	·	·	3	·	2	·	3	13	13	10	·	3	1	2
V	7	4.6	2.5	4.4	2	5.5	7.5	3.8	7.5	2.5	22.5	4.0	12.5	5.2	28.5	4.1	3	4.0	83	13.9	27	·	·	2	·	3	1	·	16	20	15	1	2	·	1
VI	12	7.4	3.5	12.7	0.5	2.0	1	3.0	8.5	3.6	22	5.3	21	5.2	17.5	3.6	4	5.1	35	13.9	4	·	·	·	2	4	2	·	10	11	8	1	1	·	1
VII	7.5	4.3	2.5	5.4	·	·	1	4.0	17	3.6	18	3.8	23	5.7	17	4.7	7	4.2	24	4.8	10	·	·	·	5	2	1	·	12	13	9	·	·	·	5
VIII	6.5	4.5	2.5	2.0	2	1.5	2.5	1.2	13.5	3.5	37.5	6.5	16.5	4.5	6	3.9	6	4.6	128	23.9	7	·	·	·	2	6	1	·	9	16	15	5	4	·	6
IX	5.5	3.4	6.5	3.2	1.5	2.7	6	3.2	15	3.8	28	7.4	15	5.6	5.5	3.9	7	4.8	54	24.4	18	·	·	·	1	7	1	1	14	13	9	2	1	·	1
X	1	6.0	0.5	5.0	1.5	1.3	8.5	3.1	16.5	3.4	19.5	5.0	19.5	4.2	12	4.5	14	3.5	1	0.3	19,27,31	·	·	5	·	1	1	1	13	7	·	·	7	·	·
XI	5	4.2	8	6.0	18.5	4.5	18	4.2	14.5	2.9	10	4.6	10	5.2	5	3.6	1	4.3	32	5.3	15	·	·	12	·	3	·	1	25	13	10	·	5	3	·
XII	15	3.6	14	3.8	1	2.0	3.5	2.1	14.5	4.9	22.5	7.3	11	5.1	10.5	5.4	1	5.0	11	–	–	11	18	27	·	4	·	2	19	12	4	·	·	19	·
Rok	86	5.4	74.5	5.3	52.5	2.7	75	3.3	179.5	3.9	276	5.9	166.5	5.4	133	5.2	52	4.9	457	24.4	18.IX	32	61	126	10	64	16	12	176	157	98	9	27	101	16

Szczytno $H_s = 144\,m$ $h_w = 15{,}3\,m$

I	6	6.0		·	1	2.0	3	1.3	15	3.2	25.5	4.7	20.5	4.9	16	3.6	6	3.9	28	5.5	20	3	6	21	·	–	–	–	–	15	9	·	–	19	·
II	10.5	6.9	2	5.5	7.5	3.3	7.5	2.2	6	4.4	8	7.1	28	6.6	12.5	8.8	2	6.0	36	5.9	16	9	13	26	·	–	–	·	14	19	11	·	–	28	·
III	11	4.1	4.5	4.2	2	1.0	21	1.8	10	3.2	7.5	1.5	9.5	2.6	13.5	3.2	14	2.3	38	10.2	12	11	8	30	·	–	–	6	13	10	8	1	–	31	·
IV	15	1.8	1.5	1.7	6	2.8	7	2.3	11	2.6	13.5	2.0	14.5	2.3	15.5	3.1	6	2.2	34	9.5	13	·	·	7	2	–	–	–	–	13	6	·	–	·	·
V	7	2.4	2.5	2.4	4	2.2	4	3.2	8.5	2.5	16	3.6	31.5	2.3	16.5	2.7	3	2.6	111	20.6	14	·	·	6	·	–	–	2	13	25	19	4	–	·	3
VI	16.5	5.4	·	·	·	·	1	3.0	1	1.0	7	2.8	27	3.8	24.5	3.3	13	3.3	23	6.3	2	·	·	·	3	–	–	6	4	12	6	·	–	·	1
VII	11	2.0	0.5	2.0	·	·	·		8	3.5	9.5	3.8	25.5	3.4	35.5	3.3	3	3.2	67	16.1	26	·	·	·	3	–	–	2	3	15	12	1	–	·	4
VIII	3	2.7	1	2.0	·	·	2.5	3.2	5.5	2.8	17.5	3.4	38.5	3.5	23	3.5	2	3.3	111	32.3	17	·	·	·	3	–	–	3	7	14	14	2	–	·	6
IX	3.5	2.0	·	·	4	1.5	9	1.7	8	4.8	13.5	4.4	27.5	3.3	20.5	3.5	4	3.2	56	25.2	18	·	·	1	1	–	–	7	11	17	12	1	–	·	2
X	4	2.5	·	·	·	·	1.5	1.0	15	2.3	13	2.4	21.5	2.7	20	2.3	18	1.9	17	3.9	5	·	·	8	·	–	–	8	13	10	6	·	–	·	·
XI	2	2.0	4	1.5	14.5	4.6	16.5	4.2	15	1.9	10	2.9	14	2.9	5	1.2	9	2.8	54	15.5	20	·	1	10	·	–	–	1	19	17	11	1	–	3	·
XII	7.5	2.0	9	1.8	8	1.9	3.5	3.1	5.5	4.5	17	3.5	21	3.9	7.5	1.7	14	2.5	15	3.5	10	9	16	26	·	–	–	4	19	15	5	·	–	17	·
Rok	97	3.3	25	1.8	47	1.6	76.5	2.2	108.5	3.1	158	3.5	279	3.5	210	3.4	94	3.1	590	32.3	17.VIII	32	44	135	12	–	–	–	–	182	119	10	–	98	15

Szczuczyn $H_s = 130\,m$ $h_w = 15\,m$

I	4	5.0	5.5	3.3	1	2.5	3.5	3.4	21.5	5.2	35	7.4	16.5	6.6	5	3.4	1	5.9	13	2.0	21	3	8	20	·	7	3	1	23	16	7	·	2	21	·
II	8	5.1	6	6.4	9	4.4	7	4.6	13	5.9	16	7.9	11	6.3	11	6.3	3	6.0	22	4.0	12	10	16	28	·	7	3	·	15	18	9	·	2	28	·
III	7.5	4.8	9	4.1	7.5	3.2	19	4.2	4	3.0	5	5.8	5.5	6.3	8.5	4.7	27	3.1	37	7.4	31	9	15	29	·	2	·	3	14	15	10	·	4	31	·
IV	7.5	3.1	8	4.4	5.5	4.2	14	4.1	12	4.2	8.5	4.4	8.5	3.4	12	4.4	14	3.4	24	11.3	13	·	·	4	3	2	·	1	11	9	5	1	2	3	2
V	2.5	2.4	4.5	3.2	3	3.3	7	2.9	9.5	3.2	10.5	4.0	26.5	3.3	15.5	4.0	14	2.9	94	19.8	20	·	·	4	·	2	1	·	19	22	15	1	·	·	6
VI	13.5	4.9	4.5	6.3	0.5	3.0	3.5	1.9	7	3.7	18	5.4	21	4.9	12	3.0	10	4.1	34	9.7	23	·	·	·	2	4	1	1	11	11	7	·	·	·	3
VII	8.5	2.2	2	4.0	·	·	1.5	2.3	10	3.1	12.5	3.6	28	3.7	16.5	3.4	14	2.9	54	12.2	26	·	·	·	4	1	·	·	11	14	9	2	1	·	3
VIII	4.5	2.2	1.5	2.3	0.5	1.0	3	2.8	9.5	3.9	31	5.7	22	4.9	11	2.5	10	4.0	108	20.4	15	·	·	·	3	7	2	·	8	16	14	4	3	·	7
IX	2	2.2	0.5	1.0	3	2.2	6.5	2.4	13	3.9	29.5	6.1	15	5.6	5.5	3.4	15	4.0	47	19.4	18	·	·	·	1	4	1	3	10	14	9	1	4	·	1
X	1.5	1.7	1	3.0	·	·	3	3.2	11	3.5	19.5	3.7	21	4.2	7	2.7	29	2.5	9	5.7	28	·	·	7	·	1	·	3	14	6	2	·	14	·	·
XI	1.5	1.3	1.5	8.7	16	7.3	20	5.1	10.5	3.4	11.5	6.0	9	3.3	7	1.9	13	4.2	49	14.5	15	·	·	13	·	6	·	1	22	17	8	2	11	2	·
XII	5.5	2.2	15.5	2.5	2.5	2.2	7.5	3.0	19.5	4.2	17	5.7	9	4.6	3.5	2.3	13	3.3	11	3.7	14	11	17	26		2	1	3	22	13	4	·	2	17	·
Rok	66.5	3.1	59.5	4.1	48.5	2.8	95.5	3.3	140.5	3.9	214	5.5	193	4.8	114.5	3.5	163	3.9	502	20.4	15.VIII	33	56	131	13	45	12	16	180	171	99	11	45	102	22

Kamień Krajeński $\varphi = 53°32'$ $\lambda = 17°32'$ 1962

MIESIĄC	CIŚNIENIE φ				TEMPERATURA T												ŚREDNIA PREŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	P_{0m}	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnio I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.0	-2.3	8.0	22	-16.8	31	-0.5	0.7	-0.5	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.5	7.6	8.4
II	–	–	–	–	0.5	-4.5	4.6	20	-16.5	1	-3.0	-0.8	-2.0	-1.9	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.4	6.6	8.0
III	–	–	–	–	1.8	-6.2	10.1	30	-14.1	15	-4.7	0.2	-2.4	-2.3	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.0	5.5	6.1
IV	–	–	–	–	13.9	3.7	26.8	23	-2.1	10	5.4	12.1	7.8	8.3	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.8	5.0	5.6
V	–	–	–	–	14.1	5.1	20.7	20	-3.1	1	8.0	12.2	8.7	9.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.5	6.6	7.0
VI	–	–	–	–	18.9	7.9	29.2	16	2.6	3	11.5	16.5	13.0	13.5	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.7	5.6	5.7
VII	–	–	–	–	20.1	9.7	27.3	21	6.2	25	14.1	18.0	14.6	15.3	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.6	5.3	5.9
VIII	–	–	–	–	19.6	10.8	27.4	4	4.7	14	13.4	17.5	14.9	15.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.3	7.4	7.2
IX	–	–	–	–	16.3	7.5	24.7	3	3.1	15	9.0	14.5	10.9	11.3	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.5	5.3	6.1
X	–	–	–	–	12.5	4.2	21.0	3	-2.5	16	5.8	11.3	7.6	8.1	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.2	5.5	6.6
XI	–	–	–	–	4.9	1.0	12.3	5	-6.8	24	2.0	3.5	2.7	2.7	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.3	8.5	8.5
XII	–	–	–	–	-2.2	-7.5	5.1	12	-20.1	22	-5.3	-3.8	-5.2	-4.9	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.8	7.1	7.8
Rok	–	–	–	–	10.2	2.4	29.2	16.VI	-20.1	22.XII	4.6	8.5	5.8	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.0	6.3	6.9

Grudziądz $\varphi = 53°30'$ $\lambda = 18°46'$

I	–	–	–	–	2.5	-1.5	8.9	22	-15.0	31	0.2	1.6	0.3	0.6	5.6	5.8	5.6	5.7	88	82	87	86	0.8	1.3	0.8	1.0	8.4	7.9	7.6	8.0
II	–	–	–	–	4.1	-4.0	4.8	12	-15.0	1	-2.4	-0.1	-1.4	-1.3	4.5	5.1	4.7	4.8	85	82	83	83	0.8	1.0	0.9	0.9	8.0	8.2	7.6	7.9
III	–	–	–	–	2.1	-4.7	10.5	31	-11.8	9	-3.6	1.0	-1.5	-1.4	4.2	5.3	4.7	4.7	86	79	84	83	0.6	1.4	0.8	0.9	6.7	6.5	5.4	6.2
IV	–	–	–	–	15.2	5.2	27.7	23	0.2	6	6.8	13.3	8.8	9.4	8.9	9.8	9.6	9.4	88	65	81	78	1.5	6.9	2.4	3.6	6.7	6.8	5.8	6.4
V	–	–	–	–	15.1	6.5	20.7	8	-2.4	1	9.0	13.4	10.2	10.7	10.3	10.4	10.8	10.5	88	70	86	81	1.4	5.3	1.9	2.9	6.8	7.7	7.4	7.3
VI	–	–	–	–	20.1	9.9	29.9	16	4.2	3	13.2	18.4	14.5	15.2	11.8	11.6	12.4	11.9	76	55	73	68	3.8	10.4	4.8	6.3	4.9	5.8	5.3	5.3
VII	–	–	–	–	21.5	11.7	28.7	21	8.1	30	14.2	19.8	15.4	16.2	14.1	14.3	14.3	14.2	86	62	81	76	2.3	9.5	3.8	5.2	5.8	6.9	5.7	6.1
VIII	–	–	–	–	21.0	12.5	28.9	12	8.4	10	14.4	19.4	15.7	16.3	14.3	14.5	15.0	14.6	87	66	84	79	2.2	8.2	3.3	4.6	6.8	7.5	7.1	7.1
IX	–	–	–	–	17.4	8.9	28.3	4	5.1	24	10.1	16.3	11.8	12.5	11.3	13.2	12.1	12.2	91	72	86	83	1.2	5.8	2.0	3.0	6.8	7.1	6.0	6.6
X	–	–	–	–	13.5	5.4	21.3	1	-0.9	29	6.6	12.3	8.6	9.0	9.4	10.5	10.3	10.1	94	73	90	86	0.6	4.2	1.2	2.0	7.1	6.3	5.8	6.4
XI	–	–	–	–	5.5	2.0	13.1	4	-1.9	18	3.0	4.6	3.5	3.6	7.2	7.5	7.2	7.3	93	87	90	90	0.6	1.2	0.9	0.9	9.6	8.7	8.1	8.8
XII	–	–	–	–	-1.7	-6.1	5.0	12	-17.8	22	-4.3	-2.8	-4.1	-3.8	4.5	4.7	4.4	4.5	94	90	92	92	0.3	0.6	0.4	0.4	6.9	6.7	7.1	6.9
Rok	–	–	–	–	11.1	3.8	29.9	16.VI	-17.8	22.XII	5.6	9.8	6.8	7.2	8.8	9.4	9.3	9.2	88	74	85	82	1.3	4.6	1.9	2.6	7.0	7.2	6.6	6.9

Osowiec $\varphi = 53°29'$ $\lambda = 22°39'$

I	–	–	–	–	-0.7	-3.3	6.2	22	-21.4	31	-1.7	0.0	-1.5	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	9.5	8.7	9.4	9.2
II	–	–	–	–	-1.7	-7.5	2.6	13	-19.3	1	-5.3	-2.7	-4.1	-4.0		–	–	–	–	–	–	–	–	–	–	–	8.6	7.4	8.8	8.3
III	–	–	–	–	-0.2	-7.4	6.0	31	-17.1	2	-5.7	-0.9	-3.7	-3.5	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.5	7.5	7.0
IV	–	–	–	–	14.6	5.2	26.4	23	-1.6	8	7.1	13.1	9.2	9.6	–	–	–	–	–	–	–	–	–	–	–	–	8.1	6.6	8.5	7.7
V	–	–	–	–	14.8	5.9	20.5	27	-1.5	1	9.0	13.5	10.1	10.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	18.8	8.4	27.7	24	3.1	3	12.9	17.5	12.7	14.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.0	7.3	7.0
VII	–	–	–	–	20.6	9.5	27.2	26	4.8	31	14.1	19.5	14.6	15.7	–	–	–	–		–	–	–	–	–	–	–	7.1	6.0	7.9	7.0
VIII	–	–	–	–	20.9	10.0	30.0	7	4.6	15	14.2	19.4	15.5	16.2	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.0	7.5	6.9
IX	–	–	–	–	16.3	6.0	26.1	5	-0.4	25	8.9	15.1	10.1	11.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	12.1	3.1	18.7	2,3	-3.6	28	5.5	11.5	6.9	7.7	–	–	–	–	–	–	–	–	–	–	–	–	8.6	6.4	7.9	7.6
XI	–	–	–	–	6.3	1.1	15.6	1	-4.1	26	2.6	5.2	3.2	3.6	–	–	–		–	–	–	–	–	–	–	–	8.8	8.5	9.0	8.8
XII	–	–	–	–	-2.9	-7.7	3.7	5	-20.3	22	-5.6	-3.9	-5.8	-5.3	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.4	8.7	8.1
Rok	–	–	–	–	9.9	1.9	30.0	7.VIII	-21.4	31.I	4.7	8.9	5.6	6.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Szczecin-Niebuszewo $\varphi = 53°28'$ $\lambda = 14°33'$

I	–	–	–	–	3.5	-0.5	8.2	21	-13.7	31	1.2	2.4	1.5	1.6	5.9	6.1	6.1	6.0	87	83	87	86	0.9	1.3	0.9	1.0	7.4	8.5	7.6	7.8
II	–	–	–	–	2.6	-2.3	7.6	8	-11.6	1	-0.5	1.8	0.0	0.3	5.2	5.4	5.0	5.2	86	75	79	80	0.8	1.7	1.3	1.3	8.1	7.8	6.7	7.5
III	–	–	–	–	3.3	-3.2	12.8	30	-8.5	14	-1.6	2.5	-0.1	0.2	4.9	4.7	4.8	4.8	86	63	78	76	0.7	2.8	1.4	1.6	7.0	6.5	6.5	6.7
IV	–	–	–	–	13.8	4.2	27.5	25	0.5	30	6.0	12.1	7.8	8.4	8.2	8.6	8.5	8.4	86	60	80	75	1.3	6.5	2.5	3.4	8.1	7.0	5.7	6.9
V	–	–	–	–	13.9	6.3	20.2	19	-0.2	1	9.2	12.4	9.1	10.0	10.0	9.1	9.9	9.7	85	64	85	78	1.8	5.6	1.9	3.1	6.7	8.1	6.4	7.1
VI	–	–	–	–	18.8	9.0	28.8	15	2.8	4	12.9	17.1	12.9	14.0	11.8	11.3	11.3	11.5	78	57	74	70	3.4	9.1	4.0	5.5	5.1	6.4	5.7	5.7
VII	–	–	–	–	19.4	11.0	25.4	21	6.6	5	13.8	18.1	13.9	14.9	13.9	13.7	13.9	13.8	88	66	87	80	2.0	7.5	2.1	3.9	6.6	7.2	6.1	6.6
VIII	–	–	–	–	19.1	11.5	28.2	12	8.4	9	13.8	18.0	14.3	15.1	13.8	14.2	14.2	14.1	87	69	87	81	2.1	6.8	2.2	3.7	8.0	8.0	5.8	7.3
IX	–	–	–	–	16.4	8.2	24.4	4	5.4	15,20	10.1	15.6	10.9	11.9	11.6	12.1	11.6	11.8	93	69	88	83	1.0	6.0	1.7	2.9	6.9	6.7	4.2	5.9
X	–	–	–	–	12.6	5.8	22.6	3	0.8	30	7.2	11.7	8.7	9.1	9.8	10.9	10.4	10.4	95	78	90	88	0.5	3.2	1.2	1.6	7.9	7.3	5.1	6.8
XI	–	–	–	–	5.2	1.5	13.3	8	-6.9	24	2.6	4.5	3.0	3.3	7.0	7.4	7.2	7.2	93	86	93	91	0.5	1.4	0.6	0.8	8.5	9.0	7.5	8.3
XII	–	–	–	–	-1.0	-5.4	5.3	12	-16.2	22	-3.5	-2.1	-3.3	-3.0	4.5	4.8	4.6	4.6	91	86	90	89	0.5	0.7	0.5	0.6	8.4	8.0	6.4	7.6
Rok	–	–	–	–	10.6	3.8	28.8	15.VI	-16.2	22.XII	5.9	9.5	6.6	7.2	8.9	9.0	9.0	9.0	88	71	85	81	1.3	4.4	1.7	2.5	7.4	7.5	6.1	7.0

Kamień Krajeński $H_s = 124\ m$ $h_w = 12\ m$ **1962**

Miesiąc	Rozkład wiatru °D, v — N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R — Suma	Max	Data	Liczba dni (n) — Temperatura T: Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v: v > 10	v > 15	◔	●	Opad R: R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	[illegible]
I	3	7.7	6	2.3	3	4.0	1	2.0	18	2.5	24	3.7	26	3.0	7	2.9	5	2.9	38	6.5	12	2	4	23	·	2	·	2	21	19	14	·	–	–	·
II	9	6.1	14	4.6	5	4.0	1	1.0	11	2.8	14	4.6	16	2.9	11	6.3	3	4.2	27	7.0	12	2	11	26	·	5	1	·	18	18	6	·	–	–	·
III	18	3.3	14	2.0	4	2.8	11	2.2	10	1.6	4	4.0	5	2.0	7	1.6	20	1.8	35	16.3	12	5	9	28	·	1	·	3	12	13	7	1	–	–	·
IV	6	3.1	17	2.8	3	1.7	4	2.8	4	2.5	16	3.1	6	2.5	12	2.2	22	2.0	26	5.3	2	·	·	5	2		·	2	9	14	10	·	–	·	·
V	9	1.9	4	1.2	4	1.2	4	2.0	10	2.0	10	2.0	18	1.5	16	3.2	18	1.7	70	19.4	14	·	·	5	·		·	·	11	20	13	2	–	·	6
VI	19	3.4	4	2.5	·	·	3	1.7	3	2.0	9	2.7	21	2.6	20	2.2	11	2.3	85	31.0	16	·	·		3	·	·	4	5	15	10	2	–	·	2
VII	11	1.6	10	1.0	3	1.0	·	·	6	2.0	13	4.3	20	2.1	10	1.4	20	1.2	51	16.2	26	·	·		2	·	·	1	6	12	9	2	–	·	3
VIII	6	1.2	2	1.0	3	1.3	·	·	5	1.8	11	3.5	35	2.6	11	1.9	20	1.8	98	43.2	7	·	·	·	2	·	·	2	15	18	14	1	–	·	4
IX	2	1.0	4	1.0	7	2.0	3	2.3	7	2.3	12	3.4	25	2.6	8	2.6	22	1.9	55	12.4	18	·		·	·	1	·	5	6	15	9	2	–	·	2
X	8	1.0	2	1.0	5	1.2	2	1.5	6	1.2	9	1.4	24	1.7	12	2.9	25	1.2	14	4.3	5,31	·	·	4	·	·	·	3	13	7	4	·	–	·	·
XI	5	2.6	9	3.9	21	3.0	9	2.7	10	1.4	10	1.1	17	1.6	1	2.0	8	2.1	46	25.0	1	·	·	13	·	·	·	1	21	13	8	1	–	–	·
XII	7	2.0	19	1.5	6	1.3	1	1.0	8	3.2	14	2.4	18	2.1	3	1.3	17	1.6	26	5.5	11,13	10	17	28	·	·		3	19	12	9	·	–	–	·
Rok	103	2.9	105	2.1	64	1.7	39	1.6	98	2.1	146	2.5	231	2.3	118	2.5	191	2.1	571	43.2	7VIII	19	41	132	9	9	1	26	156	176	113	11	–	–	17

Grudziądz $H_s = 40\ m$ $h_w = 12.5\ m$

I	1	3.5	2.5	2.6	6.5	2.3	16.5	4.9	22.5	3.6	35	5.1	5.5	5.9	3.5	1.7	·	4.4	17	4.8	25	3	3	17	·	2	·	2	18	9	8	·	–	8	⁚
II	4	4.5	2.5	4.6	17.5	4.3	14.5	4.2	11.5	3.6	19	7.4	6	8.0	8	6.5	1	5.3	30	8.4	16	2	9	23	·	5	2	·	14	11	11	·	–	14	·
III	7	2.5	13.5	2.9	13.5	2.7	23.5	2.9	9	2.2	9	3.3	3.5	3.3	6	4.3	8	2.7	37	16.0	6	2	6	28	·	·	·	4	12	7	7	1	–	16	·
IV	4.5	3.8	3.5	3.4	11.5	2.9	15	3.0	11	2.3	23.5	3.6	7.5	1.8	8.5	2.9	5	2.9	16	5.3	13	·	·	·	2	·	·	2	8	7	7	·	–	·	·
V	2.5	5.6	5	1.6	5	2.2	8.5	2.4	22	2.2	22.5	3.2	3	5.3	5.5	3.3	19	2.2	111	25.3	15	·	·	2	·	·	·	1	14	17	17	2	–	·	5
VI	3.5	4.3	3.5	4.9	2.5	1.6	2.5	1.0	16.5	1.9	30	2.6	17	2.5	9.5	3.1	5	2.4	62	14.7	29	·	·	·	4	·	·	4	6	9	8	3	–	·	4
VII	3	1.3	2.5	1.8	14.5	1.8	6.5	1.5	19	2.0	21	3.2	15.5	2.5	3	1.0	8	2.1	60	21.2	26	·	·	·	4	2	1	1	7	14	13	1	–	·	2
VIII	1.5	1.0	3.5	1.0	5	1.4	7	1.4	14	2.0	34	3.3	19.5	3.4	1.5	6.0	7	2.5	57	9.8	25	·	·	·	4	·	·	2	12	16	13	·	–	·	4
IX	·	·	2	1.5	7.5	1.6	15.5	1.7	20	3.1	26	3.5	7	5.0	·	·	12	2.5	62	24.2	18	·	·	·	1	1	·	2	13	10	10	2	–	·	1
X	1.5	3.0	2.5	1.8	5	1.7	15.5	2.0	18.5	2.5	20.5	3.2	3.5	2.9	4	2.6	22	2.0	16	8.5	6	·	·	3	·	·	·	3	11	3	3	·	–	·	·
XI	·	·	3.5	5.4	20	4.0	13.5	2.3	17	1.8	16.5	2.7	8.5	3.0	·	·	11	2.5	29	6.7	20	·	·	8	·	·	·	1	22	8	8	·	–	·	·
XII	2	2.5	1.5	1.0	15.5	2.2	20	2.8	17	2.4	22.5	3.2	4.5	2.8	2	2.5	8	2.5	20	3.8	11	9	16	24	·	·	·	4	16	9	7	·	–	13	·
Rok	30.5	2.7	46	2.7	124	2.4	158.5	2.5	198	2.5	279.5	3.7	101	3.9	51.5	2.8	106	2.8	527	25.3	15.V	16	34	105	15	10	3	26	153	120	112	9	–	51	16

Osowiec $H_s = 110\ m$ $h_w = 11\ m$ I–IV, $15\ m$ V–XII

I	·	·	10	3.2	0.5	1.0	7	2.4	28.5	3.5	32	3.9	14	2.9	·	·	1	3.4	18	4.5	6	3	10	22	·	1	·	·	25	15	6	·	1	19	–
II	9	5.4	9	6.4	5	4.2	9.5	2.6	19	4.5	11.5	8.2	7	4.7	10	7.6	4	5.2	51	9.6	12	7	16	28	·	9	3	·	16	22	12	·	3	28	–
III	13.5	4.8	15	3.2	6	1.2	18	2.8	13	2.2	5	6.8	2	3.5	7.5	4.5	13	3.0	41	8.9	31	9	15	29	·	1	·	2	14	17	11	·	1	31	–
IV	3.5	3.7	6.5	3.7	7.5	2.6	21	2.5	11	3.6	4.5	2.4	12	2.8	2	9.0	22	2.3	46	18.4	13	·	·	2	4	·	·	1	17	12	8	1	1	·	–
V	5	3.0	5	1.6	7.5	3.1	5.5	2.0	12.5	1.4	12.5	2.5	18	1.8	10	5.5	17	2.1	94	14.8	20	·	·	3	·	1	·	–	–	20	17	2	2	·	–
VI	12	3.5	11	6.2	4.5	2.1	5.5	1.6	7	2.9	11	2.4	13.5	3.1	16.5	3.2	9	3.0	53	18.0	4	·	·	·	2	1	1	·	9	10	7	1	·	·	–
VII	9	2.2	3	2.5	4.5	2.0	3.5	1.4	11	2.7	13.5	2.1	8	2.2	23.5	2.7	17	2.0	69	14.2	26	·	·	·	3	·	·	·	10	16	13	1	·	·	–
VIII	8	2.2	6.5	2.2	2.5	1.2	7	3.3	12.5	3.1	15.5	5.5	21	4.7	7	4.9	13	3.2	76	12.2	15	·	·	·	4	4	·	·	8	14	12	4	2	·	–
IX	6	3.0	·	·	10	1.6	4	1.8	15	4.0	13.5	3.9	26.5	3.6	7	4.7	8	3.1	75	21.3	18	·	·	1	1	·	·	–	–	17	14	2	2	·	–
X	1	1.0	·	·	2	1.0	0.5	2.0	7.5	2.2	8	2.3	17	2.1	11	3.3	46	1.2	3	4.3	18	·	·	7	·	·	·	·	15	6	1	·	6	·	–
XI	9	1.7	·	·	10	4.0	23	2.3	5	3.0	5	3.2	11	2.5	3	1.0	24	1.9	45	12.8	15	·	·	13	·	·	·	·	23	16	10	2	5	3	–
XII	6.5	1.3	9.5	1.5	2	1.5	8.5	1.9	6	1.7	24	3.5	9.5	3.6	1	1.0	26	1.9	16	4.9	14	11	17	27	·	1	·	1	20	13	5	·	·	18	–
Rok	82.5	2.6	75.5	2.5	62	2.1	113	2.2	148	2.9	156	3.9	159.5	3.1	98.5	3.7	200	2.7	587	21.3	18.IX	30	58	132	14	18	4	–	–	178	116	13	23	99	–

Szczecin-Niebuszewo $H_s = 69\ m$ $h_w = 10\ m$

I	5.5	4.9	3.5	2.3	2	2.5	0.5	2.0	19	5.5	39.5	4.9	15	5.3	6	3.3	2	4.7	33	5.8	6	2	4	12	·	3	·	1	17	19	10	·	2	3	·
II	13	6.8	10.5	4.9	7	5.1	4.5	2.7	5	2.7	20	4.5	18	5.9	8	6.3	1	5.2	37	11.5	12	1	7	22	·	5	1	1	17	14	8	1	1	8	1
III	12.5	4.4	12	3.5	5.5	2.7	13.5	4.6	14	3.5	7.5	3.7	6	3.8	9	2.6	13	3.2	27	8.9	5	·	6	27	·	1	·	4	17	13	6	·	2	12	·
IV	16	3.3	8.5	3.6	14.5	3.5	3.5	3.4	4	4.6	21.5	4.8	9.5	3.1	8.5	4.5	4	3.7	31	10.7	16	·	·	·	2	1	1	2	12	15	7	1	4	·	1
V	12	3.1	6	2.7	2	2.0	6	3.7	8.5	3.9	25	3.7	13.5	3.0	6	3.6	14	2.9	76	13.8	10	·	·	1	·	·	·	·	12	20	13	1	2	·	3
VI	16.5	3.7	3.5	2.3	1.5	2.0	1.5	3.3	2.5	4.6	14.5	3.7	25.5	3.4	13.5	3.7	11	3.1	66	15.6	19	·	·	·	2	·	·	2	7	13	11	2	·	·	6
VII	6.5	2.1	8.5	2.4	5	1.8	3.5	2.3	2	2.5	28	3.5	12.5	3.4	6	2.8	21	2.3	93	16.3	7	·	·	·	1	·	·	1	8	17	13	3	1	·	7
VIII	8.5	2.2	5	2.1	3	3.0	3.5	2.6	8	3.4	40	3.7	13.5	3.6	10.5	3.0	1	3.3	76	10.5	7	·	·	·	1	1	·	1	12	19	14	1	·	·	3
IX	2.5	2.0	1	2.0	10.5	2.5	6.5	5.4	5.5	4.5	21.5	4.3	23.5	3.5	8	2.7	11	3.2	61	19.9	4	·	·	·	·	·	·	2	5	12	12	1	6	·	5
X	3.5	3.1	1.5	2.3	7	2.2	7.5	3.1	10	2.7	15	3.0	14	2.8	9.5	3.2	25	2.1	10	4.4	26	·	·	·	·	·	·	2	13	5	3	·	14	·	1
XI	1.5	3.3	6.5	4.5	20.5	4.7	10	4.6	8.5	2.6	10	3.6	12.5	2.8	2.5	3.2	18	3.1	29	7.3	30	·	3	10	·	1	·	1	20	14	8	·	8	7	·
XII	·	·	6	2.3	10.5	3.5	3	5.3	10	4.0	24	4.0	9.5	3.1	10	2.5	20	2.8	30	6.2	11	8	18	26	·	·	·	3	18	13	7	·	7	5	·
Rok	98	3.2	72.5	2.9	89	3.0	60.5	3.6	97	3.7	266.5	4.0	173	3.6	97.5	3.4	141	3.3	569	19.9	4.IX	11	38	98	6	12	2	20	158	174	112	10	47	35	27

Szczecin-Dąbie $\varphi = 53°24'$ $\lambda = 14°37'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	P_{0m}	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1011.9	1040.8	982.5	1012.8	4.1	-0.4	8.8	22	-15.4	31	1.6	2.9	1.9	2.1	6.1	6.2	6.1	6.1	87	81	86	85	1.0	1.5	1.1	1.2	7.4	8.5	7.5	7.8
II	1014.6	1039.0	979.0	1015.5	3.2	-1.9	8.1	8	-14.3	1	-0.1	2.3	0.6	0.8	5.4	5.6	5.2	5.4	86	75	80	80	0.9	1.8	1.3	1.3	8.1	7.9	6.7	7.6
III	1010.0	1027.4	980.5	1010.9	3.9	-3.6	13.7	30	-10.1	16	-1.9	3.0	0.0	0.3	4.9	4.8	4.9	4.9	88	6.4	7.9	7.7	0.6	2.9	1.4	1.6	6.7	6.5	6.7	6.6
IV	1012.0	1027.2	985.1	1012.8	14.5	4.3	27.9	25	0.0	6	6.1	12.6	8.3	8.8	8.4	8.8	8.8	8.7	88	5.9	7.9	7.5	1.2	6.6	2.5	3.4	7.6	6.9	6.1	6.9
V	1011.1	1016.5	1004.9	1011.9	14.8	6.5	21.0	19	-1.7	6	9.1	13.1	9.7	10.4	10.1	9.4	10.1	9.9	8.6	6.2	8.3	7.7	1.7	6.0	2.1	3.3	7.0	8.5	7.2	7.6
VI	1017.3	1032.4	1004.8	1018.1	19.7	9.0	29.4	15,19	2.1	8	13.0	18.0	13.8	14.5	12.0	11.8	12.3	12.0	7.8	5.7	7.6	7.0	3.3	9.6	3.8	5.6	5.3	6.6	5.8	5.9
VII	1012.6	1023.4	991.0	1013.4	20.2	11.0	26.1	21	6.4	10	13.8	18.7	14.5	15.4	13.9	13.6	14.7	14.1	8.7	6.3	8.8	7.9	2.0	8.3	2.0	4.1	6.8	7.5	6.3	6.9
VIII	1012.8	1022.0	1000.8	1013.6	20.0	11.9	28.4	12	8.2	14	13.9	18.5	14.9	15.6	14.0	14.6	14.8	14.5	8.7	6.9	8.7	8.1	2.1	7.0	2.3	3.8	8.0	7.9	6.3	7.4
IX	1013.7	1027.6	991.8	1014.5	17.1	7.9	25.5	4	2.0	25	9.7	15.9	11.2	12.0	11.4	12.3	11.9	11.9	9.3	6.8	8.9	8.3	0.9	6.2	1.5	2.9	6.6	6.9	3.9	5.8
X	1020.2	1034.9	1006.0	1021.0	13.2	4.8	23.0	3	-1.7	24	6.7	12.0	8.4	8.9	9.4	11.1	10.0	10.2	9.4	7.8	8.9	8.7	0.6	3.4	1.4	1.8	7.5	7.5	5.1	6.7
XI	1014.7	1032.7	996.1	1015.6	5.6	1.5	14.2	8	-4.2	21	2.8	4.9	3.1	3.5	7.0	7.4	7.1	7.2	9.2	8.5	9.1	8.9	0.6	1.5	0.8	1.0	8.0	9.1	7.0	8.0
XII	1014.8	1047.7	967.5	1015.7	-0.7	-5.5	6.5	12	-17.3	24	-3.5	-1.6	-3.1	-2.8	4.5	4.9	4.6	4.7	9.0	8.4	8.9	8.8	0.5	0.8	0.6	0.6	7.5	8.0	6.3	7.3
Rok	1013.8	1047.7	967.5	1014.6	11.3	3.8	29.4	15,19 VI	-17.3	24 XII	5.9	10.0	6.9	7.4	8.9	9.2	9.2	9.1	8.8	7.0	8.5	8.1	1.3	4.6	1.7	2.5	7.2	7.6	6.2	7.0

Jabłonowo Pom $\varphi = 53°24'$ $\lambda = 19°10'$

I	-	-	-	-	1.8	-2.3	8.2	22	-16.5	31	-0.5	0.6	-0.6	-0.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	0.3	-4.4	3.2	13,16	-14.3	1	-3.0	-0.9	-2.1	-2.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	1.0	-5.4	9.8	31	-13.6	15	-4.1	-0.1	-2.4	-2.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	14.5	-	26.2	21	-	-	6.7	12.8	8.5	9.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	14.5	6.0	19.4	8	-2.6	1	8.4	12.6	9.7	10.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	-	-	-	19.5	8.6	28.6	16	3.7	3	12.4	17.3	13.5	14.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	-	-	-	20.6	10.3	27.7	21,26	6.6	30,31	13.2	18.9	14.3	15.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	-	-	-	19.9	11.4	26.2	12	7.4	10	13.3	18.4	14.5	15.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	-	-	-	16.6	7.9	26.7	4	3.2	27	9.4	15.2	11.0	11.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	-	-	-	12.6	4.6	20.4	1,2	-1.8	28	5.9	11.7	7.8	8.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	5.1	1.3	12.3	4	-3.1	17	2.3	4.1	3.1	3.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-	-	-	-2.4	-7.5	4.9	12	-19.6	21	-5.3	-3.9	-4.9	-4.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Rok	-	-	-	-	10.3	-	28.6	16 VI	-19.6	21 XII	4.9	8.9	6.0	6.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Wierzchowo $\varphi = 53°27'$ $\lambda = 16°06'$

I	-	-	-	-	2.3	-1.6	7.5	21,22	-16.3	31	0.1	1.5	0.1	0.4	5.8	6.0	5.7	5.8	9.0	8.6	9.0	8.9	0.6	1.0	0.7	0.8	8.3	7.7	7.1	7.7
II	-	-	-	-	0.9	-3.9	5.0	12,20	-13.4	1	-1.8	0.2	-1.2	-1.0	4.8	5.1	4.9	4.9	8.6	8.0	8.5	8.4	0.7	1.2	0.8	0.9	8.7	7.9	6.5	7.7
III	-	-	-	-	2.0	-6.2	10.7	30	-13.6	14	-3.4	1.5	-1.9	-1.4	4.3	4.7	4.7	4.6	8.7	6.9	8.6	8.1	0.6	2.2	0.8	1.2	6.3	5.9	5.9	6.0
IV	-	-	-	-	13.2	3.4	25.7	25	-1.2	6	6.1	12.1	7.4	8.2	8.5	9.1	8.8	8.8	8.7	6.4	8.3	7.8	1.4	6.0	1.9	3.1	6.8	6.0	5.1	6.0
V	-	-	-	-	13.4	5.0	19.5	19	-2.8	5	8.5	12.1	8.3	9.3	10.0	9.9	10.0	10.0	8.9	7.0	9.0	8.3	1.2	4.5	1.2	2.3	7.3	6.9	6.2	6.8
VI	-	-	-	-	18.2	7.7	28.6	15	1.0	3	12.6	16.9	11.8	13.3	11.5	11.9	11.5	11.6	7.7	6.1	8.0	7.3	3.8	8.2	2.8	4.9	5.2	5.6	4.6	5.1
VII	-	-	-	-	19.6	9.3	26.1	26	4.9	30	13.4	18.3	13.5	14.7	13.7	13.7	13.9	13.8	8.9	6.6	8.9	8.1	1.8	7.8	1.8	3.8	5.8	5.6	5.4	5.6
VIII	-	-	-	-	19.0	10.4	27.4	12	5.5	10	13.4	18.0	13.7	14.7	13.9	14.4	14.1	14.1	9.0	7.0	8.9	8.3	1.6	6.6	1.7	3.3	6.8	6.6	5.6	6.3
IX	-	-	-	-	16.0	6.9	25.4	4	0.5	18	9.9	14.9	10.1	11.2	11.4	12.1	11.3	11.6	9.3	7.2	9.0	8.5	0.9	5.3	1.2	2.5	6.8	5.3	5.0	5.7
X	-	-	-	-	12.0	3.9	21.0	2	-2.3	16	6.2	11.4	7.6	8.2	9.2	10.8	9.8	9.9	9.4	7.9	9.1	8.8	0.6	3.2	1.0	1.6	7.3	6.2	5.7	6.4
XI	-	-	-	-	4.7	1.3	12.6	5	-2.6	24,25	2.3	4.2	2.9	3.1	6.8	7.3	6.8	7.0	9.3	8.7	8.9	9.0	0.5	1.2	0.9	0.9	8.8	8.2	8.4	8.5
XII	-	-	-	-	-2.0	-7.8	-4.5	12,13	-19.8	22	-5.4	-2.9	-4.9	-4.5	4.1	4.5	4.1	4.2	8.9	8.6	8.8	8.8	0.4	0.6	0.4	0.5	8.2	7.5	6.5	7.4
Rok	-	-	-	-	9.9	2.4	28.6	15 VI	-19.8	22 XII	5.2	9.0	5.6	6.4	8.7	9.1	8.8	8.9	8.9	7.4	8.8	8.4	1.2	4.0	1.3	2.2	7.2	6.6	6.0	6.6

Jastrowie $\varphi = 53°25'$ $\lambda = 16°48'$

I	-	-	-	-	-	-1.8	-	-	-15.0	31	-0.1	0.9	0.0	0.2	-	-	-	-	-	-	-	-	-	-	-	-	8.2	7.5	8.4	8.0
II	-	-	-	-	1.1	-4.7	5.0	12	-14.8	1	-2.2	-0.1	-2.0	-1.6	-	-	-	-	-	-	-	-	-	-	-	-	7.6	6.8	7.1	7.2
III	-	-	-	-	2.4	-5.9	11.6	30	-14.3	14	-2.3	1.4	-2.3	-1.4	-	-	-	-	-	-	-	-	-	-	-	-	7.0	5.3	5.9	6.1
IV	-	-	-	-	14.5	3.8	26.1	25	-2.0	1	6.9	13.7	7.7	9.0	-	-	-	-	-	-	-	-	-	-	-	-	6.9	5.6	6.4	6.2
V	-	-	-	-	14.1	4.9	20.4	19	-2.0	5	9.2	13.4	8.4	9.8	-	-	-	-	-	-	-	-	-	-	-	-	7.5	7.5	8.0	7.7
VI	-	-	-	-	19.5	7.9	29.1	15	0.4	3	12.5	18.3	12.9	14.2	-	-	-	-	-	-	-	-	-	-	-	-	6.1	6.1	6.9	6.4
VII	-	-	-	-	20.4	9.4	27.2	26	5.9	25,29	14.6	19.5	13.7	15.4	-	-	-	-	-	-	-	-	-	-	-	-	6.8	6.8	6.8	6.8
VIII	-	-	-	-	20.1	10.1	29.0	12	6.9	10	14.1	19.6	13.9	15.4	-	-	-	-	-	-	-	-	-	-	-	-	6.7	6.9	6.8	6.8
IX	-	-	-	-	16.6	6.7	28.0	4	1.4	18	10.1	16.1	10.4	11.8	-	-	-	-	-	-	-	-	-	-	-	-	7.2	6.9	6.9	7.0
X	-	-	-	-	13.0	4.1	21.8	3	-3.0	16	6.8	12.7	7.9	8.8	-	-	-	-	-	-	-	-	-	-	-	-	7.7	6.6	6.9	7.1
XI	-	-	-	-	5.1	1.1	13.0	5	-2.5	18	2.3	4.6	2.8	3.1	-	-	-	-	-	-	-	-	-	-	-	-	7.7	7.5	7.6	7.6
XII	-	-	-	-	-2.8	-7.7	5.0	12	-19.7	22	-5.6	-4.0	-5.3	-5.0	-	-	-	-	-	-	-	-	-	-	-	-	6.7	6.5	6.6	6.6
Rok	-	-	-	-	-	2.3	29.1	15 VI	-19.7	22 XII	5.5	9.7	5.7	6.6	-	-	-	-	-	-	-	-	-	-	-	-	7.2	6.7	7.0	7.0

Szczecin-Dąbie $H_s = 1 m$ $H_b = 6,9$ $h_w = 20 m$ 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	≡	⊞	R ∞
I	5	5.8	2.5	2.6	1.5	1.7	·	·	3	6.7	49	5.8	21.5	4.7	5.5	4.9	5	5.0	28	4.7	6	2	4	10	·	4	·	1	19	19	10	·	1	3	
II	10.5	6.4	9.5	5.4	9.5	5.5	1	3.5	0.5	2.0	20.5	5.5	19.5	5.8	11	6.8	2	5.7	41	12.7	12	1	6	20	·	5	·	1	15	13	9	1	1	8	1
III	9.5	4.0	10.5	2.9	2.5	4.2	12	4.8	8.5	5.2	15.5	3.6	10.5	2.5	7	3.1	17	3.1	31	10.0	12	1	3	26	·	1	·	4	14	12	7	1	3	12	
IV	13	4.0	11	4.3	9	3.6	10	3.4	4.5	3.7	23	4.8	10	5.0	6.5	3.2	6	3.9	29	12.6	16	·		·	3	1	·	2	14	15	8	1	4		·
V	7	3.9	5.5	2.6	2	1.0	3	2.7	5	5.4	22	3.8	25	3.4	9.5	3.7	14	3.0	73	10.2	7	·	·	2	·	·	·	·	15	22	16	1	4	·	5
VI	12.5	3.6	7	3.6	1	2.0	1.5	4.0	2.5	3.6	9	6.0	29	3.8	13.5	4.1	14	3.3	46	10.7	15	·	·	·	5	·	·	3	6	13	8	1	3	·	6
VII	1.5	4.7	9	2.1	4.5	2.2	6.5	3.0	1.5	3.7	15	4.1	27.5	3.9	7.5	2.9	20	2.6	91	15.4	14	·	·	·	1	·	·	·	6	19	15	1	7	·	7
VIII	5	2.7	3	2.0	2.5	2.2	4	3.0	6	3.9	33	4.3	24.5	4.6	8	3.7	7	3.7	72	12.4	7	·	·	·	1	·	·	1	12	17	12	2	1	·	3
IX	1	2.5	0.5	1.0	1	2.5	14	5.6	·	·	18.5	5.1	26	4.2	9	3.6	20	3.6	58	22.2	4	·	·	·	1	2	·	2	4	16	12	1	10	·	4
X	2.5	2.6	2.5	3.6	·	·	14	3.2	4.5	4.2	15	3.8	22.5	3.6	7	3.6	25	2.6	9	4.0	26	·	·	3	·	·	·	·	10	7	3	·	19	·	1
XI	1	5.0	1	6.0	16	4.2	19	6.3	4	2.9	12	4.0	17	3.5	1	6.0	19	3.6	21	5.2	19	·	2	10	·	1	·	1	16	11	7	·	9	4	·
XII	2	4.0	1	1.0	11.5	4.0	3	4.0	3	4.0	16	4.0	22	4.3	7.5	4.1	27	2.9	33	7.4	11	6	16	26	·	·	·	3	16	12	7	·	7	4	
Rok	70.5	3.8	63	3.1	61	2.8	88	3.6	40	3.8	248.5	4.5	255	4.1	93	4.1	176	3.6	532	22.2	4.IX	10	31	97	11	14	·	18	147	176	114	9	69	31	26

UWAGA. Kierunki i prędkości wiatru - wg anemometru.

Jabłonowo Pom. $H_s = 97 m$ $h_w = 13 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	≡	⊞	R ∞
I	2	1.0	9	2.8	·	·	1	5.0	14	3.4	40	4.3	17	3.6	10	2.6	·	3.6	20	5.2	12,25	3	4	18	·	·	·	–	–	15	5	·	–	10	–
II	9	4.6	11	3.0	8	3.8	3	5.0	10	2.8	38	5.6	·		5	4.6	·	4.6	26	5.3	16	1	11	23	·	5	·	–	–	15	9	·	–	11	–
III	10	2.2	27	3.4	·	·	30	3.6	11	1.6	4	2.5	1	4.0	8	3.9	2	3.0	41	16.0	5	4	10	29	·	4	1	–	–	10	6	1	–	15	–
IV	10	4.4	21	3.2	2	8.5	7	6.0	21	3.3	10	4.7	3	4.0	12	3.2	4	3.6	25	5.6	5	·	·	–	1	5	·	–	–	14	10	·	–	·	–
V	7	2.1	11	4.8	4	1.5	10	5.0	12	4.2	10	5.3	16	2.6	11	5.1	12	3.5	129	42.0	14	·	·	3	·	5	·	–	–	24	15	2	–	·	–
VI	6	5.7	11	4.8	·	·	8	1.5	5	2.2	15	2.6	19	4.4	12	2.5	14	2.9	70	28.2	29	·	·	·	3	4	·	–	–	14	9	1	–	·	–
VII	9	2.0	6	1.7	1	1.0	3	1.0	11	2.6	9	1.9	12	3.6	11	1.1	31	1.4	84	27.4	12	·	·	·	4	·	·	–	–	15	13	2	–	·	–
VIII	3	2.0	·	·	3	2.3	2	5.0	17	2.7	11	3.4	22	3.9	5	1.8	30	2.2	94	12.2	5	·	·	·	2	·	·	–	–	16	15	2	–	·	–
IX	10	2.2	3	1.7	·	·	·	·	19	2.2	2	6.0	29	3.3	9	3.0	18	2.2	68	32.0	18	·	·	·	1	·	·	–	–	12	10	1	–	·	–
X	12	1.2	7	1.6	·	·	·	·	21	1.4	2	1.0	13	3.6	·	·	38	1.1	23	9.2	5	·	·	4	·	·	·	–	–	8	6	·	–	·	–
XI	3	2.3	2	1.0	15	3.9	4	2.0	27	3.0	·	·	17	1.6	·	·	22	2.0	43	11.2	20	·	2	11	·	·	·	–	–	16	9	1	–	1	–
XII	7	1.0	5	2.6	4	1.0	2	1.0	17	2.2	·	·	20	2.6	·	·	38	1.2	32	5.2	14	9	16	29	·	·	·	–	–	13	11	·	–	18	–
Rok	88	2.6	113	2.6	37	1.8	70	2.9	185	2.6	141	3.1	169	2.6	83	2.3	209	2.6	655	42.0	14.V	17	43	–	11	23	1	–	–	172	118	10	–	55	–

Wierzchowo $H_s = 140 m$ $h_w = 13 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	≡	⊞	R ∞
I	10	4.0	1	2.0	2	2.0	1	1.5	16	4.1	26.5	4.8	21	4.8	12.5	3.1	3	4.1	43	8.6	25	2	5	13	·	3	·	2	17	12	10	·	4	–	–
II	11.5	7.3	6	4.8	11	3.9	6.5	3.7	8	2.9	11.5	7.2	14.5	6.0	14	5.8	1	5.4	34	12.3	12	2	12	24	·	4	2	1	16	14	6	1	2	9	–
III	14	3.5	4.5	2.9	11	3.4	14	3.8	14.5	3.1	5.5	2.7	7	2.4	8.5	2.6	14	2.7	19	7.4	12	6	6	28	·	·	·	6	9	8	6	·	4	12	–
IV	12	3.6	6.5	3.8	9	4.2	10	2.9	8.5	3.1	14.5	3.5	14	3.6	9.5	4.3	6	3.4	55	14.1	16	·	·	7	1	·	·	4	7	9	9	2	1	1	–
V	7.5	3.3	6	2.5	2	2.5	9	1.8	8.5	3.8	12	2.5	24	2.4	19	3.3	5	2.6	75	9.7	14	·	·	5	·		·	·	8	19	17	·	·	·	–
VI	22	3.1	8	4.1	3	2.0	5.5	2.0	3	2.7	10	2.4	18.5	3.5	16	3.0	4	2.9	71	25.0	19	·	·	·	3	·	·	4	3	12	10	3	·	·	–
VII	13.5	1.9	6	1.5	5	1.4	6.5	1.5	3.5	2.4	15	2.8	27	2.5	11.5	2.4	5	2.1	64	14.7	3	·	·	·	2	·	·	1	2	14	12	2	1	·	–
VIII	12	1.8	1.5	2.7	1	2.5	3	1.7	11	2.6	20	3.4	26	3.3	13.5	3.0	5	2.7	65	14.5	24	·	·	·	1	·	·	1	5	12	12	1	·	·	–
IX	4.5	2.6	1.5	1.3	5	1.4	11.5	3.3	6.5	2.6	16.5	3.1	22	3.1	16.5	3.1	6	2.7	52	13.0	19	·	·	·	1	·	·	4	4	14	11	2	3	·	–
X	9.5	1.9	6.5	1.3	1.5	1.7	17.5	2.2	16.5	2.5	5.5	1.9	15	2.7	12	2.5	9	2.0	28	8.0	5	·		7	·	·	·	3	10	6	6	·	7	·	–
XI	4.5	2.2	5	2.6	14	3.8	15	4.6	11	2.4	17.5	2.5	9.5	2.8	2.5	3.0	11	2.8	10	3.0	1,12	·	2	11	·	·	·	1	22	6	3	·	7	4	–
XII	4.5	1.8	0.5	1.0	13.5	1.8	7.5	2.7	13	3.0	17.5	3.0	15	2.6	4.5	2.7	17	2.1	46	9.3	11	13	17	27	·	·	·	2	18	9	9	·	6	17	–
Rok	125.5	3.1	53	2.5	78	2.6	107	2.6	120	2.9	172	3.3	213.5	3.3	140	3.2	86	3.0	562	25.0	19.VI	23	42	122	8	7	2	29	121	135	111	11	35	–	–

Jastrowie $H_s = 120 m$ $h_w = 13 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	≡	⊞	R ∞
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	44	7.8	25	2	–	19	·	–	–	–	–	24	10	·	1	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	51	13.1	12	4	8	25	·	–	–	–	–	19	14	2	4	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	33	10.1	12	4	7	28	·	–	–	–	–	11	10	1	4	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	41	12.8	16	·	·	7	1	–	–	–	–	13	9	1	3	–	–
V	9.5	2.8	8.5	2.1	0.5	2.0	1.5	1.0	3.5	2.6	12.5	3.1	18.5	2.6	16.5	3.5	22	2.2	87	13.6	14	·	·	5	·	1	·	–	–	20	17	·	1	–	–
VI	14	3.6	10.5	3.0	1.5	2.7	1	4.0	4.5	4.3	9	3.0	22	3.5	13.5	3.3	17	2.7	113	41.2	16	·	·	·	3	·	·	–	–	13	11	4	3	–	–
VII	9.5	2.5	7.5	2.3	1	1.5	·	·	2	1.5	14	2.2	21.5	2.6	8.5	2.2	29	1.6	56	8.4	26	·	·	·	3	1	·	–	–	15	12	·	2	–	–
VIII	3.5	1.9	2	2.5	·	·	8	3.2	4	4.8	27.5	4.0	21.5	3.4	6.5	3.7	20	2.8	58	11.8	23	·	·	·	2	·	·	–	–	12	11	1	·	–	–
IX	3.5	3.1	1	1.5	13	2.0	5	3.2	7	4.8	22	4.5	21.5	4.3	4	2.5	13	3.2	58	15.6	11	·	·	·	1	·	·	–	–	16	13	1	4	–	–
X	11.5	2.7	8.5	2.4	6	1.7	5	1.6	1.5	1.7	15.5	2.0	15.5	3.5	10.5	3.0	19	2.0	16	6.2	31	·	·	7	·	·	·	–	–	7	4	·	12	–	–
XI	3	2.7	8	4.1	17	2.3	5	2.5	10.5	2.9	14	3.0	23.5	3.2	2	3.0	7	2.7	43	8.6	1	·	·	12	·	·	·	–	–	11	11	·	3	–	–
XII	9.5	2.2	16.5	2.6	9	2.1	8	1.6	·	·	6.5	2.5	31	3.4	3.5	2.7	9	2.4	34	8.4	16	12	20	26	·	·	·	–	–	11	8	·	2	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	634	41.2	16.VI	22	–	129	10	–	–	–	–	172	130	10	39	–	–

Kolno $\varphi = 53°25'$ $\lambda = 21°56'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.8	-3.6	6.3	22	-20.6	31	-1.7	0.2	-1.5	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.5	7.9	8.0
II	–	–	–	–	-1.2	-7.2	2.7	12	-16.5	1	-4.7	-2.2	-3.7	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.9	7.8	7.6
III	–	–	–	–	-0.1	-6.9	7.3	31	-16.3	15	-5.4	-0.9	-3.3	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.4	5.5	5.8
IV	–	–	–	–	14.2	4.6	26.2	23	-1.7	8	6.8	13.2	8.3	9.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.7	4.9	6.1
V	–	–	–	–	14.6	5.7	19.5	13	-2.7	1	8.7	13.7	9.8	10.5	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.6	7.7	7.9
VI	–	–	–	–	19.1	8.4	27.6	23	3.2	10	12.7	17.7	12.8	14.0	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.3	5.4	6.4
VII	–	–	–	–	20.9	10.0	28.2	26	5.5	30	13.8	19.2	14.3	15.4	–	–	–	–	–	–	–	–	–	–	–	–	6.1	7.6	5.8	6.5
VIII	–	–	–	–	20.8	10.8	27.5	7,13	5.4	15	13.8	19.4	14.8	15.7	–	–	–	–	–	–	–	–	–	–	–	–	7.0	8.3	5.2	6.8
IX	–	–	–	–	16.1	7.1	24.7	4	0.6	15	8.9	15.3	10.7	11.4	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.4	4.2	6.1
X	–	–	–	–	12.3	3.3	18.9	2	-3.7	28	5.5	11.6	6.8	7.7	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.2	4.4	5.8
XI	–	–	–	–	5.7	1.1	14.2	1	-2.7	25	2.5	4.8	3.2	3.4	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.2	8.6	8.5
XII	–	–	–	–	-2.8	-7.8	3.4	5	-21.4	31	-5.3	-4.0	-5.2	-5.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.3	7.6	7.6
Rok	–	–	–	–	10.0	2.1	28.2	26.VII	-21.4	31.XII	4.6	9.0	5.6	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.4	6.2	6.9

Sokółka $\varphi = 53°24'$ $\lambda = 23°30'$

I	–	–	–	–	0.1	-3.7	4.4	22	-21.9	31	-2.0	-0.6	-1.9	-1.6	5.0	5.2	4.9	5.0	9.0	8.6	8.9	8.8	0.6	0.9	0.7	0.7	8.8	7.5	7.6	8.0
II	–	–	–	–	-1.9	-8.0	2.6	13	-17.4	1	-5.4	-3.2	-4.6	-4.4	3.8	4.1	4.0	4.0	8.9	8.3	8.7	8.6	0.4	0.8	0.5	0.6	8.9	7.6	7.9	8.1
III	–	–	–	–	-0.5	-8.6	5.6	31	-16.5	26	-6.7	-1.4	-4.5	-4.3	3.5	4.1	3.9	3.8	8.9	7.1	8.5	8.2	0.4	1.6	0.6	0.9	6.6	6.4	6.5	6.5
IV	–	–	–	–	13.5	4.8	24.8	23	-1.6	8	6.3	12.1	8.4	8.8	8.8	9.8	9.2	9.3	9.0	7.0	8.3	8.1	1.1	5.6	2.3	3.0	7.7	6.9	4.9	6.5
V	–	–	–	–	14.7	6.3	21.9	27	-2.6	1	8.8	13.2	10.0	10.5	10.3	10.4	10.7	10.5	8.8	6.8	8.6	8.1	1.4	5.2	1.9	2.8	7.4	8.1	6.7	7.4
VI	–	–	–	–	18.4	8.4	26.9	23	2.2	3	12.1	17.1	12.3	13.4	11.4	11.2	11.5	11.4	7.9	5.8	7.9	7.2	3.1	9.0	3.2	5.1	6.4	6.8	5.3	6.2
VII	–	–	–	–	20.6	10.0	27.6	22	5.4	4	14.0	18.9	14.2	15.3	13.6	13.5	13.5	13.5	8.5	6.3	8.3	7.7	2.6	8.9	2.9	4.8	6.1	7.0	5.8	6.3
VIII	–	–	–	–	20.6	11.2	28.8	13	6.4	27	13.7	19.0	14.6	15.5	13.9	14.5	14.4	14.3	8.8	6.7	8.6	8.0	1.9	7.9	2.5	4.1	6.5	6.9	6.0	6.5
IX	–	–	–	–	16.0	7.2	25.7	5	1.9	25	8.9	14.6	10.4	11.1	10.6	11.8	11.6	11.3	9.2	7.1	9.1	8.5	0.9	5.2	1.2	2.4	6.8	7.1	5.0	6.3
X	–	–	–	–	11.7	4.0	19.1	2	-3.2	16	5.3	10.7	6.9	7.4	8.4	9.8	9.4	9.2	9.3	7.5	9.3	8.7	0.6	3.4	0.7	1.6	7.4	6.8	4.7	6.3
XI	–	–	–	–	5.4	1.2	16.1	1	-3.1	27	2.3	4.4	2.9	3.1	7.0	7.3	7.1	7.1	9.3	8.6	9.1	9.0	0.5	1.4	0.7	0.9	8.9	8.1	8.0	8.3
XII	–	–	–	–	-3.5	-8.5	2.5	8	-21.8	21	-5.9	-4.7	-5.8	-5.6	3.9	4.0	3.8	3.9	8.9	8.4	8.7	8.7	0.4	0.7	0.5	0.5	8.2	7.1	7.7	7.7
Rok	–	–	–	–	9.6	2.0	28.8	13.VIII	-21.9	31.I	4.3	8.3	5.2	5.8	8.4	8.8	8.7	8.6	8.9	7.3	8.7	7.3	1.2	4.2	1.5	2.3	7.5	7.2	6.3	7.0

Zawodzie $\varphi = 53°23'$ $\lambda = 21°24'$

I	–	–	–	–	1.1	-3.5	7.3	22	-22.4	31	-1.3	0.3	-1.4	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.6	7.8	8.5
II	–	–	–	–	-0.7	-7.7	3.2	12	-19.9	1	-5.1	-1.8	-3.9	-3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.2	7.1	7.9
III	–	–	–	–	0.6	-7.7	6.5	31	-18.9	15	-5.9	-0.2	-3.6	-3.3	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.0	5.7	6.5
IV	–	–	–	–	14.9	4.0	27.5	23	-2.2	8	6.8	13.8	7.8	9.0	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.4	5.1	6.7
V	–	–	–	–	14.6	5.0	20.0	8	-2.5	2	8.9	13.3	9.2	10.2	–	–	–	–	–	–	–	–	–	–	–	–	7.4	8.6	8.0	8.0
VI	–	–	–	–	19.3	7.6	27.5	23	3.0	13	12.9	17.9	12.5	14.0	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.2	5.3	6.0
VII	–	–	–	–	20.9	9.2	28.5	21,26	4.6	30	14.7	19.5	13.5	15.3	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.1	5.4	6.5
VIII	–	–	–	–	20.9	10.4	28.5	7	4.6	10	13.7	19.3	14.1	15.3	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.7	6.2	6.8
IX	–	–	–	–	16.3	6.8	25.5	4	1.4	15	9.3	15.0	10.2	11.2	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.1	5.0	6.1
X	–	–	–	–	12.5	2.5	20.0	2	-4.4	28	5.3	11.9	6.3	7.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.2	4.8	6.2
XI	–	–	–	–	5.2	0.9	12.9	1	-4.9	26	2.4	4.6	2.8	3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.1	7.8	8.2
XII	–	–	–	–	-2.6	-7.9	4.2	5	-21.4	21	-5.4	-3.6	-5.6	-5.0	–	–	–	–	–	–	–	–	–	–	–	–	8.1	6.7	7.7	7.5
Rok	–	–	–	–	10.2	1.6	28.5	21,26.VII,2.VIII	-22.4	31.I	4.7	9.2	5.2	6.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.3	6.3	7.1

Nidzica $\varphi = 53°22'$ $\lambda = 20°25'$

I	–	–	–	–	0.4	-4.2	6.6	22	-22.9	31	-1.8	-0.3	-1.9	-1.5	–	–	–	–	–	–	–	–	–	–	–	–	9.2	7.8	7.7	8.2
II	–	–	–	–	-1.1	-6.7	2.4	16,20	-18.4	1	-4.8	-2.0	-3.6	-3.5	–	–	–	–	–	–	–	–	–	–	–	–	9.5	8.4	6.6	8.2
III	–	–	–	–	0.0	-7.8	7.5	31	-21.4	15	-5.7	-0.6	-4.0	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.6	4.7	6.5
IV	–	–	–	–	14.0	4.0	26.9	23	-2.2	29	6.5	13.1	7.6	8.7	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.4	4.7	6.2
V	–	–	–	–	13.7	5.1	19.6	28	-2.6	6	8.9	12.5	8.8	9.8	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.3	6.6	7.2
VI	–	–	–	–	18.6	8.3	27.4	16	2.4	3	12.4	17.1	12.4	13.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.5	5.9	6.4
VII	–	–	–	–	19.9	9.7	27.6	26	3.5	30	13.7	18.7	13.7	15.0	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.5	5.7	6.4
VIII	–	–	–	–	19.9	10.3	27.4	7	3.7	10	13.9	18.7	14.2	15.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.5	6.0	6.9
IX	–	–	–	–	15.6	7.3	25.0	4	0.8	15	9.7	14.5	10.5	11.3	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.3	4.4	6.2
X	–	–	–	–	11.7	3.0	18.6	2	-4.5	28	5.4	11.3	6.3	7.3	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.8	5.8	6.9
XI	–	–	–	–	4.4	1.0	12.2	4	-5.3	26	1.9	3.6	2.7	2.7	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.6	8.2	8.7
XII	–	–	–	–	-3.2	-8.1	3.2	5	-20.4	22	-5.9	-4.3	-6.1	-5.6	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.8	6.9	7.6
Rok	–	–	–	–	9.5	1.8	27.6	26.VII	-22.9	31.I	4.5	8.5	5.0	5.8	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.3	6.1	7.1

Kolno — $H_s = 128\,m$ — $h_w = 13\,m$ — 1962

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	=	⊠	R
I	7	10.0	1	2.0	1	5.0	5.5	4.6	10.5	5.0	33.5	6.4	21.5	8.0	7	3.1	6	6.1	19	4.8	21	3	7	21	·	–	–	2	18	15	6	·	3	20	·
II	14.5	1.4	6	8.4	6	5.1	3.5	7.3	14	5.8	14.5	8.4	7	1.4	13.5	7.9	5	8.6	24	4.7	12	9	17	27	·	–	–	·	16	15	9	·	4	28	·
III	10.5	12.5	13.5	6.5	3	3.0	20	5.7	11	3.0	4	5.0	2	5.0	10	11.9	19	5.6	53[2]	—	—	5	14	29	·	–	–	9	14	13	8[2]	2[2]	3	27	
IV	16.5	7.8	12.5	7.6	3.5	6.7	10	5.4	14.5	5.1	8	4.9	4	5.0	11	5.5	10	5.5	30	10.5	13	·	·	4	3	–	–	1	10	9	6	1	4	·	1
V	10.5	3.6	6	4.2	1	5.0	6.5	3.7	8.5	2.8	11.5	4.3	24	4.6	10	4.8	15	3.5	122	21.2	20	·	·	3	·	–	–	·	18	20	17	5	1	·	5
VI	12.5	9.8	7	2.9	1	2.0	3.5	3.6	8.5	2.9	17.5	6.2	20	5.7	8	4.4	12	4.9	76	21.0	3	·	·	·	4	–	–	3	12	13	10	2	·	·	3
VII	13.5	5.1	·	·	·	·	0.5	7.0	10	3.6	16.5	3.8	16	4.6	21.5	5.4	15	3.9	61	13.5	26	·	·	·	4	–	–	·	6	14	9	2	4	·	3
VIII	8	6.9	1	7.0	1	2.0	2	6.0	11.5	4.8	22	4.5	22.5	6.4	7	5.6	18	4.5	138	25.7	17	·	·	·	4	–	–	·	9	15	14	5	5	·	5
IX	5	6.2	2	3.5	6	2.7	5	2.6	14	3.5	15.5	6.1	18.5	6.1	10	6.0	14	4.3	57	26.5	18	·	·	·	·	–	–	3	7	11	10	1	7	·	4
X	5	3.8	·	·	1	3.0	4	2.7	8	2.5	9	4.3	18	5.3	7	5.1	41	2.4	11	7.3	28	·	·	7	·	–	–	3	9	9	1	·	18	·	·
XI	7	4.1	4	14.0	12	7.7	18	6.2	8	2.9	8	6.2	11	5.2	1	1.0	21	4.7	53	14.0	15			11	·	–	–	2	23	12	8	1	11	2	·
XII	20	3.3	4	4.2	1	5.0	4.5	3.9	16.5	3.8	28	5.6	13	5.2	3	3.7	3	4.4	13	3.6	14	9	17	26		–	–	4	19	12	5	·	3	17	·
Rok	130	6.2	57	5.0	36.5	3.9	83	4.9	135	3.8	188	5.5	177.5	5.2	109	5.4	179	4.9	657[2]	26.5	18.IX	26	55	128	15	–	–	27	161	158	103[2]	19[2]	63	94	21

Sokółka — $H_s = 180\,m$ — $h_w = 17\,m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	=	⊠	R
I	3.5	9.3	5.5	4.8	5	4.6	3.5	6.0	15	5.4	29.5	5.9	23.5	6.6	7.5	5.3		6.0	24	4.7	13	3	10	22		9	·	1	19	19	7	·	4	28	·
II	12.5	6.4	7.5	6.3	11	6.1	7	5.0	9	8.2	14	10.0	11	7.5	12	7.5	·	7.3	37	8.7	12	9	16	28		10	7	·	18	20	10	·	3	28	·
III	16	6.0	13.5	4.1	20	3.0	11.5	5.7	2.5	4.4	3	3.2	6	8.2	12.5	4.9	8	4.4	28	4.6	31	11	16	29	·	7	2	3	13	16	10	·	6	31	·
IV	8.5	3.3	18.5	3.1	11.5	4.6	11.5	5.4	6.5	5.5	6.5	4.0	6	5.4	12	4.4	9	3.8	56	13.0	27	·	·	3	·	2	1	1	9	16	9	2	3	4	2
V	18.5	2.6	3.5	2.7	9.5	4.0	7	3.6	·	-	4	4.0	20.5	4.9	23	4.0	7	3.6	96	14.3	24	·	·	3	·	3	1	·	14	21	17	2	1	·	4
VI	19	5.6	3	5.0	3	2.3	·	·	4	3.2	9.5	5.4	18.5	5.2	24	3.2	9	4.1	67	24.0	4	·	·	·	2	3	·	·	6	13	11	2	·	·	3
VII	13.5	3.0	0.5	5.0	3	2.2	0.5	2.0	10	4.3	7.5	3.7	21.5	4.4	28.5	4.4	8	3.7	52	17.1	26	·	·	·	5	1	·	1	7	14	12	2	·	·	9
VIII	5.5	3.5	1.5	2.0	2	1.5	6.5	4.9	5	3.5	13	6.5	33	5.0	11.5	2.1	15	3.7	125	28.3	15	·	·	·	4	5	2	1	8	14	13	4	2	·	7
IX	7.5	2.9	7.5	2.3	4	2.8	5	3.0	8.5	4.5	9.5	4.9	28	4.9	12	2.5	8	3.5	83	17.5	18	·	·	·	1	3	·	3	11	16	14	2	2	·	3
X	8.5	2.1	4	1.6	4.5	2.1	11.5	2.4	3	2.3	8.5	2.7	20.5	4.7	15.5	3.7	17	2.6	4	1.3	14	·	·	4		·	·	4	12	8	1	·	9	·	·
XI	8.5	2.7	8.5	6.4	24	6.7	24	5.6	3.5	5.1	5.5	4.5	9	5.5	7	3.9	·	5.5	46	8.3	15	·	·	13	·	5	·	2	22	21	13	·	11	7	·
XII	20	3.6	11	4.8	2.5	4.8	5.5	3.1	14.5	5.4	16.5	5.8	12.5	6.2	10.5	4.8	·	4.9	19	6.5	14	12	18	27	·	3	·	3	19	15	6	·	3	21	·
Rok	141.5	4.2	84.5	4.0	100	3.7	93.5	3.9	81.5	4.3	127	5.0	210	5.7	176	4.2	81	4.4	637	28.3	15.VIII	35	60	129	12	51	13	19	158	193	123	14	44	119	28

Zawodzie — $H_s = 122\,m$ — $h_w = 12\,m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	=	⊠	R
I	4	3.0	5	2.0	1	2.0	3.5	2.4	18.5	2.2	41	3.6	17	3.2	2	3.0	1	3.0	22	4.2	25	3	6	21	·	1	·	2	20	15	6	·	1	20	·
II	10.5	3.9	6	3.5	9	2.1	4	1.8	20	3.5	12	4.5	13.5	6.0	8	6.0	1	4.1	47	10.1	16	9	15	27	·	5	·	·	15	18	11	1	2	28	·
III	9	4.3	10.5	2.5	9.5	3.1	25.5	1.9	4.5	2.1	4	2.5	16	3.1	11	2.9	3	2.6	43	10.0	5	11	9	29	·	·	·	2	13	12	8	1	·	31	
IV	7.5	2.5	10	3.0	5.5	1.8	15	2.8	13	2.7	10	2.2	11	2.5	12	2.8	6	2.4	49	13.8	26	·	·	6	4	·	·	1	12	12	6	2	2	·	1
V	8.5	1.5	5.5	1.6	6	1.8	5	2.0	7.5	1.9	17	2.3	26.5	2.8	13	2.2	4	2.1	105	14.8	14	·	·	5	·	·	·	·	19	23	19	3	1	·	2
VI	16.5	3.2	6	2.4	·	·	3.5	1.9	2.5	1.4	18.5	2.9	27	3.4	15	2.2	1	2.8	20	4.6	29	·	·	·	5	·	·	2	9	13	6	·	·	·	2
VII	13.5	2.1	4	2.2	·	·	0.5	1.0	9.5	1.5	21.5	2.2	30.5	3.2	11.5	2.3	2	2.4	59	19.4	13	·	·	·	4	·	·	·	5	16	7	2	·	·	4
VIII	3.5	2.0	0.5	1.0	2	2.5	2.5	1.2	5.5	1.7	27.5	2.7	40	2.8	10.5	2.1	1	2.5	137	29.7	17	·	·	·	4	·	·	1	9	19	16	4	·	·	7
IX	3	2.3	1.5	1.7	9	1.7	5.5	1.7	9	2.2	16.5	3.0	32	3.0	5.5	3.4	8	2.4	54	18.1	18	·	·	·	1	·	·	2	10	18	11	2	1	·	2
X	6.5	1.5	1	1.0	0.5	1.0	11.5	1.5	12	1.7	13	2.7	33	2.7	5.5	2.1	10	2.0	13	5.0	28	·	·	12	·	·	·	3	12	10	6	·	8	·	
XI	5.5	1.6	7.5	4.2	27	2.8	9.5	1.9	8	1.8	14.5	2.7	15	2.0	1	2.0	2	2.4	60	16.1	20	·	1	13	·	·	·	2	21	19	11	1	5	3	·
XII	16	1.6	15	2.0	1	1.0	9.5	1.8	20	2.2	15.5	2.8	10	3.0	4	1.8	2	2.1	12	3.3	11	9	16	28	·	·	·	3	19	11	4	·	2	20	·
Rok	104	2.5	72.5	2.3	70.5	1.6	95.5	1.8	130	2.1	211	2.8	271.5	3.1	99	2.7	41	2.6	621	29.7	17.VIII	32	47	141	18	6		18	164	186	111	16	22	102	18

Nidzica — $H_s = 170\,m$ — $h_w = 13\,m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	=	⊠	R
I	4	3.5	·		·		2.5	3.8	13.5	4.1	38	4.3	11.5	4.7	9.5	3.5	14	3.5	39	6.4	25	3	7	24	·	·	·	1	18	16	11	·	5	19	
II	9	5.8	9	3.4	5	2.6	5.5	3.4	6	3.1	20.5	6.1	5	6.6	17	6.8	7	4.8	47	7.7	12	6	13	27	·	5	3	·	17	14	13	·	–	28	
III	13	5.6	8.5	3.0	5	2.4	18.5	3.3	6.5	3.0	5.5	4.0	4	4.0	9	7.2	23	3.2	44	6.6	6	10	14	29	·	2	1	1	11	15	12	·	–	26	·
IV	17.5	3.3	4	5.2	2	5.5	11	4.3	12.5	4.9	13	4.3	0.5	5.0	11.5	4.3	18	3.4	47	8.0	5	·	·	6	2	·	·	3	8	15	14	·	–	·	1
V	6.5	1.8	8.5	2.5	3	2.0	10.5	3.9	3.5	3.1	18.5	4.2	4.5	3.9	18	4.8	20	2.9	122	29.6	14	·	·	2	·	·	·	·	8	22	18	4	–	·	5
VI	17	5.0	2	6.5	·	·	4	2.2	5.5	3.4	18.5	4.8	11	4.5	21	4.0	11	3.9	39	16.7	29	·	·	·	3	3	·	·	7	12	11	1	–	·	3
VII	16.5	3.5	0.5	4.0	1	2.0	1.5	2.3	8	3.9	15	4.3	10	4.2	24.5	3.7	16	3.1	63	20.1	13	·	·	·	3	·	·	·	4	12	8	2	–	·	2
VIII	5	3.2	·	·	·	·	4.5	2.9	6.5	3.7	34.5	5.4	12.5	4.1	17	2.6	13	3.6	90	20.3	17	·	·	·	4	1	·	·	14	15	13	3	–	·	6
IX	6	3.2	4.5	2.0	3.5	2.3	1	3.0	9	2.9	24	4.9	6.5	4.8	12.5	3.7	23	2.9	72	20.4	18	·	·	·	·	·	·	1	9	15	14	2	–	·	2
X	3.5	1.9	·	·	·	·	11	2.5	5.5	2.7	17.5	4.7	9.5	4.2	10	4.1	36	2.3	11	2.7	14,27	·	·	7	·	1	·	·	14	6	4	·	19	·	·
XI	2	3.5	9.5	4.9	10	6.4	17.5	5.3	4	4.8	22	3.7	6	3.7	4	1.8	15	3.8	50	11.5	20	·	2	12	·	2	·	·	22	12	10	1	12	3	·
XII	13.5	2.3	3.5	3.0	3	3.0	3	3.0	8	4.4	24	4.5	8	5.0	10	2.6	20	2.9	22	4.4	10	10	19	27	·	·	·	3	17	13	9	·	6	16	·
Rok	113.5	3.6	50	2.9	32.5	2.2	90.5	3.3	88.5	3.7	251	4.6	89	4.6	164	4.1	216	3.4	646	29.6	14.V	29	55	134	12	14	4	9	149	167	137	13	–	92	19

Lipki $\varphi = 53°21'$ $\lambda = 14°58'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{m.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	-	-	-	-	3.5	-0.8	8.7	22	-14.1	31	0.8	2.4	1.2	1.4	5.8	6.1	5.9	5.9	8.7	8.2	8.6	8.5	0.9	1.4	1.0	1.1	8.5	8.0	8.4	8.3
II	-	-	-	-	2.7	-2.6	8.2	8	-14.1	1	-0.4	1.5	0.0	0.3	5.3	5.6	5.1	5.3	8.7	8.0	8.2	8.3	0.8	1.4	1.2	1.1	8.1	7.3	6.6	7.3
III	-	-	-	-	3.2	-3.8	13.0	30	-12.3	16	-2.2	2.4	-0.4	-0.2	4.5	5.0	4.8	4.8	8.4	6.8	8.0	7.7	0.8	2.4	1.2	1.5	4.7	5.5	5.9	5.4
IV	-	-	-	-	13.8	3.9	27.1	25	-0.1	11	6.1	12.4	7.8	8.5	8.2	8.7	8.6	8.5	8.6	5.9	8.0	7.5	1.4	6.7	2.4	3.5	6.9	5.2	5.0	5.7
V	-	-	-	-	14.0	5.9	20.2	19	-0.2	1,2	8.9	12.5	9.4	10.0	10.0	9.5	10.0	9.8	8.7	6.5	8.3	7.8	1.6	5.4	2.0	3.0	5.8	7.0	7.6	6.8
VI	-	-	-	-	19.2	8.3	29.2	15	1.6	6	12.6	17.5	13.1	14.1	11.6	11.5	11.9	11.7	7.8	5.6	7.6	7.0	3.3	9.4	3.6	5.4	4.7	5.6	5.9	5.4
VII	-	-	-	-	20.0	10.5	26.4	21	5.0	10	14.0	18.7	13.8	15.1	14.0	13.3	14.0	13.8	8.7	6.2	8.8	7.9	2.1	8.7	2.0	4.3	6.2	6.5	6.4	6.4
VIII	-	-	-	-	19.8	11.2	28.1	12	7.5	10	14.0	18.3	14.3	15.2	14.1	14.2	14.3	14.2	8.8	6.8	8.7	8.1	2.0	7.1	2.2	3.8	7.0	7.3	7.5	7.3
IX	-	-	-	-	16.9	7.8	25.5	4	3.4	25	10.0	15.6	11.3	12.0	11.4	12.0	11.8	11.8	9.2	6.8	8.7	8.2	1.0	6.2	1.8	3.0	6.4	7.0	5.0	6.1
X	-	-	-	-	13.0	4.6	22.9	3	-0.4	15	6.4	11.8	8.0	8.6	9.2	10.6	9.9	9.9	9.4	7.5	9.0	8.6	0.6	3.7	1.1	1.8	7.0	6.5	5.1	6.2
XI	-	-	-	-	5.6	1.6	14.3	8	-2.8	17,24	2.8	4.8	3.2	3.5	6.9	7.3	7.0	7.1	9.1	8.4	8.9	8.8	0.7	1.6	0.9	1.1	8.3	7.9	7.1	7.8
XII	-	-	-	-	-0.7	-5.5	5.6	10	-15.6	22	-3.6	-1.9	-3.3	-3.0	4.3	4.7	4.4	4.5	8.6	8.3	8.5	8.5	0.6	0.8	0.6	0.7	7.8	7.2	6.8	7.3
Rok	-	-	-	-	10.9	3.4	29.2	15 VI	-15.6	22 XII	5.8	9.7	6.5	7.1	8.8	9.0	9.0	8.9	8.7	7.1	8.4	8.1	1.3	4.6	1.7	2.5	6.8	6.8	6.4	6.7

Wałcz $\varphi = 53°17'$ $\lambda = 16°28'$

I	999.4	1027.0	970.7	1013.7	2.8	-1.2	8.4	22	-14.9	31	0.4	1.8	0.6	0.8	5.7	5.8	5.7	5.7	8.8	8.2	8.6	8.5	0.8	1.3	0.9	1.0	8.0	8.8	8.5	8.4
II	1004.0	[illegible]	964.5	1015.3	1.4	-3.3	5.7	8	-12.7	1	-2.0	0.5	-0.9	-0.8	4.5	5.0	4.7	4.7	8.3	7.6	8.0	8.0	0.9	1.5	1.2	1.2	8.8	8.9	8.0	8.6
III	997.1	1013.3	969.3	1011.4	3.0	-4.9	11.6	30	-10.8	14	-3.4	2.0	-1.4	-1.0	4.3	4.8	4.3	4.5	8.6	6.7	7.7	7.7	0.7	2.4	1.3	1.5	7.5	6.9	6.0	6.8
IV	999.3	1014.1	972.9	1013.1	14.5	4.5	25.6	25	-0.8	30	6.3	13.1	8.9	9.3	8.5	9.6	9.2	9.1	8.7	6.2	7.8	7.6	1.4	6.7	2.8	3.6	7.2	7.4	6.2	6.9
V	998.4	1004.7	989.8	1012.2	14.3	6.0	20.2	19	-1.4	1	8.5	12.8	9.4	10.0	9.8	9.7	10.3	9.9	8.8	6.5	8.6	8.0	1.4	5.4	1.7	2.8	7.7	8.5	7.1	7.8
VI	1004.5	1017.6	994.6	1018.1	19.3	8.3	29.7	15	1.0	3	12.3	17.4	13.4	14.1	11.6	12.4	12.3	12.1	7.9	6.2	7.8	7.3	3.1	8.5	3.5	5.0	5.8	6.7	5.3	5.9
VII	1000.2	1011.1	980.6	1013.7	20.4	9.9	27.2	26	6.7	30	13.2	18.8	14.4	15.2	13.8	14.2	14.5	14.2	9.0	6.6	8.7	8.1	1.5	8.1	2.1	3.9	6.5	7.2	5.4	6.4
VIII	1000.5	1009.6	988.7	1014.0	19.9	11.4	28.8	12	7.5	10	13.4	18.6	14.7	15.4	13.8	14.7	14.4	14.3	8.9	6.8	8.5	8.1	1.7	7.2	2.5	3.8	7.5	8.2	5.5	7.1
IX	1001.4	1015.9	980.6	1015.1	16.6	7.6	26.2	4	2.3	18	9.4	15.5	11.0	11.7	11.0	12.0	11.7	11.6	9.2	6.8	8.9	8.3	1.0	6.1	1.6	2.9	7.3	7.0	4.3	6.2
X	1007.7	1022.7	994.4	1021.7	12.4	4.5	21.2	3	-2.1	16	6.0	11.6	7.8	8.3	9.0	10.7	9.9	9.9	9.3	7.7	9.1	8.7	0.6	3.4	1.0	1.7	7.1	6.9	4.6	6.2
XI	1002.4	1019.8	982.9	1016.5	5.0	1.5	13.1	5	-2.3	25	2.5	4.5	3.2	3.4	6.8	7.3	7.0	7.0	9.1	8.5	9.0	8.9	0.7	1.3	0.8	0.9	8.8	8.5	8.0	8.4
XII	1001.8	1033.8	956.1	1016.3	-1.7	-6.7	5.3	12	-18.9	22	-5.0	-2.8	-4.2	-4.0	4.1	4.4	4.1	4.2	8.7	8.3	8.5	8.5	0.5	0.8	0.6	0.6	6.9	8.2	6.4	7.2
Rok	1001.1	1033.8	956.1	1015.1	10.7	3.1	29.7	15 VI	-18.9	22 XII	5.1	9.5	6.4	6.8	8.6	9.2	9.0	8.9	8.8	7.2	8.4	8.1	1.2	4.4	1.7	2.4	7.4	7.8	6.3	7.2

Lidzbark $\varphi = 53°16'$ $\lambda = 19°50'$

I	-	-	-	-	1.0	-3.1	7.5	22	-19.8	31	-1.2	0.1	-1.1	-0.8	5.2	5.2	5.2	5.2	8.8	8.1	8.8	8.6	0.7	1.2	0.7	0.9	9.0	8.1	8.5	8.5
II	-	-	-	-	-0.7	-5.6	2.7	20	-15.6	1	-3.2	-1.9	-2.7	-2.6	4.3	4.5	4.4	4.4	8.7	8.2	8.5	8.4	0.6	0.9	0.7	0.7	8.8	8.1	7.2	8.0
III	-	-	-	-	0.3	-6.1	9.3	31	-15.1	15	-4.3	-0.3	-2.6	-2.4	3.8	4.5	4.2	4.2	8.2	7.3	8.1	7.9	0.8	1.6	1.0	1.1	6.4	5.5	5.8	5.9
IV	-	-	-	-	14.2	4.4	26.3	23	-0.6	30	7.3	12.7	8.8	9.4	8.4	8.3	9.3	8.7	8.1	5.7	7.9	7.2	2.3	8.1	2.7	4.4	6.1	4.5	5.2	5.3
V	-	-	-	-	14.1	5.3	19.1	13	-2.2	1	8.9	12.4	9.8	10.2	9.7	9.7	10.4	9.9	8.4	6.7	8.5	7.9	2.0	5.2	1.9	3.0	6.9	6.3	7.0	6.7
VI	-	-	-	-	19.2	8.2	28.2	16,18	2.3	3	13.2	17.1	14.5	14.8	11.1	10.9	12.0	11.3	7.2	5.5	7.2	6.6	4.6	9.4	4.9	6.3	-	-	-	-
VII	-	-	-	-	20.1	10.2	27.8	26	5.0	30	14.2	18.5	14.8	15.6	13.8	13.5	14.0	13.8	8.5	6.4	8.3	7.7	2.6	8.3	3.2	4.7	6.3	5.5	5.1	5.6
VIII	-	-	-	-	20.3	11.2	28.1	7	5.6	10	13.9	18.9	14.6	15.5	14.0	14.2	14.5	14.2	8.7	6.6	8.6	8.0	2.0	8.1	2.4	4.2	6.9	7.8	5.9	6.9
IX	-	-	-	-	16.0	7.7	26.3	4	3.1	25	9.7	14.8	11.2	11.7	11.1	11.8	11.8	11.6	9.1	7.0	8.8	8.3	1.1	5.5	1.7	2.8	6.9	7.4	4.7	6.3
X	-	-	-	-	12.3	3.4	19.7	2	-3.6	28	6.0	11.7	6.6	7.7	9.0	10.0	9.2	9.4	9.4	7.2	9.2	8.6	0.6	4.2	0.8	1.9	8.5	6.7	6.4	7.2
XI	-	-	-	-	4.8	1.2	13.0	4	-6.9	26	2.1	4.0	3.0	3.0	6.8	7.1	6.8	6.9	9.3	8.5	8.8	8.9	0.5	1.3	1.0	0.9	9.0	8.9	8.4	8.8
XII	-	-	-	-	-3.0	-7.8	3.3	12	-19.9	21	-5.6	-4.0	-5.7	-5.2	3.9	4.2	3.8	4.0	8.8	8.6	8.5	8.6	0.5	0.6	0.6	0.6	8.2	7.7	7.3	7.7
Rok	-	-	-	-	9.9	2.4	28.2	16,18 VI	-19.9	21 XII	5.1	8.7	5.9	6.4	8.4	8.7	8.8	8.6	8.6	7.2	8.4	8.1	1.5	4.5	1.8	2.6	-	-	-	-

Kisielnica $\varphi = 53°15'$ $\lambda = 22°07'$

I	-	-	-	-	0.9	-3.7	6.7	22	-19.8	31	-1.7	-0.2	-1.6	-1.3	5.1	5.3	5.1	5.2	9.0	8.4	8.9	8.8	0.5	1.0	0.6	0.7	8.0	7.9	8.3	8.1
II	-	-	-	-	-1.2	-7.8	2.3	12,20	-16.5	1	-5.0	-2.6	-4.1	-4.0	4.0	4.3	4.2	4.2	8.8	8.2	8.8	8.6	0.4	0.9	0.5	0.6	7.4	5.9	6.1	6.5
III	-	-	-	-	0.1	-8.2	7.7	31	-18.4	15	-6.3	-1.1	-4.0	-3.8	3.6	4.5	4.2	4.1	8.3	7.8	8.8	8.3	0.5	1.2	0.5	0.7	6.5	6.6	5.5	6.2
IV	-	-	-	-	14.3	4.7	26.5	22	-1.8	30	6.8	12.9	8.0	8.9	9.0	9.3	9.4	9.2	8.8	6.4	8.4	7.9	1.3	6.8	1.9	3.3	6.7	6.6	3.7	5.7
V	-	-	-	-	14.7	5.6	19.3	13,23	-2.4	1	8.8	13.5	9.5	10.3	10.3	9.9	10.2	10.1	8.8	6.3	8.7	7.9	1.3	6.0	1.7	3.0	7.8	8.1	7.4	7.8
VI	-	-	-	-	18.7	8.4	28.2	23	4.0	13	12.4	17.0	12.5	13.6	11.7	11.3	11.9	11.6	7.9	5.9	8.1	7.3	3.2	8.9	3.0	5.0	6.5	6.3	5.0	5.9
VII	-	-	-	-	20.6	9.7	27.0	26	5.2	30	13.7	19.2	13.7	15.1	14.2	13.4	13.7	13.8	9.0	6.0	8.6	7.9	1.7	9.2	2.3	4.4	6.7	6.9	5.4	6.3
VIII	-	-	-	-	20.9	10.3	28.0	13	5.5	27	13.6	19.3	14.0	15.2	14.2	14.6	14.4	14.4	9.1	6.5	8.9	8.2	1.5	8.2	1.9	3.9	6.9	6.9	5.5	6.4
IX	-	-	-	-	16.3	6.7	25.0	5	0.9	15	9.2	15.2	10.3	11.2	11.0	11.8	11.6	11.5	9.4	6.9	9.2	8.5	1.0	5.9	1.1	2.7	6.3	6.5	4.8	5.9
X	-	-	-	-	12.1	3.1	19.5	2	-3.7	16	5.1	11.2	6.4	7.3	8.6	10.1	9.2	9.3	9.6	7.6	9.3	8.8	0.4	3.5	0.6	1.5	7.0	6.7	5.1	6.3
XI	-	-	-	-	5.7	1.3	14.9	1	-2.6	18	2.4	4.7	3.1	3.3	6.9	7.2	7.0	7.0	9.2	8.3	8.9	8.8	0.5	1.7	0.9	1.0	8.2	7.8	8.1	8.0
XII	-	-	-	-	-2.7	-7.5	3.7	5	-20.4	21	-5.8	-4.4	-5.6	-5.4	4.0	4.1	3.9	4.0	9.0	8.5	8.8	8.8	0.3	0.6	0.5	0.5	8.2	7.6	7.5	7.8
Rok	-	-	-	-	10.0	1.9	28.2	23 VI	-20.4	21 XII	4.4	8.7	5.2	5.9	8.6	8.8	8.7	8.7	8.9	7.2	8.8	8.3	1.0	4.5	1.3	2.3	7.2	7.0	6.0	6.7

Lipki $H_s = 30\,m$ $h_w = 10\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v≥10	v≥15	☾	●	Opad R ≥0.1	≥1.0	≥10.0	≡	⊞	⊠
I	5	6.4	2	2.5	2.5	3.4	9	4.8	22.5	5.0	30	6.4	14.5	4.9	3.5	6.0	4	5.2	34	6.9	16	2	4	12	·	6	1	3	22	13	11	·	2	3	·
II	9	7.1	11.5	6.0	5	4.6	2.5	5.0	10	4.0	19	6.8	18.5	8.3	6.5	7.9	2	6.5	45	11.7	16	2	6	22	·	6	3	1	14	12	8	1	2	3	3
III	7.5	3.8	12	3.2	8	4.7	14.5	5.7	14	3.6	5	3.9	8.5	5.0	6.5	6.9	17	3.7	41	8.9	12	1	4	28	·	5	·	8	10	13	9	·	1	–	·
IV	10.5	4.7	7	5.4	11	4.4	7	4.2	11.5	4.1	13.5	5.9	8.5	4.8	10	4.4	11	4.2	42	8.4	16	·	·	1	3	1	·	5	8	16	12	·	2	·	1
V	10	4.3	1.5	3.3	3	3.8	6	4.8	11	4.3	20.5	3.8	15	5.2	10	5.2	16	3.7	90	9.4	9	·	·	3	·	1	·	2	12	21	19	·	·	·	9
VI	13	5.4	1	6.0	1.5	2.7	3	4.7	8	3.8	13	4.9	23.5	5.5	11	3.9	16	4.0	45	12.8	15	·	·	·	5	1	·	8	10	11	9	1	2	·	5
VII	4	2.8	3.5	3.3	4.5	2.4	5	2.3	0.5	5.0	22.5	4.2	19.5	4.7	4.5	3.6	29	2.7	73	12.5	3	·	·	·	2	·	·	2	11	17	13	2	4	·	5
VIII	6.5	3.5	1	4.0	5	3.3	3	4.0	8.5	4.8	29.5	5.5	20.5	5.7	5	4.2	14	4.3	92	13.4	5	·	·	·	1	2	·	2	13	18	15	4	·	·	3
IX	1.5	3.0	0.5	3.0	12.5	4.4	12	4.5	6	4.0	14	5.5	22.5	5.5	9	5.3	12	4.3	48	10.6	18	·	·	·	1	3	·	3	11	13	12	1	4	·	3
X	0.5	3.0	3.5	2.1	5.5	3.5	16.5	3.6	14.5	4.2	12.5	3.9	16.5	5.2	7.5	4.0	16	3.4	10	5.5	4	·		2	·	1	·	5	12	3	3	·	11	·	1
XI	0.5	3.0	10.5	6.9	17.5	5.5	10	5.6	9	4.3	13.5	5.1	12	4.5	3	4.5	14	4.5	26	4.3	18	·	1	9	·	4		4	19	10	8	·	9	5	·
XII	2.5	2.6	6.5	2.6	12.5	4.0	6.5	3.5	17.5	4.5	20.5	5.9	7	5.4	6	3.2	14	3.8	32	8.8	11	8	15	26	·	3		3	19	8	7	·	6	3	·
Rok	70.5	4.1	60.5	4.0	88.5	3.9	95	4.4	133	4.3	213.5	5.2	186.5	5.4	82.5	4.9	165	4.2	578	13.4	5.VIII	13	30	103	12	33	4	46	161	155	126	9	43	–	30

Wałcz $H_s = 111\,m$ $H_b = 113{,}8\,m$ $h_w = 23\,m$

I	2	2.2	1.5	2.0	4	1.2	7	3.8	11.5	3.5	32.5	3.8	25	2.9	9.5	3.2	·	3.3	48	9.6	12	2	4	13	·	1		1	21	20	13	·	1	15	·
II	8	3.4	1.2	3.1	2	2.0	2.5	4.8	8	3.4	16.5	5.4	24.5	3.3	10.5	5.3	·	4.0	63	18.6	12	2	8	23	·	5	·		18	21	10	1	·	17	·
III	13.5	1.6	5	2.4	1.3	2.6	3.5	2.0	8.5	1.6	5	1.2	20	1.7	21.5	2.3	3	1.9	36	12.5	12	2	5	28	·	·	·	3	16	15	8	1	2	16	·
IV	7	2.4	10.5	3.4	7	2.0	2	2.5	5	3.2	17	2.6	23.5	1.9	14	1.8	4	2.3	50	16.8	16	·	·	1	1	·	·	2	12	16	10	1	1	·	1
V	3	2.0	·	·	2	1.5	4.5	2.6	4	3.4	21.5	2.2	40.5	2.2	16.5	2.2	1	2.2	94	12.3	28	·	·	3	·	·	·	·	16	23	19	2	·	·	5
VI	11	2.7	1	3.0	4.5	1.1	1.5	1.3	5.5	1.4	20.5	3.0	28.5	2.9	13.5	2.4	4	2.5	113	38.4	16	·	·	·	4	1	·	3	8	16	13	4	·	·	5
VII	7	1.0	4	1.7	8.5	1.5	2.5	2.4	3	3.0	20.5	1.8	30	1.9	12.5	1.6	5	1.7	64	14.3	26	·	·	·	3	·	·	2	8	15	10	2	1	·	3
VIII	7	1.1	1	1.0	7.5	1.3	1	1.5	9	1.7	18	3.1	42.5	2.7	2	1.0	5	2.2	79	12.1	5.21	·	·	·	2	·	·	1	12	17	14	2	·	·	2
IX	1	1.0	3.5	1.4	1.5	1.9	3.5	2.1	1.1	2.2	11	3.1	35	2.7	5	2.2	5	2.3	56	13.8	18	·	·	·	1	·	·	3	7	16	11	1	2	·	1
X	5	1.2	1.5	1.3	1.3	1.3	3.5	1.7	14.5	1.9	11	2.3	20.5	2.1	12	1.9	12	1.6	14	6.0	31	·	·	5	·	·	·	6	12	8	4	·	7	·	·
XI	4.5	1.9	10.5	3.9	2.0	3.6	1.1	2.5	8	2.0	19.5	1.9	11.5	2.0	2	2.0	3	2.5	38	9.4	1	·	·	9	·	·	·	2	22	12	8	·	1	3	·
XII	1.0	1.0	12.5	1.3	1.4	2.0	3	1.7	8	2.1	12	3.6	23	2.7	5.5	1.4	5	2.0	44	12.4	11	7	18	26	·	·	·	3	16	14	9	1	3	18	·
Rok	7.9	1.8	6.3	2.0	11.0.5	1.8	4.5.5	2.4	9.6	2.4	20.5	2.8	32.4.5	2.4	12.4.5	2.3	4.7	2.4	699	38.4	16.VI	13	35	108	11	7	·	26	168	193	129	15	18	69	17

Lidzbark $H_s = 150\,m$ $h_w = 11{,}0\,m$ I–VI, $11{,}6\,m$ VII–XII

I	5	5.7	4	3.2	2.5	2.0	4	3.4	24.5	4.2	36.5	5.2	12.5	2.6	1	4.5	3	4.2	21	6.2	12	3	9	21	·	2	·	2	24	12	7	·	3	18	·
II	5	5.6	1	5.0	1.5.5	5.1	5.5	3.0	14.5	7.4	24	5.5	10.5	6.2	4	6.5	4	5.5	18	2.8	12	2	12	27	·	6	·	·	18	17	8	·	8	28	·
III	7.5	4.1	4	4.2	1.2	2.5	2.0	4.0	16.5	2.5	13	3.7	4	3.5	4	8.8	12	3.2	31	5.4	12	6	11	30	·	4	·	5	11	15	10	·	7	31	·
IV	1.2	3.4	1.5	1.7	5.5	6.0	1.2	4.0	17	2.8	14	4.2	8.5	2.6	11.5	4.1	8	3.3	22	6.5	1		·	4	3	3	·	5	7	14	7		3	·	1
V	2	2.0	3	3.0	3	3.7	10.5	2.5	21.5	2.8	16	2.7	25	3.9	2	3.0	10	2.8	127	28.3	14	·	·	5	·	1	·	2	11	20	17	4	6	·	9
VI	1.3	5.9	·	·	1	2.0	6.5	4.6	24	2.3	17	3.6	25.5	3.5	2	2.0	1	3.5	78	47.0	29	·	·	·	2	2	·	–	–	11	9	1	1	·	4
VII	14.5	3.2	3.5	4.3	1.5	3.0	2	6.2	7	3.6	22.5	3.2	23	2.9	1.3	2.7	6	3.0	65	22.3	13	·	·	·	3	·	·		5	15	9	1	2	·	5
VIII	4	3.0			1.5	5.0	3.5	2.9	10	4.2	13	5.1	31.5	4.7	12.5	3.4	17	3.5	78	25.6	17	·	·	·	4	2	·	2	13	13	12	2	5	·	4
IX	3.5	3.0	2.5	2.0	6	2.6	6.5	3.4	10.5	4.3	10.5	4.3	25.5	4.1	11	3.4	14	3.2	77	24.7	18	·	·	·	1	2	·	3	9	16	14	2	11	·	4
X	6.5	1.8	·		0.5	3.0	12.5	3.2	15.5	3.2	11	3.0	15.5	3.6	11.5	2.9	20	2.4	11	4.6	28	·	·	7	·	·	·	·	13	8	4		16	·	·
XI	3	1.7	5.5	5.0	1.5.5	6.5	2.1.5	5.3	7.5	3.5	13	2.8	16.5	2.7	3.5	2.8	4	4.0	41	10.7	20	·	3	11	·	3	·	1	24	15	9	1	6	9	·
XII	5	2.5	1.5.5	2.6	6.5	3.5	5	4.7	15.5	4.6	11	4.7	17.5	3.3	11	1.8	6	3.2	11	3.0	11	10	17	27	·	·	·	3	21	11	4	·	7	17	·
Rok	8.1	3.5	4.0.5	2.6	7.1	3.7	10.9.5	3.9	18.4	3.8	20.1.5	4.0	21.5.5	3.6	8.7	3.8	10.5	3.5	580	47.0	29.VI	21	52	132	13	25	·	–	–	16.7	110	11	75	103	27

Kisielnica $H_s = 140\,m$ $h_w = 14\,m$

I	1	8.0	5	5.2	4	3.9	3.5	3.0	7.5	3.9	4.2	4.3	2.5	5.2	5	5.8	·	4.6	36	8.4	26	3	6	21	·	2	·	1	18	10	9	·	2	21	·
II	3.5	7.4	5	8.0	1.2	4.8	7	5.7	11.5	4.4	17.5	4.9	16.5	6.3	11	8.4	·	5.9	37	15.2	16	10	16	28	·	9	1	3	9	13	8	·	1	28	·
III	6.5	8.3	13.5	4.1	10	2.3	22.5	3.5	6.5	2.5	6	2.7	5	4.0	11	3.8	12	3.3	39	–	–	11	13	29	·	3	1	4	11	11	9	1	1	31	·
IV	3.5	2.6	1.3	5.2	7.5	2.5	14	3.2	5.5	3.5	14	3.1	11	1.9	15.5	4.6	6	3.3	33	13.0	13	·	·	3	3	2	·	5	6	7	4	1	2	1	1
V	2.5	2.6	0.5	2.0	1.5	1.7	3.5	3.0	3.5	3.4	14.5	2.7	4.7	2.3	1.9	3.7	1	2.7	97	12.3	14,20	·	·	3	·	·	·	·	16	21	17	3	2	·	3
VI	8	8.5	0.5	8.0	·	·	·	·	·	·	6.5	2.5	56.5	2.7	14.5	3.5	4	3.3	78	16.0	3	·	·	·	1	2	·	4	9	11	10	3	1	·	2
VII	1	6.0	1.5	5.3	·	·	·	·	1	4.0	7	2.1	6.2	2.2	20.5	3.0	·	2.5	80	23.5	13	·	·	·	4	·	·	2	6	11	10	2	1	·	3
VIII	1	3.0	·	·	·	·	·	·	1.5	5.0	11.5	2.7	6.2	2.9	6	3.6	11	2.6	106	19.5	15	·	·	·	4	1	·	·	7	14	14	4	3	·	7
IX	0.5	2.0	2	1.0	1.5	2.7	1.5	1.3	1.5	4.0	1.5	2.9	5.0	2.7	7	3.6	11	2.4	69	25.0	18	·	·	·	·	1	·	3	9	12	9	2	2	·	3
X	·	·	·	·	·		0.5	4.0	1.5	2.0	10.5	2.4	33.5	2.6	6	3.2	4.1	1.5	12	5.6	28	·	·	6	·	·	·	4	12	4	3	·	8	·	·
XI	·	·	2.5	6.4	8	8.2	11	5.5	5.5	5.5	20	2.5	24.5	2.1	7.5	3.1	11	3.3	61	15.0	15	·	·	11	·	3	·	2	17	12	10	1	5	1	·
XII	11.5	4.4	3	4.7	·	·	·		2	3.5	11.5	4.8	4.1	2.6	18	2.4	6	3.0	15	4.2	14	11	16	28	·	1	·	4	20	12	4	·	2	17	·
Rok	3.9	4.4	4.6.5	4.2	4.4.5	2.2	6.3.5	2.4	4.7.5	3.5	17.6	3.1	14.3.4	3.1	14.1	4.1	10.3	3.2	66.3	25.0	18.IX	3.5	5.1	12.9	12	2.4	2	3.2	14.0	13.8	10.7	17	3.0	9.9	19

Kopna Góra $\varphi = 53°15'$ $\lambda = 23°29'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	08	-38	51	22	-239	31	-21	-02	-19	-15	50	53	50	51	90	86	89	88	06	09	06	07	88	77	83	83
II	–	–	–	–	-11	-80	34	13	-196	1	-54	-27	-45	-43	39	42	41	41	90	81	88	86	04	10	05	06	84	75	69	76
III	–	–	–	–	06	-96	65	31	-210	2	-77	-03	-42	-41	34	41	40	38	86	67	85	79	04	20	07	10	67	65	60	64
IV	–	–	–	–	146	39	268	23	-30	30	62	129	82	89	87	92	93	91	89	64	83	79	11	71	22	35	71	64	54	63
V	–	–	–	–	153	54	225	27	-32	4	91	137	94	104	104	103	109	105	87	65	90	81	15	59	12	29	70	79	60	70
VI	–	–	–	–	189	69	275	23	-02	3	124	171	119	133	116	114	119	116	79	59	85	74	32	89	23	48	62	66	45	58
VII	–	–	–	–	209	93	278	24,22	45	31	139	195	141	154	138	141	140	140	86	63	86	78	23	90	24	46	59	61	46	55
VIII	–	–	–	–	211	102	302	13	37	10	136	194	144	155	141	147	149	146	90	65	90	82	17	83	19	40	65	61	59	62
IX	–	–	–	–	165	68	263	5	-01	25	88	150	105	112	105	117	117	113	92	70	91	84	10	60	12	27	78	67	53	66
X	–	–	–	–	120	23	188	4	-55	16	46	111	61	70	81	97	90	89	94	73	94	87	05	38	07	17	83	56	44	61
XI	–	–	–	–	61	13	176	1	-29	18	25	50	33	35	72	75	73	73	95	84	91	90	04	17	08	10	90	82	80	84
XII	–	–	–	–	-29	-81	29	5,10	-215	21	-59	-42	-58	-54	40	41	40	40	90	84	90	88	03	07	04	05	79	72	74	75
Rok	–	–	–	–	102	14	302	13 VIII	-239	31 I	42	89	51	58	84	89	88	87	89	72	88	83	11	46	12	23	75	69	61	68

Drawno $\varphi = 53°13'$ $\lambda = 15°46'$

I	–	–	–	–	30	-10	79	22	-145	31	06	20	08	10	–	–	–	–	–	–	–	–	–	–	–	–	91	83	85	86
II	–	–	–	–	16	-30	66	8	-134	1	-10	07	-06	-04	–	–	–	–	–	–	–	–	–	–	–	–	94	78	72	81
III	–	–	–	–	30	-47	122	30	-105	13	-23	24	-13	-06	–	–	–	–	–	–	–	–	–	–	–	–	83	73	68	75
IV	–	–	–	–	139	38	268	25	-02	7	71	129	77	88	–	–	–	–	–	–	–	–	–	–	–	–	70	63	64	66
V	–	–	–	–	137	64	201	19	-07	1	91	124	96	102	–	–	–	–	–	–	–	–	–	–	–	–	88	78	85	84
VI	–	–	–	–	194	85	301	15	20	3	127	179	143	148	–	–	–	–	–	–	–	–	–	–	–	–	72	56	61	63
VII	–	–	–	–	202	107	275	26	64	10	135	190	146	154	–	–	–	–	–	–	–	–	–	–	–	–	78	72	77	76
VIII	–	–	–	–	197	116	285	12	75	10	131	184	154	156	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	168	80	250	4	34	25	100	157	118	123	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	123	48	215	2,3	-12	24	70	114	77	84	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	52	15	135	8	-24	25	28	47	29	34	–	–	–	–	–	–	–	–	–	–	–	–	94	84	88	89
XII	–	–	–	–	-16	-61	47	12	-184	22	-43	-24	-35	-34	–	–	–	–	–	–	–	–	–	–	–	–	83	75	79	79
Rok	–	–	–	–	106	34	301	15 VI	-184	22 XII	57	96	66	71	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Tykocin $\varphi = 53°12'$ $\lambda = 22°47'$

I	–	–	–	–	07	-33	60	22	-199	31	-16	-01	-14	-11	–	–	–	–	–	–	–	–	–	–	–	–	85	77	76	79
II	–	–	–	–	-12	-68	35	12	-167	1	-49	-26	-38	-38	–	–	–	–	–	–	–	–	–	–	–	–	83	76	72	77
III	–	–	–	–	01	-71	66	31	-154	2	-60	-12	-34	-35	–	–	–	–	–	–	–	–	–	–	–	–	69	62	62	64
IV	–	–	–	–	141	58	267	22	-06	30	69	129	89	94	–	–	–	–	–	–	–	–	–	–	–	–	73	64	48	62
V	–	–	–	–	149	68	205	20	-12	1	91	134	101	107	–	–	–	–	–	–	–	–	–	–	–	–	70	76	67	71
VI	–	–	–	–	190	95	275	23	50	7	127	172	133	141	–	–	–	–	–	–	–	–	–	–	–	–	61	70	51	61
VII	–	–	–	–	209	108	275	21	71	4	138	189	149	156	–	–	–	–	–	–	–	–	–	–	–	–	56	53	53	56
VIII	–	–	–	–	213	117	295	13	74	15	137	199	152	160	–	–	–	–	–	–	–	–	–	–	–	–	62	66	55	61
IX	–	–	–	–	165	78	265	5	18	25	90	151	111	116	–	–	–	–	–	–	–	–	–	–	–	–	57	65	49	57
X	–	–	–	–	119	39	188	4	-22	21	55	108	70	76	–	–	–	–	–	–	–	–	–	–	–	–	76	68	39	61
XI	–	–	–	–	59	13	160	1	-33	26,27	26	48	34	36	–	–	–	–	–	–	–	–	–	–	–	–	85	75	78	79
XII	–	–	–	–	-32	-73	30	5	-193	21	-56	-47	-55	-54	–	–	–	–	–	–	–	–	–	–	–	–	77	70	69	72
Rok	–	–	–	–	101	28	295	13 VIII	-199	31 I	46	87	58	62	–	–	–	–	–	–	–	–	–	–	–	–	71	69	60	67

Kończewice $\varphi = 53°11'$ $\lambda = 18°33'$

I	–	–	–	–	21	-24	86	22	-148	31	-09	05	-07	-04	–	–	–	–	–	–	–	–	–	–	–	–	84	74	81	80
II	–	–	–	–	02	-45	45	12	-135	1	-28	-07	-22	-20	–	–	–	–	–	–	–	–	–	–	–	–	86	80	72	79
III	–	–	–	–	15	-50	110	31	-127	9	-36	03	-19	-18	–	–	–	–	–	–	–	–	–	–	–	–	66	56	62	61
IV	–	–	–	–	145	48	277	23	-08	30	69	125	80	88	93	95	93	94	91	67	86	81	11	65	17	31	72	67	70	70
V	–	–	–	–	146	59	199	8	-44	1	86	127	95	101	102	100	105	102	90	69	88	82	12	50	15	26	76	79	81	79
VI	–	–	–	–	–	86	–	–	24	3	126	174	132	141	113	113	121	116	76	57	78	70	38	94	36	56	62	63	72	66
VII	–	–	–	–	204	103	283	26	61	29	135	191	141	152	140	134	137	137	90	61	85	79	17	93	26	45	68	62	75	68
VIII	–	–	–	–	204	116	279	12	76	10	140	188	148	156	146	144	144	145	91	67	85	81	15	77	26	39	69	78	65	71
IX	–	–	–	–	166	77	269	4	49	25	95	155	112	118	113	120	115	116	94	69	86	83	08	60	20	29	69	71	46	62
X	–	–	–	–	126	45	205	2,3	-08	21	58	116	77	82	92	106	98	99	96	76	91	88	04	36	10	17	70	65	53	63
XI	–	–	–	–	50	15	125	4	-36	17	25	39	31	32	70	74	72	72	93	90	92	92	05	09	06	07	86	87	79	84
XII	–	–	–	–	-28	-67	44	12	-194	22	-53	-38	-53	-49	–	–	–	–	–	–	–	–	–	–	–	–	87	78	74	80
Rok	–	–	–	–	–	30	–	–	-194	-22 XII	51	90	60	65	–	–	–	–	–	–	–	–	–	–	–	–	75	72	69	72

Kopna Góra $H_s = 160\,m$ $h_w = 15\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v>10	v>15	●	⊜	Opad R≥0.1	R≥1.0	R≥10.0	≡	⊠	⌒
I	4	5.5	1.5	2.0	1.5	3.3	2	3.0	26.5	2.9	39	3.8	7.5	3.6	4	2.5	7	3.2	31	5.6	25	3	8	25	·	·	·	2	22	19	9	·	2	25	·
II	11.5	6.5	4	5.5	9.5	4.5	2	5.0	19.5	4.3	12.5	5.1	1.5	6.3	9.5	5.2	14	4.2	50	9.2	12	11	15	28	·	5	·	·	12	20	13	·	1	28	·
III	9.5	3.9	9.5	6.1	15	2.7	12	4.6	9	2.6	6.5	3.3	5.5	2.0	7	4.1	19	3.0	49	6.5	16	11	12	29	·	2	·	6	14	16	11	·	3	31	·
IV	6.5	3.0	13	2.9	17	2.7	10	3.0	13	3.2	7	2.7	6	3.0	6.5	3.1	11	2.6	67	15.4	27	·	·	6	4	·	·	4	10	17	11	3	4	4	3
V	10.5	2.1	2.5	3.6	5.5	3.5	4	3.1	13.5	2.4	12	2.5	11.5	4.1	12.5	2.4	21	2.2	88	14.4	14	·	·	4	·	·	·	1	14	16	15	4	3	·	7
VI	18.5	4.2	4	5.4	1	2.5	1	2.5	9.5	3.1	20.5	3.5	17	3.1	6.5	3.5	12	3.1	80	42.6	4	·	·	1	3	1	·	1	6	15	9	2	·	·	3
VII	12.5	3.3	1.5	3.3	·	·	·	·	19	2.2	13.5	2.6	30	3.0	5.5	4.2	11	2.5	80	18.3	26	·	·	·	5	·	·	3	3	15	12	3	1	·	8
VIII	7	3.1	·	·	1	2.0	0.5	8.0	15.5	2.9	32.5	3.5	14	2.7	3.5	2.7	19	2.5	123	20.2	15	·	·	·	6	·	·	2	9	14	13	5	4	·	5
IX	6	2.5	4.5	2.3	4	2.4	3	3.0	16.5	3.0	19.5	3.8	16.5	3.7	3	1.7	17	2.6	98	21.3	18	·	·	4	1	·	·	2	10	17	14	3	6	·	1
X	5.5	1.9	2.5	3.6	1.5	1.7	9	2.7	14.5	2.2	15	4.5	12	3.7	3	1.5	30	1.9	7	3.0	19	·	·	9	·	·	·	2	13	7	3	·	12	·	·
XI	3	1.3	6	5.6	18.5	4.8	24.5	2.8	5	3.4	7.5	2.7	10.5	3.4	3	2.0	12	3.1	65	12.9	29	·	·	15	·	·	·	3	23	16	15	2	12	4	·
XII	14	3.0	9	3.6	2	3.0	6.5	2.9	16.5	3.9	18.5	3.5	8.5	3.1	1	2.0	17	2.8	22	6.4	14	12	17	29		·	·	4	21	14	7	·	2	21	·
Rok	108.5	3.4	58	3.7	76.5	2.8	74.5	3.4	178	3.0	204	3.5	140.5	3.5	65	2.9	190	2.8	766	42.6	4.VI	37	52	147	19	8	·	30	157	186	132	22	50	113	27

Drawno $H_s = 82\,m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	50	12.2	12	2	4	12	·	–	–	–	–	21	9	1	1	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	71	24.3	12	2	8	23	·	–	–	–	–	17	12	2	·	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	35	7.8	6	3	6	28	·	–	–	–	–	13	9	·	2	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	46	17.3	16	·	·	1	2	–	–	–	–	11	9	2	·	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	131	21.3	12	·	·	2	·	–	–	–	–	21	18	4	1	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	53	31.8	19	·	·	·	5	–	–	–	–	9	6	1	·	·	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	71	13.7	16	·	·	·	2	–	–	–	–	19	12	2	·	·	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	80	13.7	24	·	·	·	1	–	–	–	–	15	13	1	1	·	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	39	9.5	7	·	·	·	·	–	–	–	–	12	8	·	4	·	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	14	7.2	4	·	·	4	·	–	–	–	–	6	4	·	–	·	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	43	17.0	29	·	1	12	·	–	–	–	–	10	9	1	5	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	81	25.8	9	7	16	28	·	–	–	–	–	11	10	2	4	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	714	31.8	19.VI	14	35	110	10	–	–	–	–	165	119	16	–	–	–

Tykocin $H_s = 120\,m$ $h_w = 14\,m$

I	3.5	10.0	3.5	6.0	·		3.5	4.4	15	4.9	34.5	8.0	23.5	7.2	4.5	4.0	5	6.5	22	6.0	20	3	6	21	·	16	1	2	18	9	5	·	5	26	·
II	10	5.9	4.5	4.7	7	4.2	7.5	5.5	13	7.0	13	6.7	10.5	7.6	9.5	5.9	9	5.5	27	5.4	8	7	16	28	·	6	3	1	16	15	8	·	3	28	·
III	6.5	6.4	10	4.6	8	3.2	23	3.9	5	2.8	3.5	3.3	6.5	4.4	5.5	5.4	25	3.1	26	5.5	31	9	15	29	·	1	·	3	14	13	8	·	2	23	·
IV	7	2.9	7.5	5.0	8	3.1	17	4.0	11	3.0	10	3.3	3	4.2	9.5	4.1	17	3.0	45	13.5	13	·	·	1	3	1	·	2	9	14	8	1	1	1	2
V	6.5	2.5	5	2.4	3	2.3	11	3.3	4	3.1	9	3.1	17	3.5	14.5	3.8	23	2.4	110	–	–	·	·	1	·	·	·	·	13	20	18	2	1	·	7
VI	15	4.8	9	6.9	2	2.0	6.5	2.2	6	2.4	14	3.6	19	4.6	9.5	3.2	9	3.7	62	19.6	4	·	·	·	2	3	2	·	8	15	9	2	·	·	3
VII	11	2.1	6.5	2.5	1	2.0	4.5	2.1	13.5	2.5	11	3.8	25	3.5	6.5	3.6	14	2.6	55	15.3	23	·	·	·	4	·	·	·	5	13	10	2	·	·	7
VIII	4.5	4.2	2	1.8	1.5	1.0	9.5	2.0	11	3.9	21	4.4	27.5	4.5	5	3.3	11	3.4	91	16.3	15	·	·	·	5	·	·	1	6	14	14	3	2	·	6
IX	5	3.4	4	3.2	11	1.8	5.5	2.4	13	3.3	18	4.6	17	4.4	3.5	4.6	13	3.1	89	25.6	18	·	·	·	1	1	·	3	5	16	10	2	5	·	4
X	9.5	1.9	2.5	1.4	1.5	1.7	21	1.9	6	2.9	10	2.9	18	4.1	10.5	3.0	14	2.3	5	1.7	28	·	·	5	·	2	·	2	10	9	2	·	11	·	·
XI	4.5	1.0	2	4.7	14.5	5.6	30	4.4	6.5	1.8	4	4.4	11	2.1	4.5	1.7	13	3.2	47	11.6	15	·	·	10	·	3	·	3	22	16	12	1	9	2	·
XII	3.5	1.6	19.5	2.3	4.5	1.3	9	4.9	12	3.1	10.5	4.0	15	2.6	4	1.4	15	2.1	14	3.6	14	10	17	26	·	1	·	5	19	12	4	·	2	20	·
Rok	86.5	3.9	76	3.8	62	2.4	148	3.2	116	3.4	158.5	4.3	193	4.4	87	3.7	168	3.4	593	–	–	29	54	121	15	34	6	22	145	166	108	13	41	100	29

Kończewice $H_s = 94\,m$ $h_w = 12\,m$

I	4.5	3.2	4	3.5	2.5	4.0	2	1.5	10.5	3.8	32	4.3	19.5	4.4	8	4.5	10	3.6	24	8.7	25	3	6	19	·	1	1	·	18	9	7	·	–	–	–
II	5.5	6.9	12	3.0	6	1.8	1	1.0	7	3.1	10.5	7.0	18	5.8	13	6.8	11	4.5	15	4.0	12	2	10	25	·	6	2	·	14	12	5	·	–	–	–
III	15	3.6	11.5	2.8	3.5	2.9	14.5	4.7	6	2.2	25	1.8	4	5.2	8	3.6	28	2.0	23	7.7	6	3	10	30	·	1	1	1	10	10	5	·	–	–	–
IV	9	3.1	15	3.5	6	3.5	11.5	2.7	2.5	2.2	12.5	4.5	6	3.6	2.5	2.0	25	2.4	38	10.1	5	·	·	2	2	·	·	1	12	13	11	1	–	·	–
V	9	2.4	5	2.4	6	1.3	2	2.5	4.5	2.3	11	3.2	17.5	1.8	14	4.1	24	2.0	130	35.7	14	·	·	4	·	1	·	·	19	19	13	4	–	·	–
VI	17	6.2	2.5	5.8	·	·	1.5	1.0	5.5	4.7	4.5	4.0	19.5	4.8	18.5	4.0	21	3.5	59	21.3	29	·	·	·	–	4	2	3	5	11	9	2	–	·	–
VII	4.5	3.1	11.5	1.8	·	·	2	1.0	4	2.9	13	2.8	16.5	3.8	21.5	2.7	20	2.2	50	17.6	12	·	·	·	4	2	·	·	11	13	9	1	–	·	–
VIII	6	3.7	3.5	3.6	5.5	2.7	1.5	3.3	3	5.3	15.5	7.1	36.5	5.2	14.5	3.3	7	4.5	80	20.3	5	·	·	·	3	5	·	1	8	15	12	4	–	·	–
IX	2	2.5	6	3.0	9.5	3.3	3.5	4.4	4	4.4	14	6.1	27.5	6.4	13.5	4.9	10	4.6	76	32.1	18	·	·	·	1	7	·	1	9	11	10	3	–	·	–
X	9.5	3.2	8.5	2.2	5	2.5	16	3.9	9.5	4.7	9.5	5.2	22.5	5.3	8.5	4.6	4	4.0	27	11.2	31	·	·	4	·	1	·	2	8	6	6	1	–	·	–
XI	4	3.9	10	5.9	21.5	6.2	9.5	6.7	6.5	3.0	11.5	3.7	20.5	4.9	5.5	3.0	1	5.0	45	9.4	18	·	1	10	·	3	·	·	15	15	12	·	–	–	–
XII	3	5.3	18	3.6	6.5	3.5	5.5	3.3	8	4.4	15	7.1	20.5	5.7	7.5	4.9	9	4.5	12	3.5	16	12	17	27	·	3	·	2	20	11	5	·	–	–	–
Rok	89	3.9	107.5	3.4	72	2.4	70.5	2.8	71	3.3	151.5	4.7	228.5	4.7	135	4.0	170	3.6	579	35.7	14.V	20	44	121	–	34	6	11	157	145	104	16	–	–	–

Wyrzysk $\varphi = 53°09'$ $\lambda = 17°16'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PREŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{a.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.7	-1.5	9.2	22	-14.4	31	0.2	1.8	0.2	0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.2	7.9	7.8
II	–	–	–	–	1.2	-3.2	5.2	20	-15.0	1	-2.2	0.4	-1.1	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.7	6.3	7.6
III	–	–	–	–	2.7	-4.1	11.9	30	-9.1	14,16	-2.9	1.8	-1.6	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.2	4.9	5.3
IV	–	–	–	–	14.7	–	27.1	23	–	–	7.3	13.7	8.7	9.6	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.1	5.3	5.1
V	–	–	–	–	14.6	6.0	19.5	19	-1.5	1,3	8.8	13.6	8.8	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.7	5.4	6.1
VI	–	–	–	–	19.5	8.8	29.5	16	2.0	3	12.8	18.3	13.0	14.3	–	–	–	–	–	–	–	–	–	–	–	–	3.8	5.0	4.8	4.5
VII	–	–	–	–	21.0	10.0	29.7	26	6.6	29	14.0	19.8	13.8	15.4	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.4	4.5	4.9
VIII	–	–	–	–	20.6	11.7	28.1	12	7.1	10	14.1	19.6	14.4	15.6	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.3	4.8	5.8
IX	–	–	–	–	16.9	7.7	27.9	4	3.5	25	10.2	16.1	10.9	12.0	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.2	3.1	4.6
X	–	–	–	–	12.7	4.0	20.9	1,2	-2.5	16	6.5	12.0	7.5	8.4	–	–	–	–	–	–	–	–	–	–	–	–	7.3	5.8	5.7	6.3
XI	–	–	–	–	5.2	1.5	12.9	5	-2.5	18	2.4	4.5	3.2	3.4	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.2	8.1	8.3
XII	–	–	–	–	-1.9	-7.2	5.8	12	-19.1	22,24	-5.2	-3.4	-4.8	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.5	6.1	7.2
Rok	–	–	–	–	10.8	–	29.7	26.VII	-19.1	22,24.XII	5.5	9.8	6.1	6.9	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.3	5.6	6.1

Bydgoszcz, IMiUZ $\varphi = 53°08'$ $\lambda = 18°01'$

I	–	–	–	–	3.0	-1.5	9.7	22	-16.8	31	0.3	1.8	0.5	0.8	5.5	5.6	5.4	5.5	86	79	83	83	1.0	1.6	1.2	1.3	8.0	8.0	7.9	8.0
II	–	–	–	–	1.5	-3.5	5.9	12	-15.0	1	-2.3	0.1	-0.9	-1.0	4.5	4.9	4.7	4.7	86	77	80	81	0.8	1.4	1.1	1.1	8.8	8.9	8.0	8.6
III	–	–	–	–	2.7	-4.4	11.7	31	-10.3	15	-3.5	1.4	-0.9	-1.0	4.3	4.5	4.5	4.4	88	65	77	77	0.6	2.4	1.3	1.4	7.2	7.4	5.4	6.7
IV	–	–	–	–	15.3	5.4	28.0	23	0.1	1	7.1	13.1	9.9	10.0	8.6	8.8	9.2	8.9	83	59	74	72	1.9	7.7	3.7	4.4	7.6	8.0	5.5	7.0
V	–	–	–	–	14.7	6.6	20.2	19	-2.0	1	8.5	13.1	10.4	10.6	9.8	9.7	10.3	9.9	87	64	81	77	1.5	5.8	2.5	3.3	7.3	8.6	7.3	7.7
VI	–	–	–	–	19.9	9.7	29.7	16	3.5	3	12.9	17.9	14.9	15.2	10.9	10.6	11.6	11.0	72	52	67	64	4.4	10.8	5.9	7.0	5.9	6.7	6.2	6.3
VII	–	–	–	–	21.1	11.2	30.3	26	7.5	4	13.6	19.3	15.7	16.1	13.4	12.5	13.3	13.1	86	57	75	73	2.3	10.6	4.9	5.9	6.8	7.2	5.9	6.6
VIII	–	–	–	–	20.9	12.6	28.7	12	7.6	10	14.2	19.4	15.9	16.3	14.1	13.6	14.6	14.1	86	61	80	76	2.2	9.3	3.6	5.0	6.6	8.3	6.0	7.0
IX	–	–	–	–	17.2	8.3	29.0	4	4.1	24	9.7	15.9	11.7	12.2	11.1	11.7	11.8	11.5	92	66	85	81	1.1	6.8	2.3	3.4	6.9	7.0	4.0	6.0
X	–	–	–	–	13.1	5.3	21.6	2	-1.6	16	6.2	12.1	8.2	8.6	9.1	10.2	9.9	9.7	93	72	89	85	0.7	4.3	1.3	2.1	8.3	6.5	4.5	6.4
XI	–	–	–	–	5.6	2.1	13.3	4	-2.1	18	3.0	4.8	3.8	3.8	6.9	7.4	7.2	7.2	90	85	88	88	0.8	1.5	1.0	1.1	8.5	8.3	8.0	8.3
XII	–	–	–	–	-1.6	-6.2	6.2	12	-18.1	21	-4.8	-3.0	-4.2	-4.0	4.2	4.6	4.3	4.4	90	85	87	87	0.4	0.8	0.6	0.6	8.3	7.8	8.1	8.1
Rok	–	–	–	–	11.1	3.8	30.3	26.VII	-18.1	21.XII	5.4	9.7	7.1	7.3	8.5	8.7	8.9	8.7	87	68	80	78	1.5	5.2	2.4	3.0	7.5	7.7	6.4	7.2

Bydgoszcz $\varphi = 53°07'$ $\lambda = 17°58'$

I	1005.3	1032.3	978.2	1014.2	2.6	-2.0	9.5	22	-17.5	31	-0.2	1.7	0.1	0.4	5.5	5.7	5.5	5.6	88	81	85	85	0.8	1.4	1.0	1.1	7.8	8.2	7.8	7.9
II	1006.3	1029.0	971.0	1015.3	1.1	-4.3	5.3	12	-16.2	1	-2.6	0.0	-1.4	-1.4	4.4	5.0	4.8	4.7	85	80	85	83	0.8	1.3	0.8	1.0	8.8	8.5	7.4	8.2
III	1002.8	1019.1	977.2	1011.8	2.4	-5.5	11.4	31	-11.7	9	-3.7	1.5	-1.7	-1.4	4.3	4.9	4.5	4.6	89	71	81	80	0.5	2.0	1.0	1.2	6.5	7.1	5.4	6.3
IV	1004.9	1019.6	978.5	1013.5	15.2	4.6	28.4	23	-1.2	1	7.1	13.2	9.0	9.6	8.9	9.0	9.1	9.0	86	61	77	75	1.6	7.6	3.1	4.1	6.7	7.6	6.3	6.9
V	1003.7	1011.2	989.8	1012.3	14.9	5.2	20.3	19	-4.5	1	8.5	13.2	9.5	10.2	10.1	10.1	10.3	10.2	89	67	86	81	1.3	5.4	1.8	2.8	7.3	8.5	7.0	7.6
VI	1009.2	1021.4	997.0	1017.7	19.9	8.3	30.8	16	1.5	3	12.7	17.9	13.9	14.6	11.2	11.4	11.8	11.5	75	55	72	67	3.9	10.1	4.6	6.2	5.7	6.8	6.2	6.2
VII	1005.4	1016.3	988.6	1013.8	21.1	9.8	30.6	26	5.0	25	13.6	19.5	14.9	15.7	13.9	13.5	13.6	13.7	89	61	81	77	1.8	9.9	3.6	5.1	6.7	7.2	5.5	6.5
VIII	1005.8	1014.7	993.7	1014.0	21.0	11.4	29.4	12	5.5	10	14.3	19.4	14.9	15.9	14.3	14.3	14.5	14.4	87	64	85	79	2.1	8.6	2.7	4.5	6.5	8.1	6.5	7.0
IX	1006.7	1021.4	986.5	1015.2	17.2	7.4	29.5	4	3.7	25	9.6	15.9	11.0	11.9	11.2	12.0	11.5	11.6	92	67	87	82	1.0	6.7	1.9	3.2	7.2	7.2	4.3	6.2
X	1013.1	1027.8	1000.7	1021.8	13.0	3.8	21.7	3	-4.0	16	5.7	12.1	7.2	8.0	9.0	10.5	9.5	9.7	95	73	91	86	0.5	4.1	1.1	1.9	7.2	6.9	5.0	6.4
XI	1008.4	1024.9	988.4	1017.2	5.3	1.7	13.2	4,5	-2.8	21	2.6	4.6	3.5	3.6	7.0	7.4	7.3	7.2	93	87	91	90	0.6	1.3	0.8	0.9	8.9	8.5	8.1	8.5
XII	1007.6	1039.4	964.3	1016.7	-2.1	-7.0	5.9	12	-18.7	21	-5.1	-3.3	-4.6	-4.4	4.1	4.4	4.1	4.2	89	86	86	87	0.4	0.7	0.6	0.6	8.2	7.9	7.4	7.8
Rok	1006.6	1039.4	964.3	1015.3	11.0	2.8	30.8	16.VI	-18.7	21.XII	5.2	9.6	6.4	6.9	8.7	9.0	8.9	8.9	88	71	84	81	1.3	4.9	1.9	2.7	7.3	7.7	6.4	7.1

MŁawa $\varphi = 53°07'$ $\lambda = 20°22'$

I	996.0	1022.7	969.9	1014.4	1.1	-3.5	8.0	22	-20.1	31	-1.5	0.1	-1.4	-1.0	5.2	5.3	5.0	5.2	90	83	86	86	0.5	1.1	0.8	0.8	8.5	8.3	7.5	8.1
II	996.0	1018.2	959.5	1014.6	-0.3	-6.4	3.7	12	-17.9	1	-4.4	-1.7	-3.3	-3.2	4.0	4.4	4.1	4.2	85	81	82	83	0.6	1.0	0.9	0.8	9.2	8.6	7.0	8.3
III	993.3	1010.3	970.4	1011.7	1.3	-6.0	9.3	31	-16.7	15	-4.8	-0.1	-2.7	-2.6	3.9	4.5	4.2	4.2	84	72	80	79	0.7	1.7	0.9	1.1	7.7	7.5	5.4	6.9
IV	995.9	1011.6	970.7	1013.5	15.3	5.1	28.0	23	-1.4	30	6.7	13.6	8.8	9.5	8.9	9.6	9.8	9.4	88	61	83	77	1.3	7.7	2.2	3.7	7.4	7.3	5.0	6.6
V	994.4	1002.3	972.3	1012.0	14.9	6.0	19.9	8	-2.2	1	8.9	13.0	9.9	10.4	10.2	9.8	10.7	10.2	87	65	85	79	1.4	5.6	1.8	2.9	7.9	8.7	6.6	7.7
VI	999.5	1010.8	987.5	1016.9	19.4	9.0	29.0	16	3.0	3	12.8	17.8	13.6	14.4	12.1	11.9	12.7	12.2	80	57	80	72	3.1	9.4	3.4	5.3	6.7	7.2	6.5	6.8
VII	996.3	1006.7	981.7	1013.5	21.0	10.5	29.0	26	6.1	30	13.8	19.4	14.8	15.7	13.7	13.4	14.0	13.7	86	60	82	76	2.3	9.7	3.2	5.1	7.2	7.4	6.3	7.0
VIII	996.9	1005.9	987.3	1014.1	20.9	11.2	28.5	7	6.6	10	13.9	19.2	15.0	15.8	14.5	15.2	15.3	15.0	90	68	89	82	1.6	7.6	2.0	3.7	7.2	8.0	5.5	6.9
IX	997.7	1013.6	978.8	1015.2	16.5	7.7	26.7	4	3.5	15,25	9.4	15.2	10.8	11.6	11.2	12.3	12.1	11.9	95	72	92	86	0.7	5.4	1.1	2.4	6.8	7.9	4.8	6.5
X	1004.1	1019.1	990.4	1022.0	12.7	3.6	20.4	2	-4.2	16	5.2	11.6	6.8	7.6	8.8	10.8	9.5	9.7	97	78	93	89	0.3	3.2	0.7	1.4	7.5	6.6	5.3	6.5
XI	999.9	1015.1	981.5	1018.0	5.2	1.1	12.7	4	-5.8	26	2.2	4.3	3.1	3.2	6.8	7.1	6.9	6.9	92	84	88	88	0.6	1.4	1.0	1.0	8.4	8.7	7.8	8.5
XII	998.0	1029.2	956.9	1016.8	-2.7	-7.6	3.2	10,12	-20.4	21	-5.4	-4.1	-5.4	-5.1	3.9	4.2	3.9	4.0	86	83	85	85	0.5	0.7	0.6	0.6	7.8	8.4	6.8	7.7
Rok	997.3	1029.2	956.9	1015.2	10.4	2.6	29.0	16.VI,26.VII	-20.4	21.XII	4.7	9.0	5.8	6.3	8.6	9.0	9.0	8.9	88	72	85	82	1.1	4.5	1.6	2.4	7.7	7.9	6.2	7.3

Wyrzysk $H_s = 90 m$ $h_w = 12 m$ 1962

MIESIĄC	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	≥ 10	≥ 15	◉	●	≥ 0.1	≥ 1.0	≥ 10.0	═	⊠	R
	ROZKŁAD WIATRU nD, vmD																		OPAD R			LICZBA DNI (n) Temperatura T				Wiatr v				Opad R					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n																		
I	4	5.5	1	7.0	2	6.0	5	4.2	7	5.3	34	5.4	23	3.3	11	2.6	6	4.0	40	10.0	25	2	4	18	·	4	·	2	17	15	11	1	3	–	·
II	11	6.4	6	6.3	11	5.0	4	4.5	3	2.7	8	5.5	19	7.0	16	6.6	6	5.5	41	13.0	12	2	9	23	·	8	2	·	14	13	9	1	3	–	
III	15	3.3	6	4.0	6	1.8	5	5.0	18	3.4	4	2.0	4	3.5	6	3.0	29	2.3	33	10.0	12	·	5	28	·	2	·	9	10	11	8	1	2	–	
IV	17	3.0	7	4.7	6	5.5	1	1.0	17	2.6	11	5.0	10	3.6	6	3.5	15	3.0	54	14.0	16	·	·	·	2	2	·	8	9	10	10	2	·	–	1
V	12	2.0	1	5.0	2	1.5	1	3.0	16	2.8	6	4.2	17	2.8	18	3.7	20	2.4	104	22.0	14	·	·	3	·	·	·	3	8	21	20	3	·	·	5
VI	15	6.3	1	2.0					5	2.4	6	3.7	18	3.1	25	3.6	20	3.1	68	22.0	16	·	·	·	5	4	·	4	1	9	8	3	·	·	3
VII	8	2.1		·	8	2.4	1	2.0	7	2.4	11	3.5	22	2.5	11	3.2	25	2.0	53	9.0	8	·	·	·	5	·	·	8	5	13	11	·	·	·	3
VIII	8	1.4	1	2.0	1	2.0	2	3.0	3	3.3	15	4.0	28	3.4	17	4.8	18	2.9	97	34.5	7	·	·	·	2	2	·	4	7	15	15	2	·	·	3
IX	6	2.0		·	6.5	2.6	0.5	2.0	8	3.1	6	4.0	19	3.2	14	3.5	30	2.1	66	19.4	18	·	·	·	1	·	·	6	6	15	11	2	3	·	2
X	11	2.5	·	·	0.5	2.0	1.5	1.3	8	2.4	6	2.8	20	3.0	4	6.0	42	1.6	47	10.0	31	·	·	7	·	·	·	5	14	7	5	1	10	·	
XI	2	2.5		·	19	4.2	13	4.5	8.5	1.7	7.5	2.3	12	3.1	4	3.0	24	2.5	32	9.0	1	·	·	11	·		·	1	22	11	8	·	8	–	
XII	7	2.0	1	3.0	8	2.8	6	1.6	4	2.1	15.5	4.0	10.5	3.0	4	2.2	37	1.7	39	9.0	11	10	18	27	·		·	3	17	11	9	·	1	–	·
Rok	116	3.2	24	2.8	70	3.0	40	2.2	104.5	2.8	130	3.9	202.5	3.5	136	3.8	272	2.8	644	34.5	7.VIII	14	36	117	15	22	2	53	130	151	125	16	30	–	17

Bydgoszcz, IMiUZ $H_s = 47 m$ $h_w = 10 m$

I	7.5	1.9	4.5	2.1	1	1.0	3.5	2.0	17.5	2.5	30	3.7	18.5	2.9	3.5	3.1	7	2.7	29	12.4	25	3	4	17	·			1	19	16	6	1	6	4	·
II	8	3.3	11	3.3	8	2.5	1	2.0	9	3.0	6	2.7	19.5	5.0	6.5	6.0	15	3.2	28	7.5	12	2	9	22	·	1	·	·	19	16	5	·	5	14	·
III	4.5	2.9	15	2.7	8.5	2.6	9	2.3	8.5	2.4	3.5	3.7	8	2.4	5	3.6	31	1.8	27	12.4	6	1	5	27	·		·	4	15	12	5	1	9	16	·
IV	5	2.4	15	2.5	6	2.8	4.5	4.1	9.5	3.1	9.5	2.9	11.5	2.6	3	3.3	26	2.0	28	5.9	5	·	·	·	4	·	·	1	11	14	7	·	3	·	1
V	0.5	3.0	3	2.2	4.5	2.2	1	5.0	12	2.2	14.5	2.0	21	2.4	6.5	3.5	30	1.6	113	29.3	14	·	·	3	·	·	·		16	20	17	2	2	·	7
VI	12	3.8	3	3.0	·		5	2.2	4	2.5	15	3.4	21	2.7	6	2.2	24	2.2	76	16.3	19	·	·	·	6	1	·	2	12	14	13	2	·		3
VII	1.5	1.3	5.5	1.6	2	2.0	·	·	10.5	2.8	15	2.3	25.5	2.1	2	2.0	31	1.5	41	15.1	12	·	·	·	5	·	·	·	9	13	11	1	·	·	5
VIII	1.5	1.3	1	2.0	4	1.8	2.5	2.6	8	2.9	25	3.4	22	2.9	3	2.2	26	2.1	80	17.5	5	·	·	·	3	·	·	2	12	15	11	3	1	·	6
IX			2	1.5	7	1.6	2	3.5	7	3.0	16	2.9	24	3.1	2	1.5	30	1.8	52	23.5	18	·	·	·	1	1	·	3	7	12	9	2	2	·	1
X	1	1.0	1	2.0	5.5	1.5	4.5	2.1	6.5	1.7	14.5	1.7	15.5	2.8	3.5	4.0	41	1.2	29	10.2	5	·	·	2	·	·	·	3	11	7	5	1	12	·	1
XI	3	2.0	7	3.3	24.5	3.0	6.5	2.7	9	1.4	12	2.6	10	2.6			18	2.1	47	16.9	1	·	·	7	·	·	·	1	20	13	8	1	8	·	·
XII	4	1.8	8	2.2	5	2.2	3	2.0	5.5	2.5	20.5	3.0	16	2.4	3	2.7	28	1.7	17	4.8	16	10	17	25	·	1	1	4	22	13	5	·	8	16	
Rok	48.5	2.1	76	2.4	76	1.9	42.5	2.5	107	2.5	181.5	2.9	212.5	2.8	44	2.8	307	2.0	567	29.3	14.V	16	35	103	19	4	1	21	173	165	102	14	56	50	24

Bydgoszcz $H_s = 70 m$ $H_b = 70,5 m$ $h_w = 16 m$

I	3	5.7	6.5	4.2			4.5	3.2	7	5.2	29.5	5.7	28	5.7	13.5	4.6	1	5.2	27	11.8	25	3	4	19	·	6	·	1	17	12	8	1	3	8	
II	10	7.9	5	7.4	13.5	5.1	1.5	4.7	7.5	4.4	14.5	7.1	15.5	5.5	14.5	7.1	2	6.1	35	8.8	12	2	10	23	·	9	4		18	15	5	·	3	18	·
III	8	4.6	15	4.3	6	3.8	11	3.4	16	3.6	10	3.9	3.5	2.4	11.5	4.0	12	3.4	25	7.4	12	6	7	29	·	3	·	4	14	13	4		4	20	
IV	7.5	4.7	11	4.3	5.5	4.8	5	2.5	10.5	5.8	12.5	5.0	13.5	3.9	8.5	4.3	16	3.7	34	7.6	5	·	·	7	3	5		2	12	13	7	·	2		1
V	8	3.4	6.5	3.4	0.5	1.0	4.5	2.3	7.5	4.0	16.5	4.2	14	3.4	25.5	3.2	10	3.1	114	26.0	14			4	·	·	·	·	14	24	13	3	2	·	6
VI	14.5	4.0	8.5	7.1			1.5	3.0	4	4.4	12	3.5	24	4.7	19.5	4.4	6	4.2	82	15.9	29		·		6	3	·	1	7	14	13	3	2	·	5
VII	9.5	2.6	7.5	3.3	4	2.5	2.5	2.2	4	2.5	13.5	4.0	19	3.6	27	2.7	6	2.9	48	12.2	12		·	·	5	2	1	·	8	14	12	1	3	·	4
VIII	4	2.9	·		2.5	2.0	3.5	2.9	3.5	2.7	11.5	4.8	40	4.7	16	4.2	12	3.7	76	19.4	15			·	3	5	1	1	10	16	11	2	·	·	4
IX	2	3.2	1	2.0	5	3.0	9	2.9	3	3.2	10	5.6	25.5	4.2	19.5	4.4	15	3.4	56	23.8	18	·			1	5	·	3	8	13	10	2	4	·	1
X	7.5	2.7	4.5	2.1	2	1.2	7	1.9	15	3.0	10	3.2	17	3.8	8	3.4	22	2.3	21	7.0	31		·	6	·	·		4	11	8	5	·	16	·	1
XI	2.5	4.0	2	4.0	19.5	5.0	13.5	5.3	8	3.8	11	3.2	18	3.2	1.5	4.3	14	3.5	52	15.7	1			11	·		·	1	21	14	10	1	9	2	
XII	1.5	4.3	13	3.5	12	3.1	5	1.7	11	2.0	17.5	5.0	18.5	3.3	7.5	2.7	7	3.1	20	5.5	16	11	17	27	·	4		4	19	12	5	·	5	17	·
Rok	78	4.2	80.5	3.8	70.5	2.6	68.5	3.0	97	3.7	168.5	4.6	236.5	4.0	172.5	4.1	123	3.7	590	26.0	14.V	22	38	126	18	42	6	21	159	168	108	13	53	65	22

UWAGA. Kierunki i prędkości wiatru – wg anemometru.

Mława $H_s = 141 m$ $H_b = 145,8 m$ $h_w = 13 m$

I	4.5	5.0	7	2.4	2	2.0	3	1.7	24	2.2	33.5	3.7	11.5	3.1	3.5	2.4	4	2.9	31	9.4	25	4	6	22	·	1	·	1	20	15	6	·	8	21	:
II	9	5.1	8.5	4.4	9.5	3.8	6.5	1.8	6.5	2.7	16	4.4	15	5.8	9	5.1	4	4.2	46	16.1	16	6	14	26	·	5	3	·	19	16	9	2	6	28	·
III	11.5	4.7	11	2.4	16	2.6	21	2.5	5.5	1.5	3	1.8	6.5	3.4	9.5	4.2	9	2.7	41	13.7	5	5	9	29	·	1		1	12	12	9	1	2	30	
IV	14	3.0	13.5	3.1	10.5	3.2	9	2.5	10.5	2.4	14.5	2.3	4	2.5	9	4.7	5	2.8	23	7.2	13	·	·	3	4	·	·	3	10	12	7	·	2	·	1
V	9.5	1.7	7.5	2.1	10.5	1.9	11	2.1	6	1.8	10.5	3.0	15.5	2.8	18.5	2.9	4	2.3	109	30.8	14	·	·	4	·	·		·	17	23	16	2	2	·	ε
VI	15	5.1	3	1.3	1	4.0	5	1.8	4	1.8	23.5	3.5	13	3.1	18.5	2.8	7	3.1	77	28.9	29	·	·	·	4	·		1	9	14	11	2	·	·	3
VII	15.5	2.2	6	2.2			5	1.5	6.5	2.5	18	2.5	19.5	2.8	18.5	2.7	4	2.4	46	13.5	26	·	·	·	4	·	·	·	10	15	8	2	·	·	3
VIII	7	2.1	1.5	1.7	3.5	2.4	2.5	3.4	5	3.4	27.5	3.7	20.5	3.2	11.5	2.1	14	2.6	100	27.7	5	·	·	·	5	·	·	2	13	16	15	2	·	·	6
IX	5.5	2.5	7.5	2.0	7	2.4	3.5	2.1	6	2.4	18	3.6	18.5	2.9	7	3.4	17	2.3	70	23.3	18	·	·	·	1	·	·	2	13	18	10	1	2	·	3
X	8	1.2	3	1.3	16.5	1.4	11	1.6	8.5	1.1	11.5	2.1	11	2.6	8.5	2.8	15	1.5	12	4.0	28	·	·	6	·	·	·	1	12	10	5	·	5	·	·
XI	2	2.0	11.5	4.0	28.5	3.6	9.5	2.7	9.5	1.4	13	2.9	7	2.4	3	1.7	6	2.8	51	10.6	20	·	1	10	·	·	·	2	20	14	11	1	8	4	·
XII	10.5	3.0	16	2.9	5.5	2.3	10.5	2.0	12.5	2.8	15	3.3	11	2.3	7	1.4	5	2.5	18	3.3	11	9	17	28	·	·	·	3	19	13	6	·	4	17	
Rok	112	3.1	96	2.5	110.5	2.5	97.5	2.1	104.5	2.2	204	3.1	153	3.1	123.5	3.0	94	2.7	624	30.8	14.V	24	47	128	18	7	3	16	174	178	113	13	39	100	22

Białystok $\varphi = 53°07'$ $\lambda = 23°11'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0,m}$	$\overline{\text{Max}}$	$\overline{\text{Min}}$	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	997.0	1023.9	973.3	1014.8	0.7	-3.9	5.5	22	-21.3	31	-2.1	-0.2	-1.9	-1.6	5.0	5.4	5.0	5.1	91	87	89	89	0.5	0.9	0.6	0.7	8.8	8.0	8.1	8.3
II	996.5	1017.4	958.0	1014.5	-1.2	-7.5	4.0	17	-19.8	1	-5.2	-2.5	-4.3	-4.1	4.0	4.4	4.1	4.2	92	84	89	88	0.4	0.8	0.5	0.6	8.9	8.2	7.9	8.3
III	994.2	1012.1	971.7	1012.2	0.5	-8.2	6.2	31	-18.1	2	-6.6	-0.5	-3.9	-3.7	3.7	4.8	4.3	4.3	93	79	90	87	0.3	1.2	0.4	0.6	6.6	6.3	6.2	6.4
IV	997.2	1013.6	975.4	1014.3	14.8	4.8	27.4	22	-1.2	8	6.7	13.5	8.7	9.4	9.3	9.7	10.0	9.7	92	65	86	81	0.9	7.2	1.8	3.3	7.2	6.8	4.9	6.3
V	995.1	1003.5	974.7	1012.1	15.4	6.6	22.2	27	-1.8	1	9.2	13.7	10.0	10.7	10.7	10.5	11.0	10.7	90	67	88	82	1.2	5.8	1.6	2.9	7.9	8.4	7.1	7.8
VI	999.6	1009.9	987.6	1016.5	19.3	8.5	28.3	23	1.9	3	12.7	17.3	12.8	13.9	11.8	11.6	12.1	11.8	79	60	81	73	3.3	9.0	3.0	5.1	6.0	7.6	5.6	6.4
VII	996.3	1006.4	983.3	1013.0	21.1	10.3	28.3	26	6.0	4	14.0	19.4	14.9	15.8	13.7	13.7	14.0	13.8	86	61	83	77	2.4	9.3	3.1	4.9	6.8	7.8	6.9	7.2
VIII	997.7	1007.9	987.0	1014.4	21.2	11.4	29.2	13	5.4	27	13.7	19.5	15.2	15.9	14.1	14.5	14.7	14.4	89	64	85	79	1.8	8.8	2.9	4.5	6.9	7.6	5.8	6.8
IX	998.3	1015.6	980.4	1015.3	16.6	7.3	26.4	5	0.8	25	8.7	15.1	10.8	11.4	10.5	12.0	11.8	11.4	93	70	90	84	0.9	5.6	1.4	2.6	7.0	8.0	6.2	7.1
X	1005.1	1019.7	987.3	1022.4	12.1	3.2	20.0	2	-3.4	16	4.8	11.0	6.5	7.2	8.5	10.1	9.1	9.2	96	76	93	88	0.3	3.4	0.7	1.5	8.9	8.0	4.6	7.2
XI	1002.1	1015.3	985.4	1019.3	6.1	1.6	16.3	1	-2.7	27	2.7	5.0	3.4	3.6	7.3	7.6	7.3	7.4	95	86	91	91	0.3	1.5	0.7	0.8	8.9	8.4	8.8	8.7
XII	999.0	1030.4	960.3	1017.2	-2.9	-7.7	2.9	10	-21.6	21	-5.8	-4.3	-5.7	-5.4	4.1	4.3	4.0	4.1	93	89	91	91	0.3	0.5	0.4	0.4	8.5	7.9	7.2	7.9
Rok	998.2	1030.4	958.0	1015.6	10.3	2.2	29.2	13.VIII	-21.6	21.XII	4.4	8.9	5.5	6.1	8.6	9.0	9.0	8.9	91	74	88	84	1.0	4.5	1.4	2.3	7.7	7.8	6.6	7.4

Przelewice $\varphi = 53°06'$ $\lambda = 15°05'$

I	-	-	-	-	3.4	-0.8	8.4	22	-14.2	31	0.5	2.3	1.0	1.2	-	-	-	-	-	-	-	-	-	-	-	-	7.9	8.4	7.6	8.0
II	-	-	-	-	2.4	-2.6	7.8	19	-11.8	1	-1.1	1.4	-0.4	-0.1	-	-	-	-	-	-	-	-	-	-	-	-	8.4	7.3	7.0	7.6
III	-	-	-	-	3.5	-3.6	13.3	30	-8.9	16	-2.0	2.6	-0.5	-0.1	-	-	-	-	-	-	-	-	-	-	-	-	6.2	7.2	6.0	6.5
IV	-	-	-	-	14.2	4.3	27.0	25	-0.3	30	6.1	12.7	7.8	8.6	-	-	-	-	-	-	-	-	-	-	-	-	6.8	6.8	4.4	6.0
V	-	-	-	-	14.3	6.5	20.3	7,19	0.1	2	8.8	12.8	9.4	10.1	-	-	-	-	-	-	-	-	-	-	-	-	7.5	8.2	7.5	7.7
VI	-	-	-	-	19.5	8.9	29.2	15	1.3	6	12.7	17.9	13.1	14.2	-	-	-	-	-	-	-	-	-	-	-	-	5.4	7.0	6.5	6.3
VII	-	-	-	-	20.2	10.5	26.1	26	6.9	29	13.7	18.5	13.6	14.8	-	-	-	-	-	-	-	-	-	-	-	-	7.3	6.5	6.1	6.6
VIII	-	-	-	-	19.9	11.5	28.7	12	8.5	9	13.7	18.2	14.5	15.2	-	-	-	-	-	-	-	-	-	-	-	-	7.9	8.6	6.8	7.8
IX	-	-	-	-	17.0	7.6	25.4	4	4.8	25	10.0	15.7	11.0	11.9	-	-	-	-	-	-	-	-	-	-	-	-	7.2	7.1	4.7	6.3
X	-	-	-	-	12.6	5.2	22.7	3	-0.3	28	6.7	11.7	8.1	8.6	-	-	-	-	-	-	-	-	-	-	-	-	7.9	7.1	5.4	6.8
XI	-	-	-	-	5.2	0.9	13.7	8	-5.3	24	2.4	4.5	2.7	3.1	-	-	-	-	-	-	-	-	-	-	-	-	8.9	8.5	6.5	8.0
XII	-	-	-	-	-1.2	-5.8	5.9	12	-16.6	22	-4.1	-2.3	-3.8	-3.5	-	-	-	-	-	-	-	-	-	-	-	-	7.8	8.1	6.5	7.5
Rok	-	-	-	-	10.9	3.6	29.2	15.VI	-16.6	22.XII	5.6	9.7	6.4	7.0	-	-	-	-	-	-	-	-	-	-	-	-	7.4	7.6	6.2	7.1

Ostrołęka $\varphi = 53°05'$ $\lambda = 21°34'$

I	1001.8	1029.0	977.0	1013.7	1.3	-3.0	8.7	22	-20.7	31	-1.2	0.6	-1.1	-0.7	5.1	5.5	5.1	5.2	87	82	87	85	0.7	1.2	0.8	0.9	7.6	8.0	8.1	7.9
II	1001.7	1023.8	963.8	1014.0	-0.5	-6.6	3.1	7,12	-17.0	1	-4.7	-1.9	-3.4	-3.4	4.0	4.3	4.2	4.2	87	80	85	84	0.6	1.1	0.7	0.8	8.6	8.3	7.1	8.0
III	999.1	1017.2	977.2	1011.3	1.0	-6.7	8.6	31	-19.4	2	-5.5	-0.1	-2.7	-2.8	3.8	4.3	4.1	4.1	88	69	80	79	0.5	1.9	1.0	1.1	7.2	7.0	5.4	6.5
IV	1001.6	1017.9	977.8	1013.3	15.4	5.6	27.9	22	-0.6	30	7.3	13.8	9.3	9.9	9.3	9.6	9.8	9.6	89	61	81	77	1.3	7.7	2.6	3.9	7.2	7.0	3.9	6.0
V	999.9	1008.2	977.8	1011.6	15.2	6.5	20.9	28	-2.3	1	9.0	13.7	10.4	10.9	10.3	10.3	11.0	10.5	89	66	86	80	1.3	5.7	1.9	3.0	7.1	8.4	7.5	7.7
VI	1004.7	1015.8	992.5	1016.2	19.7	9.2	28.1	16	4.0	10	12.8	17.9	13.6	14.5	11.9	11.6	12.1	11.9	79	57	76	71	3.2	9.6	3.9	5.6	6.7	7.4	5.2	6.4
VII	1004.4	1014.7	987.5	1012.9	21.4	10.6	28.9	26	6.2	30	14.0	19.9	15.2	16.1	13.9	13.8	14.2	14.0	87	60	81	76	2.2	9.9	3.3	5.1	6.5	7.2	5.6	6.4
VIII	1002.2	1011.9	991.9	1013.7	21.4	11.5	29.8	13	6.5	10	13.9	19.9	15.3	16.1	14.3	14.9	15.1	14.8	89	64	86	80	1.7	9.0	2.5	4.4	7.2	7.6	5.3	6.7
IX	1003.1	1019.6	984.5	1014.7	16.7	7.8	26.5	4	2.3	15	9.4	15.5	11.1	11.8	11.0	12.1	12.0	11.7	93	69	90	84	0.9	5.9	1.4	2.7	6.5	7.3	5.2	6.3
X	1009.7	1024.7	994.4	1021.6	12.8	3.7	21.5	2	-2.8	16	5.2	11.9	7.0	7.8	8.7	10.5	9.5	9.6	96	75	93	88	0.4	3.9	0.8	1.7	7.1	7.0	4.9	6.3
XI	1006.1	1020.2	989.0	1018.1	5.9	1.7	13.8	1	-2.9	26	2.8	4.8	3.5	3.6	7.1	7.3	7.1	7.2	93	83	88	88	0.5	1.6	1.0	1.0	9.1	8.6	9.1	8.9
XII	1003.9	1035.3	963.2	1016.2	-2.5	-7.1	3.7	5	-19.3	21	-5.4	-3.9	-5.1	-4.9	4.1	4.3	4.0	4.1	90	86	88	88	0.4	0.6	0.6	0.5	7.1	8.0	7.1	7.4
Rok	1002.9	1035.3	963.2	1014.8	10.6	2.8	29.8	13.VIII	-20.7	31.I	4.8	9.3	6.1	6.6	8.6	9.0	9.0	8.9	89	71	85	82	1.1	4.8	1.7	2.5	7.3	7.6	6.2	7.0

UWAGA Ciśnienie powietrza jest za niskie przeciętnie o około 0,5 mb.

Toruń-Wrzosy $\varphi = 53°03'$ $\lambda = 18°35'$

I	1005.7	1033.1	978.4	1014.6	2.5	-1.8	9.3	22	-17.6	31	0.0	1.7	0.1	0.5	5.4	5.6	5.3	5.4	85	79	83	82	0.9	1.5	1.1	1.2	7.9	8.4	8.2	8.2
II	1006.3	1029.0	971.3	1015.3	1.1	-4.2	5.2	12	-15.8	1	-2.5	-0.1	-1.5	-1.4	4.4	4.9	4.7	4.7	84	80	82	82	0.8	1.2	0.9	1.0	8.9	9.0	7.4	8.4
III	1003.0	1019.7	978.3	1011.9	2.1	-4.9	12.1	31	-14.0	15	-3.5	1.1	-1.6	-1.4	4.2	4.9	4.6	4.6	84	72	82	79	0.7	1.8	1.0	1.2	6.7	7.8	5.2	6.5
IV	1005.2	1020.2	979.0	1013.8	15.4	5.2	28.1	23	-1.3	6	7.3	13.7	8.9	9.7	9.0	9.0	9.7	9.2	86	58	82	75	1.6	8.2	2.4	4.1	7.3	7.7	6.1	7.0
V	1003.9	1012.0	987.4	1012.4	15.1	6.4	20.4	19	-3.7	1	9.2	13.5	10.0	10.7	10.2	9.9	10.5	10.2	86	65	85	79	1.7	5.9	2.0	3.2	7.5	8.5	7.4	7.8
VI	1009.4	1021.6	997.4	1017.9	20.1	9.2	30.8	16	1.7	3	13.3	18.3	14.2	15.0	11.1	10.8	12.1	11.3	72	52	73	66	4.6	10.9	4.7	6.7	6.2	7.4	5.7	6.4
VII	1005.7	1016.8	989.7	1014.1	21.3	10.6	31.6	26	5.8	29	13.9	19.8	15.1	16.0	13.7	12.8	13.4	13.3	86	56	78	73	2.4	11.0	4.1	5.8	7.4	7.7	5.7	6.9
VIII	1006.1	1015.4	994.2	1014.5	21.5	11.9	29.6	12	6.3	10	14.6	19.8	15.4	16.3	14.2	13.9	14.4	14.2	85	61	82	76	2.5	9.8	3.4	5.2	7.4	8.5	5.9	7.3
IX	1007.1	1022.5	987.0	1015.6	17.3	8.0	29.6	4	4.4	24	10.0	16.3	11.5	12.3	11.0	11.7	11.6	11.4	90	64	85	80	1.4	7.5	2.3	3.7	7.5	7.2	4.7	6.5
X	1013.6	1028.6	1001.2	1022.3	13.1	4.5	21.4	4	-3.2	16	6.2	12.3	7.7	8.5	9.2	10.3	9.7	9.7	94	71	89	85	0.6	4.5	1.2	2.1	7.4	6.7	5.6	6.6
XI	1008.9	1025.4	989.1	1017.7	5.3	1.8	12.8	4	-4.9	17	3.1	4.6	3.6	3.7	7.1	7.4	7.2	7.2	91	86	89	89	0.7	1.4	1.0	1.0	8.8	8.6	7.9	8.4
XII	1008.0	1040.0	964.7	1017.1	-2.2	-7.1	4.9	12	-20.3	21	-4.9	-3.1	-4.9	-4.4	4.1	4.3	4.0	4.1	87	81	85	84	0.5	0.9	0.6	0.7	8.2	8.2	6.9	7.8
Rok	1006.9	1040.0	964.7	1015.6	11.0	3.3	31.6	26.VII	-20.3	21.XII	5.6	9.8	6.5	7.1	8.6	8.8	8.9	8.8	86	69	83	79	1.5	5.4	2.1	3.0	7.6	8.0	6.4	7.3

Białystok $H_s = 139\ m$ $H_b = 140{,}8\ m$ $h_w = 11\ m$ 1962

ROZKŁAD WIATRU (n D, v m/s) · OPAD R · LICZBA DNI (n)

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min<−10°	Max<0°	Min<0°	Max>25°	Wiatr v≥10	v≥15	◔	●	Opad R ≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	4	5.0	2.5	6.2	0.5	2.0	2.5	3.6	17	3.5	24.5	4.1	19	4.1	3	3.2	20	3.1	36	9.0	6	3	8	25	·	1	·	2	20	17	10		3	26	·
II	7	4.6	3	5.0	10.5	3.5	5.5	3.1	9	4.0	15	5.0	10.5	5.2	8.5	5.2	15	3.7	42	10.9	12	11	17	28	·	5	·	1	17	15	11	1	4	28	·
III	13.5	5.8	5.5	3.5	3.5	2.6	14.5	4.8	5.5	4.6	15	1.7	4.5	5.6	8.5	4.1	36	2.8	52	11.2	13	10	18	29	·	3	·	5	14	15	15	1	·	31	·
IV	8	2.4	10	3.6	6	2.6	14	4.5	11.5	3.5	4	3.1	7	3.0	11.5	3.8	18	2.8	47	11.0	27	·	·	3	3	·	·	4	11	12	9	1	1	1	·
V	11.5	2.8	3	1.5	2.5	2.4	3	3.7	10	3.1	7.5	3.5	19	3.6	12.5	2.8	24	2.3	99	14.5	24	·	·	4	·	·	·	·	14	19	13	3	2	·	8
VI	12.5	4.1	4.5	7.1	·	·	1.5	2.0	8	2.3	14	3.7	20.5	3.2	13	3.8	16	3.1	61	27.0	4	·	·	·	4	3	·	·	9	13	9	2	·	·	3
VII	8.5	3.5	4	2.9	·	·	1.5	3.7	9.5	3.3	17.5	3.7	23	4.3	10	3.0	19	3.0	40	8.1	26	·	·	·	5	·	·	·	10	13	9	·	1	·	5
VIII	2	2.5	·	·	0.5	2.0	6.5	3.4	8	3.4	15.5	3.5	27.5	4.1	11	3.8	22	2.8	76	23.7	15	·	·	·	6	·	·	·	12	13	11	2	2	·	5
IX	4.5	3.0	7.5	1.5	4	2.9	7.5	3.1	10	4.0	16	4.2	18	4.2	7.5	3.7	15	3.0	80	22.4	18	·	·	·	1	1	·	1	13	17	13	1	3	·	3
X	5.5	1.6	1.5	1.3	2	2.0	10	2.8	7	2.9	13.5	3.7	20.5	3.8	6	2.8	27	2.2	6	3.0	19	·	·	6	·	·	·	·	13	9	2	·	14	·	·
XI	3	3.0	4.5	6.3	12	6.0	34.5	4.6	4	4.8	4	4.1	11.5	4.4	8.5	3.9	8	4.3	57	10.7	15	·	·	10	·	2	·	1	24	18	15	1	7	5	·
XII	11.5	3.5	13	3.3	1.5	4.3	9	3.2	14.5	4.8	11	4.5	16	4.0	7.5	3.5	9	3.5	20	4.2	14	11	18	26	·	·	·	3	21	17	6	·	2	18	
Rok	91.5	3.5	59	3.5	43	2.5	110	3.5	114	3.7	144	3.7	197	4.1	107.5	3.6	229	3.0	616	27.0	4.VI	35	61	131	19	15	·	17	178	178	121	12	39	109	24

UWAGA. Kierunki i prędkości wiatru – wg anemometru.

Przelewice $H_s = 60\ m$ $h_w = 10\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Min<−10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	2.5	4.0	2.5	3.6	0.5	2.0	5.5	4.9	23.5	5.7	38.5	5.6	10	5.4	6	4.2	4	5.1	33	4.2	12	2	4	11	·	5	·	1	17	20	11	·	1	3	:
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	38	11.2	12	2	7	21	·	–	–	2	16	11	7	2	2	10	1
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	42	17.5	12	·	4	28	·	–	–	5	13	13	9	2	·	–	·
IV	7.5	2.2	8	3.0	6	2.6	6.5	2.5	11.5	3.4	13	3.7	12.5	3.2	9	2.1	16	2.4	39	14.9	29	·	·	1	3	·	·	5	11	14	7	1	1	1	·
V	5	1.9	1.5	1.7	2	2.0	10	2.6	12	2.1	28	2.6	10	3.3	6.5	1.7	18	2.0	97	11.3	12	·	·	·	·	·	·	·	17	20	17	2	1	·	4
VI	8	1.9	1.5	2.0	1	1.0	8	2.9	3.5	1.3	26	3.0	18	3.3	13	2.1	11	2.4	31	5.6	28	·	·	·	6	·	·	3	10	12	10	·	·	·	2
VII	2	2.0	1.5	1.3	3.5	1.6	3.5	1.9	9	2.5	27.5	2.7	10	2.3	4	2.8	32	1.6	76	15.0	3	·	·	·	2	·	·	1	10	17	12	2	1	·	3
VIII	3.5	1.7	2	1.2	0.5	1.0	6	2.8	14.5	2.7	43.5	3.4	9.5	3.1	4.5	2.0	9	2.7	75	13.6	5	·	·	·	1	·	·	1	19	15	13	3	·	·	1
IX	·	·	·	·	8	3.0	12.5	2.4	17.5	2.5	33	3.2	11	2.8	2	1.5	6	2.6	63	19.6	18	·	·	·	1	·	·	2	9	14	11	2	3	·	2
X	1	1.0	2	1.5	4.5	1.3	13	2.1	18	2.1	24.5	2.2	8.5	2.4	5.5	1.4	16	1.7	15	9.3	4	·	·	1	·	·	·	3	15	6	3	·	10	·	1
XI	1	2.0	6.5	5.8	19	3.3	12.5	2.0	14	2.3	19.5	2.8	4.5	3.3	1	1.0	12	2.6	24	5.2	18	·	2	11	·	1	·	1	18	14	8	·	7	6	
XII	0.5	2.0	8	2.8	13	2.4	7.5	1.9	26.5	3.1	20.5	4.0	7	3.4	1	2.0	9	2.8	40	8.9	11	8	15	25	·	2	·	3	17	13	8	·	2	6	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	573	19.6	18.IX	12	32	98	13	–	–	27	172	169	116	14	28	–	14

Ostrołęka $H_s = 95\ m$ $H_b = 96{,}3\ m$ $h_w = 13\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Min<−10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	5.5	4.4	3	4.5	5	1.2	1	2.0	14.5	2.8	32.5	3.7	21	4.8	6.5	2.3	4	3.5	19	4.6	25	3	6	19	·	3	·	2	21	10	7	·	9	19	
II	9	4.4	8	4.4	7.5	3.3	5	1.7	10.5	2.5	11	5.3	9.5	7.3	11.5	6.4	12	4.0	43	7.1	25	7	13	26	·	6	5	·	17	16	12	·	7	28	
III	13	4.1	12	3.6	4	2.1	21.5	1.7	8	2.2	3.5	1.4	4	2.8	8	3.8	19	2.2	46	9.2	5	5	7	29	·	1	·	3	12	15	10	·	3	31	
IV	14.5	3.6	10	3.7	3	4.2	12.5	2.5	9.5	2.8	13	2.7	6	1.7	3.5	1.7	18	2.3	44	12.7	13	·	·	3	3	1	·	2	8	11	6	1	2	1	1
V	15	2.0	6	2.1	1	2.5	5	2.3	12.5	2.1	13.5	2.7	9	2.7	10	3.6	21	1.9	130	17.5	14	·	·	2	·	·	·	·	16	24	18	5	1	·	6
VI	18	3.6	8.5	3.1	2.5	2.6	2	1.0	5	2.1	8.5	2.8	18.5	3.8	11	2.3	16	2.5	45	8.8	4	·	·	·	5	1	·	1	9	13	9	·	·	·	2
VII	12.5	3.6	9.5	2.2	1	2.0	2	1.2	5	2.4	17.5	2.6	11	2.1	12.5	3.8	22	2.1	38	15.1	26	·	·	·	4	1	1	·	6	10	7	1	1	·	2
VIII	5.5	1.6	2.5	1.8	·	·	2.5	1.4	9	3.1	14	2.3	27	3.6	9.5	3.0	23	2.2	82	18.5	15	·	·	·	5	·	·	·	7	15	12	2	3	·	6
IX	6.5	2.5	3.5	1.9	6.5	1.5	4.5	1.8	6.5	2.6	15	2.8	16	3.3	10.5	3.0	21	2.0	54	16.2	18	·	·	·	1	·	·	2	10	19	10	1	1	·	2
X	2	2.7	3	2.2	·	·	5	1.4	10	1.6	6.5	1.5	18	2.6	7.5	3.0	41	1.2	9	4.9	28	·	·	5	·	2	·	2	11	7	3	·	14	·	
XI	6	1.3	3	1.5	12.5	4.9	20	3.1	9	1.9	4.5	3.8	11	2.6	5	1.9	19	2.3	58	9.5	15	·	·	10	·	1	·	·	25	15	11	·	9	2	
XII	8.5	1.9	16.5	2.7	6	2.1	3.5	1.7	10	2.4	19	3.5	15	2.6	4.5	1.4	10	2.3	16	3.6	14	10	16	27	·	2	·	3	19	14	5	·	5	16	·
Rok	116	3.0	85.5	2.8	49	2.2	84.5	1.8	109.5	2.4	158.5	2.9	166	3.3	100	3.0	226	2.4	584	18.5	15.VIII	25	42	121	18	18	6	15	161	169	110	10	55	97	19

Toruń-Wrzosy $H_s = 69\ m$ $H_b = 70{,}2\ m$ $h_w = 20\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Min<−10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	3	4.2	4.5	3.8	1.5	3.0	4.5	3.9	19.5	3.4	34.5	3.8	15	3.8	7.5	4.1	3	3.6	27	10.6	25	2	4	20	·	1	·	2	20	14	8	1	3	12	·
II	4	6.1	10.5	5.1	6.5	4.6	5.5	3.4	9.5	3.7	13.5	5.1	17	4.7	13.5	6.1	4	4.7	31	8.8	16	3	9	24	·	6	1	·	17	17	6	·	3	17	
III	14	4.6	11.5	3.3	7.5	4.2	18	3.7	7	2.4	8.5	1.3	5.5	3.1	11	4.1	10	3.1	33	8.8	5	2	8	27	·	2		4	13	12	6	·	4	18	-
IV	11.5	4.2	7.5	4.6	8	4.6	10	3.0	9.5	3.9	9	3.8	10	2.7	10.5	3.9	14	3.2	38	8.6	5		·	2	3	2	1	1	11	14	9	·	3	·	2
V	7.5	2.3	3.5	2.0	5.5	1.7	9	2.6	7.5	2.1	16.5	2.7	17	2.9	13.5	3.5	13	2.3	121	29.4	14	·	·	3	·	2	·	1	17	21	16	3	1	·	7
VI	12	4.9	·	·	2.5	2.2	6.5	2.7	2.5	2.4	8	3.6	26	3.6	21.5	4.2	11	3.3	69	19.2	3		·	·	7	4	·	1	10	13	10	2	1	·	6
VII	9	2.7	8.5	3.2	2.5	1.6	2	3.0	8	2.6	17.5	2.8	19.5	2.8	17	2.8	9	2.5	50	12.6	14	·	·	·	5	1	1	·	12	13	10	2	4	·	5
VIII	4.5	1.7	1	1.5	0.5	3.0	6	2.9	5.5	2.5	28.5	3.2	25.5	3.3	7.5	2.9	14	2.6	63	11.0	5	·	·	·	5	2	2	1	12	17	15	1	·	·	5
IX	2	2.5	1	1.0	9.5	2.8	9.5	2.4	7	3.1	18.5	3.6	26.5	2.9	6	2.2	10	2.6	64	30.3	18	·	·	·	1	1	·	2	10	15	8	1	5	·	3
X	5.5	1.9	1.5	1.3	5	2.9	16	2.2	8.5	1.9	8.5	2.5	16	2.5	8	1.9	24	1.7	30	11.9	5	·	·	6	·	·	·	2	13	7	6	1	16	·	·
XI	2	3.7	8	4.9	22	4.7	15.5	3.0	10	1.4	12.5	2.2	8.5	2.5	2.5	2.0	9	2.9	39	8.7	20		·	10	·	·	·	1	21	15	12	·	7	1	·
XII	6.5	1.7	13.5	3.1	4	2.9	11	2.4	13.5	2.7	16	3.1	13	2.3	7.5	1.8	8	2.4	42	4.7	15	10	16	27	·	·	·	3	20	14	3	·	5	17	·
Rok	81.5	3.4	71	2.8	75	3.2	113.5	2.9	108	2.7	191.5	3.1	199.5	3.1	126	3.3	129	2.9	577	30.3	18.IX	17	37	119	21	21	5	18	176	172	109	11	51	65	28

Przasnysz $\varphi = 53°01'$ $\lambda = 20°53'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																					
	P_m	Max	Min	P_{0m}	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.9	-3.6	7.7	22	-21.1	31	-1.5	0.6	-1.6	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.9	8.2	7.6
II	–	–	–	–	-0.7	-6.8	3.0	12	-18.5	1,3	-4.3	-1.2	-3.7	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.4	8.1	7.8
III	–	–	–	–	0.5	-6.1	9.2	31	-18.3	1.5	-4.4	0.3	-2.9	-2.5	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.7	6.9	7.0
IV	–	–	–	–	15.1	5.1	27.3	23	-0.6	30	7.5	14.2	8.5	9.7	–	–	–	–	–	–	–	–	–	–	–	–	7.9	6.4	7.7	7.3
V	–	–	–	–	14.5	6.5	19.7	28	-2.1	1	9.4	13.6	9.9	10.7	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.5	8.5	7.9
VI	–	–	–	–	19.3	9.3	28.0	16,23	5.4	10	12.8	18.7	12.9	14.3	–	–	–	–	–	–	–	–	–	–	–	–	5.3	4.4	5.2	5.0
VII	–	–	–	–	21.1	10.6	29.3	26	7.1	30	13.4	19.9	14.1	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.8	4.5	4.9	5.1
VIII	–	–	–	–	21.0	11.2	29.9	13	6.5	10	13.7	19.7	14.6	15.6	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.6	7.8	7.3
IX	–	–	–	–	16.4	7.6	25.7	4	3.3	27	9.4	15.5	11.1	11.8	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.8	7.3	6.7
X	–	–	–	–	12.4	3.9	19.8	4	-2.9	16	5.8	11.8	6.8	7.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.7	7.2	7.1
XI	–	–	–	–	5.3	1.4	12.1	1	-2.3	18	2.6	5.0	3.1	3.4	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.9	8.1	8.1
XII	–	–	–	–	-2.9	-7.2	3.0	11,12	-21.0	21	-5.2	-3.5	-5.4	-4.9	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.2	7.7	7.5
Rok	–	–	–	–	10.2	2.7	29.9	13.VIII	-21.1	31.I	4.9	9.6	5.6	6.4	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.5	7.3	7.0

Chodzież $\varphi = 52°59'$ $\lambda = 16°54'$

I	–	–	–	–	2.8	-1.7	8.8	22	-15.3	31	-0.1	1.9	0.0	0.4	5.5	5.9	5.5	5.6	8.8	8.2	8.6	8.5	0.7	1.3	0.9	1.0	9.3	7.8	8.0	8.4
II	–	–	–	–	1.5	-3.8	7.0	20	-14.0	1	-2.4	0.5	-1.4	-1.2	4.6	5.5	5.1	5.1	8.8	8.6	8.7	8.7	0.6	1.0	0.7	0.8	9.1	8.0	7.1	8.1
III	–	–	–	–	3.2	-5.0	12.4	30	-9.8	16	-2.7	2.3	-2.6	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.8	4.6	5.8
IV	–	–	–	–	15.0	4.5	27.2	23	-0.9	30	7.3	13.6	7.3	8.9	8.7	9.4	8.6	8.9	8.3	6.1	8.3	7.6	1.9	7.6	2.1	3.9	5.9	5.6	5.2	5.6
V	–	–	–	–	14.7	5.8	20.7	20	-2.0	1	8.9	13.0	8.4	9.7	9.9	10.0	10.0	10.0	8.6	6.7	8.9	8.1	1.7	5.3	1.3	2.8	7.5	8.1	6.0	7.2
VI	–	–	–	–	20.1	9.0	30.2	16	1.9	3	12.8	18.0	13.1	14.2	11.5	12.3	11.9	11.9	7.6	6.0	7.8	7.1	3.7	9.4	3.6	5.4	3.6	5.5	4.7	4.6
VII	–	–	–	–	20.8	10.5	29.3	26	6.6	4	13.7	19.1	14.2	15.3	13.7	13.5	14.0	13.7	8.7	6.3	8.5	7.8	2.2	9.4	2.5	4.7	5.3	7.3	4.2	5.6
VIII	–	–	–	–	20.4	11.8	28.1	12	6.2	11	13.9	19.0	15.3	15.9	14.1	14.6	14.3	14.3	8.8	6.8	8.2	7.9	1.9	7.7	3.3	4.3	6.7	6.9	6.3	6.6
IX	–	–	–	–	16.9	7.8	28.1	4	1.8	27	9.4	15.5	11.3	11.9	10.9	12.2	11.5	11.5	9.1	6.9	8.6	8.2	1.1	6.0	2.1	3.1	6.1	6.7	3.8	5.5
X	–	–	–	–	12.4	4.6	21.0	1,2,3	0.4	16	6.3	11.7	7.5	8.2	9.0	10.5	9.7	9.7	9.1	7.5	9.0	8.5	0.8	3.7	1.0	0.8	7.7	7.4	4.7	6.7
XI	–	–	–	–	4.9	1.5	13.9	5	1.9	21,22	2.4	4.4	3.2	3.3	6.8	7.5	7.1	7.1	9.3	8.8	9.1	9.0	0.6	1.2	0.8	0.8	8.5	7.8	8.2	8.2
XII	–	–	–	–	2.0	6.9	5.2	12	19.2	22	5.2	3.2	4.6	4.4	4.0	4.5	4.2	4.2	8.6	8.6	8.7	8.6	0.5	0.6	0.5	0.5	8.1	7.4	6.6	7.4
Rok	–	–	–	–	10.9	3.2	30.2	16.VI	19.2	22.XII	5.4	9.6	6.0	6.8	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.1	5.8	6.6

Trzcińsko-Zdrój $\varphi = 52°58'$ $\lambda = 14°36'$

I	–	–	–	–	3.7	-0.6	8.7	22	-12.9	31	1.0	2.6	1.4	1.6	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.3	7.1	7.9
II	–	–	–	–	2.7	-2.3	8.0	8	-12.0	1	-0.6	1.7	0.0	0.3	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.7	6.5	7.6
III	–	–	–	–	3.9	-2.9	14.5	30	-8.8	8	-1.8	2.9	0.0	0.3	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.0	6.6	7.0
IV	–	–	–	–	14.3	4.2	27.0	25	0.4	11	6.5	12.6	8.3	8.9	8.6	9.4	9.3	9.1	8.8	6.4	8.3	7.8	1.3	6.1	2.2	3.2	7.4	6.7	5.1	6.4
V	–	–	–	–	14.5	6.4	21.4	19	-1.4	1	9.2	13.0	9.9	10.5	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.3	7.3	7.7
VI	–	–	–	–	19.5	8.3	29.1	15	1.8	7	13.2	17.8	13.4	14.4	12.5	13.0	12.8	12.8	8.1	6.3	8.1	7.5	3.2	8.3	3.0	4.8	6.1	6.5	6.4	6.3
VII	–	–	–	–	20.2	10.5	27.0	21	6.7	29	13.7	18.6	14.1	15.1	14.1	14.5	14.5	14.4	8.9	6.8	8.9	8.2	1.8	7.3	1.8	3.6	7.1	7.2	7.1	7.1
VIII	–	–	–	–	20.2	11.2	28.9	12	7.8	9	13.8	18.6	14.8	15.5	14.2	15.6	14.7	14.8	9.0	7.3	8.7	8.3	1.6	6.1	2.2	3.3	7.9	8.4	6.1	7.5
IX	–	–	–	–	17.1	8.0	27.5	3	3.5	25	9.9	16.1	11.2	12.1	11.3	12.3	11.9	11.8	9.2	6.8	8.9	8.3	1.0	6.5	1.6	3.0	7.5	7.2	4.1	6.3
X	–	–	–	–	12.9	5.2	22.9	2	-0.4	24	6.8	11.9	8.3	8.8	9.6	10.8	10.2	10.2	9.5	7.6	9.1	8.7	0.5	3.6	1.0	1.7	8.6	7.4	4.9	7.0
XI	–	–	–	–	5.3	1.4	14.2	8	-3.1	25	2.7	4.9	3.0	3.4	7.2	7.7	7.3	7.4	9.5	8.8	9.5	9.3	0.4	1.2	0.4	0.7	9.6	8.6	7.0	8.4
XII	–	–	–	–	-1.1	-5.4	5.4	12	-15.7	22	-3.6	-1.8	-3.2	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.5	6.7	7.3
Rok	–	–	–	–	11.1	3.7	29.1	15.VI	-15.7	22.XII	5.9	9.9	6.8	7.4	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.6	6.2	7.2

Wądołki Borowe $\varphi = 52°57'$ $\lambda = 22°13'$

I	–	–	–	–	0.7	-3.9	7.2	22	-21.3	31	-1.7	-0.2	-1.7	-1.3	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.5	8.0	7.8
II	–	–	–	–	-1.4	-7.4	3.6	12	-16.8	1	-5.1	-2.7	-4.0	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.2	7.3	8.0
III	–	–	–	–	-0.2	-8.1	6.4	31	-20.8	2	-6.3	-1.3	-3.8	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	7.9	6.6	5.8	6.8
IV	–	–	–	–	14.5	5.0	26.3	22	-1.3	30	7.2	13.3	8.7	9.5	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.7	5.4	7.0
V	–	–	–	–	14.6	6.2	19.5	28	-2.5	1	9.0	13.2	9.6	10.4	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.5	6.8	7.9
VI	–	–	–	–	18.8	8.5	28.4	23	4.2	13	12.9	17.2	12.1	13.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.8	5.6	6.9
VII	–	–	–	–	20.9	9.8	27.6	26	5.8	4	14.0	19.3	14.0	15.3	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.8	6.4	7.0
VIII	–	–	–	–	21.0	10.8	29.3	13	6.1	10	13.9	19.5	14.6	15.6	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.7	6.6	7.4
IX	–	–	–	–	16.2	7.0	25.7	5	1.2	25	8.9	15.0	10.5	11.2	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.9	5.4	6.9
X	–	–	–	–	11.9	3.1	18.5	2	-4.2	16	4.9	11.0	6.4	7.2	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.2	5.4	6.9
XI	–	–	–	–	5.8	1.4	15.9	1	-2.5	18	2.7	4.8	3.3	3.5	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.4	8.5	8.6
XII	–	–	–	–	-3.2	-11.0	3.0	5	-22.3	21	-5.9	-4.4	-5.6	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.4	7.7	8.1
Rok	–	–	–	–	10.0	1.8	29.3	13.VIII	-22.3	21.XII	4.5	8.7	5.3	6.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.8	6.6	7.4

Przasnysz $H_s = 120\,m$ $h_w = 14\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU (%D, v m/s) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min ≤ -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	◔	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R FO
I	7.5	3.1	4	4.0	·	·	·	·	10.5	2.8	26.5	2.7	37.5	3.1	1	2.0	6	2.6	29	12.3	25	3	7	19	·		·	·	15	8	5	1	2	17	·
II	3.5	2.7	4.5	1.9	12	2.1	2	1.5	12	2.0	6	6.7	24	4.5	17	3.8	3	3.3	24	5.2	12	7	14	28	·	2	1	·	12	16	8	·	2	21	·
III	13.5	3.4	5.5	1.5	10.5	1.7	13	1.8	18	2.2	·	·	10.5	1.9	14	2.6	8	2.1	29	9.3	5	4	10	28	·	·	·	·	14	11	6	·	1	13	·
IV	7	3.0	4	2.8	7	2.4	12	2.1	9	2.2	14.5	1.8	21.5	2.5	10	1.9	5	2.2	32	13.0	5	·	·	1	3	·	·	1	12	8	5	1	1	·	1
V	7	1.3	3	1.0	5	1.0	4	1.6	9	2.5	5	2.2	30.5	2.8	12.5	1.5	17	1.7	106	24.3	14	·	·	2	·	·	·	·	15	22	18	3	·	·	4
VI	18	3.1	·	·	·	·	·	·	3	1.0	4.5	2.6	34	2.6	22.5	1.9	8	2.2	33	15.5	29	·	·	·	5	·	·	6	4	12	8	1	·	·	2
VII	9	2.2	4	2.0	2	1.5	2	1.0	4.5	1.8	8.5	2.2	28	1.9	24	2.2	11	1.8	18	7.6	13	·	·	·	4	·	·	6	1	9	4	·	·	·	4
VIII	1	1.0	·	·	·	·	3	1.7	6.5	1.8	12.5	2.4	38	2.4	24	1.5	8	1.9	81	37.2	17	·	·	·	5	·	·	1	11	13	12	1	·	·	3
IX	2	3.0	·	·	8	1.0	3	1.3	1.5	2.0	10.5	2.2	37.5	3.0	12.5	2.1	15	2.0	55	15.5	18	·	·	·	1	·	·	·	12	12	8	2	1	·	·
X	4	1.2	5	1.2	13	1.2	7	1.0	12	1.3	8	1.1	20	2.7	7	2.6	17	1.4	5	2.9	28	·	·	4	·	·	·	·	15	4	2	·	6	·	·
XI	1	3.0	·	·	13	3.5	23	2.4	9	1.7	3	2.0	30	2.1	2	3.5	9	2.2	45	13.1	19	·	·	11	·	·	·	3	21	13	10	1	7	1	·
XII	10.5	1.2	14	1.2	·	·	0.5	1.0	15.5	2.1	10.5	3.5	25.5	2.5	1.5	3.0	15	1.8	12	5.1	16	9	17	27	·	·	·	2	17	9	4	·	4	16	·
Rok	84	2.4	44	1.0	70.5	1.2	69.5	1.3	110.5	2.0	109.5	2.4	337	2.7	148	2.4	122	2.1	469	37.2	17.VIII	23	48	120	18	2	1	19	149	137	90	10	24	68	14

Chodzież $H_s = 100\,m$ $h_w = 12\,m$

I	1.5	1.0	3.5	2.4	·	·	3.5	2.3	19	1.8	35.5	2.6	9	2.8	8	3.5	13	2.1	36	9.2	12	2	5	15	·	·	·	1	22	19	11	·	–	11	·
II	4	2.0	4	2.0	9	1.8	4	1.5	7	1.8	22	3.1	10	3.7	13	3.8	11	2.5	57	17.2	12	2	9	25	·	2	1	·	15	19	8	2	–	15	·
III	8	1.2	6.5	1.6	3.5	1.3	7.5	1.8	7	1.9	5	1.2	5	1.8	5.5	3.4	45	0.9	45	12.4	12	·	4	28	·	·	·	5	9	12	8	2	3	14	·
IV	3	1.0	7	1.6	3	3.3	2	2.5	7	1.4	11.5	2.0	9.5	1.4	8	1.4	39	1.0	40	11.2	1	·	·	2	3	·	·	6	9	13	8	1	3	·	2
V	2	1.5	2.5	1.4	3	1.0	6.5	1.8	8.5	1.4	19.5	1.7	12.5	2.0	9.5	1.8	29	1.2	94	14.0	14	·	·	2	·	·	·	·	12	23	16	3	·	·	5
VI	4.5	1.7	3.5	1.4	1	2.5	0.5	1.0	7	1.6	17	1.9	25	1.9	12.5	1.8	49	1.5	55	12.0	29	·	·	·	6	·	·	5	3	12	10	1	1	·	3
VII	0.5	1.0	3.5	1.3	2	2.5	1	2.5	4.5	1.9	28	1.7	15.5	2.0	3	1.8	35	1.1	50	10.8	3	·	·	·	5	·	·	5	8	13	9	1	–	·	4
VIII	4	2.0	4	2.9	2	1.8	3	2.0	13	1.9	26.5	2.2	22.5	2.1	7	1.7	11	1.8	83	15.9	4	·	·	·	3	·	·	2	11	19	16	2	2	·	4
IX	·	·	0.5	1.0	2.5	2.0	8	2.1	4.5	1.9	21.5	2.0	17.5	1.9	3.5	2.0	32	1.3	60	16.8	18	·	·	·	1	·	·	6	6	11	9	2	3	·	·
X	0.5	1.0	0.5	1.0	0.5	1.0	5.5	1.4	10.5	1.4	8	1.2	10.5	1.3	5	1.2	52	0.6	47	5.3	31	·	·	1	·	·	·	4	13	7	4	·	9	·	·
XI	2	1.0	3	2.0	9.5	2.3	13	1.8	6.5	1.5	9.5	1.0	7.5	1.5	1	1.0	38	0.9	42	12.8	1	·	·	8	·	·	·	3	21	13	10	1	3	4	·
XII	2	1.0	3	1.0	2.5	1.6	4	1.4	7	1.8	14.5	1.9	4.5	1.9	4.5	1.0	51	0.7	35	8.8	15	9	17	28	·	·	·	3	18	11	7	·	3	18	·
Rok	32	1.2	41.5	1.6	38.5	1.8	58.5	1.8	101.5	1.7	218.5	1.9	149	2.0	80.5	2.0	375	1.3	614	17.2	12.II	13	35	109	18	2	1	40	147	172	115	15	–	62	18

Trzcińsko-Zdrój $H_s = 60\,m$ $h_w = 11\,m$

I	5.5	4.9	4	1.6	·	·	3.5	3.0	24	3.7	37	3.7	10	4.0	6	4.2	3	3.6	36	8.2	24	1	4	10	·	·	·	1	19	13	10	·	4	–	·
II	6	5.4	14	3.3	5.5	2.2	3	2.7	6.5	2.0	10.5	3.6	18.5	6.5	15	6.9	5	4.4	39	13.5	12	2	8	22	·	4	3	2	17	10	9	1	·	–	1
III	14.5	3.1	16	2.0	13	2.0	7	2.4	5	1.3	7	1.8	9	2.5	14.5	3.2	7	2.2	27	6.9	5	·	4	26	·	1	·	3	16	9	8	·	2	6	·
IV	16.5	2.6	10.5	3.0	11	1.5	2.5	1.4	9.5	1.8	11	3.4	13.5	3.3	9.5	3.9	6	2.6	26	15.6	16	·	·	·	3	·	·	1	10	7	4	1	2	·	1
V	11	2.0	8.5	1.9	3	1.3	5	3.1	8.5	2.1	6	2.5	23.5	3.1	20.5	3.0	7	2.4	53	9.3	26	·	·	1	·	·	·	·	15	16	11	·	·	·	2
VI	14	2.8	8.5	2.9	1.5	2.7	2.5	1.8	3.5	2.1	6	2.8	29	4.4	13	3.3	12	3.0	18	4.0	28	·	·	·	5	1	·	4	9	10	7	·	·	·	2
VII	10	1.1	10	1.1	3.5	1.0	4	1.5	1.5	2.0	10.5	2.7	28	3.3	6.5	1.8	19	1.8	101	17.1	7	·	·	·	2	·	·	1	12	15	14	4	2	·	5
VIII	3.5	1.6	6.5	1.5	2.5	1.4	4	2.0	4.5	2.0	16.5	3.2	36.5	4.1	11	2.2	8	2.8	69	20.4	7	·	·	·	1	2	·	·	14	13	12	1	3	·	2
IX	1.5	4.3	1	1.0	9.5	2.3	10	2.3	9	2.6	11	2.9	26.5	4.3	8.5	3.5	13	2.7	55	11.8	18	·	·	·	2	2	·	2	7	13	12	1	3	·	2
X	4.5	1.9	3	1.0	8	2.1	14.5	2.1	11	1.7	8.5	1.6	19	2.9	8.5	2.4	16	1.8	11	4.8	5	·	·	1	·	·	·	2	13	4	3	·	14	·	1
XI	2	2.0	7	2.8	23.5	2.4	11	2.0	13	1.6	8	2.3	6.5	3.8	1	1.0	18	1.8	16	3.8	18	·	2	11	·	·	·	·	21	10	7	·	5	8	·
XII	1	3.5	8.5	1.8	12	3.2	5.5	2.1	9.5	2.6	23.5	2.3	17	3.2	5	2.8	11	2.3	26	8.2	11	6	16	25	·	·	·	4	18	5	4	·	5	5	·
Rok	90	2.7	97.5	2.0	93	1.8	72.5	2.2	105.5	2.1	155.5	2.7	237	3.8	119	3.2	125	2.6	477	20.4	7.VIII	9	34	96	13	10	3	20	171	125	101	8	40	–	16

Wądołki Borowe $H_s = 130\,m$ $h_w = 12\,m$

I	5	6.9	2.5	3.8	2	1.5	2.5	4.0	26.5	5.5	29	6.0	17.5	6.7	5	6.2	3	5.6	20	6.8	25	3	6	21	·	6	·	2	17	14	8	·	3	19	·
II	8	6.6	6.5	8.3	11	4.6	5	6.1	13.5	6.8	11	6.4	16.5	7.5	6.5	7.1	6	6.2	11	2.1	8	7	17	28	·	7	·	·	17	13	6	·	4	28	·
III	13	6.0	6.5	5.7	8	3.1	21	4.5	9	3.6	4.5	5.7	9.5	5.1	6.5	5.5	15	4.1	28	5.5	12	11	18	29	·	5	·	4	15	13	7	·	2	30	·
IV	12.5	3.9	6	5.5	4.5	4.0	13	5.0	17	5.0	4.5	2.9	8.5	3.9	9	4.3	15	3.7	36	8.8	13	·	·	3	3	2	·	1	11	12	7	·	3	1	1
V	4.5	3.1	3.5	2.7	4.5	3.6	7	3.0	14.5	2.7	19	3.4	11	4.7	15	3.6	14	2.9	102	12.5	20	·	·	2	·	1	·	1	16	22	20	3	1	·	2
VI	18.5	5.7	4.5	3.0	0.5	1.0	3.5	2.4	6.5	3.3	10	3.6	23.5	4.8	9	3.6	14	3.7	75	31.8	4	·	·	·	2	2	·	1	11	13	12	1	·	·	1
VII	12	3.2	3.5	3.0	·	·	2.5	3.2	13.5	3.8	12.5	3.5	23	4.8	13	4.1	13	3.4	48	19.5	26	·	·	·	5	3	1	·	10	12	6	1	·	·	2
VIII	4	4.0	·	·	2	2.0	3.5	4.0	14.5	3.2	30.5	4.6	21	4.9	4.5	3.1	13	3.6	94	16.9	16	·	·	·	5	3	·	·	17	16	16	4	2	·	6
IX	3	4.3	2.5	3.0	9.5	2.6	5.5	3.1	14	3.9	20.5	4.9	17	5.3	7	4.4	11	3.7	65	20.0	17	·	·	·	1	1	·	·	10	18	9	2	3	·	1
X	4	2.1	1.5	1.7	2	3.5	10	2.6	10	3.2	15	3.3	17.5	5.1	7	2.4	26	2.5	5	1.2	28	·	·	8	·	2	1	1	11	14	2	·	7	·	·
XI	5.5	4.6	3	6.5	13.5	7.9	30	5.3	6.5	3.3	6	5.4	13.5	4.4	3	2.5	9	4.6	44	11.0	15	·	·	11	·	4	·	·	20	15	9	1	6	2	·
XII	11	3.5	15	4.1	1	3.0	6.5	2.7	19.5	4.7	16.5	5.5	14	4.4	3.5	3.1	6	4.0	10	3.3	16	11	18	27	·	1	·	3	20	11	4	·	·	19	·
Rok	101	4.2	55	3.9	58.5	3.1	110	3.8	165	4.1	179	4.6	192.5	5.1	89	4.2	145	4.0	538	31.8	4.VI	32	59	129	16	37	2	13	175	173	106	12	31	99	13

17*

Krzyż $\varphi = 52°53'$ $\lambda = 16°01'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA t												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o,m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.5	-1.0	9.6	22	-16.1	31	0.5	2.6	1.2	1.4	5.6	5.8	5.4	5.6	85	78	80	81	0.9	1.7	1.3	1.3	8.2	8.4	8.3	8.3
II	–	–	–	–	2.1	-2.9	7.4	20	-13.4	1	-1.7	1.1	-0.6	-0.4	4.7	5.4	5.0	5.0	83	80	83	82	0.9	1.4	1.0	1.1	8.9	9.0	6.2	8.0
III	–	–	–	–	3.6	-4.2	12.9	30	-9.4	16	-3.0	2.8	-0.9	-0.5	4.2	4.9	4.5	4.5	80	66	77	74	0.9	2.7	1.3	1.6	6.4	7.2	4.8	6.1
IV	–	–	–	–	14.9	4.0	27.7	25	-2.4	11	6.0	13.3	8.4	9.0	8.3	8.9	9.0	8.7	86	57	78	74	1.4	7.6	2.6	3.9	6.6	6.7	4.6	6.0
V	–	–	–	–	14.6	5.8	21.7	19	-2.3	1	8.6	12.9	9.5	10.1	10.0	9.6	10.2	9.9	88	64	85	79	1.4	5.7	1.8	3.0	7.4	8.0	6.5	7.3
VI	–	–	–	–	19.8	8.3	30.1	15	(1.0)	3	12.7	17.9	13.6	14.4	11.3	11.3	11.9	11.5	75	55	74	68	3.8	10.4	4.2	6.1	5.3	6.2	5.1	5.5
VII	–	–	–	–	21.0	9.6	29.8	26	3.8	25	13.4	19.3	14.2	15.3	13.4	12.4	13.8	13.2	86	57	84	76	2.1	10.6	2.6	5.1	7.2	7.4	6.0	6.9
VIII	–	–	–	–	20.9	10.6	29.6	12	4.4	10	13.7	19.5	14.6	15.6	13.6	14.1	13.9	13.9	86	63	83	77	2.1	9.0	2.9	4.7	7.0	8.3	5.2	6.8
IX	–	–	–	–	17.5	6.8	27.0	4	1.0	15	9.0	16.0	10.3	11.4	10.9	11.5	11.2	11.2	94	64	89	82	0.8	7.2	1.6	3.2	6.6	6.1	4.1	5.6
X	–	–	–	–	13.0	3.2	22.8	2	-3.7	16	5.5	12.1	7.0	7.9	8.8	10.7	9.3	9.6	9.5	7.5	9.0	8.7	0.5	4.0	1.1	1.9	8.0	7.0	4.9	6.6
XI	–	–	–	–	5.6	1.4	14.2	5	-3.7	21	2.4	5.0	3.0	3.4	6.9	7.6	6.9	7.1	93	86	89	89	0.5	1.4	0.9	0.9	8.5	8.1	7.4	8.0
XII	–	–	–	–	-1.7	-6.3	6.5	12	-17.4	22	-4.7	-2.9	-4.0	-3.9	4.2	4.6	4.2	4.3	89	87	86	87	0.4	0.6	0.6	0.5	8.7	7.7	6.2	7.5
Rok		–	–	–	11.2	2.9	30.1	15.VI	-17.4	22.XII	5.2	10.0	6.4	7.0	8.5	8.9	8.8	8.7	87	69	83	80	1.3	5.2	1.8	2.8	7.4	7.5	5.8	6.9

Ciechocinek $\varphi = 52°53'$ $\lambda = 18°48'$

I	–	–	–	–	2.4	-1.5	9.0	22	-14.7	31	-0.1	1.5	0.2	0.4	5.5	5.7	5.5	5.6	88	82	86	85	0.7	1.3	0.9	1.0	7.8	8.0	8.2	8.0
II	–	–	–	–	1.2	-3.9	6.5	12	-13.8	1	-2.4	0.0	-1.3	-1.2	4.5	4.9	4.8	4.7	86	78	83	82	0.7	1.3	0.9	1.0	8.6	8.1	6.5	7.7
III	–	–	–	–	2.6	-4.5	12.1	31	-12.1	9	-3.2	1.7	-1.3	-1.0	4.4	5.0	4.8	4.7	88	70	85	81	0.6	2.1	0.8	1.2	7.0	6.7	5.0	6.2
IV	–	–	–	–	15.6	5.6	28.2	23	0.5	6	7.4	14.0	9.7	10.2	9.1	9.7	10.0	9.6	87	61	81	76	1.5	8.0	2.7	4.1	6.1	6.3	4.7	5.7
V	–	–	–	–	15.5	6.6	20.9	8	-3.1	1	9.3	13.8	10.4	11.0	10.6	10.7	11.1	10.8	89	68	87	81	1.4	5.5	1.8	2.9	7.4	8.0	6.4	7.3
VI	–	–	–	–	20.5	9.7	31.3	16	2.7	3	13.4	18.9	14.4	15.3	11.9	11.9	12.6	12.1	76	54	75	68	4.0	10.9	4.3	6.4	5.6	6.1	5.1	5.6
VII	–	–	–	–	21.8	10.8	30.9	26	6.9	29	14.2	20.1	15.4	16.3	14.1	13.7	14.3	14.0	86	59	82	76	2.3	10.7	3.5	5.5	6.5	6.5	5.8	6.3
VIII	–	–	–	–	22.0	12.3	30.3	12	7.6	10	15.0	20.7	15.7	16.8	14.9	15.1	15.3	15.1	86	62	85	78	2.4	9.9	2.8	5.0	6.5	7.5	5.7	6.6
IX	–	–	–	–	17.4	8.2	29.0	4	4.2	27	10.0	16.4	11.6	12.4	11.4	12.5	12.2	12.0	94	68	88	83	1.2	6.7	1.8	3.2	7.1	7.5	4.3	6.3
X	–	–	–	–	13.3	5.0	21.6	4	-2.3	16	6.5	12.6	8.0	8.8	9.4	10.7	10.0	10.0	95	72	91	86	0.6	4.3	1.1	2.0	6.9	5.6	5.2	5.9
XI	–	–	–	–	5.6	2.2	12.6	4	-1.7	17	3.2	4.9	3.8	3.9	7.2	7.5	7.4	7.4	92	85	91	89	0.6	1.4	0.8	0.9	8.1	8.9	7.8	8.3
XII	–	–	–	–	-2.2	-6.9	4.7	10	-20.1	21	-4.8	-3.0	-4.8	-4.4	4.2	4.6	4.2	4.3	92	87	89	89	0.4	0.6	0.5	0.5	8.7	8.0	6.9	7.9
Rok	–	–	–	–	11.3	3.6	31.3	16.VI	-20.1	21.XII	5.7	10.1	6.8	7.4	8.9	9.3	9.4	9.2	88	70	85	81	1.4	5.2	1.8	2.8	7.2	7.3	6.0	6.8

Kobylec $\varphi = 52°51'$ $\lambda = 17°12'$

I	–	–	–	–	3.0	-1.4	9.3	22	-13.7	31	-0.2	2.0	0.5	0.7	5.4	5.9	5.7	5.7	87	83	87	86	0.8	1.4	0.9	1.0	8.5	8.5	8.2	8.4
II	–	–	–	–	1.3	-3.7	6.2	20	-14.0	1	-2.6	0.4	-1.1	-1.1	4.9	5.4	5.0	5.1	94	85	88	89	0.3	1.0	0.7	0.7	8.9	9.1	7.2	8.4
III	–	–	–	–	2.6	-	11.7	31	–	-	-2.7	1.8	-1.5	-1.0	4.7	5.2	5.0	5.0	90	73	89	84	0.5	2.0	0.6	1.0	6.7	7.2	5.6	6.5
IV	–	–	–	–	14.9	5.2	26.7	23	-0.2	30	7.7	13.7	8.7	9.7	8.9	9.5	9.3	9.2	82	60	80	74	2.1	7.6	2.5	4.1	6.2	6.8	5.8	6.3
V	–	–	–	–	14.5	6.2	20.8	19	-2.5	1	9.2	13.3	9.2	10.2	10.1	10.3	10.6	10.3	86	67	90	81	1.7	5.4	1.3	2.8	7.5	8.2	6.9	7.5
VI	–	–	–	–	19.5	8.8	30.9	16	2.1	3	13.0	18.0	13.7	14.6	12.3	13.0	13.4	12.9	79	62	83	75	3.2	8.7	2.9	4.9	4.9	6.3	5.5	5.6
VII	–	–	–	–	20.8	10.0	31.0	26	5.3	29	13.9	19.2	14.6	15.6	14.0	13.1	14.7	14.0	87	61	88	79	2.1	10.0	2.2	4.8	6.5	6.5	5.9	6.3
VIII	–	–	–	–	20.6	12.0	28.7	12	9.0	10	14.6	19.1	15.0	15.9	15.1	15.4	15.5	15.3	91	71	91	84	1.6	7.1	1.8	3.5	6.1	8.1	6.5	6.9
IX	–	–	–	–	17.1	8.0	28.4	4	3.7	25	10.1	16.2	11.2	12.2	11.4	12.3	12.3	12.0	92	68	91	84	1.2	6.6	1.2	3.0	7.2	6.9	4.9	6.3
X	–	–	–	–	13.0	4.6	22.0	2,3	-1.3	21	6.7	12.3	7.5	8.5	9.7	10.6	9.9	10.1	96	72	93	87	0.4	4.2	0.8	1.8	8.4	6.7	5.0	6.7
XI	–	–	–	–	5.4	1.8	13.9	5	-1.6	21	2.5	4.6	3.4	3.5	7.1	7.3	7.5	7.3	96	84	95	92	0.3	1.5	0.5	0.8	8.2	7.8	7.5	7.8
XII	–	–	–	–	-1.5	-6.8	6.6	12	-18.4	22	-5.8	-3.5	-4.6	-4.6	4.1	4.2	4.4	4.2	93	83	94	90	0.3	0.8	0.3	0.5	8.2	8.1	7.7	8.0
Rok	–	–	–	–	10.9	-	31.0	26.VII	-18.4	22.XII	5.5	9.8	6.4	7.0	9.0	9.4	9.4	9.3	89	72	89	83	1.2	4.7	1.3	2.4	7.3	7.5	6.4	7.1

Więcławice $\varphi = 52°51'$ $\lambda = 18°19'$

I	–	–	–	–	1.9	-1.6	5.8	22	-15.3	31	-0.7	1.0	-0.3	-0.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	-3.8	–	–	-13.2	1	-2.7	-0.4	-1.6	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	1.6	-4.4	11.6	31	-11.5	9	-3.2	0.9	-1.3	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	15.0	5.1	27.0	23	-0.3	30	7.3	13.3	9.1	9.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15.1	6.5	20.0	19	-1.5	1	9.2	13.7	10.6	11.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	19.7	9.1	30.9	16	2.7	3	13.0	18.1	14.3	14.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	20.7	10.4	30.0	26	6.5	29	13.7	19.2	15.4	15.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.1	11.9	28.5	12	7.4	10	14.4	19.4	16.0	16.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	17.2	7.7	29.0	4	2.8	25	9.6	16.0	12.2	12.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	13.0	5.1	21.0	2,3	-1.5	16	6.8	11.9	8.1	8.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	5.3	1.9	13.0	5	-2.3	18	2.8	4.4	3.4	3.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-2.5	-7.3	4.5	12	-19.5	21	-5.2	-3.6	-5.1	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	3.4	30.9	16.VI	-19.5	21.XII	5.4	9.5	6.7	7.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Krzyż $H_s = 31\,m$ 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R/R
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	37	8.5	12	1	4	14	·	–	–	1	19	14	10	·	3	1	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	49	15.6	16	2	9	22	·	–	–	·	16	13	8	2	2	10	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	26	7.3	12	·	4	27	·	–	–	3	12	11	8	·	2	11	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	33	10.2	16	·	·	4	2	–	–	5	9	10	8	1	3	1	2
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	129	20.8	28	·	·	3	·	–	–	·	12	21	20	4	3	·	3
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	49	11.7	19	·	·	·	6	–	–	5	8	12	9	1	1	·	4
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	54	10.0	3	·	·	·	4	–	–	2	10	14	13	1	3	·	3
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	65	11.1	15	·	·	·	3	–	–	1	8	13	12	2	·	·	1
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	66	10.6	18	·	·	·	2	–	–	5	6	15	14	1	7	·	1
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	48	7.4	31	·	·	12	·	–	–	3	12	6	5	·	12	·	1
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	27	7.6	1	·	·	10	·	–	–	2	20	11	7	·	9	2	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	40	12.3	11	7	17	25	·	–	–	4	19	11	6	1	5	7	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	593	20.8	28.V	10	34	117	17	–	–	31	151	151	120	13	50	32	15

Ciechocinek $H_s = 44\,m$ $h_w = 14\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R/R
I	6.5	3.1	5	3.7	2.5	2.2	4	2.5	11	3.1	36.5	4.3	17	3.7	10.5	3.0	·	3.7	21	10.0	25	2	4	19	·	3	1	2	21	12	7	1	3	10	·
II	4	5.8	15.5	4.9	7.5	4.1	2.5	2.2	5	1.7	15.5	7.5	21	4.5	13	4.0	·	4.8	23	6.5	5,12	1	9	25	·	5	2	2	17	17	4	·	2	13	·
III	17.5	3.8	16	2.3	12	2.2	12	3.3	5	2.0	9.5	2.0	5.5	1.5	10.5	2.9	5	2.4	37	11.2	6,12	4	6	26	·	1	·	6	12	10	5	2	2	13	·
IV	13.5	2.3	13	2.6	7.5	3.7	4	4.2	40.5	2.4	14	2.8	5.5	2.9	12	2.5	10	2.4	31	7.7	5	·	·	·	3	·	·	4	7	13	7	·	1	·	·
V	12.5	4.3	9	1.3	3.5	3.3	2	1.5	6.5	1.5	10	1.8	19	3.1	17.5	1.8	13	1.7	140	44.7	14	·	·	2	·	·	·	1	13	23	16	3	·	·	5
VI	19.5	3.5	4.5	2.6	2	1.5	1.5	1.0	1.5	1.7	8.5	2.7	22.5	3.7	19	2.7	11	2.7	51	16.8	30	·	·	·	6	3	1	4	10	11	9	2	1	·	2
VII	17	1.9	6.5	2.5	0.5	1.0	2	2.5	3.5	3.1	12	2.8	20	2.4	17.5	1.9	14	1.9	40	11.6	3	·	·	·	8	2	1	·	9	13	11	1	2	·	4
VIII	9.5	1.1	2.5	1.8	4	2.0	·	·	1.5	4.7	11	3.9	35.5	3.4	12	2.2	17	2.4	64	8.6	19	·	·	·	6	1	1	2	12	17	16	·	2	·	4
IX	4.5	1.7	10	1.4	7.5	2.3	2.5	2.2	4	1.9	10	3.2	28.5	2.6	8	2.0	15	1.9	73	23.0	18	·	·	·	1	·	·	2	9	15	13	3	3	·	3
X	12	1.5	9.5	1.2	13	1.7	4	2.1	2.5	1.8	5.5	1.5	17	3.1	11.5	1.1	18	1.5	21	5.1	31	·	·	5	·	·	·	2	9	6	6	·	11	·	·
XI	7.5	1.5	16.5	3.3	24	3.9	4.5	2.8	3	1.8	13.5	2.0	10	1.8	5	1.7	6	2.6	37	8.7	18	·	·	10	·	·	·	1	19	15	10	·	8	1	·
XII	11.5	1.3	13.5	2.7	10	1.8	8.5	1.1	6.5	3.2	12.5	3.8	16	2.1	8.5	1.7	6	2.1	12	5.0	15	10	17	27	·	·	·	3	20	15	3	·	6	16	·
Rok	135.5	2.4	121.5	2.5	94	2.5	47.5	2.1	60.5	2.4	158.5	3.2	217.5	2.9	145	2.3	115	2.5	550	44.7	14.V	17	36	114	24	15	6	29	158	167	107	12	41	53	18

Kobylec $H_s = 90\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R/R
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	29	11.1	25	2	4	15	·	–	–	2	21	8	6	1	–	–	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	59	10.2	16	2	8	25	·	–	–	·	18	12	9	1	–	–	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	33	12.7	5	–	5	–	·	–	–	3	12	7	5	2	–	–	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	53	14.2	16	·	·	1	1	–	–	2	11	13	10	1	–	·	4
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	104	27.9	28	·	·	1	·	–	–	·	14	20	17	2	–	·	4
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	53	8.6	30	·	·	·	6	–	–	3	4	12	10	·	–	·	3
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	32	5.4	4,14	·	·	·	5	–	–	2	8	11	10	·	–	·	3
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	116	42.3	15	·	·	·	2	–	–	2	10	15	12	4	–	·	1
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	60	49.7	18	·	·	·	1	–	–	4	9	10	9	2	–	·	1
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	14	8.9	31	·	·	2	·	–	–	3	14	6	2	·	–	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	36	15.2	1	·	·	8	·	–	–	3	18	9	6	1	–	–	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	27	7.8	11	10	17	26	·	–	–	3	22	9	6	·	–	–	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	616	42.3	15.VIII	–	34	–	15	–	–	27	161	132	102	14	–	–	16

Więcławice $H_s = 90\,m$ $h_w = 22.0\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R/R
I	1	2.0	9	2.4	·	·	8	3.0	·	·	40	3.0	16	3.9	10	2.8	9	2.8	22	13.5	25	2	5	19	·	·	·	–	–	9	4	1	1	–	·
II	7	4.9	11	3.8	9	4.0	3	3.3	2	1.5	25	4.0	18	5.6	5	4.8	4	4.2	16	5.0	12	2	–	26	·	3		–	–	12	4		1	–	·
III	6	1.4	17	2.4	8	4.2	15	3.0	10	2.1	5	3.4	11	1.9	6	5.0	15	2.4	21	13.6	6	1	10	28	·	·		–	–	9	4	1	·	–	·
IV	21	3.0	8	2.8	4	1.8	11	2.4	6	2.5	19	3.2	9	1.9	6	4.5	6	2.7	25	6.5	5	·	·	1	2		·	–	–	10	7	·	·	·	·
V	2	3.5	3	1.7	5	1.8	11	2.3	3	1.7	21	2.4	31	3.2	8	3.8	9	2.5	134	43.0	14	·	·	1	·	1	·	–	–	20	16	3	·	·	5
VI	8	4.9	6	4.3	1	2.0	6	2.2	2	1.5	17	2.1	34	3.1	12	3.2	4	2.9	57	21.0	29	·	·	·	5	·	·	–	–	10	7	2	·	·	3
VII	4	1.8	8	2.0	1	3.0	2	1.0	3	1.0	19	2.6	33	2.0	13	2.6	10	1.9	46	18.2	26	·	·	·	5	1	1	–	–	11	8	1	1	·	3
VIII	4	1.5	4	1.8	·	·	4	2.2	6	1.3	17	2.4	41	2.9	9	1.8	8	2.2	74	9.8	21	·	·	·	4		·	–	–	15	14	·	·	·	6
IX	·	·	·	·	8	2.4	7	1.7	5	1.8	13	2.3	36	2.6	5	3.2	16	2.0	95	46.5	18	·	·	·	1		·	–	–	13	8	1	2	·	4
X	2	1.5	1	1.0	5	1.4	16	1.8	3	1.0	5	2.2	25	2.1	12	1.9	24	1.4	34	15.0	31	·	·	3	·	·	·	–	–	6	4	2	6	·	·
XI	·	·	2	10.0	32	3.8	6	2.0	2	1.5	26	1.5	11	2.3	3	2.0	8	2.5	60	15.2	1	·	1	9	·	1	·	–	–	15	13	2	8	–	·
XII	13	2.5	8	1.9	14	3.4	2	2.0	2	2.0	16	2.5	29	2.1	3	1.7	6	2.2	2	0.8	9	12	17	27	·	·	·	–	–	6	·	·	4	–	·
Rok	68	2.2	77	2.8	87	2.3	91	2.2	44	1.5	223	2.6	294	2.8	92	3.1	119	2.5	586	46.5	18.IX	17	–	114	17	6	1	–	–	136	89	13	23	–	21

Szepietowo $\varphi = 52°51'$ $\lambda = 22°33'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.7	-3.9	6.9	21	-21.1	31	-2.0	-0.4	-1.9	-1.5	5.0	5.3	5.0	5.1	88	86	88	87	0.5	0.8	0.6	0.6	8.5	7.9	7.2	7.9
II	–	–	–	–	-1.4	-7.4	2.9	7	-17.0	1	-5.2	-2.6	-4.1	-4.0	3.9	4.5	4.2	4.2	86	87	88	87	0.5	0.7	0.5	0.6	9.1	8.0	7.9	8.3
III	–	–	–	–	-0.2	-8.1	4.3	31	-17.7	2.6	-6.3	-1.0	-3.9	-3.8	3.6	4.6	4.0	4.1	86	79	83	83	0.5	1.2	0.7	0.8	7.6	6.3	6.1	6.7
IV	–	–	–	–	14.5	5.5	26.5	22	-1.5	30	7.0	13.2	8.9	9.5	9.2	10.2	9.9	9.8	89	68	84	80	1.2	6.2	2.2	3.2	7.0	6.4	4.1	5.8
V	–	–	–	–	14.7	6.7	20.5	28	-1.9	1	8.8	13.1	10.1	10.5	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.4	7.5	7.8
VI	–	–	–	–	18.6	8.8	28.0	23	4.2	7	12.6	16.8	13.2	14.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.7	5.2	6.2
VII	–	–	–	–	20.7	10.6	27.2	22	6.8	4	13.8	18.9	14.7	15.5	13.8	13.3	13.9	13.7	87	61	83	77	2.2	9.0	3.0	4.7	6.0	6.6	5.7	6.1
VIII	–	–	–	–	21.2	11.5	29.5	13	7.7	10	13.9	19.4	15.4	16.0	14.2	14.7	15.2	14.7	89	66	86	80	1.9	8.4	2.8	4.4	6.4	7.2	6.5	6.7
IX	–	–	–	–	16.4	7.6	26.0	5	2.2	25	8.9	15.1	10.9	11.4	10.6	11.8	11.9	11.4	92	69	90	84	1.0	5.8	1.4	2.7	6.5	7.3	6.0	6.6
X	–	–	–	–	11.7	3.8	19.2	2	-2.2	16	5.1	10.7	7.0	7.4	8.4	10.0	9.3	9.2	93	77	91	87	0.6	3.1	0.9	1.5	7.9	7.2	5.4	6.8
XI	–	–	–	–	5.8	1.3	16.5	1	-2.8	18	2.6	4.6	3.4	3.5	6.9	7.1	7.2	7.1	91	83	90	88	0.6	1.7	0.8	1.0	9.0	8.6	8.5	8.7
XII	–	–	–	–	-3.1	-7.8	2.9	11	-21.9	21	-6.0	-4.6	-5.8	-5.6	3.6	3.9	3.7	3.7	81	80	82	81	0.7	0.8	0.7	0.7	8.2	8.0	7.2	7.8
Rok	–	–	–	–	10.0	2.4	29.5	13.VIII	-21.9	21.XII	4.4	8.6	5.7	6.1	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.4	6.4	7.1

Głodowo $\varphi = 52°50'$ $\lambda = 19°15'$

I	–	–	–	–	1.6	-2.3	7.7	22	-15.6	31	-0.8	0.7	-0.6	-0.3	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.7	7.1	7.6
II	–	–	–	–	0.0	-4.6	4.5	20	-13.8	1	-3.1	-1.0	-2.1	-2.1	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.7	7.6	8.4
III	–	–	–	–	1.4	-4.7	11.1	31	-13.0	15	-3.4	0.5	-2.0	-1.7	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.7	6.3	6.7
IV	–	–	–	–	14.8	5.1	27.7	23	0.2	30	8.1	13.7	8.7	9.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.4	5.7	6.6
V	–	–	–	–	14.1	6.3	19.7	8	-3.5	1	9.7	13.1	9.4	10.4	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.0	7.2	7.8
VI	–	–	–	–	19.6	9.1	29.8	16	2.3	3	12.9	18.1	13.3	14.4	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.8	6.2	6.7
VII	–	–	–	–	20.7	10.4	30.1	26	6.3	10	14.4	19.2	14.1	15.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.9	5.6	6.5
VIII	–	–	–	–	21.1	11.9	28.1	12	7.0	10	15.0	19.7	15.1	16.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	8.0	6.4	7.2
IX	–	–	–	–	16.7	7.8	28.2	4	2.9	15	10.1	15.7	10.8	11.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.4	5.3	6.7
X	–	–	–	–	12.7	4.3	20.5	4	-2.5	16	6.3	11.7	7.4	8.2	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.3	5.6	6.4
XI	–	–	–	–	5.0	1.6	11.7	4	-5.5	26	2.8	4.3	3.3	3.4	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.9	8.5	8.8
XII	–	–	–	–	-2.3	-7.4	3.8	10	-20.2	21,22	-5.4	-3.7	-5.4	-5.0	–	–	–	–	–	–	–	–	–	–	–	–	9.2	7.9	7.5	8.2
Rok	–	–	–	–	10.4	3.1	30.1	26.VII	-20.2	21,22.XII	5.6	9.3	6.0	6.7	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.6	6.6	7.3

Inowrocław $\varphi = 52°48'$ $\lambda = 18°14'$

I	–	–	–	–	2.5	-1.7	8.9	22	-13.7	31	-0.1	1.7	0.1	0.4	5.5	5.7	5.6	5.6	89	81	89	86	0.7	1.4	0.7	0.9	7.9	8.3	7.1	7.8
II	–	–	–	–	1.1	-4.0	5.9	20	-12.9	1	-2.1	-0.3	-1.6	-1.4	4.7	5.0	4.8	4.8	87	78	86	84	0.7	1.4	0.7	0.9	9.1	9.1	8.0	8.0
III	–	–	–	–	2.8	-3.9	12.9	31	-9.5	7	-2.1	2.1	-1.4	-0.7	4.5	5.1	4.6	4.7	83	70	82	78	0.8	2.2	1.0	1.3	6.5	6.6	6.3	6.5
IV	–	–	–	–	15.4	5.7	27.4	23	0.8	2	7.8	14.2	9.2	10.1	8.9	9.7	9.9	9.5	82	59	81	74	2.1	8.2	2.4	4.2	6.8	7.4	5.9	6.7
V	–	–	–	–	15.1	6.9	20.5	8	-2.1	1	9.4	14.2	9.7	10.8	10.6	11.3	10.7	10.9	95	70	87	84	1.3	5.3	1.6	2.7	8.7	9.0	6.6	8.1
VI	–	–	–	–	20.0	9.7	30.9	16	3.8	3	13.8	19.1	13.7	15.1	12.2	12.6	12.8	12.5	7.6	5.7	8.0	7.1	4.0	10.5	3.2	5.9	5.9	6.5	5.6	6.0
VII	–	–	–	–	21.6	10.9	31.1	26	7.5	4	14.8	20.3	14.7	16.1	14.2	14.4	14.0	14.2	8.4	6.1	8.3	7.6	2.9	10.2	3.1	5.4	7.3	7.5	4.7	6.5
VIII	–	–	–	–	21.7	12.4	29.3	12	8.8	9,29	15.3	20.6	15.2	16.6	14.9	15.5	14.9	15.1	8.5	6.4	8.6	7.8	2.7	9.4	2.6	4.9	6.4	8.2	5.7	6.8
IX	–	–	–	–	17.7	8.2	29.4	4	3.8	25	10.6	16.7	11.6	12.6	11.6	13.1	11.9	12.2	8.9	6.9	8.6	8.1	1.4	6.6	2.0	3.3	7.3	7.1	4.3	6.2
X	–	–	–	–	13.2	5.1	21.6	2,3	-0.6	21	6.8	12.5	7.8	8.7	9.2	10.8	9.6	9.9	9.1	7.3	8.8	8.4	0.9	4.2	1.3	2.1	8.3	6.6	3.9	6.3
XI	–	–	–	–	5.6	2.3	13.4	5	-1.4	18	3.3	5.0	3.7	3.9	7.2	7.5	7.4	7.4	9.1	8.4	9.1	8.9	0.7	1.5	0.7	1.0	9.0	8.7	7.9	8.5
XII	–	–	–	–	-2.2	-6.9	5.4	12	-19.3	21	-4.7	-2.9	-4.8	-4.3	4.1	4.2	4.1	4.1	8.7	7.8	8.5	8.3	0.5	1.0	0.6	0.7	8.2	8.2	8.0	8.1
Rok	–	–	–	–	11.2	3.7	31.1	26.VII	-19.3	21.XII	6.1	10.3	6.5	7.4	9.0	9.6	9.2	9.3	8.7	7.0	8.5	8.1	1.6	5.2	1.7	2.8	7.6	7.8	6.0	7.1

Bielsk Podlaski $\varphi = 52°47'$ $\lambda = 23°11'$

I	–	–	–	–	0.7	-3.6	6.0	22	-21.3	31	-2.0	-0.1	-1.6	-1.3	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.9	7.8	8.2
II	–	–	–	–	-1.4	-7.5	2.6	12	-18.2	1	-5.0	-2.4	-4.0	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.3	6.8	7.9
III	–	–	–	–	0.2	-8.4	6.8	31	-19.2	26	-6.6	-0.7	-4.3	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.1	6.6	6.3	7.0
IV	–	–	–	–	14.6	5.1	27.0	22	-1.0	30	7.2	13.4	8.8	9.6	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.7	5.3	6.9
V	–	–	–	–	15.2	6.8	21.8	28	-1.5	1	9.2	14.0	10.3	11.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.2	6.6	7.6
VI	–	–	–	–	18.8	8.6	27.1	23	2.2	3	12.8	17.3	12.6	13.8	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.6	6.3	6.9
VII	–	–	–	–	20.9	10.2	27.2	22	6.5	31	14.2	19.6	14.5	15.7	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.5	5.8	6.6
VIII	–	–	–	–	21.2	11.3	29.8	13	6.3	10	14.2	20.1	15.3	16.2	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.2	5.9	6.6
IX	–	–	–	–	17.0	7.6	26.3	5	1.9	25	9.4	15.6	10.9	11.7	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.8	5.1	6.5
X	–	–	–	–	12.2	3.6	20.3	2	-2.7	16	5.2	11.6	6.6	7.5	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.3	5.9	7.3
XI	–	–	–	–	6.4	1.8	18.3	1	-2.4	27	3.1	5.3	3.9	4.0	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.4	8.7	8.8
XII	–	–	–	–	-3.2	-8.0	3.8	10	-23.5	21	-5.9	-4.3	-5.6	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.0	7.4	7.9
Rok	–	–	–	–	10.2	2.3	29.8	13.VIII	-23.5	21.XII	4.6	9.1	5.6	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.7	6.5	7.3

Szepietowo $H_s = 150\ m$ $h_w = 14\ m$ 1962

MIESIĄC	ROZKŁAD WIATRU (n, v) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	◐	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R
I	3	4.8	3	4.5	4	1.8	3	2.2	17.5	3.2	34	3.8	27.5	4.6	1	2.0	·	3.8	23	9.3	25	3	6	22	·	·	·	1	18	13	6	·	3	21	·
II	14	4.6	2	3.5	8.5	2.5	4.5	4.2	8.5	3.5	16.5	6.3	24.5	5.8	1.5	3.3	4	4.7	33	8.2	25	8	17	28	·	5	2	·	17	13	8	·	3	28	·
III	13.5	5.0	12	1.8	10.5	2.0	16.5	3.5	12	3.1	10	3.2	12	4.6	2.5	4.0	4	3.3	45	6.5	12,17	12	17	28	·	4	1	5	16	13	9	·	1	31	·
IV	11	2.1	8	2.8	7	2.3	16.5	3.3	19.5	2.1	11	2.1	5	4.0	7	5.0	6	2.7	37	9.1	12	·	·	2	3	1	·	4	7	10	8	·	2	1	3
V	12	2.5	0.5	2.0	3	2.2	7	3.1	10.5	2.6	15.5	3.1	30	3.6	5.5	4.9	9	2.7	88	10.6	15	·	·	2	·	·	·	1	15	18	16	3	1	·	3
VI	21	4.8	1	5.0	·	·	1	2.0	11	2.0	9	3.6	32.5	3.6	8.5	2.9	6	3.3	87	47.4	4	·	·	·	3	3	·	3	10	14	10	2	·	·	2
VII	19	2.7	1.5	3.3	1	2.0	1.5	2.7	10.5	3.1	12.5	2.5	34	4.1	8	4.6	5	3.3	33	10.7	13	·	·	·	5	·	·	2	7	11	7	1	·	·	3
VIII	6	3.8	·	·	·	·	6	3.5	11	4.0	16.5	3.8	50	3.9	1.5	4.7	2	3.8	108	29.5	15	·	·	·	6	2	·	·	10	15	13	3	1	·	3
IX	4	2.5	2	2.0	10.5	1.5	9.5	2.1	21.5	4.0	11.5	3.8	21	4.1	10	5.2	·	3.5	66	21.5	17	·	·	·	1	2	·	1	10	14	10	2	6	·	1
X	11	1.6	1	2.0	2	1.5	12	2.0	17.5	2.8	7	2.7	27.5	4.0	7	2.7	8	2.6	3	1.6	27	·	·	5	·	2	·	1	13	7	1	·	10	·	·
XI	7.5	1.8	1	6.5	10	5.4	33	5.8	6	3.5	4	3.1	15.5	3.8	8	1.9	5	4.1	65	13.0	15	·	·	13	·	6	·		24	15	11	1	8	1	·
XII	15	1.9	12	1.9	5	1.0	6.5	2.6	18.5	2.5	11	5.1	21.5	3.3	2.5	2.6	1	2.7	12	4.6	14	11	19	28	·	1	·	2	19	11	3	·	3	17	·
Rok	137	3.2	44	2.9	61.5	1.8	117	3.1	164	3.0	158.5	3.6	301	4.1	63	3.4	49	3.4	600	47.4	4.VI	34	59	128	18	26	3	20	166	154	102	12	38	99	15

Głodowo $H_s = 129\ m$ $h_w = 10\ m$

I	4	7.5	5	6.0		·	4	3.2	20	3.7	30	5.2	25.5	4.8	3.5	4.4	1	4.7	25	12.7	25	3	6	19	·	1	·	1	12	9	5	1	1	–	·
II	3	5.0	7	5.1	13	5.2	4	3.0	8	3.2	12.5	4.6	14.5	4.1	14	5.7	8	4.2	25	7.4	5	2	13	24	·	2	·	·	19	8	6	·	7	–	·
III	12	3.8	6	4.0	15	3.9	16	4.1	15.5	2.1	9.5	4.8	8	2.8	8	6.6	3	3.4	30	12.4	5	3	9	27	·	2	·	3	14	10	6	1	–	–	·
IV	11	3.3	8	3.4	9	5.2	7.5	6.0	10.5	3.2	15	3.3	12.5	3.6	5.5	6.3	11	3.5	39	10.2	13	·	·	·	4	4	·	2	10	14	8	1	–	·	1
V	1.5	2.0	3.5	2.1	1	3.0	10.5	3.0	17	2.1	19.5	3.2	19	3.5	9	4.7	12	2.7	185	70.4	14	·	·	2	·	·	·	·	15	21	18	4	2	·	4
VI	10	5.2	4	2.2	1	4.0	6	1.8	3	2.3	18.5	2.9	19.5	4.5	19	3.0	9	3.1	47	13.1	29	·	·	·	6	2	·	1	10	9	9	2	2	·	1
VII	6	2.8	2	1.5	7	1.7	3	2.0	11	1.5	25	2.8	21	3.3	11	2.7	7	2.4	58	20.9	16	·	·	·	4	3	1	1	9	11	8	2	3	·	4
VIII	3	3.0	2	3.5	4	3.8	5	3.2	8	2.1	14.5	3.3	39	5.1	6.5	3.2	11	3.6	56	12.0	17	·	·	·	6	2	·	1	12	17	13	2	5	·	3
IX	·	·	1	4.0	5	4.2	8	3.0	11.5	2.0	12.5	2.4	33.5	4.0	8.5	4.2	10	3.0	73	20.9	16	·	·	·	1	·	·	2	10	17	14	2	10	·	2
X	3	2.0	2	1.5	·	·	18	2.2	7	1.3	9	1.8	22	3.8	4	4.8	28	1.9	18	8.4	28	·	·	5	·	·	·	2	12	7	5	·	13	·	1
XI	0.5	4.0	1.5	2.0	21	6.6	19.5	5.5	6.5	2.2	12	3.2	18	2.8	2	2.5	9	4.0	39	8.7	20	·	1	10	·	4	·	1	23	15	11	·	7	–	·
XII	·	·	13	3.0	10	3.8	10	4.1	8	2.8	24	5.2	21	2.6	3	1.3	4	3.4	12	5.5	15	10	18	27	·	·	·	1	21	7	3	·	7	–	·
Rok	54	3.2	55	2.9	86	3.2	111.5	3.4	126	2.4	202	3.3	253.5	3.7	94	4.1	113	3.3	607	70.4	14.V	18	47	114	21	20	1	15	167	145	106	15	–	–	16

Inowrocław $H_s = 90\ m$ $h_w = 15\ m$

I	5	3.3	5	2.9	4	2.4	2	2.3	8.5	5.0	35.5	4.8	25.5	3.6	7.5	2.5	·	4.0	49	6.8	25	2	4	20	·	3	·	2	19	8	6	·	2	10	·
II	8.5	5.5	8	3.8	9.5	3.5	5.5	3.5	8	3.1	14	5.5	19	5.6	11.5	4.3	·	4.6	28	9.4	12	2	10	24	·	5	1	·	14	14	9	·	1	12	1
III	12	3.1	14	3.0	9.5	2.6	23	3.3	4.5	2.2	11	2.2	9	2.4	10	2.8	·	2.9	24	9.8	6	·	5	27	·	2	·	4	14	10	6	·	1	13	·
IV	5.5	2.8	12.5	3.0	7	3.6	12.5	3.0	11.5	3.0	25	3.1	9.5	2.7	6.5	3.6	·	3.1	24	5.7	5	·	·	·	3	1	·	1	7	10	8	·	·	·	·
V	3	2.5	7	2.1	7.5	2.1	12.5	3.0	7	2.9	24	2.5	16.5	2.7	15.5	3.6	·	2.9	91	31.0	14	·	·	1	·	2	·	·	16	21	17	2	·	·	5
VI	13	4.5	5.5	3.9	·	–	6	3.7	7.5	3.8	20	3.1	26.5	4.0	11.5	2.7	·	3.6	38	12.0	30	·	·	·	5	2	·	3	12	11	8	1	·	·	4
VII	5.5	4.8	10.5	1.9	3.5	2.1	6	2.0	6	2.4	24	3.4	18.5	3.2	15	2.6	4	2.6	44	15.5	26	·	·	·	5	2	·	1	11	12	8	1	2	·	2
VIII	5.5	1.5	5.5	1.9	2.5	1.8	7	3.0	4	3.6	24	4.5	32	4.0	9.5	2.4	3	3.4	44	8.8	21	·	·	·	6	1	·	1	13	17	12		·	·	3
IX	2	1.5	3	1.3	8	1.5	13	3.0	5.5	2.9	22.5	3.5	25.5	3.8	10.5	3.1	·	3.1	55	27.0	18	·		·	1	3	·	3	9	14	8	1	2	·	2
X	6.5	1.2	3	1.2	6	2.3	19.5	2.4	10	2.8	14	3.5	20.5	2.9	10.5	1.9	3	2.5	24	13.4	31	·	·	4	·	1	·	1	8	8	4	1	6	·	·
XI	3	3.0	6	4.8	23	4.5	16.5	4.9	5.5	2.8	29	2.8	7	3.3	·	·	·	3.8	50	14.2	1	·	·	9		4	·	1	22	13	10	1	2	1	·
XII	8.5	1.9	18	2.1	6.5	2.2	13	2.5	11.5	3.9	15	5.8	15.5	3.3	5	3.4	·	3.2	16	5.2	15	10	17	26		2	·	2	23	10	4	·	5	16	·
Rok	78	2.7	98	2.7	87	2.4	136.5	3.0	89.5	3.2	258	3.7	225	3.5	113	2.7	10	3.3	457	31.0	14.V	14	36	111	20	28	1	19	168	148	100	7	21	52	17

Bielsk Podlaski $H_s = 145\ m$ $h_w = 12{,}5\ m$

I	5	4.5	4	1.9	·	·	6	3.0	16.5	2.9	39.5	3.6	16	4.3	5	2.8	1	3.4	32	10.2	25	2	10	22	·	·	·	1	20	14	9	1	1	21	·
II	7.5	3.0	5	4.0	8	2.4	6	3.5	12.5	5.4	17.5	6.5	10	6.7	11.5	4.7	6	4.6	57	11.2	16	8	16	28	·	5	3	·	13	17	12	1	1	28	·
III	13	4.2	13	2.2	2.5	2.0	20	4.4	4.5	3.7	6.5	3.0	7	4.5	13.5	3.4	13	3.1	51	9.3	16	10	11	28	·	2	1	2	17	14	10	·	·	31	·
IV	7.5	1.3	9.5	3.2	4	2.8	14	3.6	9	2.6	13	2.5	7.5	3.4	17.5	2.1	8	2.4	53	10.2	7	·	·	3	3	·	·	1	9	15	11	1	3	2	1
V	7.5	1.3	4	2.2	2.5	2.6	8.5	2.9	5.5	2.2	12	3.0	26.5	2.6	20.5	1.9	6	2.2	99	17.8	24	·	·	2	·	·	·	1	15	16	13	3	1	·	2
VI	16.5	3.2	2	5.0	0.5	3.0	3.5	1.6	4.5	2.3	13	2.4	30	3.4	13	1.8	7	2.6	104	39.0	4	·	·	·	2	·	·	1	10	16	13	4	·	·	3
VII	7.5	1.8	2	3.0	·	·	1	5.0	8	2.5	22.5	2.2	27	3.0	16	2.5	9	2.3	38	7.2	3	·	·	·	5	·	·	1	8	15	10	·	·	·	4
VIII	1	5.0	1	4.0	1	4.0	2	4.0	13	2.4	25	3.2	31	3.3	10	2.0	9	2.7	76	14.5	15	·	·	·	5	1		·	12	15	10	4	2	·	4
IX	5.5	1.4	1	1.0	·	·	3	2.3	12.5	1.7	23	3.8	28.5	3.0	8.5	2.0	8	2.5	74	19.3	17	·	·	·	1	·	·	2	9	13	12	2	5	·	4
X	2	1.0	2	1.8	2	1.8	11	2.5	7	1.9	15.5	2.7	21.5	3.1	18	1.5	14	2.0	6	2.4	27	·	·	5	·	1	·	2	13	9	2	·	8	·	·
XI	3.5	2.4	10	5.3	6.5	4.5	26	4.5	7.5	3.4	6	2.7	13.5	3.4	10	2.0	7	3.5	52	8.5	15	·	·	8	·	2	·	1	23	16	14	·	8	1	·
XII	14	1.7	5	3.0	·	·	4.5	1.2	11	4.7	19	3.5	16.5	2.9	16	2.4	7	2.7	20	7.4	14	12	17	29	·	1	·	2	20	14	3	·	2	17	·
Rok	90.5	2.6	58.5	2.8	27	1.7	105.5	3.2	111.5	3.0	212.5	3.3	235	3.6	159.5	2.4	95	2.8	662	39.0	4.VI	32	54	125	16	12	4	14	169	174	119	16	31	100	18

Gorzów Wlkp. $\varphi = 52°44'$ $\lambda = 15°15'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T											ŚREDNIA PREŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1007.8	1033.7	979.0	1014.6	3.8	-0.8	9.5	22	-12.5	31	0.7	2.6	1.4	1.5	5.9	6.0	5.9	5.9	89	80	85	85	0.8	1.6	1.1	1.2	7.6	8.5	8.2	8.1
II	1008.7	1034.1	975.5	1016.3	2.2	-2.7	7.6	20	-11.8	1	-1.1	1.0	-0.3	-0.2	5.0	5.4	5.1	5.2	87	81	84	84	0.8	1.3	1.0	1.0	8.3	8.5	7.3	8.0
III	1003.8	1024.2	975.8	1011.3	4.1	-2.9	14.5	30	-7.2	14	-2.0	3.0	0.4	0.4	5.0	5.2	5.0	5.1	92	67	77	79	0.4	2.6	1.5	1.5	7.3	6.8	5.6	6.6
IV	1005.9	1020.0	978.7	1013.2	15.1	5.1	27.1	25	0.4	1	6.2	12.8	9.5	9.5	8.8	9.5	9.4	9.2	91	64	77	77	1.0	6.4	3.3	3.6	7.3	7.7	5.2	6.7
V	1005.3	1010.9	998.3	1012.6	14.8	6.9	21.1	7	0.3	1	8.4	12.8	10.2	10.4	10.1	10.0	10.5	10.2	91	67	83	80	1.0	5.2	2.1	2.8	7.8	8.2	7.3	7.8
VI	1011.5	1024.7	999.7	1018.7	19.7	9.3	29.7	15	2.9	3	12.2	17.6	14.5	14.7	11.6	11.8	11.9	11.8	79	58	70	69	3.1	9.5	5.1	5.9	5.5	7.1	6.0	6.2
VII	1007.0	1017.6	987.3	1014.2	20.7	10.8	29.7	26	7.1	29	13.0	18.7	14.9	15.4	13.7	13.6	14.2	13.8	91	64	83	79	1.5	8.6	3.0	4.4	7.3	7.3	6.2	6.9
VIII	1007.5	1017.0	995.2	1014.7	20.7	11.7	29.8	12	7.9	10	13.3	19.1	15.4	15.8	14.0	14.3	14.5	14.3	91	65	83	80	1.3	8.3	3.2	4.3	7.5	8.5	5.8	7.3
IX	1008.3	1024.4	988.1	1015.6	17.5	8.3	25.3	4	4.6	25	9.3	15.9	12.0	12.3	11.1	12.2	12.0	11.8	94	68	85	82	0.7	6.4	2.3	3.1	7.3	6.9	4.4	6.2
X	1014.5	1028.8	1000.5	1021.9	12.9	5.3	23.2	2	-0.3	24	6.3	11.6	8.6	8.8	9.4	11.0	10.2	10.2	96	79	90	88	0.4	3.2	1.5	1.7	8.2	7.3	4.6	6.7
XI	1008.6	1027.1	989.9	1016.1	5.6	1.7	15.9	8	-4.0	25	2.7	4.7	3.2	3.4	7.2	7.5	7.3	7.3	96	87	93	92	0.3	1.3	0.6	0.7	8.4	8.4	7.5	8.1
XII	1008.8	1039.6	961.7	1016.6	-1.5	-5.9	6.4	12	-16.9	22	-4.2	-2.6	-3.5	-3.4	4.6	4.8	4.5	4.6	92	89	90	90	0.3	0.5	0.4	0.4	7.8	8.2	6.7	7.6
Rok	1008.1	1039.6	961.7	1015.6	11.3	3.9	29.8	12.VIII	-16.9	22.XII	5.4	9.8	7.2	7.4	8.9	9.3	9.2	9.1	91	72	83	82	1.0	4.6	2.1	2.6	7.5	7.8	6.2	7.2

Kołuda Wielka $\varphi = 52°44'$ $\lambda = 18°09'$

I	-	-	-	-	2.4	-2.3	9.0	22	-16.0	31	-0.6	1.6	-0.4	0.0	-	-	-	-	-	-	-	-	-	-	-	-	8.0	7.8	7.6	7.8
II	-	-	-	-	4.0	-4.2	5.7	20	-13.8	1	-2.5	0.1	-1.9	-1.6	-	-	-	-	-	-	-	-	-	-	-	-	8.4	8.5	6.8	7.9
III	-	-	-	-	2.8	-4.6	13.5	31	-12.3	7	-2.7	2.2	-1.7	-1.0	-	-	-	-	-	-	-	-	-	-	-	-	6.6	6.6	6.5	6.6
IV	-	-	-	-	15.8	4.8	29.3	23	0.0	6	7.4	14.5	8.4	9.7	-	-	-	-	-	-	-	-	-	-	-	-	6.9	6.8	5.5	6.4
V	-	-	-	-	15.5	6.5	21.1	19	-2.1	1	9.2	14.0	9.3	10.4	-	-	-	-	-	-	-	-	-	-	-	-	7.0	7.9	6.9	7.3
VI	-	-	-	-	20.9	9.2	31.6	16	3.4	3	13.9	19.2	13.0	14.8	-	-	-	-	-	-	-	-	-	-	-	-	5.0	5.2	5.2	5.1
VII	-	-	-	-	21.7	10.4	32.1	26	5.7	4	14.6	20.2	14.2	15.8	-	-	-	-	-	-	-	-	-	-	-	-	5.4	5.4	4.9	5.2
VIII	-	-	-	-	22.2	11.9	31.2	12	7.5	10	15.2	20.7	15.3	16.6	-	-	-	-	-	-	-	-	-	-	-	-	6.0	7.4	6.9	6.8
IX	-	-	-	-	17.3	7.8	31.1	4	3.2	25	10.2	16.7	11.1	12.3	-	-	-	-	-	-	-	-	-	-	-	-	6.1	6.9	4.5	5.8
X	-	-	-	-	13.7	4.5	23.1	3	-1.7	16	6.4	12.9	7.3	8.5	-	-	-	-	-	-	-	-	-	-	-	-	6.9	5.7	4.6	5.7
XI	-	-	-	-	5.5	1.8	14.4	4	-2.0	18	3.0	4.8	3.3	3.6	-	-	-	-	-	-	-	-	-	-	-	-	8.4	8.5	8.0	8.3
XII	-	-	-	-	-2.2	-7.5	4.8	12	-19.5	22	-4.9	-3.2	-5.0	-4.5	-	-	-	-	-	-	-	-	-	-	-	-	8.8	7.6	6.5	7.6
Rok	-	-	-	-	11.4	3.2	32.1	26.VIII	-19.5	22.XII	5.8	10.3	6.1	7.1	-	-	-	-	-	-	-	-	-	-	-	-	7.0	7.0	6.2	6.7

Pułtusk $\varphi = 52°42'$ $\lambda = 21°06'$

I	-	-	-	-	1.6	-3.1	9.1	22	-19.9	31	-1.3	0.7	-1.3	-0.8	-	-	-	-	-	-	-	-	-	-	-	-	7.9	7.2	6.8	7.3
II	-	-	-	-	0.1	-6.0	5.1	7	-17.5	1	-4.4	-1.2	-3.2	-3.0	-	-	-	-	-	-	-	-	-	-	-	-	8.2	8.3	7.1	7.9
III	-	-	-	-	1.7	-6.1	10.1	31	-15.2	15	-5.1	0.5	-2.3	-2.3	-	-	-	-	-	-	-	-	-	-	-	-	7.4	7.0	6.8	7.1
IV	-	-	-	-	16.0	6.1	28.9	23	-0.2	3	7.5	14.6	9.8	10.4	-	-	-	-	-	-	-	-	-	-	-	-	6.4	6.2	4.0	5.5
V	-	-	-	-	15.4	7.1	20.8	13	-2.1	1	8.9	13.6	11.0	11.1	-	-	-	-	-	-	-	-	-	-	-	-	7.9	7.7	7.2	7.6
VI	-	-	-	-	19.8	10.1	29.9	16	6.1	10	13.1	18.2	14.2	14.9	-	-	-	-	-	-	-	-	-	-	-	-	6.2	5.9	5.3	5.8
VII	-	-	-	-	21.7	11.3	30.3	26	6.5	31	13.9	20.1	15.8	16.4	-	-	-	-	-	-	-	-	-	-	-	-	6.7	5.9	5.0	5.9
VIII	-	-	-	-	21.9	11.9	30.7	7	6.7	10	14.2	20.3	15.9	16.6	-	-	-	-	-	-	-	-	-	-	-	-	7.4	5.9	5.0	6.1
IX	-	-	-	-	17.3	7.6	26.9	4	2.8	26	9.3	15.7	11.4	12.0	-	-	-	-	-	-	-	-	-	-	-	-	7.3	6.7	5.2	6.4
X	-	-	-	-	13.1	3.7	21.2	2	-4.0	16	5.2	11.9	6.9	7.7	-	-	-	-	-	-	-	-	-	-	-	-	6.4	6.6	4.9	6.0
XI	-	-	-	-	6.0	1.7	13.6	1	-2.5	26	2.9	5.0	3.6	3.8	-	-	-	-	-	-	-	-	-	-	-	-	8.9	8.7	8.9	8.8
XII	-	-	-	-	-2.5	-7.0	4.2	11	-20.6	21	-5.3	-3.6	-4.9	-4.7	-	-	-	-	-	-	-	-	-	-	-	-	8.9	8.1	6.8	7.9
Rok	-	-	-	-	11.0	3.1	30.7	7.VIII	-20.6	21.XII	4.9	9.6	6.4	6.8	-	-	-	-	-	-	-	-	-	-	-	-	7.5	7.0	6.1	6.9

Białowieża $\varphi = 52°42'$ $\lambda = 23°51'$

I	995.1	1020.8	973.6	1014.8	0.5	-4.1	4.6	22	-23.6	31	-2.4	-0.3	-1.9	-1.6	4.9	5.1	4.9	5.0	89	83	88	87	0.5	1.0	0.7	0.7	8.8	8.2	8.2	8.4
II	994.1	1013.1	959.6	1014.9	-1.3	-8.3	2.8	13	-18.2	1	-5.5	-2.8	-4.4	-4.3	3.8	4.1	4.0	4.0	89	79	87	85	0.5	1.0	0.6	0.7	9.3	8.7	7.1	8.4
III	991.6	1009.9	969.0	1012.3	-0.3	-9.6	8.1	31	-20.7	21	-7.5	-0.7	-4.2	-4.2	3.5	4.3	4.1	4.0	89	71	86	82	0.3	1.6	0.6	0.8	7.8	6.7	6.3	6.9
IV	994.9	1010.8	974.2	1014.7	14.5	3.9	25.8	21	-2.3	2	6.5	13.2	8.1	9.0	8.7	9.0	9.2	9.0	88	64	83	78	1.3	7.6	2.1	3.7	6.9	6.8	5.0	6.2
V	992.6	1001.1	974.6	1012.2	15.4	5.7	25.0	27	-2.5	3	9.0	14.0	10.1	10.8	10.5	10.4	11.1	10.7	89	64	88	80	1.3	6.3	1.6	3.1	8.3	8.6	5.4	7.4
VI	996.9	1006.8	985.5	1016.3	18.5	7.7	27.3	23	2.6	3,6	12.5	17.0	12.6	13.7	11.6	11.0	11.9	11.5	79	58	80	72	3.4	9.3	3.1	5.3	6.0	7.4	4.5	6.0
VII	994.0	1004.0	981.7	1013.3	20.3	9.5	27.3	27	5.0	31	13.9	18.7	14.2	15.2	13.4	13.0	13.6	13.3	84	61	84	76	2.6	9.1	2.8	4.8	5.8	6.4	5.1	5.8
VIII	995.4	1005.4	985.3	1014.7	21.1	10.9	29.2	13	5.3	10	13.9	19.4	14.9	15.8	14.1	14.0	14.7	14.3	88	62	86	79	2.0	9.4	2.6	4.7	6.2	7.0	4.4	5.9
IX	996.1	1013.0	978.1	1015.7	16.5	7.2	26.8	5	0.2	26	9.1	15.3	10.6	11.4	10.8	11.6	11.7	11.4	92	67	90	83	1.0	6.3	1.4	2.9	6.8	6.7	4.5	6.0
X	1002.4	1017.0	985.0	1022.5	11.7	2.5	18.9	2	-4.7	16	4.1	10.9	5.9	6.7	7.9	9.3	8.7	8.6	94	70	92	85	0.5	4.2	0.7	1.8	7.7	6.5	4.8	6.3
XI	999.6	1012.0	983.9	1019.9	6.3	1.6	18.2	1	-2.0	18	2.6	5.2	3.6	3.8	7.1	7.5	7.4	7.3	93	84	90	89	0.5	1.8	0.8	1.0	8.7	8.2	8.7	8.5
XII	996.4	1025.6	959.9	1017.4	-3.2	-8.5	2.5	5	-24.8	21	-6.3	-4.3	-6.2	-5.8	3.8	4.0	3.8	3.9	88	82	87	86	0.5	0.8	0.5	0.6	7.9	8.0	7.0	7.6
Rok	995.8	1025.6	959.6	1016.8	10.0	1.5	29.2	13.VIII	-24.8	21.XII	4.2	8.8	5.3	5.9	8.3	8.6	8.8	8.6	88	70	87	82	1.2	4.9	1.5	2.5	7.5	7.4	5.9	6.9

Gorzów Wlkp. $H_s = 65\,m$ $H_b = 59{,}7\,m$ $h_w = 12\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU °D, °mD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◉	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R f0
I	6	5.5	5.5	3.0	2	1.5	4	3.4	8.5	3.3	18	3.1	37	3.9	12	4.0	·	3.7	33	7.4	24	1	4	10	·	2	·	1	18	21	8	·	4	4	·
II	8.5	6.6	7.5	5.9	13	5.6	1.5	2.7	0.5	3.0	12.5	4.1	19.5	5.0	21	5.5	·	5.3	63	20.4	12	1	7	23	·	5	4	·	17	18	11	2	2	14	2
III	11	3.6	17	2.5	9.5	3.2	16.5	3.8	4	2.9	3	2.0	12.5	1.9	19.5	2.5	·	2.8	31	11.5	12	·	3	28	·	1	·	5	16	13	8	1	2	10	·
IV	16	3.6	10.5	4.3	12.5	3.6	4	3.6	4.5	2.7	10.5	2.8	18	3.1	14	2.8	·	3.3	46	11.3	28	·	·	·	3	1	·	3	10	14	9	1	·	·	1
V	17.5	2.8	6	2.6	7	2.5	3.5	2.4	2	3.8	7.5	3.1	20.5	2.6	29	3.2	·	2.9	87	11.3	12	·	·	·	·	-	·	·	15	23	18	1	·	·	7
VI	18.5	3.3	11.5	2.9	1.5	2.3	2.5	3.8	·	·	3	3.3	22.5	3.5	30.5	3.7	·	3.4	29	7.4	15	·	·	·	6	2	·	2	8	13	9	·	·	·	3
VII	21.5	4.7	11	1.6	4.5	2.3	1.5	5.3	0.5	6.0	4.5	4.6	25	3.2	24.5	2.5	·	2.5	46	8.7	4	·	·	·	3	1	1	2	13	15	11	·	1	·	2
VIII	11.5	1.7	3.5	2.4	2.5	2.8	2	3.0	2	3.2	9.5	3.3	42	3.3	20	2.6	1	2.9	55	11.0	24	·	·	·	3	-	·	1	13	15	9	2	·	·	4
IX	2	2.0	2	2.2	16.5	3.3	6	4.2	1.5	1.3	8	3.7	26	2.7	27	2.6	·	2.9	45	11.7	18	·	·	·	2	3	·	2	9	17	11	1	5	·	2
X	12.5	2.0	8	1.2	19	2.3	7	1.5	4.5	1.2	6	1.5	17	2.4	19	3.0	·	2.2	17	13.2	4	·	·	3	·	-	·	1	13	6	3	1	13	·	1
XI	4	1.5	5	3.6	34	4.1	6.5	3.5	2.5	2.2	12	1.4	22	2.0	4	3.4	·	3.0	19	3.6	18	·	·	10	·	3	·	·	18	13	7	·	12	5	·
XII	5	2.7	15.5	2.6	12	4.2	6	1.5	2.5	4.0	14	2.1	28	2.5	10	1.8	·	2.6	30	9.4	11	7	18	26	·	·	·	2	18	11	6	·	9	7	·
Rok	134	3.1	103	2.9	134	3.1	61	3.2	33	2.8	108.5	2.9	290	3.0	230.5	3.1	1	3.1	501	20.4	12.II	9	32	100	17	18	5	19	168	179	110	9	48	40	22

Kołuda Wielka $H_s = 85\,m$ $h_w = 12\,m$

I	2.5	2.2	2	1.0	·	·	2.5	2.2	21.5	2.9	32	3.0	17	2.3	8.5	2.7	7	2.5	21	7.4	25	3	4	21	·	·	·	1	21	11	5	·	1	3	-
II	6	2.0	2	1.5	2	2.5	2.5	2.6	12.5	3.2	14	4.8	24	3.9	16	3.2	5	3.3	31	10.1	12	2	11	25	·	3	·	·	16	11	8	1	1	19	-
III	5	2.2	2	1.0	7	2.1	8	2.5	6	1.8	7	1.4	19	2.2	20	2.1	19	1.6	33	12.7	5	2	7	28	·	·	·	3	10	9	5	1	3	16	-
IV	1.5	2.7	2.5	2.6	6.5	1.8	3.5	2.0	9	3.0	14.5	2.2	14.5	2.0	20	2.2	18	1.8	23	9.6	28	·	·	·	6	·	·	2	9	10	7	·	·	·	-
V	1	2.0	0.5	1.0	1	2.0	4	2.4	12	1.5	14	1.9	33	2.2	9.5	2.8	18	1.7	107	34.7	14	·	·	1	·	·	·	1	3	21	17	2	·	·	-
VI	·	·	2	2.0	1	3.0	3	2.0	6	2.0	13.5	2.1	40	2.2	12.5	2.7	12	2.0	53	18.3	30	·	·	·	7	·	·	4	6	12	9	1	·	·	-
VII	0.5	1.0	0.5	1.0	1.5	1.7	3	1.0	9	1.4	14.5	1.9	27.5	1.9	7.5	1.5	29	1.2	44	10.2	2	·	·	·	6	·	·	6	5	11	9	1	1	·	-
VIII	·	·	2	1.5	·	·	5	1.4	5	2.2	23.5	3.0	29.5	2.0	4	1.2	24	1.7	47	7.3	4	·	·	·	10	·	·	1	14	15	11	·	·	·	-
IX	1.5	1.0	1.5	3.0	5	1.3	2	2.2	7.5	2.3	15	2.8	30.5	2.3	2	1.5	25	1.7	65	23.9	18	·	·	·	2	·	·	5	7	13	10	2	1	·	-
X	·	·	·	·	5	1.2	7.5	1.7	11	2.0	8.5	2.3	21	1.7	9	1.6	31	1.2	24	14.3	31	·	·	4	·	·	·	4	9	7	4	1	7	·	-
XI	8.5	1.9	10.5	1.7	10	2.2	4.5	1.7	11.5	1.7	14.5	1.6	12.5	1.8	6	1.2	12	1.5	45	10.1	1	·	·	11	·	·	·	1	20	13	10	1	1	1	-
XII	3.5	1.0	4	1.0	1	2.0	2	1.0	12	3.5	15.5	1.8	16	1.7	12	1.3	27	1.3	14	5.2	15	12	15	28	·	·	·	2	17	9	4	·	5	17	-
Rok	30	1.3	29.5	1.4	40	1.6	47.5	1.9	123	2.3	186.5	2.4	284.5	2.2	127	2.0	227	1.8	507	34.7	14.V	19	37	118	31	3	·	30	137	142	99	10	20	56	-

Pułtusk $H_s = 80\,m$ $h_w = 12\,m$

I	5	8.6	5	5.8	·	·	1	3.0	17	5.5	34.5	7.4	22	8.2	7.5	6.5	1	7.0	26	9.8	25	3	5	22	·	-	-	2	13	13	6	·	-	18	·
II	4.5	8.9	8.5	6.5	9.5	4.4	9	4.1	7.5	7.3	8.5	8.9	19.5	9.4	15	10.5	2	7.7	50	12.8	12	6	13	25	·	-	-	·	18	17	10	2	-	28	·
III	12	6.9	14	4.6	7	3.6	16	5.8	7	5.1	·	·	10	5.6	13	8.2	14	5.0	45	11.2	5	7	6	28	·	-	-	3	16	14	9	1	-	20	·
IV	11	6.3	8.5	6.7	2.5	5.0	10	7.1	11	4.7	14	4.2	10	4.6	13	7.0	10	5.1	21	7.7	5	·	·	1	4	-	-	2	6	9	4	·	-	·	1
V	9	2.8	3.5	3.1	1	4.0	6	6.5	8	4.9	19	4.1	13	4.4	20.5	5.1	13	3.8	124	25.5	14	·	·	2	·	-	-	·	16	21	16	4	-	·	5
VI	9	6.3	4	7.5	1.5	6.3	·	·	2.5	3.0	11	4.4	22.5	5.6	26.5	4.4	13	4.4	76	45.0	29	·	·	·	5	-	-	1	8	14	10	1	-	·	4
VII	14	3.5	1	3.0	·	·	·	·	5	4.6	18	4.1	20	4.4	24	5.4	11	3.9	29	5.4	13	·	·	·	5	-	-	1	3	12	9	·	-	·	4
VIII	2.5	1.2	0.5	2.0	0.5	2.0	1	9.5	9	5.2	25.5	5.4	23.5	5.4	11.5	3.3	19	3.9	50	8.2	24	·	·	·	6	-	-	1	7	12	12	·	-	·	8
IX	3.5	3.3	4	2.1	5	2.1	3.5	3.1	7	4.9	14	4.8	26	4.2	14	4.6	13	3.5	62	13.7	18	·	·	·	1	-	-	1	10	14	9	2	-	·	2
X	1	4.5	5.5	2.0	3.5	2.0	7	2.4	8.5	2.5	11	4.4	13.5	4.3	12	4.2	31	2.3	6	3.4	28	·	·	3	·	-	-	4	11	6	2	·	-	·	·
XI	2	2.5	4.5	9.1	9	5.0	26.5	5.6	2	5.5	6	5.7	18	3.2	8	2.9	14	4.1	51	9.2	20	·	·	8	·	-	-	1	25	13	10	·	-	1	·
XII	20.5	2.8	10.5	3.0	3.5	2.9	7.5	2.7	7.5	5.7	17.5	5.3	16.5	3.8	2.5	3.2	7	3.5	16	5.5	15	9	16	26	·	-	-	·	18	11	6	·	-	16	·
Rok	94	4.8	69.5	4.6	43	3.1	87.5	4.2	92	4.9	179	4.9	214.5	5.3	167.5	5.4	148	4.5	556	45.0	29.VI	25	40	115	21	-	-	16	151	156	103	10	-	83	24

Białowieża $H_s = 163\,m$ $H_b = 163{,}7\,m$ $h_w = 18{,}7\,m$

I	5	3.6	2.5	4.0	2.5	2.6	5	2.1	17	2.6	28.5	3.7	17.5	4.9	11	3.8	4	3.6	25	8.6	25	2	9	26	·	3	1	1	22	15	6	·	1	26	·
II	11.5	6.5	6	4.5	10.5	4.5	10	2.7	10	4.6	11.5	6.4	11	8.3	10.5	6.3	3	5.4	33	9.5	12	11	14	28	·	8	6	·	17	15	11	·	3	28	·
III	9.5	7.1	8	5.9	16.5	2.4	22	2.6	8	2.9	2.5	4.0	7.5	3.9	8	3.9	11	3.4	43	7.0	23	12	18	29	·	5	1	4	17	13	10	·	2	31	·
IV	10.5	3.3	5.5	3.0	12.5	3.0	16	3.5	16	3.6	7.5	3.1	3.5	2.9	7.5	4.1	11	3.0	64	16.1	7	·	·	5	3	3	·	3	9	13	12	1	3	5	4
V	6.5	2.8	5	2.4	5.5	2.6	8.5	2.9	4	2.5	13	3.3	15	2.9	22.5	3.2	13	2.6	90	17.2	21	·	·	3	·	1	·	1	13	16	14	3	4	·	6
VI	9	4.5	14	6.5	·	·	5.5	2.0	2.5	3.0	12	3.5	17.5	4.6	18.5	3.3	11	3.7	110	31.0	4	·	·	·	5	3	2	3	8	14	11	5	·	·	3
VII	11.5	2.6	7.5	2.5	1.5	3.0	0.5	1.0	9	2.6	17	2.9	14.5	4.8	17.5	4.3	14	2.9	39	6.2	10	·	·	·	4	1	·	3	5	15	12	·	2	·	5
VIII	4	3.6	2.5	2.0	0.5	1.0	3.5	4.4	8	3.6	20.5	3.0	26.5	4.9	10.5	4.2	17	3.2	81	16.5	18	·	·	·	5	2	·	2	7	14	12	5	3	·	6
IX	2.5	2.0	2	2.0	6.5	1.6	6	1.8	7	2.6	18	4.8	18	3.7	18	3.5	12	3.0	93	18.8	18	·	·	·	1	2	·	4	9	15	15	4	6	·	4
X	6.5	1.3	4	1.5	5.5	2.1	11.5	1.8	5	1.9	7	2.5	14	4.1	11.5	2.9	28	1.8	11	4.9	19	·	·	7	·	1	·	3	10	10	3	·	15	·	·
XI	6	2.1	6.5	3.2	14.5	5.7	34	3.9	6.5	3.8	4.5	3.1	8	3.2	7	2.8	3	3.7	50	8.7	29	·	·	10	·	2	·	4	24	20	14	·	10	2	·
XII	7	2.7	13.5	3.0	4	2.6	9	1.9	9.5	4.0	15	4.2	14.5	3.1	9.5	2.6	11	2.8	17	5.3	16	12	18	30	·	·	·	3	18	15	5	·	3	17	·
Rok	89.5	3.5	77	3.1	80	2.6	131.5	2.6	102.5	3.1	157	3.7	167.5	4.3	152	3.7	138	3.3	656	31.0	4.VI	37	59	138	18	31	10	31	159	175	125	18	52	109	28

Łagiewniki $\varphi = 52°40'$ $\lambda = 18°19'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	$\overline{\text{Max}}$	$\overline{\text{Min}}$	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.7	-1.8	8.6	22	-14.4	31	-0.1	1.8	0.0	0.4	5.7	6.0	5.6	5.8	90	85	89	88	0.6	1.1	0.7	0.8	–	–	–	–
II	–	–	–	–	0.9	-4.1	5.7	13	-13.3	1	-2.3	0.0	-1.4	-1.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	2.1	-4.3	12.1	31	-10.2	9	-1.7	1.6	-1.1	-0.6	5.1	6.1	5.2	5.5	91	88	89	89	0.5	0.9	0.6	0.7	–	–	–	–
IV	–	–	–	–	15.3	5.6	27.3	23	0.7	30	8.4	13.7	9.2	10.1	9.3	10.6	10.1	10.0	83	67	83	78	2.1	6.9	2.2	3.7	–	–	–	–
V	–	–	–	–	14.8	7.0	21.5	12	-2.1	1	9.9	13.6	10.2	11.0	10.6	11.0	10.8	10.8	86	70	85	80	1.9	5.2	1.9	3.0	–	–	–	–
VI	–	–	–	–	20.1	9.7	31.0	16	2.9	3	13.6	18.8	13.9	15.0	12.0	12.0	12.8	12.3	75	54	78	69	4.2	10.8	3.7	6.2	–	–	–	–
VII	–	–	–	–	21.0	10.7	31.4	26	5.3	29	14.4	19.7	15.0	16.0	14.2	13.8	14.4	14.1	85	61	84	77	2.5	9.9	2.9	5.1	–	–	–	–
VIII	–	–	–	–	21.5	12.0	30.6	12	7.9	24	15.2	20.3	15.3	16.5	14.6	14.7	15.0	14.8	84	64	85	78	2.8	9.1	2.6	4.8	–	–	–	–
IX	–	–	–	–	17.7	8.1	29.8	4	2.9	25	10.3	16.2	11.5	12.4	11.3	11.7	11.6	11.5	89	64	85	79	1.5	7.4	2.3	3.7	–	–	–	–
X	–	–	–	–	13.1	4.8	21.1	3	-1.5	21	6.9	12.5	7.8	8.8	9.4	10.3	9.8	9.8	92	70	90	84	0.9	4.5	1.2	2.2	–	–	–	–
XI	–	–	–	–	5.7	2.1	13.1	4,5	-2.1	17	3.2	4.8	3.6	3.8	7.2	7.5	7.2	7.3	92	86	90	89	0.6	1.3	0.8	0.9	–	–	–	–
XII	–	–	–	–	-2.3	-7.1	4.9	12	-19.8	21	-4.4	-3.3	-4.9	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	11.0	3.6	31.4	26.VII	-19.8	21.XII	6.1	10.0	6.6	7.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Wieniec-Zdrój $\varphi = 52°40'$ $\lambda = 19°00'$

I	–	–	–	–	2.0	-1.9	8.3	22	-17.5	31	-0.7	1.4	-0.1	0.1	5.5	6.2	5.7	5.8	91	89	89	90	0.5	0.8	0.7	0.7	7.6	7.5	7.8	7.6
II	–	–	–	–	0.5	-4.5	4.7	20	-13.6	1	-2.5	-0.1	-1.6	-1.4	4.6	5.0	4.9	4.8	87	81	87	85	0.6	1.1	0.7	0.8	8.5	8.8	6.6	8.0
III	–	–	–	–	2.0	-4.8	11.8	31	-13.6	15	-2.8	1.4	-1.7	-1.2	4.4	5.2	4.6	4.7	86	74	83	81	0.7	1.8	0.8	1.1	7.5	7.0	6.3	6.9
IV	–	–	–	–	15.4	4.9	28.4	23	-0.8	8	7.6	14.1	8.9	9.9	9.5	9.6	9.9	9.7	89	61	85	78	1.4	8.2	2.2	3.9	7.4	7.1	6.0	6.8
V	–	–	–	–	15.2	–	20.6	19	–	–	9.9	13.8	9.6	10.7	10.8	10.5	11.4	10.9	88	67	93	83	1.7	5.8	0.9	2.8	6.5	7.5	7.4	7.1
VI	–	–	–	–	20.1	8.8	31.1	16	0.8	4	13.8	18.4	13.7	14.9	12.0	11.7	12.8	12.2	75	56	81	71	4.4	10.5	3.4	6.1	6.1	5.4	6.4	6.0
VII	–	–	–	–	21.4	10.0	29.9	26	4.8	29	14.1	19.9	14.9	16.0	14.2	13.7	14.1	14.0	88	60	83	77	2.0	9.9	3.2	5.0	6.4	6.6	6.0	6.3
VIII	–	–	–	–	22.0	11.6	31.3	7	5.2	10	15.1	20.4	15.6	16.7	14.7	14.7	15.1	14.8	86	62	85	78	2.7	9.9	3.0	5.2	6.7	6.9	6.7	6.8
IX	–	–	–	–	17.7	7.6	29.4	4	2.5	25	10.4	16.1	11.5	12.4	11.7	12.8	12.6	12.4	93	71	92	85	1.1	6.0	1.2	2.8	6.6	7.4	4.8	6.3
X	–	–	–	–	13.1	3.7	20.8	2,3	-3.8	16	5.9	12.4	6.7	7.9	9.3	11.0	9.8	10.0	97	76	96	90	0.3	3.8	0.4	1.5	7.9	6.3	5.7	6.6
XI	–	–	–	–	5.4	1.6	13.0	4	-6.6	26	3.0	4.6	3.3	3.6	7.4	7.8	7.5	7.6	95	89	95	93	0.4	1.0	0.5	0.6	9.3	8.5	8.1	8.6
XII	–	–	–	–	-2.5	-7.1	4.6	10	-19.5	22	-5.2	-3.2	-4.9	-4.6	4.2	4.8	4.2	4.4	92	88	90	90	0.3	0.5	0.4	0.4	9.1	8.2	7.0	8.1
Rok	–	–	–	–	11.0	–	31.3	7.VIII	-19.5	22.XII	5.7	9.9	6.3	7.0	9.0	9.4	9.4	9.3	89	73	88	83	1.3	4.9	1.4	2.5	7.5	7.3	6.6	7.1

Nur $\varphi = 52°40'$ $\lambda = 22°19'$

I	–	–	–	–	1.5	-3.4	7.3	22	-21.7	31	-1.4	0.4	-1.3	-0.9	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.3	7.3	7.7
II	–	–	–	–	-0.6	-6.9	4.5	7	-17.2	1	-4.9	-1.9	-3.4	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.7	8.1	8.1
III	–	–	–	–	1.0	-7.5	8.1	31	-18.8	26	-6.0	-0.1	-3.6	-3.3	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.4	6.5	6.7
IV	–	–	–	–	15.6	5.5	27.8	22	-1.1	30	7.5	14.2	9.1	10.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.4	5.5	6.6
V	–	–	–	–	15.6	6.6	21.6	13	-2.3	1	9.0	14.0	10.1	10.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.6	6.6	7.6
VI	–	–	–	–	19.4	8.9	29.2	16,23	3.9	7	13.0	17.5	13.1	14.2	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.8	5.0	6.0
VII	–	–	–	–	21.4	10.7	28.6	21	6.8	5	14.0	20.1	14.9	16.0	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.5	4.7	5.3
VIII	–	–	–	–	21.7	11.5	30.2	13	6.7	27	14.0	20.4	15.6	16.4	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.0	4.7	5.7
IX	–	–	–	–	17.0	7.5	26.2	5	1.3	25	9.4	15.8	10.9	11.8	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.0	5.5	6.2
X	–	–	–	–	12.7	3.6	21.2	2	-3.5	16	5.3	11.7	6.7	7.6	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.1	4.3	5.9
XI	–	–	–	–	6.3	1.8	17.4	1	-2.3	27	3.1	5.2	3.8	4.0	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.2	8.7	8.7
XII	–	–	–	–	-2.7	-7.9	3.3	10	-22.1	21	-5.7	-4.1	-5.4	-5.2	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.9	6.8	7.5
Rok	–	–	–	–	10.7	2.5	30.2	13.VIII	-22.1	21.XII	4.8	9.4	5.9	6.5	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.1	6.1	6.8

Poświętne $\varphi = 52°38'$ $\lambda = 20°23'$

I	–	–	–	–	1.4	-2.5	8.3	22	-17.7	31	-0.7	0.7	-0.7	-0.4	5.3	5.4	5.2	5.3	88	82	84	85	0.7	1.2	0.8	0.9	7.4	7.6	6.4	7.1
II	–	–	–	–	-0.1	-5.2	3.5	12	-15.6	1	-3.5	-1.2	-2.4	-2.4	4.3	4.6	4.6	4.5	87	81	88	85	0.6	1.1	0.6	0.8	8.9	8.8	6.6	8.1
III	–	–	–	–	1.1	-5.2	11.3	31	-17.7	15	-4.1	0.0	-1.6	-1.8	4.2	4.9	4.6	4.6	89	78	83	83	0.5	1.4	0.9	0.9	6.9	6.8	5.3	6.3
IV	–	–	–	–	15.2	5.4	27.2	22	0.0	1	7.2	14.0	9.4	10.0	9.0	9.0	9.6	9.2	86	58	79	74	1.6	8.4	2.8	4.3	6.4	6.0	4.9	5.8
V	–	–	–	–	14.7	6.5	20.3	8	-3.3	1	9.0	13.0	10.3	10.6	10.4	10.2	11.0	10.5	89	68	86	81	1.3	5.2	1.8	2.8	7.9	7.8	6.5	7.4
VI	–	–	–	–	19.2	9.3	28.5	16	3.7	3	12.8	17.8	14.0	14.7	11.8	11.2	12.6	11.9	77	54	77	69	3.5	10.0	3.9	5.8	5.9	5.5	4.7	5.4
VII	–	–	–	–	20.9	10.2	29.2	26	4.9	31	13.9	19.1	14.8	15.6	13.8	13.1	13.9	13.6	86	60	82	76	2.3	9.6	3.3	5.1	5.0	6.1	4.7	5.3
VIII	–	–	–	–	21.5	11.4	29.6	7	5.4	10	14.5	20.0	15.2	16.2	14.6	14.5	15.5	14.9	88	62	89	80	2.0	9.6	2.0	4.5	6.4	6.9	5.1	6.1
IX	–	–	–	–	16.8	7.3	26.8	4	2.0	25	9.6	15.6	11.4	12.0	11.2	12.1	12.2	11.8	92	69	90	84	1.0	6.2	1.4	2.9	5.9	6.9	4.9	5.9
X	–	–	–	–	12.5	3.4	19.7	2	-4.6	16	5.6	11.4	7.1	7.8	8.9	10.4	9.4	9.6	95	75	90	87	0.5	3.7	1.0	1.7	5.3	5.6	4.6	5.2
XI	–	–	–	–	5.6	0.9	11.5	1,4,5	-3.2	18,26	2.9	5.0	3.6	3.8	7.1	7.4	7.1	7.2	92	83	88	88	0.6	1.6	1.0	1.1	8.6	7.9	8.0	8.2
XII	–	–	–	–	-2.8	-8.2	4.7	12	-21.7	21	-5.3	-4.1	-5.0	-4.8	4.0	4.3	4.1	4.1	91	89	90	90	0.4	0.5	0.5	0.5	7.6	7.8	6.5	7.3
Rok	–	–	–	–	10.5	2.8	29.6	7.VIII	-21.7	21.XII	5.2	9.3	6.3	6.8	8.7	8.9	9.2	8.9	88	72	86	82	1.2	4.9	1.7	2.6	6.8	7.0	5.7	6.5

Łagiewniki $H_S = 80 m$ $h_W = 10 m$ 1962

MIESIĄC	ROZKŁAD WIATRU (nD, vmD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v>10	v>15	◔	●	Opad R>0.1	R>1.0	R>10.0	≡	⊞	π ro
I	6	3.3	9	2.2	·	·	5	1.0	2.5	3.0	49	2.6	11.5	2.4	3	2.3	7	2.3	20	8.9	25	3	4	19	·	·	·	–	–	7	5	·	–	–	·
II	11	3.9	5.5	2.1	9	2.0	5	1.6	·	·	12	2.5	24.5	2.8	8	3.5	9	2.5	52	28.0	16	3	11	24	·	·	·	–	–	12	5	2	–	–	1
III	9	3.2	12	2.0	8	2.0	3	1.0	6	1.2	6	1.2	12	1.9	5	2.0	32	1.3	29	10.8	12	1	8	29	·	·	·	–	–	7	4	1	–	–	·
IV	8.5	3.4	13.5	2.1	3.5	2.1	11	1.6	0.5	2.0	14	1.8	13.5	1.4	3.5	2.6	22	1.5	27	10.2	5	·	·	·	3	·	·	–	–	10	7	1	–	·	·
V	15	2.3	2	1.5	2	2.2	8.5	1.8	1.5	2.0	17	1.9	25	2.2	20.5	2.0	24	1.5	115	36.3	14	·	·	2	·	·	·	–	–	–	–	–	–	·	3
VI	4	5.0	8	3.4	2.5	1.0	3.5	1.3	2.5	2.0	9.5	2.4	26.5	2.4	15.5	2.4	18	2.0	45	11.6	29	·	·	·	6	·	·	–	–	11	10	1	–	·	2
VII	0.5	2.0	8.5	2.5	4	1.0	3	1.3	7	1.4	7	2.1	24	2.0	20	2.4	19	1.6	23	10.0	14	·	·	·	5	·	·	–	–	7	5	1	–	·	1
VIII	·	·	2	1.5	2	1.5	·	·	8	1.4	4.5	2.6	32.5	2.8	24	2.2	20	1.8	52	20.0	25	·	·	·	5	·	·	–	–	14	8	1	–	·	2
IX	2.5	2.0	2	1.0	·	·	5	1.6	3.5	1.7	10	2.0	21.5	2.8	9.5	2.1	36	1.4	49	23.0	18	·	·	·	1	·	·	–	–	10	9	1	–	·	3
X	4.5	2.2	3	2.0	1	2.0	6.5	1.5	6	1.6	8	1.8	6.5	2.3	10.5	2.1	47	1.0	32	17.6	31	·	·	3	·	·	·	–	–	5	4	1	–	·	·
XI	·	·	4.5	2.9	24	2.1	3	2.3	5	1.3	6.5	1.4	13	2.1	·	-	34	1.3	57	11.2	1	·	1	9	·	·	·	–	–	13	12	1	–	–	·
XII	2.5	2.0	13.5	1.9	5.5	1.5	4	2.9	6.5	2.5	12	1.8	14	1.4	8	1.6	27	1.3	5	1.2	19	12	18	26	·	·	·	–	–	8	1	·	–	–	·
Rok	63.5	2.4	83.5	2.1	61.5	1.4	57.5	1.5	49	1.7	155.5	2.0	202	2.2	127.5	2.1	295	1.6	506	36.3	14.V	19	42	112	20	·	·	–	–	–	–	–	–	–	12

Wieniec-Zdrój $H_S = 82 m$ $h_W = 14 m$

I	4	1.8	1	2.0	5	1.6	·	·	13	1.5	26	1.7	15	2.5	8	1.9	21	1.4	21	12.8	25	2	7	19	·	·	·	3	19	8	5	1	3	–	–
II	3	1.7	5	2.8	11	2.4	3	3.0	9	2.8	7	3.1	13	2.8	11	1.9	22	1.9	39	8.2	12	3	11	24	·	·	·	·	12	15	8	·	2	–	–
III	12	2.8	7	1.4	6	2.0	9	2.6	11	1.5	9	1.0	7	2.1	2	3.5	30	1.4	44	7.9	12	1	8	27	·	·	·	4	16	9	8	·	3	–	–
IV	11	1.6	6	2.0	3	1.7	5	2.4	10	3.7	11	1.3	10	1.7	9	1.9	25	1.5	26	8.1	13	·	·	4	5	·	·	2	12	9	5	·	3	·	–
V	5	1.8	1	1.0	1	2.0	3	2.0	8	1.9	9	1.8	17	1.9	9	2.6	40	1.1	157	57.1	14	·	·	–	·	·	·	1	14	22	17	3	1	·	–
VI	9	2.4	2	2.0	1	1.0	2	2.0	4	1.2	11	1.9	17	3.4	14	3.6	30	1.8	47	17.6	29	·	·	·	6	·	·	4	8	12	8	1	·	·	–
VII	1	2.0	5	1.8	2	1.0	3	2.0	3	1.0	15	1.9	20	1.8	16	2.0	28	1.3	34	5.6	2	·	·	·	5	·	·	2	8	13	10	·	1	·	–
VIII	2	1.5	2	1.5	1	2.0	2	1.5	5	2.2	14	2.7	23	2.5	13	2.6	31	1.6	51	13.8	24	·	·	·	7	·	·	2	11	13	11	1	4	·	–
IX	·	·	3	1.7	3	1.7	4	2.8	5	2.8	12	1.8	17	3.1	8	2.2	38	1.4	72	23.9	18	·	·	·	2	·	·	5	11	14	11	1	4	·	–
X	1	2.0	·	·	1	1.0	3	1.0	6	2.2	3	2.0	12	1.5	4	1.5	63	0.5	23	8.6	27	·	·	8	·	·	·	3	12	5	4	·	17	·	–
XI	·	·	5	2.4	13	1.7	9	2.1	1	1.0	13	2.2	8	1.9	3	1.0	38	1.1	39	13.7	20	·	·	10	·	·	·	1	21	7	7	1	14	·	–
XII	4	1.2	5	1.6	1	1.0	4	1.5	15	2.2	15	1.9	7	1.4	3	2.3	39	1.1	45	9.7	15	11	18	26	·	·	·	·	18	3	3	·	5	–	–
Rok	52	1.6	42	1.7	48	1.6	47	1.9	90	2.0	145	1.9	166	2.2	100	2.2	405	1.3	568	57.1	14.V	17	44	–	25	·	·	27	162	130	97	8	57	–	–

Nur $H_S = 110 m$ $h_W = 13 m$

I	3.5	6.1	4	7.5		·	2	1.5	24.5	2.1	23.5	3.2	19	2.6	1.5	5.7	15	2.6	29	10.0	25	3	7	22	·	1	·	3	18	12	8	1	1	20	·
II	10	9.8	8.5	4.6	7.5	1.3	5.5	1.6	9.5	4.0	12	8.6	8.5	5.4	6.5	8.8	16	4.8	43	14.6	12	7	15	27	·	9	6	·	17	13	8	1	2	28	·
III	10	8.8	18.5	1.8	4.5	1.4	16	2.2	15	1.7	4	4.0	7	3.1	6.5	2.7	25	2.4	41	9.2	12	10	9	27	·	2	2	5	15	10	8	·	2	29	·
IV	13	3.2	10	3.4	15	1.0	14	1.4	13.5	2.3	5	1.8	3	1.3	6	6.5	24	2.0	48	12.9	26	·	·	3	3	2	1	2	14	12	9	1	1	·	1
V	9.5	1.5	3	1.3	3	3.0	3	1.0	6.5	1.5	8.5	2.2	16	3.1	8.5	1.6	35	1.3	102	15.5	14	·	·	1	·	·	·	1	18	24	18	3	1	·	2
VI	11	6.3	7.5	7.9	·	·	2	1.0	3.5	1.3	7	2.4	20	2.6	15	2.0	24	2.6	92	34.9	4	·	·	·	4	3	2	4	10	16	11	3	·	·	3
VII	11.5	2.1	·	-	·	·	2	1.0	8.5	1.5	9	1.7	19.5	2.4	7.5	2.7	35	1.3	66	14.8	13	·	·	·	5	·	·	4	5	12	8	2	·	·	5
VIII	4	3.0	1.5	3.7	·	·	0.5	3.0	8.5	1.4	22	2.7	21	2.3	5.5	2.5	30	1.6	77	15.5	13	·	·	·	6	·	·	4	8	14	13	3	1	·	3
IX	2.5	1.6	6	1.7	1	1.0	2	1.0	5.5	1.5	22	3.1	8	2.9	9	4.4	34	1.7	113	38.0	7	·	·	·	2	1	·	4	10	15	12	3	2	·	2
X	5.5	1.0	1	2.0	3.5	1.0	11.5	1.1	1	1.0	11	2.6	10.5	3.7	5	1.6	44	1.1	6	3.6	27	·	·	5	·	2	·	4	13	4	2	·	8	·	·
XI	3.5	1.3	6	3.2	11.5	5.6	21.5	2.7	1	4.0	6.5	1.6	9	3.4	7	1.9	24	2.3	66	13.0	15	·	·	10	·	2	1	2	23	15	14	1	5	1	·
XII	12	1.9	14	2.3	·	·	5	1.2	13	2.3	11	2.1	8	1.4	7	1.3	23	1.4	19	4.4	14	11	17	27	·	·	·	4	19	14	6	·	2	22	·
Rok	96	3.9	80	3.3	32.5	1.2	85	1.6	96.5	2.0	141.5	3.0	149.5	2.8	85	3.5	329	2.1	702	38.0	7.IX	31	48	122	20	22	12	37	170	161	117	18	25	100	16

Poświętne $H_S = 101 m$ $h_W = 14 m$

I	3.5	9.0	5.5	4.2	2	1.8	2.5	2.2	16	4.2	29.5	5.1	28	6.6	6	7.1	·	5.5	20	6.7	25	3	7	19	·	8	1	1	12	11	5	·	4	13	·
II	7	8.6	6	5.4	13.5	4.6	2	4.0	11	2.9	14	6.2	19	8.2	10.5	12.3	1	6.8	34	12.1	12	3	13	25	·	10	6	·	17	12	6	1	5	11	·
III	11	7.5	18	3.8	10	3.1	24.5	3.0	5	4.1	6.5	2.6	6	4.9	10	7.2	2	4.2	51	15.7	5	3	9	28	·	5	2	8	12	15	9	2	5	12	·
IV	16	4.3	7	3.3	8.5	5.1	9.5	3.9	7.5	4.3	46.5	3.7	10	3.6	10	5.0	5	3.9	25	11.4	13	·	·	·	3	3	·	3	6	12	6	1	·	·	1
V	6	2.2	8.5	1.7	4.5	1.9	6.5	2.7	6.5	2.4	17	2.4	21.5	3.9	15.5	4.9	7	2.9	193	78.2	14	·	·	3	·	2	·	2	15	24	19	4	2	·	6
VI	17	5.6	5	7.6	2.5	1.6	5	2.6	6.5	2.5	12.5	3.9	25	4.7	14.5	4.1	2	4.4	64	34.0	29	·	·	·	5	4	2	1	5	12	9	1	·	·	5
VII	10.5	4.2	3.5	2.7	0.5	3.0	5	2.3	4	4.0	18	3.1	25.5	3.8	20	3.5	6	3.3	22	4.6	2	·	·	·	5	1	·	4	2	12	7	·	1	·	6
VIII	1	4.0	6	1.3	2	2.5	3	2.5	7	3.3	20	3.3	40	4.3	9	2.9	5	3.3	82	26.8	17	·	·	·	6	2	·	3	9	15	14	2	·	·	9
IX	3.5	4.0	4	2.0	5.5	2.5	6	1.7	6.5	3.2	22	3.0	29.5	4.2	8	5.6	5	3.3	68	18.6	18	·	·	·	1	2	·	4	9	17	10	2	4	·	3
X	5.5	4.4	7	1.4	14	1.7	14	2.2	6	2.4	10	3.0	21	3.3	5.5	3.5	10	2.2	9	4.0	28	·	·	5	·	·	·	8	8	8	3	·	10	·	·
XI	3	2.8	10.5	6.1	19.5	4.2	15.5	3.8	5	2.8	7.5	3.9	20.5	3.5	5.5	1.4	3	3.8	42	10.2	20	·	·	14	·	3	·	2	18	12	9	1	6	1	
XII	5	2.2	15.5	3.5	12.5	2.5	3.5	3.4	13	4.3	13.5	5.4	17.5	3.4	12.5	3.0	·	3.6	12	3.1	15	12	18	30	·	1	·	3	17	9	5	·	2	15	
Rok	89	4.4	96.5	3.6	95	2.9	97	2.9	94	3.4	187	3.8	263.5	4.5	127	5.0	46	3.9	622	78.2	14.V	21	47	124	20	41	11	39	130	159	102	14	39	52	30

Szamotuły $\varphi = 52°37'$ $\lambda = 16°34'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA t											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0,m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnie I	II	III	Dzień	I	II	III	Dzień	I	II	III	Dzień	I	II	III	Dzień	I	II	III	Dzień
I	–	–	–	–	3.3	-1.5	9.8	22	-13.4	31	0.1	2.3	0.5	0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.8	7.7	7.9
II	–	–	–	–	2.2	-3.3	7.8	20	-12.4	1	-2.1	1.1	-0.5	-0.5	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.4	7.6	8.2
III	–	–	–	–	3.7	-3.7	14.1	30	-9.0	8	-2.6	2.6	-0.6	-0.3	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.7	6.4	6.5
IV	–	–	–	–	15.5	5.3	27.6	23	0.1	1	7.3	14.0	9.6	10.1	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.9	6.2	6.1
V	–	–	–	–	15.2	6.2	21.5	19	-1.8	1	9.0	13.8	10.8	11.1	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.5	7.6	7.7
VI	–	–	–	–	20.6	9.0	29.4	16	1.4	3	13.0	18.8	14.6	15.2	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.2	6.3	5.5
VII	–	–	–	–	21.5	10.1	31.8	26	3.3	29	14.1	19.9	16.3	16.7	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.1	7.1	6.4
VIII	–	–	–	–	21.5	12.1	29.0	12	7.8	9	14.7	20.2	16.9	17.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.3	6.8	6.7
IX	–	–	–	–	17.7	7.9	28.8	4	3.7	18,25	10.1	16.5	13.0	13.2	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.5	5.9	6.0
X	–	–	–	–	13.1	5.1	22.9	3	-1.2	16	6.5	12.3	8.8	9.1	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.8	5.5	6.7
XI	–	–	–	–	5.8	2.0	15.3	8	-2.4	17,21	2.9	5.2	3.6	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.5	8.0	7.9
XII	–	–	–	–	-4.5	-6.1	6.3	12	-18.4	22	-4.6	-2.8	-4.0	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.8	8.4	8.4
Rok	–	–	–	–	11.6	3.6	31.8	26.VII	-18.4	22.XII	5.7	10.3	7.4	7.7	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.8	7.0	7.0

Przebędowo $\varphi = 52°35'$ $\lambda = 17°01'$

I	–	–	–	–	3.2	-1.7	9.3	22	-14.0	31	0.1	1.8	0.6	0.8	5.7	6.0	5.7	5.8	8.9	8.4	8.7	8.7	0.7	1.2	0.9	0.9	8.2	8.2	8.9	8.4
II	–	–	–	–	4.3	-3.5	6.6	20	-13.5	1	-2.1	0.4	-0.8	-0.8	4.9	5.6	5.3	5.3	9.1	8.7	9.0	8.9	0.5	0.8	0.6	0.6	8.9	8.6	7.8	8.4
III	–	–	–	–	2.9	-3.8	13.0	30	-11.9	8	-2.1	1.9	-0.4	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.7	5.9	6.6
IV	–	–	–	–	15.3	5.0	26.8	23	-0.8	11	7.3	13.6	9.5	10.0	9.1	9.2	9.8	9.4	8.6	5.9	8.0	7.5	1.6	7.8	2.8	4.1	6.4	6.2	6.9	6.5
V	–	–	–	–	14.6	5.8	21.0	19	-2.4	1	9.1	13.0	9.8	10.4	10.5	10.5	11.1	10.7	9.0	7.0	9.1	8.4	1.3	5.0	1.2	2.5	8.0	8.0	7.2	7.7
VI	–	–	–	–	19.6	8.5	30.4	16	0.9	3	13.1	17.9	14.1	14.8	12.1	12.0	13.1	12.4	7.8	5.8	7.9	7.2	3.4	9.5	3.6	5.5	4.4	5.6	5.6	5.2
VII	–	–	–	–	20.9	9.5	32.0	26	3.2	29	14.0	19.3	15.4	16.0	13.8	12.1	13.5	13.1	8.6	5.6	7.7	7.3	2.4	11.1	4.4	6.0	5.7	6.5	5.9	6.0
VIII	–	–	–	–	21.8	11.7	29.5	12	6.5	10	14.6	20.0	15.8	16.6	14.2	13.2	14.4	13.9	8.5	5.8	8.0	7.4	2.5	10.8	3.9	5.7	7.0	7.3	6.8	7.0
IX	–	–	–	–	17.8	7.8	29.4	4	3.0	25	9.8	16.2	12.3	12.6	11.2	11.3	11.6	11.4	9.2	6.3	8.1	7.9	1.1	7.7	3.1	4.0	6.6	6.3	6.4	6.4
X	–	–	–	–	13.3	3.5	22.8	3	-3.1	16	6.1	11.9	7.5	8.2	9.5	10.5	9.8	9.9	9.7	7.5	9.4	8.9	0.3	3.9	0.8	1.7	8.1	6.2	6.7	7.0
XI	–	–	–	–	5.8	1.9	14.2	5	-2.2	21	2.8	4.7	3.7	3.7	7.3	8.0	7.6	7.6	9.7	9.2	9.5	9.5	0.2	0.9	0.5	0.5	8.0	7.5	7.6	7.7
XII	–	–	–	–	-1.6	-6.8	6.8	12	-18.4	22	-5.0	-3.5	-4.5	-4.4	4.2	4.5	4.3	4.3	9.1	8.9	8.9	9.0	0.3	0.5	0.4	0.4	7.6	6.8	7.2	7.2
Rok	–	–	–	–	11.2	3.2	32.0	26.VII	-18.4	22.XII	5.6	9.8	6.9	7.3	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.0	6.9	7.0

Wyszków $\varphi = 52°35'$ $\lambda = 21°27'$

I	–	–	–	–	1.7	-3.5	9.0	22	-20.0	31	-1.2	0.8	-1.1	-0.6	5.3	5.4	5.4	5.4	9.1	8.1	8.7	8.6	0.5	1.3	0.6	0.8	8.7	7.6	7.3	7.9
II	–	–	–	–	0.0	-6.7	3.6	12	-17.0	1	-4.5	-1.3	-3.3	-3.1	4.2	4.6	4.6	4.5	9.0	8.2	9.1	8.8	0.4	1.0	0.4	0.6	8.5	7.7	8.1	8.1
III	–	–	–	–	1.5	-7.1	10.2	11	-16.6	15	-4.8	0.6	-2.8	-2.4	4.1	4.9	4.7	4.6	8.9	7.6	9.0	8.5	0.4	1.6	0.5	0.8	7.3	6.7	6.5	6.8
IV	–	–	–	–	16.2	5.6	28.4	22	-1.0	8	8.3	15.1	9.3	10.5	9.2	9.8	10.0	9.7	8.3	5.8	8.3	7.5	2.2	8.9	2.3	4.5	6.0	5.5	5.4	5.6
V	–	–	–	–	15.8	6.4	21.5	28	-3.2	1	9.4	14.3	10.3	11.1	10.7	10.9	11.3	11.0	8.9	6.7	8.9	8.2	1.3	5.8	1.5	2.9	7.7	7.6	6.1	7.1
VI	–	–	–	–	20.1	8.7	30.4	16	3.0	10	13.8	18.7	12.9	14.6	12.3	11.7	12.6	12.2	7.6	5.5	8.3	7.1	4.0	10.9	2.7	5.9	5.9	5.8	4.2	5.7
VII	–	–	–	–	21.8	10.4	29.0	21,26	6.3	4	14.9	20.4	14.7	16.2	14.1	13.6	14.2	14.0	8.3	5.7	8.4	7.5	3.1	10.9	2.8	5.6	5.5	6.2	6.5	6.1
VIII	–	–	–	–	22.2	11.1	31.3	13	5.8	27	14.7	20.9	15.0	16.4	14.8	14.9	15.2	15.0	8.7	6.1	8.8	7.9	2.2	10.4	2.2	4.9	6.9	6.7	5.3	6.3
IX	–	–	–	–	17.1	7.4	25.9	4	2.9	15	9.7	15.8	11.2	12.0	11.3	12.4	12.2	12.0	9.3	6.9	9.1	8.4	0.9	6.1	1.3	2.8	5.8	7.3	4.9	6.0
X	–	–	–	–	12.8	3.1	20.0	2	-4.3	16	5.4	11.9	6.8	7.7	8.7	10.3	9.4	9.5	9.5	7.4	9.3	8.7	0.5	3.9	0.8	1.7	7.5	5.9	4.5	6.0
XI	–	–	–	–	6.5	1.6	15.7	1	-2.5	18,26	3.1	5.5	4.0	4.2	7.2	7.4	7.3	7.3	9.1	8.0	8.8	8.6	0.7	2.0	1.1	1.3	9.0	8.3	7.8	8.4
XII	–	–	–	–	-2.3	-7.4	3.7	12	-20.7	21	-5.4	-3.5	-4.8	-4.6	4.1	4.3	4.2	4.2	9.0	8.4	9.0	8.8	0.4	0.7	0.4	0.5	7.8	7.6	7.4	7.6
Rok	–	–	–	–	11.1	2.5	31.3	13.VIII	-20.7	21.XII	5.3	9.9	6.0	6.8	8.8	9.2	9.3	9.1	8.8	7.0	8.8	8.2	1.4	5.3	1.4	2.7	7.2	6.9	6.2	6.8

Gorzyń $\varphi = 52°34'$ $\lambda = 15°54'$

I	–	–	–	–	3.7	-0.9	10.1	22	-13.2	31	1.0	2.6	1.2	1.5	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.1	7.7	8.0
II	–	–	–	–	2.3	-2.7	7.6	12	-12.4	1	-1.3	1.1	0.0	0.0	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.4	7.6	8.2
III	–	–	–	–	3.8	-3.6	14.6	30	-7.9	8	-2.0	2.8	-0.2	0.1	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.3	6.4	6.1
IV	–	–	–	–	15.4	5.0	26.9	25	0.0	30	7.0	13.5	9.3	9.8	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.3	5.6	5.6
V	–	–	–	–	14.8	6.8	21.9	19	-0.9	1	9.0	13.4	10.0	10.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.9	7.0	7.4
VI	–	–	–	–	20.0	9.6	30.6	15	2.4	3	13.3	18.4	14.0	14.9	–	–	–	–	–	–	–	–	–	–	–	–	4.7	6.5	5.4	5.2
VII	–	–	–	–	20.8	10.8	31.2	26	6.1	29	14.2	19.0	14.8	15.7	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.6	6.2	6.2
VIII	–	–	–	–	21.2	12.5	30.0	12	9.7	15	14.6	19.7	15.5	16.3	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.4	6.1	6.9
IX	–	–	–	–	17.6	8.5	29.6	4	3.3	25	10.2	16.5	11.9	12.6	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.3	3.9	5.6
X	–	–	–	–	12.8	5.1	22.8	2	0.3	16	6.9	12.0	8.0	8.7	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.6	4.5	6.3
XI	–	–	–	–	5.8	2.0	15.0	8	-2.4	21	2.9	5.3	3.6	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.6	7.8	7.9
XII	–	–	–	–	-1.2	-6.0	6.6	12	-17.2	22	-4.0	-2.3	-3.4	-3.3	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.5	6.7	7.3
Rok	–	–	–	–	11.4	3.9	31.2	26.VII	-17.2	22.XII	6.0	10.2	7.1	7.6	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.0	6.2	6.7

Szamotuły $H_s = 70\ m$ $h_w = 17,5\ m$ 1962

ROZKŁAD WIATRU (°D, *mD) — OPAD R — LICZBA DNI (n)

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD Suma	Max	Data	Temperatura Min < -10°	Max < 0°	Min < 0°	Max ≥ 25°	Wiatr v ≥ 10	v ≥ 15	◕	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	11	2.7	1	3.0	2	1.5	5	2.6	8	2.6	35	2.8	29	3.0	2	2.0	·	2.8	18	6.4	11	2	4	15	·	1	·	–	–	7	6	·	6	12	·
II	5	3.2	8	3.6	8	3.4	2	2.0	5	2.0	16	5.8	24	3.4	12	3.5	4	3.6	44	11.6	12	2	8	22	·	3	2	–	–	11	8	1	2	15	1
III	14	2.0	14	2.1	6	2.5	8	2.9	7	2.3	12	2.1	7	1.7	18	2.8	7	2.1	28	4.6	31	·	2	27	·	·	·	–	–	11	10	·	3	–	
IV	18	1.9	14	2.2	4	3.0	7	2.0	4	2.2	19	3.1	9	2.1	12	2.2	3	2.3	23	5.9	1	·	·	·	3	·	·	–	–	13	9	·	2	·	1
V	22	1.5	4	2.0	2	1.0	6	2.5	5	2.4	11	2.7	11	2.1	31	2.6	1	2.2	97	17.6	14	·	·	2	·	·	·	–	–	16	13	3	·	–	5
VI	26	2.3	3	1.3	1	2.0	1	2.0	2	2.5	1	2.0	14	3.8	38	2.4	4	2.5	28	6.0	16	·	·	·	8	·	·	–	–	8	7	·	·	·	4
VII	18	1.7	7	1.3	3	1.7	2	2.0	1	3.0	14	2.5	28	3.3	14	2.4	6	2.3	154	6.0	8	·	·	·	7	·	·	–	–	6	4	·	·	·	4
VIII	8	1.6	1	2.0	1	1.0	2	3.0	2	2.0	7	3.0	41	3.0	21	2.5	10	2.4	48	12.6	7	·	·	·	5	·	·	–	–	11	10	1	·	·	3
IX	10	1.6	7	2.0	9	2.3	4	3.2	·	·	9	4.4	39	3.5	40	4.7	2	2.9	50	14.1	18	·	·	·	3	2	·	–	–	12	9	1	7	·	1
X	16	1.3	5	1.0	15	1.6	2	2.5	7	2.4	8	2.2	14	2.1	17	2.6	9	1.8	13	5.2	4	·	·	3	·	·	·	–	–	10	4	·	13	·	1
XI	3	1.3	10	2.3	25	2.7	6	3.0	4	2.2	5	1.8	26	1.9	8	1.6	3	2.1	47	21.2	1	·	·	9	·	·	·	–	–	10	7	1	–	·	·
XII	8	2.2	15	2.1	10	2.3	3	1.7	·	·	21	3.5	28	2.0	7	2.1	1	2.4	34	7.8	15	10	17	27	·	·	·	–	–	9	6	·	11	17	
Rok	159	1.9	89	2.1	86	2.1	48	2.4	45	2.0	158	3.0	270	2.7	190	2.4	50	2.4	425.4	21.2	1.XI	14	31	105	26	6	2	–	–	124	93	7	–	–	20

Przebędowo $H_s = 82\ m$ $h_w = 11\ m$

I	5	7.1	4	4.8	2	1.5	4.5	6.0	29.5	4.8	29	5.6	16.5	5.5	1.5	4.3	1	5.2	14	4.0	25	2	4	18	·	5	·	1	20	8	5	·	6	3	·
II	6	6.8	19.5	5.5	1.5	2.7	1	3.0	14	4.5	12.5	5.8	14	6.9	12.5	8.1	3	5.8	22	15.6	12	2	9	24	·	8	2	·	18	12	3	1	4	4	4
III	15.5	5.0	10	3.5	9.5	3.2	13.5	3.5	9.5	3.9	9	2.6	5	5.0	8	4.2	13	3.3	18	9.8	5	3	4	25	·	1	·	1	10	8	4	·	3	13	
IV	10.5	4.8	11	3.9	7	3.7	10.5	3.6	10.5	5.0	11.5	4.7	5.5	5.0	12.5	4.2	11	3.8	18	4.3	27	·	·	3	4	1	·	·	9	12	6	·	·	·	·
V	7	3.1	4.5	2.3	2	1.5	8	3.9	15.5	3.5	26.5	3.9	14.5	5.3	9	2.9	6	3.5	101	21.5	28	·	·	4	·	·	·	·	14	18	15	3	1	1	3
VI	9	5.3	3.5	2.4	0.5	2.0	6.5	3.2	5.5	2.9	21.5	4.3	20.5	4.7	15	3.1	8	3.7	31	6.8	10	·	·	·	7	1	·	3	3	10	8	·	·	·	3
VII	8	3.6	10.5	1.8	2	2.2	4	2.9	8.5	3.7	25.5	4.6	17	3.9	8.5	3.5	9	3.3	14	3.7	4	·	·	·	5	1	·	1	7	10	6	·	3	·	3
VIII	4	2.9	2.5	2.6	1	1.0	5	2.2	10	4.6	33.5	5.2	17	5.0	7	3.2	13	3.8	29	7.0	7	·	·	·	6	2	·	1	12	12	8	·	·	·	2
IX	·	·	5	2.6	6.5	2.6	3.5	2.6	10.5	4.3	22.5	5.4	24.5	4.1	3.5	3.7	14	3.5	33	13.9	18	·	·	·	3	1	·	4	12	10	8	1	7	·	1
X	5.5	1.8	2.5	2.2	3	1.3	12.5	2.1	14.5	3.5	11	3.8	14	4.9	5	3.1	25	2.4	12	4.5	4	·	·	7	·	·	·	2	11	6	4	·	20	·	·
XI	10	4.0	10	6.6	15	4.6	13.5	3.2	6	3.1	6.5	3.0	9	5.3	5	3.0	15	3.6	31	12.0	1	·	·	10	·	2	·	1	15	11	7	1	14	·	·
XII	14	3.6	6	4.0	5	2.8	5	2.4	17	4.5	16	3.6	9	3.3	4	3.5	17	3.0	29	7.5	15	11	15	26	·	·	·	·	13	10	6	·	7	17	·
Rok	94.5	4.0	89	3.5	55	2.4	87.5	3.2	151	4.0	225	4.4	166.5	4.9	91.5	3.9	135	3.7	352	21.5	28.V	18	32	117	25	22	2	14	144	127	80	6	65	38	16

Wyszków $H_s = 96\ m$ $h_w = 13\ m$

I	4	5.8	5	2.2	·	·	2.5	2.8	16	1.9	29.5	3.4	11	3.8	9	3.8	16	2.7	26	6.4	25	3	5	22	·	·	·	2	19	13	8	·	·	18	·
II	5	6.2	4.5	4.7	9	3.1	11	2.6	4	3.7	11	5.7	14	6.5	11.5	6.0	14	4.1	43	11.1	16	6	13	27	·	4	1	·	18	18	9	2	1	28	·
III	11.5	4.5	14	2.2	7.5	3.3	13.5	2.7	3.5	4.3	3.5	2.9	5.5	3.3	13	4.9	21	2.6	39	8.0	12	10	9	29	·	1	·	5	16	12	10	·	·	15	·
IV	7.5	2.1	6.5	3.8	4	2.0	12	2.9	4.5	1.9	11	3.1	8	3.2	15.5	3.1	21	2.2	28	11.5	26	·	·	4	4	·	·	6	9	9	6	1	·	·	1
V	3	2.0	4	1.5	7	1.9	4.5	1.9	3.5	1.9	11	2.5	10.5	3.5	16.5	2.5	33	1.6	150	29.9	14	·	·	3	·	·	·	2	14	19	17	5	·	·	4
VI	6	4.4	6.5	3.6	2	3.0	2	1.2	4	1.4	12.5	3.3	17.5	2.6	11.5	3.5	28	2.1	89	34.5	29	·	·	·	6	1	·	5	10	14	10	2	·	·	3
VII	5	2.0	9	1.8	1	1.0	3	1.0	3.5	2.1	13	2.5	21	2.7	10.5	2.5	27	1.6	45	21.2	12	·	·	·	6	·	·	4	9	10	8	1	·	·	4
VIII	·	·	1	1.0	4	2.8	5	6.0	10	1.5	19	3.0	15	3.4	9	2.1	30	2.0	61	10.2	5	·	·	·	6	·	·	2	11	15	12	1	2	·	4
IX	1	1.0	2.5	1.0	6.5	1.6	5	1.8	6.5	1.5	16	3.7	15	3.0	9.5	2.5	28	1.8	82	13.3	21	·	·	·	1	·	·	4	9	15	13	4	3	·	3
X	2	1.0	·	·	6.5	1.6	10.5	1.6	3	1.7	17.5	2.2	7.5	2.7	10	1.5	36	1.2	40	2.5	28	·	·	6	·	·	·	4	11	9	5	·	5	·	·
XI	2	9.0	9	5.6	22	4.8	8	2.1	3.5	4.3	7	2.4	8	1.6	6.5	4.2	24	2.6	42	7.8	15	·	·	10	·	1	1	1	22	11	10	·	4	·	·
XII	8	3.5	13.5	2.3	5.5	1.9	4.5	1.4	5.5	2.1	18	2.5	11.5	2.3	8.5	1.7	18	1.9	42	2.0	16	11	17	28	·	·	·	4	21	10	5	·	1	16	·
Rok	55	3.5	75.5	2.5	75	2.2	81.5	2.3	67.5	1.9	169	3.1	144.5	3.2	131	3.0	296	2.2	627	34.5	29.VI	30	44	129	23	7	2	39	169	155	113	16	16	77	19

Gorzyń $H_s = 60\ m$ $h_w = 15\ m$

I	2	4.5	4	2.8	1.5	2.7	3.5	3.7	14	3.4	39.5	4.1	15.5	3.6	10	3.6	3	3.6	27	6.4	12	1	4	10	·	1	·	1	19	16	8	·	3	–	·
II	5.5	6.1	8	4.1	12.5	3.7	1.5	3.7	11	2.8	11	7.0	25.5	6.5	7	6.6	2	5.2	51	24.6	16	2	7	23		5	2		18	16	8	1	1	–	·
III	6	4.0	5	2.7	17	3.3	14	3.7	11	2.8	4	2.0	9.5	4.4	9.5	2.7	17	2.7	28	7.9	31	·	3	27	·	·	·	4	8	12	6	·	1	–	·
IV	7.5	3.3	4	4.2	10.5	3.9	6	3.2	7.5	3.7	16.5	3.6	16	3.0	10	2.2	12	2.9	40	19.3	29	·	·	·	5	·	·	4	8	13	9	1	2	–	2
V	2	3.5	·	·	·	·	7	3.7	4	2.5	12	2.6	38	2.8	13	2.2	17	2.2	121	18.8	25	·	·	1	·	·	·	·	12	19	15	5	·	·	7
VI	7.5	3.5	2	1.0	·	·	2	2.5	2	3.5	5	3.0	36	3.2	19.5	2.4	16	2.4	59	38.8	16	·	·	·	7	1	1	4	5	11	6	1	·	·	4
VII			1	3.0	·	·	1	2.0	5.5	2.0	19	3.2	31	2.5	7.5	1.9	28	1.8	41	9.4	21	·	·	·	4	·	·	2	9	12	7	·	·	·	3
VIII	·	·	0.5	4.0	0.5	4.0	1	3.0	6	2.8	25.5	2.7	42.5	2.8	4	2.0	13	2.4	46	12.5	24	·	·	·	5	·	·	1	11	14	12	1	·	·	4
IX		·	·	·	9	3.1	8	3.7	5.5	3.0	18	3.7	33.6	3.3	5	2.2	11	2.9	42	11.0	23	·	·	·	3	2	1	4	3	14	10	1	4	·	·
X	2	2.0		·	2	2.5	17	2.5	8	2.2	10	2.4	26	1.9	5	3.6	23	1.7	18	7.2	31	·	·	·	·	·		4	10	7	4	·	8	·	1
XI	1	1.0	4.5	7.3	17.5	4.6	8	4.1	4	2.4	16	1.4	12.5	3.3	3.5	2.0	23	2.5	24	7.2	1	·	·	7	·	1	·	1	18	11	8	·	10	–	·
XII	3	2.0	8.5	3.6	14.5	3.6	4	1.8	9	4.1	9.5	4.8	27	2.3	4.5	2.9	13	2.7	39	9.8	11	7	16	26	·	·	·	3	18	14	6	·	5	–	·
Rok	36.5	2.5	37.5	2.7	86	2.6	73	3.1	87.5	2.9	186	3.4	313	3.3	98.5	2.9	178	2.8	536	38.8	16.VI	10	30	94	24	10	4	28	139	159	99	10	34	–	21

Trzemeszno $\varphi = 52°34'$ $\lambda = 17°49'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.5	-1.7	8.7	22	-14.8	31	-0.3	1.6	0.0	0.3	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.2	7.5	8.0
II	–	–	–	–	1.1	-4.2	6.3	20	-13.7	1	-2.5	0.1	-1.5	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	9.2	9.2	7.4	8.6
III	–	–	–	–	2.7	-3.8	13.4	31	-10.1	7	-2.8	2.1	-1.0	-0.7	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.0	7.0	7.1
IV	–	–	–	–	15.3	5.8	27.6	23	0.5	2,30	8.2	14.2	9.7	10.4	9.3	9.7	10.1	9.7	8.4	6.2	8.2	7.6	2.0	8.1	2.6	4.2	8.0	7.5	6.5	7.3
V	–	–	–	–	14.7	6.8	20.5	19	-2.1	1	9.3	13.6	9.9	10.7	10.7	10.8	10.7	10.7	9.0	6.9	8.7	8.2	1.2	5.2	1.7	2.7	8.1	8.7	7.7	8.2
VI	–	–	–	–	19.8	9.6	31.0	16	2.2	3	13.2	18.4	13.9	14.8	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.1	6.2	6.4
VII	–	–	–	–	21.0	10.6	31.3	26	4.5	29	14.4	19.7	14.6	15.8	14.2	14.0	13.9	14.0	8.6	6.2	8.3	7.7	2.4	9.8	3.0	5.1	7.2	7.7	6.5	7.1
VIII	–	–	–	–	21.7	12.6	29.2	13	8.2	10	15.1	20.5	15.7	16.8	14.6	14.5	14.8	14.6	8.4	6.1	8.3	7.6	2.8	10.3	3.2	5.4	7.4	8.1	6.8	7.4
IX	–	–	–	–	17.6	8.2	29.3	4	2.9	25	10.0	16.5	11.7	12.5	11.5	12.3	12.0	11.9	9.2	6.6	8.7	8.2	1.1	7.1	2.0	3.4	7.2	7.0	5.4	6.5
X	–	–	–	–	13.1	4.9	21.9	3	-1.5	16	6.7	12.6	7.4	8.5	9.6	10.9	9.7	10.1	9.5	7.4	9.2	8.7	0.5	4.2	0.9	1.9	8.0	6.9	5.5	6.8
XI	–	–	–	–	5.4	2.1	13.8	5	-1.6	17	2.9	4.8	3.5	3.7	7.2	7.9	7.4	7.5	9.5	9.0	9.3	9.3	0.4	1.1	0.6	0.7	8.7	8.5	8.2	8.5
XII	–	–	–	–	-2.3	-6.7	5.9	12	-18.5	22	-5.1	-3.2	-4.6	-4.4	4.0	4.5	4.2	4.2	8.7	8.7	8.6	8.7	0.4	0.6	0.5	0.5	9.1	7.7	7.0	7.9
Rok	–	–	–	–	11.0	3.7	31.3	26.VII	-18.5	22.XII	5.8	10.1	6.6	7.3	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.8	6.8	7.5

Gniezno $\varphi = 52°33'$ $\lambda = 17°36'$

I	–	–	–	–	2.5	-1.8	9.2	22	-16.3	31	-0.4	1.3	-0.1	0.2	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.6	8.1	8.3
II	–	–	–	–	0.9	-3.8	5.9	20	-14.5	1	-2.7	-0.2	-1.4	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	8.8	9.0	7.2	8.3
III	–	–	–	–	3.0	-4.3	13.3	31	-11.9	9	-3.1	1.8	-1.0	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.6	6.8	6.7
IV	–	–	–	–	15.4	5.7	27.7	23	0.2	30	7.4	13.6	9.5	10.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.1	5.0	6.5
V	–	–	–	–	15.1	6.7	20.4	19	-1.8	1	8.8	13.6	9.6	10.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	8.4	6.8	7.5
VI	–	–	–	–	20.4	9.4	31.5	16	3.2	3,4	13.1	18.6	13.6	14.7	–	–	–	–	–	–	–	–	–	–	–	–	5.2	6.4	5.6	5.7
VII	–	–	–	–	21.3	10.6	32.1	26	6.5	29	14.0	19.7	14.6	15.7	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.3	5.2	6.4
VIII	–	–	–	–	22.0	12.3	29.9	12	7.1	10	14.4	20.4	15.4	16.4	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.7	6.2	7.1
IX	–	–	–	–	17.5	8.0	(29.4)	4	2.2	25	9.7	16.2	11.3	12.1	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.9	5.7	6.4
X	–	–	–	–	13.2	4.5	21.9	3	-1.2	16	6.5	12.1	6.9	8.1	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.8	4.7	5.8
XI	–	–	–	–	5.4	1.9	13.3	5	-1.4	18,22	2.7	4.6	3.5	3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.4	7.6	8.2
XII	–	–	–	–	-2.1	-6.7	5.9	12	-19.0	22	-5.2	-3.4	-4.6	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.8	6.8	7.8
Rok	–	–	–	–	11.2	3.5	32.1	26.VII	-19.0	22.XII	5.4	9.9	6.4	7.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.6	6.3	7.1

Krzemień $\varphi = 52°33'$ $\lambda = 22°30'$

I	–	–	–	–	1.1	-3.5	6.3	22	-19.6	31	-1.4	0.3	-1.4	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	-0.8	-6.8	3.4	12	-16.0	1	-4.5	-2.2	-3.3	-3.3	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.8	7.3	7.2
III	–	–	–	–	0.2	-8.4	7.7	31	-20.8	27	-5.7	-0.7	-4.0	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	7.0	5.3	5.6	6.0
IV	–	–	–	–	14.9	5.6	27.2	22	-0.1	30	8.0	13.9	9.5	10.2	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.0	4.9	5.1
V	–	–	–	–	15.1	7.0	19.9	13	-1.3	1	9.9	14.0	10.5	11.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	19.2	9.3	28.2	16	4.1	6	13.9	17.7	12.9	14.4	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.7	3.5	4.7
VII	–	–	–	–	20.8	10.6	27.4	27	6.4	5	15.1	19.4	14.7	16.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.7	11.4	30.7	13	6.2	10	15.2	20.6	15.9	16.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	16.9	7.6	26.7	5	1.2	25	10.4	15.7	11.6	12.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	12.3	3.4	19.3	2,3	-3.5	16	6.2	11.5	6.5	7.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	1.9	17.5	1	-2.2	27	3.5	5.5	3.8	4.2	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.7	8.0	7.9
XII	–	–	–	–	–	-7.4	–	–	-20.6	21	-5.5	-3.9	-5.1	-4.9	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.5	6.5	6.7
Rok	–	–	–	–	–	2.6	30.7	13.VIII	-20.8	27.III	5.4	9.3	6.0	6.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Płock-Radziwie $\varphi = 52°32'$ $\lambda = 19°40'$

I	1007.5	1033.4	981.4	1015.6	2.4	-1.9	8.9	22	-15.0	31	-0.1	1.3	0.1	0.3	5.4	5.5	5.4	5.4	8.7	8.1	8.4	8.4	0.9	1.4	1.0	1.1	7.5	8.5	7.6	7.9
II	1007.5	1029.5	973.8	1015.7	0.8	-4.4	4.6	20	-13.7	3	-3.0	-0.5	-1.8	-1.8	4.4	4.8	4.7	4.6	8.6	8.0	8.5	8.4	0.8	1.2	0.8	0.9	8.6	9.0	7.7	8.4
III	1004.0	1020.7	981.3	1012.0	2.2	-3.9	12.8	31	-10.6	15	-3.0	0.8	-0.9	-1.0	4.4	4.9	4.8	4.7	8.8	7.3	8.2	8.1	0.6	1.8	1.0	1.1	7.6	7.5	6.1	7.1
IV	1006.3	1021.2	980.1	1014.1	15.8	6.0	28.5	23	0.3	8	7.7	14.2	10.0	10.5	9.3	9.5	10.0	9.8	8.7	6.0	7.9	7.5	1.6	8.4	3.0	4.3	7.1	7.0	5.5	6.5
V	1005.1	1012.9	984.3	1012.8	15.4	6.8	20.7	31	-2.7	1	9.3	13.7	10.7	11.1	10.6	10.3	11.2	10.7	8.8	6.7	8.5	8.0	1.4	5.8	2.0	3.1	7.6	8.3	7.0	7.6
VI	1010.2	1021.3	999.1	1017.8	20.3	10.4	30.3	16	4.5	3	13.4	18.6	14.9	15.4	12.1	11.6	13.1	12.3	7.6	5.4	7.5	6.8	3.7	10.9	4.4	6.3	6.8	6.6	5.9	6.4
VII	1006.7	1017.8	992.4	1014.3	21.6	11.2	30.7	26	5.8	29	14.4	19.8	15.8	16.4	14.1	13.5	14.2	13.9	8.6	5.9	7.9	7.5	2.4	10.2	4.1	5.6	6.3	6.7	5.7	6.2
VIII	1007.6	1016.7	996.3	1015.2	22.3	12.6	31.7	7	8.1	10	14.8	20.4	16.0	16.8	14.7	14.9	15.6	15.1	8.6	6.3	8.5	7.8	2.3	10.0	2.9	5.1	6.7	7.6	5.5	6.6
IX	1008.4	1023.6	990.3	1016.1	17.6	8.4	28.8	4	4.2	15	10.0	16.2	11.9	12.5	11.3	12.4	12.7	12.1	9.1	6.8	9.0	8.3	1.2	6.6	1.5	3.1	6.8	7.4	5.2	6.5
X	1014.8	1029.5	1002.2	1022.7	13.3	4.7	20.6	2	-3.1	16	6.0	12.6	8.0	8.6	9.3	10.9	10.1	10.1	9.6	7.4	9.2	8.7	0.4	4.1	0.9	1.8	7.9	6.3	6.2	6.8
XI	1010.2	1026.3	990.9	1018.2	5.9	2.3	12.5	4	-3.9	26	3.3	5.1	4.1	4.2	7.3	7.5	7.4	7.4	9.2	8.4	8.9	8.8	0.7	1.5	1.0	1.1	8.5	8.6	8.0	8.4
XII	1009.2	1038.6	965.4	1017.4	-2.3	-6.9	4.9	12	-18.9	21	-4.7	-3.4	-4.4	-4.2	4.1	4.4	4.1	4.2	8.8	8.4	8.6	8.6	0.5	0.7	0.6	0.6	8.5	8.3	7.6	8.1
Rok	1008.1	1038.6	965.4	1016.0	11.3	3.8	31.7	7.VIII	-18.9	21.XII	5.7	9.9	7.0	7.4	8.9	9.2	9.4	9.2	8.8	7.1	8.4	8.1	1.4	5.2	1.9	2.8	7.5	7.6	6.5	7.2

Trzemeszno $H_s = 105\,m$ $h_w = 15.4\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v≥10	v>15	◑	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	π/Γ
I	2	4.7	6.5	2.5	2.5	1.4	4.5	2.1	15	2.8	27.5	3.6	27	3.8	8	4.1	·	3.4	22	6.0	25	3	4	20	·	1	·	2	17	11	8	·	2	12	·
II	3.5	2.9	12	3.5	8.5	3.1	3	2.2	10.5	2.0	14	4.9	17.5	4.9	15	4.6	·	3.9	46	14.4	12	3	9	24	·	1	·	·	19	16	10	1	1	16	·
III	7.5	1.5	19.5	1.6	10.5	2.8	15.5	1.9	12.5	1.2	6	1.1	7.5	2.7	14	3.0	·	2.0	32	11.7	5	1	5	27	·	·	·	1	11	12	5	1	5	18	·
IV	9	2.4	11	2.4	10.5	2.0	10	2.0	11.5	2.9	10	3.0	10.5	2.2	17.5	2.1	·	2.3	29	7.7	29	·	·	·	3	·	·	·	12	14	8	·	1	·	1
V	6.5	1.2	6	1.4	1.5	1.0	9	1.4	12	1.3	10	1.4	23.5	1.9	24.5	2.9	·	1.9	99	28.2	14	·	·	1	·	·	·	·	19	26	20	1	1	·	6
VI	10.5	2.0	6	2.0	3	1.0	4	2.1	7.5	1.5	14.5	2.0	24	2.6	20.5	2.0	·	2.1	28	6.9	29	·	·	·	6	·	·	2	10	9	9	·	·	·	2
VII	7.5	1.3	13	1.0	3	1.2	15	1.0	8	1.6	17	1.8	24.5	1.8	18.5	1.6	·	1.5	28	5.1	3	·	·	·	5	·	·	1	11	14	10	·	·	·	2
VIII	6	1.0	5	1.2	2.5	1.4	4	1.8	7.5	1.7	18	2.6	32	2.7	18	1.7	·	2.1	41	9.2	24	·	·	·	6	·	·	1	13	15	11	·	·	·	1
IX	2.5	1.4	5	1.1	11	1.9	5	1.5	6	1.8	11.5	1.7	31	2.5	17	1.9	1	1.9	51	26.9	18	·	·	·	2	·	·	3	12	12	8	1	4	·	2
X	4	1.0	4.5	1.0	11	1.1	19	1.5	10	1.6	10	1.4	21	2.3	13.5	1.9	·	1.6	18	10.2	31	·	·	2	·	·	·	1	10	8	4	1	11	·	·
XI	3.5	1.3	4.5	2.0	29.5	2.6	10	1.7	10.5	1.3	14.5	1.8	14	2.2	3.5	1.7	·	2.0	44	13.4	1	·	·	9	·	·	·	1	22	15	11	1	4	·	·
XII	4	1.0	20.5	1.5	8	1.6	8	1.2	10	2.6	15	2.5	19	2.5	8.5	1.8	·	2.0	15	7.0	15	9	18	27	·	·	·	1	18	13	4	·	6	17	·
Rok	66.5	1.8	113.5	1.8	101.5	1.8	93.5	1.7	121	1.9	168	2.3	251.5	2.7	178.5	2.4	1	2.2	453	28.2	14.V	16	36	110	22	2	·	13	174	165	108	6	35	63	14

Gniezno $H_s = 110\,m$ $h_w = 10\,m$

I	1	5.5	6.5	4.2	0.5	1.0	0.5	1.0	18	2.0	46	3.4	14.5	3.2	3	8.7	3	3.2	26	6.6	25	3	4	19	·	4	1	1	17	14	8	·	3	12	·
II	5.5	8.7	12	5.1	7.5	3.5	1.5	1.0	10.5	3.0	24	6.9	16	5.6	5	3.3	2	5.2	48	18.5	12	2	11	24	·	8	6	·	16	14	10	2	3	14	·
III	7	6.6	13	2.9	3	2.0	8.5	2.8	14	1.8	8.5	1.8	9.5	2.1	8.5	4.2	21	2.3	46	18.5	6	2	3	28	·	3	·	4	14	11	8	2	3	16	·
IV	5.5	3.9	15	4.6	5	5.6	3.5	1.6	15.5	2.0	18	3.2	5	3.2	9.5	2.7	13	2.8	39	14.1	29	·	·	·	3	3	1	3	9	14	10	1	·	1	3
V	3	3.2	3.5	1.9	3	1.0	3.5	1.4	7	2.6	20	2.1	26.5	2.5	8.5	5.4	18	2.1	108	35.5	14	·	·	1	·	3	·	·	13	26	23	1	·	1	5
VI	8.5	4.1	5.5	4.5	1	3.0	0.5	1.0	6.5	1.2	12	2.4	31.5	3.1	13.5	2.4	11	2.6	33	5.8	29	·	·	·	7	2	1	2	6	13	9	·	·	·	3
VII	4.5	1.3	7	2.0	0.5	1.0	0.5	1.0	5.5	1.5	19.5	1.8	27	2.7	5.5	2.3	23	1.6	26	6.6	2	·	·	·	7	1	·	1	11	12	7	·	1	·	5
VIII	4.5	1.2	2	1.0	1	1.0	3	1.7	9.5	1.8	22	3.3	31	3.0	3	3.3	17	2.2	42	10.9	24	·	·	·	7	·	·	1	12	15	13	1	1	·	1
IX	2	1.5	1.5	1.0	9.5	1.9	2	3.5	6	2.2	26	3.2	21	2.8	7	1.9	15	2.2	60	24.7	18	·	·	·	1	2	1	3	13	16	10	2	4	·	2
X	4	1.2	2.5	1.4	2.5	1.4	5	1.2	19	1.2	17	1.6	12	2.6	5	1.4	26	1.2	13	8.7	31	·	·	4	·	·	·	4	10	8	3	·	15	·	·
XI	3	2.0	5.5	5.9	18	5.4	13	2.7	8	1.2	16	2.0	8.5	1.5	2	1.7	16	2.5	43	15.3	1	·	·	10	·	2	·	2	21	13	9	1	13	·	·
XII	8	1.4	14.5	3.2	5	4.0	2.5	2.2	10	2.3	21	3.0	19.5	1.7	3.5	2.1	9	2.3	23	10.1	15	10	17	28	·	·	·	3	18	9	5	1	10	17	·
Rok	56.5	3.4	88.5	3.1	56.5	2.6	44	1.8	129.5	1.9	250	2.9	222	2.8	74	3.3	174	2.5	507	35.5	14.V	17	35	114	25	28	10	24	160	165	115	11	53	61	19

Krzemień $H_s = 111\,m$ $h_w = 10\,m$

I	6	7.6	3	1.3	·	·	4	3.2	15.5	4.3	25.5	4.4	15.5	4.5	1.5	3.0	22	3.4	19	10.2	25	4	7	21	·	2	·	–	–	11	4	1	1	19	·
II	7	5.3	6	4.9	11	3.4	4.5	4.5	6	3.5	7	5.4	17.5	6.0	8	7.6	17	4.2	17	6.2	12	8	14	27	·	3	·	–	–	10	5	·	1	28	·
III	6	7.1	11.5	3.2	7	3.8	15	3.8	0.5	2.0	2.5	7.0	4.5	5.0	11	4.1	35	2.7	31	7.6	12	10	16	28	·	2	·	–	–	10	7	·	1	23	·
IV	7.5	3.2	10.5	4.3	4	4.1	15.5	3.2	3	3.8	8	3.8	2	3.8	12.5	3.4	27	2.5	41	14.3	26	·	·	1	3	·	·	–	–	11	9	1	1	·	2
V	1.5	2.3	2.5	3.4	2.5	3.4	4.5	3.6	4	2.4	6	2.3	13.5	4.3	7.5	2.9	51	1.5	104	16.0	14	·	·	1	·	·	·	–	–	17	14	3	·	·	3
VI	12.5	7.3	1	2.0		·	1	3.0	2.5	4.2	11	4.1	17	3.9	7	2.8	38	2.6	88	25.8	4	·	·	·	4	1	·	–	–	11	7	4	·	·	2
VII	3.5	4.0	1	3.0	·	·	1	2.5	6	3.0	9.5	3.2	22.5	3.3	9.5	3.0	40	1.8	67	23.6	23	·	·	·	5	·	·	–	–	12	10	2	·	·	7
VIII					0.5	5.0	1	4.0	4.5	4.2	19	3.8	21	4.3	4	3.6	43	2.2	50	14.1	16	·	·	·	6	2	1	–	–	12	10	1	·	·	2
IX	2.5	4.0	5	3.0	0.5	2.0	3	2.3	4.5	3.8	15	3.9	23	4.1	3.5	3.6	33	2.4	81	20.0	18	·	·	·	2	·	·	–	–	13	10	3	2	·	1
X	1.5	3.0	0.5	1.0	4.5	1.7	5.5	2.8	0.5	3.0	7	3.9	9	3.7	6.5	4.7	58	1.3	5	2.0	27	·	·	5	·	·	·	–	–	3	3	·	10	·	·
XI	2	3.5	2	9.2	19.5	6.2	19.5	4.6	2	4.0	5.5	3.5	9.5	3.9	4	3.0	26	3.5	52	9.3	30	·	–	8	·	3	·	–	–	12	11	·	2	1	–
XII	10.5	3.4	9	3.8		·	11	2.8	6.5	4.4	6.5	5.0	15.5	2.9	3	2.8	31	2.3	13	6.6	14	11	–	26	·	1	·	–	–	10	4	·	·	17	·
Rok	60.5	4.2	52	3.3	49.5	2.5	85.5	3.4	55.5	3.6	122.5	4.2	170.5	4.1	78	3.7	421	2.5	568	25.8	4.VI	33	–	117	20	14	1	–	–	132	94	15	18	88	17

Płock-Radziwie $H_s = 63\,m$ $H_b = 63.8\,m$ $h_w = 14\,m$

I	4	6.6	4	5.4	4	3.2	7.5	2.5	11	3.6	33	5.4	25	5.2	3.5	4.4	1	4.7	25	12.8	25	3	6	17	·	2	·	2	18	9	6	1	4	4	·
II	5.5	4.4	6.5	5.0	12	3.7	7.5	2.8	5	4.7	10.5	4.9	19	6.6	10	7.0	8	4.7	31	8.5	12	2	12	23	·	4	2	1	20	19	8	·	4	16	·
III	10	4.7	6	3.2	19.5	3.0	19.5	3.7	4	1.8	3.5	2.3	9.5	4.7	12	3.6	9	3.2	44	13.7	5	1	7	27	·	2	·	2	13	14	7	2	2	10	·
IV	8.5	4.1	8	4.4	11.5	3.6	14	4.0	6.5	3.3	14	3.6	5	3.1	13.5	4.1	9	3.5	20	4.0	13	·	·	·	5	1	·	3	9	11	7	·	1	·	1
V	1.5	1.0	7	2.4	7	1.9	11	3.3	6.5	2.8	19	3.3	20	4.0	13	4.6	8	3.2	178	83.8	14	·	·	3	·	2	·	1	15	25	19	3	3	·	5
VI	11.5	4.4	2	3.5	8.5	1.9	7.5	2.5	3.5	2.6	11.5	4.3	27.5	4.7	16	3.4	2	3.7	76	22.5	29	·	·	·	6	1	·	1	9	13	11	2	·	·	4
VII	8	2.9	3.5	2.6	4.5	2.2	4.5	3.1	3	2.8	19	3.2	34	3.0	9.5	2.8	7	2.8	32	8.6	2	·	·	·	6	1	·	·	4	12	8	·	·	·	5
VIII	2	2.0	1.5	2.3	7	3.6	6	2.2	5.5	3.2	23.5	4.0	28	4.6	7.5	3.5	12	3.4	53	10.8	17	·	·	·	8	1	·	·	10	14	11	1	2	·	5
IX	1.5	2.3	3	2.3	11.5	2.9	10.5	2.6	5.5	3.3	18	4.6	25.5	3.7	6.5	3.8	8	3.2	65	20.6	18	·	·	·	2	·	·	2	11	14	13	1	5	·	4
X	4	3.1	4	1.9	10.5	2.2	22.5	2.4	3	2.0	11.5	3.1	13	3.7	4.5	2.9	20	2.2	16	5.4	6	·	·	3	·	2	·	1	11	8	6	·	16	·	·
XI	2.5	3.6	4.5	5.0	25	3.8	16.5	3.7	3	2.5	14	2.4	13	3.2	2.5	2.6	9	3.1	42	9.8	20	·	·	8	·	·	·	1	21	13	9	·	6	1	·
XII	5	1.6	8.5	3.5	10.5	2.3	14	2.1	8.5	4.3	15	4.1	20	2.8	2.5	3.0	9	2.7	13	3.9	16	9	16	27	·	·	·	1	19	9	3	·	6	16	·
Rok	64	3.4	58.5	3.5	131.5	2.9	141	2.9	65	3.1	192.5	3.8	239.5	4.1	101	3.8	102	3.4	595	83.8	14.V	15	41	108	27	16	2	15	160	161	108	10	49	47	24

Przybroda $\varphi = 52°31'$ $\lambda = 16°40'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	P_{0m}	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	-	-	-	-	2.9	-1.4	9.6	22	-13.0	31	0.3	2.0	0.5	0.8	5.4	5.6	5.3	5.4	84	77	81	81	1.0	1.7	1.2	1.3	8.3	8.1	7.5	8.0
II	-	-	-	-	1.7	-3.1	7.5	20	-12.5	1	-1.7	0.7	-0.7	-0.6	4.5	5.1	4.6	4.7	80	76	78	78	1.0	1.5	1.3	1.3	8.5	9.0	6.4	8.0
III	-	-	-	-	3.1	-3.5	13.6	30	-11.0	8	-2.0	2.4	-0.5	-0.2	4.4	4.6	4.5	4.5	79	61	74	71	1.0	2.9	1.6	1.8	6.9	6.5	5.1	6.2
IV	-	-	-	-	15.1	5.1	26.9	23	0.0	1	7.5	13.8	9.2	9.9	9.0	8.9	9.3	9.1	84	54	76	71	1.8	8.3	3.0	4.4	6.3	6.5	5.2	6.0
V	-	-	-	-	14.7	5.7	21.1	19	-2.2	1	9.2	13.4	9.4	10.4	10.3	9.7	10.2	10.1	87	63	85	78	1.6	6.1	1.8	3.2	7.4	7.4	6.5	7.1
VI	-	-	-	-	19.9	8.8	30.3	16	2.0	3	13.3	18.0	13.3	14.5	11.4	10.9	11.9	11.4	72	53	75	67	4.4	10.8	3.9	6.4	4.4	5.7	5.4	5.2
VII	-	-	-	-	21.1	10.1	32.3	26	5.0	29	14.6	19.6	14.3	15.7	13.6	11.8	13.3	12.9	82	54	82	73	3.3	11.9	3.3	6.2	5.9	6.6	5.5	6.0
VIII	-	-	-	-	21.6	11.7	29.6	12	7.4	9	15.0	20.1	15.3	16.4	14.1	13.3	14.0	13.8	82	58	80	73	3.1	10.9	3.6	5.9	7.2	7.1	5.0	6.4
IX	-	-	-	-	17.6	7.8	29.1	4	3.4	25	10.3	16.5	11.8	12.6	11.1	11.3	11.4	11.3	88	62	83	78	1.6	8.1	2.6	4.1	6.5	6.6	3.8	5.6
X	-	-	-	-	12.7	4.5	23.0	3	-0.8	16	6.7	11.9	7.5	8.4	9.3	10.1	9.5	9.6	92	71	88	84	0.8	4.5	1.4	2.2	7.2	6.3	3.9	5.8
XI	-	-	-	-	5.8	2.2	15.5	8	-1.8	21	3.1	5.2	3.9	4.0	6.9	7.5	7.2	7.2	89	83	87	86	0.9	1.7	1.0	1.2	8.4	8.2	8.0	8.2
XII	-	-	-	-	-1.9	-6.3	6.0	12	-18.2	22	-4.5	-2.9	-4.1	-3.9	-	-	-	-	-	-	-	-	-	-	-	-	8.7	7.5	6.7	7.6
Rok	-	-	-	-	11.2	3.5	32.3	26.VII	-18.2	22.XII	6.0	10.1	6.7	7.4	-	-	-	-	-	-	-	-	-	-	-	-	7.1	7.1	5.8	6.7

Wieliszew $\varphi = 52°27'$ $\lambda = 20°58'$

I	-	-	-	-	2.2	-2.4	8.9	22	-14.0	31	-0.7	0.9	-0.5	-0.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	0.2	-5.4	4.5	12	-16.1	1	-3.7	-1.2	-2.6	-2.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	1.7	-5.5	12.7	31	-13.4	15	-3.3	0.3	-1.8	-1.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	15.9	6.2	27.7	23	-0.1	8	8.4	14.3	10.5	10.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	15.5	7.0	23.9	23	-1.7	1	9.6	13.6	11.2	11.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	-	-	-	19.7	9.9	29.4	23	5.8	7	12.7	17.5	15.2	15.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	-	-	-	21.5	10.6	29.9	26	6.4	4	13.4	19.5	16.1	16.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	-	-	-	22.1	10.7	30.3	7	5.9	27	14.0	20.0	16.5	16.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	-	-	-	17.2	6.1	26.6	4	0.6	15	9.8	15.4	12.0	12.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	-	-	-	12.7	3.6	20.4	2	-4.3	17	5.9	11.6	7.7	8.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	6.8	1.8	15.2	4	-2.3	17	3.2	5.3	4.1	4.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-	-	-	-1.8	-7.0	6.6	12	-18.9	22	-5.2	-3.9	-4.8	-4.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Rok	-	-	-	-	11.1	3.0	30.3	7.VIII	-18.9	22.XII	5.3	9.4	7.0	7.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Sulęcin $\varphi = 52°26'$ $\lambda = 15°07'$

I	-	-	-	-	4.0	-0.9	10.0	22	-14.7	31	0.8	2.8	1.0	1.4	-	-	-	-	-	-	-	-	-	-	-	-	9.1	8.7	9.3	9.0
II	-	-	-	-	2.3	-2.7	7.9	8	-12.2	1	-1.1	1.2	-0.5	-0.2	-	-	-	-	-	-	-	-	-	-	-	-	9.5	9.2	8.8	9.2
III	-	-	-	-	3.8	-4.0	15.0	30	-11.7	8	-2.6	3.0	-0.7	-0.2	-	-	-	-	-	-	-	-	-	-	-	-	6.6	7.3	4.6	6.2
IV	-	-	-	-	15.0	4.4	28.3	25	-2.2	11	6.7	13.3	8.1	9.0	-	-	-	-	-	-	-	-	-	-	-	-	7.7	6.1	4.8	6.2
V	-	-	-	-	14.6	5.6	21.2	19	-2.2	1	9.0	13.2	9.3	10.2	-	-	-	-	-	-	-	-	-	-	-	-	7.2	8.5	7.0	7.6
VI	-	-	-	-	20.3	7.7	30.8	15	0.0	3	13.2	18.7	13.4	14.7	-	-	-	-	-	-	-	-	-	-	-	-	5.3	5.8	6.8	6.0
VII	-	-	-	-	20.6	10.2	31.2	26	4.4	29	13.9	18.8	14.0	15.2	-	-	-	-	-	-	-	-	-	-	-	-	7.3	7.0	8.0	7.4
VIII	-	-	-	-	21.0	11.3	29.8	12	6.1	10	14.1	19.6	14.4	15.6	-	-	-	-	-	-	-	-	-	-	-	-	7.8	7.2	7.0	7.3
IX	-	-	-	-	17.6	7.2	27.1	4	0.4	15	9.7	16.6	10.5	11.8	-	-	-	-	-	-	-	-	-	-	-	-	7.7	6.8	4.0	6.1
X	-	-	-	-	13.3	3.6	23.4	2	-2.2	16	6.2	12.3	6.6	7.9	-	-	-	-	-	-	-	-	-	-	-	-	8.6	7.0	5.0	6.9
XI	-	-	-	-	5.9	1.2	15.8	8	-4.0	25	2.8	5.2	2.9	3.4	-	-	-	-	-	-	-	-	-	-	-	-	8.9	8.6	7.6	8.4
XII	-	-	-	-	-1.4	-6.2	6.4	12	-17.4	22	-4.5	-2.3	-3.9	-3.6	-	-	-	-	-	-	-	-	-	-	-	-	8.4	7.7	7.2	7.8
Rok	-	-	-	-	11.4	3.1	31.2	26.VII	-17.4	22.XII	5.7	10.2	6.3	7.1	-	-	-	-	-	-	-	-	-	-	-	-	7.8	7.5	6.7	7.3

Poznań-Sołacz $\varphi = 52°26'$ $\lambda = 16°54'$

I	-	-	-	-	3.2	-1.2	9.5	22	-13.3	31	0.4	2.2	0.7	1.0	5.6	5.9	5.6	5.7	87	81	85	84	0.9	1.4	1.1	1.1	-	-	-	-
II	-	-	-	-	1.6	-3.1	7.5	20	-13.1	1	-1.8	0.5	-0.6	-0.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	3.6	-3.6	14.0	30	-10.8	8	-2.3	2.6	-0.2	0.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	15.8	5.6	27.6	23	-1.3	11	7.6	14.0	9.9	10.4	8.8	9.1	9.6	9.2	82	57	76	72	2.1	8.4	3.3	4.6	-	-	-	-
V	-	-	-	-	15.1	6.6	22.0	19	-1.8	1	8.9	13.7	10.4	10.8	9.9	9.7	10.5	10.0	86	61	82	76	1.7	6.5	2.4	3.5	-	-	-	-
VI	-	-	-	-	20.3	9.6	31.0	16	2.8	3,6	13.3	18.5	14.6	15.2	11.4	11.1	12.4	11.6	73	52	72	66	4.4	11.4	4.8	6.9	-	-	-	-
VII	-	-	-	-	21.2	10.7	32.0	26	5.3	29	13.9	20.0	15.4	16.2	13.3	12.4	14.0	13.2	83	54	79	72	2.9	11.9	4.0	6.3	-	-	-	-
VIII	-	-	-	-	21.7	12.4	29.5	12	7.3	10	14.5	20.2	16.1	16.7	14.0	13.6	14.3	14.0	84	58	78	73	2.7	10.7	4.3	5.9	-	-	-	-
IX	-	-	-	-	17.7	8.0	29.0	4	3.1	15	9.7	16.5	11.6	12.4	10.8	11.7	11.7	11.4	89	63	86	79	1.5	7.7	2.2	3.8	-	-	-	-
X	-	-	-	-	12.9	4.6	22.7	3	-2.4	16	6.6	11.9	7.6	8.4	9.2	10.5	9.7	9.8	92	75	89	85	0.8	3.9	1.2	2.0	-	-	-	-
XI	-	-	-	-	6.0	2.4	15.6	8	-1.8	22	3.2	5.2	4.1	4.2	7.0	7.5	7.4	7.3	89	84	88	87	0.8	1.6	1.0	1.1	-	-	-	-
XII	-	-	-	-	-1.4	-6.0	7.0	12	-18.3	22	-4.3	-2.8	-3.8	-3.7	4.2	4.8	4.5	4.5	86	89	89	88	0.5	0.5	0.4	0.5	-	-	-	-
Rok	-	-	-	-	11.5	3.8	32.0	26.VII	-18.3	22.XII	5.8	10.2	7.2	7.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Przybroda $H_s = 88 m$ $h_w = 10 m$ 1962

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Max<-10°	Max<0°	Min<0°	Max>25°	v≥10	v>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	R̲
I	4	3.8	3	3.7	1	2.0	4	3.6	26	4.2	32	5.3	18	4.0	4	4.8	1	4.4	13	3.0	24	2	4	13	·	·	·	1	16	10	6	·	2	–	·
II	4.5	6.9	10.5	5.2	7	4.4	2.5	2.4	12	4.0	12.5	5.2	25	5.6	10	6.4		5.2	45	14.8	5	2	8	22	·	3	·	·	15	13	9	1	1	–	1
III	13.5	3.4	8.5	3.6	12	3.5	10.5	3.0	10	2.6	10	2.6	9.5	4.6	10	4.7	9	3.2	32	18.0	5	2	4	22	·	·	·	2	9	7	5	1	4	–	·
IV	7.5	3.4	12	4.1	5	2.8	6.5	2.6	14	3.7	13.5	4.9	14.5	3.8	13	3.3	4	3.6	26	6.2	28	·	·	·	3	·	·	3	8	10	9	·	·	·	1
V	5.5	2.5	2	2.8	1.5	3.0	6.5	2.4	8.5	3.4	20	2.6	24	3.8	12	4.6	13	2.9	87	15.1	14	·	·	2	·	·	·	·	10	16	13	3	·	·	4
VI	10.5	3.5	2	3.8	1.5	2.3	2.5	2.8	7	3.0	10.5	4.4	27.5	4.4	17.5	2.9	11	3.3	24	5.6	29	·	·	·	7	·	·	2	3	10	6	·	·	·	4
VII	6	2.1	5	2.5	2.5	1.6	1.5	1.3	6.5	2.5	27	3.3	19.5	3.4	5	3.1	20	2.3	24	3.6	2	·	·	·	6	·	·	1	6	10	9	·	·	·	2
VIII	4.5	3.1	1	2.5	1.5	2.3	1	2.5	11	3.0	28	4.4	26	4.0	7	3.1	13	3.3	40	8.9	24	·	·	·	7	·	·	1	10	12	8	·	·	·	3
IX	1.5	2.3	4.5	4.8	11.5	3.3	4	3.4	12	3.4	17.5	4.4	22.5	4.2	4.5	2.9	12	3.2	40	14.2	18	·	·	·	3	·	·	4	4	8	6	1	3	·	1
X	3.5	2.1	2	3.0	13	2.4	12	2.4	9.5	2.9	14.5	2.8	15.5	3.3	10	3.0	13	2.4	18	5.3	31	·	·	4	·	·	·	6	5	11	4		18	·	1
XI	1	3.0	10	5.2	25.5	4.5	3.5	2.7	8.5	2.8	14.5	3.6	11	2.8	5	2.8	11	3.4	27	10.3	1	·	·	8	·	·	·	2	20	11	5	1	10	–	·
XII	12.5	2.8	11	4.4	4.5	2.9	3.5	2.3	13.5	4.2	22.5	3.8	11	3.5	5.5	2.7	9	3.2	26	6.9	15	10	16	26	·	·	·	2	18	8	7	·	8	–	
Rok	74.5	3.2	71.5	3.6	86.5	2.9	58	2.6	138.5	3.3	222.5	3.9	224	4.0	103.5	3.7	116	3.4	402	18.0	5.III	16	32	103	26	3	·	24	124	126	87	7	46	–	17

Wieliszew $H_s = 78 m$ $h_w = 13 m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Max<-10°	Max<0°	Min<0°	Max>25°	v≥10	v>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	R̲
I	3	5.8	5.5	4.7	0.5	3.0	3	3.2	13.5	4.3	37	4.5	23	5.0	5.5	6.8	2	4.6	22	7.7	25	3	7	20	·	2	·	–	–	11	5	·	3	–	·
II	6	7.8	10	5.5	10	5.4	4.5	3.4	8.5	4.6	14	5.9	16.5	6.2	10.5	6.7	4	5.5	45	13.5	12	4	13	25	·	6	1	–	–	14	6	2	7	–	·
III	11	6.9	16.5	4.1	9	3.5	15	2.9	9	3.2	2.5	2.6	8.5	5.0	6.5	4.5	15	3.5	39	10.4	12	5	9	27	·	3		–	–	15	7	1	3	–	·
IV	10.5	4.3	9.5	4.5	7	4.9	9	4.6	9.5	4.4	11.5	4.7	4	3.9	8	4.6	21	3.5	28	7.5	5	·	·	1	4	1		–	–	9	4	·	·	·	1
V	5.5	2.7	4	2.6	1.5	3.7	7	2.7	8.5	3.2	17	4.0	16	3.5	8.5	3.1	25	2.5	158	50.4	14	·	·	3	·	·	·	–	–	18	13	5	·	·	4
VI	12.5	3.5	4.5	7.1	1	3.5	3	2.2	3	3.2	11.5	2.9	27	3.7	7.5	4.0	20	2.9	96	27.8	29	·	·	·	5	1	1	–	–	13	10	4	·	·	4
VII	10	3.0	3	2.8	1.5	3.0	1.5	3.0	5.5	3.0	13	3.5	21.5	3.5	12	2.7	25	2.2	58	26.0	12	·	·	·	5	·	·	–	–	10	8	2	·	·	5
VIII	1.5	2.0	0.5	2.0	1.5	3.3	4	2.6	8.5	3.5	24	4.0	19.5	3.8	5.5	3.7	28	2.6	80	12.3	16	·	·	·	7	·	·	–	–	16	13	2	1	·	5
IX	3	4.7			6	2.8	5.5	2.5	9	4.1	30	4.4	13	4.3	1.5	2.3	22	3.0	64	11.2	18	·	·	·	1	·	·	–	–	17	13	1	3	·	3
X	5.5	3.5	1.5	2.3	8.5	1.8	8	3.1	10	3.1	15	3.8	8	3.8	3.5	1.9	33	2.0	10	2.9	28	·	·	5	·	·	·	–	–	9	4	·	6	·	·
XI	2	4.0	4	6.4	13.5	4.0	16	4.5	10.5	3.9	11.5	4.0	6	3.2	2.5	3.2	24	3.1	29	8.2	15	·	·	8	·	2	1	–	–	8	7	·	2	1	·
XII	5.5	3.4	9	4.6	1.5	3.0	6	3.0	12.5	4.4	23.5	4.0	7	3.8	4	2.8	24	2.9	15	3.4	15	10	16	28	·		·	–	–	9	6	·	2	16	·
Rok	76	4.3	68	3.9	61.5	3.5	82.5	3.1	108	3.7	210.5	4.0	170	4.1	75.5	3.9	243	3.2	644	50.4	14.V	22	45	117	22	15	3	–	–	149	96	17	27	–	22

Sulęcin $H_s = 80 m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Max<-10°	Max<0°	Min<0°	Max>25°	v≥10	v>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	R̲
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	31	8.7	24	2	4	12	·	–	–	·	25	17	11		6	–	1
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	62	16.5	12	1	10	22	·	–	–		24	20	13	2	3	–	1
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	34	10.3	31	1	4	27	·	–	–	7	13	10	7	1	1	–	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	34	8.3	29	·	·	4	4	–	–	3	10	12	9	·	3	–	·
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	118	20.8	12	·	·	3	·	–	–		14	26	16	4	2		9
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	26	6.6	15,28	·	·	·	8	–	–	3	8	10	6	·	·	·	4
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	123	34.3	16	·	·	·	3	–	–	1	13	18	15	2	1	·	5
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	78	15.9	24	·	·	·	5	–	–	1	13	15	13	1	1	·	3
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	63	15.1	23	·	·	·	2	–	–	5	10	11	10	1	4		4
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	14	6.1	5	·	·	7	·	–	–	3	14	5	4	·	13	·	1
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	22	4.4	1,29	·	·	12	·	–	–	1	20	12	7	·	14	–	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	48	17.4	11	8	16	26	·	–	–	1	18	11	8	1	6	–	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	653	34.3	16.VII	12	34	113	22	–	–	25	182	167	119	12	54	–	28

Poznań-Sołacz $H_s = 71 m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Max<-10°	Max<0°	Min<0°	Max>25°	v≥10	v>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	R̲
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	24	5.0	12	2	4	15	·	–	–	–	–	16	9	·	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	44	12.5	16	2	9	22	·	–	–	–	–	17	8	2	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	33	14.2	5	1	3	27	·	–	–	–	–	11	7	1	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	29	7.5	29	·	·	1	4	–	–	–	–	16	9	·	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	99	23.0	14	·	·	1	·	–	–	–	–	23	17	2	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	32	6.6	16,23	·	·	·	7	–	–	–	–	8	8	·	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	23	4.4	6	·	·	·	5	–	–	–	–	13	9	·	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	48	10.0	24	·	·	·	5	–	–	–	–	15	12	1	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	52	15.1	18	·	·	·	2	–	–	–	–	14	11	1	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	21	7.3	4	·	·	3	·	–	–	–	–	10	5	·	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	31	12.3	1	·	·	8	·	–	–	–	–	13	6	1	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	29	9.5	15	8	14	25	·	–	–	–	–	13	7	·	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	465	23.0	14.V	13	30	102	23	–	–	–	–	169	108	8	–	–	–

Poznań-Ławica $\varphi = 52°25'$ $\lambda = 16°50'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0,m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1004.0	1029.5	977.0	1015.6	3.0	-1.7	9.3	22	-14.0	31	0.1	2.0	0.3	0.7	5.5	5.8	5.5	5.6	86	80	85	84	0.9	1.5	0.9	1.1	7.3	8.0	7.5	7.6
II	1004.8	1026.4	972.9	1016.4	1.6	-3.3	7.7	20	-12.5	1	-1.9	0.3	-0.9	-0.8	4.6	5.2	4.9	4.9	84	80	82	82	0.9	1.2	1.0	1.0	8.6	9.4	7.6	8.5
III	1000.4	1017.6	974.6	1012.0	3.4	-4.2	14.3	30	-11.4	7,8	-2.6	2.3	-0.7	-0.4	4.5	4.9	4.7	4.7	85	66	79	77	0.7	2.5	1.3	1.5	7.4	6.5	6.3	6.7
IV	1002.8	1016.6	976.0	1014.0	15.7	5.2	27.9	23	-0.2	10	7.1	14.0	9.5	10.0	8.9	8.9	9.5	9.1	86	55	77	73	1.6	8.5	3.1	4.4	6.6	7.3	6.5	6.8
V	1002.0	1007.8	992.4	1013.2	15.3	5.9	22.4	19	-3.0	1	8.6	13.5	9.9	10.5	10.1	9.3	10.4	9.9	89	60	84	78	1.3	6.6	2.0	3.3	7.6	8.3	7.4	7.8
VI	1007.8	1019.5	996.4	1018.9	20.7	9.1	32.7	16	2.1	3	13.1	18.8	14.4	15.2	11.1	10.4	12.1	11.2	71	48	71	63	4.5	12.4	5.0	7.3	4.8	6.5	5.5	5.6
VII	1003.8	1014.5	986.8	1014.8	21.5	10.3	33.0	26	4.7	29	14.1	19.8	15.4	16.2	13.3	11.7	13.6	12.9	82	53	77	71	3.0	12.4	4.3	6.6	6.7	7.6	5.6	6.6
VIII	1004.4	1013.4	990.5	1015.4	22.1	12.0	29.8	12	7.9	9	14.4	20.4	15.8	16.6	14.0	13.2	14.0	13.7	85	56	78	73	2.6	11.4	4.2	6.1	7.0	8.1	5.5	6.9
IX	1005.2	1018.8	986.4	1016.4	17.9	7.8	29.7	4	3.4	15	9.6	16.4	11.7	12.4	10.9	11.3	11.5	11.2	91	62	84	79	1.2	8.0	2.5	3.9	7.0	6.9	4.8	6.2
X	1011.3	1025.8	998.4	1022.7	12.9	4.3	23.1	3	-1.9	24	6.2	11.9	7.3	8.2	9.3	10.1	9.6	9.7	95	71	90	85	0.5	4.5	1.1	2.0	7.0	6.9	4.2	6.0
XI	1005.6	1023.6	988.3	1017.1	5.9	2.2	15.6	8	-2.6	21	3.0	5.1	3.9	4.0	7.1	7.5	7.3	7.3	92	84	89	88	0.6	1.6	0.9	1.0	8.2	8.1	8.2	8.2
XII	1005.4	1035.4	956.9	1017.3	-1.8	-6.5	6.5	12	-19.4	22	-4.5	-2.8	-4.2	-3.9	4.1	4.4	4.1	4.2	86	81	84	84	0.5	0.9	0.6	0.7	8.3	7.6	7.2	7.7
Rok	1004.8	1035.4	956.9	1016.1	11.5	3.4	33.0	26.VII	-19.4	22.XII	5.6	10.1	6.9	7.4	8.6	8.6	8.9	8.7	86	66	82	78	1.5	6.0	2.2	3.2	7.2	7.6	6.4	7.1

Nowy Dwór Mazowiecki $\varphi = 52°26'$ $\lambda = 20°43'$

I	-	-	-	-	2.2	-2.2	9.0	22	-17.4	31	-0.7	1.2	-0.3	0.0	-	-	-	-	-	-	-	-	-	-	-	-	8.5	7.9	7.5	8.0
II	-	-	-	-	0.5	-4.9	5.0	10	-14.9	1	-3.7	-1.0	-2.2	-2.3	-	-	-	-	-	-	-	-	-	-	-	-	9.2	7.9	7.8	8.3
III	-	-	-	-	2.1	-5.0	12.9	31	-12.7	15	-4.0	0.9	-1.4	-1.5	-	-	-	-	-	-	-	-	-	-	-	-	7.9	6.9	6.5	7.1
IV	-	-	-	-	16.2	6.6	28.5	23	0.5	3,8	8.0	14.3	10.5	10.8	-	-	-	-	-	-	-	-	-	-	-	-	5.8	5.3	4.9	5.3
V	-	-	-	-	15.6	7.6	21.9	8	-1.6	1	9.1	13.6	11.2	11.3	-	-	-	-	-	-	-	-	-	-	-	-	7.8	7.7	8.3	7.9
VI	-	-	-	-	19.7	11.0	29.9	16	6.5	7	13.2	17.9	15.1	15.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	-	-	-	21.9	12.1	30.5	26	8.1	4	14.4	20.2	16.1	16.7	-	-	-	-	-	-	-	-	-	-	-	-	5.9	6.6	7.8	6.8
VIII	-	-	-	-	22.5	12.9	34.3	7	8.5	10	14.9	20.9	16.1	17.0	-	-	-	-	-	-	-	-	-	-	-	-	7.3	6.8	6.7	6.9
IX	-	-	-	-	17.3	8.2	27.4	4	3.8	27	9.3	16.0	11.7	12.2	-	-	-	-	-	-	-	-	-	-	-	-	6.7	6.8	6.6	6.7
X	-	-	-	-	12.9	4.6	21.1	2	-3.0	16	5.7	11.9	7.7	8.2	-	-	-	-	-	-	-	-	-	-	-	-	8.3	5.4	6.0	6.6
XI	-	-	-	-	6.0	2.1	13.1	1	-2.1	18	3.3	5.3	4.0	4.2	-	-	-	-	-	-	-	-	-	-	-	-	9.1	8.6	7.9	8.5
XII	-	-	-	-	-2.3	-6.6	4.4	12	-19.2	21	-4.9	-3.6	-4.5	-4.4	-	-	-	-	-	-	-	-	-	-	-	-	7.5	7.7	6.5	7.2
Rok	-	-	-	-	11.2	3.9	31.3	7.VIII	-19.2	21.XII	5.4	9.8	7.0	7.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Siemiatycze $\varphi = 52°26'$ $\lambda = 22°52'$

I	-	-	-	-	0.6	-3.4	5.0	22	-20.4	31	-1.7	0.1	-1.4	-1.1	5.0	5.3	5.0	5.1	88	84	87	86	0.7	1.0	0.7	0.8	8.4	7.5	7.9	7.9
II	-	-	-	-	-1.3	-6.9	2.6	13	-16.7	1	-4.7	-2.1	-3.5	-3.4	3.9	4.7	4.3	4.3	84	87	88	86	0.7	0.7	0.6	0.7	8.7	8.3	8.6	8.5
III	-	-	-	-	0.5	-7.7	6.9	31	-19.1	26	-4.9	-0.4	-3.6	-3.1	-	-	-	-	-	-	-	-	-	-	-	-	7.0	6.4	5.8	6.4
IV	-	-	-	-	15.2	5.5	27.4	22	-0.7	8	8.2	14.2	9.4	10.3	9.4	9.9	10.0	9.8	85	63	83	77	2.0	7.8	2.4	4.1	6.7	5.6	4.3	5.5
V	-	-	-	-	15.5	7.1	22.6	28	-1.7	1	9.7	14.2	10.4	11.2	11.0	11.1	11.5	11.2	89	69	89	82	1.4	5.6	1.5	2.8	8.0	8.0	5.7	7.2
VI	-	-	-	-	19.7	9.0	29.6	23	3.3	6	13.5	18.0	13.7	14.7	12.2	11.5	12.6	12.1	78	57	79	71	3.9	10.2	3.7	5.9	5.3	6.5	4.9	5.6
VII	-	-	-	-	21.3	11.4	29.4	27	6.7	5	14.7	19.7	15.2	16.2	14.2	14.1	14.4	14.2	85	62	83	77	2.7	9.4	3.1	5.1	5.9	6.8	3.2	5.3
VIII	-	-	-	-	22.1	11.6	34.8	13	6.8	10	14.9	20.6	16.0	16.9	14.9	14.8	15.2	15.0	87	62	84	78	2.3	10.2	3.4	5.3	-	-	-	-
IX	-	-	-	-	17.2	8.2	26.8	5	2.9	25	10.0	16.0	11.5	12.2	11.5	12.4	12.3	12.1	93	69	90	84	1.0	6.4	1.5	3.0	5.6	6.3	4.0	5.3
X	-	-	-	-	12.2	3.6	19.6	2	-3.3	16	5.5	11.4	7.0	7.7	8.8	10.2	9.5	9.5	95	75	93	88	0.4	3.7	0.8	1.6	8.1	6.4	4.3	6.3
XI	-	-	-	-	6.3	2.0	18.1	1	-1.9	18	3.3	5.2	4.0	4.1	7.3	7.8	7.5	7.5	91	86	89	89	0.7	1.5	0.9	1.0	8.8	8.1	8.6	8.5
XII	-	-	-	-	-2.9	-7.6	3.5	10	-20.9	21	-5.7	-3.9	-5.4	-5.1	3.7	4.2	3.9	3.9	83	84	84	84	0.7	0.7	0.6	0.7	8.1	7.4	7.1	7.5
Rok	-	-	-	-	10.5	2.7	31.8	13.VIII	-20.9	21.XII	5.2	9.4	6.1	6.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Legionowo $\varphi = 52°24'$ $\lambda = 20°58'$

I	1002.7	1027.7	977.8	1015.8	2.2	-2.3	9.4	22	-19.0	31	-0.8	1.0	-0.5	-0.2	5.3	5.3	5.3	5.3	90	80	87	86	0.7	1.5	0.9	1.0	8.2	7.6	7.0	7.6
II	1002.2	1023.0	966.9	1015.4	0.1	-5.3	4.8	12	-16.5	1	-4.0	-1.2	-2.5	-2.6	4.2	4.6	4.6	4.5	89	80	88	86	0.6	1.1	0.7	0.8	8.0	8.7	7.3	8.0
III	999.0	1016.4	977.7	1012.2	1.6	-5.5	13.3	31	-13.8	15	-4.2	0.2	-1.7	-1.8	4.4	4.6	4.6	4.5	93	72	83	83	0.3	1.8	0.9	1.0	7.7	7.4	6.3	7.1
IV	1001.7	1016.9	977.0	1014.3	16.2	5.9	27.9	23	0.3	30	7.9	14.5	10.3	10.7	9.3	8.8	9.7	9.3	86	56	76	73	1.7	9.2	3.5	4.8	7.7	7.1	3.8	6.2
V	1000.3	1008.2	979.4	1012.8	15.5	6.9	21.4	8	-3.0	1	9.1	13.8	10.9	11.1	10.7	10.0	11.2	10.6	91	64	85	80	1.1	6.3	2.1	3.2	8.2	8.2	6.9	7.8
VI	1005.2	1016.1	994.2	1017.6	19.8	10.1	29.7	16	5.0	7	13.2	18.0	14.8	15.2	11.9	10.7	12.2	11.6	76	52	72	67	3.8	11.0	5.1	6.6	7.2	6.8	5.8	6.6
VII	1002.0	1012.9	988.7	1014.3	21.7	11.5	30.7	26	7.7	4	14.4	20.0	15.9	16.5	13.7	12.8	13.8	13.4	83	55	76	71	2.9	11.1	4.6	6.2	6.3	6.8	5.3	6.1
VIII	1002.9	1012.0	992.3	1015.2	22.1	12.3	30.8	7	7.3	10	14.7	20.4	16.2	16.9	14.5	13.8	15.2	14.5	86	59	82	76	2.4	11.0	3.5	5.6	7.2	7.0	4.8	6.3
IX	1003.7	1018.8	986.1	1016.2	17.0	8.2	27.0	4	3.2	25	9.7	15.7	12.1	12.4	11.2	11.8	12.4	11.8	92	67	88	82	1.0	6.6	2.2	3.3	6.7	7.1	5.9	6.6
X	1010.1	1024.6	996.5	1022.9	12.8	4.0	20.3	2	-3.5	16	5.4	11.5	7.7	8.1	8.8	10.1	9.9	9.6	96	74	92	87	0.4	3.8	0.9	1.7	7.3	6.5	4.7	6.2
XI	1005.6	1020.3	988.1	1018.6	6.1	1.9	14.4	1	-2.5	18	3.0	5.1	3.8	3.9	7.2	7.5	7.4	7.4	93	83	90	89	0.5	1.6	0.9	1.0	9.1	8.8	8.3	8.7
XII	1004.1	1033.3	962.3	1017.4	-2.4	-7.0	4.7	12	-20.8	21	-5.2	-3.9	-4.9	-4.7	4.0	4.1	4.0	4.0	88	83	86	86	0.5	0.8	0.6	0.6	8.0	8.1	7.2	7.8
Rok	1003.3	1033.3	962.3	1016.2	11.1	3.4	30.8	7.VIII	-20.8	21.XII	5.3	9.6	6.8	7.1	8.8	8.7	9.2	8.9	89	69	84	81	1.3	5.5	2.2	3.0	7.6	7.5	6.1	7.1

Poznań-Ławica $H_s = 86 m$ $H_b = 92,1 m$ $h_w = 13 m$ 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	[thunderstorm]	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	[fog]	R̃
I	3	7.7	4	6.8	3	2.7	1	3.0	21	5.4	36	5.9	18.5	7.0	5.5	8.0	1	6.0	23	5.5	12	2	4	18	·	9	2	2	16	16	7	·	3	9	·
II	5	8.8	6.5	7.8	13	6.8	1.5	2.7	9.5	4.5	15.5	5.3	20	7.9	12	9.3	1	6.9	46	14.5	16	2	9	24	·	14	1	·	18	18	9	2	1	7	·
III	9.5	6.5	10.5	5.3	10	4.8	16	4.5	12	3.5	9.5	3.4	8	5.6	11.5	5.8	6	4.6	27	10.1	5	3	4	28	·	6	·	2	13	11	6	1	2	12	·
IV	8	4.3	9	5.6	10	6.0	10	3.4	8.5	4.4	20.5	5.2	7.5	5.0	14.5	6.2	2	5.0	30	5.5	29	·	·	1	3	12	·	2	11	16	10	·	·	·	1
V	4.5	4.6	5.5	3.1	3.5	2.9	6	2.0	6	3.5	16	4.2	27	4.8	19.5	5.8	5	4.2	83	18.8	28	·	·	2	·	6	·	·	16	23	14	2	·	·	3
VI	17	6.2	1	1.0	2	1.5	3.5	2.7	6	3.4	11.5	4.3	25.5	6.9	19.5	4.3	4	5.0	34	7.9	26	·	·	·	7	9	·	3	6	10	7	·	1	·	4
VII	8.5	2.8	4.5	4.1	8	1.9	2	1.5	6.5	3.2	22	4.8	20.5	5.7	13	5.3	8	4.0	25	5.1	3	·	·	·	6	3	·	1	9	14	8	·	3	·	5
VIII	2	1.5	6	4.0	3	3.7	3	2.0	9.5	3.1	27	4.8	29.5	6.3	7	4.7	6	4.5	60	11.4	24	·	·	·	6	10	·	1	12	13	11	1	·	·	4
IX	3	3.0	1	3.0	7	3.8	13	2.8	4	3.1	23	4.1	21.5	6.1	9.5	5.1	8	4.0	66	20.9	18	·	·	·	3	8	2	3	9	17	10	1	7	·	3
X	5	3.0	3	3.3	5	2.0	16	2.6	9.5	3.1	15	3.1	17.5	4.1	12	4.4	10	3.0	22	6.6	4	·	·	5	·	2	·	3	7	10	5	·	10	·	1
XI	5	4.8	0.5	12.0	21.5	6.5	15	5.5	9	2.7	11.5	3.4	15	4.7	2.5	3.0	10	4.4	34	13.5	1	·	·	8	·	6	·	2	20	16	6	1	12	·	·
XII	6.5	3.5	6.5	4.7	16.5	5.4	4.5	1.8	9	4.4	20	4.5	16.5	4.5	7.5	3.7	8	4.0	31	8.3	15	9	15	25	·	3	·	2	19	13	7	·	8	17	·
Rok	77	4.7	58	5.1	102.5	4.0	91.5	2.9	108.5	3.7	227.5	4.4	227	5.7	134	5.5	69	4.6	481	20.9	18.IX	16	32	111	25	88	5	21	156	177	100	8	47	45	21

UWAGA. Kierunki i prędkości wiatru - wg anemometru.

Nowy Dwór Mazowiecki $H_s = 70 m$ $h_w = 13 m$

I	3.5	6.0	4.5	6.1	3.5	1.3	3.5	2.0	14.5	4.6	31.5	2.0	19	2.5	4	3.1	9	2.2	26	8.2	25	2	6	20	·	1	·	2	20	12	9	·	2	15	:
II	5	6.6	6	3.2	11	1.5	7	1.6	9	2.8	14	2.9	13	4.0	11	6.3	8	3.2	45	14.3	12	3	13	25	·	2	·		21	16	7	2	3	26	·
III	7.5	6.4	13	3.3	8.5	1.8	12.5	2.8	5	1.1	1.5	1.3	6	2.3	11	5.0	28	2.3	38	10.0	12	2	6	27	·	1	·	4	15	14	8	1	2	23	·
IV	10.5	3.0	8	2.2	8.5	2.5	6.5	2.2	10.5	2.3	10.5	1.7	7.5	2.9	7	4.2	21	2.0	28	9.5	13		·	·	5	·	·	6	9	11	5	·	1	·	1
V	1.5	2.0	7	1.5	6	1.6	3.5	1.9	6.5	1.7	10.5	1.6	16.5	2.6	13.5	3.6	28	1.6	18.5	78.5	14	·	·	1	·	1	·	1	20	28	17	4	2	·	2
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	67	21.8	29	·	·	·	5	–	–	–	–	14	12	2	·	·	4
VII	8	2.1	5	1.4	2.5	1.4	1	1.0	11	1.5	17.5	1.4	22	2.1	12	2.1	14	1.5	36	12.1	10	·		·	6	·	·	1	12	12	9	1	·	·	6
VIII	3.5	1.9	0.5	1.0	2	1.5	4.5	1.6	7	2.2	17.5	2.0	23	2.3	3	4.2	32	1.4	75	22.0	16	·	·	·	7	·	·	2	11	18	13	2	·	·	6
IX	3	2.3	2	2.0	3.5	4.0	1.5	1.0	7.5	1.7	15.5	1.7	19.5	2.3	5.5	2.4	32	1.3	64	13.3	18		·	·	1	·	·	4	15	16	12	1	4	·	4
X	2.5	1.4			3.5	1.0	6	1.2	4	1.4	8.5	1.8	9.5	2.7	7	2.3	52	0.8	8	4.8	28		·	3	·	·	·	1	15	3	2	·	16	·	·
XI	1.5	1.0	4	2.6	15.5	2.2	17	2.4	4.5	1.9	6	1.7	8.5	1.6	3	1.5	30	1.4	38	7.5	15	·		7	·	·	·	1	21	17	9	·	5	·	·
XII	1	1.0	15	2.1	10.5	1.6	7.5	1.4	10	2.0	15	1.9	13	1.5	8	1.8	13	1.5	14	4.0	15	10	17	27	·	·	·	5	20	13	5	·	7	16	·
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	624	78.5	14.V	17	42	110	24	–	–	–	–	174	108	13	42	80	23

Siemiatycze $H_s = 145 m$ $h_w = 16 m$

I	3	2.0	9	2.4			6	1.7	26.5	2.4	25.5	2.6	17	2.5	5	2.0	1	2.4	38	10.7	25	2	7	22	·	·		4	19	12	9	1	4	23	–
II	3	1.7	9.5	3.3	15	2.0	6.5	1.7	17	3.4	9.5	5.5	8.5	3.5	13	4.2	2	3.2	48	11.1	12	8	15	28	·	3	1	·	20	18	11	1	5	28	–
III	5.5	2.9	21.5	2.1	17.5	2.6	12	1.9	6	1.5	4.5	3.0	8.5	4.4	16.5	1.8	1	2.4	42	7.8	23	11	12	28	·	1	·	8	15	14	9	·	5	30	–
IV	8	2.1	11	2.7	10	2.4	11	1.7	14.5	2.1	5.5	1.9	10.5	2.1	17.5	2.0	2	2.1	60	9.5	26	·	·	2	3	1	·	5	6	12	11		2	·	–
V	3.5	1.9	4	1.2	4	1.0	7	1.6	7	1.6	18.5	1.6	26.5	2.3	20.5	2.0	2	1.9	154	30.1	14	·	·	2	·	·	·	2	13	23	16	6	1	·	–
VI	19	2.5	5.5	1.6	1	1.5	4	1.0	7	1.3	8.5	2.3	28.5	2.4	12.5	1.7	4	2.0	95	30.8	4	·	·	·	7	·	·	3	9	15	12	3	·	·	–
VII	11.5	1.2	1.5	1.0	0.5	1.0	2	1.0	9	1.1	21	1.5	22	2.4	14.5	1.9	11	1.5	70	13.8	23	·	·	·	5	·	·	3	1	12	11	3	1	·	–
VIII	0.5	2.0	4	1.5	0.5	2.0	5	2.2	11	2.1	19	2.6	28.5	2.6	8.5	2.3	16	2.0	74	16.8	15	·	·	·	7	·	·	–	–	15	12	3	1	·	–
IX	3	1.7	2.5	1.4	5	1.6	7.5	1.5	13	2.0	19.5	3.1	21	2.0	5.5	2.0	13	1.9	101	21.6	17.18	·	·	·	2	1	·	5	7	18	10	4	4	·	–
X	6.5	1.2	4.5	1.3	8.5	1.5	15	1.3	2.5	1.0	17.5	2.1	10.5	2.9	7	1.5	21	1.3	9	5.4	27	·	·	5	·	·	·	3	10	11	1	·	13	·	–
XI	9	1.6	7	3.0	22	4.7	21	2.9	8	1.8	1	1.0	10	2.6	10	2.0	2	2.9	57	12.2	15	·	·	9	·	1	·	1	22	16	12	1	7	2	–
XII	10.5	1.7	17	1.8	0.5	1.0	17.5	1.3	10	2.5	9	3.3	17.5	1.6	9	1.6	2	1.8	17	6.5	14	10	18	30	·	·	·	3	19	12	4	·	4	17	–
Rok	83	1.9	97	1.9	84.5	1.8	114.5	1.6	131.5	1.9	159	2.5	209	2.6	139.5	2.1	77	2.1	765	30.8	4.VI	31	52	126	24	7	1	–	–	178	118	22	47	100	–

Legionowo $H_s = 93 m$ $H_b = 103,7 m$ $h_w = 12 m$

I	1	8.0	6	6.4	2.5	2.8	1.5	1.7	14.5	4.1	39	5.4	21.5	5.5	5	4.8	2	5.0	17	6.8	25	2	7	20	·	5	·	2	17	10	4	·	2	15	·
II	2.5	7.8	9.5	5.8	11	4.0	5	3.4	9.5	4.4	20	5.6	15.5	7.8	8	7.1	3	5.6	24	6.6	12	4	14	25	·	7	·	·	16	13	7	·	5	16	·
III	6	7.4	16.5	4.0	11	2.7	20.5	3.0	4.5	4.1	4.5	3.3	9.5	5.5	6.5	5.8	14	3.5	40	9.7	12	4	10	27	·	5	·	3	16	13	7	·	5	20	·
IV	5	4.3	11.5	5.1	7.5	4.5	10	4.2	9.5	4.2	14.5	4.1	8.5	5.3	9.5	3.8	14	3.7	37	11.8	26	·	·	·	4	4	·	2	6	10	6	1	2	·	1
V	2	2.2	5.5	3.2	5.5	2.6	6	2.7	9	3.3	22.5	3.9	23.5	5.0	10	3.0	9	3.4	147	49.2	14	·	·	2	·	3	·	1	17	23	14	4	1	·	3
VI	3	3.0	7	3.6	2	3.5	4.5	2.6	9	2.4	17.5	3.6	24.5	4.6	14.5	5.6	8	3.6	82	23.2	29	·	·	·	5	4	·	1	9	13	12	3	·	·	3
VII	5	2.8	8.5	3.0	2	1.0	4	2.2	6	2.9	17	3.1	33	3.4	7.5	4.3	10	2.8	18	5.6	10	·	·	·	6	·	·	1	7	9	5	·	·	·	5
VIII	1	1.0	4.5	2.3	2	2.5	8.5	2.9	8.5	3.8	28	4.4	19.5	4.1	6	3.7	18	3.1	92	24.4	16	·	·	·	7	3	1	1	8	15	12	4	·	·	6
IX	2.5	3.2	3	2.5	11	2.8	6	2.7	12.5	3.5	26.5	4.3	14.5	4.5	7	3.4	7	3.4	55	13.0	18	·	·	·	1	·	·	3	12	16	10	1	4	·	2
X	3	2.0	3	2.7	15	1.7	14.5	2.5	7	2.6	13	3.3	17	3.8	3.5	3.4	17	2.3	6	2.5	28	·	·	3	·	1	·	1	10	5	2	·	13	·	·
XI	3	2.3	7.5	5.7	28.5	4.9	9.5	3.6	1	2.0	10	4.4	10	4.0	2.5	2.4	18	3.5	40	9.2	15		·	8	·	2	·	1	23	12	10	·	6	1	·
XII	2.5	3.4	18.5	4.8	4.5	3.0	6	2.8	12.5	4.8	13.5	4.6	12.5	3.8	3	3.0	20	3.3	8	2.5	15	10	17	27	·	·	·	2	19	10	3	·	5	16	·
Rok	36.5	4.0	98	4.1	102.5	3.0	96	2.9	103.5	3.5	226	4.2	209.5	4.8	83	4.2	140	3.6	566	49.2	14.V	20	48	112	23	34	1	18	160	149	92	13	43	68	20

Słubice $\varphi = 52°21'$ $\lambda = 14°36'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0,m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnie I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1012.3	1038.1	984.4	1015.1	4.6	-0.2	10.4	22	-12.8	31	1.4	3.4	2.0	2.2	6.1	6.0	6.0	6.0	87	76	83	82	1.0	2.0	1.3	1.4	7.2	8.2	7.8	7.7
II	1014.1	1036.1	982.9	1016.9	3.1	-2.3	9.3	8	-13.3	1	-0.3	1.7	0.1	0.4	5.2	5.6	5.2	5.3	86	79	82	82	0.9	1.5	1.2	1.2	8.6	8.0	6.6	7.7
III	1008.5	1026.4	980.7	1014.3	4.7	-3.4	15.9	30	-10.5	7	-2.0	3.6	0.2	0.5	4.9	4.8	5.0	4.9	88	59	78	75	0.6	3.4	1.4	1.8	6.5	6.4	5.3	6.1
IV	1010.6	1023.3	983.8	1013.3	15.6	4.7	27.8	22	-1.8	11	6.6	13.4	9.3	9.6	8.7	8.7	9.1	8.8	87	56	76	73	1.3	7.9	3.3	4.2	6.5	6.6	5.0	6.0
V	1010.2	1015.7	1003.2	1012.9	15.3	6.4	22.6	19	-2.5	1	9.0	13.5	10.3	10.8	10.2	9.8	10.2	10.1	87	63	81	77	1.5	6.1	2.6	3.4	6.9	8.6	6.4	7.3
VI	1016.3	1030.0	1005.4	1019.0	20.3	8.6	29.8	15	2.1	3	13.1	18.6	14.2	15.0	11.9	11.8	12.0	11.9	77	54	72	68	3.6	10.6	4.7	6.3	4.6	6.6	5.1	5.4
VII	1011.7	1022.5	992.4	1014.3	21.0	10.8	30.6	26	5.9	25	13.7	19.0	14.7	15.5	13.9	13.4	14.2	13.8	88	62	84	78	2.0	9.3	2.7	4.7	6.5	7.3	5.5	6.4
VIII	1012.3	1021.2	1000.2	1014.9	21.2	11.9	29.9	12	6.9	10	14.1	19.9	15.4	16.2	14.1	14.0	14.2	14.1	87	61	81	76	2.1	9.6	3.5	5.1	7.5	7.8	5.9	7.1
IX	1012.9	1025.4	993.4	1015.6	17.9	7.2	26.9	4	1.1	15	9.4	16.7	11.2	12.1	11.0	11.9	11.7	11.5	92	64	87	81	1.1	7.7	2.0	3.6	5.8	6.4	3.5	5.2
X	1019.2	1032.6	1005.1	1022.0	13.9	4.0	24.7	3	-2.7	28	6.5	12.6	7.5	8.5	9.4	10.8	9.6	9.9	95	73	91	86	0.5	4.4	1.1	2.0	7.9	6.9	4.1	6.3
XI	1013.0	1032.6	995.3	1015.8	6.5	1.3	16.7	8	-4.8	25	2.9	5.8	3.4	3.9	7.2	7.7	7.2	7.4	93	82	91	89	0.6	2.0	0.8	1.1	9.0	7.9	7.4	8.1
XII	1013.8	1044.1	968.1	1016.5	-0.9	-6.1	7.5	12	-17.0	22	-4.0	-2.0	-3.7	-3.4	4.4	4.7	4.4	4.5	88	84	87	86	0.6	0.8	0.6	0.7	7.1	7.4	6.1	6.9
Rok	1012.9	1044.1	968.1	1015.6	11.9	3.6	30.6	26.VII	-17.0	22.XII	5.9	10.5	7.0	7.6	8.9	9.1	9.1	9.0	88	68	83	80	1.3	5.4	2.1	2.9	7.0	7.3	5.7	6.7

Paproć $\varphi = 52°19'$ $\lambda = 16°08'$

I	-	-	-	-	3.7	-1.1	10.4	22	-12.6	31	0.7	2.4	0.8	1.2	5.9	6.1	5.8	5.9	89	81	87	86	0.8	1.4	0.9	1.0	6.9	6.8	7.3	7.0
II	-	-	-	-	2.5	-3.0	8.9	12	-12.6	1	-1.6	1.1	-0.7	-0.5	4.7	5.3	4.9	5.0	84	78	81	81	0.9	1.5	1.1	1.2	8.2	8.1	7.0	7.8
III	-	-	-	-	4.2	-3.5	15.1	30	-9.6	7	-2.2	3.0	-0.3	0.0	4.6	4.7	4.7	4.7	84	61	77	74	0.8	3.1	1.4	1.8	6.0	5.5	5.0	5.5
IV	-	-	-	-	15.9	5.0	28.2	23	-1.0	10	7.0	14.0	9.4	10.0	8.9	9.0	9.6	9.2	87	57	78	74	1.4	8.4	2.9	4.2	5.0	5.2	5.3	5.2
V	-	-	-	-	15.3	5.9	22.6	19	-2.4	1	8.7	13.7	10.0	10.6	10.3	9.7	10.4	10.1	90	62	84	79	1.2	6.5	2.0	3.2	6.3	7.0	6.2	6.5
VI	-	-	-	-	20.5	8.6	31.1	16	1.3	3	13.2	18.4	14.2	15.0	12.0	11.6	12.5	12.0	77	54	74	68	3.7	10.7	4.3	6.2	3.7	5.4	4.3	4.5
VII	-	-	-	-	21.0	9.9	31.0	26	3.4	29	14.0	19.1	14.7	15.6	14.1	13.3	14.2	13.9	88	62	85	78	2.1	9.8	2.7	4.9	5.4	6.2	5.0	5.5
VIII	-	-	-	-	21.3	11.5	28.7	12	5.4	10	14.3	19.7	15.1	16.0	14.5	14.7	14.4	14.5	88	64	83	78	2.0	8.8	3.0	4.6	6.4	6.9	6.0	6.4
IX	-	-	-	-	17.8	6.9	28.3	4	-0.1	15	9.2	16.3	11.0	11.9	10.9	12.4	11.4	11.6	92	67	87	82	1.0	6.8	2.1	3.3	6.2	5.6	4.4	5.4
X	-	-	-	-	13.3	3.5	22.6	3	-3.8	16,21	5.9	12.1	6.9	8.0	9.1	10.4	9.5	9.7	95	72	92	86	0.5	4.3	0.9	1.9	7.0	5.9	4.8	5.9
XI	-	-	-	-	6.3	2.0	16.5	8	-2.7	21	3.0	5.4	3.7	4.0	7.2	7.6	7.3	7.4	94	84	90	89	0.5	1.7	0.8	1.0	8.0	7.6	7.7	7.8
XII	-	-	-	-	-1.2	-5.9	7.3	12	-17.3	22	-4.2	-2.5	-3.9	-3.6	4.3	4.3	4.3	4.3	88	79	87	85	0.5	1.1	0.6	0.7	8.1	6.8	6.3	7.1
Rok	-	-	-	-	11.7	3.3	31.1	16.VI	-17.3	22.XII	5.7	10.2	6.7	7.3	8.9	9.1	9.1	9.0	88	68	84	80	1.3	5.3	1.9	2.8	6.4	6.4	5.8	6.2

Ostrowy $\varphi = 52°18'$ $\lambda = 19°10'$

I	-	-	-	-	2.2	-2.3	8.4	22	-14.4	31	-0.7	0.9	-0.3	-0.1	-	-	-	-	-	-	-	-	-	-	-	-	7.6	7.2	6.5	7.1
II	-	-	-	-	0.6	-4.7	4.2	20	-13.3	1	-3.1	-1.0	-1.8	-1.9	-	-	-	-	-	-	-	-	-	-	-	-	8.6	8.4	8.1	8.4
III	-	-	-	-	2.4	-4.0	12.4	31	-9.9	15	-3.2	0.7	-1.1	-1.2	-	-	-	-	-	-	-	-	-	-	-	-	7.3	6.8	7.2	7.1
IV	-	-	-	-	15.5	5.6	27.3	23	0.7	30	7.2	13.6	9.2	9.8	-	-	-	-	-	-	-	-	-	-	-	-	6.7	6.1	7.1	6.6
V	-	-	-	-	15.4	6.3	20.7	8	-2.3	1	8.6	12.9	9.9	10.3	-	-	-	-	-	-	-	-	-	-	-	-	7.4	7.5	7.9	7.6
VI	-	-	-	-	20.0	9.2	29.1	16	3.0	3	12.7	17.8	13.4	14.3	-	-	-	-	-	-	-	-	-	-	-	-	5.5	5.6	6.2	5.8
VII	-	-	-	-	21.1	10.2	30.1	26	5.5	31	13.7	19.1	14.0	15.2	-	-	-	-	-	-	-	-	-	-	-	-	5.9	5.6	6.3	5.9
VIII	-	-	-	-	21.7	11.5	30.3	7	5.4	10	14.3	20.0	14.6	15.9	-	-	-	-	-	-	-	-	-	-	-	-	6.6	6.7	6.6	6.6
IX	-	-	-	-	17.1	7.4	28.3	4	0.8	25	9.1	15.6	11.0	11.7	-	-	-	-	-	-	-	-	-	-	-	-	6.7	6.8	5.8	6.4
X	-	-	-	-	12.7	3.6	20.4	2	-3.0	16	5.5	11.8	6.8	7.7	-	-	-	-	-	-	-	-	-	-	-	-	7.1	6.1	6.3	6.5
XI	-	-	-	-	5.5	1.6	13.1	4	-5.5	26	2.6	4.4	3.3	3.4	-	-	-	-	-	-	-	-	-	-	-	-	8.5	7.8	8.1	8.1
XII	-	-	-	-	-2.6	-7.5	4.3	12	-20.4	22	-5.3	-4.1	-5.1	-4.9	-	-	-	-	-	-	-	-	-	-	-	-	8.5	7.8	7.5	7.9
Rok	-	-	-	-	11.0	3.1	30.3	7.VIII	-20.4	22.XII	5.1	9.3	6.2	6.7	-	-	-	-	-	-	-	-	-	-	-	-	7.2	6.9	7.0	7.0

Słupca $\varphi = 52°17'$ $\lambda = 17°52'$

I	-	-	-	-	2.4	-1.9	8.6	22	-13.3	31	-0.4	1.5	0.0	0.3	-	-	-	-	-	-	-	-	-	-	-	-	7.9	8.5	7.7	8.0
II	-	-	-	-	0.9	-3.9	6.3	20	-12.4	1	-2.5	-0.1	-1.6	-1.4	-	-	-	-	-	-	-	-	-	-	-	-	8.7	9.2	6.3	8.1
III	-	-	-	-	2.6	-3.5	12.4	31	-10.4	8	-2.5	1.6	-0.8	-0.6	-	-	-	-	-	-	-	-	-	-	-	-	6.5	7.1	7.4	7.0
IV	-	-	-	-	15.3	5.9	28.1	23	0.7	2	7.9	13.8	9.5	10.2	-	-	-	-	-	-	-	-	-	-	-	-	6.8	7.3	5.4	6.5
V	-	-	-	-	15.0	6.8	20.1	19	-1.2	1	9.2	13.8	10.0	10.8	-	-	-	-	-	-	-	-	-	-	-	-	7.7	8.4	7.6	7.9
VI	-	-	-	-	20.2	9.6	31.1	16	2.4	3	13.7	18.9	13.8	15.0	-	-	-	-	-	-	-	-	-	-	-	-	6.2	7.0	5.2	6.1
VII	-	-	-	-	21.2	10.4	31.8	26	5.8	29	14.9	19.8	14.8	16.1	-	-	-	-	-	-	-	-	-	-	-	-	6.6	7.6	6.0	6.7
VIII	-	-	-	-	21.8	11.9	30.4	13	7.1	10	15.2	20.4	15.3	16.6	-	-	-	-	-	-	-	-	-	-	-	-	6.8	8.6	5.9	7.1
IX	-	-	-	-	17.5	7.5	29.5	4	1.7	15	9.9	16.3	11.2	12.2	-	-	-	-	-	-	-	-	-	-	-	-	6.4	7.0	5.8	6.4
X	-	-	-	-	13.0	4.0	21.8	3	-2.7	24	6.0	12.2	6.8	8.0	-	-	-	-	-	-	-	-	-	-	-	-	6.9	7.3	4.3	6.2
XI	-	-	-	-	5.5	2.1	14.0	5	-2.1	21	3.0	5.0	3.4	3.7	-	-	-	-	-	-	-	-	-	-	-	-	8.7	8.4	8.7	8.6
XII	-	-	-	-	-2.2	-7.0	6.0	12	-18.9	22	-5.0	-3.2	-4.7	-4.4	-	-	-	-	-	-	-	-	-	-	-	-	8.7	7.6	7.1	7.8
Rok	-	-	-	-	11.1	3.5	31.8	26.VII	-18.9	22.XII	5.8	10.0	6.5	7.2	-	-	-	-	-	-	-	-	-	-	-	-	7.3	7.8	6.4	7.2

Słubice $H_s = 20\,m$ $H_b = 22{,}2\,m$ $h_w = 15\,m$ 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R
I	5	5.5	3	4.7	·	·	·	·	8.5	3.2	46	4.7	22.5	5.9	5	3.5	3	4.7	30	10.0	24	1	4	10	·	6	·	1	17	16	10	1	2	·	
II	8.5	5.8	11	3.5	7	4.6	·	·	3	2.5	23.5	4.0	20	6.6	9	6.9	2	5.0	47	14.4	12	2	5	19	·	8	3	·	15	20	9	2	2	6	1
III	10	3.2	9.5	2.9	2	4.0	7	3.4	9.5	3.5	13	3.8	9.5	3.9	10.5	4.4	22	2.8	34	9.1	12	2	2	27	·	2	·	4	12	12	8	·	1	10	·
IV	8.5	3.6	7	4.0	6.5	4.2	5.5	2.7	7	3.0	22.5	3.9	13.5	4.8	10.5	3.7	9	3.5	22	5.6	16	·	·	1	4	5	·	5	10	11	10	·	1	·	·
V	6	3.6	2	3.8	·	·	0.5	3.0	10.5	2.4	25.5	2.7	24	4.2	9.5	3.8	15	2.8	56	15.4	26	·	·	2	·	·	·	·	11	23	11	1	·	·	3
VI	10.5	4.8	4.5	4.1	1	3.0	1.5	1.7	5.5	3.1	12	2.7	23	5.7	14	3.6	18	3.4	26	9.2	26	·	·	·	8	5	·	3	2	12	5	·	·	·	4
VII	4.5	1.6	3.5	1.4	2	1.5	·	·	7	1.7	21.5	3.5	21.5	3.3	13	3.4	20	2.4	53	12.8	12	·	·	·	4	1	·	1	9	13	10	1	2	·	4
VIII	4	2.8	2	3.0	1	2.0	1.5	3.3	11	2.9	20.5	3.8	37.5	4.3	25	4.4	13	3.3	41	7.7	24	·	·	·	5	3	·	1	13	16	11	·	·	·	3
IX	·	·	·	·	5	3.2	4	4.0	8.5	1.6	26.5	2.9	28	3.7	4	3.9	14	2.7	47	9.7	18	·	·	·	3	3	·	5	5	11	9	·	4	·	4
X	4	3.0	2	2.5	6	1.8	1.5	2.7	10.5	1.9	26.5	2.2	14	2.6	4.5	3.1	24	1.7	10	3.9	4	·	·	6	·	·	·	3	9	8	3	·	13	·	1
XI	4	1.0	6	4.1	19	4.1	5.5	2.1	4.5	1.8	20.5	2.5	12.5	2.3	3	4.3	15	2.4	17	3.5	22	·	·	12	·	2	·	·	18	14	7	·	9	4	·
XII	4.5	2.6	12	2.8	7	3.4	2	4.0	6.5	2.3	32.5	3.0	12.5	4.0	1	6.0	15	2.6	35	11.3	11	8	13	26	·	2	·	4	16	12	8	1	8	13	·
Rok	69.5	3.1	62.5	3.1	56.5	2.6	29	2.2	92	2.5	290.5	3.3	238.5	4.3	86.5	4.2	170	3.1	418	15.4	26.V	13	24	103	24	37	3	27	137	168	101	6	42	33	20

Paproć $H_s = 75\,m$ $h_w = 11\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R
I	2	4.2	4	2.9	2	2.0	8.5	2.4	49.5	2.2	22.5	3.4	23.5	3.2	8	3.4	3	2.8	34	7.1	24	2	4	13	·	·	·	2	11	18	10	·	2	9	·
II	4	3.8	10	4.0	10	3.0	1.5	2.7	7	4.7	16	4.4	16	4.3	13.5	4.6	6	3.6	54	13.4	16	2	7	24	·	3	2	·	13	21	12	2	2	11	·
III	8.5	3.6	15.5	2.8	10.5	3.3	9	2.4	9	1.9	4	1.2	9	2.3	14.5	2.5	13	2.3	29	8.1	12	·	3	27	·	·	·	4	8	10	7	·	2	9	·
IV	1	1.0	12.5	2.7	7.5	2.8	7	2.1	11	2.5	18	2.6	6	2.1	20	2.4	7	2.3	46	12.2	29	·	·	3	5	·	·	6	7	13	7	1	·	1	1
V	3.5	2.3	4	1.5	3	1.8	6	1.9	8	2.7	22.5	2.1	22	2.2	19	2.7	5	2.1	95	13.2	12	·	·	3	·	·	·	·	7	26	17	3	·	·	4
VI	10	3.2	6.5	1.8	3.5	1.9	3.5	1.9	1	2.0	14.5	2.0	21.5	2.9	19.5	2.2	10	2.1	80	57.5	16	·	·	·	8	·	·	5	4	10	5	2	·	·	3
VII	7.5	1.8	8	1.6	2.5	1.2	4	1.2	1	4.0	21	2.3	23	1.8	10	1.7	16	1.6	27	5.2	2	·	·	·	3	·	·	2	3	15	10	·	2	·	4
VIII	2.5	1.2	1.5	2.0	2	2.0	2	1.0	6	1.8	31.5	2.6	28.5	2.2	5	1.8	14	1.9	74	20.1	13	·	·	·	5	·	·	1	8	16	11	3	1	·	2
IX	2	1.2	1.5	2.0	14.5	2.7	3.5	2.4	5.5	1.4	16	2.4	32	2.2	6	2.2	9	2.0	46	13.1	18	·	·	1	3	·	·	5	3	11	7	2	8	·	1
X	6	2.0	2.5	2.2	13	1.5	8	1.2	8	1.1	7.5	2.2	10.5	2.0	10.5	2.3	27	1.3	18	5.4	5	·	·	8	·	·	·	3	8	11	5	·	20	·	1
XI	2	2.0	5	2.6	29.5	2.9	2.5	2.2	6	1.2	16	1.8	10	2.1	6	2.5	13	2.0	27	13.8	1	·	·	8	·	·	·	1	17	14	5	1	10	1	·
XII	8	2.2	18	2.9	5	2.6	2	1.0	11.5	2.3	23	2.5	7.5	2.7	2	2.5	16	2.1	34	11.4	15	6	15	25	·	·	·	2	13	10	7	1	12	17	·
Rok	57	2.4	89	2.4	103	2.3	57.5	1.9	93.5	2.1	212.5	2.5	209.5	2.5	134	2.6	139	2.2	564	57.5	16.VI	10	29	112	24	3	2	31	102	175	103	15	59	48	16

Ostrowy $H_s = 120\,m$ $h_w = 11\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R
I	5	7.3	7	6.6	0.5	2.0		·	15.5	5.0	34	5.6	24	5.4	9	4.5	1	5.5	15	4.6	25	2	7	19	·	3	·	–	–	9	6	·	1	–	·
II	9	7.2	6.5	5.0	10	3.9	0.5	6.0	9.5	3.6	14.5	6.0	22.5	7.4	9.5	7.9	2	6.0	26	8.2	12	2	11	23	·	7	1	–	–	16	7	·		–	·
III	16	4.6	8	3.4	16	3.5	10	3.8	7.5	3.7	7.5	3.5	8.5	3.8	16.5	4.2	3	3.8	45	16.0	12	·	4	26		1	·	–	–	12	7	2	4	–	·
IV	5	4.4	5	4.2	12	3.8	4	4.8	17	3.2	16.5	3.9	8	4.4	15.5	4.1	7	3.6	27	6.0	13	·	·	·	3	1	·	–	–	14	9	·	·	·	·
V	10	3.0	2	2.7	4.5	2.8	6.5	2.6	3	2.8	14.5	4.1	28	3.6	13.5	3.9	11	3.1	164	72.3	14	·	·	4	·	2	·	–	–	22	18	2	1	·	5
VI	16	4.2	3.5	5.6	2	2.7	0.5	4.0	2.5	2.8	4.5	3.8	35	4.6	16	2.9	10	3.6	58	18.0	29	·	·	·	7	·	·	–	–	13	10	2	·	·	4
VII	8	2.3	5.5	2.8	0.5	3.0	2	2.0	6.5	3.1	12	3.6	23	3.8	19.5	2.8	16	2.6	71	16.9	14	·	·	·	5	·	·	–	–	13	11	1	1	·	4
VIII	2	3.2	2	4.0	0.5	3.0	1	3.0	5.5	4.1	22.5	3.9	37	4.2	13.5	4.3	9	3.7	53	16.4	17	·	·	·	5	2	·	–	–	13	10	1	·	·	2
IX	3	3.8	·	·	13	2.8	4	3.1	5	3.8	11	4.1	39.5	4.1	10.5	3.9	4	3.6	62	19.7	18	·	·	·	2	·	·	–	–	11	8	2	–	·	3
X	9.5	2.2	8	2.2	17.5	2.7	8	2.6	3	3.3	18	3.6	13	4.0	10	3.5	6	2.9	22	9.3	6	·		6	·	·	·	–	–	9	6	·	14	·	1
XI	5.5	1.5	·	·	32.5	3.8	5.5	5.3	9	3.8	10.5	3.7	20.5	3.2	3.5	4.0	3	3.4	42	11.0	20	·	·	9	·	·		–	–	13	10	1	–	–	·
XII	18	3.7	14	3.8	6	3.2	5	2.2	6.5	2.5	1.5	4.3	25	3.8	16	5.1	1	3.8	10	3.7	16	12	17	28	·	·		–	–	8	3	·	–	–	·
Rok	107	4.0	61.5	3.4	115	3.1	47	3.3	90.5	3.5	164	4.2	284	4.4	153	4.0	73	3.8	595	72.3	14.V	46	39	115	22	16	1	–	–	153	105	11	–	–	19

Słupca $H_s = 90\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	24	6.4	25	2	4	19	·	–	–	1	19	12	8	·	2	–	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	42	15.8	12	2	11	24	·	–	–	·	13	14	8	1	1	–	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	34	9.3	5	1	6	27	·	–	–	3	14	12	6	·	·	–	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	39	14.2	29	·	·	·	3	–	–	2	8	13	8	1	·	·	1
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	97	29.6	14	·	·	1	·	–	–	·	16	24	18	1	·	·	3
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	21	4.5	1	·	·	·	7	–	–	3	8	9	5	·	·	·	2
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	28	5.1	13	·	·	·	4	–	–	1	9	12	8	·	·	·	3
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	55	17.2	13	·	·	·	6	–	–	1	10	13	11	2	·	·	3
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	63	19.6	18	·	·	·	3	–	–	3	7	12	11	2	4	·	2
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	26	13.8	31	·	·	5	·	–	–	5	8	9	5	1	9	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	47	9.6	18	·	1	10	·	–	–	1	21	18	12	·	3	·	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	21	7.5	16	12	16	28	·	–	–	2	18	10	6	·	6	–	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	497	29.6	14.V	17	38	114	23	–	–	22	151	158	106	8	25	–	14

Warszawa - Bielany $\varphi = 52°17'$ $\lambda = 20°58'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0,m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1003,0	1027,7	978,6	1016,2	2,1	-1,9	8,9	22	-18,0	31	-0,5	0,9	-0,2	0,0	5,2	5,2	5,2	5,2	85	76	83	81	1,0	1,6	1,1	1,2	8,3	7,9	7,3	7,8
II	1002,4	1021,9	967,9	1015,7	0,0	-4,6	5,4	12	-15,2	1	-3,5	-1,3	-2,0	-2,2	4,1	4,5	4,5	4,4	84	78	83	82	0,8	1,2	0,9	1,0	8,3	8,8	7,3	8,1
III	999,0	1017,1	977,8	1012,3	1,7	-4,4	12,7	31	-9,5	15	-3,5	0,2	-1,1	-1,4	4,3	4,4	4,5	4,4	87	68	76	77	0,6	2,0	1,3	1,3	7,7	7,5	6,3	7,2
IV	1004,6	1016,9	976,7	1014,2	16,1	7,0	27,8	23	0,2	30	8,4	14,4	10,8	11,1	8,8	8,7	9,4	9,0	80	55	72	69	2,7	9,3	4,4	5,5	7,7	7,4	4,9	6,7
V	1000,5	1008,6	980,2	1013,1	15,3	7,6	20,9	8	-2,0	1	9,2	13,8	11,2	11,4	10,4	10,0	11,1	10,5	88	64	82	78	1,5	6,2	2,6	3,4	8,0	7,9	7,2	7,7
VI	1005,4	1015,8	994,7	1017,9	19,8	11,2	29,5	16,23	5,2	7	13,4	18,0	15,1	15,4	11,7	10,5	12,0	11,4	75	52	69	65	4,2	11,2	5,9	7,1	6,9	6,9	5,6	6,5
VII	1002,2	1012,9	988,6	1014,6	21,4	12,4	30,3	26	8,7	4	14,4	19,7	16,3	16,7	13,4	12,9	13,4	13,2	81	56	72	70	3,2	10,6	5,5	6,4	5,8	6,8	5,1	5,9
VIII	1003,2	1012,2	993,5	1015,5	22,0	13,5	30,7	7	9,4	29	15,2	20,2	16,6	17,2	14,1	14,1	15,1	14,4	81	61	80	74	3,3	10,3	4,1	5,9	7,1	7,4	5,4	6,6
IX	1003,9	1019,0	986,7	1016,5	17,1	9,0	27,6	4	3,7	27	10,1	15,8	12,4	12,7	11,1	11,6	12,2	11,6	89	65	84	79	1,6	6,9	2,6	3,7	6,9	7,4	5,5	6,6
X	1010,2	1024,8	996,3	1023,1	12,5	5,3	20,1	2	-1,4	16	6,0	11,4	8,3	8,5	8,9	9,9	9,8	9,5	94	73	87	85	0,6	3,9	1,3	1,9	6,7	6,8	5,0	6,2
XI	1005,6	1020,2	988,4	1018,7	6,2	2,2	14,5	1	-1,5	18	3,3	5,1	4,1	4,2	7,2	7,3	7,2	7,2	90	81	86	86	0,8	1,8	1,3	1,3	9,2	8,9	8,5	8,9
XII	1004,2	1033,1	962,3	1017,6	-2,3	-6,6	4,4	12	-19,9	21	-5,1	-3,9	-4,6	-4,6	4,0	4,1	4,0	4,0	87	83	85	85	0,6	0,8	0,7	0,7	8,4	8,6	8,2	8,4
Rok	1003,4	1033,1	962,3	1016,2	11,0	4,2	30,7	7.VIII	-19,9	21.XII	5,6	9,5	7,2	7,4	8,6	8,6	9,0	8,7	85	68	80	78	1,7	5,5	2,6	3,3	7,6	7,7	6,4	7,2

Warszawa, Inst. Geogr. UW $\varphi = 52°14'$ $\lambda = 21°01'$

I	-	-	-	-	2,3	-1,5	9,1	22	-17,6	31	-0,1	1,2	0,2	0,4	5,3	5,4	5,4	5,4	84	78	84	82	1,1	1,6	1,1	1,3	8,2	8,0	7,8	8,0
II	-	-	-	-	0,2	-4,1	5,3	12	-13,6	1	-3,0	-0,8	-1,6	-1,8	4,2	4,5	4,5	4,4	82	76	81	80	0,9	1,4	1,0	1,1	8,0	9,0	7,5	8,2
III	-	-	-	-	1,8	-4,1	13,1	31	-9,1	21	-3,0	0,6	-0,7	-1,0	4,3	4,4	4,6	4,4	83	67	76	75	0,8	2,2	1,3	1,4	7,5	7,6	6,7	7,3
IV	-	-	-	-	16,0	7,3	27,8	23	0,6	30	8,5	14,7	11,5	11,6	9,2	9,2	10,0	9,5	81	57	73	70	2,4	9,0	4,2	5,2	7,7	7,8	5,0	6,8
V	-	-	-	-	15,5	8,2	21,4	8	-1,0	1	9,5	14,2	11,8	11,8	10,6	10,5	11,4	10,8	88	65	82	78	1,6	6,1	2,8	3,5	8,5	8,1	7,3	8,0
VI	-	-	-	-	19,6	11,9	30,4	23	5,4	7	13,8	18,2	15,7	15,8	11,8	11,7	12,6	12,0	74	56	70	67	4,6	10,3	5,9	6,9	7,0	7,2	5,7	6,6
VII	-	-	-	-	21,4	13,1	29,8	26	8,9	4	14,6	20,0	17,1	17,2	13,8	13,7	14,0	13,8	82	58	71	70	3,1	10,2	5,9	6,4	5,9	7,8	6,2	6,6
VIII	-	-	-	-	21,9	14,1	30,3	13	9,6	27	15,2	20,4	17,4	17,6	14,3	14,6	15,4	14,8	82	62	77	74	3,1	9,9	4,7	5,9	7,7	8,4	4,9	7,0
IX	-	-	-	-	17,0	9,6	26,4	4	4,5	27	10,4	15,8	13,0	13,0	11,4	12,8	12,8	12,3	90	71	85	82	1,4	5,3	2,6	3,1	6,7	7,6	6,3	6,9
X	-	-	-	-	12,1	5,9	18,8	2	0,8	16,26	6,7	11,3	9,1	9,0	9,1	10,3	10,0	9,8	92	76	85	84	0,8	3,4	1,7	2,0	7,8	7,0	5,5	6,8
XI	-	-	-	-	6,4	2,6	14,8	1	-1,0	18	3,7	5,3	4,4	4,4	7,3	7,5	7,4	7,4	89	82	87	86	0,9	1,7	1,2	1,3	9,3	8,9	8,4	8,9
XII	-	-	-	-	-1,9	-6,1	4,9	12	-18,6	21,22	-4,5	-3,4	-4,1	-4,0	4,1	4,1	4,1	4,1	85	80	82	82	0,7	1,0	0,8	0,8	7,0	8,4	8,3	7,9
Rok	-	-	-	-	11,0	4,7	30,4	23.VI	-18,6	21,22.XII	6,0	9,8	7,8	7,8	8,8	9,1	9,4	9,1	84	69	79	77	1,8	5,2	2,8	3,2	7,6	8,0	6,6	7,4

Warszawa, Obserw. Astr. UW $\varphi = 52°13'$ $\lambda = 21°02'$

I	1001,1	1025,9	976,6	1015,6	2,3	-2,1	9,4	22	-18,2	31	-0,6	1,1	-0,3	0,0	5,6	5,5	5,6	5,6	91	81	89	87	0,5	1,4	0,7	0,9	8,3	7,2	7,5	7,7
II	1000,6	1021,2	965,9	1015,2	0,3	-4,8	4,0	7,12	-14,2	1	-3,5	-0,9	-2,0	-2,1	4,5	4,8	4,8	4,7	90	83	90	88	0,4	1,0	0,6	0,7	8,7	7,8	7,6	8,0
III	997,1	1014,8	976,1	1011,6	2,1	-4,7	13,3	31	-10,2	21	-3,7	0,7	-1,3	-1,4	4,5	4,9	5,1	4,8	91	75	89	85	0,4	1,7	0,6	0,9	7,5	6,7	6,1	6,8
IV	999,9	1014,9	974,9	1013,8	16,5	6,8	28,2	23	0,5	30	8,3	15,0	11,8	11,2	9,4	9,7	10,1	9,7	85	58	76	73	2,0	9,0	3,6	4,9	6,6	6,9	4,9	6,1
V	998,6	1006,5	978,3	1012,5	15,9	7,6	22,3	8	-1,3	1	9,2	14,4	11,2	11,5	10,7	11,0	11,4	11,0	90	67	85	81	1,1	5,9	2,2	3,1	8,3	8,5	6,5	7,8
VI	1003,6	1014,0	992,8	1017,3	20,0	10,9	29,7	16,23	5,4	7	13,2	18,4	14,8	15,3	12,4	12,6	12,7	12,6	79	60	74	71	3,3	9,8	4,8	6,0	6,7	6,3	4,8	5,9
VII	1000,4	1011,2	987,0	1014,1	21,8	12,5	30,5	26	8,6	4	14,3	20,3	16,2	16,8	14,4	15,4	14,6	14,8	88	65	79	77	2,0	9,0	4,1	5,0	5,4	6,7	5,6	5,9
VIII	1001,5	1011,5	991,8	1015,1	22,3	13,2	31,4	13	8,0	27	15,0	20,5	16,5	17,1	14,8	16,2	16,1	15,7	86	67	85	79	2,4	8,8	2,9	4,7	5,8	6,5	4,5	5,6
IX	1002,2	1017,1	984,6	1016,1	17,4	8,7	27,2	4	3,9	27	10,0	16,1	12,2	12,6	11,5	13,7	13,0	12,7	92	76	90	86	1,0	5,1	1,5	2,5	6,2	7,2	5,1	6,2
X	1008,4	1022,9	994,7	1022,6	12,8	5,1	20,4	2	-1,0	16	5,8	11,8	8,2	8,5	9,0	11,3	10,1	10,1	96	80	91	89	0,4	2,9	0,9	1,4	7,9	6,2	4,8	6,3
XI	1004,1	1017,7	986,9	1018,4	6,4	2,3	15,0	1	-1,6	18	3,4	5,3	4,1	4,2	7,4	8,0	7,6	7,7	93	88	91	91	0,6	1,2	0,8	0,9	9,3	8,8	8,2	8,8
XII	1002,3	1031,3	960,2	1016,9	-1,9	-6,4	4,5	12	-19,5	21	-5,0	-3,3	-4,3	-4,2	4,2	4,5	4,4	4,4	90	86	91	89	0,4	0,7	0,4	0,5	8,5	8,1	8,6	8,4
Rok	1001,6	1031,3	960,2	1015,7	11,3	4,1	31,4	13.VIII	-19,5	21.XII	5,5	10,0	7,2	7,5	9,0	9,8	9,6	9,5	89	74	86	83	1,2	4,7	1,9	2,6	7,4	7,2	6,2	6,9

Warszawa, St. Pomp Rzeczn. $\varphi = 52°13'$ $\lambda = 21°03'$

I	-	-	-	-	2,3	-2,4	9,4	22	-17,8	31	-0,4	1,0	-0,3	0,0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	0,4	-4,9	5,3	12	-13,9	1	-3,4	-0,8	-2,2	-2,2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	1,8	-4,9	13,3	31	-11,5	15	-3,7	0,5	-1,4	-1,5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	16,1	6,3	27,9	23	0,1	30	8,3	14,6	10,5	11,0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	15,5	6,7	21,3	8	-2,1	6,1	9,4	14,4	10,8	11,4	-	-	-	-	-	-	-	-	-	-	-	-	8,2	7,7	7,2	7,7
VI	-	-	-	-	19,4	10,8	29,8	23	6,4	5,6	13,4	18,3	14,8	15,3	-	-	-	-	-	-	-	-	-	-	-	-	6,1	5,6	5,0	5,6
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	-	-	-	22,0	13,0	30,6	7,13	7,3	27	15,2	20,4	16,7	17,2	-	-	-	-	-	-	-	-	-	-	-	-	6,1	6,6	4,9	5,9
IX	-	-	-	-	17,1	8,4	26,9	4	4,3	26,27	10,3	15,6	12,0	12,5	-	-	-	-	-	-	-	-	-	-	-	-	6,0	6,6	5,8	6,1
X	-	-	-	-	12,6	4,4	19,9	2	-2,0	16	5,8	11,7	8,1	8,4	-	-	-	-	-	-	-	-	-	-	-	-	7,0	5,8	5,9	6,2
XI	-	-	-	-	6,6	2,2	15,0	1	-1,6	18	3,4	5,2	4,0	4,2	-	-	-	-	-	-	-	-	-	-	-	-	9,1	8,7	8,8	8,9
XII	-	-	-	-	-2,0	-6,5	4,6	12	-19,3	21	-4,8	-3,4	-4,4	-4,2	-	-	-	-	-	-	-	-	-	-	-	-	8,2	8,1	8,6	8,3
Rok	-	-	-	-	-	-	-	-	-19,3	21.XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Warszawa-Bielany $H_s = 98 m$ $H_b = 104,7 m$ $h_w = 16 m$ 1962

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◐	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	2	6.0	5.5	4.5	2	2.5	5	5.6	14	3.8	33	3.9	26	4.2	3.5	5.1	2	3.9	22	6.7	25	2	7	18	·	1	·	2	19	12	6	·	1	15	·
II	4.5	5.1	7	5.4	10	4.6	6.5	4.5	5	2.9	13.5	4.0	19	5.6	13.5	6.3	5	4.7	30	7.3	12	2	14	25	·	5	1	·	16	14	9	·	3	20	1
III	11.5	4.2	11.5	3.1	6	3.8	18.5	4.2	8	2.8	3.5	2.1	6.5	3.6	13.5	4.8	14	3.3	46	9.2	5	·	9	27	·	1	1	4	18	15	8	·	·	18	·
IV	14	3.6	9	3.9	4.5	5.1	12	4.7	12	3.8	9.5	3.1	8.5	4.1	9.5	3.9	11	3.5	46	12.2	26	·	·	·	4	2	·	·	9	12	6	2	·	1	1
V	4.5	2.6	3	2.2	2	2.0	5.5	3.5	5	3.2	16.5	2.9	25	3.9	13.5	2.9	18	2.6	199	68.5	14	·	·	2	·	·	·	1	16	26	18	4	·	·	5
VI	9.5	3.8	6	3.1	2.5	3.8	3.5	2.7	2.5	2.6	9.5	4.1	26	4.2	19.5	2.8	11	3.1	81	25.8	4	·	·	·	7	·	·	1	9	12	11	2	·	·	4
VII	9.5	2.2	2.5	2.6	1.5	2.3	1.5	2.0	6	2.2	15	3.4	32	3.2	7	2.7	18	2.4	45	15.2	10	·	·	·	5	·	·	2	5	9	7	1	1	·	6
VIII	0.5	2.0	2	1.5	0.5	4.0	6.5	3.6	7.5	2.9	18.5	2.9	27	3.6	13.5	2.5	17	2.5	76	13.6	5	·	·	·	6	·	·	2	11	17	13	3	·	·	8
IX	2	3.5	2.5	3.0	9	2.7	5	2.5	9	2.4	19.5	3.0	28.5	3.2	7.5	3.0	7	2.7	59	14.0	18	·	·	·	1	1	1	1	11	14	10	2	3	·	2
X	3	3.2	4	2.0	2	1.5	15.5	2.6	6	2.3	9.5	2.7	20	3.2	9	2.5	24	2.0	9	3.4	27	·	·	2	·	·	·	4	10	9	2	·	11	·	·
XI	3.5	4.6	4	5.4	24	4.6	13	4.1	7	2.7	6	3.9	15	3.5	5.5	4.8	12	3.3	51	40.0	19	·	·	7	·	·	·	1	25	13	10	1	6	1	·
XII	6	2.8	17	3.5	2	1.8	8.5	2.4	9	2.8	15.5	3.4	17.5	3.1	8.5	2.4	9	2.7	13	3.7	13	10	17	26	·	·	·	1	22	12	4	·	3	16	·
Rok	70.5	3.4	74	3.4	66	3.2	101	3.5	91	2.9	169.5	3.3	251	3.8	124	3.4	148	3.1	677	68.5	14.V	14	47	107	23	10	3	19	171	165	104	15	28	71	27

Warszawa, Inst. Geogr. UW $H_s = 108 m$ $h_w = 20 m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◐	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	1	4.0	6	3.0	8.5	3.8	8.5	3.8	30	4.1	26.5	4.2	7.5	2.9	4	3.2	1	3.8	47	6.2	25	2	5	18	·	–	–	2	22	11	3	·	5	15	·
II	6.5	2.7	6	3.4	12	3.3	10.5	2.8	13.5	4.0	11.5	3.7	14	4.6	9	5.0	1	3.7	39	8.0	24	1	13	23	·	–	–	1	17	14	11	·	2	21	1
III	9	2.8	16	2.0	16.5	2.8	17	2.9	6.5	2.9	6.5	3.6	9	4.0	8.5	2.9	4	2.8	38	9.6	12	·	8	27	·	–	–	4	17	12	8	·	4	22	·
IV	10.5	2.3	8	2.5	11.5	3.5	16.5	3.4	12	3.1	11	3.0	5.5	3.0	9	3.6	6	2.9	40	8.7	26	·	·	·	4	–	–	2	10	8	6	·	·	·	1
V	4.5	1.4	8.5	1.5	6	2.2	10	2.6	20.5	2.9	13.5	2.4	14.5	4.2	7.5	2.2	8	2.4	155	46.6	14	·	·	1	·	–	–	1	17	26	18	4	1	·	3
VI	11.5	3.1	8.5	2.5	2	3.5	7	3.3	13.5	2.7	18	2.8	18	3.2	8.5	2.5	3	2.9	79	25.1	4	·	·	·	5	–	–	2	13	12	10	3	·	·	2
VII	9	2.3	6	2.0	7.5	1.7	7.5	2.7	21	2.7	12.5	3.3	11.5	3.6	16	3.7	2	2.8	36	10.1	15	·	·	·	5	–	–	1	11	13	8	1	·	·	4
VIII	2	2.5	4.5	1.2	2	2.8	11.5	4.0	28	2.9	28.5	3.5	8.5	3.2	4	3.0	4	3.0	106	33.9	4	·	·	·	6	–	–	·	11	16	13	3	·	·	6
IX	2	2.2	4	1.6	12.5	2.3	10.5	2.6	21.5	3.0	16.5	2.9	14.5	3.3	6.5	3.7	2	2.8	56	17.0	17	·	·	·	1	–	–	2	13	12	9	2	3	·	1
X	2.5	2.6	5.5	1.9	13	2.0	18	2.1	15	2.6	14.5	2.9	3.5	3.3	9	1.9	12	2.0	5	3.8	27	·	·	·	·	–	–	1	12	6	1	·	–	·	·
XI	11	1.8	9.5	3.6	23.5	3.4	18.5	3.1	7.5	3.0	9	2.9	5.5	3.4	25	2.2	3	2.9	39	–	–	·	·	4	·	–	–	2	26	13	9	·	5	·	·
XII	6.5	1.7	15.5	2.3	10.5	2.4	14.5	2.7	13	3.2	15	3.2	13.5	3.0	25	2.2	2	2.6	12	3.9	15	9	15	27	·	–	–	2	19	9	3	·	3	16	·
Rok	76	2.4	98	2.3	125.5	2.8	150	3.0	202	3.1	183	3.2	125.5	3.5	87	3.0	48	2.9	622	46.6	14.V	12	41	100	21	–	–	20	188	152	99	13	–	74	18

Warszawa, Obserw. Astr. UW $H_s = 110 m$ $H_b = 114,8 m$ $h_w = 25 m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◐	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	2	1.0	4	1.0	1	1.0	3	1.0	19	1.3	14	1.0	24	2.0	7	1.6	19	1.2	28	12.4	25	2	5	18	·	·	·	2	19	17	7	1	·	16	–
II	6	1.0	4	1.0	4	1.0	8	1.0	21	2.0	13	1.6	11	2.6	8	2.0	9	1.5	46	10.7	12	2	12	26	·	·	·	·	14	15	10	2	·	28	–
III	22	1.0	4	1.0	7	1.0	15	1.0	21	1.1	2	1.0	10	1.4	4	1.5	8	1.0	54	11.3	31	1	7	26		·	·	6	16	13	9	1	2	24	–
IV	18	1.2	6	1.7	6	1.3	5	1.8	22	1.3	7	1.6	8	1.2	7	1.3	11	1.2	47	14.2	26	·	·	·	4	·	·	4	7	12	6	2	1	1	–
V	9	1.0	3	1.0	1	1.0	1	1.0	13	1.3	13	1.6	24	1.8	14	1.7	15	1.3	194	57.7	14	·	·	1	·	·	·	2	16	26	22	5	·	·	–
VI	20	2.2	6	2.0	2	2.0	2	1.0	6	1.3	13	2.1	24	2.8	12	1.8	5	2.1	87	29.3	29	·	·	·	6	·	·	7	11	13	11	2	·	·	–
VII	12	1.0	4	1.0	5	1.0	2	1.0	9	1.4	18	1.3	24	2.0	19	1.4	·	1.4	43	14.0	15	·	·	·	5	·	·	5	10	14	9	1	·		–
VIII	1	1.0	2	1.0	·	·	1	1.0	15	1.7	12	2.2	34	2.1	8	2.3	20	1.5	118	28.0	16	·	·	·	7	·	·	6	9	15	13	4	·		–
IX	5	1.8	·	·	5	1.0	6	1.0	15	1.4	13	2.2	26	2.5	3	2.3	17	1.6	80	23.2	17	·	·	·	1	·	·	5	10	17	11	3	2	·	–
X	7	1.0	7	1.0	5	1.0	13	1.0	13	1.0	5	1.0	18	1.9	9	1.7	16	1.1	9	4.2	27	·	·	1	·	·	·	3	12	5	2	·	8	·	–
XI	12	1.2	4	1.0	8	1.8	29	1.8	15	1.3	4	1.0	11	1.4	7	1.0	·	1.4	49	13.4	20	·	·	7	·	·	·	2	23	11	9	2	3	·	–
XII	5	1.0	6	1.0	5	1.0	6	1.0	16	1.0	7	1.6	18	1.2	3	1.1	27	0.8	15	3.9	16	9	15	27	·	·	·	·	21	9	5	·	2	16	–
Rok	119	1.2	50	1.1	49	1.1	91	1.1	185	1.3	121	1.5	232	1.9	101	1.6	147	1.3	770	57.7	14.V	14	39	106	23	·	·	42	168	167	114	23	18	85	–

Warszawa, St. Pomp Rzeczn. $H_s = 85 m$ $h_w = 14 m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◐	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	3.5	4.6	4.5	3.1	2.5	1.8	5.5	2.8	12	2.8	29	3.5	30	4.8	6	3.2	·	3.8	20	6.7	25	2	5	19	·	·	·	–	–	12	5	·	3	13	–
II	8.5	4.5	5.5	3.4	12.5	4.0	9	2.2	6.5	2.0	12	4.9	18.5	6.3	9.5	5.6	2	4.4	39	11.3	12	4	13	25	·	5	·	–	–	15	8	1	7	20	–
III	16	3.9	10.5	2.6	14	2.4	19	2.9	5	4.0	4.5	1.2	9.5	4.0	9.5	3.2	5	3.0	45	9.7	31	2	9	27	·	1	·	–	–	12	8	·	10	18	–
IV	19	2.7	6.5	3.2	6	3.5	8.5	4.5	14	2.1	10.5	2.5	9.5	2.7	9	3.1	7	2.7	45	12.5	26	·	·	·	4	1	·	–	–	10	6	2	8	·	–
V	13.5	2.3	5	1.6	6	2.1	3.5	1.9	7	1.8	10.5	2.1	30	3.1	13.5	2.1	4	2.3	173	53.6	14	·	·	2	·	·	·	·	16	26	20	4	5	·	–
VI	19.5	2.7	3.5	2.4	2.5	1.6	1.5	1.3	1.5	1.3	14	2.4	28	3.4	9.5	2.8	10	2.5	53	25.0	4	·	·	·	5	·	·	4	8	11	9	2	1	·	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	18.5	4.5	8	·	·	·	–	–	–	–	–	9	6	·	–	·	–
VIII	3.5	1.6	3	1.0	2.5	3.0	6.5	3.7	5.5	2.9	15	2.4	33.5	4.2	11.5	2.4	12	2.8	104	25.4	16	·	·	·	7	·	·	3	5	14	12	4	2	·	–
IX	5	2.0	5	1.8	7	2.4	7	1.3	5.5	1.4	18	1.9	30.5	3.4	8	2.5	4	2.4	72	20.2	17	·	·	·	1	·	·	3	10	13	11	3	6	·	–
X	9.5	1.6	3	1.3	10	1.1	9.5	1.7	4	1.1	11	2.0	16.5	3.3	7.5	1.6	22	1.5	5	3.6	27	·	·	1	·	·	·	·	10	3	1	·	11	·	–
XI	10.5	1.3	1	1.0	28	3.5	17.5	3.8	4	1.5	2	2.5	15	2.9	6	1.9	6	2.7	43	8.5	15	·	·	6	·	1	·	·	24	13	9	·	18	1	–
XII	12.5	2.3	11.5	2.5	9	2.4	10	1.5	6.5	1.6	13	2.2	21	2.5	5.5	2.1	4	2.1	14	4.7	15	11	15	27	·	·	·	1	21	10	3	·	15	16	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	631.5	53.6	14.V	19	42	107	–	–	–	–	–	148	98	16	–	–	–

Warszawa-Okęcie $\varphi = 52°09'$ $\lambda = 20°59'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T											ŚREDNIA PREŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0,m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Diss	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1002.6	1026.8	978.2	1016.0	1.9	-2.4	9.1	22	-18.1	31	-0.8	0.8	-0.4	-0.2	5.2	5.3	5.3	5.3	87	80	85	84	0.8	1.4	0.9	1.0	8.2	7.9	7.7	7.9
II	1002.0	1022.0	968.0	1015.5	-0.1	-5.0	4.9	12	-13.9	1	-3.8	-4.2	-2.5	-2.5	4.2	4.5	4.6	4.4	86	79	87	84	0.6	1.2	0.6	0.8	8.4	8.5	7.9	8.3
III	998.4	1015.7	977.6	1011.9	1.5	-4.9	13.0	31	-11.5	15	-3.9	0.5	-1.6	-1.6	4.3	4.7	4.6	4.5	89	71	82	81	0.5	1.8	0.9	1.1	7.8	7.2	6.8	7.3
IV	1001.1	1015.9	976.4	1014.0	16.0	5.9	27.5	22,23	-0.4	1	7.7	14.6	9.9	10.5	9.3	9.6	10.0	9.6	86	59	80	75	1.6	8.6	2.8	4.3	7.4	7.0	6.0	6.8
V	999.9	1007.8	979.9	1012.8	15.3	7.1	21.7	8	-2.7	1	9.1	13.8	10.6	11.0	10.8	10.9	11.5	11.1	92	69	89	83	1.0	5.4	1.6	2.7	8.0	8.1	7.2	7.8
VI	1004.8	1014.8	994.2	1017.5	19.4	9.9	29.3	23	5.3	8	13.2	17.7	14.1	14.8	12.3	11.4	12.7	12.1	78	57	77	71	3.4	9.8	3.9	5.7	6.4	6.5	5.4	6.1
VII	1001.5	1012.4	988.3	1014.2	21.3	11.4	29.9	26	7.4	31	14.3	19.9	15.3	16.2	14.0	13.7	14.1	13.9	85	59	80	75	2.5	10.1	3.6	5.4	5.8	6.6	5.5	6.0
VIII	1002.6	1011.5	993.0	1015.3	21.8	12.0	30.2	7,13	7.2	27	14.7	20.2	15.5	16.5	14.6	14.9	15.4	15.0	87	64	86	79	2.3	9.4	2.6	4.8	6.6	7.0	5.3	6.3
IX	1003.4	1018.1	986.2	1016.2	17.0	7.9	27.2	4	3.7	15	9.7	15.8	11.6	12.2	11.2	12.1	12.3	11.9	92	68	89	83	1.1	6.5	1.6	3.1	6.6	7.0	5.0	6.2
X	1009.6	1023.9	996.2	1022.7	12.4	4.2	19.7	2	-2.8	16	5.5	11.5	7.5	8.0	8.8	10.1	9.6	9.5	96	74	91	87	0.4	3.8	0.9	1.7	7.2	6.3	5.0	6.2
XI	1004.9	1019.3	987.9	1018.1	6.0	1.9	14.9	1	-1.7	18,24,26	3.2	5.2	3.9	4.0	7.2	7.4	7.2	7.3	92	82	88	87	0.6	1.7	1.0	1.1	8.9	8.8	8.6	8.8
XII	1003.6	1032.2	961.9	1017.2	-2.4	-6.9	4.2	12	-19.6	21	-5.2	-3.8	-4.5	-4.5	4.0	4.2	4.1	4.1	90	84	87	87	0.5	0.8	0.6	0.6	8.2	8.1	8.1	8.1
Rok	1002.9	1032.2	961.9	1016.0	10.8	3.4	30.2	7,13.VIII	-19.6	21.XII	5.3	9.6	6.6	7.0	8.8	9.3	9.3	9.1	88	70	85	81	1.3	5.0	1.8	2.7	7.5	7.4	6.5	7.1

Jeziory $\varphi = 52°16'$ $\lambda = 16°48'$

I	-	-	-	-	3.1	-1.8	9.4	22	-14.2	31	0.3	2.0	0.4	0.8	5.6	5.9	5.6	5.7	87	81	86	85	0.9	1.4	0.9	1.1	7.9	7.9	7.5	7.8
II	-	-	-	-	1.8	-3.2	8.0	20	-13.3	1	-2.0	0.7	-0.9	-0.8	4.8	5.5	5.1	5.1	87	84	88	86	0.7	1.1	0.7	0.8	9.0	8.8	6.5	8.1
III	-	-	-	-	3.9	-4.0	13.8	30	-9.7	7	-2.7	2.8	-0.8	-0.4	4.7	5.2	5.0	5.0	90	68	84	81	0.5	2.5	1.0	1.3	6.9	6.3	5.0	6.1
IV	-	-	-	-	15.9	5.3	27.8	23	-1.0	11	7.5	14.2	9.2	10.0	9.0	8.9	9.5	9.1	85	55	79	73	1.8	8.8	3.0	4.5	5.6	6.4	4.9	5.6
V	-	-	-	-	15.3	5.8	22.0	19	-3.0	1	9.1	13.6	9.5	10.4	10.3	10.0	10.6	10.3	87	64	88	80	1.5	6.2	1.5	3.1	7.0	8.3	6.4	7.2
VI	-	-	-	-	20.7	9.0	31.3	16	1.2	3	13.6	19.1	13.4	14.9	12.0	11.5	12.8	12.1	75	52	80	69	4.1	11.6	3.1	6.3	3.8	4.8	3.6	4.1
VII	-	-	-	-	21.1	10.2	32.3	26	5.2	29	14.1	19.6	14.0	15.4	14.4	13.9	14.6	14.3	89	63	90	81	1.9	9.7	1.6	4.4	5.4	6.1	5.1	5.5
VIII	-	-	-	-	21.6	12.1	29.3	12,13	7.3	10	14.5	20.1	15.1	16.2	15.0	15.6	14.9	15.2	90	67	87	81	1.7	8.5	2.5	4.2	7.0	6.5	4.0	5.8
IX	-	-	-	-	17.8	7.7	29.0	4	1.9	15	9.9	16.5	11.2	12.2	11.1	12.3	11.7	11.7	91	66	88	82	1.3	7.1	2.0	3.5	6.1	6.1	3.8	5.3
X	-	-	-	-	13.1	4.5	23.0	3	-2.9	21	6.3	12.3	7.3	8.3	9.3	10.9	9.7	10.0	94	75	92	87	0.6	4.0	0.9	1.8	6.4	6.3	3.9	5.5
XI	-	-	-	-	-	2.1	-	-	-2.6	21	3.1	5.3	3.9	4.0	7.2	8.0	7.5	7.6	93	88	91	91	0.5	1.3	0.8	0.9	8.0	8.0	7.4	7.8
XII	-	-	-	-	-1.2	-6.1	6.6	12	-18.6	22	-4.5	-2.8	-4.1	-3.9	4.2	4.5	4.3	4.3	87	84	88	86	0.5	0.8	0.5	0.6	7.8	6.7	6.7	7.1
Rok	-	-	-	-	-	3.5	32.3	26.VII	-18.6	22.XII	5.8	10.3	6.5	7.3	9.0	9.4	9.3	9.2	88	71	87	82	1.3	5.2	1.5	2.7	6.7	6.8	5.4	6.3

Świebodzin $\varphi = 52°15'$ $\lambda = 15°32'$

I	-	-	-	-	4.2	-0.9	10.8	21	-12.0	31	0.8	2.7	1.1	1.4	5.9	6.1	5.9	6.0	88	81	87	85	0.9	1.5	0.9	1.1	7.4	8.0	8.0	7.8
II	-	-	-	-	2.4	-2.7	8.6	12	-12.7	1	-1.2	1.1	-0.5	-0.3	5.1	5.7	5.4	5.4	88	84	89	87	0.7	1.1	0.6	0.8	8.7	8.5	6.6	7.9
III	-	-	-	-	4.2	-3.3	15.8	30	-8.5	8	-2.1	3.3	-0.2	0.2	-	-	-	-	-	-	-	-	-	-	-	-	6.0	6.6	4.6	5.7
IV	-	-	-	-	15.6	5.2	28.1	25	0.3	1,30	6.8	14.0	9.2	9.8	8.9	9.2	9.6	9.2	88	58	81	74	1.3	8.2	2.6	4.0	6.4	6.8	4.7	6.0
V	-	-	-	-	15.3	6.3	22.6	19	-0.7	1	8.9	13.5	9.8	10.5	10.3	10.0	10.6	10.3	89	65	86	80	1.3	6.0	1.7	3.0	7.3	8.1	5.4	6.9
VI	-	-	-	-	20.9	9.2	31.6	16	2.8	3	13.3	19.1	14.2	15.2	11.8	12.0	12.6	12.1	75	53	75	68	4.0	11.3	4.2	6.5	4.5	6.4	4.8	5.2
VII	-	-	-	-	21.5	10.8	31.2	26	6.5	4	14.6	19.7	14.8	16.0	14.2	14.2	14.6	14.3	85	63	86	78	2.7	9.6	2.5	4.9	5.8	6.2	6.1	6.0
VIII	-	-	-	-	21.7	12.0	30.3	12	7.9	10,27	14.5	20.2	15.3	16.3	14.4	14.7	14.9	14.7	87	74	86	82	2.3	9.6	2.6	4.8	7.1	7.3	4.7	6.4
IX	-	-	-	-	18.2	7.5	29.0	4	2.6	15	9.4	16.8	11.3	12.2	11.1	12.5	12.0	11.9	93	66	89	83	0.9	7.2	1.6	3.2	6.8	6.2	3.9	5.6
X	-	-	-	-	13.8	4.6	23.7	2	-0.7	21,23,24	6.5	12.5	7.3	8.4	9.4	11.4	9.9	10.2	97	77	94	89	0.4	3.7	0.7	1.6	7.9	6.6	5.6	6.7
XI	-	-	-	-	6.2	1.8	16.5	8	-2.4	21	2.9	5.5	3.2	3.7	7.2	8.1	7.5	7.6	95	88	95	9.3	0.4	1.2	0.4	0.7	7.7	8.2	7.2	7.7
XII	-	-	-	-	-1.2	-5.9	7.0	12	-16.9	22	-4.2	-2.8	-3.8	-3.6	4.2	4.5	4.2	4.3	85	82	83	83	0.6	0.8	0.7	0.7	8.1	7.4	6.7	7.4
Rok	-	-	-	-	11.9	3.7	31.6	16.VI	-16.9	22.XII	5.8	10.5	6.8	7.5	-	-	-	-	-	-	-	-	-	-	-	-	7.0	7.2	5.7	6.6

Zbąszyń $\varphi = 52°15'$ $\lambda = 15°56'$

I	-	-	-	-	3.7	-0.8	10.1	22	-13.2	31	0.9	2.7	1.1	1.4	-	-	-	-	-	-	-	-	-	-	-	-	8.2	8.0	8.8	8.3
II	-	-	-	-	2.2	-2.7	7.7	20	-12.6	1	-1.3	1.1	-0.5	-0.3	-	-	-	-	-	-	-	-	-	-	-	-	8.5	9.3	8.1	8.6
III	-	-	-	-	4.2	-3.3	15.6	30	-10.5	8	-2.2	3.2	-0.1	0.2	-	-	-	-	-	-	-	-	-	-	-	-	6.9	7.4	7.2	7.2
IV	-	-	-	-	15.8	5.2	28.6	25	0.0	11	6.9	14.2	9.6	10.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	15.4	6.5	22.6	19	-1.1	1	8.8	13.6	10.2	10.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	-	-	-	20.9	9.1	32.0	16	2.6	8	13.7	19.3	14.6	15.6	-	-	-	-	-	-	-	-	-	-	-	-	5.2	6.5	6.4	6.0
VII	-	-	-	-	21.5	10.5	32.3	26	5.6	25	14.2	19.6	15.2	16.0	-	-	-	-	-	-	-	-	-	-	-	-	6.2	7.4	7.4	7.0
VIII	-	-	-	-	21.6	12.2	30.3	12	7.5	10	14.6	20.0	16.0	16.6	-	-	-	-	-	-	-	-	-	-	-	-	7.5	8.0	8.3	7.9
IX	-	-	-	-	18.1	7.7	28.9	4	1.5	15	9.7	16.6	11.7	12.4	-	-	-	-	-	-	-	-	-	-	-	-	6.7	7.2	5.6	6.5
X	-	-	-	-	13.5	4.1	23.7	2	-2.3	16	6.1	12.4	7.6	8.4	-	-	-	-	-	-	-	-	-	-	-	-	7.1	6.7	5.7	6.5
XI	-	-	-	-	6.2	2.2	16.7	8	-2.5	21	3.2	5.7	3.9	4.2	-	-	-	-	-	-	-	-	-	-	-	-	8.6	8.2	8.3	8.4
XII	-	-	-	-	-1.1	-5.8	7.4	12	-16.8	22	-4.1	-2.1	-3.6	-3.4	-	-	-	-	-	-	-	-	-	-	-	-	8.3	7.1	7.1	7.5
Rok	-	-	-	-	11.8	3.7	32.3	26.VII	-16.8	22.XII	5.9	10.5	7.1	7.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Warszawa-Okęcie $H_s = 106\,m$ $H_b = 106{,}9\,m$ $h_w = 8{,}8\,m$ I–X, $10{,}4\,m$ XI–XII 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◐	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K
I	3.5	8.3	5	5.0	2	4.0	4	4.1	18.5	3.8	29.5	5.2	27	6.2	3.5	6.4	·	5.3	21	7.4	25	2	6	20	·	3	·	2	21	11	5	·	3	15	·
II	5	7.4	5.5	5.6	12	5.0	6	4.6	9.5	4.1	10	5.6	20.5	7.3	12.5	8.0	3	5.9	34	7.9	12	3	14	25	·	9	·	1	19	18	9		2	19	1
III	10	5.6	11	5.0	18	3.2	20.5	3.5	7	3.2	2	4.8	12	4.8	6.5	7.5	6	4.1	46	11.4	31	1	9	27	·	4	·	2	16	13	8	1	5	14	·
IV	14.5	3.3	9	4.7	11.5	3.8	9.5	4.3	9	4.3	8	4.2	12	4.5	7.5	4.9	9	3.8	45	13.2	26	·	·	1	4	3	·	2	12	12	9	2	·	1	1
V	6	2.9	2	3.0	8	2.3	7.5	2.7	10.5	2.7	12	3.5	27.5	3.8	11.5	3.9	8	3.0	183	64.8	14	·	·	2	·	2	1	·	17	25	19	4	4	·	4
VI	11	4.9	5.5	3.4	2.5	1.8	4.5	2.3	8.5	4.8	5.5	3.2	32.5	4.6	14	3.7	6	3.5	86	32.1	29	·	·	·	5	1	·	2	11	13	9	3	·	·	5
VII	5	3.8	7.5	3.1	2	2.0	5	1.9	7	2.6	21.5	3.3	31	4.1	11	3.7	3	3.3	22	4.8	13	·	·	·	5	·	·	·	5	13	5	·	1	·	8
VIII	1.5	2.3	2.5	2.6	4	3.6	9	2.9	9.5	2.9	20.5	3.5	31	5.0	5	4.0	10	3.5	48	18.5	15	·	·	·	7	·	·	1	7	15	10	1	·	·	7
IX	2.5	3.6	3.5	3.1	10.5	2.6	7	3.2	11.5	2.8	14.5	3.8	29	4.9	5.5	4.7	6	3.6	75	20.9	17	·	·	·	1	·	·	1	8	15	12	3	4	·	3
X	2	2.2	6.5	1.9	10.5	2.0	12.5	2.6	9.5	2.6	6.5	3.6	23.5	3.6	9	3.3	13	2.5	10	4.1	27	·	·	4	·	·	·	4	11	6	3	·	16	·	·
XI	5.5	3.3	6	6.1	17.5	4.6	20	4.1	7.5	2.9	4.5	4.4	14	5.0	8	2.8	7	3.9	40	8.6	15	·	·	9	·	·	·	1	25	14	9	·	7	·	·
XII	3	3.5	17.5	4.5	7	3.1	6	3.8	16	3.7	9.5	5.9	24	4.8	7	3.9	3	4.2	11	3.3	13	11	16	27	·	·	·	1	21	10	5	·	7	16	·
Rok	69.5	4.3	81.5	4.0	105.5	3.2	111.5	3.3	124	3.1	144	4.2	284	4.9	101	4.7	74	3.9	621	64.8	14.V	17	45	115	22	22	1	17	173	165	103	14	49	65	29

UWAGA. [1] Dn. 24.X.1962 r. stacja została przeniesiona na południowo-zachodnią stronę lotniska.
[2] Kierunki i prędkości wiatru – wg anemometru.

Jeziory $H_s = 84\,m$ $h_w = 15\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◐	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K
I	1	3.0	5	1.4	2	1.5	7	1.4	1	1.0	60	1.9	12	1.7	5	2.4	·	1.8	24	5.7	25	2	6	18	·	·	·	2	17	14	7	·	4	11	·
II	1	3.0	19	2.1	4	2.0	1	1.0	·	·	38	1.8	11	1.6	10	2.3	·	1.9	66	18.3	16	2	9	21	·	·	·	·	17	23	11	3	9	6	·
III	2	3.5	12	1.8	3	2.7	13	2.3	3	1.0	27	1.3	5	2.0	9	1.8	19	1.4	46	15.0	5	·	3	27	·	·	·	4	10	11	9	2	6	12	·
IV	6	1.2	12	1.7	2	1.5	8	2.0	3	1.0	29	1.8	12	1.8	13	1.6	5	1.6	23	5.0	29	·	·	1	4	·	·	6	9	13	9	·	1	1	1
V	2	1.0	8	1.2	2	2.0	4	1.2	2	1.5	45	1.3	20	2.4	6	1.7	4	1.5	86	23.5	14	·	·	2	·	·	·	1	13	21	16	1	7	·	4
VI	9	2.3	5	2.0		·	5	1.0	1	1.0	34	1.4	14	1.6	22	1.5	·	1.6	46	4.3	16	·	·	·	9	·	·	11	3	9	6	·	·	·	3
VII	1	1.0	13	1.2	1	1.0	7	1.0	1	2.0	49	1.4	15	1.3	5	1.4	1	1.3	53	7.8	12,28	·	·	·	6	·	·	5	8	15	13	·	7	·	6
VIII	4	1.2	1	1.0	·	·	7	1.1	2	2.5	64	1.5	12	1.9	3	1.7	·	1.5	66	15.2	13	·	·	·	6	·	·	5	8	13	13	2	3	·	4
IX	1	1.0	·	·	9	1.7	12	1.3	6	1.2	23	1.4	19	1.9	4	1.0	16	1.3	48	14.5	18	·	·	·	3	·	·	6	7	11	8	1	4	·	1
X	3	1.3	3	1.0	7	1.1	18	1.3	6	1.1	47	1.1	1	2.0	7	1.3	1	1.2	16	5.3	31	·	·	3	·	·	·	6	9	8	4	·	19	·	1
XI	1	1.0	16	1.8	11	2.2	21	1.6	·	·	32	1.2	4	1.5	3	1.7	2	1.5	28	7.1	1	·	–	8	·	·	·	3	21	15	7	·	11	·	·
XII	1	2.0	17	1.2	7	2.4	8	1.1	2	1.5	49	1.4	1	1.0	7	1.3	1	1.4	31	13.4	15	9	14	24	·	·	·	4	17	12	6	1	12	17	·
Rok	32	1.8	111	1.4	48	1.5	111	1.4	27	1.2	497	1.5	126	1.7	94	1.6	49	1.5	503	23.5	14.V	13	–	104	28	·	·	53	139	165	109	10	83	47	20

Świebodzin $H_s = 78\,m$ $h_w = 12{,}0\,m$ I–VIII, $13{,}5\,m$ IX–XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◐	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K
I	7.5	4.9	2	4.5	1	3.0	·	·	18.5	3.9	31	4.9	27.5	4.6	2.5	6.4	3	4.4	29	9.2	24	1	4	11	·	1	·	1	18	14	8	·	–	9	1
II	8.5	5.6	9.5	4.1	7.5	3.9	·	·	10	5.8	13.5	5.6	21	6.5	10	6.6	4	5.4	53	14.1	16	1	8	22	·	4	3	1	16	14	11	2	–	14	·
III	10	3.1	8	2.7	11	3.0	6.5	4.0	8	2.1	7	1.9	15.5	3.6	11	2.9	16	2.5	30	7.7	12	·	3	26	·	1	·	7	11	10	8	·	–	11	·
IV	12	3.4	4	3.4	7	4.4	4.5	3.4	5.5	1.5	14.5	4.1	21	3.7	7.5	3.7	14	3.0	36	8.2	16	·	·	·	5	·	·	6	10	11	8	·	–	1	·
V	10	2.6	1.5	3.7	3	2.3	4	1.8	5	2.9	8	2.0	43	2.7	8.5	2.9	10	2.4	109	20.6	12	·	·	3	·	1	·	·	9	21	16	4	–	·	4
VI	13	2.7	5	2.2	1	2.0	1.5	3.7	2	1.5	8	2.9	31.5	4.0	19	2.4	9	2.8	50	35.1	16	·	·	·	7	·	·	4	5	10	8	1	–	·	3
VII	13	1.3	4	1.4	0.5	1.0		·	11.5	2.5	14.5	2.3	28.5	2.6	10	1.9	11	1.9	47	6.5	12	·	·	·	7	1	·	2	8	11	10	·	–	·	2
VIII	5.5	2.5	6	2.8	1	1.0	3	2.3	11.5	2.8	15.5	3.0	21	3.0	10.5	3.0	19	2.3	68	14.8	13	·	·	·	5	·	·	2	7	12	12	1	–	·	4
IX	9.5	1.4	9	1.6	11.5	1.6	1.5	2.3	11.5	2.2	12.5	3.4	19	2.9	2.5	4.0	13	2.0	39	7.8	16	·	·	·	3	1	·	6	6	11	8	·	–	·	·
X	8.5	1.8	10	1.6	11.5	1.7	3.5	1.7	10.5	2.1	16	2.0	18	2.5	4	2.8	11	1.8	13	9.4	31	·	·	4	·	·	·	3	11	6	2	·	–	·	1
XI	8.5	1.6	14.5	3.1	13.5	3.4	10.5	2.8	9	2.2	15.5	2.6	11	1.5	4.5	2.6	3	2.5	20	5.2	1	·	·	9	·	2	·	2	19	11	8	·	–	2	·
XII	7.5	1.9	21	2.3	9	3.8	3.5	2.6	10	3.2	21.5	2.9	14.5	2.1	·	·	6	2.5	29	11.2	15	8	16	26	·	·	·	4	18	7	6	1	–	17	·
Rok	113.5	2.7	94.5	2.5	77.5	2.6	38.5	2.0	113	2.7	177.5	3.1	271.5	3.3	90	3.0	119	2.8	523	35.1	16.VI	10	31	101	27	11	3	38	138	138	105	9	–	54	15

Zbąszyń $H_s = 57\,m$ $h_w = 10\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◐	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K
I	8	3.0		·	·		2.5	2.2	25	2.8	28.5	4.5	19	5.6	7	4.3	3	3.9	31	8.6	24	2	4	12	·	5	·	·	18	16	9	·	1	–	·
II	3.5	3.6	4.5	2.9	12	3.2	5	1.9	5.5	2.7	19	4.6	20	7.0	10.5	6.8	4	4.6	38	10.4	12	1	7	22	·	6	2	·	20	19	10	1	·	–	1
III	10	3.0	9.5	2.2	9.5	2.5	18	2.7	10	2.2	8.5	2.8	5.5	3.3	11	3.8	11	2.5	29	7.0	12	1	5	27	·	·	·	1	15	10	9	·	3	–	·
IV	8.5	2.3	7.5	3.3	8.5	3.4	5.5	2.5	9.5	3.1	17	4.1	14.5	4.6	13	3.5	6	3.3	40	13.4	29	·	·	·	5	·	·	–	–	13	9	1	·	–	1
V	4	2.0	1.5	2.0	6	2.1	5.5	2.2	8.5	2.5	19	3.3	29	3.8	9.5	3.7	10	2.9	107	21.1	12	·	·	2	·	·	·	–	–	23	15	4	1	–	5
VI	11	4.8	4	2.5	3.5	1.6	6	2.2	1.5	3.3	11.5	3.2	29	4.6	13.5	3.0	10	3.3	11	4.8	16	·	·	·	8	1	·	3	8	5	4	·	·	–	3
VII	6.5	2.1	4.5	1.7	5	1.8	3.5	2.1	6.5	2.4	19	3.5	23.5	3.4	6.5	3.0	18	2.4	35	4.6	4	·	·	·	7	·	·	1	13	15	13	·	·	–	3
VIII	5	2.4	2	2.0	4	2.0	4	2.2	10	3.4	23.5	4.5	28.5	3.6	4	2.5	12	3.1	89	29.5	13	·	·	·	5	1	·	1	19	15	13	3	·	–	4
IX	·	·	1	2.0	11.5	4.0	2.5	2.0	9	2.7	10	4.4	33.5	5.0	1.5	2.3	21	3.2	33	8.2	16	·	·	·	3	1	1	5	13	13	5	·	3	–	·
X	4	1.9	3	1.0	19.5	2.1	6.5	2.0	4.5	2.7	6.5	2.2	20.5	3.6	7.5	3.0	21	2.0	16	8.6	5	·	·	5	·	·	·	4	12	5	2	·	6	–	·
XI	3.5	2.8	5.5	3.8	34	3.7	2.5	2.0	6	2.3	15	3.3	11.5	3.7	5	2.7	7	3.1	20	7.6	1	·	·	8	·	1	·	1	21	14	6	·	–	–	·
XII	9	2.2	10.5	3.4	12	3.1	3.5	2.3	17.5	2.8	18	4.2	11	3.5	4.5	2.8	7	3.0	25	10.4	15	9	14	27	·	2	·	3	17	10	5	1	–	–	·
Rok	73	2.5	53.5	2.2	125.5	2.5	65	2.2	113.5	2.7	195.5	3.7	245.5	4.3	93.5	3.4	130	3.1	474	29.5	13.VIII	13	30	103	28	17	3	–	–	158	100	10	–	–	17

Kórnik $\varphi = 52°15'$ $\lambda = 17°06'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.9	-1.6	9.4	22	-13.1	31	0.3	1.9	0.4	0.8	5.6	5.7	5.5	5.6	86	79	84	83	0.9	1.5	1.1	1.2	7.8	8.3	6.9	7.7
II	–	–	–	–	1.6	-3.2	7.5	20	-12.8	1	-2.2	0.3	-0.8	-0.9	4.4	5.3	4.9	4.9	83	81	79	81	0.9	1.2	1.0	1.0	8.6	9.0	6.8	8.1
III	–	–	–	–	2.8	-3.8	13.3	30	-13.3	8	-2.8	1.8	-0.8	-0.6	4.4	5.3	4.8	4.8	83	73	81	79	0.8	1.9	1.1	1.3	6.8	6.1	5.8	6.2
IV	–	–	–	–	15.4	5.6	27.7	23	-0.4	11	7.3	13.6	9.7	10.1	9.0	8.5	9.6	9.0	86	55	77	73	1.6	8.6	3.1	4.4	6.4	6.3	5.0	5.9
V	–	–	–	–	15.1	6.3	22.3	19	-2.0	1	8.9	13.5	10.0	10.6	10.2	9.8	10.6	10.2	88	64	86	79	1.4	6.1	1.8	3.1	7.2	8.0	7.6	7.6
VI	–	–	–	–	20.4	9.4	32.0	16	3.5	6	13.3	18.6	14.1	15.0	11.2	10.8	12.0	11.3	72	49	72	64	4.6	11.7	4.7	7.0	4.6	6.2	6.0	5.6
VII	–	–	–	–	21.1	10.1	32.8	26	5.0	29	13.9	19.5	14.9	15.8	13.6	12.8	14.0	13.5	85	58	82	75	2.5	10.7	3.2	5.5	6.5	6.5	6.0	6.4
VIII	–	–	–	–	21.7	12.5	30.1	12	7.2	10	14.6	20.2	15.9	16.6	14.2	13.8	14.1	14.0	85	60	78	74	2.5	10.5	4.2	5.7	6.6	7.5	4.9	6.3
IX	–	–	–	–	17.5	8.1	29.4	4	2.2	15	9.9	15.9	11.5	12.2	11.3	11.8	11.6	11.6	91	66	86	81	1.2	7.0	2.2	3.5	7.3	6.6	5.1	6.3
X	–	–	–	–	12.7	4.1	22.4	3	-1.8	16	5.9	11.8	7.0	7.9	9.2	10.3	9.5	9.7	96	74	92	87	0.4	4.1	0.9	1.8	7.6	5.9	4.5	6.0
XI	–	–	–	–	5.7	2.0	14.4	8	-2.4	21	2.9	5.2	3.6	3.8	7.2	7.7	7.5	7.5	94	86	92	91	0.5	1.4	0.6	0.8	8.8	8.3	8.2	8.4
XII	–	–	–	–	-1.9	-6.4	6.7	12	-18.4	22	-4.9	-3.1	-4.5	-4.2	4.3	4.5	4.3	4.4	9.3	8.8	9.1	9.1	0.3	0.7	0.4	0.5	8.4	7.4	6.7	7.5
Rok	–	–	–	–	11.2	3.6	32.8	26.VII	-18.4	22.XII	5.6	9.9	6.8	7.3	8.7	8.9	9.0	8.9	87	69	83	80	1.5	5.4	2.0	3.0	7.2	7.2	6.1	6.8

Sinołęka $\varphi = 52°13'$ $\lambda = 21°55'$

I	–	–	–	–	1.1	-3.1	6.3	23	-20.5	31	-1.6	-0.2	-1.1	-1.0	5.0	5.1	5.0	5.0	88	82	85	85	0.7	1.2	0.9	0.9	8.1	7.7	7.0	7.6
II	–	–	–	–	-1.0	-6.6	3.6	13	-16.8	1,2	-5.0	-2.3	-3.3	-3.5	3.8	4.2	4.2	4.1	84	80	85	83	0.7	1.0	0.7	0.8	7.8	8.5	7.4	7.9
III	–	–	–	–	0.4	-6.5	9.6	31	-18.0	26	-5.2	-1.0	-2.9	-3.0	3.8	4.3	4.2	4.1	84	73	81	79	0.6	1.5	0.9	1.0	8.2	7.0	5.5	6.9
IV	–	–	–	–	15.3	5.9	27.2	22	-0.2	8	7.5	14.0	9.9	10.3	9.1	10.1	10.1	9.8	86	62	80	76	1.6	7.4	2.7	3.9	6.8	6.2	4.7	5.9
V	–	–	–	–	15.0	6.7	20.3	28	-2.6	1	8.9	13.4	10.5	10.8	10.2	10.6	11.1	10.6	87	68	86	80	1.6	5.2	1.9	2.9	8.2	7.9	6.9	7.7
VI	–	–	–	–	18.9	9.4	28.7	23	4.7	6	13.0	16.9	13.8	14.4	11.9	11.7	12.6	12.1	78	60	78	72	3.6	8.7	3.8	5.4	5.7	6.2	5.3	5.7
VII	–	–	–	–	20.8	11.3	27.7	22,26	6.9	31	14.0	19.1	15.2	15.9	13.4	12.8	13.7	13.3	83	58	78	73	2.8	9.8	3.8	5.5	5.6	6.0	5.0	5.5
VIII	–	–	–	–	21.3	11.8	30.3	13	6.7	27	14.4	19.8	15.9	16.5	14.0	13.9	14.9	14.3	85	61	82	76	2.5	9.8	3.5	5.3	6.5	7.3	4.8	6.2
IX	–	–	–	–	16.6	8.0	25.8	5	1.5	25	9.1	15.2	11.4	11.8	10.7	11.5	11.8	11.3	92	67	87	82	1.0	6.2	1.9	3.0	6.0	6.8	4.4	5.7
X	–	–	–	–	12.1	3.8	18.8	2	-3.3	16	5.0	11.0	7.1	7.6	8.4	9.5	9.1	9.0	94	71	88	84	0.5	3.9	1.2	1.9	7.2	6.3	3.7	5.7
XI	–	–	–	–	6.0	1.6	16.0	1	-3.0	18	2.8	4.8	3.7	3.8	6.9	7.1	7.1	7.0	90	82	88	87	0.7	1.8	1.1	1.2	9.4	8.4	7.8	8.5
XII	–	–	–	–	-3.0	-7.6	3.4	10	-22.2	21	-5.7	-4.4	-5.6	-5.3	3.8	3.9	3.9	3.9	88	82	88	86	0.5	0.8	0.5	0.6	7.5	7.7	7.0	7.4
Rok	–	–	–	–	10.3	2.9	30.3	13.VIII	-22.2	21.XII	4.8	8.9	6.2	6.5	8.4	8.7	9.0	8.7	87	70	84	80	1.4	4.8	1.9	2.7	7.2	7.2	5.8	6.7

Pętkowo $\varphi = 52°12'$ $\lambda = 17°15'$

I	–	–	–	–	2.8	-1.6	9.2	22	-13.6	31	0.0	1.8	0.3	0.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	8.3	6.9	7.5
II	–	–	–	–	1.5	-3.6	7.3	20	-13.7	1	-2.3	0.2	-0.8	-0.9	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.2	6.4	7.6
III	–	–	–	–	3.2	-3.7	13.9	30	-12.3	8	-2.4	2.2	-0.3	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.1	6.3	6.3
IV	–	–	–	–	15.8	5.9	28.1	23	0.4	10	7.8	14.2	10.2	10.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.5	5.0	5.9
V	–	–	–	–	15.3	6.2	21.8	19	-2.9	1	9.3	13.8	10.2	10.9	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.4	6.6	7.0
VI	–	–	–	–	20.4	9.0	31.8	16	3.3	3	13.6	18.7	14.1	15.1	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.8	4.8	5.3
VII	–	–	–	–	20.7	9.7	30.3	26	4.9	29	14.1	19.3	16.0	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.8	6.3	6.4
VIII	–	–	–	–	21.4	11.6	29.7	13	6.6	10	14.8	20.0	16.0	16.7	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.6	5.2	6.5
IX	–	–	–	–	17.5	7.8	28.5	4	1.8	15	10.1	16.1	11.5	12.3	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.3	5.0	5.9
X	–	–	–	–	12.9	4.1	22.3	4	-2.1	24	6.0	12.0	7.1	8.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.0	4.4	5.7
XI	–	–	–	–	5.9	2.2	14.5	8	-5.3	21	3.0	5.3	3.9	4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.7	8.6	8.1
XII	–	–	–	–	-1.7	-6.1	6.6	12	-18.4	22	-4.6	-3.0	-4.3	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.1	6.9	7.6
Rok	–	–	–	–	11.3	3.5	31.8	16.VI	-18.4	22.XII	5.8	10.0	6.9	7.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.0	6.0	6.6

Koło $\varphi = 52°12'$ $\lambda = 18°38'$

I	–	–	–	–	2.6	-1.6	8.7	22	-14.1	31	-0.1	1.5	0.2	0.4	5.4	5.5	5.3	5.4	86	79	82	82	0.9	1.5	1.1	1.2	7.4	8.3	7.2	7.6
II	–	–	–	–	0.9	-4.1	5.4	12,20	-12.7	1	-2.6	-0.4	-1.4	-1.4	4.4	4.8	4.7	4.6	84	79	83	82	0.8	1.2	1.0	1.0	8.6	9.2	7.1	8.3
III	–	–	–	–	2.7	-3.5	14.0	31	-9.1	15	-2.5	1.8	-0.6	-0.5	4.5	4.9	4.8	4.7	86	69	80	78	0.7	2.2	1.1	1.3	7.9	7.3	6.5	7.2
IV	–	–	–	–	15.8	6.3	28.4	23	1.1	30	8.0	14.1	10.2	10.6	9.3	9.3	10.2	9.6	85	60	79	75	1.8	8.8	3.1	4.6	7.1	6.9	5.4	6.5
V	–	–	–	–	15.3	7.1	22.0	19	-2.1	1	9.1	13.8	10.6	11.0	10.5	10.5	11.3	10.8	8.9	67	86	81	1.4	5.8	1.8	3.0	7.8	7.9	7.4	7.7
VI	–	–	–	–	20.6	9.9	31.8	16	3.2	3	13.1	18.7	14.6	15.2	11.7	10.8	12.5	11.7	76	51	73	67	3.8	12.1	4.7	6.9	5.6	6.7	5.6	6.0
VII	–	–	–	–	21.7	10.6	32.4	26	6.5	29	14.0	20.1	15.5	16.3	13.8	12.5	13.9	13.4	8.5	54	78	72	2.5	11.8	4.2	6.2	5.8	7.1	5.7	6.2
VIII	–	–	–	–	22.4	12.6	31.2	7	7.9	10	14.9	20.7	16.0	16.9	14.5	14.0	15.2	14.6	8.5	58	82	75	2.5	11.3	3.3	5.7	6.9	8.0	5.3	6.7
IX	–	–	–	–	17.9	7.8	29.6	4	1.8	15	9.5	16.1	11.5	12.2	10.9	11.5	11.4	11.3	91	64	83	79	1.3	7.6	2.5	3.8	6.8	7.2	3.7	5.9
X	–	–	–	–	13.5	4.0	22.8	3	-3.4	24	5.7	12.5	7.1	8.1	9.1	10.0	9.4	9.5	9.6	69	91	8.5	0.4	5.0	1.1	2.2	7.3	6.5	3.5	5.8
XI	–	–	–	–	5.8	1.7	14.5	5	-5.5	26	2.9	5.0	3.5	3.7	7.1	7.6	7.4	7.4	9.3	8.5	9.2	9.0	0.5	1.5	0.7	0.9	8.7	7.8	7.5	8.0
XII	–	–	–	–	-2.3	-6.9	5.4	12	-20.6	22	-4.9	-3.3	-4.6	-4.4	4.0	4.3	4.1	4.1	8.7	8.3	8.6	8.5	0.5	0.8	0.6	0.6	8.6	8.3	7.3	8.1
Rok	–	–	–	–	11.4	3.7	32.4	26.VII	-20.6	22.XII	5.6	10.0	6.9	7.4	8.8	8.8	9.2	8.9	8.7	6.8	8.3	7.9	1.4	5.8	2.1	3.1	7.4	7.6	6.0	7.0

Kórnik $H_s = 77 m$ $h_w = 16 m$ 1962

MIESIĄC	ROZKŁAD WIATRU °D, °mD																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr v		◐	●	Opad R			═	⊠	R (G)
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15			R ≥ 0.1	R ≥ 1.0	R ≥ 10.0			
I	1	9.5	6	7.4	0.5	2.0	1.5	1.3	12.5	5.0	48.5	5.4	14.5	4.9	6.5	6.3	2	5.3	23	6.2	25	2	6	17	·	8	1	1	13	15	7	·	3	7	·
II	3.5	5.4	12	7.5	6.5	6.2	3.5	2.6	6.5	4.4	14	5.6	24	7.0	9	8.4	5	6.1	48	16.3	16	1	9	22	·	9	3		14	17	8	2	1	7	·
III	10	3.6	6	4.0	13	3.2	16	4.3	6.5	3.2	11	3.0	4.5	1.9	9	6.9	17	3.2	32	13.6	5	2	5	28	·	2	·	2	10	11	8	1	2	13	·
IV	5	5.2	6.5	5.3	8	4.9	7	3.0	7.5	4.1	22	4.7	8	3.2	12	4.8	14	3.8	23	5.1	13	·	·	1	3	6	2	4	8	15	8	·	1	·	1
V	3	3.3	3	3.0	0.5	3.0	5	2.0	9	2.6	25	2.6	22	3.8	5.5	8.0	20	2.6	93	30.3	14	·	·	2	·	2	1	·	14	22	17	1	·	·	4
VI	10.5	5.1	0.5	1.0	·		2.5	1.8	6.5	2.1	17	4.5	22	4.5	13	3.9	18	3.3	15	3.6	16	·	·	·	7	4	1	2	6	9	7	·	·	·	3
VII	2.5	2.2	5	4.6	1.5	1.7	·	·	4	2.1	27	3.1	23	3.2	9	3.7	21	2.5	39	8.4	3	·	·	·	6	·	·	1	11	14	9	·	2	·	7
VIII	5	1.4	1.5	1.3	0.5	2.0	5	3.4	5.5	3.2	28	3.7	25	4.2	4.5	2.9	18	2.9	66	21.7	13	·	·	·	6	3	·	2	11	15	13	2	·	·	2
IX	1.5	1.7	0.5	3.0	5	2.2	8.5	4.4	4.5	2.3	15.5	2.9	27	4.0	6.5	8.3	21	2.6	54	16.7	18	·	·	·	2	4	·	3	10	14	8	2	5	·	·
X	5.5	2.8	1.5	2.0	1.5	2.0	16	1.4	6	2.5	14.5	2.8	11.5	3.0	2.5	3.8	34	1.5	19	9.3	31	·	·	5	·	·	·	5	8	11	5	·	9	·	·
XI	1	3.0	5.5	5.3	13	4.5	13	3.5	4.5	3.3	23.5	3.3	10	2.4	4.5	2.3	15	2.9	39	14.0	1	·	·	9	·	3	·	3	24	17	7	1	8	·	·
XII	5	3.6	10.5	4.1	10.5	4.7	9.5	1.4	5.5	6.9	28.5	3.5	11	3.0	15	5.7	11	3.3	23	5.4	16	10	15	26	·	2	·	4	18	9	6	·	8	17	·
Rok	53.5	3.9	58.5	4.0	60.5	3.0	87.5	2.4	78.5	3.5	274.5	3.8	202.5	3.8	83.5	5.0	196	3.3	474	30.3	14.V	15	35	110	24	43	8	27	144	169	103	9	39	44	17

Sinołęka $H_s = 160 m$ $h_w = 11 m$

I	4.5	5.0	5	2.9	1.5	1.0	1	2.5	23	3.2	27.5	2.7	21.5	3.9	8	3.4	1	3.2	19	5.2	25	2	8	22	·	1	·	2	17	12	4	·	1	20	·
II	8.5	6.1	4	4.4	12.5	3.6	4	3.0	7.5	5.3	11	5.3	18.5	7.4	13	6.1	5	5.2	37	10.3	12	6	15	27	·	8	3	·	15	17	8	1	1	28	1
III	13	6.3	10	3.0	4.5	2.3	12.5	4.2	10.5	2.5	1.5	4.7	6.5	5.1	10	5.4	14	3.4	41	7.7	12	6	16	28	·	5	1	3	13	12	10	·	1	30	·
IV	8.5	2.4	8.5	3.9	9	2.7	11.5	4.0	13	3.9	7.5	2.9	5.5	3.5	7.5	7.3	19	3.0	51	11.8	26	·	·	1	4	1	1	3	7	10	8	1	1	2	3
V	6.5	2.1	2	1.5	2.5	2.8	6	3.2	10.5	2.8	9.5	2.8	17.5	4.3	22.5	3.2	16	2.6	114	34.6	14	·	·	1	·	3	·	·	17	21	17	2	2	·	3
VI	17	5.8	7.5	3.7	·	·	3	1.5	3.5	1.7	5	4.0	25.5	3.6	17.5	3.4	11	3.4	113	50.7	29	·	·	·	5	4		3	9	9	7	3	·	·	2
VII	10.5	2.3	6	2.0	·	·	1.5	1.7	5.5	2.3	19.5	2.1	19	3.6	18	3.1	13	2.3	48	11.8	22	·	·	·	5			2	5	11	10	1	·	·	3
VIII	5.5	2.5	0.5	3.0	4.5	3.0	4	3.0	7.5	2.3	21	2.5	25.5	3.2	10.5	3.1	17	2.3	53	19.9	15	·	·	·	5	·		1	6	12	9	1	1	·	3
IX	3.5	2.4	3.5	2.3	7.5	2.0	4	1.9	7.5	2.7	14.5	2.4	23	3.5	11.5	3.3	15	2.4	82	21.6	18	·	·	·	2			6	7	13	12	3	4	·	1
X	5	1.6	4	1.5	3.5	1.3	12	2.1	2	1.5	7.5	2.7	15.5	3.6	12.5	2.5	31	1.7	6	3.4	27	·		4	·			4	8	4	3	·	15	·	·
XI	12	1.8	3	7.2	11	6.0	28	4.4	5.5	1.9	3.5	3.7	14	3.4	6	2.5	7	3.5	40	8.9	15	·	·	8		1	·		21	14	12	·	6	1	
XII	11	2.3	12.5	2.7	3.5	1.6	10	2.3	14	4.0	9.5	3.7	17.5	3.2	6	2.3	9	2.7	12	4.0	16	10	20	29				4	16	11	4	·	4	21	·
Rok	105.5	3.4	66.5	3.2	67.5	2.2	97.5	2.8	110	2.8	137.5	3.3	209.5	4.0	143	3.8	158	3.0	616	50.7	29.VI	24	59	120	21	23	5	28	141	146	104	12	36	102	16

Pętkowo $H_s = 86 m$ $h_w = 13.5 m$ I–IV, $17.5 m$ V–XII

I	5	7.8	6	4.0			0.5	5.0	22.5	5.8	35	6.5	21	6.0	3	6.0	·	6.1	19	6.7	25	2	6	18	·	5	·	1	12	9	6	·	6	9	–
II	8	7.6	10.5	7.5	6	6.0	3.5	2.1	12.5	4.3	16	7.5	19.5	10.5	8	6.6	·	7.3	29	9.5	12	2	8	23	·	9	4	1	14	12	8	·	3	7	–
III	16	4.9	10	4.2	9.5	3.7	16.5	5.2	11.5	3.0	7.5	3.1	10	3.6	7	4.1	5	3.9	25	11.7	5	3	5	28	·	2	1	3	11	8	6	1	14	9	–
IV	11	4.1	8.5	5.9	9	3.3	5.5	5.5	7.5	6.0	20.5	5.3	15	4.3	11	4.4	2	4.7	19	5.2	13	·	·	·	5	5	·	4	7	12	7		3	·	–
V	3.5	3.1	3.5	2.9	5.5	2.9	7	3.9	14.5	2.8	22	3.8	31	5.6	5	4.2	1	3.9	92	29.1	14	·	·	2		2	·		8	23	17	1	4	·	–
VI	11	5.0	3	2.3	2.5	3.0	4	3.0	6.5	3.5	17.5	5.8	24	5.0	17.5	4.1	4	4.4	17	8.6	16	·	·	·	7	5	1	1	4	5	5		·	·	–
VII	13	3.0	2	2.2	2.5	2.2	2.5	1.6	5.5	2.7	26	4.1	18	3.6	8.5	3.5	15	2.9	43	7.0	3	·	·	·	3	·			8	14	12	·	2	·	–
VIII	3	3.0	3.5	3.7	0.5	5.0	5.5	4.5	9.5	3.2	20	4.8	39	4.7	11	3.2	1	4.2	69	18.7	13	·	·	·	6	2		2	8	14	13	2	4	·	–
IX	4	3.0	5	3.9	10.5	5.5	3.5	2.7	5.5	4.8	12	6.0	33	3.8	14.5	3.7	5	4.1	52	19.7	18	·			1	2		5	8	13	11	1	8	·	–
X	6	2.5	10.5	3.3	15.5	2.5	6.5	3.2	9	3.7	12	2.3	19.5	3.8	10	4.0	4	3.1	20	16.2	31	·	·	5		1		5	9	7	3	1	20	·	–
XI	2.5	4.0	20.5	8.4	15	6.4	5.5	4.8	5.5	2.7	10	3.4	15.5	3.7	9.5	3.1	6	4.9	32	7.3	18	·	·	8		5	1	2	21	13	8	·	13	·	–
XII	2	4.0	17	6.1	5	3.4	1	3.0	7	4.1	23	4.8	22	3.7	12	3.6	4	4.3	12	4.2	15	10	16	26	·	3	3	2	17	9	5	·	12	5	–
Rok	82	4.3	100	4.5	81.5	3.7	61.5	3.7	117	3.9	221.5	4.8	267.5	4.8	117	4.2	47	4.5	429	29.1	14.V	17	35	110	22	41	10	26	127	139	101	6	89	30	–

Koło $H_s = 95 m$ $h_w = 13.3 m$

I	3.5	5.0	4.5	2.9	1	1.0	4	2.9	15	2.2	16	3.3	33	4.3	5	4.2	11	3.1	19	8.9	25	2	4	19	·	1	1	2	15	14	4	·	7	14	·
II	4.5	3.9	6.5	3.2	11	3.4	3	1.3	6.5	2.6	11.5	4.2	19.5	6.1	11.5	5.4	10	3.8	46	16.7	12	2	11	24	·	5	2	·	18	15	8	2	2	13	·
III	8	4.0	8	2.9	17.5	2.1	13.5	1.9	3.5	1.9	4.5	1.8	7	2.9	9	4.3	22	2.1	36	10.0	12	·	7	27	·	·	·	2	15	12	6	1	2	11	
IV	7.5	3.0	6.5	2.6	14.5	2.4	6.5	2.2	11	1.9	8.5	3.5	13	2.8	8.5	3.4	14	2.3	32	8.5	29	·	·	·	6	·	·	4	10	12	7	·	·		
V	0.5	2.0	4.5	1.1	5.5	1.7	8.5	1.4	8	2.0	11.5	2.2	19	3.3	10.5	4.4	25	1.9	125	35.1	14	·	·	2		2	·	·	17	25	18	3	2	·	6
VI	10.5	3.8	3.5	3.0	4	1.0	5	1.2	2	1.2	3	3.0	29.5	4.0	14.5	3.0	18	2.6	30	14.5	30	·	·	·	7	·	·	2	10	10	6	1	1		6
VII	6	1.5	3.5	1.7	5	1.5	0.5	3.0	2	1.5	5	4.0	35.5	2.4	8.5	2.9	27	1.7	26	5.0	2	·	·	·	7	·	·	·	8	13	8	·	2	·	5
VIII	2.5	1.4	2	1.0	4	2.2	3	2.0	2.5	2.6	6.5	4.0	38.5	3.6	7	2.8	27	2.3	45	9.6	13	·	·	·	7	·	·	1	10	16	9	·	1	·	3
IX	1	3.0	2.5	1.0	7.5	1.7	2	1.0	3.5	1.6	4.5	4.2	28.5	3.4	12.5	2.4	28	1.9	49	18.2	18	·	·	·	3	·	·	2	7	15	7	2	4	·	3
X	4.5	1.6	3	1.0	8.5	1.6	6	1.8	3	2.0	2	1.5	18.5	2.7	5.5	1.6	42	1.1	22	6.2	28	·	·	5	·	·	·	2	7	11	5	·	17	·	·
XI	1	1.0	6	5.1	24.5	2.7	5	1.9	2.5	1.0	5.5	1.5	14	2.6	5.5	2.8	26	1.9	50	10.7	20	·	·	10	·		·	1	19	14	12	1	12	4	
XII	5	1.0	13	1.4	10	2.0	4	1.2	6	3.1	11.5	3.4	22.5	2.3	4	1.8	17	1.8	18	6.2	15	11	15	27	·	·	·	1	20	9	5	·	7	16	·
Rok	54.5	2.6	63.5	2.2	113	1.9	61	1.8	65.5	2.0	90	3.0	278.5	3.4	102	3.2	267	2.2	498	35.1	14.V	15	37	114	30	8	3	17	156	166	95	10	57	58	23

Niepokalanów $\varphi = 52°12'$ $\lambda = 20°25'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{s.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.6	-2.0	9.7	22	-17.1	31	-0.4	1.4	-0.1	0.2	5.3	5.2	5.3	5.3	85	75	84	81	0.9	1.8	1.1	1.3	7.9	6.9	6.3	7.0
II	–	–	–	–	0.8	-4.6	5.7	12	-14.9	1	-3.2	-0.7	-2.1	-2.0	4.2	4.8	4.5	4.5	84	81	84	83	0.8	1.2	0.8	0.9	7.8	8.3	7.2	7.8
III	–	–	–	–	2.4	-4.7	14.3	31	-13.1	15	-3.6	1.0	-1.4	-1.4	4.3	5.3	5.0	4.9	86	79	88	84	0.6	1.6	0.5	0.9	6.7	6.7	5.7	6.4
IV	–	–	–	–	16.2	6.1	28.1	23	0.4	30	8.1	14.7	9.9	10.6	9.2	9.5	10.1	9.6	84	57	79	73	2.0	8.8	2.8	4.5	6.1	5.8	5.2	5.7
V	–	–	–	–	15.8	6.9	22.3	8	-2.2	1	9.4	14.0	10.4	11.0	10.6	10.6	11.4	10.9	88	66	89	81	1.4	6.0	1.4	2.9	7.2	7.0	6.5	6.9
VI	–	–	–	–	19.9	9.8	30.0	16	4.5	8	13.1	18.4	14.1	14.9	12.2	11.8	13.4	12.5	78	56	81	72	3.4	10.4	3.2	5.7	6.4	5.3	4.8	5.5
VII	–	–	–	–	21.7	11.0	30.9	26	7.1	31	14.4	20.0	15.3	16.2	14.1	13.7	14.5	14.1	85	59	83	76	2.5	10.3	3.2	5.3	5.0	5.2	4.4	4.9
VIII	–	–	–	–	22.4	12.2	31.2	7	7.2	10	14.6	20.7	15.6	16.6	14.7	15.1	15.8	15.2	87	63	88	79	2.1	10.1	2.1	4.8	6.4	5.9	4.5	5.6
IX	–	–	–	–	17.8	7.7	28.8	4	2.5	25	9.4	16.4	11.4	12.2	11.0	12.2	12.3	11.8	92	66	90	83	1.1	7.0	1.4	3.2	6.0	6.6	4.4	5.7
X	–	–	–	–	13.4	4.1	21.1	2	-3.3	16	5.5	12.2	7.4	8.1	8.7	10.6	9.6	9.6	94	73	91	86	0.6	4.0	0.9	1.8	7.2	6.0	5.1	6.1
XI	–	–	–	–	6.1	2.3	12.7	1	-1.7	26	3.4	5.2	3.9	4.1	7.2	7.3	7.2	7.2	89	81	88	86	0.8	1.8	1.0	1.2	8.8	8.4	8.9	8.7
XII	–	–	–	–	-2.1	-6.8	5.0	12	-22.4	21	-5.1	-3.6	-4.5	-4.4	3.9	4.1	4.0	4.0	85	80	84	83	0.6	0.9	0.7	0.7	7.9	7.6	7.5	7.7
Rok	–	–	–	–	11.4	3.5	31.2	7.VIII	-22.4	21.XII	5.5	10.0	6.7	7.2	8.8	9.2	9.4	9.1	86	70	86	81	1.4	5.3	1.6	2.8	7.0	6.6	5.9	6.5

Łosice $\varphi = 52°12'$ $\lambda = 22°43'$

I	–	–	–	–	1.2	-3.4	5.5	22	-19.5	31	-1.7	-0.1	-1.5	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.5	8.0	8.0
II	–	–	–	–	-1.1	-6.6	3.2	13	-17.7	1	-4.8	-2.4	-3.4	-3.5	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.9	8.4	8.8
III	–	–	–	–	0.2	-7.4	7.0	31	-22.7	26	-5.3	-1.0	-3.7	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.9	6.5	7.0
IV	–	–	–	–	15.6	5.6	30.1	22	-0.3	2,3,8	8.2	14.1	9.6	10.4	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.6	5.1	6.3
V	–	–	–	–	15.6	6.9	21.0	28	-2.0	1	9.8	14.0	10.4	11.2	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.6	7.0	7.8
VI	–	–	–	–	19.4	9.3	29.0	23	3.8	7	13.4	17.5	13.3	14.4	–	–	–	–	–	–	–	–	–	–	–	–	6.1	7.2	5.4	6.2
VII	–	–	–	–	21.2	10.9	29.5	27	5.9	5	14.5	19.6	14.7	15.9	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.8	5.3	6.4
VIII	–	–	–	–	22.2	11.8	30.7	13	7.5	27	15.0	20.7	15.5	16.7	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.3	4.2	6.1
IX	–	–	–	–	17.1	7.8	26.9	5	1.4	25	9.8	15.8	11.4	12.1	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.9	4.1	5.8
X	–	–	–	–	12.2	3.6	19.0	2	-2.1	16	5.4	11.3	6.9	7.6	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.3	4.1	6.4
XI	–	–	–	–	6.6	1.8	18.9	1	-2.3	18	3.1	5.3	3.8	4.0	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.3	8.7	8.7
XII	–	–	–	–	-2.6	-8.3	3.3	10	-23.7	21	-6.3	-4.3	-5.9	-5.6	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.7	6.7	7.6
Rok	–	–	–	–	10.6	2.7	30.7	13.VIII	-23.7	21.XII	5.1	9.2	5.9	6.5	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.6	6.1	7.1

Siedlce $\varphi = 52°11'$ $\lambda = 22°16'$

I	997.2	1021.3	974.3	1015.9	1.1	-3.2	6.5	22	-21.6	31	-1.5	-0.2	-1.2	-1.0	5.2	5.3	5.2	5.2	91	85	89	88	0.5	1.0	0.7	0.7	8.2	8.0	7.9	8.0
II	996.2	1015.8	960.9	1015.2	-1.0	-6.9	2.8	12,13	-15.8	1	-5.1	-2.2	-3.2	-3.4	3.9	4.5	4.4	4.3	89	84	89	87	0.5	0.8	0.5	0.6	8.4	8.9	8.5	8.6
III	992.9	1010.7	971.2	1011.8	0.6	-7.3	8.9	31	-19.6	26	-5.5	-0.7	-3.4	-3.2	4.0	4.5	4.3	4.3	90	75	86	84	0.4	1.4	0.7	0.8	7.8	7.2	6.4	7.1
IV	–	–	–	–	15.5	5.5	27.1	22	-0.2	8	7.5	14.2	9.7	10.3	9.5	10.3	10.4	10.1	89	65	84	79	1.2	7.4	2.3	3.6	7.6	7.3	6.1	7.0
V	994.5	1002.8	972.2	1012.4	15.3	6.8	20.8	13	-2.4	1	9.3	13.8	10.7	11.1	10.9	11.3	11.6	11.3	91	71	89	84	1.2	5.0	1.6	2.6	8.2	8.6	7.4	8.1
VI	999.1	1009.1	988.5	1017.0	19.1	9.1	28.8	16	3.6	6	13.2	17.5	13.6	14.5	12.6	12.0	12.9	12.5	81	60	81	74	3.1	9.2	3.2	5.2	6.6	7.2	6.1	6.6
VII	996.2	1006.9	983.1	1013.8	21.0	10.7	28.4	27	6.0	31	14.2	19.5	14.7	15.8	14.0	13.8	14.0	13.9	86	61	83	77	2.4	9.4	3.1	5.0	6.4	7.3	5.3	6.3
VIII	997.4	1006.8	986.4	1015.0	21.6	11.3	30.8	13	6.3	10	14.6	20.1	15.5	16.4	14.8	15.0	15.3	15.0	88	64	86	79	2.0	9.1	2.7	4.6	6.7	7.1	5.5	6.4
IX	993.0	1013.3	980.3	1016.0	17.0	7.5	26.6	5	1.5	25	9.2	15.6	11.1	11.8	11.0	12.1	12.0	11.7	93	69	90	84	0.9	6.2	1.5	2.9	6.2	7.2	4.9	6.1
X	1004.3	1019.3	989.6	1022.6	12.1	3.1	19.6	2	-3.6	16	4.8	11.1	6.5	7.2	8.4	10.2	9.2	9.3	96	76	94	89	0.3	3.3	0.6	1.4	7.4	6.6	4.5	6.2
XI	1000.1	1014.0	984.7	1018.6	6.3	1.8	17.4	1	-1.9	18	3.0	5.3	3.8	4.0	7.2	7.6	7.4	7.4	92	85	90	89	0.6	1.7	0.9	1.1	9.2	8.3	8.7	8.7
XII	998.1	1026.7	957.3	1017.3	-2.9	-8.0	3.6	10	-22.7	21	-5.8	-4.1	-5.6	-5.3	3.9	4.1	3.9	4.0	90	85	89	88	0.4	0.8	0.5	0.6	8.5	7.8	7.4	7.9
Rok	–	1026.7	957.3	–	10.5	2.5	30.8	13.VIII	-22.7	21.XII	4.8	9.2	6.0	6.5	8.8	9.2	9.2	9.1	90	73	88	84	1.1	4.6	1.5	2.4	7.6	7.6	6.6	7.3

Reguły $\varphi = 52°10'$ $\lambda = 20°51'$

I	–	–	–	–	2.1	-2.3	9.0	22	-17.0	31	-0.6	0.9	-0.3	-0.1	5.7	5.8	5.7	5.7	93	86	92	90	0.4	1.0	0.5	0.6	8.5	7.7	7.5	7.9
II	–	–	–	–	0.0	-5.2	4.7	12	-14.1	1	-3.7	-1.1	-2.4	-2.4	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.1	8.0	8.3
III	–	–	–	–	1.6	-5.3	13.1	31	-13.8	15	-4.0	0.5	-1.9	-1.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.2	6.6	7.1
IV	–	–	–	–	15.8	5.7	27.5	23	0.0	30	7.6	14.6	9.4	10.2	9.6	9.8	10.5	10.0	90	61	86	79	1.3	8.5	1.8	3.9	7.0	6.6	5.7	6.4
V	–	–	–	–	15.2	6.7	22.1	8	-2.5	1	9.1	13.8	10.1	10.8	10.9	11.0	11.6	11.2	93	69	92	85	0.9	5.3	1.5	2.6	8.3	8.0	7.3	7.9
VI	–	–	–	–	19.5	9.5	29.8	16	5.2	7	13.4	18.0	13.5	14.6	12.4	11.7	13.1	12.4	79	57	82	73	3.5	10.1	2.9	5.5	6.8	6.3	5.8	6.3
VII	–	–	–	–	21.4	11.0	30.7	26	6.5	30	14.4	19.7	14.8	15.9	14.3	14.0	14.5	14.3	87	61	85	78	2.3	9.5	2.6	4.8	5.6	6.5	5.4	5.8
VIII	–	–	–	–	22.1	11.9	30.8	13	7.0	10	14.8	20.4	15.3	16.4	14.9	15.1	15.9	15.3	88	64	90	81	2.1	9.6	1.8	4.5	6.6	7.1	5.4	6.4
IX	–	–	–	–	17.3	7.7	27.3	4	3.1	25	10.1	15.9	11.2	12.1	11.4	12.3	12.3	12.0	92	69	92	84	1.2	6.3	1.2	2.9	6.5	7.1	5.1	6.2
X	–	–	–	–	12.5	3.9	20.1	2	-3.8	16	5.4	11.6	7.0	7.8	8.9	10.6	9.7	9.7	98	77	95	90	0.2	3.4	0.5	1.4	7.8	6.7	5.6	6.7
XI	–	–	–	–	5.8	1.6	14.4	1	-2.1	18	3.0	5.0	3.7	3.8	7.5	7.8	7.6	7.6	96	88	94	93	0.3	1.2	0.6	0.7	8.9	8.9	8.9	8.9
XII	–	–	–	–	-2.4	-7.1	3.9	12	-21.2	21	-5.3	-3.7	-4.6	-4.6	4.2	4.5	4.4	4.4	94	90	94	93	0.3	0.5	0.3	0.4	8.1	7.7	7.9	7.9
Rok	–	–	–	–	10.9	3.2	30.8	13.VIII	-21.2	21.XII	5.4	9.6	6.3	6.9	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.3	6.6	7.1

Niepokalanów $H_s = 92m$ $h_w = 24{,}5m$ 1962

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v≥10	v≥15	◔	●	Opad R ≥0.1	≥1.0	≥10.0	≡	⊞	⊠
I	2	6.0	7	5.8	2	3.2	1.5	2.0	6.5	4.2	24.5	4.7	35	6.0	14.5	5.1	·	5.3	21	7.1	25	2	6	19	·	2	·	2	14	14	5	·	3	11	·
II	6.5	6.3	7	4.4	11	5.1	7.5	2.9	4	4.8	9.5	4.7	21.5	6.2	17	7.5	·	5.6	38	9.3	12	2	12	24	·	6	·	1	17	19	10	·	2	14	·
III	10.5	5.6	5	3.0	26.5	2.5	18	2.7	9.5	4.2	4.5	2.3	4	5.2	11	6.3	4	3.5	53	12.9	12	1	6	27	·	1	·	7	14	16	11	1	4	19	·
IV	22.5	3.4	9.5	4.1	2	7.0	10.5	3.8	4.5	3.8	11	4.0	8.5	3.8	12.5	4.0	9	3.5	42	11.6	13	·	·	·	5	·	·	3	5	13	9	1	2	·	1
V	16	2.8	4.5	2.1	0.5	3.0	1.5	4.0	3	5.2	7.5	4.3	19.5	4.5	25.5	4.1	15	3.2	183	79.0	14	·	·	4	·	2	·	3	10	24	18	3	2	·	5
VI	21	3.7	4.5	3.9	1	7.0	2	3.2	3	2.3	5	3.2	20.5	4.9	27	4.5	6	3.9	79	25.6	29	·	·	·	6	·	·	2	7	12	11	3	·	·	5
VII	15	2.8	7.5	1.9	3	1.0	·	·	1	4.0	6.5	4.4	23.5	3.7	30.5	4.1	6	3.3	36	12.0	12	·	·	·	5	·	·	3	2	12	8	1	2	·	5
VIII	5	1.5	1	1.5	·	·	3.5	3.3	1.5	3.0	16	4.0	29	4.6	21	4.5	16	3.4	74	36.8	17	·	·	·	8	·	·	2	5	15	8	1	2	·	4
IX	2.5	4.4	1	4.5	6.5	2.2	10	3.1	4	2.2	10.5	4.9	25.5	4.4	20	4.6	10	3.6	68	21.2	18	·	·	·	2	·	·	4	7	17	9	3	5	·	1
X	6	2.9	5.5	2.2	8.5	2.1	17.5	2.3	5.5	2.5	6	3.2	12.5	4.2	12.5	4.1	19	2.4	10	4.0	27	·	·	5	·	·	·	3	10	7	3	·	14	·	·
XI	10	2.1	3	2.3	16.5	5.0	25	5.0	5.5	3.2	5	3.2	15	4.1	8	4.5	2	4.1	40	7.0	20	·	·	7	·	·	·	1	21	14	11	·	9	·	·
XII	7	2.7	18	3.6	3.5	3.7	9	3.2	4	2.6	17	4.4	13	3.9	21.5	3.5	·	3.6	15	6.2	16	11	15	26	·	·	·	1	15	10	6	·	7	17	·
Rok	124	3.7	73.5	3.3	81	3.5	106	3.0	52	3.5	123	3.9	227.5	4.6	221	4.7	87	3.8	659	79.0	14.V	16	39	112	26	11	·	32	127	173	109	13	52	61	21

Łosice $H_s = 153m$ $h_w = 14m$

I	4	8.8	2.5	2.2	2.5	2.6	4.5	4.1	2.7	5.1	4.0	4.7	10	4.0	15	5.7	1	4.7	21	6.4	25	2	6	24	·	2	·	1	19	11	6	·	-	20	·
II	8.5	4.9	5.5	4.9	13.5	4.6	6	6.4	16.5	6.3	15.5	5.4	11	5.8	6.5	7.1	1	5.5	25	6.9	12	4	16	28	·	5	3	·	19	18	7	·	-	28	·
III	7	6.2	3.5	4.4	15	3.7	22	5.0	18	3.5	10.5	4.7	8	4.4	7	5.2	2	4.4	37	13.6	12	9	15	28	·	1	1	4	17	11	8	1	-	31	·
IV	5	3.6	4.5	3.9	8.5	3.3	18	5.4	3.5	3.6	5.5	3.3	5.5	3.5	8	5.0	·	4.0	49	8.7	26	·	·	3	3	1	·	2	8	11	10	·	-	1	1
V	1.5	4.3	1	3.0	2.5	4.6	12	4.0	2.8	2.8	21.5	3.1	11	6.2	12.5	3.1	3	3.4	131	26.5	14	·	·	2	·	·	·	·	17	20	18	3	-	·	4
VI	13.5	6.4	1	7.5	2	3.0	1.5	3.7	16.5	2.8	3.6	3.3	1.0	3.0	7.5	3.3	2	3.6	89	26.7	4	·	·	·	6	3	·	3	13	11	10	3	-	·	3
VII	6	3.5	2	2.0	1	1.0	4	2.8	20.5	3.6	3.2	2.8	13.5	4.4	8	3.2	6	3.1	55	15.8	22	·	·	·	5	·	·	1	10	15	12	1	-	·	7
VIII	·	·	1	3.0	1	5.0	8.5	6.0	2.9	3.5	4.1	4.4	2	4.2	4.5	4.3	6	4.0	60	20.5	15	·	·	·	7	1	·	1	7	15	12	2	-	·	4
IX	3	3.3	1.5	2.0	6.5	3.5	10.5	3.4	15	3.5	37.5	4.1	10.5	4.3	15	4.7	4	3.6	67	13.8	17	·	·	·	2	1	·	4	7	14	11	3	-	·	1
X	5	2.4	·	·	1	3.0	22.5	3.6	14.5	2.1	3.1	2.6	8	3.9	7	2.7	4	2.8	7	4.1	27	·	·	5	·	1	·	3	11	5	2	·	-	·	·
XI	10.5	3.1	1.5	6.0	17.5	7.9	33	5.8	3.5	3.4	10.5	5.0	8.5	3.4	5	3.2	·	5.3	46	9.7	23	·	·	8	·	3	·	1	24	14	13	·	-	3	·
XII	10.5	4.1	11	3.4	1.5	2.3	15.5	3.4	19.5	5.9	22.5	4.2	5.5	4.1	5	3.0	2	4.1	15	5.1	14	10	17	31	·	1	·	2	18	9	4	·	-	22	·
Rok	74.5	4.2	3.5	3.5	72.5	3.7	158	4.5	243	3.8	303.5	4.0	103.5	4.3	74	4.0	31	4.0	602	26.7	4.VI	25	54	129	23	19	4	22	170	154	113	13	-	105	20

Siedlce $H_s = 146m$ $H_b = 149{,}1m$ $h_w = 13m$

I	2.5	6.2	6	3.5	1.5	2.3	2	2.0	2.4	4.4	32.5	5.1	19.5	5.0	5	3.5	·	4.6	22	5.0	25	2	8	23	·	1	·	1	20	14	6	·	2	18	·
II	9.5	4.4	3.5	4.9	13	4.0	8.5	3.4	9.5	5.8	12	8.2	14.5	6.5	9.5	7.2	4	5.4	30	7.3	12	7	15	28	·	9	5	·	19	18	8	·	2	28	·
III	18	3.9	13	3.7	12.5	2.1	22	2.7	5	4.4	5	3.5	9.5	4.4	6	3.2	2	3.3	44	10.3	12	9	15	28	·	3	·	3	17	13	9	1	3	26	·
IV	5.5	5.7	11.5	3.9	10	2.6	16	2.9	11.5	3.9	13	3.3	3	3.3	9.5	3.2	10	3.1	51	16.5	13	·	·	1	4	2	2	2	12	15	7	2	2	1	2
V	7.5	1.6	5.5	2.0	2.5	1.8	4.5	3.3	7	3.3	15.5	3.3	21	4.2	16.5	3.6	13	2.8	109	22.5	14	·	·	1	·	2	·	·	20	24	18	3	1	·	5
VI	17.5	3.9	7	2.9	·	·	4.5	2.3	5	2.5	11.5	3.1	24	3.9	12.5	3.0	8	3.1	93	28.9	4	·	·	·	6	4	1	2	11	11	11	3	·	·	5
VII	9	2.3	5.5	2.1	·	·	3.5	2.3	7.5	3.0	16	3.2	28	3.4	12.5	2.4	11	2.6	55	18.0	23	·	·	·	4	1	·	·	4	16	10	1	·	·	7
VIII	3.5	1.9	2	1.8	0.5	2.0	8.5	2.5	13.5	2.5	23.5	3.8	27.5	4.0	6	3.8	8	3.1	55	13.2	15	·	·	·	6	3	·	·	10	17	10	2	1	·	5
IX	1	3.0	5	2.2	8.5	1.6	6.5	1.9	8	3.7	25.5	4.0	20	4.4	6.5	3.8	9	3.2	85	20.6	18	·	·	·	2	3	1	3	8	18	15	4	4	·	1
X	3	1.7	8	1.6	7.5	1.6	14.5	2.7	4	2.5	8	4.1	16.5	3.4	6.5	2.5	2.5	2.0	8	3.2	27	·	·	6	·	·	·	2	10	6	3	·	16	·	·
XI	9.5	2.1	3.5	4.4	2.2	5.0	2.5	3.8	5	2.6	6.5	4.5	12	3.4	3.5	2.1	3	3.7	44	6.6	15	·	·	6	·	·	·	·	23	15	13	·	9	2	·
XII	7.5	4.2	18.5	3.8	1.5	3.0	16	2.1	13	5.6	13	5.3	16	3.8	5.5	3.0	2	3.9	19	6.2	14	10	19	29	·	·	·	1	19	11	4	·	7	17	·
Rok	94	3.4	89	3.1	79.5	2.2	131.5	2.7	113	3.7	182	4.3	211.5	4.1	99.5	3.4	95	3.4	615	28.9	4.VI	28	57	122	22	28	9	14	173	178	114	16	47	92	25

Reguły $H_s = 98m$ $h_w = 14{,}5m$

I	4.5	4.8	4.5	4.2	2.5	3.4	4	2.4	1.8	2.2	2.8	2.0	25.5	3.2	6	2.9	·	2.7	23	8.3	25	2	7	19	·	·	·	1	19	13	8	·	4	13	·
II	6	6.6	6	3.8	11	3.7	8	2.3	8	2.9	12.5	4.1	17	4.9	10.5	6.2	5	4.1	45	10.0	12	3	13	25	·	4	·	·	19	16	10	1	3	20	·
III	15.5	4.2	9	3.3	14.5	2.5	20	2.8	5.5	2.0	0.5	3.0	9	4.0	8	3.6	11	2.8	53	10.5	12	3	7	26	·	1	·	3	17	14	11	2	7	20	·
IV	15.5	2.8	6	2.1	8	2.5	12.5	3.2	9	3.7	8	3.5	9	3.6	6	3.8	16	2.6	38	9.4	13,26	·	·	·	4	·	·	2	8	11	7	·	7	·	2
V	10	2.2	2	1.0	6.5	3.0	7.5	2.1	6	2.2	9	1.6	23	2.7	17	2.2	12	2.0	189	56.4	14	·	·	2	·	·	·	2	18	24	20	4	4	·	1
VI	12.5	3.3	4	2.4	3	1.7	7	1.6	2.5	1.4	9	2.1	22	2.7	18	2.7	12	2.2	127	44.0	29	·	·	·	5	·	·	2	11	12	9	4	·	·	4
VII	12.5	2.4	3	2.3	2.5	2.6	4.5	1.4	4.5	1.3	10	1.8	33	2.5	14	2.4	9	2.0	25	7.4	12	·	·	·	5	·	·	1	5	9	7	·	2	·	4
VIII	1	1.0	0.5	2.0	2	2.5	6	2.2	6	2.6	16	2.0	30.5	2.9	8	2.7	23	1.9	67	21.0	15	·	·	·	6	·	·	1	9	15	11	2	5	·	6
IX	4	2.2	4.5	2.0	10.5	2.3	4	2.1	9.5	2.5	12.5	2.6	31.5	2.5	7.5	3.1	6	2.3	77	17.1	17	·	·	·	1	1	·	3	9	14	11	4	4	·	2
X	5.5	1.5	5.5	2.0	8	1.9	18.5	1.8	1.5	2.7	5.5	1.2	21.5	2.1	11	1.5	16	1.5	12	5.6	27	·	·	5	·	·	·	1	11	6	3	·	17	·	·
XI	5.5	1.5	7	2.8	2.1	3.6	12	4.1	3.5	3.1	6.5	4.0	13	3.7	9.5	1.7	12	2.8	50	10.0	15	·	·	7	·	·	·	1	24	12	10	1	6	·	·
XII	7	2.8	12.5	2.0	5	2.6	13	1.9	8	3.1	10.5	4.0	22.5	3.2	11.5	2.2	3	2.6	14	3.8	15	12	15	27	·	·	·	1	18	8	5	·	5	16	·
Rok	99.5	2.9	64.5	2.5	94.5	2.7	117	2.3	82	2.5	128	2.7	257.5	3.2	127	2.9	125	2.5	720	56.4	14.V	20	42	111	21	6	·	18	168	154	112	18	64	69	19

Brwinów $\varphi = 52°08'$ $\lambda = 20°43'$ 196_

MIESIĄC	CIŚNIENIE p				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1003.4	1028.0	978.3	1015.8	2.4	-1.9	9.2	22	-16.7	31	-0.4	1.0	-0.1	0.1	5.2	5.2	5.2	5.2	8.5	7.7	8.3	8.2	1.0	1.6	1.1	1.2	7.8	7.2	7.0	7.3
II	1002.8	1023.2	968.5	1015.3	0.4	-4.8	5.6	12	-14.1	1	-3.5	-1.1	-2.3	-2.3	4.1	4.5	4.6	4.4	8.4	7.9	8.6	8.3	0.8	1.2	0.7	0.9	7.7	8.4	7.6	7.9
III	999.2	1016.3	977.5	1011.7	2.1	-5.0	13.8	31	-12.5	15	-3.8	0.5	-1.6	-1.6	4.3	4.5	4.5	4.4	8.8	6.9	8.0	7.9	0.6	2.0	1.0	1.2	7.1	7.2	6.4	6.9
IV	1001.8	1016.8	976.3	1013.7	16.1	6.4	27.3	23	0.2	30	8.0	14.4	10.1	10.6	9.2	9.5	10.2	9.6	8.4	5.9	8.0	7.4	2.0	8.5	2.8	4.4	7.1	6.6	5.2	6.5
V	1000.6	1008.5	980.2	1012.5	15.4	7.2	22.0	8	-2.3	1	9.1	13.7	10.4	10.9	10.6	10.8	11.5	11.0	9.0	6.9	9.0	8.3	1.3	5.4	1.4	2.7	8.4	7.7	6.8	7.6
VI	1005.7	1016.3	995.0	1017.6	19.6	10.1	29.7	16	4.1	8	13.1	17.8	14.0	14.7	12.1	11.6	13.2	12.3	7.9	5.7	8.1	7.2	3.6	9.8	3.4	5.6	6.8	5.9	5.3	6.0
VII	1002.4	1013.8	988.6	1014.1	21.5	11.1	30.8	26	6.8	31	14.0	19.8	15.1	16.0	13.9	13.5	14.3	13.9	8.7	5.9	8.2	7.6	2.3	10.2	3.3	5.3	5.5	6.0	5.1	5.5
VIII	1003.4	1012.4	993.0	1015.1	22.2	12.9	31.0	7	7.1	10	15.0	20.2	15.6	16.6	14.6	14.7	15.6	15.0	8.5	6.3	8.7	7.8	2.6	9.8	2.4	4.9	6.3	6.5	4.8	5.9
IX	1004.1	1018.9	986.9	1015.9	17.4	8.4	27.7	4	3.5	25	9.8	15.8	11.7	12.2	11.3	12.7	12.5	12.2	9.2	7.2	9.0	8.5	1.1	5.8	1.6	2.8	6.2	6.7	3.8	5.6
X	1014.4	1025.0	997.3	1022.6	12.8	4.3	20.0	2	-3.3	16	5.6	11.6	7.4	8.0	9.0	10.5	9.7	9.7	9.6	7.6	9.2	8.8	0.3	3.5	0.8	1.5	7.2	6.1	4.4	5.9
XI	1005.7	1020.6	988.0	1018.0	6.1	2.1	13.7	1	-1.5	18	3.2	5.0	3.8	4.0	7.3	7.4	7.3	7.3	9.2	8.4	8.9	8.8	0.6	1.5	1.0	1.0	8.7	8.9	8.9	8.8
XII	1004.6	1033.7	961.4	1017.2	-2.1	-6.6	5.0	12	-20.1	21	-5.2	-3.7	-4.5	-4.5	4.0	4.1	4.1	4.1	8.8	8.2	8.6	8.5	0.5	0.9	0.7	0.7	8.1	7.7	8.0	7.9
Rok	1003.7	1033.7	961.4	1015.8	11.2	3.7	31.0	7.VIII	-20.1	21.XII	5.4	9.6	6.6	7.0	8.8	9.1	9.4	9.1	8.8	7.0	8.6	8.1	1.4	5.0	1.7	2.7	7.2	7.1	6.1	6.8

Wielichowo $\varphi = 52°07'$ $\lambda = 16°21'$

I	-	-	-	-	3.5	-1.6	9.8	22	-11.2	31	0.5	2.6	0.5	1.0	-	-	-	-	-	-	-	-	-	-	-	-	7.7	7.9	6.7	7.4
II	-	-	-	-	2.0	-3.4	7.8	20	-12.3	1	-1.5	0.8	-1.1	-0.7	-	-	-	-	-	-	-	-	-	-	-	-	8.6	8.9	6.6	8.0
III	-	-	-	-	3.5	-3.2	14.4	30	-11.4	8	-2.1	2.7	-0.1	0.1	-	-	-	-	-	-	-	-	-	-	-	-	6.5	6.5	6.2	6.4
IV	-	-	-	-	15.8	4.9	27.8	23	-1.6	10	7.4	14.1	9.4	10.1	-	-	-	-	-	-	-	-	-	-	-	-	6.2	6.4	5.6	6.1
V	-	-	-	-	14.8	5.5	24.8	19	-3.3	1	8.8	13.7	9.5	10.4	-	-	-	-	-	-	-	-	-	-	-	-	7.5	8.4	7.1	7.7
VI	-	-	-	-	20.2	8.6	30.7	16	0.1	3	13.1	18.8	13.8	14.9	-	-	-	-	-	-	-	-	-	-	-	-	5.2	6.0	5.2	5.5
VII	-	-	-	-	21.0	9.7	32.5	26	4.6	25	13.7	19.2	14.6	15.5	-	-	-	-	-	-	-	-	-	-	-	-	6.3	6.7	6.4	6.5
VIII	-	-	-	-	21.7	11.6	29.6	12	6.2	10	14.3	20.1	15.3	16.2	-	-	-	-	-	-	-	-	-	-	-	-	6.9	7.5	5.5	6.6
IX	-	-	-	-	17.8	6.9	29.4	4	0.0	15	9.1	16.6	11.1	12.0	-	-	-	-	-	-	-	-	-	-	-	-	6.8	6.5	3.7	5.[illegible]
X	-	-	-	-	13.2	4.0	23.5	3	-3.8	24	5.6	12.6	7.2	8.2	-	-	-	-	-	-	-	-	-	-	-	-	7.4	5.9	4.4	5.[illegible]
XI	-	-	-	-	6.1	2.0	16.6	8	-4.1	21	3.0	5.6	3.8	4.0	-	-	-	-	-	-	-	-	-	-	-	-	8.6	8.4	7.4	8.[illegible]
XII	-	-	-	-	-1.4	-6.0	7.4	12	-17.0	22	-4.3	-2.3	-3.8	-3.6	-	-	-	-	-	-	-	-	-	-	-	-	7.9	7.8	6.5	7.[illegible]
Rok	-	-	-	-	11.5	3.2	32.5	26.VII	-17.0	22.XII	5.6	10.4	6.7	7.4	-	-	-	-	-	-	-	-	-	-	-	-	7.1	7.2	5.9	6.7

Łowicz $\varphi = 52°07'$ $\lambda = 19°56'$

I	-	-	-	-	2.6	-2.2	9.5	22	-16.1	31	-0.1	1.5	0.0	0.4	-	-	-	-	-	-	-	-	-	-	-	-	8.7	8.4	7.2	8.1
II	-	-	-	-	0.8	-4.5	5.6	12	-14.3	1	-2.7	-0.6	-2.0	-1.8	-	-	-	-	-	-	-	-	-	-	-	-	9.4	9.2	8.1	8.3
III	-	-	-	-	2.3	-4.0	14.5	31	-9.0	4,15	-2.9	1.0	-0.8	-0.9	-	-	-	-	-	-	-	-	-	-	-	-	7.6	7.9	6.9	7.5
IV	-	-	-	-	16.1	6.4	28.5	23	1.0	30	8.5	14.6	10.2	10.9	-	-	-	-	-	-	-	-	-	-	-	-	7.7	7.7	6.2	7.2
V	-	-	-	-	15.4	7.3	22.8	8	-2.1	1	10.0	13.8	10.7	11.3	-	-	-	-	-	-	-	-	-	-	-	-	8.5	8.6	7.6	8.2
VI	-	-	-	-	19.9	10.4	30.4	16	5.3	3	13.6	18.2	14.7	15.3	-	-	-	-	-	-	-	-	-	-	-	-	6.5	6.9	6.4	6.6
VII	-	-	-	-	21.6	11.3	31.4	26	6.2	29	15.5	20.0	15.0	16.4	-	-	-	-	-	-	-	-	-	-	-	-	6.4	7.1	6.5	6.7
VIII	-	-	-	-	22.5	12.5	31.6	7	7.4	10	15.6	20.8	15.8	17.0	-	-	-	-	-	-	-	-	-	-	-	-	7.3	8.1	6.9	7.4
IX	-	-	-	-	17.6	8.0	28.1	4	2.5	25	10.0	16.2	11.7	12.4	-	-	-	-	-	-	-	-	-	-	-	-	6.9	7.6	5.6	6.8
X	-	-	-	-	13.4	4.3	21.0	2	-3.0	16	5.7	12.5	7.2	8.2	-	-	-	-	-	-	-	-	-	-	-	-	8.3	6.3	5.9	6.8
XI	-	-	-	-	5.9	2.2	13.1	5	-1.6	18	3.2	5.2	3.8	4.0	-	-	-	-	-	-	-	-	-	-	-	-	8.9	9.2	8.3	9.0
XII	-	-	-	-	-2.2	-6.6	5.2	12	-20.5	22	-4.9	-3.5	-4.5	-4.4	-	-	-	-	-	-	-	-	-	-	-	-	9.0	8.0	8.0	8.3
Rok	-	-	-	-	11.3	3.8	31.6	7.VIII	-20.5	22.XII	6.0	10.0	6.8	7.4	-	-	-	-	-	-	-	-	-	-	-	-	7.9	7.9	7.0	7.6

Świder $\varphi = 52°07'$ $\lambda = 21°15'$

I	-	-	-	-	2.0	-3.0	9.5	22	-20.2	31	-1.2	0.9	-0.7	-0.4	5.0	5.1	5.1	5.1	8.6	7.6	8.4	8.2	0.8	1.6	1.0	1.1	8.3	8.2	8.1	8.2
II	-	-	-	-	0.3	-5.7	4.7	10	-15.2	1	-4.2	-0.7	-2.5	-2.4	3.8	4.2	4.4	4.1	8.0	7.2	8.3	7.8	0.9	1.7	0.8	1.1	8.5	8.4	7.3	8.1
III	-	-	-	-	2.3	-5.9	13.7	31	-14.6	26	-4.5	0.9	-1.9	-1.8	3.9	4.2	4.3	4.1	8.3	6.3	7.7	7.4	0.7	2.5	1.2	1.5	8.2	7.7	7.1	7.7
IV	-	-	-	-	16.6	5.6	28.3	23	-3.2	8	8.1	15.1	9.6	10.6	9.1	9.1	9.6	9.3	8.3	5.6	7.9	7.3	2.1	9.7	2.9	4.9	7.9	7.0	6.5	7.4
V	-	-	-	-	15.9	6.5	23.3	8	-2.9	1	9.3	14.3	10.2	11.0	10.8	10.4	11.1	10.8	9.0	6.4	8.8	8.1	1.2	6.5	1.6	3.1	8.6	8.2	7.7	8.2
VI	-	-	-	-	20.0	9.0	30.3	23	3.8	8	13.5	18.5	13.4	14.7	12.2	11.3	12.6	12.0	7.7	5.4	8.1	7.1	3.8	11.2	3.2	6.1	7.0	7.0	6.1	6.7
VII	-	-	-	-	22.0	11.0	30.3	26	5.7	31	14.5	20.6	14.9	16.2	14.0	13.1	14.1	13.7	8.4	5.4	8.3	7.4	2.8	11.8	3.2	5.9	5.6	6.9	5.5	6.0
VIII	-	-	-	-	22.3	11.8	31.6	7	6.2	29	14.5	20.7	15.2	16.4	14.8	14.6	15.4	14.9	8.9	6.2	8.8	8.0	1.9	10.5	2.2	4.9	7.4	7.5	5.1	6.7
IX	-	-	-	-	17.5	7.8	27.5	4	2.4	15	9.5	16.2	11.4	12.1	11.2	12.4	12.1	11.9	9.4	6.8	8.9	8.4	0.9	6.7	1.7	3.1	7.1	7.5	5.6	6.7
X	-	-	-	-	12.9	3.4	20.7	2	-4.5	16	5.1	12.1	6.6	7.6	8.5	10.1	9.2	9.3	9.5	7.2	9.2	8.6	0.5	4.4	0.8	1.9	8.4	6.7	5.6	6.9
XI	-	-	-	-	6.4	2.1	16.4	1	-2.2	26	3.3	5.6	4.0	4.2	7.2	7.5	7.2	7.3	9.1	8.1	8.7	8.6	0.7	2.0	1.2	1.3	9.2	9.0	8.2	8.8
XII	-	-	-	-	-2.2	-7.1	3.5	10	-20.7	22	-5.1	-3.4	-4.7	-4.5	3.9	4.1	4.0	4.0	8.5	7.8	8.4	8.2	0.6	1.1	0.7	0.8	8.2	8.5	8.9	8.5
Rok	-	-	-	-	11.3	3.0	31.6	7.VIII	-20.7	22.XII	5.2	10.1	6.3	7.0	8.7	8.8	9.1	8.9	8.6	6.7	8.5	7.9	1.4	5.8	1.7	3.0	7.9	7.8	6.8	7.5

Brwinów $H_s = 96\,m$ $H_b = 98.0\,m$ $h_w = 11\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU (n D, v m/s) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v > 15	◐	●	Opad R R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	☈
I	3.5	6.0	4	4.1	1	4.5	4	4.0	19.5	4.1	34.5	5.1	23.5	4.6	3	4.0	·	4.6	18	7.4	25	2	6	18	·	2	·	2	16	12	4	·	1	7	·
II	7	4.6	6	3.7	10	4.0	7.5	3.7	8.5	4.6	17	7.4	12	5.1	10	8.0	6	5.1	32	7.8	12	2	12	23	·	6	3	1	15	16	11	·	2	12	2
III	10.5	4.2	6.5	2.9	15.5	2.7	17	3.2	7	2.4	15	4.7	9.5	4.1	9.5	3.5	16	2.8	48	10.2	12	4	7	27	·	1	·	6	16	13	7	2	·	16	
IV	11	2.9	6.5	2.6	6.5	3.2	11.5	4.6	8	3.6	18.5	2.9	5	4.2	12	3.8	11	3.0	46	17.7	26	·	·	·	3	·	·	2	9	12	10	1	·	·	1
V	5	2.0	1	2.0	3	1.8	10	2.8	6	2.5	15	2.8	26.5	4.4	15.5	2.5	11	2.8	215	91.3	14	·	·	2	·	2	·	3	18	23	16	4	1	·	3
VI	9.5	3.5	3	2.8	·	·	6	2.8	2	2.5	16.5	3.5	25.5	3.9	14.5	2.7	13	2.9	110	35.4	29	·	·	·	5	·	·	4	9	12	10	3	·	·	4
VII	8	2.7	3	1.7	·	·	4	2.5	10.5	3.0	13.5	2.7	32.5	2.4	2.5	3.6	19	2.1	29	16.0	13	·	·	·	5	·	·	3	5	9	4	1	1	·	5
VIII		·	2	1.5	1	3.0	9	3.4	8	3.0	23	3.8	24.5	3.8	6.5	2.7	19	2.8	57	25.2	17	·	·	·	7	·	·	3	7	14	10	1	·	·	6
IX	3	2.0	·	·	8.5	2.4	7.5	2.3	9.5	3.3	16.5	4.0	25.5	3.2	6.5	3.1	13	2.7	76	15.6	17	·	·	·	1	·	·	4	6	15	9	4	3	·	·
X	1.5	1.3	1.5	2.0	10	2.7	19	2.2	5	2.7	11	2.7	14.5	3.7	6.5	2.8	24	2.0	13	5.7	27	·	·	2	·	·	·	4	8	5	3	·	10	·	·
XI	4	2.0	2	4.0	25.5	3.8	20	3.5	3	2.3	6.5	4.2	11	3.2	8	1.7	10	3.0	41	7.5	15	·	·	7	·	·	·	1	23	14	9	·	6	·	·
XII	8	2.1	8.5	2.3	8	2.7	6	3.3	10.5	4.1	10	5.1	24	2.8	5	2.2	13	2.7	11	3.3	16	11	15	26	·	·	·	1	19	9	4	·	3	16	·
Rok	71	2.8	44	2.5	89	2.6	121.5	3.2	97.5	3.2	183.5	4.1	234	3.8	99.5	3.4	155	3.0	696	91.3	14.V	19	40	105	21	11	3	34	151	154	97	16	27	51	21

Wielichowo $H_s = 65\,m$ $h_w = 10\,m$

I	3.5	2.0	6	3.2	1.5	1.3	2	3.2	15	2.8	27.5	3.3	27	3.5	7.5	2.7	3	3.0	30	8.1	25	1	6	17	·	·	·	2	13	12	9	·	-	-	:
II	4.5	3.4	8.5	3.5	11.5	3.3	3	1.0	3	2.3	9.5	4.3	25.5	4.4	11.5	3.4	7	3.4	34	9.8	16	2	8	25	·	2	·	1	16	17	6	·	-	-	1
III	6.5	2.8	17	2.2	11	2.6	14.5	2.6	7	2.4	3	2.5	5.5	3.7	9.5	3.3	19	2.1	24	10.1	5	1	4	27	·	·	·	4	12	10	7	1	-	-	·
IV	7	1.9	11	2.8	4	4.0	5.5	3.5	7.5	2.5	14.5	3.0	11	3.1	11.5	1.9	18	2.2	28	6.7	16	·	·	3	5	·	·	4	11	13	8	·	-	-	2
V	7.5	1.3	2	1.0	·	·	4.5	2.7	2.5	3.4	10.5	2.3	30.5	2.2	8.5	2.8	27	1.6	78	11.4	14	·	·	3	·	·	·	·	19	25	18	2	-	·	5
VI	12.5	2.8	4.5	1.3	0.5	1.0	4	1.9	2.5	2.2	9	3.1	24	2.6	10	1.8	23	1.8	27	10.1	16	·	·	·	7	·	·	3	5	9	5	1	-	·	4
VII	1.5	1.0	5.5	1.7	4	1.5	5.5	1.7	3.5	2.3	16	2.4	20	1.9	2	1.8	35	1.2	54	16.5	11	·	·	·	4	·	·	1	12	13	11	1	-	·	6
VIII	1.5	1.0	4.5	1.9	3	2.0	2.5	1.0	6	1.6	23.5	2.3	26.5	1.9	1.5	1.0	24	1.4	68	20.3	13	·	·	·	5	·	·	2	11	16	10	2	-	·	2
IX	1	2.0	2	1.5	16	1.6	3	3.3	2	2.2	8.5	2.4	27	2.4	6.5	1.8	24	1.6	46	14.2	18	·	·	·	3	1	·	5	5	12	8	2	-	·	·
X	1	2.0	6	1.5	10	1.4	6	1.5	6	2.0	5.5	2.3	15.5	2.0	11	1.6	32	1.2	19	6.5	31	·	·	8	·	·	·	4	10	9	4	·	-	·	1
XI	1.5	2.3	13	3.4	22	3.0	5.5	3.7	9	1.7	12	2.4	6.5	2.8	0.5	3.0	20	2.2	25	10.2	1	·	·	8	·	·	·	2	20	15	7	1	-	·	·
XII	1.5	1.7	19	2.8	7.5	2.6	7	1.9	9	2.5	14.5	3.0	13	2.1	5.5	1.8	16	2.1	21	7.6	15	8	15	26	·	·	·	2	18	11	5	·	-	-	
Rok	49.5	2.0	99	2.2	91	2.0	63	2.3	73	2.3	154	2.8	232	2.7	85.5	2.2	248	2.0	454	20.3	13.VIII	12	33	117	24	3	·	30	152	162	98	10	-	-	21

Łowicz $H_s = 95\,m$ $h_w = 14\,m$

I	5	6.2	4	2.3	3	1.3	1	1.0	12	2.2	34	2.2	24	2.5	7	2.0	3	2.4	15	5.6	25	2	6	18	·	2	·		18	11	4	·	2	-	
II	4.5	3.8	10.5	1.7	6.5	1.2	6.5	1.8	5.5	1.5	18.5	4.7	17.5	3.1	10.5	6.7	4	3.3	31	11.0	12	2	12	23	·	6	3	·	21	15	8	1	3	-	1
III	12.5	3.3	12	1.2	9	1.4	18	1.4	4.5	1.1	6.5	1.4	11	1.6	9.5	3.9	10	1.8	43	13.0	12	·	8	25	·	2	·	2	18	11	7	2	7	-	·
IV	12.5	1.9	11	2.0	3	1.3	7	3.4	10	3.1	21	1.7	5	1.8	12.5	2.6	8	2.0	25	6.3	29	·	·	·	5	·	·	1	13	14	8	·	·	·	1
V	2.5	1.2	5	1.2	8	1.1	7	1.6	6	1.8	12.5	1.4	24.5	2.6	14.5	2.1	13	1.6	166	74.0	14	·	·	3	·	1	·	·	18	22	16	3	4	·	4
VI	17.5	2.9	1.5	1.7	1.5	1.3	5.5	1.5	2	1.0	14	1.8	24.5	2.1	17.5	2.3	6	2.0	77	21.6	23	·	·	·	7	1	·	1	11	13	13	2	·	·	4
VII	11.5	1.3	1.5	1.0	1	1.0	6	1.3	2	2.2	11.5	1.8	35.5	1.9	14	2.0	10	1.5	36	12.4	6	·	·	·	6	-	·	·	9	9	7	1	1	·	4
VIII	1	1.0	1	1.0	2	1.0	7.5	1.2	6	2.0	14.5	1.7	32	1.9	11	2.0	18	1.4	64	21.0	17	·	·	·	7	-	·	1	13	15	10	3	1	·	6
IX	1.5	1.3	0.5	1.0	5.5	1.2	8	1.2	6	1.3	12.5	1.7	31.5	1.7	7.5	1.5	17	1.3	90	22.6	18	·	·	·	3	·	·	1	11	15	11	3	5	·	4
X	3	1.3	6.5	1.2	8	1.1	24	1.2	7	1.1	8.5	1.5	17	1.3	5	1.2	14	1.0	7	3.2	27	·	·	4	·	·	·	1	9	5	2	·	16	·	·
XI	3.5	1.6	7	3.7	17.5	2.2	17	2.1	6.5	1.5	4	1.2	17	1.1	5.5	1.0	12	1.6	48	11.6	20	·	·	6	·	·	·	·	23	12	10	1	4	-	·
XII	4	1.0	14	1.1	3.5	1.3	15.5	1.4	9	2.2	11	2.6	19.5	1.2	6.5	1.2	10	1.3	15	4.1	16	12	15	26	·	·	·	·	22	12	4	·	5	-	·
Rok	79	2.2	74.5	1.6	68.5	1.3	123	1.6	76.5	1.8	168.5	2.0	259	1.9	121	2.4	125	1.8	617	74.0	14.V	16	41	105	28	12	3	7	186	154	100	16	48	-	24

Świder $H_s = 94\,m$ $h_w = 16.9\,m$

I	5	3.8	4	2.2	1	2.0	9.5	2.5	24	2.7	20	3.3	21.5	3.9	5	3.1	3	3.1	26	6.5	25	2	7	22	·	·	·	2	21	14	6	·	2	24	:
II	9	2.8	5	3.1	9.5	2.5	8	2.7	10.5	3.1	8.5	4.0	15	4.5	11.5	4.9	7	3.3	46	10.5	12	5	13	25	·	1	·	·	16	15	11	1	3	28	1
III	13.5	3.2	12	1.8	11.5	2.0	18	2.4	10	2.5	2	3.0	8	3.2	7	3.8	11	2.3	56	11.5	31	7	7	27	·	·	·	4	20	15	9	2	1	27	·
IV	15.5	2.1	8.5	2.3	8	3.1	10.5	3.1	16	2.9	6.5	3.0	7.5	2.4	6.5	3.2	11	2.4	49	12.3	26	·	·	2	6	·	·	1	14	13	6	2	2	1	1
V	10	1.8	1	2.0	5.5	2.1	9	2.1	14	2.0	12.5	2.2	14.5	2.2	8.5	2.6	18	1.7	168	43.0	14	·	·	2	·	·	·	·	19	25	18	5	4	·	5
VI	9.5	2.6	2	2.2	3.5	1.6	6.5	1.8	8	2.7	27	3.7	9.5	2.8	13	3.3	11	2.6	100	36.0	4	·	·	·	8	·	·	3	11	12	11	3	1	·	3
VII	9.5	2.4	1.5	1.3	0.5	2.0	10.5	2.5	15	2.4	24.5	2.4	19.5	2.7	5	3.0	7	2.3	59	15.5	22	·	·	·	6	·	·	2	7	15	11	1	·	·	8
VIII	2	1.0	1	1.0	5.5	2.4	15	2.1	18.5	2.4	24	3.4	11	2.8	2	1.8	14	2.2	70	22.2	4	·	·	·	6	·	·	1	9	19	10	3	1	·	3
IX	2.5	2.0	7	2.1	6.5	2.3	12.5	2.3	11.5	2.4	23	3.2	13	3.0	3	2.2	11	2.3	78	26.7	17	·	·	·	2	·	·	1	11	18	11	2	5	·	2
X	6	1.7	6.5	1.3	12.5	1.6	17.5	2.1	4	2.5	16	2.6	9.5	2.3	6	1.5	15	1.7	7	3.6	27	·	·	6	·	·	·	1	13	7	2	·	13	·	·
XI	4	1.5	11.5	3.6	26.5	3.2	7	2.6	3.5	2.6	12	2.5	6.5	4.8	6	1.4	13	2.3	40	8.6	15	·	·	6	·	·	·	1	23	18	11	·	3	1	·
XII	19	1.9	3	1.7	6.5	2.7	15.5	2.5	9	2.5	15	1.9	13	1.7	3	1.5	9	1.9	18	4.7	16	10	16	27	·	·	·	·	22	11	4	·	4	16	·
Rok	105.5	2.2	63	2.0	97	2.3	139.5	2.4	144	2.6	191	2.9	148.5	2.8	76.5	2.7	130	2.3	717	43.0	14.V	24	43	117	28	1	·	46	186	182	110	19	39	97	23

UWAGA. Kierunki i prędkości wiatru - wg anemografu

Śrem $\varphi = 52°05'$ $\lambda = 17°01'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																		
	P_m	Max	Min	P_{0m}	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.9	-14	9.3	22	-13.2	31	0.2	1.9	0.4	0.7	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.5	7.6	8.0
II	–	–	–	–	1.7	-3.2	7.1	12	-13.2	1	-1.9	0.6	-0.8	-0.7	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.7	6.7	8.0
III	–	–	–	–	3.2	-3.4	13.7	30	-11.2	7,8	-2.4	2.2	-0.3	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.4	6.6	7.4
IV	–	–	–	–	15.8	5.5	28.5	23	-0.4	11	7.5	13.9	9.7	10.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.7	6.1	6.6
V	–	–	–	–	15.4	6.3	22.5	19	-3.1	1	9.2	13.7	10.0	10.7	–	–	–	–	–	–	–	–	–	–	–	–	7.4	8.3	7.8	7.8
VI	–	–	–	–	20.5	9.2	31.5	16	2.5	3	13.3	18.8	14.2	15.1	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.5	5.4	5.6
VII	–	–	–	–	21.5	10.0	32.6	26	5.1	29	13.8	19.9	14.6	15.7	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.2	6.3	6.7
VIII	–	–	–	–	22.2	12.0	30.5	13	7.0	10	14.6	20.5	15.7	16.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	8.0	6.0	6.9
IX	–	–	–	–	18.1	7.9	29.8	4	2.7	25	10.0	16.7	11.4	12.4	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.6	4.9	6.0
X	–	–	–	–	13.3	4.5	24.0	3	-1.7	21	6.0	12.4	7.5	8.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.8	5.4	6.7
XI	–	–	–	–	6.1	2.3	16.5	8	-1.9	21	3.2	5.6	3.9	4.2	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.2	8.3	8.4
XII	–	–	–	–	-1.5	-6.0	6.9	12	-18.1	22	-4.6	-2.6	-4.0	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.3	7.3	8.1
Rok	–	–	–	–	11.6	3.6	32.6	26.VII	-18.1	22.XII	5.7	10.3	6.9	7.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.6	6.5	7.2

Topola - Błonie $\varphi = 52°05'$ $\lambda = 19°11'$

I	–	–	–	–	2.0	-1.8	8.5	22	-13.8	31	-0.6	1.1	-0.3	0.0	5.6	5.7	5.6	5.6	9.2	8.4	9.0	8.9	0.4	1.1	0.6	0.7	7.6	7.3	7.4	7.4
II	–	–	–	–	0.3	-4.2	4.9	20	-13.8	1	-2.9	-0.9	-2.0	-2.0	4.5	5.1	4.8	4.8	8.8	8.8	8.9	8.8	0.6	0.7	0.6	0.6	8.4	8.8	6.5	7.9
III	–	–	–	–	1.8	-3.4	13.3	31	-8.9	15	-2.7	0.8	-1.0	-1.0	4.6	5.4	5.2	5.1	8.9	8.2	9.0	8.7	0.5	1.2	0.6	0.8	7.0	6.5	5.7	6.4
IV	–	–	–	–	15.0	5.9	27.3	23	0.7	1	7.6	13.6	9.5	10.0	9.6	10.0	10.5	10.0	9.0	6.6	8.5	8.0	1.3	7.2	2.0	3.5	6.2	6.0	5.3	5.8
V	–	–	–	–	14.8	6.6	21.3	8	-0.8	3	8.8	13.1	10.3	10.6	10.4	10.5	11.0	10.6	9.1	7.0	8.7	8.3	1.1	5.0	1.8	2.6	7.5	7.2	7.3	7.3
VI	–	–	–	–	19.4	9.3	29.9	16	2.5	3	12.8	17.6	14.0	14.6	12.1	11.3	12.4	11.9	8.0	5.7	7.6	7.1	3.2	10.1	4.2	5.8	5.3	5.7	5.1	5.4
VII	–	–	–	–	21.0	10.5	30.2	26	5.2	29	13.7	19.3	14.7	15.6	14.0	13.3	14.0	13.8	8.8	6.0	8.3	7.7	1.9	9.8	3.1	4.9	5.9	5.8	5.6	5.8
VIII	–	–	–	–	22.1	12.2	31.0	7	7.8	10	14.4	20.5	15.6	16.5	14.9	14.4	15.5	14.9	9.0	6.0	8.7	7.9	1.7	10.5	2.5	4.9	6.1	6.6	4.9	5.9
IX	–	–	–	–	17.4	7.6	27.9	4	1.8	25	9.4	15.5	11.4	11.9	11.1	12.0	11.8	11.6	9.3	7.0	8.6	8.3	1.0	6.4	2.1	3.2	6.2	6.5	4.3	5.7
X	–	–	–	–	13.0	3.9	21.5	4	-3.6	24	5.1	12.0	7.0	7.8	8.9	10.3	9.5	9.6	9.7	7.3	9.2	8.7	0.2	4.3	0.8	1.8	7.7	5.6	5.4	6.2
XI	–	–	–	–	5.7	2.0	14.3	5	-2.9	26	2.8	4.8	3.4	3.6	7.3	7.8	7.5	7.5	9.6	8.9	9.5	9.3	0.3	1.1	0.5	0.6	9.0	8.3	7.9	8.4
XII	–	–	–	–	-2.5	-6.6	4.7	12	-20.3	22	-4.9	-3.6	-4.8	-4.5	4.1	4.3	4.1	4.2	9.0	8.6	8.8	8.8	0.4	0.7	0.5	0.5	8.9	8.0	7.3	8.1
Rok	–	–	–	–	10.8	3.5	31.0	7.VIII	-20.3	22.XII	5.3	9.5	6.5	7.0	8.9	9.2	9.3	9.1	9.0	7.4	8.7	8.4	1.0	4.8	1.6	2.5	7.2	6.9	6.1	6.7

Terespol $\varphi = 52°05'$ $\lambda = 23°37'$

I	99.8.8	102.2.8	97.7.5	101.5.9	1.3	-3.4	6.8	22	-19.3	31	-1.8	0.0	-1.3	-1.1	5.1	5.3	5.1	5.2	9.0	8.4	8.9	8.8	0.5	1.1	0.6	0.7	8.4	7.6	8.1	8.0
II	99.7.6	101.5.9	96.2.6	101.4.9	-1.1	-6.6	3.4	13	-17.4	1	-4.7	-2.1	-3.4	-3.4	4.1	4.3	4.3	4.2	9.1	8.0	8.8	8.6	0.4	1.0	0.6	0.7	9.1	9.2	9.3	9.2
III	99.4.5	101.2.5	97.6.1	101.1.7	0.5	-7.3	8.2	6	-19.0	26	-5.4	-0.8	-3.3	-3.2	4.0	4.4	4.3	4.2	9.0	7.4	8.5	8.3	0.4	1.5	0.7	0.9	7.6	7.1	6.9	7.2
IV	99.7.7	101.3.2	97.5.9	101.4.1	15.8	5.6	26.8	23	-0.4	2,8	7.6	13.9	9.9	10.3	9.6	9.8	9.9	9.8	8.9	6.4	8.0	7.8	1.3	7.6	3.1	4.0	6.5	6.6	4.5	5.9
V	99.5.7	100.4.4	97.1.6	101.2.0	16.1	7.5	24.4	28	-0.9	1	9.9	14.5	11.3	11.8	11.5	11.6	11.9	11.7	9.2	6.9	8.7	8.3	1.0	5.6	1.8	2.8	7.4	8.6	7.4	7.8
VI	100.0.0	100.9.6	98.9.4	101.6.1	19.4	9.6	28.3	16	3.4	6	13.2	17.9	13.9	14.7	12.8	11.9	12.8	12.5	8.3	6.0	7.9	7.4	3.0	9.8	3.7	5.5	6.2	7.4	5.5	6.4
VII	99.7.3	100.7.6	98.4.6	101.3.3	21.4	11.1	30.2	27	7.2	2	14.5	19.8	15.1	16.1	14.5	13.7	14.8	14.3	8.7	6.0	8.5	7.7	2.3	10.0	2.6	5.0	6.0	6.5	4.6	5.7
VIII	99.8.8	100.8.2	98.8.9	101.4.8	22.2	11.9	30.1	13	6.3	27	14.5	20.8	15.9	16.8	15.0	14.8	15.5	15.1	9.0	6.1	8.5	7.9	1.8	10.3	2.9	5.0	5.2	6.5	5.6	5.8
IX	99.9.5	101.5.4	98.2.2	101.5.8	17.6	7.8	27.5	5	2.8	15	9.8	16.1	11.3	12.1	11.6	12.0	12.4	12.0	9.5	6.7	9.2	8.5	0.6	6.9	1.2	2.9	6.7	6.6	4.3	5.9
X	100.5.7	101.9.7	98.8.8	102.2.3	12.4	3.5	19.6	2	-2.9	16	4.7	11.5	6.8	7.4	8.4	9.8	9.3	9.2	9.6	7.2	9.2	8.7	0.3	4.2	0.8	1.8	7.0	6.5	4.5	6.0
XI	100.2.2	101.5.3	98.6.2	101.8.9	7.1	2.1	19.1	1	-4.9	18	3.4	6.0	4.4	4.6	7.4	7.6	7.7	7.6	9.4	8.2	8.9	8.8	0.5	2.2	1.0	1.2	8.6	8.4	8.4	8.5
XII	99.9.6	102.7.7	95.9.7	101.6.9	-2.7	-7.9	2.8	13	-21.9	22	-5.5	-3.8	-5.3	-5.0	4.0	4.2	4.0	4.1	9.0	8.5	8.8	8.8	0.4	0.7	0.4	0.5	9.1	7.5	7.0	7.9
Rok	99.9.0	102.7.7	95.9.7	101.5.6	10.8	2.8	30.2	27.VII	-21.9	22.XII	5.0	9.5	6.3	6.8	9.0	9.1	9.3	9.1	9.1	7.2	8.7	8.3	1.0	5.1	1.6	2.6	7.3	7.4	6.3	7.0

Młochów $\varphi = 52°03'$ $\lambda = 20°47'$

I	–	–	–	–	2.1	-2.4	9.2	22	-18.1	31	-0.8	0.6	-0.5	-0.3	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.3	6.7	7.7
II	–	–	–	–	0.1	-5.5	5.4	12	-15.5	1	-3.8	-1.4	-2.8	-2.7	–	–	–	–	–	–	–	–	–	–	–	–	9.5	9.5	8.1	9.0
III	–	–	–	–	1.7	-5.6	13.2	31	-12.2	21	-4.3	0.2	-2.0	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.0	6.0	7.3
IV	–	–	–	–	15.8	6.0	27.4	22	-0.1	30	7.9	14.2	9.6	10.4	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.2	5.2	7.2
V	–	–	–	–	15.2	7.0	21.4	8	-2.0	1	9.1	13.8	10.3	10.9	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.5	7.0	7.9
VI	–	–	–	–	19.4	9.9	29.0	16	5.0	7,8	13.2	17.6	13.6	14.5	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.7	7.1	6.7
VII	–	–	–	–	21.4	11.1	30.3	26	6.9	31	14.5	19.2	15.0	15.9	–	–	–	–	–	–	–	–	–	–	–	–	5.7	7.2	6.5	6.5
VIII	–	–	–	–	22.0	12.8	30.7	7	8.5	10	15.1	20.0	15.5	16.5	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.1	5.0	6.9
IX	–	–	–	–	17.4	8.2	27.7	4	2.7	27	9.7	15.7	11.6	12.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.6	4.6	6.4
X	–	–	–	–	12.6	4.5	20.1	2	-1.8	16	5.7	11.3	7.3	7.9	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.9	4.2	6.9
XI	–	–	–	–	5.8	1.6	14.2	1	-2.0	18	2.9	4.7	3.5	3.6	–	–	–	–	–	–	–	–	–	–	–	–	9.6	9.5	8.4	9.2
XII	–	–	–	–	-2.1	-7.0	4.4	12	-20.6	22	-5.5	-4.0	-4.7	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	8.4	9.1	7.9	8.5
Rok	–	–	–	–	11.0	3.4	30.7	7.VIII	-20.6	22.XII	5.3	9.3	6.4	6.8	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.2	6.4	7.5

Śrem $H_s = 85 m$ $h_w = 10 m$ 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R (R)
I	6	3.3	3	1.3		·	1	3.5	26	2.6	28.5	2.9	15.5	4.2	9	2.9	4	2.9	20	6.6	25	2	5	16	·	·	·	1	17	12	5	·	1	–	·
II	6	2.9	16	2.0	1.5	4.0	2	1.0	8	2.9	14.5	4.1	17.5	4.9	12.5	3.5	6	3.2	31	10.2	12	1	9	24	·	4	·	1	16	13	6	1	·	–	·
III	12	3.7	12.5	2.4	10.5	2.5	9.5	2.5	8	2.1	2.5	3.2	9	4.7	8	3.4	21	2.3	31	13.2	5	2	3	26	·	·	·	1	14	11	8	1	4	–	·
IV	10	2.4	12.5	4.2	3	4.7	4.5	3.3	9	2.2	13	4.2	11.5	3.3	12.5	3.3	14	2.9	15	3.1	29	·	·	1	4	·	·	3	10	11	7	·	1	–	1
V	4	2.8	6.5	2.2	2.5	1.6	5.5	2.5	9	2.6	16	3.0	25.5	4.3	8	2.1	16	2.6	85	26.5	14	·	·	2	·	·	·	·	16	25	20	1	1	·	5
VI	13	3.7	4	2.0	1	1.0	5.5	2.4	3	2.7	5.5	4.4	21	4.6	17	2.9	20	2.7	31	12.2	16	·	·	·	7	·	·	1	6	8	6	1	·	·	2
VII	9.5	2.0	2.5	2.4	·	·	·	·	7.5	2.1	14.5	3.3	21.5	3.6	6.5	3.0	31	2.0	44	13.5	16	·	·	·	6	·	·	1	11	14	13	1	2	·	4
VIII	4	1.5	2	3.5	1	3.0	3	2.0	7	2.3	24.5	5.2	20	3.8	11.5	2.3	20	2.9	64	24.6	13	·	·	·	6	·	·	1	15	16	11	2	·	·	2
IX	4	1.2	11	2.9	3	3.3	2	1.5	8.5	2.9	9	4.2	26	4.2	9.5	1.8	17	2.7	38	13.7	18	·	·		3	·	·	5	8	12	7	1	5	·	2
X	7.5	2.3	5	2.4	7	2.4	2	1.0	9	2.6	7	2.8	9	4.6	15.5	2.0	31	1.8	29	10.8	31	·	·	4	·	1	·	3	12	8	4	1	10	·	·
XI	2.5	2.0	15	3.7	17	3.9	2	2.5	6	1.5	10	3.7	11	4.5	9.5	2.1	17	2.8	39	13.8	1	·	·	8	·	·	·	1	21	12	8	1	7	–	·
XII	11	2.3	16	3.0	2	3.2	2	2.0	12.5	3.6	12.5	4.6	13.5	3.1	6.5	2.6	17	2.6	16	6.3	15	9	13	24	·	·	·	·	21	8	5	·	4	–	·
Rok	89.5	2.5	106	2.7	48.5	2.2	39	2.0	113.5	2.5	157.5	3.8	201	4.2	126	2.7	214	2.6	443	26.5	14.V	14	30	105	26	5	·	18	167	150	100	10	35	–	16

Topola-Błonie $H_s = 109 m$ $h_w = 12 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R (R)
I	2	9.2	5.5	5.1	1	2.5	·	·	18	4.0	33.5	4.6	21.5	4.9	8.5	5.5	3	4.6	26	10.5	25	2	5	17	·	4		2	15	14	6	1	4	·	:
II	2	4.0	11.5	4.8	8.5	5.1	1.5	2.7	11.5	4.3	15	5.8	20.5	5.9	8.5	6.1	5	5.0	24	8.2	12	2	12	25	·	6	1	·	16	14	7	·	2	5	·
III	8	5.8	15.5	4.1	14	3.2	8.5	2.5	6.5	1.7	5	3.2	7.5	4.3	9	6.1	19	3.1	49	14.5	5	·	8	26	·	3	·	3	11	11	7	2	6	8	·
IV	11	3.1	6.5	6.4	6	2.5	3.5	5.6	11	4.5	23	4.0	5	2.3	9	4.4	15	3.4	31	7.1	29	·	·	·	4	2	·	5	11	15	8	·	·	·	1
V	2.5	1.6	5.5	2.7	3.5	1.3	5.5	1.8	9	3.1	23	2.9	16.5	4.4	12.5	5.4	15	2.9	148	59.6	14	·	·	3	·	3	·	·	11	25	19	3	3	·	5
VI	12.5	5.6	3	4.7	4	1.8	3.5	1.0	6	1.6	11	3.6	24	4.5	13	4.1	13	3.4	52	12.9	30	·	·	·	6	1	·	4	9	13	10	2	·	·	4
VII	6.5	2.2	9.5	1.8	3.5	1.6	4	1.4	4	1.8	27	2.7	21	2.9	6.5	3.6	11	2.2	46	13.1	3	·	·	·	6	·	·	1	5	14	9	1	1	·	5
VIII	2.5	2.2	2.5	1.6	2.5	2.4	3	2.7	5.5	3.0	31	3.7	19	4.8	6	4.5	21	2.9	77	35.0	17	·	·	·	6	1	·	2	8	16	11	2	·	·	4
IX	3.5	2.4	3.5	2.6	11	2.0	2.5	3.2	6.5	2.5	24.5	3.2	19.5	3.8	7	4.2	12	2.7	71	22.8	18	·	·	·	1	·	·	5	8	14	8	3	5	·	2
X	1.5	1.0	8	1.3	18.5	2.1	5.5	2.2	6.5	2.4	11	2.4	14	3.9	6	3.5	22	1.9	20	4.8	27	·	·	5	·	·	·	4	12	13	5	·	18	·	·
XI	4.5	1.7	7.5	6.6	29	2.8	6.5	3.8	3.5	2.4	14	2.4	5.5	4.1	6.5	1.9	13	2.7	37	7.7	20	·	·	8	·	2	·	1	21	13	10	·	9	·	·
XII	6	2.7	14	3.6	9	2.0	8.5	2.7	10	5.5	18	4.9	14	3.0	6.5	3.2	7	3.4	13	5.0	16	11	15	27	·	4	·	1	19	10	4	·	5	16	·
Rok	62.5	3.5	92.5	3.8	110.5	2.4	52.5	2.5	98	3.1	236	3.6	188	4.1	99	4.4	156	3.2	594	59.6	14.V	15	40	111	23	26	1	28	146	172	104	14	53	29	21

Terespol $H_s = 133 m$ $H_b = 135,0 m$ $h_w = 12,5 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R (R)
I	5	4.0	7	3.1	·	·	1	2.0	21	2.8	26	3.1	18.5	5.1	14.5	3.0	·	3.5	26	8.9	25	2	7	27	·	·	·	2	20	13	8	·	2	19	·
II	15	4.5	10	4.3	8.5	3.5	4.5	3.6	7.5	4.5	12	5.1	11	5.3	15.5	4.8	·	4.6	33	9.6	12	6	15	28	·	4	·	·	25	18	10	·	4	28	·
III	21.5	3.5	23.5	2.4	8	2.4	14.5	3.6	3.5	2.6	2	4.5	8.5	3.6	8.5	2.9	3	3.1	42	10.1	23	9	13	29	·	1	1	2	16	12	10	1	3	24	·
IV	12.5	2.8	22	3.0	6.5	2.8	14.5	2.8	8.5	3.3	6.5	3.3	4	2.5	12.5	3.4	3	2.9	51	9.2	7	·	·	3	5	·	·	4	7	11	11	·	1	1	2
V	22	2.3	2.5	1.6	2	3.8	4	3.1	7.5	1.1	9.5	2.7	18.5	3.3	24	2.8	3	2.6	91	22.7	14	·	·	1	·	·	·	·	16	17	12	4	1	·	6
VI	25	3.9	4.5	3.1	0.5	2.0	2.5	1.6	3	1.8	6	2.1	17	3.4	24.5	2.2	7	2.7	86	15.2	4	·	·	·	6	1	·	4	11	13	11	4	·	·	4
VII	15	3.0	1	3.0	1.5	2.0	0.5	2.0	7.5	2.8	9.5	2.2	16.5	2.5	31.5	2.7	10	2.4	58	9.0	14	·	·	·	4	·	·	2	6	18	15	·	1	·	4
VIII	4	2.3	1	5.0	2	1.8	3.5	2.6	6.5	3.1	12.5	1.9	35	2.9	18.5	3.7	10	2.6	48	9.9	15	·	·	·	6	·	·	2	7	13	10	·	2	·	4
IX	2	3.0	9.5	2.0	2.5	2.4	4	1.6	9	2.7	12	3.3	25	2.9	20	2.7	6	2.5	55	18.3	18	·	·	·	2	·	·	4	7	14	11	2	2	·	2
X	13.5	1.6	10	1.7	5.5	2.0	11	1.8	·	·	7	2.1	13	2.9	14	2.9	19	1.7	4	4.7	19	·	·	5	·	·	·	3	11	6	2	·	10	·	·
XI	10.5	2.8	6.5	5.0	22.5	4.7	24	3.9	3	3.8	5	4.1	6.5	3.6	10	3.3	2	3.9	54	9.3	30	·	·	8	·	·	·	3	23	17	13	·	8	1	·
XII	15	2.9	13.5	2.7	3	2.0	7.5	2.6	12.5	4.1	6.5	4.8	15	2.7	9	2.6	11	2.7	24	11.1	16	10	19	30	·	·	·	1	18	12	6	1	1	22	·
Rok	161	3.0	111	3.1	62.5	2.4	91.5	2.6	89.5	2.7	114.5	3.3	188.5	3.4	202.5	3.1	74	2.9	572	22.7	14.V	27	54	131	23	6	1	27	167	164	119	12	35	95	22

Młochów $H_s = 141 m$ $h_w = 12,5 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R (R)
I	1.5	9.0	5.5	6.2	2	3.5	5.5	3.0	19.5	4.4	35.5	5.8	18.5	7.6	3	7.2	2	5.6	18	6.1	25	2	8	19	·	4	1	2	18	14	5	·	1	8	:
II	4	4.0	7	4.6	9.5	3.4	8	2.4	10	2.8	19.5	5.1	11.5	6.1	9.5	7.5	5	4.4	38	12.4	12	5	13	24	·	4	·	·	22	16	8	1	2	15	2
III	9	7.7	9.5	3.8	12	3.0	17	2.5	10	3.3	8	3.3	7.5	6.0	8	6.8	12	3.7	40	9.6	31	5	11	27	·	3	·	3	16	13	8	·	·	19	·
IV	9	3.7	9.5	4.6	5.5	4.6	11.5	3.4	10	4.6	14.5	4.7	5.5	5.7	10.5	4.8	14	3.7	36	10.8	29	·	·	1	4	1	·	1	9	13	7	1	·	1	1
V	3.5	2.6	4.5	2.6	5	2.6	9.5	2.9	10.5	3.1	21	3.9	23	5.3	8	5.2	8	3.6	188	60.9	14	·	·	1	·	2	·	·	19	25	20	5	2	·	3
VI	5.5	6.3	5	3.7	5.5	1.9	5.5	2.7	8.5	2.5	15.5	4.6	25	5.2	11.5	5.2	8	4.0	89	30.5	4	·	·	·	5	3	·	2	12	11	9	3	·	·	3
VII	5	4.1	6	2.0	3	1.7	4	1.8	10	3.4	28	3.5	24.5	4.3	10.5	4.3	2	3.5	30	14.6	13	·	·	·	5	·	·	·	10	12	6	1	·	·	5
VIII	1.5	2.3	2.5	3.0	2.5	2.0	6.5	2.9	11.5	3.4	29.5	4.7	26	5.3	4	3.9	9	3.9	64	25.0	15	·	·	·	6	·	·	·	10	12	11	2	1	·	8
IX	3	4.8	0.5	5.0	9	2.6	6	2.8	14.5	3.8	23.5	4.3	16	4.8	8.5	6.4	9	3.8	90	22.0	17	·	·	·	1	2	·	1	7	20	13	3	4	·	4
X	2	4.0	3.5	2.3	7	2.4	20.5	3.0	11	3.6	17.5	3.9	13	4.3	5.5	3.6	13	3.0	14	6.0	27	·	·	3	·	1	·	2	10	19	3	·	10	·	·
XI	1.5	1.3	5	5.0	26.5	4.6	15	3.1	6	2.9	8.5	4.6	7.5	4.7	11	3.2	9	3.6	44	7.7	15,19	·	·	10	·	·	·	·	25	15	10	·	6	1	·
XII	2.5	3.2	13	4.3	9.5	2.2	7.5	2.7	16	4.2	21	4.9	12	4.5	4.5	3.4	7	3.7	14	5.2	16	12	16	28	·	1	·	·	25	9	4	.	4	16	·
Rok	48	4.4	71.5	3.9	97	2.9	116.5	2.8	137.5	3.5	242	4.4	190	5.3	94.5	5.1	98	3.9	665	60.9	14.V	24	48	113	21	21	1	11	183	179	104	16	30	60	26

Trzebiechów $\varphi = 52°01'$ $\lambda = 15°44'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA t												ŚREDNIA PREŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																					
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	4.3	-0.6	10.7	22	-12.5	31	1.1	3.2	1.8	2.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	2.6	–	8.5	12, 13	–	–	-1.1	1.1	0.0	0.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	4.5	-2.7	15.2	30	-7.4	8	-2.0	3.3	0.8	0.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	16.3	5.1	29.0	23	-1.1	11	7.0	14.5	10.6	10.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15.6	6.3	22.7	19	-1.3	1	9.0	13.9	10.8	11.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	21.2	9.2	32.5	16	2.1	3	13.1	19.6	14.6	15.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.8	10.7	33.0	26	6.6	29	14.5	19.7	15.7	16.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	22.0	12.1	30.4	12	7.6	10	14.9	20.4	16.6	17.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	18.6	7.6	30.0	4	0.6	15	9.8	17.1	12.4	12.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	14.0	4.4	23.7	2,3	-2.2	21	6.6	13.0	8.4	9.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.6	2.2	17.0	8	-3.5	21	3.3	5.8	4.4	4.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-0.6	-5.3	8.0	12	-16.5	22	-3.9	-1.8	-3.2	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	12.2	–	33.0	26.VII	-16.5	22.XII	6.0	10.8	7.7	8.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Biała Podlaska $\varphi = 52°01'$ $\lambda = 23°08'$

I	–	–	–	–	1.4	-3.4	6.4	22	-19.2	31	-1.7	0.1	-1.1	-1.0	5.0	5.0	5.0	5.0	88	79	85	84	0.6	1.3	0.9	0.9	8.5	7.7	7.9	8.0
II	–	–	–	–	-0.8	-6.9	3.5	13	-17.5	1	-4.8	-2.1	-3.4	-3.4	4.0	4.3	4.3	4.2	89	80	88	86	0.5	1.0	0.6	0.7	9.5	9.0	8.1	8.8
III	–	–	–	–	0.8	-7.6	7.8	31	-20.0	26	-5.5	-0.4	-3.6	-3.3	3.9	4.4	4.2	4.2	87	72	85	81	0.5	1.7	0.7	1.0	8.1	7.4	6.0	7.2
IV	–	–	–	–	15.8	5.0	27.4	22	-0.6	30	7.7	14.5	9.6	10.4	9.3	10.3	10.1	9.9	86	63	82	77	1.6	7.8	2.4	3.9	7.3	6.8	4.5	6.2
V	–	–	–	–	16.1	7.0	23.8	28	-1.4	1,3	9.7	14.4	10.9	11.5	11.2	11.6	11.9	11.6	90	70	89	83	1.2	5.4	1.4	2.7	7.7	8.6	6.3	7.5
VI	–	–	–	–	19.6	9.1	29.1	16	3.4	7	13.3	17.9	13.6	14.6	12.7	12.4	13.3	12.8	83	62	84	76	3.1	9.3	2.9	5.1	5.9	7.5	5.5	6.3
VII	–	–	–	–	21.4	11.0	29.4	27	6.6	31	14.3	19.8	14.9	16.0	13.9	13.8	14.1	13.9	84	60	83	76	2.6	10.0	3.0	5.2	5.8	7.0	4.2	5.7
VIII	–	–	–	–	22.4	11.9	31.0	13	6.1	27	14.6	20.9	16.0	16.9	14.7	15.1	15.3	15.0	87	61	83	77	2.2	10.3	3.2	5.2	6.2	7.0	4.6	5.9
IX	–	–	–	–	17.6	7.7	27.9	5	2.8	25	9.7	16.4	11.3	12.2	10.9	11.5	11.8	11.4	89	62	88	80	1.4	7.7	1.8	3.6	6.3	7.0	4.1	5.8
X	–	–	–	–	12.5	2.6	19.7	1	-3.9	16	4.7	11.6	6.3	7.2	8.2	9.8	8.8	8.9	94	71	90	85	0.6	4.4	1.0	2.0	7.9	6.7	4.2	6.3
XI	–	–	–	–	6.8	1.9	19.4	1	-3.1	18	3.1	5.7	4.1	4.2	7.2	7.5	7.5	7.4	92	82	88	87	0.6	2.2	1.0	1.3	8.7	8.4	8.5	8.5
XII	–	–	–	–	-2.5	-7.9	3.2	13	-21.0	21,22	-5.7	-3.7	-5.5	-5.1	3.9	4.0	3.9	3.9	88	81	88	86	0.4	0.9	0.5	0.6	8.9	8.0	6.2	7.7
Rok	–	–	–	–	10.9	2.5	31.0	13.VIII	-21.0	21,22.XII	5.0	9.6	6.1	6.7	8.7	9.1	9.2	9.0	88	70	86	81	1.3	5.2	1.6	2.7	7.6	7.6	5.8	7.0

Skierniewice $\varphi = 51°58'$ $\lambda = 20°10'$

I	1000.1	1023.9	975.1	1016.4	2.6	-2.0	8.8	22	-17.3	31	-0.4	1.1	-0.1	0.1	5.3	5.4	5.3	5.3	88	80	84	84	0.8	1.4	1.0	1.1	8.6	7.5	7.1	7.7
II	999.9	1019.7	988.0	1016.3	0.5	-4.6	5.7	12	-15.3	1	-3.2	-0.8	-2.0	-2.0	4.3	4.8	4.8	4.6	86	82	87	85	0.7	1.3	0.7	0.9	9.2	8.4	7.9	8.5
III	995.8	1012.6	974.9	1012.2	4.7	-4.9	14.0	31	-12.7	25,26	-3.8	0.5	-1.4	-1.5	4.2	5.2	4.9	4.8	87	81	86	85	0.6	1.3	0.8	0.9	7.3	7.5	6.3	7.0
IV	998.6	1012.8	973.1	1014.3	15.7	6.0	27.0	23	0.4	30	7.8	14.4	10.0	10.6	8.9	9.3	9.9	9.4	82	57	78	72	2.1	8.7	3.0	4.6	6.3	5.9	5.9	6.0
V	997.4	1004.5	978.7	1013.1	15.0	7.0	22.4	8	-1.8	1	9.5	13.7	10.4	11.0	10.3	10.1	10.8	10.4	85	64	83	77	1.9	6.1	2.1	3.4	7.5	7.8	7.8	7.7
VI	1002.4	1012.7	992.7	1017.9	19.4	10.0	29.2	16,23	5.4	3,8	13.1	17.8	14.0	14.7	11.8	10.2	12.6	11.5	76	51	77	68	3.8	11.0	3.9	6.2	6.5	5.9	5.9	6.1
VII	999.1	1010.4	985.5	1014.5	21.4	11.2	30.8	26	7.0	30	14.4	19.6	15.6	16.3	13.3	13.1	13.6	13.3	80	57	76	71	3.3	10.4	4.4	6.0	5.7	6.2	6.3	6.1
VIII	1000.2	1008.8	989.7	1015.6	22.3	12.5	32.2	7	7.5	10	14.9	20.4	15.7	16.7	14.7	14.6	15.6	15.0	86	63	87	79	2.4	10.2	2.5	5.0	7.2	7.5	5.5	6.7
IX	1000.8	1015.3	983.6	1016.4	17.5	8.0	28.3	4	2.5	25	9.7	15.8	11.5	12.1	10.8	11.7	12.1	11.5	88	66	87	80	1.5	7.1	1.8	3.5	6.6	6.5	5.8	6.3
X	1007.0	1021.3	994.8	1023.0	13.0	4.1	19.7	2	-2.4	16	5.8	12.0	7.3	8.1	8.6	10.2	9.2	9.3	92	72	88	84	0.8	4.2	1.2	2.1	8.7	6.1	5.7	6.8
XI	1001.9	1017.4	982.1	1018.0	5.8	2.3	12.5	8	-1.5	18	3.4	5.0	3.9	4.0	7.0	7.4	7.2	7.2	88	83	87	86	0.9	1.6	1.1	1.2	9.5	8.9	8.7	9.0
XII	1000.8	1029.3	957.2	1017.3	-2.1	-7.1	4.5	12	-21.7	22	-5.0	-3.5	-4.4	-4.3	3.7	3.9	3.9	3.8	77	76	78	77	0.9	1.2	0.9	1.0	9.5	8.3	8.8	8.9
Rok	1000.3	1029.3	957.2	1016.3	11.1	3.5	32.2	7.VIII	-21.7	22.XII	5.5	9.7	6.7	7.2	8.6	8.8	9.2	8.9	85	69	83	79	1.6	5.4	2.0	3.0	7.7	7.2	6.8	7.2

Zielona Góra $\varphi = 51°56'$ $\lambda = 15°30'$

I	994.5	1018.2	968.1	1016.2	3.3	-1.2	9.6	22	-13.0	31	0.5	2.4	0.9	1.2	5.6	5.5	5.5	5.5	85	74	82	80	1.0	2.0	1.3	1.4	7.7	8.3	7.8	7.9
II	995.5	1016.1	965.2	1017.5	4.9	-3.2	7.5	12	-13.4	1	-1.6	0.6	-0.6	-0.6	4.9	5.2	4.9	5.0	87	81	82	83	0.7	1.3	1.1	1.0	9.0	9.1	7.8	8.6
III	990.1	1007.7	965.0	1011.9	3.6	-3.0	14.8	30	-7.5	14	-2.1	2.5	-0.1	0.0	4.7	4.8	4.7	4.7	87	65	74	75	0.7	2.7	1.6	1.7	7.5	7.8	6.2	7.2
IV	992.9	1005.7	966.8	1014.1	15.3	5.8	27.6	25	0.5	30	7.3	13.5	9.9	10.2	8.4	8.3	8.7	8.5	82	55	72	70	2.3	8.9	4.4	5.2	7.5	7.4	6.7	7.2
V	992.5	998.4	983.8	1013.5	14.6	7.0	21.9	19	-0.4	1	8.7	13.2	10.1	10.5	9.8	9.1	9.8	9.6	86	60	78	75	1.6	6.5	2.8	3.6	7.8	8.5	7.8	8.0
VI	998.6	1010.1	988.4	1019.4	20.1	10.2	31.0	16	2.5	6	12.9	18.5	14.7	15.2	11.1	11.0	11.5	11.2	73	51	68	64	4.4	11.8	6.0	7.4	5.7	7.3	6.3	6.4
VII	994.4	1005.1	977.4	1015.1	20.5	11.9	31.8	26	7.2	4	14.0	19.0	15.3	15.9	13.3	12.8	13.6	13.2	83	59	78	73	3.0	10.1	4.2	5.8	6.6	7.6	7.0	7.1
VIII	995.2	1003.8	982.9	1015.9	21.1	12.7	29.0	12	9.6	9,31	14.2	19.4	15.9	16.4	13.9	13.9	13.9	13.9	85	63	77	75	2.5	9.3	4.4	5.4	7.3	8.2	6.4	7.3
IX	995.7	1007.3	977.9	1016.6	17.4	9.0	28.7	4	5.8	15	10.0	15.9	12.5	12.7	10.9	11.6	11.2	11.2	88	65	78	77	1.6	7.2	3.6	4.1	7.1	6.7	4.4	6.1
X	1001.3	1014.3	988.0	1022.6	13.1	6.3	23.2	2	1.4	23	7.0	12.0	8.9	9.2	9.4	10.2	9.7	9.8	92	71	84	82	0.8	4.4	2.0	2.4	7.4	6.1	4.7	6.1
XI	995.0	1013.6	977.4	1016.6	5.7	1.9	16.3	8	-3.1	21	2.8	5.1	3.5	3.7	7.2	7.5	7.2	7.3	94	84	90	89	0.5	1.7	0.9	1.0	8.5	8.8	8.2	8.5
XII	995.2	1023.5	950.6	1017.5	-1.7	-5.9	6.5	12	-17.6	22	-4.3	-2.5	-3.9	-3.6	4.3	4.4	4.2	4.3	88	81	86	85	0.6	1.0	0.7	0.8	7.8	7.7	6.2	7.2
Rok	995.1	1023.5	950.6	1016.4	11.2	4.3	31.8	26.VIII	-17.6	22.XII	5.8	10.0	7.3	7.6	8.6	8.7	8.7	8.7	86	67	79	77	1.6	5.6	2.8	3.3	7.5	7.8	6.6	7.3

Trzebiechów $H_s = 55 m$ $h_w = 10,4 m$ 1962

MIESIĄC	ROZKŁAD WIATRU (D, v m/s) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◔	●	Opad R R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	℞
I	25	48	35	24	1	10	·	·	5	41	215	36	375	50	8	51	14	37	29	117	24	1	5	13	·	4	·	–	–	13	10	1	–	–	–
II	3	52	6	29	115	28	1	10	05	50	8	36	21	68	19	82	14	47	41	108	16	–	7	–	·	7	3	–	–	11	9	1	–	–	–
III	4	32	3	23	95	20	85	31	6	13	8	27	95	34	135	47	31	20	26	60	5,12	·	1	26	·	1	·	–	–	9	6	·	–	–	–
IV	6	12	105	20	5	32	45	33	5	24	11	40	15	38	15	47	18	27	26	84	29	·	·	1	5	1	·	–	–	11	5	·	–	·	–
V	4	15	2	10	1	30	4	11	2	12	4	28	335	35	165	40	26	23	114	178	26	·	·	2	·	1	·	–	–	22	18	4	–	·	–
VI	115	30	3	10	·	·	25	12	35	23	3	25	295	37	20	27	17	25	33	236	16	·	·	·	8	1	·	–	–	8	4	1	–	·	–
VII	95	19	45	18	2	12	35	10	1	10	75	32	295	30	175	27	18	21	39	90	1	·	·	·	9	1	·	–	–	10	8	·	–	·	–
VIII	15	27	15	20	15	20	05	20	25	14	7	42	41	44	165	39	21	31	92	363	13	·	·	·	7	2	1	–	–	17	13	3	–	·	–
IX	1	20	·	·	1	15	13	23	2	10	55	31	22	35	215	33	24	22	39	136	18	·	·	·	3	·	·	–	–	11	8	1	–	·	–
X	55	17	2	12	1	10	15	14	55	11	75	16	145	31	13	19	29	13	14	95	31	·	·	6	·	·	·	–	–	7	2	·	–	·	–
XI	3	15	05	40	17	31	125	26	15	13	6	20	15	30	55	41	29	19	19	68	1	·	·	7	·	·	·	–	–	10	6	·	–	–	–
XII	2	25	35	33	14	30	55	20	15	17	14	38	23	34	75	35	22	25	26	95	15	8	13	24	·	1	·	–	–	9	7	·	–	–	–
Rok	535	26	40	20	645	20	705	18	36	20	103	31	291	39	1735	41	263	26	498	363	13.VIII	–	26	–	32	19	4	–	–	138	96	11	–	–	–

Biała Podlaska $H_s = 145 m$ $h_w = 12 m$

I	3	47	6	28	05	30	2	30	16	31	27	36	20	47	55	31	13	32	30	80	25	2	7	26	·	·	·	1	18	14	5	·	2	25	·
II	6	37	6	37	85	31	5	34	75	76	7	65	165	71	115	69	16	46	54	174	12	7	15	28	·	6	3	·	21	17	10	1	2	28	1
III	75	47	65	28	65	28	16	45	15	33	25	60	6	58	105	37	36	26	60	145	16	9	11	29	·	5	3	1	16	13	10	2	3	27	·
IV	2	18	10	40	5	50	95	42	11	37	55	32	5	33	10	47	32	26	74	140	9	·	·	3	5	1	1	3	9	10	8	5	2	1	2
V	55	18	1	30	35	36	25	42	7	31	45	40	12	55	13	37	44	20	119	256	14	·	·	2	·	2	1	·	12	21	16	4	·	·	4
VI	175	49	2	37	·	·	4	28	25	24	65	35	205	45	12	33	25	30	92	188	4	·	·	·	7	4	3	2	10	13	11	4	·	·	1
VII	4	20	05	30	·	·	2	25	85	28	105	25	23	40	135	31	31	21	82	246	13	·	·	·	4	4	2		3	17	11	3	·	·	5
VIII	05	30	05	20	3	27	35	34	65	31	205	34	215	50	7	59	30	28	44	167	15	·	·	·	7	5	4	2	8	13	10	1	1	·	2
IX	3	20	5	18	2	13	5	30	11	28	165	38	20	41	75	36	20	26	72	219	18	·	·	·	2	3	2	6	10	15	11	2	4	·	2
X	3	20	3	23	4	26	9	26	15	23	95	36	11	42	8	34	44	17	4	17	19		·	8	·	·	·	4	11	5	2	·	11	·	·
XI	65	22	55	68	22	60	185	53	3	38	8	42	75	35	10	25	9	42	55	76	23		·	6	·	3		2	24	17	14	·	5	2	·
XII	14	26	75	27	3	13	65	27	125	50	12	46	145	33	6	34	17	28	22	87	16	10	16	30	·	·	·	1	19	10	5	·	2	16	·
Rok	725	30	535	32	58	26	835	35	885	36	130	41	1775	46	1145	39	317	28	708	256	14 V	28	49	132	25	33	19	22	161	165	113	22	32	99	17

Skierniewice $H_s = 128 m$ $H_b = 129,5 m$ $h_w = 8,3 m$

I	35	64	35	39	15	30	05	30	19	47	35	46	23	51	6	48	1	47	19	74	25	2	5	18		4	1	1	19	10	5	·	·	9	·
II	6	51	6	48	10	56	4	44	105	44	14	69	205	67	12	71	1	59	25	85	12	3	11	24	·	7	2		21	14	9		·	16	·
III	65	45	135	31	75	45	14	44	115	20	7	26	165	38	135	43	3	35	42	407	31	3	11	25	·	2	·	3	16	13	9	1	3	17	·
IV	75	33	65	31	9	51	9	59	12	36	12	34	13	38	17	52	4	41	35	765	29	·	·	·	3	2	·	2	4	13	9	1		1	1
V	45	28	7	29	65	23	5	27	12	28	18	33	22	45	17	46	1	36	166	793	14	·	·	2	·	3	·	·	18	22	15	5	·	·	3
VI	95	38	55	45	3	25	55	34	55	32	115	42	29	39	185	34	2	37	57	190	4	·	·	·	6	1	·	4	8	12	8	2	·	·	3
VII	8	23	45	18	25	14	35	17	8	31	165	37	31	29	15	30	3	27	28	76	3	·	·	·	5	·	·	2	7	9	6	·	–	·	2
VIII	3	28	2	15	15	23	65	21	12	22	215	39	315	40	9	37	6	32	51	471	47	·	·	·	6	·		·	8	11	11	1	–	·	5
IX	25	22	15	47	75	20	45	27	8	33	22	37	235	42	75	39	13	30	59	191	18	·	·	·	1	·	·	3	9	13	10	2	–	·	2
X	3	22	55	23	9	26	115	31	95	22	13	27	175	36	7	33	17	24	10	56	27	·	·	3	·	·	·	1	13	5	3	·	–	·	·
XI	3	27	55	45	24	55	14	40	4	35	8	22	115	36	13	18	7	35	33	65	20	·	·	7	·	2	-	·	25	12	8	·	–	–	·
XII	8	21	125	44	55	35	6	30	155	51	115	53	21	29	4	22	9	34	14	40	16	12	15	25	·		·	·	23	10	6	·	–	–	·
Rok	65	34	735	32	875	34	84	34	1275	33	190	39	260	41	1405	39	67	36	539	793	14 V	20	42	104	21	21	3	16	171	144	99	12	–	–	16

Zielona Góra $H_s = 180 m$ $H_b = 173,8 m$ $h_w = 17 m$ wiatromierz Wilda, 12 m anemometr

I	25	36	5	36	15	30	1	30	175	47	35	53	23	52	75	45	·	49	43	141	24	2	6	13	·	2	·	1	19	17	11	1	10	11	·
II	3	32	45	31	13	37	25	30	3	37	24	48	215	59	125	49	·	47	42	111	12	1	10	22	·	3	·	·	20	18	12	2	2	18	
III	15	47	8	31	14	28	16	40	85	35	12	35	205	33	105	34	2	33	37	76	12	·	5	27	·	·	·	3	14	15	8	·	7	13	
IV	4	32	55	32	105	43	10	35	8	36	20	48	195	44	125	40	·	41	35	59	16	·	·	·	4	3	·	2	15	16	10	·	3	·	2
V	55	20	15	17	15	27	65	30	9	29	26	36	31	38	10	32	2	33	124	281	26	·	·	1	·	·	·	·	17	23	17	4	3	·	4
VI	10	34	3	25	45	24	2	28	65	32	155	40	295	41	18	30	1	35	63	490	16	·	·	·	7	·	·	2	8	10	5	1	·	·	2
VII	75	24	35	30	5	25	55	25	35	30	235	40	30	34	95	25	5	31	33	64	2	·	·	·	5	·	·	·	13	14	12	·	1	·	5
VIII	2	25	2	25	35	40	45	22	105	30	29	50	33	46	65	33	2	41	122	376	13	·	·	·	5	1	·	1	13	18	15	4	2	·	5
IX	15	37	05	50	5	43	175	34	75	30	185	43	315	37	8	28	·	37	57	126	23	·	·	·	3	1	·	5	10	16	11	2	6	·	1
X	45	24	05	30	6	28	19	28	145	30	18	31	15	32	135	24	2	28	14	92	31	·	·	·	·	·	·	3	11	12	2	·	15	·	·
XI	05	30	45	47	215	38	15	40	7	21	155	35	165	33	75	23	2	34	23	92	1	·	2	7	·	·	·	·	20	20	5	·	16	3	·
XII	5	24	5	30	13	38	2	52	75	40	295	40	185	39	35	30	9	35	28	104	15	10	16	26	·	2	·	3	15	12	6	1	10	17	·
Rok	475	30	435	32	99	33	1015	33	103	33	2665	42	2895	41	1195	33	25	37	621	490	16.VI	13	39	96	24	12	·	20	175	191	144	15	75	62	19

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Pleszew $\varphi = 51°54$ $\lambda = 17°47'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{n.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.6	-1.6	9.3	22	-13.5	31	0.1	1.5	0.2	0.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	1.1	-3.5	6.6	20	-12.9	1	-2.5	-0.2	-1.4	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	3.0	-3.2	13.4	30	-9.1	8	-2.2	2.1	-0.4	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	15.9	6.1	28.2	23	1.5	30	8.2	14.3	10.0	10.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15.5	6.9	22.8	19	-1.8	1	9.3	13.8	10.2	10.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	20.4	9.5	31.8	16	2.2	3	13.6	19.1	14.1	15.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.5	10.5	33.0	26	6.1	29	14.1	19.9	14.7	15.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	22.2	12.4	31.5	13	7.9	10	15.1	20.7	15.5	16.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	17.9	7.9	30.9	4	1.6	15	10.3	16.5	11.4	12.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	13.0	4.3	22.7	3	-1.9	21	6.1	12.0	7.0	8.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	5.8	2.1	15.1	7	-2.6	26	3.0	5.3	3.6	3.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-1.9	–	6.5	12	–	–	-4.9	-2.7	-4.3	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	11.4	–	33.0	26.VII	–	–	5.8	10.2	6.7	7.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Leszno-Strzyżewice $\varphi = 51°50'$ $\lambda = 16°32'$

I	–	–	–	–	3.3	-1.8	9.7	22	-13.8	31	0.3	2.4	0.5	0.9	5.6	5.7	5.5	5.6	86	76	83	82	0.9	1.9	1.1	1.3	7.7	8.6	7.5	7.9
II	–	–	–	–	1.9	-3.5	7.9	12,20	-13.0	1,2	-1.7	0.8	-0.9	-0.7	4.7	5.4	5.0	5.0	84	81	85	83	0.9	1.2	0.9	1.0	8.8	9.3	7.3	8.5
III	–	–	–	–	3.8	-3.2	15.2	30	-11.1	8	-2.0	2.8	0.0	0.2	4.8	4.9	4.9	4.9	86	65	78	76	0.7	2.8	1.4	1.6	8.2	7.4	7.1	7.6
IV	–	–	–	–	15.9	4.9	28.0	23	-2.7	11	7.5	14.3	9.5	10.2	9.1	8.8	9.6	9.2	86	55	79	73	1.7	9.2	2.9	4.6	7.7	7.8	6.7	7.4
V	–	–	–	–	15.1	6.0	22.0	19	-2.6	1	9.1	13.8	9.8	10.6	10.5	10.1	11.0	10.5	89	64	89	81	1.3	6.2	1.4	3.0	8.3	8.6	8.1	8.3
VI	–	–	–	–	20.5	8.4	31.1	16	1.6	3	13.0	18.9	13.9	14.9	11.9	11.2	12.3	11.8	77	50	75	67	3.6	11.9	4.2	6.6	5.4	7.0	5.8	6.1
VII	–	–	–	–	21.3	9.4	32.4	26	5.4	11	14.0	19.7	14.7	15.8	14.0	12.8	14.1	13.6	87	57	84	76	2.1	11.1	3.0	5.4	7.3	7.5	6.6	7.1
VIII	–	–	–	–	22.2	11.7	30.7	13	6.7	2	14.6	20.5	15.6	16.6	14.6	14.6	14.7	14.6	87	61	83	77	2.1	10.2	3.2	5.2	6.9	8.2	5.6	6.9
IX	–	–	–	–	18.1	7.0	30.4	4	-0.2	15	9.7	16.8	11.2	12.2	11.2	12.0	11.5	11.6	92	64	87	81	1.1	7.9	2.2	3.7	7.5	7.0	4.5	6.3
X	–	–	–	–	13.3	4.0	23.8	3	-3.3	24	5.5	12.4	7.4	8.2	9.2	10.3	9.8	9.8	97	72	92	87	0.3	4.7	1.0	2.0	8.4	6.2	5.0	6.5
XI	–	–	–	–	6.3	2.1	17.5	8	-3.7	21	3.4	5.8	3.9	4.2	7.3	7.8	7.5	7.5	93	83	91	89	0.6	1.8	0.8	1.1	8.7	8.9	8.1	8.6
XII	–	–	–	–	-1.4	-6.3	6.6	12	-17.2	22	-4.3	-2.4	-4.0	-3.7	4.2	4.4	4.2	4.3	88	82	87	86	0.5	1.0	0.6	0.7	8.1	8.7	6.3	7.7
Rok	–	–	–	–	11.7	3.2	32.4	26.VII	-17.2	22.XII	5.8	10.5	6.8	7.5	8.9	9.0	9.2	9.0	88	68	84	80	1.3	5.8	1.9	3.0	7.8	7.9	6.6	7.4

Belsk $\varphi = 51°50'$ $\lambda = 20°48'$

I	–	–	–	–	1.4	-2.9	8.6	22	-18.4	31	-1.4	0.0	-0.9	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.6	7.8	8.2
II	–	–	–	–	-0.4	-5.8	4.8	12	-15.9	1	-3.9	-1.8	-3.0	-2.9	–	–	–	–	–	–	–	–	–	–	–	–	9.6	9.3	7.8	8.9
III	–	–	–	–	1.2	-7.0	12.6	31	-17.5	27	-4.8	-0.2	-2.6	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.7	6.8	7.4
IV	–	–	–	–	15.6	5.0	26.5	22	0.0	8,30	7.8	13.8	8.8	9.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.0	6.6	7.0
V	–	–	–	–	14.7	5.6	22.7	8	-2.1	1	9.1	13.1	8.7	9.9	–	–	–	–	–	–	–	–	–	–	–	–	8.1	9.0	7.6	8.2
VI	–	–	–	–	18.6	8.1	28.4	23	3.1	14	12.7	16.8	12.1	13.4	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.4	5.8	6.8
VII	–	–	–	–	20.8	9.9	29.8	26	3.9	31	14.1	19.1	13.7	15.2	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.7	6.0	6.7
VIII	–	–	–	–	21.6	10.9	30.4	7,13	4.2	10	14.3	19.7	14.1	15.6	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.9	5.1	6.2
IX	–	–	–	–	16.8	7.0	27.0	4	-0.3	25	9.0	15.3	10.8	11.5	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.6	5.7	6.7
X	–	–	–	–	12.1	2.9	18.7	2	-4.0	16	5.1	11.0	6.2	7.1	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.0	4.8	6.7
XI	–	–	–	–	5.5	1.5	13.6	1	-2.0	24	2.8	4.4	3.2	3.4	–	–	–	–	–	–	–	–	–	–	–	–	9.2	9.1	8.6	9.0
XII	–	–	–	–	-2.4	-7.7	4.2	12	-22.7	21	-5.7	-4.3	-5.2	-5.1	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.1	7.4	7.9
Rok	–	–	–	–	10.5	2.3	30.4	7,13.VIII	-22.7	21.XII	4.9	8.9	5.5	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.9	6.7	7.5

Strzelna $\varphi = 51°49'$ $\lambda = 19°54'$

I	–	–	–	–	1.8	-2.7	7.7	22	-18.4	31	-1.1	0.4	-0.8	-0.6	5.2	5.5	5.3	5.3	90	86	89	88	0.6	1.0	0.7	0.8	7.5	7.1	6.3	7.0
II	–	–	–	–	0.1	-5.4	4.1	7	-15.1	1	-3.8	-1.3	-2.6	-2.6	4.4	4.8	4.7	4.6	90	86	90	89	0.5	0.8	0.5	0.6	7.7	8.6	6.5	7.6
III	–	–	–	–	1.7	-5.9	13.7	31	-14.1	20	-4.8	0.4	-1.9	-2.0	4.2	5.4	4.9	4.8	90	82	88	87	0.4	1.2	0.6	0.7	7.3	6.7	5.7	6.6
IV	–	–	–	–	15.5	4.8	27.2	23	-0.6	8	7.1	13.9	8.9	9.7	8.8	8.9	9.7	9.1	85	58	83	75	1.8	8.7	2.4	4.3	6.1	5.8	4.3	5.4
V	–	–	–	–	14.6	5.8	23.0	23	-2.2	1	8.9	13.1	9.3	10.2	10.4	10.4	10.9	10.6	89	69	92	83	1.5	5.3	1.1	2.6	7.7	7.5	6.8	7.3
VI	–	–	–	–	19.0	8.6	30.0	16	3.8	3	12.6	17.3	12.7	13.8	11.9	10.6	13.0	11.8	79	54	86	73	3.2	10.7	2.2	5.4	6.1	5.6	4.4	5.4
VII	–	–	–	–	20.7	10.2	30.6	26	5.4	7	13.7	18.8	14.4	15.3	13.6	12.8	13.8	13.4	86	60	84	77	2.4	9.5	2.9	4.9	5.8	6.0	5.1	5.6
VIII	–	–	–	–	21.8	11.0	31.6	7	5.9	10	14.1	20.0	14.6	15.8	14.3	14.3	15.2	14.6	88	62	90	80	2.0	9.9	1.6	4.5	6.3	6.5	4.1	5.6
IX	–	–	–	–	17.1	7.0	27.9	4	-0.1	25	8.9	15.5	10.7	11.4	10.8	11.5	11.8	11.4	93	66	90	83	0.9	6.8	1.4	3.0	6.8	6.2	4.1	5.7
X	–	–	–	–	12.7	3.1	19.9	2	-4.3	16	4.7	11.8	5.9	7.1	8.6	9.9	9.1	9.2	97	71	95	88	0.3	4.4	0.5	1.7	8.3	5.6	2.6	5.5
XI	–	–	–	–	5.5	1.8	13.2	5	-2.1	24	2.6	4.6	3.3	3.4	7.2	7.6	7.5	7.4	95	88	94	92	0.4	1.2	0.5	0.7	8.5	8.1	7.6	8.1
XII	–	–	–	–	-2.7	-7.3	3.5	12	-20.5	22	-5.5	-4.1	-5.3	-5.0	4.0	4.3	4.2	4.2	91	88	91	90	0.3	0.5	0.3	0.4	7.5	7.7	6.3	7.2
Rok	–	–	–	–	10.6	2.6	31.6	7.VIII	-20.5	22.XII	4.8	9.2	5.8	6.4	8.6	8.8	9.2	8.9	89	72	89	83	1.2	5.0	1.2	2.5	7.1	6.8	5.3	6.4

Pleszew $H_s = 120m$ 1962

MIESIĄC	ROZKŁAD WIATRU n_D, v_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v > 15	◔	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R/ro
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	21	6.8	25	1	6	17	·	–	–	–	–	13	7	·	1	–	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	42	11.7	16	2	10	24	·	–	–	–	–	19	8	2	·	–	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	35	12.7	5	·	7	26	·	–	–	–	–	11	6	1	2	–	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	37	11.0	28	·	·	·	7	–	–	–	–	11	8	1	1	·	·
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	97	32.4	14	·	·	1	·	–	–	–	–	25	17	1	·	·	6
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	23	5.4	1	·	·	·	7	–	–	–	–	9	7	·	·	·	3
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	52	11.0	13	·	·	·	6	–	–	–	–	16	13	1	1	·	6
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	58	21.3	13	·	·	·	7	–	–	–	–	14	13	1	·	·	1
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	54	23.1	18	·	·	·	4	–	–	–	–	14	8	2	3	·	·
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	40	12.7	31	·	·	4	·	–	–	–	–	17	7	1	9	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	49	14.6	1	·	1	8	·	–	–	–	–	17	10	1	4	–	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	20	8.2	15	–	15	–	·	–	–	–	–	14	4	·	3	–	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	528	32.4	14.V	–	39	–	31	–	–	–	–	180	108	11	24	–	16

Leszno-Strzyżewice $H_s = 91m$ 11,3 m anemometr $h_w = 14,2m$ wiatromierz Wilda

I	0.5	7.0	7	3.6	0.5	4.0	7	4.5	19.5	5.3	34.5	5.7	15	6.4	9	6.0	·	5.5	30	12.9	24	2	5	18	·	8	1	1	19	14	9	1	1	9	:
II	1.5	6.0	12.5	4.9	7.5	4.2	8	1.9	5.5	5.4	40.5	5.7	27	7.4	11.5	7.0	·	5.8	33	9.4	12	2	9	23	·	8	2	·	16	12	8	·	1	13	·
III	10	5.0	16	3.7	7.5	4.5	22	3.8	4	3.8	4.5	3.9	12	5.0	13	4.7	4	4.1	25	10.6	5	1	2	27	·	3	·	1	15	10	7	1	3	12	·
IV	5	5.0	9	4.6	10	4.2	11	4.1	6.5	4.5	14	5.9	18	4.2	14.5	4.8	2	4.6	25	6.1	16	·	·	2	5	5	·	3	16	11	8	·	·	·	3
V	3.5	3.3	2.5	3.6	2.5	4.4	8	3.4	4.5	2.4	18	4.2	36.5	4.3	13.5	4.2	4	3.8	84	20.9	14	·	·	2	·	4	·	·	17	22	15	2	5	·	6
VI	11	5.1	7	3.4	3.5	2.3	7	3.4	3.5	2.6	11.5	4.6	28.5	4.7	17	3.6	1	4.1	23	7.2	3	·	·	·	7	5	·	·	8	10	7	·	·	·	5
VII	9	2.6	5.5	2.7	9.5	2.6	3	2.2	3	2.7	20.5	4.4	28.5	4.4	10	2.8	4	3.5	31	6.2	13	·	·	·	7	3	·	·	12	12	8	·	2	·	11
VIII	3	3.7	2	3.5	1	4.0	6.5	2.9	7.5	4.0	24.5	5.3	36	4.5	7.5	2.7	5	4.1	74	20.7	5	·	·	·	8	5	·	2	13	15	11	2	1	·	4
IX	2	2.0	2.5	2.4	15	2.9	7.5	2.8	6	2.2	15	5.2	29.5	4.4	7.5	3.7	5	3.6	45	12.7	16	·	·	1	3	3	·	4	9	12	7	2	6	·	1
X	2	3.8	5.5	3.5	13.5	2.7	14.5	2.7	6.5	3.0	7	3.2	16.5	4.1	9.5	3.7	18	2.7	21	8.6	31	·	·	8	·	·	·	2	13	10	5	·	15	·	1
XI	1	3.5	10.5	4.1	24.5	4.5	7	4.1	5.5	3.0	15	4.1	12.5	4.6	6	2.8	8	3.8	27	8.8	1	·	·	9	·	2	·	·	20	14	8	·	7	·	·
XII	5	3.3	16.5	4.7	7	4.1	4.5	3.6	9	4.7	22	3.6	18.5	3.9	4.5	5.0	6	3.8	22	14.1	15	9	15	25	·	2	·	2	18	10	4	1	5	17	·
Rok	53.5	4.2	96.5	3.7	102	3.7	106	3.3	81	3.6	197	4.6	278.5	4.8	123.5	4.2	57	4.1	440	20.9	14.V	14	31	115	30	48	3	15	176	152	97	9	46	51	31

UWAGA. Kierunki wiatru – wg wiatromierza Wilda, prędkości wg anemometru.

Belsk $H_s = 180m$ $h_w = 10m$

I	2.5	4.6	7	3.4	0.5	3.0	3.5	2.0	13	2.8	40.5	3.4	20	3.8	4	4.9	2	3.4	20	5.6	25	2	8	20	·	1	·	1	19	12	5	·	2	16?	·
II	4	3.4	8	4.4	11	3.7	3	3.3	7.5	4.2	15	3.9	16	5.7	12.5	6.2	7	4.2	22	6.1	16	7	14	27	·	4	1	·	22	14	5	·	3	28?	1
III	10	4.4	11.5	2.5	5.5	4.3	12.5	2.8	5.5	2.6	4	3.0	10	3.6	8	2.9	26	2.3	46	12.0	31	11	14	27	·	·	·	3	18	12	8	2	5	23?	·
IV	11	3.5	8	3.6	15	2.3	10.5	3.7	10	3.6	15.5	2.9	6.5	4.5	12	3.2	15	2.9	41	11.8	26	·	·	·	4	2	·	2	15	16	8	2	·	1	3
V	4	2.0	·	·	2.5	2.8	9.5	2.5	6.5	2.2	11.5	3.3	21	3.0	6	2.5	32	1.8	160	55.0	14	·	·	2	·	1	·	·	19	23	17	3	2	·	3
VI	6	4.2	3.5	3.6	2	3.0	3.5	1.4	4.5	2.0	18.5	2.9	20.5	3.3	9.5	3.5	22	2.3	95	34.8	4	·	·	·	4	·	·	3	14	13	11	3	·	·	2
VII	5	2.5	4	2.4	1	2.0	2.5	2.6	7	2.4	20.5	2.9	28	3.1	11	3.4	14	2.5	45	14.6	2	·	·	·	5	·	·	·	9	11	7	2	·	·	4
VIII	1	2.0	·	·	1	2.0	4.5	3.6	10.5	2.5	35.5	2.9	26	3.7	6.5	3.7	8	2.9	64	23.5	15	·	·	·	6	·	·	1	6	15	9	2	1	·	2
IX	3.5	3.1	2	4.8	7.5	2.1	5	2.0	10.5	2.6	20.5	3.3	21.5	3.8	5.5	3.5	14	2.7	75	30.7	17	·	·	2	1	1	·	1	13	15	13	2	5	·	3
X	2	3.5	2.5	2.2	5.5	3.1	12.5	2.4	9	2.4	10.5	3.8	18	2.9	4	2.5	29	2.0	13	7.2	27	·	·	9	·	1	·	1	11	6	3	·	12	·	·
XI	1.5	2.0	7.5	3.4	21	5.0	13	4.6	5.5	2.5	10	4.1	8.5	3.7	6	2.2	17	3.2	41	9.1	15	·	·	10	·	1	·	1	25	17	11	·	5	2?	·
XII	8	3.2	12.5	3.7	2	3.7	7	3.6	12.5	3.7	17	4.4	20	2.8	2	1.8	12	3.1	11	3.5	16	12	15	28	·	·	·	1	17	10	4	·	6	16	·
Rok	58.5	3.2	66.5	2.8	61	3.1	87	2.9	102	2.8	219	3.4	216	3.7	87	3.4	198	2.8	633	55.0	14.V	32	51	125	20	11	1	14	188	164	101	16	41	86?	18

Strzelna $H_s = 194m$ $h_w = 18m$

I	4	3.5	4.5	4.2	0.5	2.0	·	·	29	1.9	27	3.3	9.5	2.9	5.5	4.5	13	2.5	29	10.0	25	3	8	21	·	·	·	3	15	10	9	1	7	16	:
II	3	4.3	11	2.5	5	2.3	2	1.5	10	3.3	7	9.2	16.5	6.3	13.5	5.4	16	3.9	49	13.6	12	5	12	24	·	5	1	1	14	17	13	2	5	18	2
III	8.5	3.9	10.5	2.7	6	2.2	8	2.0	7	1.7	2	2.0	5	4.8	7	5.1	39	1.8	57	16.0	31	7	12	26	·	2	·	7	16	12	8	2	8	14	·
IV	15	2.0	9.5	2.1	5	3.0	8	2.5	10	2.4	5	2.0	4	2.5	5.5	5.3	28	1.7	42	14.5	29	·	·	4	5	1	·	3	4	15	9	1	2	1	1
V	5	2.2	5	1.4	9	1.0	7.5	2.1	3	3.2	9	1.9	11.5	4.1	12	2.9	31	1.6	181	65.3	14	·	·	3	·	1	1	3	16	25	16	7	6	·	5
VI	10	2.4	4	2.5	4	1.0	3	1.3	5	1.5	1.5	2.3	15.5	3.0	20	2.2	27	1.6	62	17.5	4	·	·	·	6	·	·	7	8	12	9	2	3	·	3
VII	11	1.4	7	1.9	4	1.0	1	2.0	7	1.7	10	1.8	12	1.8	12	2.2	29	1.2	33	10.0	27	·	·	·	4	·	·	2	7	13	7	1	1	·	4
VIII	·	·	6	1.0	6	1.3	8.5	2.4	7	2.4	17.5	3.1	10	2.7	13	2.4	25	1.7	66	19.0	17	·	·	·	6	·	·	2	7	15	12	2	8	·	5
IX	6	1.3	1	1.0	9	1.3	4	1.0	13	2.1	14	2.4	13	2.2	10	2.5	20	1.5	71	22.0	17	·	·	1	2	·	·	3	8	15	11	2	9	·	3
X	3	1.0	5	1.2	11	1.3	8	1.5	6	1.3	·	·	9	2.1	8	3.0	43	0.9	12	7.0	27	·	·	9	·	·	·	4	7	10	3	·	24	·	
XI	8	1.5	4	2.8	25.5	2.7	8.5	2.1	3	1.3	6	1.3	10	2.5	·	·	25	1.6	51	10.8	20	·	·	9	·	·	·	1	19	15	9	1	18	·	
XII	11	1.7	14	1.9	5	1.6	1.5	3.3	16.5	3.5	5	2.4	7	1.3	5	1.6	28	1.6	24	6.7	17	11	15	28	·	·	·	·	13	11	6	·	9	16	·
Rok	84.5	2.1	81.5	2.1	90	1.7	60	1.8	116.5	2.2	104	2.6	123	3.0	111.5	3.1	324	1.8	677	65.3	14.V	26	47	125	23	9	2	36	134	170	112	21	100	65	23

Żelechów $\varphi = 51°49'$ $\lambda = 21°54'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	P_{0m}	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.2	-3.4	5.8	22	-21.6	31	-1.7	-0.2	-1.2	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.6	6.2	6.9
II	–	–	–	–	-0.6	-6.7	5.0	12	-15.3	1	-5.0	-1.7	-3.1	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.2	8.1	8.1
III	–	–	–	–	0.7	-6.8	9.8	31	-19.2	26	-5.2	-0.4	-2.8	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.7	6.5	6.9
IV	–	–	–	–	15.9	6.2	27.0	22	0.0	8	8.0	14.8	9.7	10.6	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.1	4.3	5.4
V	–	–	–	–	15.5	6.7	22.0	28	-2.2	1	9.4	14.2	10.4	11.1	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.5	6.9	8.0
VI	–	–	–	–	19.0	9.2	29.6	16	3.8	6	12.7	17.8	13.3	14.3	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.2	5.0	5.8
VII	–	–	–	–	21.2	10.5	29.2	27	5.2	5	14.0	20.2	14.7	15.9	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.1	5.3	6.0
VIII	–	–	–	–	21.8	11.7	30.4	13	6.3	10	14.8	20.4	16.0	16.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.6	3.5	5.4
IX	–	–	–	–	17.0	7.5	27.0	5	1.6	25	9.3	15.7	11.1	11.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.1	4.9	6.2
X	–	–	–	–	12.5	3.2	19.1	2	-4.6	16	5.5	11.7	6.7	7.6	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.0	4.0	6.0
XI	–	–	–	–	6.1	2.0	16.5	1	-1.7	17,18	3.0	5.1	3.9	4.0	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.4	8.0	8.5
XII	–	–	–	–	-2.8	-7.5	3.5	10	-21.0	21	-5.3	-4.0	-5.4	-5.0	–	–	–	–	–	–	–	–	–	–	–	–	9.4	7.0	7.5	8.0
Rok	–	–	–	–	10.6	2.7	30.4	13.VIII	-21.6	31.I	5.0	9.5	6.1	6.7	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.9	5.8	6.8

Radzyń Podlaski $\varphi = 51°48'$ $\lambda = 22°38'$

I	–	–	–	–	1.4	-3.4	6.2	23	-20.3	31	-1.8	0.2	-1.4	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.1	6.3	7.2
II	–	–	–	–	-0.6	-6.6	3.9	13	-16.2	1	-4.7	-1.8	-3.4	-3.3	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.8	8.5	8.8
III	–	–	–	–	1.0	-7.0	8.6	31	-18.7	26	-5.2	0.0	-3.3	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.0	6.8	7.1
IV	–	–	–	–	16.3	5.3	27.7	22	-0.5	8	8.0	15.0	9.3	10.4	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.7	3.7	5.0
V	–	–	–	–	16.4	6.6	23.4	28	-1.4	1	9.8	14.6	10.0	11.1	–	–	–	–	–	–	–	–	–	–	–	–	7.4	8.2	6.9	7.5
VI	–	–	–	–	20.3	8.3	29.6	23	3.2	6	13.2	18.7	12.2	14.1	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.0	4.7	5.5
VII	–	–	–	–	22.6	9.9	30.6	27	4.5	5	15.0	21.2	13.4	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.5	5.3	5.4
VIII	–	–	–	–	22.4	10.9	31.6	13	5.9	29	15.2	21.7	14.9	16.7	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.6	4.0	5.0
IX	–	–	–	–	17.7	6.9	28.1	5	1.6	15	9.6	16.7	10.6	11.9	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.8	5.0	6.0
X	–	–	–	–	12.7	2.6	19.1	2	-4.0	16	4.5	11.5	6.2	7.1	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.5	4.6	6.0
XI	–	–	–	–	6.5	2.0	18.4	1	-1.8	18	3.0	5.5	3.8	4.0	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.6	8.6	8.8
XII	–	–	–	–	-2.8	-7.8	2.9	13	-21.8	21	-5.5	-4.1	-5.4	-5.1	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.1	7.1	7.9
Rok	–	–	–	–	11.2	2.3	31.6	13.VIII	-21.8	21.XII	5.1	9.9	5.6	6.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.0	6.0	6.7

Puczniew $\varphi = 51°47'$ $\lambda = 19°05'$

I	–	–	–	–	2.1	-1.9	8.6	22	-15.3	31	-0.5	1.2	-0.2	0.1	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.0	7.5	7.9
II	–	–	–	–	0.7	-4.4	4.6	20	-13.7	1	-3.0	-0.9	-2.0	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	8.9	9.1	7.9	8.6
III	–	–	–	–	2.3	-3.6	14.5	31	-10.3	15	-2.7	1.3	-0.9	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.5	7.5	7.7
IV	–	–	–	–	15.5	5.5	27.6	23	0.5	10	8.2	14.2	9.6	10.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.4	6.4	7.1
V	–	–	–	–	14.9	6.6	22.3	8	-1.8	1	9.0	13.3	10.1	10.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.8	8.0	8.4
VI	–	–	–	–	19.6	9.4	30.3	16	3.0	3	12.8	17.8	14.1	14.7	–	–	–	–	–	–	–	–	–	–	–	–	6.1	7.0	6.3	6.5
VII	–	–	–	–	20.9	10.8	30.6	26	5.3	29	13.9	19.5	15.0	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.3	7.0	7.0
VIII	–	–	–	–	22.0	12.4	32.2	7	7.5	10	14.9	20.4	15.8	16.7	–	–	–	–	–	–	–	–	–	–	–	–	7.3	8.5	7.0	7.6
IX	–	–	–	–	17.3	7.6	28.8	4	1.6	15	9.6	15.9	11.3	12.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.4	5.8	6.7
X	–	–	–	–	13.1	3.7	21.6	3	-3.3	16	5.6	12.2	6.6	7.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.1	4.9	6.1
XI	–	–	–	–	6.0	2.1	14.3	7	-3.3	24	3.1	5.1	3.6	3.8	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.1	8.2	8.5
XII	–	–	–	–	-2.4	-6.5	4.6	12	-19.2	22	-4.8	-3.4	-4.4	-4.2	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.4	8.1	8.6
Rok	–	–	–	–	11.0	3.5	32.2	7.VIII	-19.2	22.XII	5.5	9.7	6.6	7.1	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.8	7.0	7.5

Warka $\varphi = 51°47'$ $\lambda = 21°12'$

I	–	–	–	–	2.0	-3.2	9.3	22	-19.5	31	-1.2	0.7	-0.6	-0.4	5.1	5.2	5.2	5.2	8.7	7.8	8.5	8.3	0.7	1.5	0.9	1.0	7.5	7.2	6.8	7.2
II	–	–	–	–	0.4	-5.9	5.4	12	-15.5	1	-3.9	-1.0	-2.3	-2.4	4.0	4.4	4.6	4.3	8.2	7.7	8.6	8.2	0.8	1.4	0.7	1.0	8.8	8.8	6.9	8.2
III	–	–	–	–	2.2	-6.5	13.4	31	-17.6	26	-4.6	0.8	-2.1	-2.0	3.9	4.5	4.5	4.3	8.2	6.8	8.1	7.7	0.7	2.2	0.9	1.3	7.4	6.9	6.6	7.0
IV	–	–	–	–	16.6	5.6	28.3	23,24	0.0	1	8.3	15.0	10.4	11.0	9.3	9.4	10.3	9.7	8.4	5.9	7.9	7.4	2.0	9.4	2.9	4.8	6.7	6.6	6.3	6.5
V	–	–	–	–	16.0	7.1	22.8	8	-1.1	1	9.4	14.3	10.7	11.3	10.8	11.2	11.5	11.2	8.9	6.8	8.8	8.2	1.3	5.5	1.6	2.8	7.8	8.3	7.3	7.8
VI	–	–	–	–	19.9	9.4	30.5	16	4.5	8	13.3	18.3	13.4	14.6	12.6	11.9	13.1	12.5	8.0	5.8	8.3	7.4	3.2	10.6	2.7	5.5	6.1	6.4	5.8	6.1
VII	–	–	–	–	22.2	10.9	29.9	26	6.6	31	14.4	20.6	14.7	16.1	14.5	14.1	14.7	14.4	8.8	5.8	8.7	7.8	2.1	10.8	2.3	5.1	5.8	6.8	5.8	6.1
VIII	–	–	–	–	22.5	11.5	31.3	7	6.2	10	14.6	20.8	15.7	16.7	14.6	15.4	15.9	15.3	8.7	6.4	8.8	8.0	2.1	10.0	2.1	4.7	6.8	7.4	5.4	6.5
IX	–	–	–	–	17.7	7.7	27.7	4	1.8	25	9.5	16.6	11.5	12.3	10.9	12.3	12.4	11.9	9.0	6.6	9.1	8.2	1.2	7.3	1.3	3.3	6.2	7.0	5.0	6.1
X	–	–	–	–	13.1	3.3	19.9	2	-4.5	16	4.8	12.0	6.7	7.6	8.5	10.4	9.2	9.4	9.6	7.3	9.2	8.7	0.3	4.0	0.8	1.7	8.2	6.3	3.2	5.9
XI	–	–	–	–	6.3	1.9	16.0	1	-2.0	18	3.2	5.3	3.9	4.1	7.2	7.6	7.3	7.4	9.1	8.4	8.9	8.8	0.6	1.6	1.0	1.1	9.1	9.1	8.4	8.9
XII	–	–	–	–	-1.8	-7.5	4.1	10	-20.7	22	-5.1	-3.3	-4.6	-4.4	4.0	4.1	4.1	4.1	8.7	8.0	8.6	8.4	0.5	1.0	0.6	0.7	8.2	7.4	7.5	7.7
Rok	–	–	–	–	11.4	2.9	31.3	7.VIII	-20.7	22.XII	5.2	10.0	6.4	7.0	8.8	9.2	9.4	9.1	8.7	6.9	8.6	8.1	1.3	5.4	1.5	2.7	7.4	7.4	6.2	7.0

Żelechów $H_s = 175\,m$ $h_w = 14{,}5\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU nD, vmD																		OPAD R			LICZBA DNI (n)														
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr v		◉	●	Opad R			≡	⊠	R K
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15			R≥0.1	R≥1.0	R≥10.0			
I	5	4.4	2	5.0	·	·	·	·	12	5.0	44	6.6	25	6.4	4	7.0	1	6.1	24	8.0	25	2	8	23	·	8	1	5	18	10	5	·	–	•	·
II	6	4.0	10	5.5	6	4.7	4	4.0	5	8.2	21	8.3	16	8.6	13	11.4	3	7.4	28	6.2	12	7	15	27	·	10	6	3	20	15	10	·	–	–	·
III	15	6.2	16	5.8	4	2.2	10	7.1	9	4.2	11	5.1	7	9.7	11	3.6	10	5.0	50	10.6	31	7	14	28	·	6	4	5	18	10	8	1	–	–	·
IV	8	5.4	11	4.3	3	10.7	6	7.0	13	6.2	14	4.6	9	2.4	14	5.9	12	4.6	50	20.3	26	·	·	·	5	6	2	5	8	13	7	2	–	·	2
V	1	1.0	2	1.0	2	4.0	4	3.5	2	4.0	23	4.5	24	4.8	28	4.4	7	4.0	162	41.0	14	·	·	1	·	3	3	2	19	21	15	4	–	·	3
VI	12	8.0	·	·	·	·	·	·	·	·	36	5.4	23	3.8	16	5.4	3	5.2	93	27.5	6	·	·	·	6	4	2	6	10	11	9	4	–	·	2
VII	8	3.6	·	·	·	·	·	·	4	4.2	20	3.6	26.5	3.7	16.5	4.2	18	3.1	74	18.0	4,23	·	·	·	6	1	·	5	11	14	13	3	–	·	5
VIII	1	2.0	1	3.0	1	2.0	4	5.5	5	5.2	35	5.5	24	4.0	14	4.4	8	4.4	82	28.5	16	·	·	·	6	5	3	4	6	16	10	3	–	·	4
IX	6	2.5	5	3.4	1	7.0	1	4.0	3	6.3	22	3.9	25	4.6	23	5.2	4	4.2	404	23.0	18	·	·	·	2	2	·	6	11	16	14	3	–	·	2
X	5	1.6	9	3.0	2	4.0	9	2.7	3	4.3	9	3.6	18	5.3	26	3.4	12	3.2	9	5.6	28	·	·	7	·	2	2	4	12	5	3		–	·	
XI	3	3.0	10	6.9	2	5.0	29	7.2	6	3.0	11	4.7	4	9.5	19	3.0	6	5.1	46	8.2	15	·	·	6	·	7	3	2	24	16	11	·	–	–	·
XII	19	3.4	6	5.4	1	3.0	5	4.3	45	7.3	29.5	6.7	12	4.6	13	4.1	3	4.9	13	4.8	13	11	17	29	·	4	·	1	21	10	5	·	–	–	·
Rok	89	3.8	72	3.6	22	3.6	72	3.8	66.5	4.8	275.5	5.2	213.5	5.6	197.5	5.2	87	4.8	735	41.0	14.V	27	54	121	25	58	26	48	178	157	110	20	–	–	18

Radzyń Podlaski $H_s = 151\,m$ $h_w = 13\,m$

I	6	7.1	4	6.4	·	·	1	2.0	5	2.2	17	2.7	35	3.3	5	3.8	20	2.8	26	7.0	25	2	7	23	·	1	·	2	16	16	8	·	1	20	·
II	14.5	6.9	6.5	3.6	13	3.1	4	2.5	2	3.0	8	9.9	17	5.4	3	8.7	16	4.5	46	12.6	12	6	14	28	·	5	3	·	21	18	10	1	2	28	1
III	16	6.5	13	4.0	12	2.2	7	4.1	3	2.0	2	4.5	5	5.0	6	3.8	29	2.9	60	10.8	16	9	12	28	·	3	·	2	16	13	10	2	4	29	
IV	16.5	2.4	5.5	3.5	19	3.4	6	3.8	9	2.6	4	3.8	7	2.1	7	7.0	16	2.8	58	12.3	26	·	·	3	5	1	·	4	5	11	9	2	1	·	1
V	31	2.3	7.5	2.4	7	2.7	1	3.0	3	5.0	3	3.7	12	6.3	7.5	2.7	21	2.5	127	28.4	14	·	·	3	·	1	·	·	16	23	17	3	1	·	5
VI	32	4.1	7	4.0	5	1.8	0.5	2.0	0.5	2.0	3	2.0	9	4.3	17	2.6	16	2.9	98	24.3	4	·	·	·	8	2	·	4	8	12	10	5	·	·	·
VII	21	2.6	7	2.3	1	2.0	1	2.0	5	2.8	3	2.3	22	3.0	18	2.3	15	2.2	64	17.3	22	·	·	·	7	·	·	6	6	15	12	2	·	·	4
VIII	16	2.8	1	2.0	1	2.0	·	·	3	3.7	2	2.5	15	3.1	29	2.1	26	1.9	46	15.1	15	·	·	·	10	·	·	7	5	11	8	1	4	·	3
IX	12	2.0	7	2.1	3	2.7	3	1.7	2	3.5	2	3.5	17	3.5	25	3.1	19	2.3	98	32.1	18	·	·	·	2	·	·	4	10	14	13	3	6	·	2
X	15	2.3	8.5	2.2	14.5	2.3	·	·	1	3.0	·	·	6	3.0	13	3.5	35	1.6	2	4.0	27	·	·	9	·	·	·	6	11	5	1	·	15	·	·
XI	4	3.2	10	8.0	31	4.1	2	6.0	1	1.0	2	3.0	10	3.9	20	3.2	10	3.8	48	10.2	15	·	·	6	·	1	·	1	24	16	11	1	7	3	·
XII	20	4.0	5.5	4.2	7	2.4	4.5	3.1	9.5	4.6	5.5	4.6	11.5	2.7	21.5	3.4	8	3.3	15	5.0	16	10	17	31	·	·	·	2	20	13	4	·	3	18	·
Rok	204	3.8	82.5	3.7	113.5	2.4	30	2.5	44	3.0	51.5	3.5	166.5	3.8	172	3.8	231	2.8	688	32.1	18.IX	27	50	131	32	14	3	38	158	167	113	20	44	98	16

Pucznie $H_s = 142\,m$ $h_w = 10\,m$

I	3	7.7	6	4.2	1	5.5	·	·	10	4.7	41	4.7	20	7.0	11	5.6	1	5.4	23	6.8	25	2	7	19	·	2	2	1	16	17	8	·	4	14	
II	3.5	6.1	9.5	6.3	10.5	5.3	3.5	4.7	8	4.2	13	6.1	16	6.8	15	7.9	5	5.9	37	12.3	12	2	10	24	·	7	3	1	21	21	8	1	3	18	·
III	14.5	4.8	19.5	4.1	4	3.8	12	4.8	10	2.8	7.5	4.1	10	4.3	14.5	5.3	1	4.3	42	12.7	5	1	9	26	·	2	·	·	16	13	8	2	5	5	·
IV	9.5	3.9	10.5	3.5	6	6.1	9.5	4.7	5	3.8	13.5	4.7	15	4.2	13	4.7	8	4.0	33	10.2	30	·	·	·	5	7	·	1	9	12	8	1	1	·	2
V	3	2.7	9	2.6	1.5	2.7	4.5	3.8	5	1.9	13	3.9	20	4.6	22	5.5	15	3.5	105	32.6	14	·	·	3	·	3	2	·	22	23	18	2	2	·	7
VI	6	6.8	8	3.8	1	3.0	3	3.0	2	3.0	3	1.7	28	4.9	23	3.8	16	3.5	47	12.3	23	·	·	·	6	1	·	1	11	13	9	1	1	·	5
VII	6.5	2.8	6.5	3.2	3	1.7	2.5	2.0	2	4.0	11.5	3.3	36	3.2	12	3.8	13	2.8	33	9.9	11	·	·	·	5	·	·	·	15	12	8	·	3	·	5
VIII	2	2.5	3	1.0	2	1.5	4	3.8	4	3.8	11	4.1	40	5.2	8	4.0	19	3.5	62	13.0	13	·	·	·	6	1	·	·	15	14	10	2	3	·	4
IX	3	3.0	1	2.0	8.5	3.4	4	2.8	6	2.5	17	3.0	29	4.2	10.5	4.3	11	3.2	65	21.6	18	·	·	·	3	2	1	3	10	15	9	2	4	·	1
X	0.5	3.0	4	3.5	6.5	2.2	11	2.5	4	2.8	7	3.9	15.5	3.8	14.5	4.0	30	2.3	20	4.9	27	·	·	6		·	·	3	11	9	6	·	11	·	
XI	3.5	3.0	7.5	5.3	22	5.2	17.5	4.4	4.5	2.3	7	2.3	17	5.1	6	3.1	5	4.2	49	10.2	20	·	·	9	·	3	1	1	20	15	12	1	8	1	·
XII	3.5	4.3	15	5.4	9	6.1	9.5	3.5	2	8.2	21.5	5.7	20.5	4.7	12	4.2	·	5.0	9	4.6	15	11	14	28	·	4	·	·	20	11	2	·	4	16	·
Rok	58.5	4.2	99.5	3.7	75	3.9	81	3.3	62.5	3.7	166	4.0	267	4.8	161.5	4.7	124	4.0	525	32.6	14.V	16	40	115	25	32	9	41	186	175	106	12	49	54	24

Warka $H_s = 120\,m$ $h_w = 13\,m$

I	3.5	4.9	6	3.0		·	4.5	2.1	16	2.1	24	2.8	25.5	3.8	4.5	4.7	9	2.8	20	5.0	25	2	7	23	·	1	1	2	16	13	7	·		16	·
II	5	4.3	2.5	4.8	10.5	3.0	4.5	2.5	5.5	2.5	10.5	4.7	12.5	7.6	18	8.0	15	4.5	43	11.1	12	6	13	25	·	7	3	·	18	15	9	1	1	24	1
III	13.5	4.3	8.5	2.1	5.5	2.5	11	2.0	11	2.0		·	6.5	3.8	12	3.8	25	2.3	52	11.3	31	6	9	27	·	1	1	6	18	14	10	1	3	23	·
IV	8	2.1	5	3.6	7.5	2.7	6	3.6	12	3.6	7.5	2.8	10	2.8	13	4.6	21	2.5	55	17.4	26	·	·	·	6	1	1	4	11	11	10	1	·	1	2
V	6.5	1.4	0.5	2.0	1	2.5	5	1.8	4	1.8	7	2.9	21.5	4.7	15.5	2.7	32	2.1	165	46.8	14	·	·	1	·	3	1	1	18	22	18	5	2	·	6
VI	14	3.0	6	2.7	·	·	1	4.0	1	4.0	5	4.8	24.5	4.3	17.5	3.0	21	2.6	89	32.5	4	·	·	·	7	·	·	8	14	13	11	4	·	·	2
VII	4	2.2	8	1.8		·	·	2.2	4.5	2.2	12	2.9	23	3.2	20.5	3.0	21	2.2	82	19.5	22	·	·	·	7	·	·	4	12	12	9	3	·	·	5
VIII	·	·	1	1.0	0.5	8.0	2.5	2.0	3.5	2.0	17.5	2.6	25.5	4.1	8.5	3.2	34	2.1	62	23.8	15	·	·	·	6	1	·	3	9	14	11	2	1	·	4
IX	3	2.3	2	2.0	7	4.6	3	2.2	5.5	2.2	8	3.5	20.5	3.4	14	3.6	27	2.1	75	19.2	17	·	·	·	2	·	·	5	13	14	12	2	3	·	3
X	15	1.3	4.5	1.3	6.5	4.6	6	2.0	1	2.0	3.5	2.6	14.5	3.1	11.5	3.2	44	1.3	8	5.3	27	·	·	7	·	·	·	3	8	5	2	·	15	·	
XI	4	1.2	2	4.0	15	3.2	23	4.5	2	4.5	1	3.0	14	3.5	4	1.8	25	2.4	42	8.2	15	·	·	7	·	·	·	1	24	17	13	·	5	·	
XII	7	2.1	13.5	2.1	3.5	4.7	4.5	2.8	10	2.8	9.5	4.1	18	3.1	7	3.1	20	2.2	18	5.2	13	11	15	26	·	·	·	2	18	10	6	·	3	16	
Rok	70	2.4	59.5	2.5	57	2.2	71	2.4	76	2.6	105.5	2.8	216	4.0	146	3.7	294	2.4	711	46.8	14.V	25	44	116	28	14	7	39	179	160	118	19	33	80	23

Wisznice $\varphi = 51°47'$ $\lambda = 23°13'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.1	-3.3	6.4	22	-19.5	31	-2.1	0.0	-1.7	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.0	7.2	6.9
II	–	–	–	–	-1.1	-6.4	3.5	13	-15.7	1	-4.7	-2.1	-3.7	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.5	8.6	8.1
III	–	–	–	–	1.1	-7.2	7.7	6,31	-18.5	26	-5.4	-0.2	-3.8	-3.3	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.7	7.2	6.6
IV	–	–	–	–	16.4	5.6	27.9	22	-0.9	30	7.7	14.9	10.1	10.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	16.4	7.1	23.6	28	-1.5	1	9.9	14.5	11.0	11.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	19.6	9.1	28.8	16	3.0	3	13.1	17.9	14.0	14.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.5	10.8	29.3	27	6.3	3	14.7	19.7	14.5	15.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	22.4	11.4	30.3	13	6.7	10	14.9	20.9	16.2	17.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	17.6	7.6	28.8	5	2.2	15	9.9	16.1	11.4	12.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	12.7	2.6	19.9	1	-4.0	16	4.4	11.4	6.4	7.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	7.0	1.9	20.2	1	-2.2	18	3.2	5.9	3.8	4.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-2.8	-8.0	3.1	13	-20.5	21	-5.8	-4.2	-6.0	-5.5	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.0	6.8	7.4
Rok	–	–	–	–	11.0	2.6	30.3	13.VIII	-20.5	21.XII	5.0	9.6	6.0	6.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kalisz $\varphi = 51°44'$ $\lambda = 18°05'$

I	998.6	1021.5	972.9	1016.7	2.2	-2.3	8.6	22	-13.5	31	-0.6	1.0	-0.4	-0.1	5.5	5.6	5.4	5.5	91	83	89	88	0.6	1.2	0.7	0.8	7.4	8.4	7.1	7.6
II	998.4	1018.4	968.3	1016.6	0.9	-3.9	5.9	20	-13.1	1	-3.1	-0.5	-1.5	-1.6	4.5	4.9	5.0	4.8	90	85	89	88	0.5	0.9	0.6	0.7	8.2	8.7	6.6	7.8
III	993.8	1011.0	970.7	1011.9	2.7	-3.3	13.7	31	-8.9	15	-2.6	1.5	-0.7	-0.6	4.7	5.0	5.1	4.9	91	71	85	82	0.5	2.1	0.9	1.2	7.6	7.6	7.5	7.6
IV	996.6	1009.7	970.5	1014.0	15.6	5.8	27.4	23	0.6	30	7.7	13.9	9.8	10.3	9.4	8.9	9.6	9.3	88	58	79	75	1.4	8.8	3.2	4.5	7.2	6.9	5.2	6.4
V	996.0	1002.6	984.1	1013.3	15.3	6.6	22.1	8	-1.9	1	9.0	13.5	10.0	10.6	10.5	10.6	11.0	10.7	90	69	88	82	1.2	5.4	1.6	2.7	7.2	8.0	6.5	7.2
VI	1001.4	1011.9	991.1	1018.6	20.3	9.2	30.6	16	2.6	3	12.8	18.3	14.0	14.8	11.9	11.2	12.3	11.8	78	53	74	68	3.4	11.2	4.2	6.3	4.7	7.2	5.3	5.7
VII	997.8	1008.2	983.2	1014.7	21.1	10.6	31.5	26	7.0	4	13.8	19.5	14.7	15.7	14.0	12.8	13.8	13.5	88	58	82	76	2.0	10.7	3.2	5.3	6.6	6.9	5.7	6.4
VIII	998.7	1007.2	984.7	1015.7	22.4	12.4	31.6	13	8.5	31	14.8	21.0	15.6	16.8	14.8	14.2	15.1	14.7	87	58	84	76	2.2	11.5	3.0	5.6	7.0	7.4	4.9	6.4
IX	999.4	1012.4	982.4	1016.7	18.0	7.5	30.7	4	1.4	15	9.6	16.2	11.5	12.2	11.2	11.9	11.5	11.5	93	66	85	81	1.0	7.5	2.4	3.6	7.0	6.9	4.0	6.0
X	1005.1	1018.9	992.6	1022.8	13.2	4.0	22.1	1,2,3	-2.5	24	5.2	12.1	7.2	7.9	9.0	10.5	9.8	9.8	98	75	94	89	0.2	4.1	0.7	1.7	7.7	5.9	4.6	6.1
XI	999.3	1016.3	980.3	1017.1	5.9	1.7	15.1	8	-4.4	26	2.8	5.1	3.2	3.6	7.2	7.9	7.4	7.5	95	88	94	92	0.4	1.3	0.5	0.7	8.2	8.5	6.9	7.9
XII	999.0	1027.1	954.4	1017.4	-2.0	-6.5	5.1	12	-18.6	22	-5.2	-3.2	-4.5	-4.4	4.2	4.5	4.3	4.3	92	89	91	91	0.3	0.6	0.4	0.4	7.2	8.3	7.0	7.5
Rok	998.7	1027.1	954.4	1016.3	11.3	3.5	31.6	13.VIII	-18.6	22.XII	5.4	9.9	6.6	7.1	8.9	9.0	9.2	9.0	90	71	86	82	1.1	5.4	1.8	2.8	7.2	7.6	5.9	6.9

Łódź-Lublinek $\varphi = 51°44'$ $\lambda = 19°24'$

I	992.5	1015.1	967.4	1015.9	2.2	-2.7	8.7	22	-16.8	31	-0.9	0.5	-0.6	-0.4	5.2	5.3	5.2	5.2	88	82	86	85	0.8	1.2	0.9	1.0	7.9	8.2	7.4	7.8
II	991.9	1011.7	961.7	1015.5	0.7	-5.2	5.6	12	-15.4	3	-3.7	-1.5	-2.4	-2.5	4.2	4.6	4.7	4.5	87	82	89	86	0.7	1.0	0.6	0.8	9.1	9.0	7.7	8.6
III	987.8	1004.2	967.4	1011.2	2.8	-4.5	15.1	31	-11.1	15	-3.6	0.8	-1.2	-1.3	4.4	4.9	4.8	4.7	90	73	83	82	0.5	1.8	0.9	1.1	8.4	7.6	6.5	7.5
IV	990.9	1004.1	965.5	1013.5	16.1	5.5	28.0	23	0.0	7	7.6	14.1	9.8	10.3	8.9	8.7	9.5	9.0	84	57	77	73	2.0	9.3	3.5	4.9	7.4	7.0	5.5	6.6
V	990.0	996.7	974.6	1012.6	15.5	6.5	22.6	8	-2.2	1	8.9	13.3	10.0	10.6	10.2	9.9	10.6	10.2	88	65	85	79	1.4	5.9	1.9	3.1	8.3	8.4	7.6	8.1
VI	995.2	1005.2	985.3	1017.7	19.8	9.2	30.2	16	3.0	3	12.6	17.6	14.0	14.6	11.6	10.7	12.3	11.5	77	54	75	69	3.5	10.6	4.5	6.2	6.2	6.7	5.6	6.2
VII	991.9	1002.4	978.8	1014.1	21.5	10.7	32.1	26	4.8	29	13.8	19.0	14.7	15.6	13.5	12.6	13.4	13.2	85	58	80	74	2.5	10.0	3.8	5.4	6.9	6.7	6.8	6.8
VIII	992.9	1001.2	981.6	1015.1	22.5	12.1	31.6	7	7.8	31	14.6	20.5	15.8	16.7	14.3	13.9	14.9	14.4	85	59	83	76	2.4	11.0	3.3	5.6	7.1	7.5	5.9	6.8
IX	993.4	1006.7	977.5	1016.0	17.9	7.5	28.9	4	2.2	25	9.4	15.6	11.5	12.0	10.7	11.3	11.6	11.2	90	65	85	80	1.3	7.1	2.4	3.6	6.9	7.4	5.0	6.4
X	999.1	1013.2	987.0	1022.2	13.3	4.1	20.8	1,2	-2.6	21	5.4	11.9	7.1	7.9	9.0	9.8	9.3	9.4	97	70	91	86	0.3	4.6	1.0	2.0	7.4	6.0	4.3	5.9
XI	993.6	1009.7	976.0	1016.8	6.3	2.0	14.2	5	-3.4	24	2.9	4.9	3.5	3.7	7.1	7.5	7.4	7.3	93	85	92	90	0.5	1.5	0.7	0.9	9.1	8.6	8.8	8.8
XII	992.9	1020.5	950.4	1016.7	-2.1	-7.3	4.5	12	-19.2	22	-5.3	-3.7	-4.9	-4.7	4.0	4.3	4.1	4.1	91	88	89	89	0.4	0.7	0.5	0.5	8.9	8.4	7.7	8.3
Rok	992.7	1020.5	950.4	1015.6	11.4	3.2	32.1	26.VII	-19.2	22.XII	5.1	9.4	6.4	6.8	8.6	8.6	9.0	8.7	88	70	85	81	1.4	5.4	2.0	2.9	7.8	7.6	6.6	7.3

UWAGA. Ciśnienie powietrza jest za niskie przeciętnie o około 0,6 mb.

Łódź-Ruda Pabianicka $\varphi = 51°42'$ $\lambda = 19°27'$

I	–	–	–	–	1.9	-2.7	8.2	22	-17.2	31	-1.1	0.7	-0.7	-0.4	5.1	5.3	5.1	5.2	88	80	85	84	0.7	1.3	0.9	1.0	8.4	8.2	7.4	8.0
II	–	–	–	–	0.3	-5.4	4.9	12	-15.5	3	-3.8	-1.1	-2.7	-2.6	4.1	4.5	4.6	4.4	86	78	87	84	0.7	1.3	0.6	0.9	10.0	9.2	7.6	8.9
III	–	–	–	–	2.8	-4.9	14.9	31	-13.4	15	-3.8	1.3	-1.4	-1.3	4.2	4.7	4.6	4.5	87	66	81	78	0.6	2.4	1.0	1.3	8.2	7.7	6.6	7.5
IV	–	–	–	–	16.1	4.8	27.9	22,23	-0.5	8	7.5	14.7	9.2	10.2	8.8	8.7	9.6	9.0	8.3	5.5	8.0	7.3	2.0	10.0	2.8	4.9	7.2	7.0	5.5	6.6
V	–	–	–	–	15.3	6.0	22.7	8	-2.6	3	9.0	13.7	9.5	10.4	10.3	10.3	10.7	10.4	8.9	6.6	8.9	8.1	1.3	6.0	1.4	2.9	8.3	8.2	7.6	8.0
VI	–	–	–	–	19.6	8.9	30.1	16	2.2	3	12.8	18.2	13.1	14.3	11.8	11.1	12.6	11.8	7.7	5.4	8.2	7.1	3.5	11.2	3.0	5.9	5.8	6.9	6.5	6.4
VII	–	–	–	–	21.2	10.3	32.2	26	5.2	29	13.8	19.4	14.3	15.4	13.6	12.8	13.5	13.3	8.5	5.8	8.2	7.5	2.4	10.5	3.2	5.4	7.2	7.0	7.0	7.1
VIII	–	–	–	–	22.1	11.5	31.4	13	7.2	10	14.5	20.7	14.9	16.2	14.4	14.5	15.1	14.7	8.6	6.0	8.8	7.8	2.2	10.9	2.1	5.1	7.4	7.7	5.4	6.8
IX	–	–	–	–	17.4	7.1	28.3	4	1.1	15	9.2	15.8	10.7	11.6	10.7	11.6	11.5	11.3	9.1	6.6	8.8	8.2	1.2	7.0	1.6	3.3	7.2	7.0	4.9	6.4
X	–	–	–	–	13.1	3.5	20.9	2	-3.5	16,21	5.1	12.1	6.0	7.3	8.7	9.9	8.9	9.2	9.6	7.0	9.3	8.6	0.4	4.5	0.7	1.9	8.4	5.8	4.3	6.2
XI	–	–	–	–	5.9	1.9	14.3	5	-3.3	24	2.8	5.0	3.4	3.6	7.0	7.5	7.3	7.3	9.2	8.4	9.1	8.9	0.6	1.6	0.7	1.0	9.4	8.5	8.5	8.8
XII	–	–	–	–	-2.4	-7.3	4.6	12	-19.4	22	-5.4	-3.6	-5.1	-4.8	3.9	4.2	4.0	4.0	8.9	8.4	8.7	8.7	0.5	0.8	0.6	0.6	9.8	8.2	7.8	8.6
Rok	–	–	–	–	11.1	2.8	32.2	26.VII	-19.4	22.XII	5.0	9.7	5.9	6.6	8.6	8.8	9.0	8.8	8.7	6.8	8.6	8.0	1.3	5.6	1.6	2.8	8.1	7.6	6.6	7.4

Wisznice $H_s = 152\,m$ $h_w = 13\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU (n), (v) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◑	●	Opad R R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	3	6.3	4.5	3.3	2.5	2.4	2	3.0	2.4	2.4	32.5	3.9	19.5	4.9	4	3.8	1	3.7	20	8.4	25	2	8	24	·	·	·	4	15	9	5	·	·	17	–
II	12.5	3.4	4	3.8	12	2.3	4.5	2.7	9	7.4	11.5	8.0	15.5	7.4	7	5.9	8	4.9	38	15.7	12	5	16	28		8	6	·	15	15	8	1	·	28	–
III	10.5	5.1	12.5	1.9	13	2.5	7.5	3.4	8	4.4	2.5	8.0	9.5	6.1	5.5	3.2	24	2.9	43	11.7	16	8	12	28	·	5	3	6	15	10	8	1	4	25	–
IV	5.5	4.4	2	2.2	10.5	2.0	12.5	2.7	13.5	2.9	8	2.0	8	2.1	5	3.6	25	1.9	58	14.2	7	·	·	3	5	·	·	–	–	9	7	2	3		–
V	4.5	1.7	2	2.0	5	1.6	3.5	2.1	4.5	2.1	21.5	3.8	19.5	2.9	6.5	2.2	26	2.0	113	32.5	14	·	·	3	·	1	1	–	–	16	14	4	2	·	–
VI	12.5	4.5	8.5	2.8	1.5	3.0	7	1.6	3	1.7	8	2.6	25	4.6	7.5	2.4	17	2.8	107	30.2	4	·	·	·	7	1	·	–	–	10	10	6	·	·	–
VII	10	2.0	5	1.8	1.5	1.0	0.5	1.0	9.5	2.4	7.5	2.3	31	3.4	19	1.7	9	2.2	75	35.2	18	·	·	·	4	1	·	–	–	12	9	1	·	·	–
VIII	8.5	2.2	4.5	1.4	3	1.0	2.5	1.8	13.5	4.8	14	2.6	28	3.1	2	3.5	17	2.0	47	17.8	5	·	·	·	6	·	·	–	–	12	10	1	1	·	–
IX	3	1.7	4	1.6	5.5	1.4	4	1.9	16	2.1	14	4.6	27.5	3.7	3	3.5	13	2.6	76	19.5	18	·	·	·	2	·	·	–	–	12	10	3	6	·	–
X	4	1.9	4.5	1.4	9.5	1.4	3.5	1.9	4	1.0	16.5	3.1	14	3.0	8	2.6	29	1.6	4	4.4	19	·	·	7	·	·	·	–	–	6	3	·	13	·	–
XI	7	1.6	3	2.3	26	3.4	18	3.1	3.5	3.3	6.5	2.4	11	2.5	7	1.9	8	2.6	62	10.2	12	·		6	·	·	·	–	–	19	12	1	9	·	–
XII	16	2.2	9	2.5	- 4	1.5	4.5	1.8	15.5	3.3	12	2.8	13	2.4	5	1.4	14	2.1	15	5.8	16	11	19	30	·	·	·	–	–	13	3	·	·	22	–
Rok	97	3.1	63.5	2.2	94	2.0	70	2.2	124	2.9	154.5	3.8	221.5	3.8	79.5	3.0	191	2.6	658	35.2	18 VII	26	55	129	24	16	10	–	–	143	99	20	38	92	–

Kalisz $H_s = 140\,m$ $H_b = 143{,}1\,m$ $h_w = 13{,}5\,m$

I	3.5	5.6	6	3.7	0.5	1.0	2.5	2.6	23	3.7	34.5	4.5	45	4.5	8	4.9	·	4.2	19	9.6	25	2	7	20	·	1	·	1	16	12	4	·	1	15	·
II	7	6.0	11.5	3.9	6	4.5	3.5	3.0	14	2.1	12	5.7	48.5	6.9	10.5	5.1	1	4.8	34	11.4	12	2	10	23	·	7	1	·	16	13	7	1	·	12	·
III	10.5	5.0	11	2.5	9.5	2.7	10	2.8	12	1.8	6.5	2.6	40.5	3.7	9	4.4	14	2.7	36	9.4	31	·	7	25	·	3	2	2	19	9	7	·	2	12	·
IV	8	2.7	11.5	3.0	5	2.6	8	2.8	15	3.6	13	3.7	9.5	2.5	42	3.9	8	2.9	38	10.3	29	·	·	·	6	1	·	4	9	10	8	2	1	·	1
V	2.5	2.2	5.5	1.7	0.5	3.0	8	1.8	12.5	4.8	20.5	2.5	23.5	3.8	13	4.2	7	2.7	83	23.9	14	·	·	2	·	2	2	1	12	23	20	1	·	·	6
VI	12	3.6	3	1.5	0.5	1.0	3	2.2	7.5	1.7	7	2.9	26	3.9	17	2.5	14	2.6	22	5.5	16	·	·	·	8	·	·	·	8	11	8	·	·	·	4
VII	3.5	2.4	6.5	1.5	2	1.2	3.5	1.1	6	2.2	17	2.4	26	2.4	15.5	2.3	13	1.9	53	13.7	11	·	·	·	6	·	·	1	12	16	9	2	2	·	7
VIII	0.5	6.0	2	2.8	2	1.0	7.5	1.7	8.5	3.4	20.5	3.7	35	4.0	7	3.8	10	3.2	62	15.4	4	·	·	·	8	·		2	13	15	12	2	·	·	4
IX	2	1.8	2	1.8	7.5	2.2	6.5	3.1	8	2.3	16	3.4	28	3.5	11	3.5	9	2.8	47	19.7	18	·	·	·	4	2	·	3	8	9	5	1	2	·	
X	4.5	1.3	3.5	3.0	5	1.8	15.5	1.7	14	1.2	6	2.2	12.5	3.1	8	2.3	24	1.5	34	12.5	31	·	·	5	·	·	·	4	12	8	6	1	12		·
XI	3	2.3	6	3.9	15	3.1	14	3.4	6	2.2	9.5	3.6	11	2.6	8.5	2.5	17	2.5	43	11.8	1	·	·	8	·	·	·	1	18	13	9	2	8	8	·
XII	9.5	1.7	13	3.0	7	3.5	5.5	1.7	12	3.8	12	4.1	19.5	3.3	7.5	2.4	7	2.9	16	4.7	15	11	15	27	·	·	·	2	16	10	5	·	4	17	·
Rok	66.5	3.4	81.5	2.7	60.5	2.3	87.5	2.3	138.5	2.5	174.5	3.4	235	3.7	127	3.5	124	2.9	487	23.9	14 V	15	39	110	32	16	5	21	159	149	100	12	32	64	22

Łódź-Lublinek $H_s = 187\,m$ $H_b = 187{,}7\,m$ $h_w = 11\,m$

I	3.5	8.1	5	6.5	2	4.0	1	2.0	22.5	5.5	34.5	5.8	18	6.4	6.5	6.8	·	6.0	31	10.6	25	3	5	21		10	1	1	16	17	9	1	2	17	
II	2.5	6.0	6.5	6.3	12.5	4.6	4.5	2.9	8	4.5	9	6.6	20	7.8	15	8.3	6	6.0	30	9.3	12	3	12	25	·	9	2	1	21	19	6	·	6	19	
III	10	6.7	10.5	4.6	19	3.5	12.5	3.4	4.5	3.4	4.5	4.8	10.5	5.1	12.5	5.2	9	4.1	49	16.7	31	2	8	26	·	4	·	1	17	15	8	3	4	13	·
IV	11.5	3.4	7	5.4	12.5	4.0	6.5	7.5	9.5	3.9	16	4.9	8	4.1	12	5.0	7	4.3	50	42.1	13		·	·	7	5	·	3	12	15	10	2	2	1	1
V	1.5	5.3	5	2.5	13.5	1.7	6	3.4	3	2.5	20	3.1	19.5	6.1	14.5	4.7	10	3.5	157	49.4	14	·	·	2	·	4	1	·	19	22	17	6	1	·	5
VI	12.5	5.2	4	3.9	5.5	1.4	3.5	1.9	6.5	2.1	5.5	3.3	26	5.3	18.5	4.6	8	3.9	81	30.7	23	·	·	·	7	4	·	1	10	15	9	3	·	·	3
VII	6.5	2.8	3.5	3.9	9	2.2	2.5	3.8	4.5	2.3	18	3.2	26	3.2	11	4.5	12	2.8	50	16.1	13	·	·	·	6	1	·	·	12	16	10	1	·	·	6
VIII	1.5	2.0	3	1.3	7.5	1.9	5.5	2.6	9.5	2.8	15.5	4.9	29	5.5	8.5	6.0	13	3.8	79	19.8	13	·		·	9	4	·	1	11	15	12	3	2	·	6
IX	2	4.0	1	3.5	14	2.9	8	3.2	8	2.8	17	4.8	22	5.0	10	5.6	8	3.9	62	18.8	17,18	·		·	4	4	·	3	11	15	10	2	5	·	1
X	2.5	1.4	8	2.6	21.5	2.3	11.5	2.5	6	2.9	4.5	4.6	14.5	4.6	7.5	4.3	17	2.6	16	7.2	27	·	·	6	·	·	·	4	10	12	3	·	17	·	·
XI	5.5	2.2	6	7.0	27.5	5.2	12.5	5.2	4.5	3.4	9	4.4	12.5	4.1	3.5	3.6	9	4.2	41	10.6	20	·	·	10	·	2	·	·	22	15	10	1	4	1	·
XII	8.5	5.2	12	6.2	11.5	4.3	4.5	3.2	10.5	5.8	15.5	5.9	16	3.9	5.5	3.5	9	4.5	18	7.6	15	12	14	28	·	6	·	·	21	17	4	·	6	17	·
Rok	68	4.4	71.5	4.5	156	3.2	78.5	3.5	97	3.5	169	4.7	222	5.1	125	5.2	108	4.1	664	49.4	14 V	20	39	118	33	53	4	15	182	193	108	22	49	68	22

Łódź-Ruda Pabianicka $H_s = 181\,m$ $h_w = 18\,m$

I	4.5	5.0	1.5	1.7	2	3.0	3	2.0	23	3.8	32	5.3	20.5	5.5	5.5	5.2	1	4.7	40	9.0	25	3	7	21	·	2		2	19	18	12		9	18	·
II	5.5	4.5	4	4.4	15.5	4.6	4	3.5	9.5	2.9	10	5.2	24.5	7.1	9	7.7	2	5.4	60	19.5	12	4	12	25	·	5	·		21	22	13	2	7	22	
III	5.5	5.8	11.5	2.9	23.5	3.0	13	4.1	4	3.1	7	4.0	16	5.3	9.5	4.4	3	3.8	58	17.2	12	4	8	26	·	5	·	2	20	15	9	2	9	14	·
IV	5.5	3.0	6	3.2	11.5	3.9	10	4.3	9.5	3.5	16.5	3.8	12.5	4.7	13.5	3.9	5	3.7	55	14.5	13	·	·	3	6	3	·	3	8	14	11	3	4	·	1
V	·	·	4.5	1.2	8.5	1.5	14	2.2	5.5	1.5	18.5	2.8	22	4.4	9	4.1	11	2.6	162	45.6	14	·	·	2	·	3	·	·	20	25	18	4	8	·	4
VI	4.5	3.0	1	3.0	7	2.6	5.5	1.9	4	1.2	5.5	4.1	27.5	4.0	21	4.1	14	3.0	62	16.1	5	·	·	·	6	3	·	2	12	15	10	2	1	·	3
VII	2	3.5	4	1.5	4.5	1.4	5.5	2.8	5	2.1	19.5	2.8	24.5	2.8	14	3.0	14	2.3	41	14.3	11	·			5	1	·	2	15	12	7	1	1		5
VIII	1	1.0	3	1.0	3	2.0	11.5	1.9	9.5	2.7	9	4.4	36.5	4.1	5.5	2.9	14	2.8	91	29.4	13	·		·	7	1	·	·	11	18	13	2	6		5
IX	2	1.0	0.5	2.0	14	2.5	8	1.9	8.5	2.1	19.5	2.6	23	3.8	9.5	3.7	5	2.7	62	21.5	17	·		·	2	3	·	2	10	12	7	2	7	·	2
X	1.5	1.0	5.5	1.8	16	1.8	22	2.0	5	2.2	10	2.9	15.5	3.7	6.5	2.6	11	2.1	14	6.5	27	·	·	7	·	·	·	3	10	9	3	·	24	·	·
XI	2	1.5	3	2.5	31	4.7	12.5	4.4	5.5	1.7	8	3.5	13.5	3.7	5.5	2.1	9	3.5	42	12.6	20	·	·	9		·		1	23	17	10	1	14	1	·
XII	3	3.3	10.5	2.9	14.5	3.9	9	3.1	8	4.5	14	3.9	24	3.0	5	2.8	5	3.2	16	7.3	15	12	14	28	·	·		·	22	12	4	·	8	17	·
Rok	37	2.7	55	2.3	151	2.9	118	2.8	97	2.6	163.5	3.8	260	4.3	113.5	3.9	54	3.3	703	45.6	14 V	23	41	121	26	26	·	17	191	189	117	19	98	72	20

Smolice $\varphi = 51°42'$ $\lambda = 17°11'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0,m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.7	-2.1	8.8	22	-13.8	31	0.0	1.9	0.1	0.5	5.3	5.6	5.4	5.4	84	79	84	82	1.0	1.6	1.0	1.2	7.4	8.4	7.5	7.8
II	–	–	–	–	1.4	-3.6	7.4	12	-13.5	1	-2.0	0.6	-1.0	-0.8	4.7	5.5	5.0	5.1	87	84	87	86	0.8	1.0	0.8	0.9	8.8	8.8	6.4	8.0
III	–	–	–	–	3.2	-2.9	13.7	30	-11.2	8	-1.9	2.3	-0.1	0.0	4.9	5.4	5.2	5.2	89	73	84	82	0.6	2.0	1.0	1.2	8.2	7.6	6.6	7.5
IV	–	–	–	–	16.0	5.8	28.2	23	-0.1	11	8.1	14.6	9.8	10.6	9.6	9.1	10.0	9.6	86	57	80	74	1.7	9.4	2.8	4.6	7.6	7.6	5.2	6.8
V	–	–	–	–	15.3	6.4	22.4	19	-1.7	1	9.3	13.9	10.1	10.9	10.5	10.3	10.9	10.6	89	65	87	80	1.4	6.1	1.7	3.1	7.7	7.9	6.1	7.2
VI	–	–	–	–	20.3	9.2	31.7	16	2.0	3	13.3	19.1	14.6	15.4	11.9	11.1	12.7	11.9	76	50	74	67	4.0	12.2	4.5	6.9	5.4	6.4	5.1	5.6
VII	–	–	–	–	20.8	10.1	31.1	26	6.2	29	14.2	19.4	15.0	15.9	14.9	13.9	15.3	14.7	90	63	89	81	1.5	9.5	2.0	4.3	6.5	6.6	5.2	6.1
VIII	–	–	–	–	22.3	12.1	31.5	13	7.4	9	15.0	20.9	15.7	16.8	15.0	14.4	15.3	14.9	87	60	85	77	2.3	11.0	2.8	5.4	6.7	7.4	5.7	6.6
IX	–	–	–	–	18.3	7.5	31.6	4	1.9	15	10.0	16.7	11.5	12.4	11.4	11.9	11.5	11.6	92	64	85	80	1.1	8.1	2.4	3.9	6.5	6.6	3.0	5.4
X	–	–	–	–	13.2	4.1	23.6	3	-3.7	21	5.6	12.5	7.5	8.3	9.2	10.6	9.8	9.9	96	73	92	87	0.3	4.6	0.9	1.9	7.5	6.2	5.1	6.3
XI	–	–	–	–	6.5	2.2	17.8	8	-2.8	21	3.4	5.9	3.9	4.3	7.4	7.9	7.6	7.6	94	83	92	90	0.5	1.8	0.6	1.0	8.5	7.6	7.6	7.9
XII	–	–	–	–	-1.6	-6.5	7.0	12	-17.6	22	-4.5	-2.4	-4.2	-3.8	4.3	4.6	4.3	4.4	91	85	89	88	0.4	0.8	0.5	0.6	8.2	7.8	6.8	7.6
Rok	–	–	–	–	11.5	3.5	31.7	16.VI	-17.6	22.XII	5.9	10.4	6.9	7.5	9.1	9.2	9.4	9.2	88	70	86	81	1.3	5.7	1.8	2.9	7.4	7.4	5.9	6.9

Głogów $\varphi = 51°39'$ $\lambda = 16°06'$

I	–	–	–	–	3.6	-1.3	10.2	22	-13.4	31	0.7	2.6	0.9	1.3	5.8	5.9	5.5	5.7	86	79	82	82	1.0	1.7	1.3	1.3	7.1	8.1	7.7	7.6
II	–	–	–	–	2.2	-3.1	8.3	12	-13.7	1	-1.3	0.9	-0.4	-0.3	5.0	5.6	5.2	5.3	88	83	86	86	0.7	1.1	0.9	0.9	8.9	9.5	7.2	8.5
III	–	–	–	–	3.8	-3.1	15.0	30	-7.7	8	-1.6	2.8	0.1	0.4	5.0	5.1	5.2	5.1	89	67	82	79	0.7	2.6	1.2	1.5	7.5	7.5	7.5	7.5
IV	–	–	–	–	16.0	5.8	29.3	25	0.3	30	7.8	14.3	9.9	10.5	8.8	8.4	8.9	8.7	81	54	73	69	2.4	9.8	4.0	5.4	7.0	6.7	6.7	6.8
V	–	–	–	–	15.3	7.2	22.7	8	-0.7	1	9.2	13.9	10.2	10.9	10.2	10.0	10.6	10.3	87	63	84	78	1.6	6.3	2.0	3.3	7.8	8.3	8.5	8.2
VI	–	–	–	–	20.7	9.7	31.2	16	2.3	6	12.8	19.1	14.5	15.2	11.8	10.9	12.0	11.6	78	48	70	65	3.5	12.7	5.3	7.2	5.2	6.2	5.9	5.8
VII	–	–	–	–	21.2	10.7	32.9	26	7.4	4	14.6	19.8	15.0	16.1	14.0	13.2	13.8	13.7	83	58	80	74	2.9	10.9	3.6	5.8	5.4	7.5	6.4	6.4
VIII	–	–	–	–	22.1	12.6	31.0	13	9.1	9	15.2	20.8	16.0	17.0	14.2	14.3	14.3	14.3	82	59	78	73	3.1	11.0	4.1	6.1	7.2	7.8	7.9	7.6
IX	–	–	–	–	18.3	8.1	30.5	4	1.5	15	10.1	17.0	12.0	12.8	11.1	12.0	11.2	11.4	89	63	80	77	1.6	8.3	3.2	4.4	6.8	6.9	4.4	6.0
X	–	–	–	–	13.5	4.9	24.1	3	-2.3	23	6.5	12.5	8.1	8.8	9.4	10.6	9.9	10.0	94	73	90	86	0.6	4.6	1.2	2.1	8.1	6.6	4.9	6.5
XI	–	–	–	–	6.3	2.0	16.8	8	-1.5	21	3.0	5.7	3.7	4.0	7.1	7.8	7.2	7.4	92	84	89	88	0.6	1.8	0.9	1.1	9.1	8.4	7.9	8.5
XII	–	–	–	–	-1.2	-6.2	7.9	12	-16.7	22	-3.9	-2.1	-3.7	-3.4	4.3	4.4	4.2	4.3	87	80	86	84	0.6	1.2	0.7	0.8	8.5	8.0	6.7	7.7
Rok	–	–	–	–	11.8	3.9	32.9	26.VII	-16.7	22.XII	6.1	10.6	7.2	7.8	8.9	9.0	9.0	9.0	86	68	82	79	1.6	6.0	2.4	3.3	7.4	7.6	6.8	7.3

Ostrów Wlkp. $\varphi = 51°39'$ $\lambda = 17°49'$

I	–	–	–	–	2.7	-1.9	9.1	22	-15.5	31	0.2	2.0	0.3	0.7	–	–	–	–	–	–	–	–	–	–	–	–	7.1	8.2	7.4	7.6
II	–	–	–	–	1.3	-3.7	6.9	12	-13.8	1	-2.5	0.3	-1.1	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.9	6.8	8.2
III	–	–	–	–	3.4	-3.2	15.0	31	-10.3	8	-2.0	2.5	-0.1	0.1	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.5	7.5	7.4
IV	–	–	–	–	16.3	6.4	28.4	23	1.4	30	8.5	15.1	10.2	11.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.0	5.1	6.4
V	–	–	–	–	15.7	7.2	22.9	8,19	-1.8	1	9.5	14.1	10.4	11.1	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.0	7.4	7.6
VI	–	–	–	–	20.8	–	32.1	16	–	–	13.7	19.4	14.7	15.6	–	–	–	–	–	–	–	–	–	–	–	–	4.7	6.6	5.1	5.5
VII	–	–	–	–	21.3	–	32.3	26	–	–	14.5	20.0	15.2	16.2	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.8	6.5	6.4
VIII	–	–	–	–	22.8	–	32.3	13	–	–	15.4	21.6	16.0	17.2	–	–	–	–	–	–	–	–	–	–	–	–	5.8	7.3	5.1	6.1
IX	–	–	–	–	18.3	–	30.8	4	–	–	10.5	17.0	11.8	12.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.6	5.2	6.0
X	–	–	–	–	13.4	4.6	22.5	2	-2.6	16	6.0	12.6	7.3	8.3	–	–	–	–	–	–	–	–	–	–	–	–	7.5	5.0	5.7	6.1
XI	–	–	–	–	6.4	2.0	15.0	5	-4.1	26	3.3	5.8	3.9	4.2	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.3	7.2	7.6
XII	–	–	–	–	-1.4	-6.0	6.6	12	-18.1	22	-4.7	-2.2	-3.8	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.3	7.1	7.4
Rok	–	–	–	–	11.8	–	32.3	26.VII	-18.1	22.XII	6.0	10.7	7.1	7.7	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.2	6.3	6.8

Żary $\varphi = 51°38'$ $\lambda = 15°08'$

I	–	–	–	–	3.3	-1.2	9.9	22	-11.9	31	0.3	2.4	0.7	1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.7	7.8	7.8
II	–	–	–	–	2.1	-3.1	7.9	12	-12.8	1	-1.5	0.9	-1.0	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.8	7.8	8.6
III	–	–	–	–	4.3	-3.3	15.4	30	-9.5	7	-2.1	2.9	-0.4	0.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.1	6.5	6.8
IV	–	–	–	–	15.3	4.8	28.0	23	-1.0	5	7.0	13.8	9.1	9.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.9	5.5	6.3
V	–	–	–	–	15.2	6.3	22.9	19	-1.6	1	8.7	13.7	9.8	10.5	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.8	6.5	7.2
VI	–	–	–	–	20.7	9.3	31.2	15,16	1.4	6	13.3	19.3	14.1	15.2	–	–	–	–	–	–	–	–	–	–	–	–	4.9	6.6	5.2	5.6
VII	–	–	–	–	20.8	10.3	32.3	26	6.8	4,10	13.8	19.3	14.6	15.6	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.1	5.6	6.4
VIII	–	–	–	–	21.5	11.9	30.0	13	7.9	27	14.5	19.9	15.4	16.3	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.6	7.5	7.3
IX	–	–	–	–	17.7	7.6	29.4	4	2.3	25	9.7	16.2	11.1	12.0	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.0	3.6	5.6
X	–	–	–	–	13.7	5.2	24.9	3	-2.5	23	6.5	13.0	8.2	9.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	5.4	4.9	5.9
XI	–	–	–	–	6.1	1.1	16.9	8	-3.9	25	2.4	5.5	3.0	3.5	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.2	7.5	7.7
XII	–	–	–	–	-1.5	-6.6	6.5	12	-19.4	23	-4.5	-2.7	-4.5	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.5	7.0	7.4
Rok	–	–	–	–	11.6	3.5	32.3	26.VII	-19.4	23.XII	5.7	10.4	6.7	7.4	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.2	6.3	6.9

Smolice $H_s = 107 m$ $h_w = 15 m$ 1962

MIESIĄC	ROZKŁAD WIATRU °D, V m/s: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n) Temperatura T: Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr: v > 10	v > 15	◑	●	Opad R: R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R/K
I	4	4.2	2.5	3.4	·		3.5	3.1	22.5	4.5	33.5	2.8	11.5	4.1	11.5	3.0	4	3.4	35	8.3	24	3	5	19	·	·	·	1	16	13	10	·	2	11	·
II	7	3.6	7.5	3.2	10.5	2.9	3.5	2.4	7	2.5	11.5	5.5	14	4.2	11	4.5	12	3.3	35	10.2	12	2	10	24	·	3	·		16	18	7	1	1	18	
III	9.5	4.9	14	2.9	8	2.9	15.5	3.1	11	2.8	4	3.4	7.5	3.3	8.5	2.7	15	2.7	31	13.3	5	1	4	26	·	·	·	·	15	11	6	1	4	10	
IV	4.5	3.1	12	3.1	5	4.4	4.5	5.2	8	4.6	10	5.6	13	2.8	11	3.3	22	2.9	20	6.1	13	·	·	1	6	1	·	2	12	8	5	·	·		1
V	3	2.3	3.5	2.6	4.5	2.2	7.5	2.4	5.5	2.0	18	2.7	24.5	2.9	13.5	2.5	13	2.2	107	33.7	14	·	·	1	·	·	·	·	11	23	18	2		·	6
VI	13	3.8	8.5	2.2	·	·	3.5	2.4	3.5	3.6	14	2.2	20	3.3	13.5	3.5	14	2.6	31	17.2	16	·	·	·	7	·	·	3	7	8	7	1		·	2
VII	5.5	1.8	5.5	2.0	1	2.0	1	1.0	5	1.8	18.5	2.4	20.5	2.1	3	1.5	33	1.3	71	12.8	13	·	·	·	7	·	·	4	11	11	11	2	2	·	6
VIII	3	2.0	1	4.0	4	1.2	1	1.0	8	2.0	15	3.1	23	3.0	8	2.6	30	1.8	52	14.9	13	·	·	·	6	·	·	2	11	13	11	1	·		2
IX	1	2.0	1	2.0	9	2.3	5	2.2	4	4.2	11.5	1.8	21	3.1	4.5	2.4	33	1.7	59	21.1	18	·	·	·	3	·	·	6	7	12	10	1	5		
X	3.5	2.6	6	2.0	10.5	2.0	5	1.6	10	2.5	9	2.0	8.5	2.6	6.5	2.8	34	1.4	42	12.8	31	·	·	6		·		3	11	8	6	1	15	·	
XI	5	3.4	5.5	5.5	19.5	3.2	10.5	3.3	4.5	2.7	15	2.3	10.5	2.8	4.5	2.2	15	2.6	55	15.9	1	·	·	8	·			2	19	14	8	1	7	1	·
XII	9	3.0	18	3.6	5	1.2	3	2.7	10.5	4.7	18	3.1	14	3.0	3.5	1.4	12	2.8	16	9.6	15	11	14	26			·	3	17	7	4	·	4	17	
Rok	68	3.1	85	3.0	77	2.0	63.5	2.5	99.5	3.2	178	3.1	188	3.1	99	2.7	237	2.4	554	33.7	14.V	17	33	111	29	4		26	153	146	103	11	40	57	17

Głogów $H_s = 112 m$ $h_w = 10 m$

I	6	3.3	1	1.0	1.5	2.7	2.5	2.4	6.5	2.5	28	6.2	30.5	5.9	13	6.5	4	5.2	26	9.9	24	1	4	14	·	6	·	1	14	13	9	·	-	3	
II	3	5.0	12.5	4.6	4	3.6	0.5	5.0	4	2.8	11	7.7	23.5	8.1	20.5	7.9	5	6.4	35	7.2	16	2	8	23	·	7	4		19	14	9	·	-	11	
III	4	4.1	11.5	3.2	4	4.6	12	4.5	4	3.9	6	4.2	14.5	3.6	19	4.4	18	3.2	28	13.2	5	·	2	28		·	·	·	13	7	5	1	-	11	
IV	6	3.6	9.5	3.6	1	3.5	6	6.7	4.5	5.6	12	5.4	19	4.3	20	3.8	12	3.9	27	6.8	28		·	·	5	1	·	3	11	14	9		-	·	2
V	15	3.0	1	3.0	1	6.0	2.5	4.4	2.5	3.2	9	4.4	34	4.9	29.5	4.3	12	3.9	112	17.9	25	·	·	1	·	3	1	·	17	22	17	4	-	·	5
VI	7	5.7	2.5	2.8	0.5	2.0	2	4.5	4	3.0	2	5.8	30.5	4.5	35.5	3.7	6	3.9	16	3.2	3	·	·	·	8	3	1	2	8	9	7		-		2
VII	4	1.7	1.5	1.7	2.5	1.4	·	·	1	4.0	5.5	6.1	36	3.5	26.5	2.8	16	2.7	46	15.0	21	·	·	·	7	·	·	1	10	11	11	2	-	·	4
VIII	2	2.0	1	2.0	2	2.5	1	3.0	1	7.0	13	4.9	40.5	4.2	20.5	3.6	12	3.5	57	15.0	13	·	·	·	6	·	·	·	17	10	9	3	-	·	2
IX	·	·	5.5	2.9	10.5	2.9	1	3.0	·	·	8	5.0	33.5	3.8	21.5	3.3	10	3.2	50	16.2	18	·	·	·	3	1	·	3	9	9	6	2	-		
X	4	1.2	3.5	2.3	7.5	2.2	5	2.7	5	2.6	4	3.0	19	3.4	24	2.3	21	2.0	14	5.0	27	·		4	·			3	15	6	3	·	-	·	
XI	2	2.5	18	4.3	12.5	2.9	7	7.6	1	4.0	3.5	1.9	28	3.7	13	2.7	5	3.6	29	14.2	1	·		7		3	·	1	19	11	7	1	-	·	
XII	4.5	1.6	16	3.6	7.5	2.6	1	5.0	1.5	7.3	17.5	8.7	30.5	4.4	8.5	4.2	6	4.5	23	8.9	15	10	15	26		5	2	3	18	11	4	·	-	16	
Rok	44	2.8	83.5	2.9	54.5	3.1	40.5	4.1	35	3.8	119.5	5.3	339.5	4.5	251.5	4.1	127	3.8	463	17.9	25.V	13	29	103	29	29	8	17	170	137	96	13	-	41	15

Ostrów Wlkp. $H_s = 126 m$ $h_w = 11 m$

I	2.5	5.8	4.5	4.9	3.5	3.7	4	4.6	23.5	4.0	23.5	4.3	12.5	4.9	8	3.8	11	3.8	29	6.3	24	1	6	17		·	·	1	14	16	9	·	1	15	
II	9.5	7.7	6.5	5.2	10	4.2	5	4.4	13	4.3	9	6.1	13	7.4	10	8.2	8	5.5	53	17.2	12	3	10	23		6	2	·	16	18	10	2	2	20²	1
III	6.5	5.9	8.5	5.6	13.5	3.3	11.5	4.5	8.5	3.7	6	3.7	5	4.8	11.5	5.3	22	3.5	42	11.5	12	1	5	24	·	4	1	1	18	10	6	2	4	12²	
IV	3	5.2	5.5	3.6	9.5	5.5	5	4.5	14	4.8	13	4.6	4.5	5.0	9.5	4.5	26	3.4	28	7.4	4	·	·	·	8	5	·	4	10	11	6	·	2		1
V	3	7.2	0.5	3.0	3.5	2.7	8.5	2.9	10	3.2	18	3.8	5.5	4.1	18	5.6	26	3.0	77	21.9	14		·	1		2	·		13	23	16	1			6
VI	7.5	4.5	5.5	4.1	0.5	2.0	6	2.7	7.5	2.7	12.5	2.6	15	5.2	14.5	4.5	21	3.0	17	3.3	3			·	9	1	·	4	7	11	6	·		·	4
VII	0.5	5.0	1	3.5	4	3.1	5.5	2.2	15	2.6	19.5	3.5	8.5	4.2	10	3.9	29	2.3	65	20.0	22			·	8	·	·	3	12	14	11	2		·	7
VIII	0.5	7.0	2.5	2.2	1.5	2.3	5	2.8	19.5	3.2	23.5	4.1	15.5	5.7	4	4.0	21	3.1	40	7.4	13	·	·	·	10	3		3	12	15	11	·	1	·	6
IX	2	4.2	0.5	4.0	7	4.2	9	3.6	10	4.0	16.5	3.5	6.5	5.8	12.5	4.1	26	2.9	45	20.6	18			-	4	2	1	5	9	12	9	1	5		
X	3	3.2	3	3.0	4	3.5	7	3.8	9	2.6	13	3.6	2.5	3.8	9.5	3.3	42	1.8	30	13.9	31	·		5		·	·	3	10	9	6	1	13	·	
XI	3.5	3.1	7	4.8	13.5	4.1	18	4.6	4	2.9	12.5	3.4	4.5	4.9	3	4.3	24	3.0	45	10.5	20	·	·	8		·		2	17	15	8	1	11	·	
XII	2	3.2	10	2.9	14	3.2	4.5	3.6	9.5	4.9	22.5	4.1	3.5	3.9	5	3.8	22	2.9	22	13.8	15	11	13	26		1	·	3	17	8	5	1	-	17	
Rok	43.5	5.2	55	3.9	84.5	3.5	89	3.7	143.5	3.6	189.5	3.9	96.5	5.0	115.5	4.6	278	3.2	493	21.9	14.V	16	34	-	39	24	4	29	155	162	103	11	-	64²	25

Żary $H_s = 162 m$ $h_w = 20 m$

I	3.5	6.0	5	2.9	1.5	2.7	·	·	20.5	6.6	27	6.4	28	6.9	5.5	5.3	2	6.1	52	14.1	24	1	6	14	·	16	8	·	17	19	13	1	6	5	·
II	7	5.2	4	3.9	11.5	4.4	3.5	5.1	6	3.6	14	7.7	26	6.9	12	8.5	·	6.3	50	11.3	12	1	10	21	·	9	6	·	20	20	11	1	2	16	
III	5	3.0	8	2.9	14	3.0	7	4.9	17	3.9	13	4.2	13.5	3.9	10.5	5.3	5	3.7	34	7.7	5	·	2	26	·	3	·	2	15	15	9	·	5	10	
IV	6	3.3	5	5.4	10	4.2	5.5	3.7	10	4.0	17	5.0	18	5.6	15.5	4.4	3	4.5	45	7.8	29		·	1	4	5	·	3	12	16	11	·	·		2
V	7	3.7	2.5	2.0	4.5	2.9	2.5	3.2	9.5	3.5	22	3.5	30	3.8	11	4.0	4	3.4	151	32.7	8		·	1		3	·	·	13	23	19	5	4	·	7
VI	10.5	3.0	4.5	3.0	3	2.7	0.5	3.0	5	3.5	11.5	3.3	32.5	4.0	19.5	3.8	3	3.5	22	6.5	28			·	8	4	·	3	6	10	7	·		·	3
VII	4	2.5	5.5	2.8	2.5	2.6	6.5	2.1	7.5	3.1	17.5	4.4	29	3.5	12.5	2.5	8	3.0	65	16.6	16		·	·	4	3	·	2	10	15	12	2		·	4
VIII		·	4.5	2.4	4	1.6	1.5	2.3	11	3.4	25.5	4.6	33	4.5	5.5	2.5	8	3.6	91	30.1	13		·	·	6	4	·	1	15	16	12	3	2	·	2
IX	2	4.2	0.5	2.0	9.5	2.9	7	2.4	9.5	3.8	19.5	4.8	26	4.3	7	4.1	9	3.6	74	15.9	19			·	3	2	·	5	7	16	15	1	6	·	2
X	1	2.0	2	3.5	7.5	4.0	10	2.1	13.5	4.8	10.5	3.2	19	4.0	10.5	4.1	19	3.0	19	12.7	31		·	4		2	·	4	9	12	3	1	16	·	·
XI	2.5	1.4	2.5	2.2	14.5	4.1	11	5.0	12	2.9	11	3.2	17.5	3.3	5	2.4	14	2.9	28	6.8	1	·	1	13	·	2	·	1	17	14	8	·	14	1	
XII	3.5	2.3	8.5	2.8	14.5	4.9	6	3.0	12.5	4.3	19	4.9	17	5.2	4	2.1	8	3.9	51	17.2	15	9	16	26	·	6	1	2	17	12	9	1	8	17	·
Rok	52	3.0	52.5	3.0	97	3.3	61	3.1	134	4.0	207.5	4.6	289.5	4.7	118.5	4.1	83	4.0	682	32.7	8.V	11	35	106	25	59	15	23	158	188	129	15	63	49	20

Nowe Miasto n.P. $\varphi = 51°37'$ $\lambda = 20°35'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																		
	P_m	Max	Min	$P_{e.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1,9	–	9,0	22	–	–	-1,0	0,7	-0,5	-0,3	–	–	–	–	–	–	–	–	–	–	–	–	7,3	6,3	6,5	6,7
II	–	–	–	–	0,0	-5,0	5,0	13	-14,9	1	-3,8	-1,2	-2,3	-2,4	–	–	–	–	–	–	–	–	–	–	–	–	10,0	8,7	7,7	8,8
III	–	–	–	–	1,9	–	13,6	31	–	–	-4,5	0,8	-1,7	-1,8	–	–	–	–	–	–	–	–	–	–	–	–	7,7	7,0	6,0	6,9
IV	–	–	–	–	16,2	6,1	28,0	23	0,1	8	7,6	14,7	10,3	10,7	–	–	–	–	–	–	–	–	–	–	–	–	6,9	6,4	5,8	6,4
V	–	–	–	–	15,2	7,1	22,7	8	-1,9	1	9,0	13,4	10,6	10,9	–	–	–	–	–	–	–	–	–	–	–	–	8,1	8,6	7,0	7,9
VI	–	–	–	–	19,2	9,9	30,2	16	5,0	2,7,8	12,8	17,6	14,2	14,7	–	–	–	–	–	–	–	–	–	–	–	–	5,6	5,7	5,5	5,6
VII	–	–	–	–	21,8	11,0	31,7	26	7,2	4	14,2	20,0	15,1	16,1	–	–	–	–	–	–	–	–	–	–	–	–	5,7	6,3	6,3	6,1
VIII	–	–	–	–	22,2	–	30,7	7,13	–	–	14,3	20,3	16,1	16,7	–	–	–	–	–	–	–	–	–	–	–	–	6,4	7,2	4,7	6,1
IX	–	–	–	–	17,4	9,6	27,7	4	0,8	25	9,5	16,0	11,7	12,2	–	–	–	–	–	–	–	–	–	–	–	–	6,1	6,8	5,1	6,0
X	–	–	–	–	13,3	3,3	20,2	2	-3,7	16	4,7	12,0	7,2	7,8	–	–	–	–	–	–	–	–	–	–	–	–	9,0	5,7	3,7	6,1
XI	–	–	–	–	6,1	1,8	13,9	1	-2,2	18,24	3,0	5,0	3,5	3,8	–	–	–	–	–	–	–	–	–	–	–	–	9,1	8,6	8,5	8,7
XII	–	–	–	–	-2,1	-8,2	4,5	12	-22,9	22	-5,6	-4,0	-5,6	-5,2	–	–	–	–	–	–	–	–	–	–	–	–	8,9	7,7	7,4	8,0
Rok	–	–	–	–	11,1	–	31,7	26.VII	-22,9	22.XII	5,0	9,6	6,6	7,0	–	–	–	–	–	–	–	–	–	–	–	–	7,6	7,1	6,2	7,0

Sieradz $\varphi = 51°36'$ $\lambda = 18°44'$

I	–	–	–	–	2,1	-2,0	8,6	22	-14,7	31	-0,7	1,2	-0,3	0,0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	0,6	-4,6	4,8	20	-13,6	3	-2,9	-0,7	-1,8	-1,8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	2,8	-3,8	14,7	31	-9,6	15	-2,2	1,8	-0,8	-0,5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	15,7	5,8	27,8	23	1,3	1,3,6	8,1	14,2	9,7	10,4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15,4	6,6	22,6	8	-1,4	1	9,7	13,8	10,1	10,9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	20,2	9,1	31,0	16	2,6	3	13,5	18,4	13,5	14,7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21,5	10,3	31,2	26	5,5	29	14,6	20,0	14,4	15,8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	22,6	12,4	31,7	13	8,5	31	15,2	21,3	15,2	16,7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	17,9	7,5	29,6	4	2,3	15	10,5	16,6	10,7	12,1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	13,5	3,6	22,0	1	-2,9	24	5,8	12,3	6,7	7,9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6,1	2,1	15,6	8	-2,9	24	3,2	5,3	3,8	4,0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-2,2	-7,0	4,6	12	-18,4	22	-5,1	-3,0	-4,7	-4,4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	11,4	3,3	31,7	13.VIII	-18,4	22.XII	5,8	10,1	6,4	7,2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Sobieszyn $\varphi = 51°36'$ $\lambda = 22°10'$

I	–	–	–	–	1,3	-3,1	6,6	22	-19,6	31	-1,5	0,0	-1,0	-0,9	4,9	5,2	5,0	5,0	86	83	85	85	0,7	1,1	0,9	0,9	8,2	7,8	7,0	7,7
II	–	–	–	–	-0,7	-6,5	4,7	13	-16,0	1	-4,6	-2,2	-3,0	-3,2	3,8	4,4	4,4	4,2	84	83	88	85	0,7	0,9	0,6	0,7	9,1	9,0	8,4	8,8
III	–	–	–	–	0,8	-6,2	9,7	31	-16,6	26	-4,7	-0,6	-2,4	-2,5	3,9	4,7	4,6	4,4	84	78	85	82	0,7	1,4	0,7	0,9	8,6	7,4	6,6	7,5
IV	–	–	–	–	15,8	6,2	26,1	22	0,0	3,8	7,9	14,4	10,2	10,7	9,1	9,0	9,7	9,3	84	57	76	72	1,9	8,8	3,4	4,7	7,2	6,6	2,9	5,6
V	–	–	–	–	15,2	7,1	21,8	28	-1,4	1	9,2	14,1	10,6	11,1	10,6	10,9	11,1	10,9	89	67	85	80	1,3	5,6	2,0	3,0	8,5	8,4	5,7	7,5
VI	–	–	–	–	18,5	9,7	28,1	16	3,5	6	12,8	17,0	13,7	14,3	12,2	11,4	12,1	11,9	81	60	76	72	3,1	9,1	4,3	5,5	6,7	7,2	7,0	7,0
VII	–	–	–	–	20,8	11,2	28,3	22	5,9	5	14,0	19,5	15,0	15,9	13,6	13,1	13,9	13,5	85	58	81	75	2,6	10,1	3,4	5,4	6,3	6,9	6,0	6,4
VIII	–	–	–	–	21,6	12,4	29,3	13	7,7	10,27,29	14,4	20,0	16,2	16,7	14,6	14,8	15,3	14,9	88	64	82	78	2,0	9,1	3,6	4,9	6,9	6,7	4,8	6,1
IX	–	–	–	–	16,8	8,0	26,8	5	2,3	25	9,3	15,4	11,4	11,9	10,7	11,5	11,6	11,3	90	67	86	81	1,3	6,6	2,1	3,3	7,5	7,0	4,8	6,4
X	–	–	–	–	12,2	3,5	18,8	2	-3,0	16	4,8	11,0	7,2	7,6	8,3	9,8	9,1	9,1	95	73	88	85	0,5	3,7	1,2	1,8	8,7	7,0	4,0	6,6
XI	–	–	–	–	6,1	1,8	16,9	1	-2,3	17	2,9	5,2	3,8	3,9	7,1	7,5	7,2	7,3	92	83	88	88	0,6	1,8	1,0	1,1	9,3	8,6	8,1	8,7
XII	–	–	–	–	-2,5	-7,7	3,5	13	-20,6	21	-5,5	-4,0	-5,2	-5,0	3,7	4,0	3,8	3,8	84	81	83	83	0,6	0,8	0,7	0,7	9,1	8,2	7,5	8,3
Rok	–	–	–	–	10,5	3,0	29,3	13.VIII	-20,6	21.XII	4,9	9,2	6,4	6,7	8,5	8,9	9,0	8,8	87	71	84	81	1,3	4,9	2,0	2,7	8,0	7,6	6,1	7,2

Szprotawa $\varphi = 51°34'$ $\lambda = 15°32'$

I	–	–	–	–	3,8	-1,5	9,9	22	-15,8	31	0,7	3,0	1,2	1,5	5,4	5,5	5,4	5,4	82	72	79	78	1,3	2,3	1,6	1,7	8,0	8,4	7,9	8,1
II	–	–	–	–	2,2	-3,3	8,4	12	-14,5	1	-1,1	1,4	-0,8	-0,3	4,9	5,3	5,0	5,1	84	77	85	82	0,9	1,7	0,9	1,2	9,6	9,2	7,9	8,9
III	–	–	–	–	4,3	-3,6	17,0	30	-10,7	7	-2,0	3,2	-0,1	0,2	4,7	5,1	5,0	4,9	84	66	81	77	0,9	2,8	1,2	1,6	7,8	8,0	6,1	7,3
IV	–	–	–	–	15,9	4,3	27,7	24	-2,8	11	7,1	14,3	9,3	10,0	8,6	8,5	9,0	8,7	83	54	75	71	2,0	9,6	3,7	5,1	6,8	7,5	5,7	6,7
V	–	–	–	–	15,6	6,2	23,6	19	-2,4	1	9,2	14,0	9,9	10,8	10,0	10,2	10,4	10,2	84	63	84	77	1,9	6,3	2,0	3,4	7,7	8,5	7,1	7,8
VI	–	–	–	–	21,1	8,6	32,0	16	1,0	8	13,3	19,8	14,1	15,3	11,6	11,2	12,3	11,7	74	47	74	65	4,3	13,4	4,4	7,4	5,7	7,3	5,4	6,1
VII	–	–	–	–	21,6	10,1	33,2	26	5,1	9	13,9	20,0	15,0	16,0	13,3	13,2	14,3	13,6	83	58	83	75	2,8	11,4	3,1	5,8	6,2	7,8	6,3	6,8
VIII	–	–	–	–	22,2	11,5	31,5	13	6,1	27	14,4	20,8	15,5	16,6	14,1	14,5	14,8	14,5	85	59	83	76	2,5	10,8	3,1	5,5	6,8	8,3	6,2	7,1
IX	–	–	–	–	18,3	7,1	30,2	4	1,3	15	9,3	17,3	11,1	12,2	10,9	11,8	11,3	11,3	92	61	86	80	1,0	8,7	2,2	4,0	7,6	6,3	4,4	6,1
X	–	–	–	–	13,9	4,1	24,1	2,3	-3,9	23	5,7	13,1	7,3	8,4	8,9	11,2	9,7	9,9	94	73	91	86	0,6	4,6	1,0	2,1	7,9	6,1	4,5	6,2
XI	–	–	–	–	6,6	1,2	17,7	8	-4,0	21	2,8	6,1	3,5	4,0	7,0	7,9	7,2	7,4	92	83	90	88	0,7	2,0	0,9	1,2	8,7	8,1	7,6	8,1
XII	–	–	–	–	-1,2	-7,0	7,6	12	-20,2	23	-4,6	-2,2	-4,2	-3,8	4,1	4,5	4,1	4,2	85	80	85	83	0,7	1,1	0,7	0,8	8,9	8,0	7,2	8,0
Rok	–	–	–	–	12,0	3,1	33,2	26.VII	-20,2	23.XII	5,7	10,9	6,8	7,6	8,6	9,1	9,0	8,9	85	66	83	78	1,6	6,2	2,1	3,3	7,6	7,8	6,4	7,3

Nowe Miasto n.P. $H_S = 155 m$ $h_W = 13,5 m$ 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v>10	v>15	◔	●	Opad R≥0,1	R≥1,0	R≥10,0	≡	⊠	⊓
I	3.5	13.6	4.5	3.0	1.5	1.0	1	5.0	10	3.2	32.5	2.5	27	4.4	13	4.7	·	3.9	25	6.0	12	–	8	–	·	5	2	3	12	12	9	·	·	–	·
II	2.5	4.8	6.5	1.9	12	1.9	4.5	1.7	4	3.0	16.5	2.7	19	5.3	19	8.7	·	4.5	40	15.5	12	3	13	24		7	3	·	20	16	8	1	·	–	
III	11	5.6	12	1.6	7	2.3	9.5	2.1	7.5	2.3	17	2.2	10.5	3.9	18.5	3.2	·	2.9	47	14.0	31	–	12	–	·	4	1	4	16	14	12	2	2	–	
IV	11	2.1	9	5.7	8	4.0	8	3.2	6	2.4	18	2.0	8	2.2	22	3.1	·	3.0	64	28.5	26	·	·	·	6	3	1	5	13	13	12	1	·	·	2
V	6.5	1.0	3.5	1.0	5	1.0	3	1.0	6.5	1.1	28.5	1.5	22.5	4.7	17.5	1.3	·	2.1	148	42.0	14	·	·	2	·	2	2	1	18	24	21	3	2	·	5
VI	12.5	4.8	7.5	1.5	2	1.2	4.5	1.3	0.5	3.0	7.5	2.9	25	3.3	30.5	3.3	·	3.2	85	26.0	4	·	·	·	7	3	·	8	12	11	11	2	·	·	2
VII	3	1.7	6.5	2.4	1.5	1.0	3.5	1.9	2.5	2.2	17	1.7	25	1.9	34	1.9	·	1.9	35	9.5	27	·	·	·	6	·	·	3	8	11	9	·	·	·	4
VIII	1.5	1.3	0.5	1.0	1.5	1.0	4	2.5	4.5	1.7	24	1.6	32.5	2.5	24.5	2.1	·	2.1	88	25.0	15	·	·	·	6			3	9	14	12	3	1	·	3
IX	0.5	2.0	2	1.0	8.5	1.8	6	1.4	10	1.5	19.5	2.4	25	2.2	18.5	2.3	·	2.0	70	34.5	17	·	·	·	2	·	·	5	9	16	11	2	5	·	1
X	8	1.3	14	1.6	14	1.3	18	1.4	11.5	1.5	8	1.4	8.5	2.6	11	1.3	·	1.5	13	5.8	27	·	·	7	·	·	·	1	8	6	3	·	16	·	
XI	6	1.0	3	2.8	19.5	2.6	25	2.2	6.5	1.4	8	1.2	8	2.0	14	1.7	·	2.0	36	8.1	15	·	·	8	·	·	·	·	21	16	9	·	5	–	
XII	8.5	1.2	13.5	1.9	5	1.4	12	1.2	10.5	2.1	19.5	1.9	15.5	1.9	8.5	1.4	·	1.7	24	4.7	13	11	15	28	·	·	·	·	19	9	8	·	5	–	
Rok	74.5	3.4	82.5	2.1	85.5	1.7	99	2.1	80	2.1	216	2.0	226.5	3.1	231	2.9	·	2.6	675	42.0	14.V	–	48	–	27	24	9	33	165	162	125	14	36	–	17

Sieradz $H_S = 137 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	◔	●	R≥0,1	R≥1,0	R≥10,0	≡	⊠	⊓
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	24	6.4	25	1	6	19	·	–	–	–	–	15	9	·	·	–	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	77	41.6	12	4	12	24	·	–	–	–	–	15	9	1	·	–	1
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	37	13.2	5	·	8	26	·	–	–	–	–	11	7	2	2	–	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	40	9.3	29	·	·	·	6	–	–	–	–	13	8	·	·	·	2
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	94	27.4	14	·	·	2	·	–	–	–	–	23	17	1	·	·	·
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	29	8.5	30	·	·	·	6	–	–	–	–	11	8	·	·	·	3
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	28	6.1	15	·	·	·	5	–	–	–	–	11	7	·	·	·	5
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	56	13.4	17	·	·	·	8	–	–	–	–	17	10	1	2	·	3
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	65	19.6	17	·	·	·	4	–	–	–	–	12	8	3	4	·	·
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	18	5.2	31	·	·	7	·	–	–	–	–	7	5	·	8	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	41	9.4	15	·	·	8	·	–	–	–	–	11	8	·	4	–	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	14	6.4	15	10	15	27	·	–	–	–	–	8	4	·	2	–	
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	523	41.6	12.II	15	41	113	29	–	–	–	–	154	100	8	22	–	14

Sobieszyn $H_S = 159 m$ $h_W = 13 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	◔	●	R≥0,1	R≥1,0	R≥10,0	≡	⊠	⊓
I	3	5.0	5.5	3.0	1	1.0	1	1.0	8	2.4	44.5	1.9	27	2.9	3	2.0	·	2.4	23	7.0	25	2	9	23	·	·	·	·	18	14	7	·	–	18	·
II	9	2.3	4.5	3.7	15.5	2.7	2	1.5	4.5	2.7	15.5	5.2	21	4.8	6	5.6	6	3.7	31	8.2	12	6	15	28		4	·	·	21	16	9	·	–	28	1
III	15.5	3.7	11.5	1.6	17.5	1.3	10	2.8	11	1.3	4	3.4	13.5	3.3	4	2.0	6	2.2	41	8.4	12	6	13	29	·	2	·	1	14	12	10	·	–	24	·
IV	6.5	1.5	15	1.7	6	1.7	10	2.4	5	3.0	15	1.4	9	2.0	7.5	3.3	16	1.6	46	10.4	26	·	·	·	4	1	·	2	3	12	8	1	–	·	1
V	7	1.0	2	1.0	6.5	1.2	4.5	1.3	3	1.0	21	2.8	18	2.7	7	1.6	24	1.5	138	33.9	14	·	·	1	·	2	·	·	16	21	15	4	–	·	5
VI	16	2.8	1	1.0	3	1.0	1	1.0	3	1.0	15.5	2.1	22	2.8	8.5	2.1	20	1.8	116	29.8	4	·	·	·	5	·	·	2	13	13	10	5	–	·	2
VII	10.5	1.3	1.5	1.0	1.5	1.0	4	1.0	6.5	1.0	19.5	1.3	28.5	2.1	8	1.1	13	1.3	86	44.4	22	·	·	·	4	·	·	2	13	15	12	2	–	·	5
VIII	2	1.0	1.5	1.0	6	1.1	3.5	2.3	3.5	1.6	27.5	1.9	25	3.0	1	1.0	23	1.6	59	17.8	14	·	·	·	5	·	·	2	5	12	7	2	–	·	3
IX	1.5	1.0	8	1.0	8.5	1.2	2	1.0	4	1.0	31	2.7	23	2.9	3	1.3	9	2.0	64	22.5	18	·	·	·	2	·	·	3	9	15	12	2	–	·	1
X	6.5	1.0	2.5	1.0	18.5	1.1	6	1.5	1	1.0	13.5	2.1	15	1.9	3	2.0	27	1.1	5	2.2	14	·	·	4	·	·	·	1	10	15	1	·	–	·	·
XI	10.5	1.0	8.5	3.0	25	3.3	11.5	2.1	2.5	1.6	4.5	2.9	14.5	2.6	3	1.0	10	2.2	49	7.9	15	·	·	8	·	·	·	2	23	18	13	·	–	3	·
XII	11	1.6	12	2.2	4.5	1.4	4	1.5	9.5	2.5	22	2.9	18	1.7	4	2.0	8	2.0	13	3.2	14	11	17	31	·	·	·	1	20	13	4	·	–	18	·
Rok	99	1.9	73.5	1.8	113.5	1.5	59.5	1.6	61.5	1.7	233.5	2.6	234.5	2.7	58	2.1	162	2.0	671	44.4	22.VII	25	54	124	20	9	·	16	165	176	108	16	–	91	18

Szprotawa $H_S = 122 m$ $h_W = 14,5 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	◔	●	R≥0,1	R≥1,0	R≥10,0	≡	⊠	⊓
I	3.5	3.9	2	2.2	0.5	2.0	·	·	11	3.5	50.5	4.9	8	6.3	5.5	4.0	12	4.0	40	12.1	24	1	6	14	·	2	1	·	20	17	8	1	3	10	:
II	3.5	2.9	6.5	3.1	11.5	3.2	0.5	1.0	3	2.7	22.5	5.5	15	7.1	11.5	4.8	10	4.3	47	12.0	12	2	10	22	·	5	2	·	21	14	10	1	2	15	·
III	3	2.0	4	2.9	8	2.9	7.5	3.0	6	2.7	17.5	2.3	6.5	3.1	8.5	3.8	32	1.8	32	9.3	5	1	3	26	·	·	·	1	17	12	8	·	6	12	·
IV	2.5	1.4	6.5	2.5	9	3.4	7.5	3.7	8	2.2	19	4.1	8.5	4.5	9	4.1	20	2.8	47	10.7	16	·	·	3	5	1	·	2	13	15	10	1	3	·	1
V	1.5	1.3	1	1.0	2	4.0	8.5	1.9	4.5	2.6	28.5	2.9	15	4.1	7	2.6	25	2.2	96	16.5	8	·	·	2	·	·	·	·	16	21	16	3	1	·	3
VI	8	1.8	2	3.0	5	2.6	1.5	1.3	3	1.3	12.5	3.7	19	4.0	8	2.6	31	2.0	30	18.5	16	·	·	·	8	1	1	4	9	8	4	1	·	·	2
VII	1.5	1.0	4	2.2	2.5	1.4	1	1.0	4	1.9	30	2.7	13.5	3.3	3.5	2.9	33	1.7	34	8.6	13	·	·	·	8	·	·	1	12	12	8	·	2	·	6
VIII	1.5	1.0	3.5	2.4	1	1.0	2	2.0	6	2.3	36	3.6	14	4.2	1	3.0	28	2.4	74	26.5	13	·	·	·	7	·	·	1	12	16	11	2	5	·	3
IX	·	·	1	3.5	10	2.8	2	5.0	3	1.3	28	3.3	12	3.2	3	3.2	31	2.1	58	13.0	16	·	·	·	3	1	1	4	9	13	10	1	7	·	1
X	·	·	2	2.5	9.5	3.1	1.5	3.0	2	1.0	15.5	3.4	8.5	2.5	4	2.1	50	1.3	20	10.1	31	·	·	8	·	·	·	3	12	14	4	1	19	·	·
XI	1	4.5	7	4.4	12.5	3.6	10	3.6	1.5	1.3	23	4.3	2	4.5	3	2.7	30	2.6	25	9.4	1	·	·	10	·	·	·	1	18	13	7	·	14	·	·
XII	1.5	3.0	8	3.4	13.5	3.3	·	·	2.5	1.4	32	5.1	6.5	4.5	3	2.5	26	3.0	37	17.5	15	10	15	25	·	4	·	2	21	13	6	1	6	17	·
Rok	27.5	1.9	47.5	2.8	85	2.8	42	2.1	54.5	2.0	315	3.8	128.5	4.3	67	3.2	328	2.5	540	26.5	13.VIII	14	34	110	31	14	5	19	130	168	102	12	68	54	16

Włodawa $\varphi = 51°33'$ $\lambda = 23°33'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	994.4	1016.6	974.0	1016.6	1.2	-3.8	6.7	22	-20.2	31	-2.0	0.0	-1.3	-1.2	5.1	5.3	5.2	5.2	91	84	89	88	0.4	1.0	0.6	0.7	8.3	7.7	7.9	8.0
II	992.8	1010.3	960.2	1015.1	-1.4	-6.8	2.6	13	-15.3	1	-4.7	-2.3	-3.6	-3.6	4.1	4.4	4.3	4.3	91	83	90	88	0.4	0.9	0.5	0.6	9.0	9.1	8.7	8.9
III	989.4	1006.9	967.4	1011.7	0.7	-7.0	11.1	5	-19.6	26	-5.0	-0.4	-3.2	-3.0	4.1	4.7	4.4	4.4	91	77	87	85	0.4	1.4	0.6	0.8	8.3	7.2	7.7	7.7
IV	992.8	1007.4	971.2	1014.0	16.0	5.1	27.3	24	-1.4	2	7.3	14.6	9.6	10.3	9.2	9.4	9.7	9.4	88	59	79	75	1.5	8.8	2.9	4.4	7.1	6.6	5.2	6.3
V	994.2	999.6	977.4	1012.3	16.2	7.2	24.3	28	-0.8	3	10.0	14.5	10.9	11.6	11.4	11.7	11.8	11.6	91	69	88	83	1.2	5.5	1.6	2.8	7.3	8.4	6.6	7.4
VI	995.4	1004.8	986.0	1016.4	19.1	9.2	28.0	16	2.9	6	13.1	17.5	13.6	14.4	12.7	12.4	12.8	12.6	83	63	81	76	3.0	8.9	3.3	5.1	6.3	7.3	5.8	6.5
VII	992.8	1003.3	980.6	1013.6	21.1	10.8	29.5	27	6.0	2	14.4	19.6	14.9	16.0	14.3	14.1	14.6	14.3	86	63	85	78	2.4	9.3	2.6	4.8	6.0	6.9	5.5	6.1
VIII	994.7	1003.5	985.3	1015.5	22.5	11.7	30.7	13	5.9	27	14.6	20.8	16.1	16.9	14.8	14.6	15.4	14.9	88	60	83	77	2.0	10.6	3.3	5.3	6.5	6.8	5.1	6.1
IX	995.2	1010.2	979.7	1016.4	17.4	7.8	28.3	5	1.9	26	9.5	16.0	11.5	12.1	11.3	12.1	12.5	12.0	94	68	91	84	0.8	6.8	1.4	3.0	6.6	7.2	4.9	6.2
X	1004.1	1014.8	986.3	1022.7	12.8	2.6	19.9	2	-4.2	16	4.3	11.8	6.9	7.5	8.2	9.7	9.3	9.1	97	70	91	86	0.3	4.6	0.9	1.9	7.3	6.3	5.2	6.3
XI	997.1	1009.7	982.1	1018.9	7.0	2.1	19.3	1	-2.7	18	3.2	5.9	4.2	4.4	7.5	7.8	7.8	7.7	95	84	92	90	0.4	2.0	0.7	1.0	8.6	8.4	8.4	8.5
XII	994.7	1020.6	955.5	1017.2	-2.8	-8.6	3.2	1,13	-25.4	22	-5.9	-4.2	-5.7	-5.4	3.8	4.1	3.9	3.9	89	85	88	87	0.4	0.7	0.5	0.5	9.0	7.7	7.4	8.0
Rok	994.3	1020.6	955.5	1015.9	10.8	2.5	30.7	13.VIII	-25.4	22.XII	4.9	9.5	6.2	6.7	8.9	9.2	9.3	9.1	90	72	87	83	1.1	5.0	1.6	2.6	7.5	7.5	6.5	7.2

Wińsko $\varphi = 51°28'$ $\lambda = 16°37'$

I	-	-	-	-	3.0	-1.7	9.1	22	-13.4	31	0.3	1.9	0.2	0.6	-	-	-	-	-	-	-	-	-	-	-	-	6.6	7.5	7.5	7.2
II	-	-	-	-	1.8	-3.8	8.1	12	-14.3	1	-2.1	0.2	-0.7	-0.8	-	-	-	-	-	-	-	-	-	-	-	-	8.8	8.5	6.5	7.9
III	-	-	-	-	3.2	-3.3	15.1	30	-8.0	14	-1.9	1.9	-0.2	-0.1	-	-	-	-	-	-	-	-	-	-	-	-	6.7	6.8	6.1	6.5
IV	-	-	-	-	15.4	6.0	27.8	23	0.1	30	7.7	13.7	10.2	10.4	-	-	-	-	-	-	-	-	-	-	-	-	6.3	6.3	5.3	6.0
V	-	-	-	-	15.1	6.7	22.8	8	-2.5	1	8.9	13.8	10.4	10.9	-	-	-	-	-	-	-	-	-	-	-	-	7.1	7.6	7.2	7.3
VI	-	-	-	-	20.4	9.6	31.1	16	1.5	6	12.6	18.6	14.8	15.2	-	-	-	-	-	-	-	-	-	-	-	-	5.0	5.8	4.8	5.2
VII	-	-	-	-	20.9	11.3	31.9	26	6.9	4	13.7	19.3	15.5	16.0	-	-	-	-	-	-	-	-	-	-	-	-	5.9	6.3	4.8	5.7
VIII	-	-	-	-	22.1	12.9	31.6	13	9.2	30	14.8	20.4	17.0	17.3	-	-	-	-	-	-	-	-	-	-	-	-	5.7	7.2	5.9	6.3
IX	-	-	-	-	18.3	8.6	30.6	4	3.8	15,27	10.3	16.5	12.6	13.0	-	-	-	-	-	-	-	-	-	-	-	-	6.9	6.3	4.4	5.9
X	-	-	-	-	13.1	5.2	23.4	3	-0.6	23	6.7	11.9	8.4	8.8	-	-	-	-	-	-	-	-	-	-	-	-	6.5	5.0	4.0	5.2
XI	-	-	-	-	6.1	1.9	16.8	8	-2.3	25	3.0	5.6	3.7	4.0	-	-	-	-	-	-	-	-	-	-	-	-	8.1	7.7	7.6	7.8
XII	-	-	-	-	-1.8	-6.5	6.3	12	-19.0	23	-4.5	-2.9	-4.2	-4.0	-	-	-	-	-	-	-	-	-	-	-	-	7.8	7.7	6.0	7.2
Rok	-	-	-	-	11.5	3.9	31.9	26.VIII	-19.0	23.XII	5.8	10.1	7.3	7.6	-	-	-	-	-	-	-	-	-	-	-	-	6.8	6.9	5.8	6.5

Grabownica $\varphi = 51°28'$ $\lambda = 17°27'$

I	-	-	-	-	3.2	-1.9	8.9	22	-15.8	31	0.0	2.0	0.2	0.6	5.5	5.7	5.3	5.5	87	77	83	82	0.9	1.7	1.1	1.2	6.8	7.0	6.7	6.8
II	-	-	-	-	2.0	-3.9	7.1	20	-14.1	1	-2.2	0.5	-0.9	-0.9	4.5	5.2	5.1	4.9	84	80	86	83	0.9	1.2	0.8	1.0	9.2	8.5	6.1	7.9
III	-	-	-	-	3.4	-3.9	14.9	31	-10.1	9	-2.2	2.5	-0.6	-0.2	4.7	5.0	4.9	4.9	88	66	82	79	0.7	2.6	1.1	1.5	6.2	6.5	5.5	6.1
IV	-	-	-	-	15.7	4.8	27.4	23	0.4	11	7.7	14.3	9.4	10.2	9.4	9.3	10.1	9.6	88	59	84	77	1.4	8.9	2.3	4.2	7.0	6.3	4.9	6.1
V	-	-	-	-	15.3	6.1	23.0	8	-3.0	1	9.3	13.9	9.8	10.7	10.7	11.6	11.2	11.2	91	72	91	85	1.2	4.9	1.1	2.4	6.8	7.0	6.7	6.8
VI	-	-	-	-	20.2	8.7	30.7	16	1.5	8	13.2	18.7	13.6	14.8	12.4	11.9	12.7	12.3	80	54	80	71	3.3	11.0	3.4	5.9	-	-	-	-
VII	-	-	-	-	20.6	9.8	31.0	26	5.4	30	14.3	19.4	14.4	15.6	14.2	14.1	14.2	14.2	86	63	85	78	2.3	9.2	2.6	4.7	-	-	-	-
VIII	-	-	-	-	22.1	11.8	31.2	13	6.4	10	15.2	20.9	15.4	16.7	14.8	14.6	14.6	14.7	85	60	83	76	2.8	10.8	3.0	5.5	-	-	-	-
IX	-	-	-	-	18.0	7.0	30.5	4	-0.8	15	9.9	16.9	10.8	12.1	11.3	12.0	11.4	11.6	91	64	88	81	1.3	8.3	2.0	3.9	-	-	-	-
X	-	-	-	-	13.2	2.9	22.8	3,4	-4.8	23	5.3	12.7	6.5	7.8	9.0	11.0	9.5	9.8	97	75	95	89	0.3	4.3	0.6	1.7	-	-	-	-
XI	-	-	-	-	6.8	1.9	18.2	8	-2.6	25	3.1	6.3	3.6	4.2	7.4	8.2	7.7	7.8	96	86	96	93	0.3	1.8	0.4	0.8	-	-	-	-
XII	-	-	-	-	-1.3	-6.6	6.7	12	-18.4	23	-4.3	-2.0	-4.3	-3.7	4.3	4.8	4.3	4.5	88	85	89	87	0.4	0.8	0.5	0.6	8.7	6.9	6.7	7.4
Rok	-	-	-	-	11.6	3.1	31.2	13.VIII	-18.4	23.XII	5.8	10.5	6.5	7.3	9.0	9.4	9.2	9.2	88	70	87	82	1.3	5.5	1.6	2.8	-	-	-	-

Nowa Wieś $\varphi = 51°27'$ $\lambda = 22°45'$

I	-	-	-	-	1.4	-2.7	6.6	22	-19.4	31	-1.3	0.3	-0.8	-0.6	5.0	4.9	4.9	4.9	85	75	82	81	0.8	1.6	1.1	1.2	8.4	7.4	7.1	7.5
II	-	-	-	-	-1.0	-6.3	3.3	13	-14.8	1	-4.4	-2.1	-3.2	-3.2	3.9	4.2	4.2	4.1	83	79	83	82	0.7	1.1	0.8	0.9	9.0	9.1	8.0	8.7
III	-	-	-	-	0.8	-6.1	9.7	31	-17.2	26	-4.4	-0.5	-2.4	-2.4	3.9	4.1	4.3	4.1	80	68	80	76	0.8	1.9	1.0	1.2	7.9	7.1	7.1	7.4
IV	-	-	-	-	16.2	5.9	26.7	24	-0.3	30	8.0	14.7	10.1	10.7	9.0	8.7	9.2	9.0	83	55	74	71	2.1	9.4	3.8	5.1	6.6	5.8	4.2	5.5
V	-	-	-	-	15.6	7.0	22.5	28	-1.0	1	9.7	14.1	10.4	11.2	10.9	11.0	11.1	11.0	88	67	85	80	1.6	5.6	1.9	3.0	7.6	8.9	5.9	7.5
VI	-	-	-	-	18.8	9.3	28.3	16	3.3	6	13.3	17.5	13.2	14.3	12.3	11.7	12.3	12.1	79	59	79	72	3.7	9.5	3.5	5.6	6.5	7.4	5.7	6.5
VII	-	-	-	-	21.0	11.1	29.0	27	6.1	5	14.4	19.5	14.5	15.7	13.8	13.2	13.9	13.6	84	58	83	75	2.8	10.0	2.8	5.2	6.1	6.9	5.4	6.1
VIII	-	-	-	-	22.1	12.0	29.8	7	6.6	27	15.0	20.6	16.2	17.0	14.8	14.4	15.3	14.8	85	60	82	76	2.5	10.4	3.4	5.4	6.2	6.6	5.5	6.1
IX	-	-	-	-	17.1	7.9	26.9	5	3.3	15	9.7	15.6	11.4	12.0	10.8	11.4	11.7	11.3	89	66	86	80	1.5	7.0	2.1	3.5	6.2	7.5	5.4	6.4
X	-	-	-	-	12.3	3.3	19.2	2	-2.6	16	4.5	11.3	7.1	7.5	8.0	9.7	9.1	8.9	93	72	88	84	0.6	4.1	1.2	2.0	8.1	7.0	4.7	6.6
XI	-	-	-	-	6.6	2.2	18.9	1	-1.9	18	3.1	5.7	3.9	4.2	7.2	7.6	7.4	7.4	91	83	90	88	0.7	2.0	0.9	1.2	9.4	8.5	8.4	8.8
XII	-	-	-	-	-2.4	-7.5	3.1	13	-22.2	22	-5.5	-3.9	-5.0	-4.8	3.7	3.9	3.8	3.8	83	78	83	81	0.7	1.0	0.7	0.8	9.4	8.0	7.1	8.2
Rok	-	-	-	-	10.7	3.0	29.8	7.VIII	-22.2	22.XII	5.2	9.4	6.3	6.8	8.6	8.7	8.9	8.7	85	68	83	79	1.5	5.3	1.9	2.9	7.6	7.5	6.2	7.1

Włodawa — $H_s = 175\,m$ — $H_b = 175{,}9$ — $h_w = 13\,m$ — 1962

Miesiąc	Rozkład wiatru (%D, vmD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Liczba dni (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	≥15	◐	●	Opad R ≥0,1	≥10	≥100	≡	⊞	⊠
I	3	4,2	5	4,0	1,5	4,3	5	4,1	16	4,0	30	4,3	25	6,1	6,5	4,1	1	4,6	27	8,1	25	2	8	27	·	·	·	1	21	14	6		1	26	·
II	4,5	3,9	7	3,6	10	2,5	7	3,5	8	4,4	10,5	6,8	16	5,7	17	6,0	4	4,7	48	9,5	18	6	16	28	·	7	3	·	20	19	14		3	28	·
III	7	3,6	13,5	3,0	11,5	2,1	17,5	3,6	7,5	2,2	5	3,2	13	4,7	13	4,5	5	3,3	89	39,4	16	9	15	29	·	2	·	·	16	13	10	2	3	26	·
IV	3,5	4,1	12	2,6	15	2,4	13	2,7	9	2,9	9,5	3,3	9	4,8	10	3,3	9	3,8	60	12,6	7	·	·	4	5	1	·	3	9	12	11	2	1	·	·
V	5,5	2,2	2,5	2,4	5,5	2,3	6	2,6	7	2,5	13	3,5	26,5	3,5	18	2,4	9	2,6	100	18,5	14	·	·	3	·	3	1	·	12	20	13	4	2	·	5
VI	13,5	4,3	1,5	4,3	·	·	3	2,0	6,5	2,0	12	3,3	23	3,5	24,5	2,2	6	2,9	100	21,6	1	·	·	·	5	2	·	2	13	12	12	5	·	·	3
VII	11,5	1,7	1	3,5	0,5	2,0	3	1,8	8,5	1,8	14,5	2,4	27	3,4	19	2,7	8	2,4	64	18,0	18	·	·	·	4	·	·	2	10	11	10	2	·	·	3
VIII	2,5	2,2	1,5	2,3	2	1,0	6	2,4	7	2,6	22,5	3,2	33	4,3	8,5	2,9	10	3,1	32	8,1	5	·	·	·	8	·	·	2	7	12	7		4	·	3
IX	2,5	1,8	5,5	1,9	6	1,9	10	2,4	6	3,6	15,5	3,9	30,5	4,1	8	4,1	6	3,2	59	16,6	28	·	·	·	2	·	·	3	8	16	12	1	8	·	2
X	6,5	2,1	1,5	1,0	10,5	1,8	12	2,0	2,5	2,4	10	3,8	16	3,6	14	2,8	20	2,1	5	1,6	19	·	·	7	·	·	·	3	12	12	2	·	15	·	·
XI	5,5	2,5	6	4,8	1,9	4,7	2,7	4,3	3,5	2,4	8	3,4	10,5	3,9	8,5	2,9	2	3,9	59	15,8	10	·	·	6	·	·	·	2	22	19	11	1	8	1	·
XII	9	2,9	10,5	3,2	4	1,6	1,5	1,8	8,5	4,8	12,5	4,8	18	3,6	11,5	3,4	4	3,2	24	9,8	18	10	16	30	·	·	·	1	20	14	6		1	23	·
Rok	74,5	3,0	67,5	3,0	85,5	2,2	124,5	2,8	90	3,0	163	3,8	247,5	4,3	158,5	3,4	84	3,2	667	39,4	16.III	27	55	134	24	15	4	19	170	174	114	17	46	104	16

Wińsko — $H_s = 180\,m$ — $h_w = 14\,m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	≥15	◐	●	Opad R ≥0,1	≥10	≥100	≡	⊞	⊠
I	7,5	3,5	3,5	3,1			1	2,0	16,5	5,8	18,5	4,4	36	5,0	11	5,4	1	4,8	29	14,5	24	2	6	15	·	2	·	1	14	15	7	1	3	10	·
II	7,5	4,2	10	3,6	5,5	2,3	1	3,0	9	3,2	8,5	5,4	23,5	7,0	19	5,1	·	5,0	36	7,5	12	1	10	24	·	7	3,2	·	14	17	11		1	16	·
III	13,5	3,1	9,5	1,4	9	2,8	13	3,2	9,5	3,5	7,5	1,8	9	3,7	20	4,1	2	3,1	36	14,1	5	·	4	26	·	1	·	3	13	10	7	1	7	13	·
IV	5	2,6	15,5	3,1	3,5	3,1	3	3,7	11	4,3	7	4,7	17	4,1	27	3,9	1	3,8	27	5,9	13	·	·	·	5	2	·	5	9	14	11		2	·	2
V	9	2,4	3	2,0	4	2,8	4	2,8	4	3,2	4	3,0	3,5	4,6	28	3,3	2	3,5	88	24,8	14	·	·	1	·	3	·	·	14	22	14	2	2	·	3
VI	16,5	3,3	3	2,3	·	·	1,5	1,0	6,5	2,2	2,5	1,0	23,5	5,0	36,5	3,5		3,6	24	13,3	16	·	·	·	7	2	·	5	5	9	5	1		·	3
VII	1,2	1,3	7	2,4	1	3,0	5	1,4	4	1,8	8	3,6	32,5	3,7	20,5	3,6	3	3,0	47	17,2	22	·	·	·	8	1	·	2	9	18	10	1	3	·	5
VIII	4,5	2,2	3,5	1,7	1	4,0	3	2,3	3	3,3	6,5	2,8	59,5	4,3	11	4,8	1	3,9	41	8,2	24	·	·	·	7	1	·	3	11	16	13	·	2	·	2
IX	6	1,5	7	1,9	7	3,0	3,5	2,9	2,5	1,6	9	5,0	3,5	5,0	13	4,0	7	3,7	66	15,5	18	·	·	·	3	3	1	7	9	13	8	2	5	·	1
X	6	2,0	9	2,1	10,5	2,2	8,5	2,2	8,5	2,4	3	2,8	17,5	4,0	26	3,7	4	2,9	38	15,7	31	·	·	1	·	1	·	5	8	15	6	2	18	·	·
XI	5,5	2,2	14,5	3,6	11,5	3,5	1,7	3,9	1	1,0	3	1,7	2,4	3,4	12,5	3,1	1	3,3	45	12,3	1	·	·	8	·	2	·	3	18	13	7	1	10	·	·
XII	7	2,1	13,5	2,8	13,5	2,1	1	3,0	9	5,5	4,5	4,3	33,5	3,8	9	3,2	2	3,3	27	12,2	15	10	18	26	·	1	·	3	12	13	4	1	4	18	·
Rok	9,8	2,5	9,9	2,5	6,6,5	2,4	6,1,5	2,6	8,4,5	3,2	8,2	3,4	34,6	4,5	23,3,5	4,0	24	3,7	504	24,8	14.V	13	38	101	30	26	4,2	37	136	176	103	12	57	57	16

Grabownica — $H_s = 119\,m$ — $h_w = 12\,m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	≥15	◐	●	Opad R ≥0,1	≥10	≥100	≡	⊞	⊠
I	5	5,3	6	3,3	·	·	·		1,6	5,2	37,5	3,9	14,5	4,3	11	5,0	3	4,2	39	12,8	24	1	5	19	·	2	·	2	11	15	10	1	1	–	–
II	5,5	4,9	9	4,2	5	2,8	4	2,5	8,5	2,3	10	6,3	21,5	5,0	15,5	5,9	5	4,4	44	21,7	12	3	10	25	·	4	1	·	15	17	5	1	·	–	–
III	5	4,5	15,5	4,4	4,5	3,2	9,5	4,4	1,0	3,2	4	2,9	6,5	2,8	10	5,2	2,8	2,8	40	12,4	31	1	3	25	·	2	·	6	12	12	8	1	4	–	–
IV	8	2,8	5	4,4	3,5	3,9	3,5	7,1	8,5	5,2	8,5	3,3	10,5	3,6	14,5	3,3	2,8	2,7	29	8,3	28	·	·	·	7	2	·	4	12	10	8	·	3	·	–
V	4	1,9	2	1,5	2	3,5	3,5	3,0	4,5	2,9	11	2,5	27,5	2,6	17,5	3,9	2,1	2,2	106	32,1	14	·	·	3	·	·	·	1	11	22	18	2	1	·	–
VI	1,5	3,8	3	1,7	0,5	2,0	1,5	2,0	2	1,5	6,5	2,3	26	3,1	17,5	3,0	1,8	2,4	17	5,7	1	·	·	·	7	·	·	–	–	11	6	·	·	·	–
VII	5	1,1	1,5	1,3	1	1,0	3	2,0	2	1,0	8,5	1,5	23	1,9	18	2,0	3,1	1,2	81	28,0	26	·	·	·	7	·	·	–	–	13	13	1	1	·	–
VIII	1	2,0	3	1,3	·	·	2	1,5	6	2,1	15,5	2,4	32,5	3,0	12	3,2	2,1	2,1	49	13,2	24	·	·	·	8	·	·	–	–	17	10	1	·	·	–
IX	3	2,0	·	·	5,5	2,7	5,5	2,7	5	2,1	9	3,2	26	3,3	11	2,9	2,5	2,1	51	17,2	18	·	·	1	4	1	·	–	–	12	10	2	6	·	–
X	6	2,7	5	2,9	4,5	1,7	5	1,9	6	2,4	8,5	2,3	15	2,8	8	2,9	3,5	1,6	33	14,0	31	·	·	11	·	·	·	–	–	9	5	1	15	·	–
XI	3	1,3	6	3,5	8,5	2,9	11,5	3,6	8,5	3,6	5,5	1,9	17,5	2,4	7,5	2,1	2,2	2,1	45	10,2	1	·	·	7	·	·	·	–	–	11	8	1	2	·	–
XII	2	2,0	1,4	2,9	6,5	3,3	6	2,0	5,5	3,5	12,5	3,4	20,5	2,2	8	2,5	1,8	2,2	26	14,0	15	1,1	1,5	25	·	·	·	1	16	7	4	1	4	–	–
Rok	62,5	2,9	70	2,6	41,5	2,2	55	2,7	82,5	2,9	137	3,0	241	3,1	150,5	3,5	25,5	2,5	560	32,1	14.V	16	33	116	33	11	1	–	–	156	105	12	37	–	–

Nowa Wieś — $H_s = 179\,m$ — $h_w = 16\,m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	≥15	◐	●	Opad R ≥0,1	≥10	≥100	≡	⊞	⊠
I	2,5	3,8	5,5	3,7	2	3,5	1	2,0	2,0	3,8	3,3	3,1	2,2	4,3	7	3,4	·	3,6	15	4,7	25	2	8	22	·	·	·	1	18	12	5	·	·	19	–
II	6,5	4,2	3,5	2,9	1,5,5	4,2	4,5	3,0	8	4,3	11	5,5	22,5	4,8	7,5	7,1	5	4,4	34	12,9	12	4	16	28	·	2	·	·	18	18	7	1	·	28	–
III	6,5	4,4	7	3,4	2,1	2,7	1,5	3,5	7	3,4	1	3,5	14,5	4,3	13	4,2	8	3,3	35	7,5	12	4	15	27	·	·	·	2	16	14	8	·	2	24	–
IV	2,5	3,0	2,5	3,8	18,5	2,7	12,5	3,1	11,5	3,0	9	2,8	8	3,4	10,5	4,1	1,5	2,6	45	7,8	26	·	·	1	4	1	·	4	6	11	9	·	·	·	–
V	8	2,3	1,5	1,3	5,5	1,9	4,5	2,7	4,5	2,7	1,4	2,4	2,5,5	3,7	10,5	2,8	1,9	2,3	91	20,1	14	·	·	2	·	·	·	1	14	22	16	1	·	·	–
VI	1,9	3,7	1,5	2,3	1,5	2,0	5,5	1,5	3,5	2,7	8,5	1,9	2,6	3,7	12,5	2,6	1,2	2,6	102	31,2	4	·	·	·	5	·	·	2	12	14	11	3	·	·	–
VII	9	2,2	4,5	1,9	1	1,0	3,5	1,7	5,5	1,8	12,5	1,8	30,5	3,0	14,5	2,3	1,2	2,1	101	28,9	18	·	·	·	4	·	·	2	8	18	15	3	·	·	–
VIII	0,5	1,0	1,5	1,0	5	2,4	4	2,8	6,5	1,9	2,0	2,0	29,5	3,4	7	3,1	1,9	2,2	47	10,5	15	·	·	·	6	·	·	1	5	9	8	1	1	·	–
IX	2,5	2,4	2,5	2,0	9	2,0	5	1,4	8,5	2,6	2,1,5	2,6	28	3,7	4	3,8	9	2,6	55	15,2	18	·	·	·	2	·	·	3	11	14	10	1	4	·	–
X	6,5	1,8	3,5	2,3	8,5	1,4	1,6	1,7	4,5	1,4	1,0	2,0	15	2,7	9	2,4	2,0	1,6	2	1,3	14	·	·	7	·	·	·	1	11	2	1	·	16	·	–
XI	7,5	2,0	4	3,4	18,5	4,6	2,6	3,2	3	3,7	5,5	3,4	9,5	3,1	12	2,4	4	3,2	51	8,8	15	·	·	6	·	·	·	·	22	17	13	·	5	3	–
XII	10,5	2,7	9,5	3,6	6	3,1	4,5	2,2	1,1	3,8	14,5	3,0	18	2,4	7	2,8	1,2	2,6	15	4,6	18	1,1	1,6	30	·	·	·	·	19	8	5	·	2	17	–
Rok	8,1,5	2,8	4,7	2,6	11,2	2,6	10,2	2,4	9,3,5	2,9	1,6,0,5	2,8	24,9	3,5	11,4,5	3,4	13,5	2,8	593	31,2	4.VI	21	55	123	21	3	·	17	160	159	108	10	30	91	–

Ustrzeszów $\varphi = 51°26'$ $\lambda = 17°56'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2,3	-2,3	8,0	22	-15,4	31	-0,8	1,2	-0,5	-0,2	–	–	–	–	–	–	–	–	–	–	–	–	7,4	7,5	7,5	7,5
II	–	–	–	–	0,9	-4,1	5,7	20	-13,4	3	-3,0	-0,6	-1,7	-1,8	–	–	–	–	–	–	–	–	–	–	–	–	9,0	9,6	7,7	8,8
III	–	–	–	–	2,7	-3,6	14,5	31	-8,9	8	-2,6	1,8	-0,9	-0,6	–	–	–	–	–	–	–	–	–	–	–	–	7,5	7,8	7,8	7,7
IV	–	–	–	–	15,7	6,6	27,5	26	0,6	30	8,6	14,4	10,1	10,8	–	–	–	–	–	–	–	–	–	–	–	–	7,2	7,5	5,3	6,7
V	–	–	–	–	15,3	7,0	23,4	8	-0,9	1	9,4	13,3	9,9	10,6	–	–	–	–	–	–	–	–	–	–	–	–	7,0	8,6	7,0	7,5
VI	–	–	–	–	20,3	11,1	31,4	16	3,6	3	12,9	18,6	13,9	14,8	–	–	–	–	–	–	–	–	–	–	–	–	4,8	7,0	5,5	5,8
VII	–	–	–	–	20,9	10,9	31,9	26	7,1	4	14,5	19,3	14,4	15,6	–	–	–	–	–	–	–	–	–	–	–	–	5,7	7,2	5,5	6,1
VIII	–	–	–	–	22,4	13,6	31,4	13	9,8	30	15,6	20,9	16,0	17,1	–	–	–	–	–	–	–	–	–	–	–	–	5,7	8,3	4,8	6,3
IX	–	–	–	–	17,8	8,5	29,9	4	2,6	15	10,4	16,0	11,8	12,5	–	–	–	–	–	–	–	–	–	–	–	–	6,7	6,5	4,5	5,9
X	–	–	–	–	12,9	4,7	22,0	4	-2,5	21	6,5	11,9	7,4	8,3	–	–	–	–	–	–	–	–	–	–	–	–	6,5	5,3	4,4	5,4
XI	–	–	–	–	5,9	1,6	16,0	8	-4,4	26	2,7	5,0	3,3	3,6	–	–	–	–	–	–	–	–	–	–	–	–	8,9	8,2	7,2	8,1
XII	–	–	–	–	-1,8	-6,8	4,5	12	-24,1	22	-5,2	-3,0	-4,8	-4,4	–	–	–	–	–	–	–	–	–	–	–	–	8,7	7,7	6,7	7,7
Rok	–	–	–	–	11,3	3,9	31,9	26.VII	-24,1	22.XII	5,8	9,9	6,6	7,2	–	–	–	–	–	–	–	–	–	–	–	–	7,1	7,6	6,2	7,0

Zawołocze $\varphi = 51°26'$ $\lambda = 23°34'$

I	–	–	–	–	1,6	-3,3	6,8	22	-21,4	31	-4,7	0,4	-1,0	-0,8	5,4	5,7	5,5	5,5	9,4	9,0	9,4	9,3	0,3	0,8	0,4	0,5	7,7	6,5	6,5	6,9
II	–	–	–	–	-1,1	-6,9	2,7	13	-16,0	1,28	-4,8	-1,9	-3,7	-3,5	4,2	4,7	4,5	4,5	9,2	8,6	9,2	9,0	0,3	0,8	0,3	0,5	9,4	8,9	8,7	9,0
III	–	–	–	–	1,5	-7,4	12,7	5	-21,1	26	-5,3	0,3	-3,2	-2,8	4,1	5,0	4,6	4,6	9,0	9,8	9,1	8,6	0,4	1,5	0,4	0,8	7,9	7,1	7,7	7,6
IV	–	–	–	–	16,5	4,8	27,6	24	-0,4	2,8	7,6	15,0	9,2	10,2	9,3	9,4	9,9	9,5	8,8	5,9	8,3	7,7	1,5	8,7	2,3	4,2	6,8	6,3	5,4	6,2
V	–	–	–	–	17,0	7,3	26,0	28	-0,5	3	10,1	15,2	10,9	11,8	11,6	12,0	12,4	12,0	9,2	6,8	9,2	8,4	1,1	6,1	1,1	2,8	8,3	8,7	7,0	8,0
VI	–	–	–	–	20,0	9,5	29,5	16	3,3	7	13,3	18,3	13,4	14,6	13,1	12,8	13,7	13,2	8,4	6,2	8,8	7,8	2,9	11,0	2,2	5,4	6,4	7,5	6,5	6,8
VII	–	–	–	–	22,1	11,0	30,7	27	6,4	31	14,3	20,0	14,7	15,9	14,5	14,3	15,1	14,6	8,9	6,2	8,9	8,0	2,0	9,7	1,9	4,5	6,6	7,6	6,8	7,0
VIII	–	–	–	–	23,1	11,4	32,0	13	5,4	27	14,7	21,0	15,8	16,8	15,4	14,9	16,2	15,5	9,1	6,1	8,9	8,0	1,6	10,7	2,0	4,8	7,7	7,5	6,3	7,2
IX	–	–	–	–	17,9	7,8	29,2	5	1,9	26	9,5	16,6	11,4	12,2	11,4	12,6	12,7	12,2	9,5	6,8	9,2	8,5	0,7	7,1	1,1	3,0	6,8	7,5	5,8	6,7
X	–	–	–	–	13,2	2,6	20,2	2	-3,7	16	3,9	12,3	6,1	7,1	8,0	10,2	9,0	9,1	9,6	7,1	9,5	8,7	0,3	4,7	0,6	1,9	7,1	6,6	4,4	6,0
XI	–	–	–	–	7,2	2,1	19,5	1	-3,1	18	3,3	6,1	4,3	4,5	7,7	8,0	8,0	7,9	9,6	8,5	9,3	9,1	0,3	2,0	0,6	1,0	8,8	8,5	8,5	8,6
XII	–	–	–	–	-2,3	-8,3	3,4	1,13	-22,6	23	-5,8	-3,7	-5,5	-5,1	4,0	4,4	4,1	4,2	9,2	9,0	9,2	9,1	0,3	0,5	0,3	0,4	8,8	7,6	6,9	7,8
Rok	–	–	–	–	11,4	2,6	32,0	13.VIII	-22,6	23.XII	4,9	10,0	6,0	6,7	9,1	9,5	9,6	9,4	9,2	7,3	9,1	8,5	1,0	5,3	1,1	2,5	7,7	7,5	6,7	7,3

Piotrków Trybunalski $\varphi = 51°25'$ $\lambda = 19°42'$

I	–	–	–	–	1,4	-2,5	7,9	22	-17,6	31	-1,1	-0,3	-0,9	-0,8	5,4	5,6	5,4	5,5	9,3	8,8	9,2	9,1	0,4	0,9	0,5	0,6	–	–	–	–
II	–	–	–	–	0,0	-5,1	4,1	12,13	-15,1	1,3	-3,8	-1,7	-2,2	-2,5	4,5	4,9	4,9	4,8	9,3	8,9	9,1	9,1	0,4	0,6	0,5	0,5	–	–	–	–
III	–	–	–	–	2,0	-5,0	14,5	31	-11,0	25	-4,0	0,7	-1,4	-1,5	4,2	5,0	4,7	4,6	8,8	7,5	8,2	8,2	0,5	1,7	0,9	1,0	–	–	–	–
IV	–	–	–	–	15,5	5,7	27,3	23	0,5	30	8,0	13,8	9,9	10,4	8,7	8,3	9,0	8,7	8,1	5,7	7,4	7,1	2,5	9,2	4,1	5,3	–	–	–	–
V	–	–	–	–	14,8	6,5	22,4	8	-1,8	1	8,8	13,1	10,1	10,5	10,3	10,2	10,8	10,4	8,8	6,8	8,6	8,1	1,3	5,5	1,9	2,9	7,5	7,6	6,9	7,3
VI	–	–	–	–	19,6	9,7	30,5	23	4,2	2,3	12,5	17,5	14,1	14,6	12,5	12,6	13,8	13,0	8,3	6,3	8,3	7,6	2,6	8,9	3,0	4,8	4,9	5,5	4,2	4,9
VII	–	–	–	–	21,4	11,0	31,1	26	7,2	30	14,2	19,3	15,0	15,9	13,3	12,7	13,1	13,0	8,2	5,7	7,7	7,2	3,1	10,3	4,3	5,9	7,2	6,5	6,4	6,7
VIII	–	–	–	–	22,5	12,1	31,1	7,13	7,3	31	14,7	20,5	16,0	16,8	14,0	14,6	14,7	14,4	8,3	6,1	8,0	7,5	2,9	10,3	3,8	5,7	7,0	6,8	4,8	6,2
IX	–	–	–	–	17,7	7,4	28,1	4	1,8	25	9,4	15,7	11,5	12,0	10,6	11,1	11,5	11,1	8,9	6,4	8,4	7,9	1,5	7,4	2,4	3,8	7,6	7,6	3,9	6,4
X	–	–	–	–	13,3	3,6	21,7	3	-3,4	16	4,9	11,8	6,7	7,5	8,5	9,6	9,2	9,1	9,5	6,9	9,1	8,5	0,4	4,6	0,9	2,0	8,9	6,0	3,7	6,2
XI	–	–	–	–	6,3	1,9	15,2	8	-2,0	24	2,7	5,0	3,4	3,6	7,2	7,6	7,4	7,4	9,4	8,6	9,3	9,1	0,5	1,5	0,6	0,9	8,8	8,5	8,2	8,5
XII	–	–	–	–	-2,5	-7,3	4,8	12	-20,0	22	-5,6	-3,7	-5,3	-5,0	3,8	4,3	3,9	4,0	8,7	8,6	8,5	8,6	0,5	0,7	0,6	0,6	9,2	8,6	6,7	8,2
Rok	–	–	–	–	11,0	3,2	31,1	26.VII,27.VIII	-20,0	22.XII	5,1	9,3	6,4	6,8	8,6	8,9	9,0	8,8	8,8	7,2	8,5	8,2	1,4	5,1	2,0	2,8	–	–	–	–

Radom $\varphi = 51°25'$ $\lambda = 21°07'$

I	–	–	–	–	1,9	-3,0	7,9	22	-20,0	31	-1,1	0,6	-0,9	-0,6	5,2	5,1	5,2	5,2	8,8	7,7	8,6	8,4	0,7	1,5	0,8	1,0	7,6	7,4	7,4	7,5
II	–	–	–	–	0,1	-5,2	5,6	13	-13,6	1	-3,8	-1,2	-2,4	-2,4	4,4	4,8	4,8	4,7	9,0	8,4	9,1	8,8	0,5	1,0	0,5	0,7	9,0	9,0	8,4	8,8
III	–	–	–	–	1,6	-5,5	13,3	31	-14,8	26	-4,3	0,4	-2,1	-2,0	4,3	5,3	5,0	4,9	9,0	8,2	9,2	8,8	0,4	1,3	0,4	0,7	7,7	7,2	6,2	7,0
IV	–	–	–	–	16,0	6,4	26,4	22,23	0,6	8	8,4	14,4	10,6	11,0	9,2	9,2	9,8	9,4	8,2	6,0	7,7	7,3	2,3	8,8	3,7	4,9	6,8	6,7	5,9	6,5
V	–	–	–	–	15,1	7,0	23,1	8	-2,1	1	9,4	13,7	10,6	11,1	10,9	10,8	11,3	11,0	9,0	6,8	8,7	8,2	1,3	5,5	1,8	2,9	8,4	8,6	7,9	8,3
VI	–	–	–	–	18,9	9,9	29,4	16.23	4,5	7	13,0	17,2	14,3	14,7	12,6	11,9	12,8	12,4	8,2	6,1	7,7	7,3	3,3	9,0	4,3	5,5	6,4	7,2	6,2	6,6
VII	–	–	–	–	21,3	11,1	29,4	26	6,3	2	14,6	19,6	15,5	16,3	13,9	13,3	14,1	13,8	8,3	5,8	8,0	7,4	3,0	10,2	4,1	5,8	6,5	7,9	6,4	6,9
VIII	–	–	–	–	22,1	12,5	30,9	13	8,0	31	15,1	20,2	16,5	17,1	14,6	15,0	15,5	15,0	8,5	6,4	8,1	7,7	2,7	9,4	3,6	5,2	6,7	7,2	5,7	6,5
IX	–	–	–	–	17,3	7,9	27,0	4	2,3	25	10,0	15,9	12,0	12,5	11,0	11,5	12,0	11,5	8,9	6,6	8,5	8,0	1,5	7,3	2,4	3,7	6,8	7,2	5,1	6,4
X	–	–	–	–	13,0	3,5	19,8	3	-2,7	16,17	5,0	11,6	7,4	7,8	8,5	10,0	9,5	9,3	9,5	7,2	9,0	8,6	0,4	4,1	1,0	1,8	8,2	6,6	5,6	6,8
XI	–	–	–	–	6,3	2,1	15,4	1	-2,2	18	2,9	5,1	3,8	3,9	7,2	7,7	7,3	7,4	9,4	8,5	8,9	8,9	0,5	1,5	0,9	1,0	9,1	9,1	9,1	9,1
XII	–	–	–	–	-2,1	-7,2	4,0	12	-19,5	21	-5,6	-3,7	-5,3	-5,0	3,8	4,1	3,9	3,9	8,5	8,0	8,4	8,3	0,6	0,9	0,6	0,7	8,8	8,5	7,6	8,3
Rok	–	–	–	–	11,0	3,3	30,9	13.VIII	-20,0	31.I	5,3	9,5	6,7	7,0	8,8	9,1	9,3	9,1	8,8	7,1	8,5	8,1	1,4	5,0	2,0	2,8	7,7	7,7	6,8	7,4

Ostrzeszów $H_s = 198\ m$ $h_w = 12\ m$ 1962

MIESIĄC	ROZKŁAD WIATRU °D, v mD: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n) Temperatura T: Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr: v ≥ 10	v > 15	◔	●	Opad R: R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	ꞧ
I	1	8.0	6.5	5.2	1.5	3.7	3.5	4.1	20.5	4.6	25.5	3.9	20	4.5	7.5	4.9	7	4.1	28	11.3	20	2	7	19	·	·	·	3	16	10	5	1	1	-	
II	2.5	5.4	8.5	3.9	9	3.1	5	3.9	7	3.1	8.5	5.0	28.5	6.7	11	6.3	4	5.0	31	14.5	12	3	10	22	·	5	·	·	20	8	5	1	3	-	1
III	9.5	5.0	4.5	4.0	15.5	3.2	14	3.1	8	2.2	6.5	2.4	14.5	5.1	40.5	2.4	10	3.1	39	14.6	31	·	7	27	·	1	·	1	17	8	6	2	4	-	
IV	4	4.1	9.5	3.2	4.5	3.4	10	4.7	13	3.4	16	3.4	8	4.2	16	4.2	9	3.4	30	9.8	4	·	·	·	7	1	·	4	14	10	7	·	1	·	1
V	2	4.2	1.5	4.0	3	3.5	5	1.8	7	3.6	17.5	3.1	39.5	3.7	40.5	3.6	7	3.2	109	33.1	14	·	·	2	·	2	·	·	14	22	17	2	1	·	2
VI	10.5	4.1	5.5	3.4	1	2.5	4	2.6	6.5	1.8	7.5	2.3	29	4.3	21	3.4	5	3.3	24	13.0	23	·	·	·	8	·	·	2	6	7	5	1	·	·	2
VII	10.5	2.3	7	2.9	15	4.3	1	3.0	6	1.8	9	2.9	26	3.0	15	2.3	17	2.3	86	18.0	13	·	·	·	6	·	·	4	12	15	10	2	1	·	6
VIII	1.5	3.6	1.5	2.0	2	2.2	3	2.3	7.5	3.2	19	3.7	32.5	3.7	8	4.1	18	2.9	76	18.3	13	·	·	·	8	·	·	1	11	13	11	2	1	·	2
IX	3	1.7	1	3.0	5	3.3	9	3.2	5	3.1	13	3.4	28	3.1	10	3.6	16	2.6	67	21.1	18	·	·	·	4	1	1	6	9	15	8	2	6	·	·
X	3	2.5	7.5	2.3	7.5	2.9	16.5	2.7	8.5	3.4	11	3.0	13	2.4	15	3.1	11	2.5	32	14.0	31	·	·	2	·	·	·	7	9	8	6	1	16	·	·
XI	1	1.5	1	3.5	22	3.7	16	3.7	3.5	3.1	9	3.0	17.5	3.0	6	2.6	14	2.8	53	12.5	20	·	1	9	·	·	·	1	19	10	10	1	11	-	·
XII	2.5	2.8	5	2.7	17	3.4	10.5	1.7	7	3.9	12	4.2	26.6	3.3	5.5	2.8	7	3.0	22	12.0	15	11	15	27	·	1	·	3	18	8	5	1	10	-	·
Rok	51	3.8	59	3.3	89.5	3.3	97.5	3.1	99.5	3.1	154.5	3.4	283	3.9	136	3.6	125	3.2	597	33.1	14.V	16	40	108	33	11	1	32	165	134	95	16	55	-	14

Zawołocze $H_s = 165\ m$ $h_w = 12\ m$

I	3.5	4.1	5	2.5	1.5	2.7	3.5	2.7	9.5	3.4	24	5.2	26.5	5.4	5.5	3.0	14	3.8	30	9.4	25	3	8	25	·	3	1	2	13	15	7	·	3	24	-
II	4	7.6	3.5	3.1	6	3.0	6	2.9	6	9.0	10.5	11.7	13	8.2	8	8.4	27	5.1	68	18.2	12	7	15	28	·	6	4	·	22	21	14	1	·	28	-
III	10	5.6	3.5	7.6	5	2.0	17.5	4.7	3.5	4.1	5.5	5.1	7	9.0	7	5.8	34	3.4	65	19.2	16	8	10	27	·	6	1	2	16	17	12	1	2	31	-
IV	2	7.5	9.5	4.1	6	3.8	14.5	4.5	12	3.7	11	4.0	11.5	5.5	3.5	7.0	20	3.5	87	16.2	28	·	·	4	5	2	·	3	9	11	10	5	2	1	-
V	3	3.8	2	3.0	·	·	5.5	3.2	6	2.8	14.5	5.3	18	6.4	13	2.4	31	3.0	106	17.7	30	·	·	3	2	2	2	·	16	18	13	5	·	·	-
VI	10	2.9	4.5	2.8	·	·	1	3.0	4	2.0	13.5	2.2	18	3.2	10	2.1	29	1.8	116	25.6	4	·	·	·	8	·	·	1	13	13	11	4	·	·	-
VII	6	2.3	2	3.0	·	·	1	2.0	7.5	2.0	14	2.2	21.5	2.5	14	3.2	27	1.8	68	20.3	18	·	·	·	6	·	·	1	12	15	11	3	2	·	-
VIII	0.5	1.0	1	5.0	1	5.0	5.5	2.9	8	2.2	22.5	2.9	23.5	3.3	11	2.3	20	2.3	33	9.1	5	·	·	·	9	·	·	1	9	12	8	·	4	·	-
IX	0.5	2.0	3	1.7	4	1.8	10.5	1.7	7.5	2.1	16.5	3.4	25.5	3.0	25	4.8	20	2.1	61	13.9	28	·	·	·	2	·	·	2	10	15	14	2	4	·	-
X	5	2.0	1	4.0	1.5	2.3	14.5	1.9	4	2.1	10	3.6	14.5	3.1	7.5	3.1	35	1.7	4	2.5	19	·	·	8	·	·	·	3	9	4	2	·	15	·	-
XI	2.5	1.2	3.5	2.3	14.5	4.4	32.5	4.4	2.5	2.4	10.5	4.1	7.5	3.1	6.5	1.8	10	3.4	68	10.6	16	·	·	5	·	5	1	3	23	19	13	1	4	1	-
XII	3.5	2.0	13	2.8			9.5	1.9	11.5	2.7	14.5	3.3	14.5	2.6	8.5	2.6	18	2.2	22	5.6	14	11	16	30	·	·	·	·	18	13	7	·	1	22	-
Rok	50.5	3.5	51.5	3.5	39.5	2.1	121.5	3.0	82	3.2	167	4.4	201	4.6	97	3.9	285	2.8	728	25.6	4.VI	29	49	130	32	24	9	18	170	173	122	22	37	107	-

Piotrków Trybunalski $H_s = 200\ m$ $h_w = 13.5\ m$

I	3	5.7	4.5	5.0	1	5.0	1.5	3.0	7	2.9	37	3.0	22.5	3.1	8.5	3.7	8	3.0	37	8.5	25	2	8	18	·	·	·	-	-	11	11	·	5	-	·
II	5	3.6	8.5	3.1	4	2.2	3.5	3.3	3	4.7	11.5	5.0	18	4.5	19.5	4.3	11	3.6	42	8.5	11	3	13	25	·	2	·	-	-	11	11	·	3	-	
III	8.5	3.8	9	4.2	3.5	3.0	9	2.9	8	3.0	6.5	3.0	10.5	2.9	16	3.1	22	2.5	-	-	-	6	10	24	·	·	·	-	-	-	-	-	5	-	
IV	13	2.6	7	3.1	2.5	3.4	5.5	3.5	6.5	3.9	13.5	3.0	11.5	2.9	12.5	2.9	18	2.4	70	12.8	27	·	·	·	4	·	·	-	-	14	14	2	2	-	
V	2.5	1.0	4.5	2.1	2.5	2.6	6.5	2.7	3.5	2.7	13	2.9	24.5	2.9	14	3.7	22	2.2	162	-	-	·	·	2	·	1	·	2	15	23	23	6	·	·	3
VI	16	2.8	4	3.0	1	1.0	2	2.5	6.5	2.4	4.5	1.9	24	3.5	18	2.8	14	2.4	46	18.0	4	·	·	·	7	·	·	10	7	9	9	1	·	·	1
VII	10	2.8	2.5	3.8		·	4.5	2.3	6.5	4.1	11	2.6	31	3.1	18.5	3.3	12	2.7	51	6.3	2,3	·	·	·	5	·	·	2	10	14	14	·	·	·	4
VIII	3	2.3	2	3.0	·		2	2.0	7.5	3.3	6.5	3.6	48	3.4	15	3.5	9	3.0	78	15.4	15	·	·	·	8	·	·	1	9	15	12	3	·	·	4
IX	3	4.3	2	2.5	7	4.0	4.5	3.2	3.5	3.9	13	4.2	34.5	3.9	16.5	3.4	6	3.5	58	21.8	17	·	·	·	2	2	·	1	10	14	8	2	·	·	1
X	9	2.1	6	2.5	10	2.7	7.5	3.0	14.5	2.5	4	5.0	19	3.3	12	3.1	11	2.6	17	5.4	27	·	·	6	·	·	·	4	12	14	4	·	14	-	
XI	10.5	1.9	10.5	5.0	18.5	3.6	11	3.7	6.5	3.8	3	3.7	17	3.3	10	2.4	3	3.3	43	12.2	20	·	·	10	·	·	·	1	21	18	9	1	5	-	·
XII	11	2.6	13.5	4.1	7.5	2.5	2.5	3.8	12.5	4.8	8.5	6.2	22.5	3.0	7	2.1	8	3.3	18	4.6	13	11	14	29	·	2	·	1	19	15	6	·	2	-	·
Rok	94.5	3.0	74	3.4	57.5	2.5	57	3.0	85.5	3.5	132	3.7	283	3.3	167.5	3.2	144	2.9	-	-	-	22	45	114	26	7	·	-	-	-	-	-	36	-	13

Radom $H_s = 178\ m$ $h_w = 13\ m$

I	6.5	6.5	1.5	6.0		·	5.5	4.1	23	4.1	28	4.3	24.5	3.4	4	4.8	·	4.2	23	6.5	25	2	8	22	·	3	·	·	16	11	7	·	·	6	·
II	6	5.3	5	3.2	8	3.5	5	4.6	11.5	8.0	17	5.3	19.5	6.5	12	7.1	·	5.9	30	9.7	12	4	14	26	·	6	4	·	21	16	8	·	·	12	·
III	9.5	5.9	13.5	2.5	8	3.0	18.5	3.0	4.5	2.4	8	3.4	9.5	4.3	20.5	4.1	1	3.6	43	9.2	12,31	5	11	26	·	3	1	4	16	13	10	·	3	21	
IV	12.5	3.2	5	3.7	6.5	2.7	15.5	3.6	8.5	5.1	15	2.7	10.5	2.8	13.5	4.9	3	3.4	52	12.4	13	·	·	·	5	1	·	3	10	8	8	2	·	·	1
V	8	2.4	0.5	1.0	2	2.5	11	1.5	11	2.5	17	3.4	23	3.2	15.5	2.5	5	2.6	172	46.0	14	·	·	1	·	1	·	·	21	19	18	7	2	·	3
VI	9	3.0	1.5	2.1	2	2.0	4	1.5	4	2.0	6.5	2.5	33.5	2.6	28.5	4.1	4	2.9	105	45.0	4	·	·	·	6	3	·	4	11	10	8	3	·	·	1
VII	12	2.2	1	3.5	1	1.0	4	1.8	3	1.8	11	2.7	34	2.2	20	2.8	7	2.2	88	35.4	23	·	·	·	5	·	·	2	12	10	10	2	·	·	5
VIII	3	1.3	·	·	3.5	2.0	4.5	3.3	7	2.0	27	2.9	29	2.4	10	3.0	9	2.4	42	14.8	15	·	·	·	6	·	·	1	9	9	9	1	·	·	2
IX	4	3.0	10	1.6	3	2.3	2.5	2.0	13	2.8	22	3.2	26.5	2.8	4	4.2	5	2.6	71	22.4	17	·	·	·	2	1	·	5	12	14	11	2	3	·	1
X	9	2.1	3	1.3	11	1.5	11	1.7	8	1.6	6.5	2.4	16	2.2	15.5	2.5	13	1.7	2	1.4	27	·	·	7	·	·	·	3	15	2	1	·	14	·	·
XI	5.5	2.5	6	3.7	17.5	2.8	21	3.4	2	2.5	5.5	2.2	16	2.6	11.5	2.4	5	2.7	39	7.8	15	·	·	6	·	·	·	1	25	14	12	·	2	·	·
XII	13.5	3.2	4.5	4.1	3	3.3	5.5	3.0	16.5	3.8	13	3.6	21	2.2	6	3.2	10	2.8	20	8.4	13	11	14	28	·	1	·	1	20	10	5	·	4	14	·
Rok	98.5	3.4	51.5	2.7	65.5	2.2	108	2.8	109	3.2	176.5	3.2	263	3.1	161	3.8	67	3.1	687	46.0	14.V	22	47	116	24	19	5	24	188	136	107	17	28	53	13

Puławy $\varphi = 51°25'$ $\lambda = 21°58'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PREŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	P_{am}	$\overline{Max}$	$\overline{Min}$	Max obs.	Data	Min obs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	997.2	1018.9	974.9	1016.8	1.9	-2.9	6.8	22	-18.8	31	-1.3	0.5	-0.8	-0.6	5.2	5.2	5.2	5.2	90	81	87	86	0.5	1.3	0.8	0.9	7.6	6.7	6.8	7.0
II	995.9	1013.1	963.5	1015.6	-0.1	-5.5	5.3	13	-13.2	1	-4.2	-1.5	-2.4	-2.6	4.1	4.4	4.5	4.3	87	78	86	84	0.6	1.2	0.7	0.8	9.0	9.1	8.0	8.7
III	992.0	1009.5	972.6	1011.5	1.5	-5.3	12.0	31	-14.5	26	-4.1	0.1	-1.9	-2.0	4.3	4.5	4.8	4.5	89	71	85	82	0.5	1.9	0.7	1.0	8.0	6.9	6.6	7.2
IV	995.1	1009.0	971.7	1013.8	16.7	5.4	26.8	23	0.3	3	8.5	15.2	10.8	11.3	9.1	8.9	9.7	9.2	82	55	74	70	2.4	9.9	3.9	5.4	6.8	6.5	4.3	5.5
V	993.9	1001.7	975.7	1012.6	15.7	7.5	22.8	28	-1.0	1	9.6	14.4	10.8	11.4	10.7	10.8	11.3	10.9	88	64	86	79	1.5	6.2	2.0	3.2	8.1	8.3	6.4	7.6
VI	998.5	1007.9	988.8	1017.1	19.0	9.9	29.0	23	3.8	7	13.1	17.4	14.2	14.7	12.6	11.6	12.5	12.2	81	58	76	72	3.2	9.6	4.3	5.7	6.1	6.4	5.2	5.9
VII	995.7	1006.3	983.7	1014.1	21.4	11.5	28.8	22	6.1	2	14.4	20.1	15.6	16.4	14.0	13.4	14.4	13.9	85	57	80	74	2.6	10.7	3.6	5.6	5.5	6.5	6.2	6.1
VIII	997.0	1005.7	989.0	1015.2	22.6	12.8	30.7	13	7.8	27	15.2	21.0	17.0	17.5	14.9	14.9	15.8	15.2	86	61	81	76	2.5	10.6	4.0	5.7	6.5	6.3	5.6	6.1
IX	997.9	1011.9	982.0	1016.7	17.3	8.3	27.0	4	2.9	25	9.9	16.1	12.0	12.5	11.1	11.8	12.0	11.6	90	65	86	80	1.4	7.2	2.3	3.6	6.1	6.9	5.4	6.1
X	1003.5	1016.8	990.3	1022.6	12.8	3.2	19.6	2	-3.6	16	4.6	11.9	7.3	7.8	8.4	9.9	9.5	9.3	96	70	91	86	0.3	4.5	1.0	1.9	8.5	6.0	4.4	6.3
XI	998.8	1012.6	984.3	1018.1	6.7	2.3	16.8	1	-1.7	17	3.4	5.7	4.2	4.4	7.4	7.7	7.5	7.5	92	83	89	88	0.6	1.9	1.0	1.2	9.2	8.2	7.8	8.4
XII	997.3	1023.8	956.2	1017.2	-2.0	-7.3	3.9	13	-20.1	22	-5.2	-3.5	-4.8	-4.6	4.0	4.2	4.1	4.1	90	83	89	87	0.4	0.9	0.5	0.6	8.6	7.8	6.6	7.7
Rok	996.9	1023.8	956.2	1015.8	11.1	3.4	30.7	13.VIII	-20.1	22.XII	5.3	9.8	6.8	7.2	8.8	8.9	9.3	9.0	88	69	84	80	1.4	5.5	2.1	3.0	7.5	7.1	6.1	6.9

Opoczno $\varphi = 51°23'$ $\lambda = 20°16'$

I	-	-	-	-	1.7	-	8.0	22	-	-	-0.8	0.6	-0.8	-0.4	5.2	5.6	5.2	5.3	86	84	87	86	0.7	1.1	0.8	0.9	7.7	7.3	6.4	7.1
II	-	-	-	-	0.2	-	5.2	12	-	-	-3.6	-1.4	-2.5	-2.5	4.2	4.7	4.7	4.5	86	83	89	86	0.7	1.0	0.5	0.7	9.5	8.9	7.9	8.8
III	-	-	-	-	1.9	-6.2	14.5	31	-16.1	15	-4.3	0.6	-2.1	-2.0	4.1	5.4	4.6	4.7	84	82	85	84	0.6	1.2	0.7	0.8	7.6	7.4	7.0	7.3
IV	-	-	-	-	15.8	5.3	26.8	22	0.1	8	7.9	14.4	9.9	10.5	9.3	9.8	10.3	9.8	86	62	82	77	1.7	8.3	2.6	4.2	6.2	6.2	6.3	6.2
V	-	-	-	-	14.8	6.7	22.4	8	-0.5	3	9.2	13.1	9.9	10.5	10.9	11.0	11.4	11.1	92	74	92	86	1.0	4.7	1.1	2.3	6.5	7.6	6.7	6.9
VI	-	-	-	-	19.3	8.9	30.3	16	3.5	8	13.0	17.6	13.5	14.4	13.1	12.5	14.1	13.2	84	63	88	78	2.6	9.2	2.0	4.6	5.6	5.7	5.5	5.6
VII	-	-	-	-	21.3	10.4	30.5	26	5.7	30	14.1	19.5	14.6	15.7	13.9	13.9	14.4	14.1	85	62	86	78	2.5	9.4	2.5	4.8	6.1	6.7	5.1	6.0
VIII	-	-	-	-	22.0	11.6	31.3	7	6.8	10	14.6	20.8	15.8	16.8	14.3	14.9	15.8	15.0	86	61	87	78	2.5	10.4	2.4	5.1	5.9	6.4	6.0	6.1
IX	-	-	-	-	17.3	7.5	27.8	4	2.2	25	9.6	15.6	11.4	12.0	10.9	12.1	11.8	11.6	91	69	87	82	1.3	6.4	2.1	3.3	6.5	7.2	4.6	6.1
X	-	-	-	-	13.1	2.5	21.4	4	-4.1	16	4.5	12.2	6.2	7.3	8.2	9.9	9.0	9.0	94	70	93	86	0.5	4.6	0.7	1.9	6.8	5.6	3.8	5.4
XI	-	-	-	-	6.2	1.8	15.8	8	-1.5	18	3.1	5.2	3.7	3.9	7.2	7.8	7.4	7.5	93	86	92	90	0.6	1.5	0.7	0.9	8.8	8.6	8.0	8.5
XII	-	-	-	-	-2.2	-8.4	4.9	12	-20.0	22	-5.5	-3.6	-5.7	-5.1	3.6	4.2	3.8	3.9	80	82	80	81	0.7	0.8	0.7	0.7	8.1	8.3	6.9	7.8
Rok	-	-	-	-	11.0	-	31.3	7.VIII	-20.0	22.XII	5.2	9.6	6.2	6.8	8.7	9.3	9.4	9.1	87	73	87	82	1.3	4.9	1.4	2.5	7.1	7.2	6.2	6.8

Sulejów $\varphi = 51°22'$ $\lambda = 19°53'$

I	-	-	-	-	1.8	-3.3	8.1	22	-17.2	31	-1.0	0.4	-1.0	-0.6	-	-	-	-	-	-	-	-	-	-	-	-	8.2	7.2	6.2	7.2
II	-	-	-	-	0.1	-6.0	4.6	12	-16.0	1	-3.8	-1.4	-2.7	-2.6	-	-	-	-	-	-	-	-	-	-	-	-	9.0	8.5	7.8	8.4
III	-	-	-	-	1.9	-5.8	14.2	31	-14.1	19	-3.9	0.8	-1.9	-1.7	-	-	-	-	-	-	-	-	-	-	-	-	7.5	7.5	7.0	7.3
IV	-	-	-	-	15.6	5.1	27.1	23	0.5	6-8	7.4	14.2	9.3	10.0	-	-	-	-	-	-	-	-	-	-	-	-	6.4	5.8	4.4	5.5
V	-	-	-	-	14.7	6.4	21.7	8	-1.9	1	9.0	13.3	9.8	10.5	-	-	-	-	-	-	-	-	-	-	-	-	7.1	8.0	7.1	7.4
VI	-	-	-	-	19.2	8.9	29.3	16	4.0	3	12.9	17.7	13.2	14.2	-	-	-	-	-	-	-	-	-	-	-	-	4.9	5.2	4.5	4.9
VII	-	-	-	-	21.1	9.9	30.0	26	5.8	30	14.1	19.7	14.3	15.6	-	-	-	-	-	-	-	-	-	-	-	-	4.8	6.4	6.0	5.7
VIII	-	-	-	-	22.3	11.7	31.6	7	5.6	10	14.6	20.8	15.4	16.6	-	-	-	-	-	-	-	-	-	-	-	-	5.8	6.7	4.3	5.6
IX	-	-	-	-	17.2	7.3	28.1	4	2.2	15	9.5	15.6	11.0	11.8	-	-	-	-	-	-	-	-	-	-	-	-	6.8	6.7	3.5	5.7
X	-	-	-	-	13.0	2.7	21.0	3	-4.4	16	4.6	12.0	5.8	7.0	-	-	-	-	-	-	-	-	-	-	-	-	5.9	4.5	3.2	4.5
XI	-	-	-	-	6.2	1.8	14.6	8	-2.2	18	3.2	5.3	3.4	3.8	-	-	-	-	-	-	-	-	-	-	-	-	8.6	8.4	7.5	8.2
XII	-	-	-	-	-2.4	-8.0	5.1	12	-19.6	21-23	-5.5	-3.5	-5.5	-5.0	-	-	-	-	-	-	-	-	-	-	-	-	7.9	7.0	7.7	7.5
Rok	-	-	-	-	10.9	2.6	31.6	7.VIII	-19.6	21-23.XII	5.1	9.6	5.9	6.6	-	-	-	-	-	-	-	-	-	-	-	-	6.9	6.8	5.8	6.5

Szczerców $\varphi = 51°20'$ $\lambda = 19°07'$

I	-	-	-	-	2.7	-3.3	9.0	22	-16.7	31	-0.3	1.6	-0.4	0.1	-	-	-	-	-	-	-	-	-	-	-	-	7.2	7.1	7.5	7.3
II	-	-	-	-	0.6	-5.2	5.6	7	-16.7	3	-3.2	0.0	-2.1	-1.8	-	-	-	-	-	-	-	-	-	-	-	-	8.8	8.0	8.0	8.3
III	-	-	-	-	3.3	-4.5	15.8	31	-10.0	15	-2.7	2.7	-1.3	-0.6	-	-	-	-	-	-	-	-	-	-	-	-	6.8	6.4	7.7	7.0
IV	-	-	-	-	16.3	5.5	28.6	23	0.0	30	8.5	15.6	8.5	10.3	-	-	-	-	-	-	-	-	-	-	-	-	6.6	5.4	6.4	6.1
V	-	-	-	-	15.8	5.8	22.9	8	-1.5	1	9.7	14.6	9.2	10.7	-	-	-	-	-	-	-	-	-	-	-	-	7.9	7.6	6.7	7.4
VI	-	-	-	-	20.2	8.9	32.4	16	3.2	3	12.6	19.1	12.9	14.4	-	-	-	-	-	-	-	-	-	-	-	-	5.9	5.8	5.9	5.9
VII	-	-	-	-	22.3	10.2	32.4	26	5.1	30	13.5	20.8	14.0	15.6	-	-	-	-	-	-	-	-	-	-	-	-	6.8	6.1	6.4	6.4
VIII	-	-	-	-	23.0	12.1	31.9	7,13	7.4	10	14.7	21.8	15.3	16.8	-	-	-	-	-	-	-	-	-	-	-	-	7.3	5.9	5.7	6.3
IX	-	-	-	-	18.2	7.2	30.3	4	2.5	15,25	9.2	17.2	10.5	11.8	-	-	-	-	-	-	-	-	-	-	-	-	7.6	6.2	5.8	6.5
X	-	-	-	-	14.1	3.6	22.6	1	-3.7	23	5.5	13.5	6.1	7.8	-	-	-	-	-	-	-	-	-	-	-	-	7.7	5.7	7.4	6.9
XI	-	-	-	-	6.3	2.6	16.3	8	-3.5	24	3.5	6.0	3.7	4.2	-	-	-	-	-	-	-	-	-	-	-	-	9.2	8.1	8.8	8.7
XII	-	-	-	-	-1.8	-7.3	5.1	12	-19.9	22	-5.4	-2.6	-5.3	-4.6	-	-	-	-	-	-	-	-	-	-	-	-	8.9	7.6	7.3	7.9
Rok	-	-	-	-	11.8	3.0	32.4	16.VI 26.VIII	-19.9	22.XII	5.5	10.9	5.9	7.0	-	-	-	-	-	-	-	-	-	-	-	-	7.6	6.7	7.0	7.1

Puławy $H_s = 142\,m$ $H_b = 155{,}2\,m$ $h_w = 12\,m$ 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R fo
I	3	2.3	5	1.7	0.5	1.0	2.5	2.2	23	1.8	16.5	4.7	15.5	2.5	11	2.4	16	1.7	24	7.0	13	2	7	25	·	·	·	2	13	14	7	·	2	20	·
II	5	3.0	5.5	1.6	10	2.3	9	1.6	9.5	1.9	7.5	5.1	9.5	2.6	20	4.0	8	2.7	49	16.4	12	5	14	28	·	6	4	·	22	15	9	2	4	28	1
III	11.5	3.5	4.5	2.7	13	2.0	12	2.8	12	2.2	1	1.5	8	3.4	13	2.9	18	2.2	44	8.6	31	3	11	26	·	2	1	2	16	13	10	·	5	24	·
IV	3	2.0	7	2.5	12.5	1.8	9	3.6	13	1.7	5.5	1.6	8.5	1.4	12.5	3.4	19	1.8	40	13.4	26	·	·	·	5	1	·	3	8	11	7	1	2	·	2
V	6	1.5	0.5	1.0	2.5	1.0	5	1.6	8	1.3	6.5	1.4	14.5	2.5	18	1.6	32	1.1	156	42.0	14	·	·	1	·	1	1	1	18	22	14	5	3	·	5
VI	9	1.9	2.5	2.2	·	·	2.5	1.0	6.5	1.2	3	1.3	13.5	2.1	20	2.2	33	1.2	93	36.0	4	·	·	·	6	·	·	5	8	11	8	3	·	·	2
VII	6.5	1.8	1.5	1.0	2.5	1.0	4	1.0	4	1.0	3	1.5	10.5	1.5	19	1.6	42	0.8	71	24.1	22	·	·	·	4	·	·	3	8	18	14	2	·	·	5
VIII	0.5	3.0	·	·	1.5	1.0	3	1.0	6	1.2	7	1.6	12	2.4	13	2.2	50	0.9	47	15.9	15	·	·	·	7	1	·	3	8	12	8	2	3	·	4
IX	1	1.0	3	1.0	4	1.2	4	1.0	7	1.5	9	1.5	16.5	1.5	11.5	2.0	34	0.9	64	22.5	18	·	·	·	2	·	·	4	10	16	10	2	8	·	2
X	3.5	1.7	2.5	1.2	8	1.1	8	1.1	3	1.0	2.5	1.6	7	1.9	7.5	1.6	51	0.6	3	1.7	14	·	·	4	·	·	·	2	10	5	1	·	21	·	·
XI	9	1.1	3	1.8	16	2.2	22	2.2	3.5	1.7	3.5	1.7	10	1.2	8	1.1	15	1.5	53	11.4	13	·	·	5	·	·	·	1	21	19	14	1	5	2	·
XII	11	1.3	10	1.4	4.5	1.1	4	1.1	13.5	2.1	9.5	1.5	9	1.3	12.5	1.6	19	1.2	45	5.0	18	11	16	29	·	·	·	1	15	14	4	·	6	17	·
Rok	69	2.0	45	1.5	75	1.3	85	1.7	109	1.6	74.5	1.8	134.5	2.0	166	2.2	337	1.4	659	42.0	14.V	21	48	118	24	11	6	27	157	170	106	18	59	91	21

Opoczno $H_s = 180\,m$ $h_w = 14{,}6\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R fo
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	28	6.2	27	–	8	–	·	–	–	·	12	12	8	·	1	3	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	33	6.5	12	–	13	–	·	–	–	·	20	17	8	·	1	17	1
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	61	15.1	12	7	11	24	·	–	–	6	20	14	10	3	6	16	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	57	21.6	26	·	·	·	4	–	–	2	9	14	8	1	·	·	2
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	169	48.6	14	·	·	2	·	–	–	2	13	24	24	4	4	·	5
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	81	32.3	4	·	·	·	6	–	–	5	10	10	8	3	·	·	1
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	73	21.2	16	·	·	·	6	–	–	2	7	15	11	2	·	·	4
VIII	4.5	1.9	2	1.5	4.5	3.0	8	2.6	19.5	2.7	20	4.0	22	5.5	5.5	3.5	7	3.4	66	25.8	15	·	·	·	6	2	1	2	8	15	10	2	·	·	3
IX	6	3.2	10	3.4	4	2.8	9	1.8	11.5	2.5	19	4.6	25	4.8	5.5	3.5	·	3.7	98	39.6	17	·	·	·	1	4	·	6	8	11	8	4	8	·	1
X	9.5	2.6	12	2.2	13.5	2.1	7	1.9	12	2.5	11.5	3.0	10	4.5	6.5	3.2	11	2.4	10	5.5	28	·	·	9	·	1	·	8	9	5	2	·	15	·	·
XI	10.5	3.0	14	4.9	21	3.8	11	3.2	5	3.3	12	4.9	11	3.5	3.5	2.7	2	3.8	56	9.0	15	·	·	9	·	·	·	1	21	15	13	·	5	·	·
XII	10	3.7	14	4.2	6.5	3.5	6.5	2.9	13.5	4.3	19	4.2	14	3.9	5.5	3.3	4	3.8	17	7.6	13	11	16	29	·	2	·	·	16	15	3	·	3	18	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	749	48.6	14.V	–	48	–	23	–	–	34	153	167	113	19	43	54	17

Sulejów $H_s = 186\,m$ $h_w - 14\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R fo
I	2.5	7.4	7	3.0	·	·	1.5	3.3	19	3.5	31.5	5.6	19	5.6	5.5	5.2	7	4.5	29	8.0	25	2	8	21	·	1	·		13	13	9	·	2	16	·
II	3.5	3.9	11.5	3.3	4.5	3.4	4	3.2	6	6.5	15	6.1	19	7.3	12.5	7.4	8	5.3	26	7.1	12	6	13	26	·	6	·		19	16	9	·	–	18	·
III	9.5	5.3	15.5	2.9	2.5	3.6	13	3.5	7	3.7	5.5	6.5	7	6.3	9	4.5	24	3.2	54	12.9	31	6	10	26	·	3	·	4	19	15	10	3	–	18	1
IV	5.5	2.5	11	3.7	3	2.8	13	3.8	11.5	3.7	11.5	5.2	9	4.1	12.5	4.6	13	3.4	65	29.1	26	·	·	·	4	·	·	4	6	13	9	2	–	·	1
V	2.5	3.4	3.5	2.6	5.5	1.3	7	2.5	7.5	1.9	10.5	3.2	25.5	5.1	10	3.2	21	2.7	153	28.2	14	·	·	2	·	3	·	·	15	23	21	4	–	·	5
VI	6.5	3.8	3	1.7	4	1.2	2.5	2.8	3	3.5	8	2.9	24	4.3	20	3.8	19	2.8	48	23.2	4	·	·	·	6	1	·	7	4	10	7	1	–	·	3
VII	4	3.0	5	3.4	1	2.0	2	2.0	2	2.0	18	3.1	22	3.8	14	3.5	25	2.4	64	27.5	22	·	·	·	5	1	1	3	7	12	10	2	–	·	7
VIII	1	3.0	2	1.5	·	·	4.5	3.0	9.5	2.6	12.5	3.2	33.5	4.4	13	4.0	17	3.0	60	23.5	15	·	·	·	7	·	·	4	9	17	12	2	–	·	4
IX	3	2.3	1.5	3.3	10.5	1.8	3.5	2.9	6.5	4.0	14.5	3.8	24.5	3.8	7	4.2	19	2.7	72	25.4	17	·	·	·	2	·	·	5	5	12	9	3	5	·	2
X	4	2.8	4	2.0	2	3.0	9	2.8	6	2.3	3	7.0	11	4.3	9	4.3	45	1.8	12	4.7	27	·	·	7	·	·	·	11	8	6	3	·	13	·	·
XI	9	1.4	11	4.9	14	1.9	19	3.5	4.5	3.9	6	3.8	16	3.9	2.5	3.8	8	3.0	40	8.0	19	·	·	9	·	·	·	1	19	17	8	·	1	3	·
XII	6.5	2.4	12	3.9	8	2.4	7	3.7	5	5.2	17.5	4.1	12.5	4.5	8.5	3.7	16	3.2	17	4.4	13	11	14	29	·	1	·	1	15	17	5	·	1	17	·
Rok	57.5	3.4	87	3.0	55	2.0	86	3.1	87.5	3.6	153.5	4.5	223	4.8	123.5	4.4	222	3.2	640	29.1	26.IV	25	45	120	24	16	1	40	139	171	112	17	–	72	23

Szczerców $H_s = 160\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R fo
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	41	9.0	25	2	4	23	·	–	–	·	13	11	9	·	–	–	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	58	16.2	12	4	11	27	·	–	–	·	20	17	12	2	–	–	
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	62	17.0	31	·	7	25	·	–	–	3	15	13	11	3	–	–	
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	57	21.0	26	·	·	·	7	–	–	3	7	12	11	1	–	–	1
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	156	34.0	14	·	·	3	·	–	–	·	12	23	20	6	–	·	3
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	41	15.5	4	·	·	·	9	–	–	3	9	9	9	1	–	·	2
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	31	8.0	2	·	·	·	9	–	–	1	8	10	9	·	–	·	2
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	85	22.2	17	·	·	·	8	–	–	2	7	18	14	2	–	·	4
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	88	32.5	17	·	·	·	4	–	–	1	12	12	8	3	–	·	1
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	20	9.5	27	·	·	6	·	–	–	1	10	5	4	·	–	·	
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	57	15.5	15	·	·	7	·	–	–	·	22	11	9	1	–	–	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	26	8.5	15	11	14	28	·	–	–	1	18	11	6	·	–	–	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	722	34.0	14.V	17	36	119	37	–	–	15	153	152	122	19	–	–	13

Oborniki Śląskie $\varphi = 51°18'$ $\lambda = 16°55'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.3	-1.8	9.9	22	-14.2	31	0.1	2.2	0.3	0.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	1.8	-3.8	7.7	12	-13.6	1	-2.3	0.2	-1.1	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	3.6	-3.3	14.7	31	-9.1	8	-1.8	2.4	-0.6	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	16.3	6.1	28.5	23	-0.2	30	8.9	14.2	9.5	10.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15.7	6.3	23.4	19	0.2	2,3	9.0	13.6	9.2	10.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	20.8	9.3	31.3	16	2.6	6	12.3	19.4	13.4	14.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.6	10.5	32.5	26	7.0	4,6	13.9	19.7	14.1	15.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	23.1	12.3	31.9	13	7.5	31	15.0	21.4	15.4	16.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	18.8	8.1	31.5	4	2.6	15	10.4	17.0	11.2	12.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	13.7	4.3	23.1	3	-4.5	23	5.9	12.4	7.3	8.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.6	2.2	17.1	8	-3.0	21	3.2	5.8	3.7	4.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-1.0	-6.2	7.2	13	-19.4	22	-4.8	-1.9	-4.6	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	12.0	3.7	32.5	26.VII	-19.4	22.XII	5.8	10.5	6.5	7.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kraśnik Dolny $\varphi = 51°17'$ $\lambda = 15°36'$

I	–	–	–	–	4.0	-1.1	11.8	22	-15.4	31	0.6	2.7	0.9	1.2	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.6	6.9	7.6
II	–	–	–	–	2.1	-3.4	7.3	7	-15.7	1	-1.3	0.9	-0.8	-0.5	–	–	–	–	–	–	–	–	–	–	–	–	9.8	8.7	8.2	8.9
III	–	–	–	–	3.7	-3.1	14.6	30	-8.1	7	-1.7	2.5	-0.5	0.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.9	5.3	6.5
IV	–	–	–	–	15.4	5.5	27.1	24,25	-0.2	11	6.9	13.5	8.9	9.6	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.3	5.4	6.1
V	–	–	–	–	15.1	8.1	23.8	19	1.9	1	9.3	13.5	9.8	10.6	–	–	–	–	–	–	–	–	–	–	–	–	7.7	8.0	6.0	7.2
VI	–	–	–	–	20.4	11.1	30.6	16	3.5	4,6	13.2	18.7	13.8	14.9	–	–	–	–	–	–	–	–	–	–	–	–	4.9	6.3	5.4	5.5
VII	–	–	–	–	20.8	10.2	32.1	26	4.5	9	14.1	19.0	14.6	15.6	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.7	5.7	6.1
VIII	–	–	–	–	21.8	11.5	30.7	13	6.6	21	15.1	19.8	15.3	16.3	–	–	–	–	–	–	–	–	–	–	–	–	5.8	7.3	5.2	6.1
IX	–	–	–	–	18.4	7.5	29.4	4	0.8	25	10.0	16.6	11.3	12.3	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.1	4.0	5.3
X	–	–	–	–	13.6	5.0	24.6	3	-3.1	22	5.9	12.5	7.4	8.3	–	–	–	–	–	–	–	–	–	–	–	–	7.6	5.5	5.3	6.1
XI	–	–	–	–	6.4	1.2	16.1	8	-3.4	21	2.5	5.6	3.2	3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.1	8.0	8.2
XII	–	–	–	–	-1.3	-6.9	7.5	12	-21.1	23	-4.8	-2.6	-4.1	-3.9	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.1	7.4	8.0
Rok	–	–	–	–	11.7	3.8	32.1	26.VII	-21.1	23.XII	5.8	10.2	6.6	7.3	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.0	6.1	6.8

Bolesławiec $\varphi = 51°16'$ $\lambda = 15°35'$

II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.3	12.1	31.0	13	8.0	21	15.0	19.6	15.2	16.2	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.6	5.0	6.5
IX	–	–	–	–	17.8	7.9	29.4	4	1.6	25	10.5	16.3	11.2	12.3	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.4	3.3	5.6
X	–	–	–	–	13.3	4.7	23.6	3	-2.1	22	6.3	12.1	7.6	8.4	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.1	4.2	5.9
XI	–	–	–	–	5.9	1.2	16.8	8	-3.6	21	2.3	5.3	3.2	3.5	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.0	7.8	7.9
XII	–	–	–	–	-1.3	-6.6	8.3	12	-19.3	23	-4.9	-2.6	-4.1	-3.9	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.6	7.6	7.7
Rok	–	–	–	–	–	–	–	–	-19.3	23.XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Motycz $\varphi = 51°15'$ $\lambda = 22°25'$

I	–	–	–	–	0.9	-3.3	5.6	22	-19.2	31	-1.6	-0.3	-1.2	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	-1.3	-6.7	3.8	13	-13.9	1	-4.6	-2.2	-3.5	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	0.3	-6.9	8.5	31	-19.0	26	-4.9	-0.9	-3.0	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	15.5	5.7	25.5	22	-0.1	8	8.2	14.1	9.8	10.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	14.8	6.9	21.2	28	-1.3	1	9.6	13.5	10.2	10.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	18.1	8.8	27.1	23	2.7	6	12.7	16.8	12.5	13.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	20.9	10.4	28.4	27	6.0	2	14.1	19.6	14.0	15.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.8	11.8	29.7	13	7.3	10,27	15.3	20.6	16.0	17.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	16.5	7.7	26.8	5	1.6	25	9.7	15.4	11.1	11.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	12.1	2.5	18.4	2	-3.5	16	4.4	11.5	6.4	7.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.1	1.6	18.2	1	-2.0	18	2.8	5.3	3.6	3.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-2.8	-8.0	2.9	13	-21.4	21	-5.9	-4.3	-5.5	-5.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	10.2	2.5	29.7	13.VIII	-21.4	21.XII	5.0	9.1	5.9	6.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Oborniki Śląskie — $H_s = 180\,m$ — $h_w = 12\,m$ — 1962

MIESIĄC	ROZKŁAD WIATRU °D, %D																		Średnia prędkość	OPAD R			LICZBA DNI (n)														
	N		NE		E		SE		S		SW		W		NW		C						Temperatura T				Wiatr				Opad R						
	n	%	n	%	n	%	n	%	n	%	n	%	n	%	n	%	n	%		Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	≥10	≥15	◐	●	≥0.1	≥1.0	≥10.0	≡	⊞	⊠
I	7	2.9	0.5	3.0	1.5	3.3	4.5	3.7	9	3.1	11.5	2.3	16	2.5	14	3.0	29	1.9		28	4.8	26	1	5	16	·	·	·	–	–	15	9	·	1	16	·
II	15.5	3.8	3	3.2	15	2.3	4	2.0	1.5	3.7	3	3.5	10	5.7	23	4.0	9	3.3		51	11.9	12	2	10	25	·	2	·	–	–	17	11	1	2	18	·
III	6	2.8	2.5	3.0	14.5	2.2	9.5	2.2	12.5	2.5	8	3.1	9.5	2.8	21.5	3.4	9	2.5		56	16.4	5	·	4	26	·	·	·	–	–	9	8	3	2	–	·
IV	7.5	1.9	6	2.2	7	3.0	4	3.4	10.5	3.1	8.5	2.8	12	2.8	18.5	2.6	16	2.2		28	9.4	28	·	·	1	8	·	·	–	–	13	7	·	·	·	2
V	7.5	1.5	4.5	1.3	3	2.0	3	2.2	3.5	2.4	6.5	2.3	25.5	2.2	22.5	2.5	11	2.0		104	23.5	14	·	·	·	·	·	·	–	–	21	16	3	2	·	2
VI	17.5	1.9	3	1.2	1	2.5	3	1.5	7.5	1.3	9	2.4	10.5	2.8	22.5	1.7	16	1.6		18	7.0	28	·	·	·	8	·	·	–	–	8	8	·	·	·	1
VII	8.5	1.6	4.5	1.7	2	1.5	0.5	3.0	1.5	2.3	11	2.1	26.5	2.2	18.5	2.6	20	1.7		39	6.7	13	·	·	·	7	·	·	–	–	15	11	·	1	·	5
VIII	3.5	1.6	3	2.5	1.5	2.3	2.5	2.0	1	1.0	16.5	2.3	3.6	2.3	18	2.1	11	2.0		44	7.4	17	·	·	·	10	·	·	–	–	13	12	·	·	·	3
IX	2	2.0	·	·	12	2.2	2	3.5	10	1.6	4	2.0	29.5	2.5	14.5	2.1	16	1.8		52	8.9	6	·	·	·	4	·	·	–	–	11	9	·	6	·	·
X	9	1.3	6	2.0	19.5	1.7	1.5	2.0	6	1.5	1	2.0	7	2.1	17	1.4	26	1.2		43	15.4	31	·	·	6	·	·	·	–	–	8	5	2	13	·	·
XI	0.5	1.0	18	2.9	9.5	2.5	19.5	3.5	1	1.5	2	3.0	2.5	1.0	23	2.0	14	2.2		50	14.5	1	·	·	6	·	·	·	–	–	12	9	1	8	·	·
XII	4	2.9	6.5	2.6	25.5	3.3	·	·	7	3.7	9	2.8	12.5	3.1	13.5	2.7	15	2.6		38	15.6	15	9	15	26	·	·	·	–	–	9	7	1	2	14	·
Rok	88.5	2.1	57.5	2.1	112	2.4	54	2.4	71	2.3	90	2.8	197.5	2.7	232.5	2.5	192	2.1		551	23.5	14.V	12	34	106	37	2	·	–	–	151	112	11	37	–	13

Kraśnik Dolny — $H_s = 180\,m$ — $h_w = 10.8\,m$

I	4.5	3.2	2	1.0	2	1.0	·	·	3.5	2.1	15	5.9	36	3.7	16	4.6	14	3.4		28	10.2	24	1	4	12	·	3		·	17	11	6	1	·	3	·
II	9	5.6	5	3.4	12	2.7	·	·	·	·	2	17.0	18.5	6.3	25.5	7.2	12	5.2		40	13.3	12	2	9	19	·	5	4	·	20	12	8	1	1	12	·
III	8.5	1.6	3.5	1.6	15	2.6	1	5.0	1	3.0	5.5	2.5	15.5	3.1	6	4.7	37	1.7		28	9.1	5	·	4	26	·	·	·	3	13	11	7	·	6	8	·
IV	4.5	2.6	7	3.4	4.5	3.1	2	4.0	1.5	5.7	8	3.8	23	3.1	10.5	3.9	29	2.3		53	9.8	28	·	·	1	4	·	·	4	8	15	12	·	6	·	1
V	3	2.3	1	3.0	2	3.0	2	1.0	1.5	2.3	12	4.2	32	2.8	6.5	3.5	33	2.0		110	15.3	12	·	·	·	·	·	·	·	12	20	18	4	1	·	3
VI	12.5	1.9	0.5	3.0	4	1.8	2.5	2.0	3.5	2.0	10	3.3	19	3.9	11	2.8	27	2.0		15	5.0	28	·	·	·	8	·	·	4	6	6	6	·	·	·	2
VII	·	·	0.5	1.0	5.5	1.8	1	2.5	1	1.0	11	4.2	36	2.3	3	3.7	35	1.7		45	14.3	21	·	·	·	5	·	·	1	10	12	8	1	4	·	6
VIII	·	·	2	3.0	2	1.0	·	·	2	4.5	11	4.4	37	3.4	2	4.8	37	2.1		60	13.7	4	·	·	·	7	·	·	2	9	16	10	1	2	·	5
IX	1	1.0	0.5	3.0	7.5	3.0	3	3.3	1	1.0	5	4.2	28	2.9	10	3.6	34	1.9		65	18.7	16	·	·	·	3	1	·	6	7	15	10	3	6	·	·
X	5	1.8	1	1.0	15.5	2.5	1.5	2.3	·	·	2.5	2.2	26	2.6	1.5	1.7	40	1.4		21	14.2	31	·	·	8	·	·	·	4	12	8	3	1	14	·	·
XI	3.5	1.6	9	3.4	11.5	2.2	2	4.0	2	3.5	7	4.1	21	2.6	·	·	34	1.8		28	11.2	1	·	·	11	·	·	·	1	20	12	7	1	12	·	·
XII	5	2.3	11.5	3.5	5.5	3.7	2	2.0	3	2.8	4	4.4	30	3.7	7	4.0	25	2.6		28	8.6	15	10	14	26	·	2	·	1	20	9	6	·	4	14	·
Rok	56.5	2.0	43.5	2.5	87	2.4	17	2.2	20	2.3	93	5.0	322	3.4	99	3.7	357	2.3		521	18.7	16.IX	13	31	103	27	11	4	26	154	147	101	13	56	37	17

Bolesławiec — $H_s = 208\,m$ — $h_w = 12.6\,m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	3	2.7	2	3.2	2.5	1.4	2.5	1.6	7.5	3.3	16.5	3.8	26.5	4.1	6.5	3.7	26	2.6		63	10.0	5	·	·	·	6	·	·	1	7	18	13	1	1	·	3
IX	1.5	1.0	0.5	1.0	8.5	2.8	6	3.6	5	1.3	12	3.5	26	3.7	8.5	2.4	22	2.4		62	19.1	16	·	·	·	3	1	·	4	6	14	8	2	·	·	·
X	1.	1.0	2.5	1.0	8	2.2	7	2.2	2.5	1.2	11	1.9	15	2.1	7	2.2	39	1.2		28	16.8	31	·	·	6	·	·	·	6	12	16	4	1	6	·	·
XI	4.5	1.0	3	3.2	12	2.4	12.5	4.4	1.5	4.0	4.5	2.2	18	2.7	4	2.0	30	1.9		29	12.7	1	·	1	11	·	1	·	·	17	17	7	1	5	·	·
XII	1.5	1.7	4	1.4	17	1.9	3	2.0	4	1.9	15.5	3.4	16	2.9	5	1.4	27	1.7		34	10.5	15	11	15	26	·	2	·	1	15	16	5	1	·	16	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Motycz — $H_s = 213\,m$ — $h_w = 14\,m$

I	2	7.5	5	7.4	3	7.0		·	1.8	4.3	3.5	4.1	22.5	5.6	7.5	5.7	·	5.0		19	7.3	25	2	8	25	·	·		–	–	11	5	·	2	22	·
II	8.5	3.5	5.5	4.9	12.5	5.1	4.5	4.4	6.5	3.9	16.5	5.2	13.5	7.3	13.5	7.3	3	5.3		21	7.2	12	6	16	28	·	7	3	–	–	18	7		1	28	1
III	9.5	6.7	8.5	5.1	15	3.7	12	5.0	13.5	3.9	5	3.9	10	5.9	13.5	4.9	6	4.5		38	7.5	12	7	18	29	·	6		–	–	14	10	·	2	24	·
IV	5	3.5	6.5	4.6	17	3.7	11.5	4.7	10.5	3.6	13.5	3.5	9	5.3	7	5.8	10	3.7		48	6.7	28	·	·	1	3	1	·	–	–	12	11	·	1	·	2
V	4	3.5	2.5	4.2	4	4.0	5.5	3.7	11	2.7	17.5	3.4	22.5	4.3	16	4.7	10	3.5		139	37.8	15	·	·	1	·	2	1	–	–	27	16	3	·	·	9
VI	1.5	5.3	7.5	3.2	0.5	3.0	6	2.7	9.5	2.8	9	3.7	26	4.1	12.5	4.1	4	3.8		131	51.0	4	·	·	·	3	1	·	–	–	12	11	3	·	·	2
VII	6	3.5	6.5	3.0	5	2.6	5	2.9	8.5	2.4	13.5	2.7	32.5	3.7	13	4.0	3	3.2		77	23.9	18	·	·	·	4	·	·	–	–	15	12	2	·	·	9
VIII	1.5	1.7	1	3.0	3	2.7	8	3.3	13	3.1	18.5	2.6	29.5	4.3	7.5	4.2	11	3.1		40	10.1	19	·	·	·	6	·	·	–	–	11	8	1	3	·	5
IX	1.5	3.0	4.5	3.9	8	3.1	4	3.4	12	3.5	22.5	3.6	26	5.0	6.5	4.8	5	3.8		72	27.8	18	·	·	·	2	·	·	–	–	15	10	2	3	·	3
X	5.5	3.1	5.5	3.3	14	2.5	14.5	2.6	4	2.0	17.5	2.8	16.5	4.1	8.5	4.2	7	2.9		4	2.7	14	·	·	7	·	·	·	–	–	9	1	·	16	·	·
XI	11.5	3.1	5	5.2	20.5	6.5	21.5	5.2	6	3.2	8.5	4.2	10.5	4.4	6.5	3.7	·	4.8		60	9.2	15	·	1	8	·	2	·	–	–	19	13	·	10	3	·
XII	12.5	3.4	10.5	4.5	6	3.6	4.5	3.8	13.5	4.7	19	4.0	20.5	3.9	5.5	5.7	1	4.1		13	4.4	18	11	17	30	·	1	·	–	–	14	3	·	3	22	·
Rok	82.5	4.0	68.5	4.4	108.5	4.0	97	3.5	126	3.3	156	3.6	239	4.8	117.5	4.9	60	4.0		662	51.0	4.VI	26	60	129	18	20	4	–	–	177	107	11	41	99	31

Lublin $\varphi = 51°14'$ $\lambda = 22°34'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA t						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o\,m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	995.0	1016.1	973.4	1017.3	1.6	−2.5	7.4	22	−18.7	31	−1.1	0.4	−0.8	−0.6	5.3	5.3	5.2	5.3	91	82	87	87	0.5	1.2	0.8	0.8	81	71	75	76
II	993.5	1011.0	961.8	1015.9	−0.5	−6.3	3.7	13	−12.8	1	−4.2	−1.7	−3.1	−3.0	4.2	4.6	4.6	4.5	91	84	91	89	0.4	0.9	0.4	0.6	88	90	80	86
III	989.5	1007.1	970.2	1011.7	1.6	−6.0	11.0	31	−17.0	21	−4.4	0.3	−2.4	−2.2	4.4	4.9	4.8	4.7	93	75	89	86	0.3	1.6	0.5	0.8	84	74	74	77
IV	993.0	1007.1	969.7	1014.3	16.9	5.3	27.1	24	−0.4	30	7.6	15.3	10.2	10.8	9.5	9.3	10.2	9.7	89	57	80	75	1.3	9.6	2.9	4.6	67	61	48	59
V	991.8	1000.0	973.5	1012.9	16.0	6.8	22.4	28	−1.0	1	9.8	14.4	10.8	11.4	11.4	11.4	11.8	11.5	92	69	89	83	1.1	5.7	1.5	2.8	74	84	57	72
VI	996.1	1005.5	986.6	1017.3	19.1	8.9	29.2	16	3.3	6	12.8	17.5	13.9	14.5	13.0	12.4	13.3	12.9	85	63	82	77	2.4	8.9	3.2	4.8	64	74	55	64
VII	993.5	1003.9	981.0	1014.4	21.4	10.5	28.6	26	5.9	5	14.1	20.0	15.1	16.1	14.6	14.5	15.0	14.7	90	62	87	80	1.7	9.5	2.4	4.5	57	69	5.0	5.9
VIII	995.1	1003.7	984.8	1016.0	22.7	11.4	30.4	7	4.4	27	14.5	21.2	16.2	17.0	15.5	15.6	16.6	15.9	93	63	89	82	1.2	10.1	2.2	4.5	62	66	48	5.9
IX	995.7	1010.1	980.7	1016.9	17.6	7.0	27.5	5	1.4	15	9.4	16.1	11.3	12.0	11.2	12.1	12.3	11.9	94	68	91	84	0.9	6.9	1.4	3.1	61	72	4.2	5.8
X	1001.4	1015.4	988.5	1023.1	13.0	2.2	19.9	2	−4.6	16	4.0	12.0	6.3	7.2	8.2	10.1	9.3	9.2	98	71	95	88	0.2	4.3	0.5	1.7	82	64	4.9	6.5
XI	996.8	1010.2	982.6	1018.7	6.9	2.1	19.4	1	−1.9	18	3.4	6.0	4.1	4.4	7.5	7.9	7.7	7.7	94	84	91	90	0.5	1.9	0.8	1.1	91	84	8.0	8.5
XII	995.1	1021.4	953.9	1017.7	−2.3	−7.7	3.6	13	−19.2	21, 22	−5.4	−3.6	−5.1	−4.8	4.0	4.3	4.1	4.1	91	86	90	89	0.4	0.7	0.5	0.5	84	77	7.3	7.8
Rok	994.7	1021.4	953.9	1016.3	11.2	2.6	30.4	7. VIII	−19.2	21.22.XII	5.0	9.8	6.4	6.9	9.1	9.4	9.6	9.4	92	72	88	84	0.9	5.1	1.4	2.5	75	74	6.1	7.0

Felin $\varphi = 51°14'$ $\lambda = 22°38'$

I	—	—	—	—	1.0	−2.9	5.7	22	−18.9	31	−1.4	−0.1	−1.0	−0.9	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.1	6.5	7.4
II	—	—	—	—	−1.2	−7.0	3.1	13	−13.7	16	−4.5	−2.3	−3.3	−3.4	—	—	—	—	—	—	—	—	—	—	—	—	8.8	9.4	7.5	8.6
III	—	—	—	—	0.3	−6.6	8.6	6	−18.9	26	−4.3	−0.6	−2.5	−2.5	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.5	7.3	7.4
IV	—	—	—	—	15.5	5.6	25.4	22	−0.1	3, 8	7.8	14.3	10.3	10.7	—	—	—	—	—	—	—	—	—	—	—	—	4.8	4.5	4.0	4.4
V	—	—	—	—	15.2	6.7	21.7	28	−1.1	1	9.6	13.8	10.8	11.2	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.4	5.6	6.7
VI	—	—	—	—	18.1	9.3	26.9	16	2.8	7	12.7	16.8	13.6	14.2	—	—	—	—	—	—	—	—	—	—	—	—	5.6	6.2	5.7	5.8
VII	—	—	—	—	20.5	10.8	28.1	27	6.0	2	14.2	19.4	14.8	15.8	—	—	—	—	—	—	—	—	—	—	—	—	5.5	6.3	5.3	5.7
VIII	—	—	—	—	22.1	12.0	29.4	13	7.4	31	14.9	20.7	16.1	16.9	—	—	—	—	—	—	—	—	—	—	—	—	5.7	5.7	4.5	5.3
IX	—	—	—	—	16.9	7.9	27.1	5	2.1	15	9.8	15.3	11.6	12.1	—	—	—	—	—	—	—	—	—	—	—	—	5.6	6.2	4.2	5.3
X	—	—	—	—	12.2	3.0	18.9	2	−2.4	16, 17	4.2	11.2	7.2	7.4	—	—	—	—	—	—	—	—	—	—	—	—	7.2	5.6	4.3	5.7
XI	—	—	—	—	6.4	2.2	18.5	1	−1.6	18	3.2	5.6	3.9	4.2	—	—	—	—	—	—	—	—	—	—	—	—	9.3	7.9	7.9	8.4
XII	—	—	—	—	−2.8	−7.8	3.2	13	−21.5	22	−5.7	−4.3	−5.4	−5.2	—	—	—	—	—	—	—	—	—	—	—	—	9.0	7.7	7.3	8.0
Rok	—	—	—	—	10.4	2.8	29.4	13. VIII	−21.5	22. XII	5.0	9.2	6.3	6.7	—	—	—	—	—	—	—	—	—	—	—	—	7.0	6.8	5.8	6.5

Legnica $\varphi = 51°13'$ $\lambda = 16°10'$

I	1001.1	1023.7	976.0	1016.9	4.5	−1.1	10.8	22	−15.2	31	1.0	3.0	1.1	1.6	5.5	5.7	5.6	5.6	8.2	7.4	8.2	7.9	1.4	2.2	1.3	1.6	7.0	7.8	7.8	7.5
II	1001.6	1021.1	971.6	1017.5	2.4	−3.3	9.4	12	−17.6	1	−1.4	1.0	−0.4	−0.3	4.9	5.4	5.2	5.2	8.6	8.0	8.6	8.4	0.9	1.4	0.9	1.1	8.7	8.6	7.0	8.1
III	995.9	1014.1	972.8	1011.8	3.6	−2.6	15.0	3.0	−7.7	8	−1.3	2.4	0.1	0.3	5.2	5.3	5.2	5.2	8.9	7.1	8.3	8.1	0.7	2.3	1.1	1.4	8.3	7.8	5.8	7.3
IV	998.5	1011.1	972.4	1013.8	16.0	5.5	28.0	2.4	−1.8	11	7.4	14.2	10.0	10.4	9.0	8.9	9.2	9.0	8.6	5.7	7.4	7.2	1.6	9.1	3.8	4.8	7.2	7.4	5.4	6.7
V	998.3	1004.6	990.0	1013.5	15.7	7.0	23.8	19	−0.9	1	9.5	14.0	10.7	11.2	10.4	10.3	11.1	10.6	8.6	6.4	8.5	7.8	1.7	6.2	2.1	3.3	7.5	8.3	8.1	8.0
VI	1004.0	1014.8	994.8	1019.0	20.6	9.7	31.1	16	2.6	6	13.2	18.9	14.9	15.5	12.3	11.8	12.5	12.2	7.8	5.2	7.1	6.7	3.5	11.5	5.1	6.7	5.4	6.6	5.3	5.8
VII	1000.1	1010.5	985.1	1015.1	21.5	10.5	33.6	2.6	5.0	9	13.9	20.0	15.4	16.2	14.0	13.0	14.3	13.8	8.7	5.7	8.1	7.5	2.2	11.3	3.5	5.7	5.9	7.2	6.0	6.4
VIII	1001.1	1009.2	987.9	1016.0	23.0	12.5	32.4	13	6.4	27	15.1	21.2	16.6	17.4	14.8	14.6	15.1	14.8	8.6	5.8	8.0	7.5	2.5	11.3	3.9	5.9	6.1	7.3	4.8	6.1
IX	1001.4	1012.9	984.3	1016.6	19.3	8.0	31.2	4	0.2	15	10.1	17.6	12.1	13.0	11.2	11.7	11.6	11.5	9.0	6.0	8.3	7.8	1.6	9.6	2.9	4.7	7.8	6.3	3.9	6.0
X	1007.0	1019.6	993.5	1022.6	13.8	4.2	25.4	3	−3.9	26	5.1	12.5	7.6	8.2	9.0	10.4	9.8	9.7	9.8	7.3	9.2	8.8	0.3	4.9	1.0	2.1	6.9	6.1	4.4	5.8
XI	1000.7	1019.5	983.0	1016.4	7.0	2.2	12.1	7	−2.2	17	3.4	6.1	4.0	4.4	7.3	8.1	7.4	7.6	9.2	8.4	9.0	8.9	0.6	1.8	0.9	1.1	8.3	8.5	7.8	8.2
XII	1001.2	1029.4	957.4	1017.3	−0.6	−6.7	6.9	12	−19.9	24	−4.6	−2.4	−3.7	−3.6	4.1	4.5	4.2	4.3	8.7	8.2	8.5	8.5	0.6	1.1	0.9	0.9	8.4	8.4	8.1	8.3
Rok	1000.9	1029.4	957.4	1016.3	12.2	3.8	33.6	26. VII	−19.9	24. XII	6.0	10.7	7.4	7.9	9.0	9.1	9.3	9.1	8.7	6.8	8.3	7.9	1.5	6.1	2.3	3.3	7.3	7.5	6.2	7.0

Wieluń $\varphi = 51°13'$ $\lambda = 18°35'$

I	992.2	1013.2	967.7	1017.0	2.3	−2.6	7.9	22	−16.3	31	−0.7	1.2	−0.7	−0.2	5.1	5.3	5.1	5.2	8.5	7.9	8.4	8.3	0.9	1.5	1.0	1.1	6.8	7.6	7.7	7.4
II	991.7	1010.5	961.8	1016.7	0.7	−4.6	6.0	12, 13	−15.6	1	−3.3	−0.8	−1.6	−1.8	4.2	4.8	4.8	4.6	8.5	8.1	8.5	8.4	0.8	1.1	0.8	0.9	8.7	9.0	7.4	8.4
III	986.8	1004.2	965.8	1011.5	3.1	−3.8	15.2	31	−9.3	15	−2.5	1.8	−0.7	−0.5	4.6	5.1	5.0	4.9	8.7	7.0	8.3	8.0	0.6	2.2	1.0	1.3	8.2	7.8	7.1	7.7
IV	990.0	1002.9	964.1	1014.0	16.1	5.7	27.8	2.3	0.7	2	8.0	14.7	9.6	10.5	9.0	8.9	9.2	9.0	8.3	5.5	7.6	7.1	2.1	9.7	3.3	5.0	7.9	6.9	5.3	6.7
V	989.4	995.9	976.0	1013.4	15.5	6.7	23.0	8	−1.3	1	9.2	13.7	10.0	10.7	10.4	10.3	10.7	10.5	8.7	6.7	8.6	8.0	1.5	5.9	1.8	3.1	7.8	7.9	7.4	7.7
VI	994.9	1004.9	984.6	1018.5	20.1	9.5	30.8	16	3.0	3	13.1	18.3	13.8	14.8	12.1	11.4	12.2	11.9	7.7	5.4	7.5	6.9	3.6	11.2	4.2	6.3	5.8	6.9	5.9	6.2
VII	991.4	1001.6	977.9	1014.8	21.6	10.6	32.5	2.6	6.0	30	14.2	19.9	14.6	15.8	13.8	13.5	13.7	13.7	8.4	5.9	8.1	7.5	2.7	10.6	3.3	5.5	6.2	6.4	6.3	6.3
VIII	992.5	1000.7	979.3	1015.9	22.8	12.4	31.8	7	8.2	10	14.9	21.4	15.6	16.9	14.7	15.2	15.1	15.0	8.6	6.0	8.4	7.7	2.3	11.2	2.9	5.5	7.0	7.5	5.4	6.6
IX	992.9	1005.2	977.1	1016.9	17.8	7.9	29.9	4	2.4	27	10.0	16.2	11.2	12.2	10.9	12.0	11.3	11.4	8.8	6.7	8.5	8.0	1.7	7.4	2.3	3.8	7.5	7.0	3.7	6.1
X	998.4	1011.5	985.8	1022.7	13.5	4.1	22.3	1	−1.8	23	5.9	12.5	7.0	8.1	9.1	10.4	9.3	9.6	9.5	7.1	9.0	8.5	0.5	4.6	1.0	2.0	6.9	4.8	3.4	5.0
XI	992.5	1009.0	975.3	1016.9	6.1	1.9	16.4	8	−3.3	24	2.9	5.3	3.6	3.8	7.1	7.8	7.4	7.4	9.3	8.5	9.2	9.0	0.5	1.5	0.7	0.9	8.9	8.3	8.1	8.4
XII	992.1	1020.0	948.6	1017.4	−2.0	−7.5	4.6	12	−21.9	22	−5.5	−3.1	−4.9	−4.6	3.9	4.3	3.9	4.0	8.7	8.3	8.5	8.5	0.5	0.9	0.7	0.7	8.2	8.1	7.3	7.9
Rok	992.1	1020.0	948.6	1016.2	11.5	3.4	32.5	26. VII	−21.9	22. XII	5.5	10.1	6.5	7.2	8.7	9.1	9.0	8.9	8.6	6.9	8.4	8.0	1.5	5.6	1.9	3.0	7.5	7.4	6.2	7.0

Lublin $H_s = 171m$ $H_b = 176{,}7m$ $h_w = 10m$ 1962

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◉	●	Opad R R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R
I	3.5	5.4	5.5	4.0	·	·	1.5	3.7	20.5	3.9	41	4.3	18	4.9	3	4.8	·	4.3	26	8.1	13	2	6	20	·	2	·	1	18	17	6	·	·	19	·
II	9	4.1	8.5	3.2	10	3.4	5	3.4	6.5	5.0	16	6.5	17.5	6.5	8.5	6.3	3	5.0	67	18.8	12	6	14	28	·	9	6	·	20	23	14	2	2	28	·
III	10	4.7	9.5	2.4	10.5	3.1	11	3.8	13	2.8	6.5	4.5	8.5	5.1	16	3.7	8	3.4	59	17.3	16	5	11	27	·	6	3	·	16	16	10	1	4	24	·
IV	6.5	4.1	12.5	4.0	18.5	3.2	5	3.6	14	3.4	13	3.7	12	3.2	2.5	6.6	6	3.4	42	7.4	28	·	·	1	5	3	1	4	8	12	9	·	1	·	·
V	7.5	2.0	2	2.5	6	2.9	7	2.7	9.5	3.6	20.5	3.7	21	3.9	11.5	2.6	8	3.1	118	32.5	15	·	·	3	·	3	3	·	12	27	16	2	2	·	7
VI	12	4.2	5.5	3.2	4	2.2	1	2.0	8.5	2.6	18.5	4.1	17	3.9	17.5	3.3	6	3.3	109	36.1	4	·	·	·	6	4	1	1	11	12	11	4	·	·	2
VII	7	2.6	7.5	1.5	2	2.5	4.5	1.7	9	2.2	22.5	3.0	18.5	3.4	11	2.4	11	2.4	109	32.1	18	·	·	·	4	·	·	2	5	18	16	3	1	·	7
VIII	2	2.5	3	3.3	6	1.6	1	1.5	8.5	3.2	32.5	3.2	14	3.5	3	4.0	23	2.4	50	13.3	5	·	·	·	8	4	·	3	6	11	8	3	6	·	5
IX	5	1.6	5.5	2.4	3	1.3	3.5	1.4	11.5	2.8	32.5	3.5	11.5	3.9	4.5	3.8	13	2.6	69	27.5	18	·	·	·	2	2	·	3	8	16	11	1	8	·	3
X	3.5	2.1	4.5	2.3	9	1.9	7.5	2.2	3.5	2.1	15.5	3.8	7.5	3.7	9	2.5	33	1.8	2	1.6	14	·	·	10	·	3	·	1	10	6	1	·	18	·	·
XI	10.5	2.4	9	4.2	16.5	4.2	22.5	3.6	2	4.5	13.5	4.0	6	3.5	6	2.6	4	3.5	60	8.7	23	·	·	6	·	4	·	·	20	19	13	·	7	3	·
XII	11	2.6	15.5	3.6	3.5	4.0	4.5	2.7	14.5	4.7	24.5	3.9	14.5	2.8	4	4.0	4	3.4	19	5.3	18	11	16	30	·	3	·	1	19	15	5	·	5	22	·
Rok	87.5	3.2	88.5	3.0	89	2.5	74	2.7	118	3.4	256.5	4.0	166	4.0	96.5	3.9	119	3.2	730	36.1	4 VI	24	47	125	25	43	14	16	153	192	120	16	54	96	24

Felin $H_s = 215m$ $h_w = 13m$

I	7	6.2	3	2.8	·	·	·	·	23	2.0	31	2.0	18.5	2.4	4.5	1.4	6	2.3	—	—	—	2	9	22	·	1	·	1	15	—	—	—	·	—	—
II	9	1.1	5	2.2	13	2.0	2	2.8	10	5.7	12.5	5.6	13	3.3	12.5	5.2	7	3.4	20	7.5	12	5	16	28	·	4	2	·	18	16	8	·	1	—	—
III	14.5	4.1	8.5	4.3	8	2.2	7.5	4.1	14	2.1	8	1.8	11.5	2.9	3	1.5	18	2.4	31	6.8	12	5	16	30	·	2	1	1	18	12	8	·	4	—	—
IV	12	2.7	5.5	1.6	8	1.9	6.5	2.5	5	3.4	14	2.2	5	2.0	5	3.4	29	1.6	39	9.1	27	·	·	2	1	2	·	8	6	11	9	·	3	·	—
V	5.5	1.2	·	·	4.5	1.1	0.5	2.0	9	5.2	10	4.7	20	1.9	8.5	1.1	35	1.7	107	28.8	15	·	·	1	·	2	2	1	9	19	13	4	1	·	—
VI	19	3.6	·	·	2	1.0	2	1.0	1.5	1.0	10.5	2.1	17	1.5	10	1.2	28	1.5	108	35.0	4	·	·	·	3	·	·	5	11	12	11	3	·	·	—
VII	12.5	1.8	2.5	1.6	0.5	1.0	4	1.1	6	2.2	14.5	1.6	19	1.9	15	1.7	19	1.4	102	27.9	18	·	·	·	4	·	·	2	7	17	13	4	·	·	—
VIII	5	1.3	5	2.2	2	1.5	8.5	2.6	5.5	2.5	20.5	2.5	24	2.4	7.5	2.5	15	2.0	45	15.8	1	·	·	·	5	·	·	6	6	11	8	1	2	·	—
IX	3.5	1.4	6	1.8	4.5	1.9	2.5	1.6	11.5	2.8	20	3.3	23.5	2.5	11.5	2.0	7	2.3	69	26.4	18	·	·	·	2	·	·	7	7	15	11	1	4	·	—
X	5	1.7	7.5	1.7	11.5	2.3	4	3.2	4	2.6	12.5	4.0	17	3.9	11.5	3.3	20	2.4	2	1.1	14	·	·	7	·	1	·	4	9	3	1	·	13	·	—
XI	10	3.2	8.5	5.1	17	6.7	20	5.0	6	6.6	9.5	5.9	7	4.1	8	3.4	4	4.9	56	9.0	15	·	1	6	·	2	·	·	20	17	13	·	7	—	—
XII	17	4.2	9.5	4.5	1	3.5	4.5	3.9	11	7.5	21.5	5.6	15	3.4	9.5	4.1	4	4.6	13	4.2	18	11	18	30	·	4	·	1	17	15	3	·	3	—	—
Rok	120	2.7	61	2.3	72	2.1	62	2.5	106.5	3.6	184.5	3.4	190.5	2.7	106.5	2.6	192	2.5	—	35.0	4.VI	23	60	126	15	18	5	36	143	—	—	—	38	—	—

Legnica $H_s = 121m$ $H_b = 126.3m$ $h_w = 12m$

I	6.5	3.6	0.5	3.0		·	0.5	3.0	17.5	3.8	20	2.5	36	3.5	9	3.3	3	3.2	36	10.9	24	1	4	15	·	1	1	·	14	13	8	1	1	4	·
II	6	3.3	6.5	4.0	6	2.4	5.5	3.2	7.5	2.5	2.5	2.8	29	5.4	11	5.6	10	3.8	35	7.5	12	2	10	21	·	6	2	·	16	13	9	·	1	14	·
III	5	4.4	7.5	2.1	7.5	1.9	13	3.2	6.5	2.8	4	3.0	11	3.4	17.5	3.6	21	2.4	40	13.6	5	·	4	24	·	2	·	·	14	10	7	1	2	11	·
IV	1	3.5	6.5	2.2	2	2.0	11	4.0	7	4.1	4	3.0	18	2.9	24.5	3.4	16	2.7	35	15.4	28	·	·	1	4	5	·	4	14	14	7	1	·	·	1
V	5	2.2	2	1.5	2.5	2.0	7	2.7	4.5	2.2	7.5	2.1	38	2.7	19.5	2.5	7	2.3	93	27.2	14	·	·	1	·	1	1	·	17	20	15	2	·	·	3
VI	4	3.2	3	1.3	·	·	4	1.9	2.5	1.9	2.5	2.0	29.5	3.0	27.5	3.1	12	2.4	20	7.8	3	·	·	·	7	·	·	5	9	9	7	·	·	·	3
VII	4.5	2.2	3	2.2	5.5	2.0	5	1.7	2.5	2.2	5	2.4	35	2.3	17.5	2.4	15	1.9	53	7.8	13	·	·	·	8	·	·	2	11	17	15	·	2	·	7
VIII	1	2.0	2.5	1.8	3.5	1.6	4	1.0	6.5	2.0	6	2.3	41.5	2.8	13	3.3	15	2.2	36	7.7	5	·	·	·	10	·	·	3	9	14	9	·	·	·	2
IX	1	6.0	0.5	2.0	9	1.9	8	3.1	5.5	1.7	1.5	1.0	31.5	2.9	21	2.5	12	2.3	50	18.0	18	·	·	·	5	4	·	3	8	12	5	2	6	·	1
X	2	3.0	3.5	2.0	9	2.3	12.5	2.4	3	2.8	5.5	1.2	17.5	2.0	20	2.4	20	1.7	32	14.1	31	·	·	8	1	·	·	5	10	9	6	1	16	·	·
XI	0.5	1.0	12.5	2.1	8	2.8	17.5	4.0	8	3.2	2	1.5	26	2.1	11.5	1.6	4	2.4	38	13.0	1	·	·	7	·	·	·	1	19	12	8	1	5	·	·
XII	4.5	2.4	7	2.1	12	2.5	7.5	2.5	8	3.5	3.5	3.0	23.5	2.9	14	2.5	13	2.3	21	8.3	17	9	15	24	·	1	1	·	23	11	4	·	3	14	·
Rok	41	3.1	55	2.2	65	1.8	95.5	2.7	84	2.7	64	2.2	336.5	3.0	206	3.0	148	2.5	489	27.2	14.V	12	33	101	35	20	5	23	164	154	100	9	36	43	17

Wieluń $H_s = 195m$ $H_b = 198{,}4m$ $h_w = 11m$

I	3.5	5.3	6	2.2	·	·	·	·	21	4.3	32.5	3.9	23.5	3.3	6.5	3.6	·	3.8	31	5.7	25	2	7	20	·	4	1	1	15	17	11	·	·	13	·
II	5.5	3.9	9	2.1	8	2.1	5.5	1.8	10.5	2.8	11	4.9	24.5	5.3	10	6.1	·	4.1	52	12.1	17	4	12	23	·	7	4	1	20	20	12	2	2	20	·
III	13	4.2	8.5	2.9	17	2.2	7.5	2.6	11	1.8	12.5	1.6	15	3.2	8.5	1.9	·	2.6	70	16.9	5	·	8	26	·	2	1	2	19	17	11	3	4	14	·
IV	5.5	2.1	15	2.2	10	2.0	7.5	3.2	8.5	2.8	18.5	2.8	12	2.9	13	3.9	·	2.8	51	24.2	26	·	·	·	6	·	·	2	11	11	10	1	1	·	2
V	2	2.2	3	2.2	2.5	2.4	6.5	2.2	5	2.2	22.5	2.2	35.5	2.4	16	2.5	·	2.3	116	26.2	14	·	·	2	·	2	·	·	15	24	19	5	1	·	4
VI	14.5	3.6	1	1.5	1	1.5	5	2.3	2.5	1.8	8	2.3	33	3.0	24	2.4	1	2.8	30	8.6	4	·	·	·	7	1	·	1	11	12	6	·	·	·	4
VII	9.5	1.3	5.5	1.4	2.5	1.0	3.5	2.3	5.5	1.6	18	2.7	28.5	2.3	20	2.0	·	2.1	41	9.7	27	·	·	·	7	·	·	2	9	14	9	·	·	·	6
VIII	1	2.5	1	2.5	4	1.6	4	2.5	8.5	2.5	17	2.6	46.5	2.8	10	2.6	1	2.6	61	15.4	7	·	·	·	8	·	·	1	9	16	10	2	2	·	7
IX	1.5	3.0	1	1.5	16.5	1.7	2.5	3.0	8	2.8	22	2.5	27	2.4	11.5	2.5	·	2.3	67	22.2	18	·	·	·	4	·	·	4	10	11	7	2	4	·	2
X	6	2.3	10	1.6	14	2.0	15	1.8	4.5	2.3	8	2.7	18	2.0	14.5	1.7	3	1.9	19	4.6	31	·	·	6	·	·	·	8	9	10	6	·	16	·	·
XI	12	1.4	10.5	3.2	24.5	2.6	11	3.3	3	2.7	11.5	2.1	16	2.2	0.5	2.0	1	2.4	56	15.8	20	·	1	8	·	·	·	·	20	15	8	2	13	1	·
XII	9	1.8	12	2.4	14	1.6	3	1.2	13.5	4.7	16.5	3.0	16	2.2	9	1.4	·	2.5	27	5.9	16	11	14	28	·	2	·	2	18	16	8	·	6	23	·
Rok	83	2.8	82.5	2.1	114	1.7	71	2.2	101.5	2.7	198	2.8	295.5	2.8	143.5	2.7	6	2.7	621	26.2	14.V	17	42	113	32	18	6	24	166	183	117	17	49	71	25

Siemianice $\varphi = 51°11'$ $\lambda = 18°09'$ 1962

Miesiąc	Ciśnienie p: P_m	Max	Min	$P_{o.m}$	Temperatura T: — Max	— Min	Max abs.	Data	Min abs.	Data	Średnia: I	II	III	Dies	Średnia prężność pary e_m: I	II	III	Dies	Średnia wilgotność względna U_m: I	II	III	Dies	Średni niedosyt wilgotności Δ_m: I	II	III	Dies	Średnie zachmurzenie N_m: I	II	III	Dies
I	–	–	–	–	2.3	-2.7	8.4	22	-16.1	31	-0.8	1.0	-0.7	-0.3	–	–	–	–	–	–	–	–	–	–	–	–	70	71	72	71
II	–	–	–	–	1.0	-4.2	6.7	13	-12.1	1-3	-3.2	-0.6	-1.4	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	88	87	71	82
III	–	–	–	–	2.8	-3.3	14.6	31	-7.4	8, 14	-2.5	1.4	-0.5	-0.5	–	–	–	–	–	–	–	–	–	–	–	–	78	75	71	75
IV	–	–	–	–	15.6	5.4	26.8	23	0.4	2	8.0	14.1	9.9	10.5	–	–	–	–	–	–	–	–	–	–	–	–	76	65	61	67
V	–	–	–	–	15.3	6.9	23.2	8	-2.1	1	9.0	13.3	10.3	10.7	–	–	–	–	–	–	–	–	–	–	–	–	80	79	73	77
VI	–	–	–	–	19.9	9.4	30.5	16	3.1	3	12.9	18.1	14.2	14.8	–	–	–	–	–	–	–	–	–	–	–	–	59	64	56	60
VII	–	–	–	–	21.0	10.7	31.5	26	5.9	30	13.9	19.3	14.9	15.8	–	–	–	–	–	–	–	–	–	–	–	–	60	66	63	63
VIII	–	–	–	–	22.8	12.7	31.1	7	8.3	31	14.8	21.1	16.3	17.1	–	–	–	–	–	–	–	–	–	–	–	–	63	67	60	60
IX	–	–	–	–	17.8	7.9	30.0	4	1.7	15	9.7	16.1	11.9	12.4	–	–	–	–	–	–	–	–	–	–	–	–	75	65	39	60
X	–	–	–	–	13.2	4.0	22.6	4	-2.6	16	5.4	12.0	7.3	8.0	–	–	–	–	–	–	–	–	–	–	–	–	66	53	41	53
XI	–	–	–	–	6.1	1.8	12.3	8	-3.5	21	2.8	5.4	3.7	3.9	–	–	–	–	–	–	–	–	–	–	–	–	84	82	77	81
XII	–	–	–	–	-2.0	-6.9	4.9	13	-20.1	22	-5.3	-3.1	-4.7	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	83	80	75	79
Rok	–	–	–	–	11.3	3.5	31.5	26. VII	-20.1	22. XII	5.4	9.8	6.8	7.2	–	–	–	–	–	–	–	–	–	–	–	–	74	71	62	69

Opole Lubelskie $\varphi = 51°09'$ $\lambda = 21°59'$

I	–	–	–	–	1.9	-2.7	6.9	22	-18.4	31	-0.9	1.0	-0.5	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	86	72	68	75
II	–	–	–	–	0.1	-5.3	5.4	13	-12.4	1	-3.5	-0.9	-2.4	-2.3	–	–	–	–	–	–	–	–	–	–	–	–	89	88	88	88
III	–	–	–	–	2.0	-6.0	11.3	5	-17.3	26	-3.4	0.9	-2.1	-1.7	–	–	–	–	–	–	–	–	–	–	–	–	75	71	62	69
IV	–	–	–	–	16.9	5.9	27.4	22	0.0	8	9.7[3]	15.9	10.2	11.5[3]	–	–	–	–	–	–	–	–	–	–	–	–	43	52	36	44
V	–	–	–	–	16.2	7.3	23.2	8	-1.6	1	10.5[3]	14.9	10.8	11.8[3]	–	–	–	–	–	–	–	–	–	–	–	–	74	72	67	71
VI	–	–	–	–	19.3	9.3	29.6	23	2.9	8	13.7[3]	18.2	13.8	14.9[3]	–	–	–	–	–	–	–	–	–	–	–	–	58	64	45	56
VII	–	–	–	–	22.0	11.3	30.2	22	5.7	2	14.9[3]	21.0	15.2	16.6[3]	–	–	–	–	–	–	–	–	–	–	–	–	46	45	48	46
VIII	–	–	–	–	23.3	12.4	31.6	13	7.0	27	16.1[3]	21.8	17.1	18.0[3]	–	–	–	–	–	–	–	–	–	–	–	–	60	52	45	52
IX	–	–	–	–	17.9	8.3	28.2	5	1.9	15	10.7[3]	16.7	12.0	12.8[3]	–	–	–	–	–	–	–	–	–	–	–	–	59	59	37	52
X	–	–	–	–	13.2	2.6	19.7	2	-4.2	16	4.9	12.5	6.1	7.4	–	–	–	–	–	–	–	–	–	–	–	–	66	56	40	54
XI	–	–	–	–	7.0	2.6	17.5	1	-1.1	17, 18	3.8	6.5	4.6	4.9	–	–	–	–	–	–	–	–	–	–	–	–	89	82	81	84
XII	–	–	–	–	-2.0	-7.7	4.2	13	-22.8	22	-5.0	-3.0	-4.9	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	95	76	68	80
Rok	–	–	–	–	11.5	3.2	31.6	13. VIII	-22.8	22. XII	6.0[3]	10.5	6.7	7.5[3]	–	–	–	–	–	–	–	–	–	–	–	–	70	66	57	64

Zgorzelec $\varphi = 51°08'$ $\lambda = 15°02'$

I	990.4	1012.1	965.2	1017.8	2.8	-1.9	8.7	22	-11.9	31	-0.1	1.6	0.3	0.5	5.8	6.1	5.8	5.9	9.2	8.6	8.9	8.9	0.5	1.0	0.7	0.7	7.5	8.2	7.3	7.7
II	991.1	1009.8	960.7	1018.6	2.0	-3.7	8.0	12	-15.6	1	-1.9	0.5	-1.1	-0.9	5.1	5.6	5.2	5.3	9.2	8.6	9.0	8.9	0.4	0.9	0.6	0.6	9.1	8.1	5.6	7.6
III	984.8	1002.4	961.6	1012.0	3.3	-3.5	13.0	3.0	-12.0	7	-2.2	2.1	-0.1	-0.1	4.7	5.5	5.0	5.1	8.7	7.5	8.0	8.1	0.7	1.8	1.2	1.2	7.8	7.6	6.3	7.2
IV	987.9	1000.3	961.5	1014.2	15.0	4.7	27.1	23	-0.7	11	6.4	12.8	9.4	9.5	8.8	10.6	9.8	9.7	8.8	7.0	8.0	7.9	1.2	5.9	2.9	3.3	7.5	7.6	5.8	7.0
V	987.9	993.7	979.6	1014.2	14.9	6.1	22.9	19	-1.4	1	8.4	13.4	9.8	10.4	10.1	10.7	10.7	10.5	9.0	6.9	8.7	8.2	1.2	5.2	1.7	2.7	8.2	8.2	7.2	7.9
VI	994.0	1004.7	985.1	1020.1	20.1	8.7	29.8	15	1.5	6	12.3	18.5	14.0	14.7	13.0	13.8	13.3	13.4	8.7	6.2	8.0	7.6	1.9	9.0	3.4	4.8	5.7	7.1	5.1	6.0
VII	989.8	1000.2	975.2	1015.7	20.3	10.3	31.0	26	5.5	6	13.1	18.7	15.0	15.4	14.3	15.6	15.2	15.0	9.4	7.2	8.8	8.5	1.1	6.8	2.2	3.4	6.7	7.7	6.2	6.9
VIII	990.8	998.8	978.8	1016.7	21.8	11.6	31.0	13	7.2	9, 10	13.9	20.0	15.6	16.3	14.7	16.1	15.6	15.5	9.2	6.9	8.7	8.3	1.4	7.8	2.3	3.8	7.1	8.2	6.2	7.2
IX	990.7	1001.4	974.0	1017.3	18.2	7.5	28.7	4, 12	0.9	15	9.3	16.8	11.4	12.2	10.8	11.5	11.6	11.3	9.1	6.2	8.6	8.0	1.3	8.4	2.3	4.0	6.6	7.0	4.0	5.9
X	996.2	1008.0	982.9	1022.8	13.9	4.5	24.2	2, 3	-1.9	22	6.1	12.9	7.8	8.6	9.1	10.2	9.9	9.7	9.4	6.9	9.1	8.5	0.6	5.5	1.1	2.4	7.1	5.5	4.6	5.7
XI	989.6	1008.4	971.6	1016.6	6.3	1.3	18.5	8	-4.3	25	2.4	5.5	3.5	3.7	6.8	7.5	7.1	7.1	9.2	8.2	8.9	8.8	0.7	2.1	1.0	1.3	8.4	8.2	7.9	8.2
XII	990.0	1017.8	948.3	1017.8	-1.8	-6.8	5.3	12	-19.7	23	-5.2	-3.1	-4.6	-4.4	4.0	4.4	4.2	4.2	8.7	8.4	8.9	8.7	0.5	0.8	0.5	0.6	7.4	7.5	6.7	7.2
Rok	990.3	1017.8	948.3	1017.0	11.4	3.2	31.0	26.VII, 13.VIII	-19.7	23. XII	5.2	10.0	6.8	7.2	8.9	9.8	9.4	9.4	9.0	7.4	8.6	8.3	1.0	4.6	1.7	2.4	7.4	7.6	6.1	7.0

Szymanów $\varphi = 51°08'$ $\lambda = 16°29'$

I	–	–	–	–	3.5°	-1.5	8.2	20	-13.3	31	0.5	2.1	0.8	1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.7	6.9	7.8	7.8
II	–	–	–	–	1.4	-3.0	6.7	20	-10.9	1	-1.1	0.6	-0.7	-0.5	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.7	7.9	8.7
III	–	–	–	–	3.0	-2.3	14.5	30	-8.8	16	-1.1	2.0	-0.2	0.1	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.3	6.7	7.5
IV	–	–	–	–	15.4	5.5	26.9	24	-0.7	11	8.2	13.4	9.2	10.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.6	6.3	7.2
V	–	–	–	–	15.3	6.8	23.0	8	0.5	6	9.9	13.9	10.3	11.1	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.9	8.1	8.1
VI	–	–	–	–	20.2	9.5	29.9	16	1.9	6	13.4	18.7	14.1	15.1	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.2	5.8	5.7
VII	–	–	–	–	21.1	10.2	31.9	26	5.3	9	14.5	19.6	14.7	15.9	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.6	6.5	6.7
VIII	–	–	–	–	23.0	12.1	32.1	13	6.3	10	15.8	21.6	15.9	17.3	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.5	5.3	5.9
IX	–	–	–	–	19.0	2.8	31.5	4	-0.6	15	10.9	17.6	11.6	12.9	–	–	–	–	–	–	–	–	–	–	–	–	9.1	7.7	5.4	7.4
X	–	–	–	–	13.4	4.3	23.7	1	-3.7	22	5.9	12.2	7.4	8.2	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.5	6.9	7.1
XI	–	–	–	–	6.4	2.1	16.2	8	-2.1	17	3.1	6.0	3.8	4.2	–	–	–	–	–	–	–	–	–	–	–	–	9.7	8.5	8.0	8.6
XII	–	–	–	–	-1.2	-6.8	6.5	12	-21.6	22	-4.3	-2.3	-4.4	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.8	7.7	8.5
Rok	–	–	–	–	11.7	3.7	32.1	13. VIII	-21.6	22. XII	6.3	10.4	6.9	7.6	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.3	6.9	7.4

Siemianice $H_s = 182 m$ $h_w = 10 m$ 1962

MIESIĄC	ROZKŁAD WIATRU °D, °mD																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr v		◉	●	Opad R			≡	⊞	R (R)
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15			R ≥ 0.1	R ≥ 1.0	R ≥ 10.0			
I	5	8.7	4	6.5	·	·	1.5	5.0	17.5	4.5	38	5.0	16.5	6.4	6.5	9.8	4	5.6	28	6.4	24	2	7	20	·	7	1	2	12	12	9	·	2	5	·
II	9	7.6	8	5.0	6.5	4.9	0.5	5.0	9	4.8	16.5	6.1	15.5	10.6	13	10.3	6	7.0	30	9.0	12	3	11	24	·	9	5	1	18	13	6	·	4	12	·
III	10.5	8.4	11.5	4.4	5	5.1	11.5	3.9	7	2.4	9	2.4	13.5	6.5	11	6.9	14	4.4	51	14.2	31	·	8	25	·	7	2	3	19	12	8	3	5	11	·
IV	9	6.3	8	5.7	6.5	7.1	4	5.4	9.5	4.2	17.5	3.9	11.5	5.1	12	6.9	12	4.7	41	20.1	26	·	·	·	7	5	3	2	12	10	8	1	2	·	2
V	4	7.0	2	5.0	3.5	4.0	6.5	3.2	7	2.9	21	3.3	24	5.7	17	6.5	8	4.4	110	30.3	14	·	·	2	·	4	2	·	14	21	15	3	1	·	4
VI	11.5	7.6	2.5	3.2	2	2.0	4	3.2	3	3.0	10.5	2.5	26.5	4.8	25	5.4	5	4.5	22	8.1	28	·	·	·	6	6	1	2	8	8	6	·	·	·	3
VII	3	3.8	4	2.6	1	2.0	5	2.4	4	2.0	15.5	3.5	26.5	3.8	17	4.4	17	2.3	82	31.2	15	·	·	·	6	·	·	2	10	13	9	2	·	·	7
VIII	2.5	6.6	3	1.8	2	1.8	5.5	3.5	5.5	1.8	22	4.6	28.5	5.6	14	6.2	10	4.3	45	8.8	24	·	·	·	9	7	2	2	10	14	9	·	2	·	6
IX	2.5	5.4	3	4.3	8	4.8	4.5	3.3	8	1.8	18	3.4	21	5.0	16	6.0	9	4.0	60	24.8	18	·	·	·	4	2	·	3	8	11	6	2	7	·	2
X	1.5	3.7	4	3.5	10	3.4	8.5	3.1	6.5	3.4	9.5	2.3	15	3.7	17	4.5	21	2.8	29	12.4	31	·	·	7	·	1	·	7	9	7	5	1	12	·	·
XI	6.5	2.8	10	7.3	11.5	4.1	18	4.1	4.5	2.3	9.5	3.7	14.5	4.8	6.5	4.5	9	4.0	50	13.7	20	·	1	9	·	2	·	1	19	14	8	2	8	·	·
XII	6	5.6	16.5	4.5	5	6.3	2	5.8	4	6.0	20.5	5.2	16	4.7	8	3.4	15	4.1	21	10.0	15	10	16	28	·	5	·	2	20	12	5	1	6	16	·
Rok	71	6.1	76.5	4.5	61	3.8	71.5	4.0	85.5	3.3	207.5	3.8	229	5.6	163	6.2	130	4.4	569	31.2	15.VII	15	43	115	32	55	16	27	159	147	94	15	49	44	24

Opole Lubelskie $H_s = 149 m$ $h_w = 12,5 m$

I	4	4.8	1	7.0	6	3.0	·	·	16	5.1	22	5.0	20	2.8	24	2.6	·	3.8	28	6.8	25	2	7	22	·	3	·	1	13	15	9	·	·	15	
II	10	3.1	7	2.6	12	2.9	2	1.5	5	2.8	10	6.4	11	4.4	27	7.1	·	4.8	35	9.6	12	4	12	27	·	5	·	1	23	19	8	·	·	27	–
III	9	3.7	15	4.3	7	2.0	14	3.2	14	3.1	10	2.5	3	3.0	21	5.2	·	3.7	45	11.4	16	6	11	27	·	2	·	3	16	15	10	1	1	22	–
IV	3	2.0	5	3.6	12	3.1	11	2.8	13	4.2	23	3.3	4	3.8	19	4.5	·	3.6	33	11.2	27	·	·	·	5	2	·	7	6	11	7	1	·	·	–
V	8	2.9	2	1.5	3	1.0	7	3.4	5	3.2	24	2.8	14	2.6	30	4.0	·	3.1	134	31.0	15	·	·	1	·	2	1	3	13	22	16	3	·	·	–
VI	20	3.2	3	2.0	2	1.5	2	1.0	5	1.0	7	1.7	16	3.5	35	3.0	·	2.8	101	38.0	4	·	·	·	6	·	·	5	8	12	10	3	·	·	–
VII	8	2.2	7	1.6	1	3.0	4	1.2	9	1.7	10	1.9	24	2.0	30	2.2	·	2.0	42	7.8	18	·	·	·	4	·	·	5	5	17	9	·	1	·	–
VIII	1	1.0	7	1.1	3	1.0	5	2.6	4	3.8	10	2.3	24	2.1	39	3.6	·	2.7	39	13.0	5	·	·	·	11	·	·	1	4	11	9	1	1	·	–
IX	3	2.3	9	1.8	7	1.6	6	2.5	6	2.8	9	3.6	19	2.4	31	3.3	·	2.7	66	23.8	18	·	·	·	2	·	·	7	7	14	8	2	5	·	–
X	7	2.3	11	1.4	14	1.5	17	1.5	2	1.0	5	2.2	16	2.2	21	2.1	·	1.8	2	2.2	14	·	·	8	·		·	4	6	1	1	·	14	·	–
XI	19	2.2	5	3.6	7	4.4	32	3.6	7	2.3	2	5.5	7	3.1	11	2.4	·	3.1	48	9.6	15	·	·	5	·	·	·	·	21	22	13	·	5	2	–
XII	11	2.6	15	3.5	8.5	2.5	5.5	1.8	8	4.6	17	3.3	12.5	2.6	15.5	3.1	·	3.1	21	4.0	18	11	16	30	·	1	·	1	17	17	6	·	2	17	–
Rok	103	2.7	87	2.8	82.5	2.3	105.5	2.1	94	3.0	149	3.4	170.5	2.9	303.5	2.8	·	3.1	594	38.0	4.VI	23	46	120	28	15	1	38	139	176	106	11	29	83	–

UWAGA. Obserwator nie notował cisz.

Zgorzelec $H_s = 219 m$ $H_b = 217,9 m$ $h_w = 10,4 m$

I	7	4.6	5	2.4	·	·	·	·	4	5.8	56	5.0	13	3.9	4	3.2	4	4.4	52	11.9	24	2	4	18	·	5	·	·	13	18	10	1	·	5	·
II	4	5.5	13	4.5	7	5.0	·	·	·	·	26.5	4.9	15.5	5.6	12	4.4	6	4.6	43	11.4	12	1	10	24	·	3	1	1	14	20	9	1	·	12	·
III	9	2.8	11.5	2.7	9	2.6	2	1.0	7	2.8	22.5	3.7	10.5	2.1	6.5	2.3	15	2.4	36	10.7	5	1	4	26	·	·	·	1	17	15	8	1	·	9	·
IV	2.5	3.2	9.5	2.8	5.5	3.8	2.5	2.0	17	3.2	21	3.0	9.5	3.7	11.5	2.7	11	2.7	46	17.7	28	·	·	1	4	1	·	3	15	15	8	1	·	·	·
V	6	3.5	5	2.2	1.5	1.7	0.5	1.0	7	2.2	26.5	3.0	27	2.7	10.5	3.3	9	2.5	89	13.6	26	·	·	1	·	·	·	·	18	23	18	3	·	·	2
VI	15.5	3.8	4.5	4.3	2	1.5	1	4.0	8	2.8	15	4.1	21.5	3.3	13.5	4.0	9	3.3	15	5.5	28	·	·	·	8	1	·	2	8	9	4	·	·	·	2
VII	8	2.4	6.5	2.3	3.5	2.0	2	1.5	7	3.4	19.5	3.8	22.5	2.4	12	3.0	12	2.5	59	13.0	16	·	·	·	5	·	·	1	15	18	14	1	·	·	7
VIII	3.5	3.3	3	2.7	1	3.0	1.5	2.3	9.5	3.2	30.5	3.8	22	3.2	11	3.5	11	3.0	66	17.7	5	·	·	·	5	·	·	2	12	15	10	3	·	·	3
IX	1	1.0	3.5	2.3	3.5	3.6	0.5	2.0	10	2.6	26.5	3.6	13.5	2.6	13.5	2.6	18	2.4	50	11.3	18	·	·	·	3	·	·	6	9	15	10	3	1	·	1
X	6	2.2	6	3.3	6.5	2.4	1.5	1.0	10.5	2.4	35	2.8	11	2.5	4.5	2.1	12	2.3	27	16.6	31	·	·	4	·	·	·	7	13	11	3	1	5	·	1
XI	3	2.0	11	4.5	7.5	3.4	2.5	3.8	7	2.5	43	3.0	7	3.0	1	1.0	8	2.9	31	11.4	1	·	1	8	·	·	·	·	18	15	8	1	5	·	·
XII	3.5	1.7	18.5	2.9	10	3.6	·	·	4	4.1	35	4.7	14	3.1	5	2.9	3	3.6	36	9.5	15	10	15	26	·	3	1	2	16	12	8	·	2	15	·
Rok	69	3.0	97	3.1	57	2.7	14	1.6	91	2.9	357	3.8	187	3.2	105	2.9	118	3.0	550	17.7	28.IV, 5.VIII	14	34	108	25	13	2	25	168	186	110	16	13	41	16

Szymanów $H_s = 145 m$ $h_w = 12 m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	28	9.9	24	2	4	17	·	–	–	·	15	15	5	·	1	–	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	25	5.3	12	1	10	18	·	–	–	·	19	17	7	·	1	13	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	45	14.3	31	·	5	23	·	–	–	1	14	11	6	2	1	10	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	23	5.6	13	·	·	1	4	–	–	1	13	13	6	·	·	·	3
V	4	2.9	3.5	2.1	3.5	2.9	6	3.1	8	3.6	9	2.9	37	3.7	15	4.2	7	3.3	76	16.7	14	·	·	·	·	1	·	·	16	22	14	2	·	·	4
VI	9.5	3.7	1.5	1.0	1	2.5	8.5	2.5	6.5	2.2	5	2.5	28.5	4.3	24.5	4.7	5	3.6	25	9.0	16	·	·	·	7	1	1	3	6	7	6	·	·	·	1
VII	4	2.4	4	1.4	4.5	1.8	7	2.5	7	1.8	12	2.9	30.5	3.5	17	3.8	7	2.8	45	14.2	22	·	·	·	7	·	·	·	13	14	9	1	·	·	6
VIII	1.5	2.3	2.5	1.0	1.5	1.3	5	2.2	7.5	2.5	11	3.2	43	4.6	10	3.7	11	3.3	28	5.1	5	·	·	·	9	1	·	3	8	13	7	·	·	·	3
IX	2.5	1.8	1	1.0	8.5	2.4	12.5	3.6	8	3.2	10	3.9	28.5	4.7	10	4.0	9	3.5	39	17.6	18	·	·	1	5	1	·	1	12	14	6	1	5	·	·
X	3.5	3.3	6	2.4	8	3.5	18	2.7	7	2.1	3	1.7	19.5	3.4	13	2.7	15	2.4	45	17.8	31	·	·	7	·	·	·	3	15	9	6	2	8	·	·
XI	4.5	2.1	7.5	3.8	9.5	3.8	21	5.1	6	3.5	7	3.8	21.5	4.0	9	3.1	4	3.8	37	13.5	1	·	·	8	·	1	·	·	22	13	8	1	5	·	·
XII	5.5	3.1	11	3.0	4	2.9	10.5	3.4	6.5	4.8	13.5	4.5	19	4.5	16	3.1	7	3.5	16	5.4	17	9	15	26	·	2	1	·	20	10	4	·	1	15	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	432	17.8	31.X	12	34	101	32	–	–	12	173	158	84	9	22	–	17

Wrocław-Gądów Mały $\varphi = 51°08'$ $\lambda = 16°59'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PREŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	P_{0m}	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1002.0	1024.0	976.7	1017.0	3.5	-2.6	9.7	25	-18.8	31	-0.3	2.5	0.2	0.6	5.4	5.7	5.5	5.5	87	77	86	83	0.9	1.8	0.9	1.2	7.1	7.9	8.1	7.7
II	1002.1	1021.2	971.8	1017.1	2.1	-4.2	8.2	12	-15.7	2	-1.8	0.5	-0.9	-0.8	4.7	5.2	5.1	5.0	87	80	86	84	0.8	1.3	0.8	1.0	8.4	8.8	7.0	8.1
III	996.5	1014.6	974.2	1011.4	3.9	-4.1	15.4	30	-11.1	8	-2.0	2.4	-0.3	0.0	4.9	5.2	5.1	5.1	89	70	82	80	0.6	2.3	1.1	1.3	7.9	8.0	6.7	7.5
IV	999.3	1011.8	972.8	1013.7	16.5	4.8	27.9	25	-0.9	11	8.0	14.6	9.8	10.6	9.3	8.8	9.3	9.1	85	56	76	72	1.9	9.8	3.6	5.1	7.6	7.3	6.3	7.1
V	999.0	1005.2	988.2	1013.4	15.8	6.0	23.1	19	-4.0	1	9.4	13.9	10.2	10.9	10.4	10.7	11.0	10.7	87	67	87	80	1.7	5.8	1.8	3.1	7.7	7.8	7.8	7.8
VI	1004.6	1015.1	994.9	1018.7	21.1	8.8	31.4	16	1.4	3	13.2	18.8	14.7	15.4	12.0	11.1	12.3	11.8	76	50	71	66	3.9	12.0	5.2	7.0	5.6	6.7	5.3	5.9
VII	1000.7	1011.0	986.2	1014.8	21.6	10.0	31.9	26	5.6	11	13.9	20.0	15.2	16.1	13.9	13.4	14.1	13.8	87	58	81	75	2.2	10.8	3.6	5.5	6.0	6.9	6.4	6.4
VIII	1001.8	1009.7	986.9	1015.8	23.2	12.0	32.2	13	6.3	10	15.2	21.5	16.2	17.3	15.0	14.7	15.3	15.0	86	58	83	76	2.5	11.5	3.3	5.8	6.3	7.2	5.4	6.3
IX	1002.3	1013.9	985.6	1016.6	19.1	7.4	31.8	4	1.4	15	10.1	17.2	11.7	12.7	11.4	12.2	11.7	11.8	92	65	86	81	1.3	8.4	2.6	4.1	7.1	6.6	4.4	6.0
X	1007.8	1020.1	994.7	1022.4	13.7	3.5	22.8	1	-6.0	23	5.3	12.1	7.3	8.0	9.2	10.5	9.8	9.8	98	75	93	89	0.2	4.2	0.8	1.7	6.8	5.8	4.8	5.8
XI	1001.7	1019.6	984.9	1016.5	7.0	1.9	17.7	8	-3.3	23	3.6	6.3	3.9	4.4	7.4	7.9	7.5	7.6	92	82	91	88	0.6	2.1	0.9	1.2	8.6	8.2	7.6	8.1
XII	1002.0	1029.4	957.5	1017.2	-0.7	-7.2	6.4	12	-19.7	23	-4.8	-2.0	-4.2	-3.8	4.1	4.5	4.1	4.2	87	81	86	85	0.5	1.1	0.7	0.8	7.5	7.6	7.0	7.4
Rok	1001.6	1029.4	957.5	1016.1	12.2	3.0	32.2	13.VIII	-19.7	23.XII	5.8	10.6	7.0	7.6	9.0	9.2	9.2	9.1	88	68	84	80	1.4	5.9	2.1	3.1	7.2	7.4	6.4	7.0

Czarniecka Góra $\varphi = 51°08'$ $\lambda = 20°31'$

I	–	–	–	–	1.4	-3.7	7.2	22	-21.3	31	-1.6	0.5	-1.2	-0.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	0.0	-6.5	4.5	7, 12	-15.8	1, 3	-4.2	-1.1	-2.5	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	2.3	-7.3	13.7	31	-17.9	19	-5.1	1.0	-1.5	-1.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	16.0	5.5	27.4	24	-0.3	2	7.5	14.5	9.6	10.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	14.8	6.3	22.9	8	-1.6	1	9.1	13.3	9.9	10.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	19.0	7.5	29.9	23	0.1	8	12.3	17.7	13.2	14.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	20.9	9.4	28.9	26	3.7	2	13.5	19.4	14.4	15.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.8	10.7	30.2	13	5.0	30	14.4	20.6	15.4	16.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	17.0	6.5	26.9	4	-0.4	15	9.2	15.9	11.0	11.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	13.4	2.0	21.5	4	-6.1	16	3.9	12.7	5.7	7.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.6	1.9	15.5	8	-3.2	18	3.1	5.6	3.7	4.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-2.4	-8.6	4.0	12	-20.0	22	-5.5	-3.4	-5.8	-5.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	10.9	2.0	30.2	13.VIII	-21.3	31.I	4.7	9.7	6.0	6.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Pszczela Wola $\varphi = 51°07'$ $\lambda = 22°31'$

I	–	–	–	–	1.4	-2.8	6.2	22	-18.7	31	-1.1	0.4	-0.8	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.3	7.5	7.8
II	–	–	–	–	-0.6	-6.7	2.9	13	-13.4	2	-4.3	-1.7	-3.4	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.9	7.9	8.6
III	–	–	–	–	1.4	-7.0	10.9	31	-20.5	26	-4.9	0.5	-2.9	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.5	6.0	7.1
IV	–	–	–	–	16.6	5.0	26.4	22	-0.5	30	8.0	15.7	9.4	10.6	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.6	3.4	5.1
V	–	–	–	–	16.0	6.6	22.3	28	-1.3	1	10.1	14.6	10.0	11.2	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.2	6.1	7.3
VI	–	–	–	–	19.0	8.7	28.2	16	2.7	8	13.1	17.7	12.4	13.9	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.1	6.2	6.6
VII	–	–	–	–	21.5	10.2	28.0	26, 27	6.1	2	14.4	20.2	14.2	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.8	5.4	6.1
VIII	–	–	–	–	22.8	11.2	29.7	13	6.1	27	15.0	21.1	15.6	16.8	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.8	4.9	5.7
IX	–	–	–	–	17.6	7.4	26.8	5	1.8	15	9.6	16.1	11.0	11.9	–	–	–	–	–	–	–	–	–	–	–	–	4.8	7.1	4.4	5.4
X	–	–	–	–	12.9	1.8	19.6	2	-3.7	16	4.0	12.3	5.6	6.9	–	–	–	–	–	–	–	–	–	–	–	–	7.1	5.7	3.9	5.6
XI	–	–	–	–	6.9	1.8	18.6	1	-2.2	18	3.4	6.2	3.8	4.3	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.2	8.2	8.5
XII	–	–	–	–	-2.4	-8.3	3.5	13	-23.3	21	-5.6	-3.5	-5.4	-5.0	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.7	6.5	7.7
Rok	–	–	–	–	11.1	2.3	29.7	13.VIII	-23.3	21.XII	5.1	10.0	5.8	6.7	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.2	5.9	6.8

Chełm Lubelski $\varphi = 51°07'$ $\lambda = 23°30'$

I	990.8	1011.0	971.3	1017.2	1.2	-3.5	6.2	22	-20.0	31	-1.6	-0.1	-1.4	-1.1	5.0	5.2	5.1	5.1	89	83	89	87	0.6	1.1	0.6	0.8	8.1	7.3	7.5	7.6
II	989.1	1006.3	958.8	1015.8	-1.4	-7.0	2.2	13	-15.5	1	-4.8	-2.5	-3.8	-3.7	4.0	4.3	4.3	4.2	90	82	90	87	0.4	0.9	0.5	0.6	8.9	8.5	7.9	8.4
III	985.4	1002.6	965.3	1011.9	0.5	-6.6	10.8	5	-19.5	26	-4.7	-0.7	-3.0	-2.8	4.2	4.7	4.4	4.4	89	79	86	85	0.5	1.3	0.7	0.8	7.5	7.1	6.8	7.1
IV	989.1	1002.9	967.7	1014.5	16.1	5.2	26.4	21	-0.7	8	7.4	14.5	9.9	10.4	8.7	9.0	9.2	9.0	83	57	76	72	2.0	9.0	3.6	4.9	5.9	5.7	4.0	5.2
V	987.6	995.8	970.4	1012.8	16.0	7.1	24.2	28	-0.8	2	9.8	14.3	10.7	11.4	11.0	11.5	11.4	11.3	89	69	86	81	1.4	5.5	1.9	2.9	6.6	8.0	4.7	6.4
VI	991.7	1000.6	982.4	1016.7	19.0	9.6	27.8	23	3.0	6	13.1	17.1	13.3	14.2	12.4	12.2	12.6	12.4	81	63	81	75	3.3	8.4	3.3	5.0	6.0	6.5	5.1	5.9
VII	989.3	999.4	977.5	1014.2	20.7	10.8	28.5	27	6.2	2	14.2	19.0	14.6	15.6	14.2	14.7	14.3	14.4	87	67	85	80	2.2	7.8	2.6	4.2	5.3	6.9	4.8	5.7
VIII	991.1	999.4	982.2	1015.9	22.3	12.1	30.2	13	7.1	27, 31	14.9	20.6	15.9	16.8	15.2	15.1	15.7	15.3	89	62	85	79	1.9	9.7	2.8	4.8	5.5	7.0	3.8	5.4
IX	991.6	1005.7	977.4	1016.8	17.3	8.0	28.2	5	3.0	15	9.8	16.0	11.5	12.2	11.1	12.0	12.2	11.8	91	67	88	82	1.3	6.9	1.8	3.3	4.9	6.6	4.2	5.2
X	997.1	1010.3	983.5	1022.9	12.9	2.6	19.1	1	-3.3	16	3.9	11.6	6.7	7.2	7.9	8.9	9.0	8.9	95	71	89	85	0.4	4.2	1.1	1.9	6.2	6.0	3.4	5.2
XI	993.0	1005.3	979.0	1019.0	7.0	1.9	19.3	1	-3.4	18	3.2	5.7	4.0	4.2	7.4	7.8	7.7	7.6	93	84	91	89	0.5	1.9	0.7	1.0	8.6	8.1	8.1	8.3
XII	990.8	1016.5	952.3	1017.6	-2.6	-7.9	3.0	1	-18.3	21	-5.9	-4.1	-5.4	-5.2	3.7	4.0	3.9	3.9	89	84	88	87	0.4	0.8	0.5	0.6	8.5	7.5	6.8	7.6
Rok	990.6	1016.5	952.3	1016.3	10.8	2.7	30.2	13.VIII	-20.0	31.I	4.9	9.3	6.1	6.6	8.7	9.2	9.2	9.0	89	72	86	82	1.2	4.8	1.7	2.6	6.8	7.1	5.6	6.5

Wrocław-Gądów Mały $H_s = 116\,m$ $H_b = 118{,}6\,m$ $h_w = 20\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU (°D, v=D) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v >10	>15	☁	●	Opad R ≥0.1	≥1.0	≥10.0	≡	⊠	R ro
I	4.5	5.0	2.5	1.8		·	5.5	2.7	26.5	4.4	22.5	5.3	17.5	5.4	9	5.1	5	4.5	33	11.4	24	2	4	20	·	8	·	·	14	14	10	1	2	4	·
II	6	4.8	8.5	2.8	6.5	3.1	4.5	3.2	13	3.3	8	5.7	20	8.0	13.5	6.1	4	5.0	33	7.8	12	2	10	25	·	10	3	·	14	15	8	·	2	14	·
III	12	4.5	12	2.5	6.5	2.2	12.5	4.9	10	4.5	4.5	3.6	9.5	5.8	13	6.0	13	3.8	56	21.9	31	1	4	26	·	5	·	·	17	11	7	3	3	12	·
IV	5	3.0	9.5	2.8	8	3.3	6.5	4.8	15	5.6	12.5	4.5	11.5	4.9	13	3.9	9	3.9	26	5.4	29	·	·	2	8	6	1	3	14	10	8	·	1	·	2
V	8.5	1.5	6.5	1.6	3	3.3	7.5	4.2	8	4.1	13.5	3.3	30.5	4.9	9.5	3.4	6	3.5	75	22.1	14	·	·	2	·	4	·	·	15	20	11	3	2	·	4
VI	8.5	4.4	2	2.0	3	1.5	8	3.2	4	2.6	12	2.8	31.5	4.7	11	3.6	10	3.3	14	5.4	1	·	·	·	9	3	·	2	7	8	4	·	·	·	2
VII	3	1.5	6	1.7	3.5	1.9	5.5	2.5	8	3.2	14.5	2.9	24	4.1	10.5	2.7	18	2.5	77	13.7	26	·	·	·	7	1	·	3	13	15	13	3	2	·	7
VIII	4.5	2.3	1.5	2.3	3	1.3	7	2.1	9	1.8	16	4.6	36	4.3	7	4.4	9	3.3	75	38.7	15	·	·	·	11	4	·	1	8	15	11	1	1	·	5
IX	2	2.5	1.5	3.3	9.5	2.5	10	2.6	10	3.0	12.5	3.9	25	4.0	8.5	3.4	11	3.0	33	13.9	18	·	·	·	4	3	·	3	7	13	7	1	5	·	·
X	3.5	2.7	5.5	2.1	17.5	1.7	14	2.0	8	3.1	2	2.2	17	3.3	10.5	3.2	15	2.1	33	13.4	31	·	·	9	·	·	·	8	12	7	6	1	21	·	·
XI	4	1.4	11	3.1	8.5	3.9	18.5	4.9	3	4.3	10	3.9	17	4.1	7	3.2	11	3.4	51	15.5	1	·	·	8	·	1	·	·	19	14	8	1	6	·	·
XII	4	2.4	12	2.7	9	3.4	7.5	1.9	9	5.3	9	5.0	19	4.0	11.5	2.7	12	3.1	17	5.8	15	11	13	27	·	1	·	2	19	9	3	·	4	15	·
Rok	65.5	3.0	78.5	2.4	78	2.3	107	3.2	123.5	3.8	137	4.0	258.5	4.8	124	4.0	123	3.4	523	38.7	15.VIII	16	31	119	39	46	4	22	159	151	96	14	49	45	20

UWAGA. Kierunki i prędkości wiatru - wg anemometru.

Czarniecka Góra $H_s = 256\,m$ $h_w = 10{,}0\,m$ I–V, $14{,}5\,m$ VI–XII

I	5	4.6	3	5.0	6	3.5	3	2.7	19	3.9	19	3.6	22	4.8	8	3.1	8	4.0	51	8.9	27	5	8	26	·	·	·	–	–	14	14	·	8	–	–
II	9	5.6	2	2.5	9	2.6	8	4.4	8	6.9	13	5.0	17	5.6	12	6.3	6	4.8	60	13.2	12	6	13	28	·	8	2	–	–	15	13	1	5	28	–
III	8	4.6	9	3.4	16	4.1	11	2.8	6	2.7	8	3.5	14	5.0	9	3.0	12	3.3	82	24.2	17	11	10	28	·	3	·	–	–	11	10	3	6	20	–
IV	7	3.0	8	2.8	14	2.9	8	5.4	14	3.8	12	3.2	9	3.4	6	5.5	12	3.1	64	13.0	28	·	·	1	6	3	·	–	–	14	11	1	3	·	–
V	7	2.1	4	1.8	2	3.5	9	3.0	10	4.2	17	3.0	21	4.7	14	3.4	9	3.2	173	27.8	14	·	·	4	·	2	1	–	–	21	21	5	4	·	–
VI	14	5.2	10	4.7	6	1.8	1	5.0	4	2.7	7	3.4	26	4.3	15	3.5	7	3.7	114	44.5	4	·	·	·	6	4	·	–	–	10	10	3	·	·	–
VII	10	2.1	4	2.8	7.5	2.3	2.5	2.0	6	3.0	17.5	3.4	20.5	4.2	14	2.7	11	2.8	121	46.5	22	·	·	·	5	·	·	–	–	15	15	4	1	·	–
VIII	4.5	2.7	·	·	6	1.5	3.5	3.4	10	2.9	15.5	3.5	23.5	4.0	18	3.2	12	2.9	79	16.0	15	·	·	·	7	7	2	–	–	14	13	3	7	·	–
IX	2	2.0	1	3.0	12	2.6	7	3.4	8	2.8	17	3.2	20	3.8	11	3.0	12	2.7	65	20.0	17	·	·	1	1	4	1	–	–	12	7	3	8	·	–
X	1.6	1.9	1.0	2.3	1.6	2.8	7	3.3	8	2.0	10	2.4	13	3.2	5	3.4	8	2.4	5	3.3	28	·	·	10	·	·	·	–	–	4	2	·	1.8	·	–
XI	7	1.7	5	5.6	1.6	2.8	2.3	4.0	5	2.6	1.3	3.2	9	3.3	6	2.0	6	3.1	43	9.0	15	·	1	5	·	1	·	–	–	15	11	·	12^2	4	–
XII	8	2.6	7	4.3	11	3.5	10	4.1	10	3.3	15	4.0	15	2.9	9	2.8	8	3.2	36	8.9	13	13	16	29	·	1	·	–	–	9	9	·	6	19	–
Rok	97.5	3.2	63	3.2	121.5	2.8	93	3.6	108	3.4	164	3.4	210	4.1	127	3.5	111	3.3	893	46.5	22.VII	35	48	132	25	33	6	–	–	154	136	23	78^2	–	–

Pszczela Wola $H_s = 195\,m$ $h_w = 18\,m$

I	·	·	5.5	2.6	0.5	1.0	1.5	1.7	20.5	2.3	30.5	2.1	22.5	2.4	4	2.6	8	2.1	20	7.4	13	2	8	22	·		·	·	15	9	5	·		25	–
II	2.5	2.4	4.5	1.9	1.2	1.6	6	1.9	9	3.7	11	6.0	13.5	2.9	8.5	3.6	17	2.5	26^2	2.7	5	6	14	28	·	2	·	·	21	15	13	·	·	28	–
III	8.5	2.6	4	2.4	7.5	1.1	4.5	2.4	14	1.9	4	1.1	9.5	2.9	9	2.5	3.2	1.4	26	8.0	12	6	14	28	·	·	·	4	17	11	7	·	3	27	–
IV	3.5	2.9	5.5	2.4	11.5	1.7	7.5	1.8	12.5	1.7	10.5	2.2	8.5	1.6	2.5	4.4	2.8	1.4	3.6	10.9	27	·	·	2	5	·	·	6	6	11	8	1	2	1	–
V	1	2.0	2	1.0	·	·	·	·	11	3.3	6.5	1.4	28.5	3.3	3	1.2	4.1	1.6	12.2	34.1	15	·	·	3	·	2	1	1	11	25	15	4	·	·	–
VI	4.5	3.0	6	2.0	·	·	1	2.0	1	1.0	8	1.6	2.5	1.9	7.5	2.9	3.7	1.2	110	40.2	4	·	·	·	7	·	·	2	11	12	11	3	·	·	–
VII	6	1.0	·	·	1	1.0	0.5	2.0	2.5	2.0	1.2	1.6	24.5	1.7	4.5	1.4	4.2	0.9	9.0	26.4	18	·	·	·	4	1	1	4	12	16	11	3	·	·	–
VIII	·	·	2	2.5	·	·	4.5	1.7	3.5	2.4	2.0	1.9	2.7	2.1	2	2.0	3.4	1.3	43	17.0	5		·	·	8	·	·	2	7	11	9	1	4	·	–
IX	·	·	1	2.0	2	2.0	4.5	2.7	15.5	2.4	6	2.4	23.5	2.2	0.5	1.0	3.7	1.4	8.0	33.0	18	·	·	·	2	·	·	4	6	17	11	1	6	·	–
X	1	3.0	3	1.3	5	1.6	3	1.7	1	2.0	8.5	2.5	12.5	1.8	1	2.5	5.8	0.7	3	1.1	19	·	·	11	·	·	·	3	8	3	2	·	14	·	–
XI	3	1.3	1	1.0	1.8	4.0	1.0	2.8	6	1.7	7	1.6	13.5	1.7	7.5	1.5	2.4	1.8	4.2	7.8	15	·	·	7	·	·	·	·	21	14	11	·	6	·	–
XII	3.5	2.0	1.3	2.2	6	1.7	1	1.0	7.5	1.7	1.8	3.4	16.5	1.7	5.5	2.7	2.2	1.7	15	5.2	14	11	17	30			·	·	15	7	4	·	4	17	–
Rok	33.5	1.7	47.5	1.8	63.5	1.3	44	1.8	104	2.2	142	2.3	225	2.2	55.5	2.4	380	1.5	61.3^2	40.2	4.VI	25	53	131	26	5	2	26	150	151	107	13	39	98	–

Chełm Lubelski $H_s = 208\,m$ $H_b = 209{,}6\,m$ $h_w = 12\,m$

I	2.5	5.6	6	4.7	3	3.5	9.5	2.8	23.5	4.1	3.2	5.6	11	6.6	5.5	6.4	·	5.0	24	6.5	25	2	9	25	·	5	·	1	17	17	6	·	1	26	
II	2.5	5.0	9	2.8	16.5	3.8	11.5	2.9	10.5	4.3	13	9.3	11.5	7.6	9.5	7.9	·	5.5	47	16.2	12	6	17	28	·	9	2	·	18	20	13	1	4	28	·
III	7.5	4.9	7	4.4	17	2.4	3.0	3.6	8	3.3	6.5	4.2	5	8.3	7	4.3	5	3.6	41	11.6	16	7	16	27	·	4	·	4	14	14	9	1	3	25	·
IV	3.5	5.6	5.5	3.4	19.5	3.2	2.6	4.1	14.5	3.6	8.5	3.8	2.5	7.0	5	6.2	5	3.8	34	9.3	6	·	·	4	5	2	·	4	4	12	8	·	2	1	·
V	4	3.2	6	2.3	8	2.7	1.6	2.7	21.5	3.0	1.6	5.5	9.5	6.3	6	5.1	6	3.6	10.3	25.8	15	·	·	3	·	3	2	1	10	18	14	5	3	·	5
VI	15.5	3.9	8	3.0	7.5	1.9	1.7	2.1	12	2.0	1.0	3.5	11	5.6	3	4.0	6	3.0	8.5	22.3	1	·	·	·	4	·	·	3	11	12	12	2	·	·	4
VII	5	3.5	6	2.2	9.5	1.3	11.5	2.0	18.5	2.1	18.5	3.4	12	5.3	4	5.1	8	2.7	7.2	12.7	18	·	·	·	4	·	·	6	7	15	12	3	2	·	6
VIII	1	4.0	2	3.5	2	3.0	21.5	2.4	2.0	2.7	1.6	4.1	11	5.8	2.5	3.4	1.7	2.8	3.8	12.7	5	·	·	·	5	1	·	3	4	10	8	1	4	·	4
IX	·	·	·		5	1.8	5	2.4	16.5	2.7	3.1	3.9	7.5	4.9	2	5.0	2.3	2.6	4.0	8.0	5	·	·	·	2	2	·	3	6	16	10	·	4	·	3
X	2	4.5	3.5	2.1	12.5	1.9	2.5	1.9	10.5	1.9	13.5	3.1	7	5.6	5	4.3	1.4	2.3	3	1.5	19	·	·	8	·	·	·	4	6	4	2	·	16		
XI	2	1.5	6	2.5	15.5	3.6	3.8	4.7	4	3.1	9	4.6	6	5.4	3.5	4.1	6	3.9	5.7	11.0	16	·	·	5	·	2	·	3	23	18	13	1	7	1	·
XII	0.5	3.0	17.5	3.3	6.5	2.7	16	3.0	1.4	4.2	1.7	4.8	7.5	4.5	8	3.6	6	3.5	14	3.4	15	11	17	30	·	3	·	·	17	14	4		4	22	·
Rok	4.6	3.7	76.5	2.8	122.5	2.6	227	2.9	173.5	3.1	191	4.6	101.5	6.1	61	5.0	9.6	3.5	55.8	25.8	15.V	26	59	130	20	31	4	32	137	170	111	14	50	103	22

UWAGA. Kierunki wiatru - wg wiatromierza Wilda, prędkości - wg anemometru.

Grabowiec $\varphi = 51°06'$ $\lambda = 21°23'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	–	-3.2	–	–	-19.8	31	-1.4	0.5	-0.9	-0.7	–	–	–	–	–	–	–	–	–	–	–	–	82	66	65	71
II	–	–	–	–	–	-5.7	–	–	-18.7	1	-3.8	-1.1	-2.3	-2.4	–	–	–	–	–	–	–	–	–	–	–	–	92	89	90	90
III	–	–	–	–	1.1	-6.0	12.8	31	-15.8	19	-4.5	0.2	-2.4	-2.3	–	–	–	–	–	–	–	–	–	–	–	–	80	72	74	75
IV	–	–	–	–	15.5	5.8	25.9	22, 23	0.6	8	8.2	14.1	9.7	10.4	–	–	–	–	–	–	–	–	–	–	–	–	72	66	59	66
V	–	–	–	–	14.7	6.5	22.4	8	-1.4	1	9.5	13.5	10.0	10.8	–	–	–	–	–	–	–	–	–	–	–	–	85	83	75	81
VI	–	–	–	–	18.4	8.6	28.5	23	3.1	3	13.2	17.1	12.9	14.0	–	–	–	–	–	–	–	–	–	–	–	–	64	72	65	67
VII	–	–	–	–	21.0	10.0	28.8	22	5.2	5	14.4	19.6	13.9	15.4	–	–	–	–	–	–	–	–	–	–	–	–	61	72	65	66
VIII	–	–	–	–	22.2	11.5	30.6	13	6.7	10	15.0	20.8	15.8	16.8	–	–	–	–	–	–	–	–	–	–	–	–	66	71	69	69
IX	–	–	–	–	17.3	7.2	26.6	4	1.6	15	9.7	15.9	11.5	12.2	–	–	–	–	–	–	–	–	–	–	–	–	66	70	55	64
X	–	–	–	–	12.8	2.6	19.3	4	-3.6	16	4.3	12.1	6.0	7.1	–	–	–	–	–	–	–	–	–	–	–	–	70	58	49	59
XI	–	–	–	–	6.2	2.0	14.6	1, 8	-1.6	17	2.9	5.3	4.0	4.0	–	–	–	–	–	–	–	–	–	–	–	–	93	88	81	87
XII	–	–	–	–	-2.4	-7.9	3.5	7	-17.0	26, 31	-5.6	-3.7	-5.2	-4.9	–	–	–	–	–	–	–	–	–	–	–	–	95	75	71	80
Rok	–	–	–	–	–	2.6	30.6	13.VIII	-19.8	31.I	5.2	9.5	6.1	6.7	–	–	–	–	–	–	–	–	–	–	–	–	77	74	68	73

Namysłów $\varphi = 51°05'$ $\lambda = 17°43'$

I	–	–	–	–	3.7	-2.3	10.0	22	-14.5	31	-0.8	2.9	-0.1	0.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	1.9	-4.1	7.4	10	-14.1	1	-3.3	1.3	-1.4	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	4.0	-3.4	15.4	31	-8.9	8	-2.4	3.3	-0.7	-0.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	16.3	6.3	27.6	26	0.5	2	8.8	15.0	10.1	11.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15.6	6.5	23.0	19	-0.9	1	9.5	14.5	10.3	11.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	21.1	9.2	31.6	16	1.9	3	13.6	19.4	14.1	15.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	22.0	10.5	32.2	26	5.2	11	14.6	20.5	14.9	16.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	23.6	12.1	32.3	13	7.6	31	15.4	22.3	15.6	17.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	19.1	7.1	31.0	4	0.2	15	10.4	17.3	11.9	12.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	14.5	3.4	24.0	3	-3.6	23	5.0	13.6	6.6	8.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	7.0	2.4	18.8	8	-3.3	26	3.4	6.3	4.0	4.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-1.5	-7.5	6.3	13	-21.2	22	-6.2	-2.4	-5.1	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	12.3	3.4	32.3	13.VIII	-21.2	22.XII	5.7	11.2	6.7	7.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Przedbórz $\varphi = 51°05'$ $\lambda = 19°53'$

I	–	–	–	–	1.9	-3.6	8.2	22	-18.3	31	-1.4	0.8	-1.4	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	89	66	71	75
II	–	–	–	–	0.4	-5.6	5.4	13	-16.4	1	-3.9	-1.2	-2.3	-2.4	–	–	–	–	–	–	–	–	–	–	–	–	93	84	75	84
III	–	–	–	–	2.1	-5.9	14.2	31	-15.2	26	-4.4	0.7	-2.0	-1.9	–	–	–	–	–	–	–	–	–	–	–	–	71	70	68	70
IV	–	–	–	–	15.7	5.1	27.0	22	-0.9	8	7.4	14.0	9.4	10.0	–	–	–	–	–	–	–	–	–	–	–	–	61	63	50	58
V	–	–	–	–	15.1	6.6	22.8	8	-1.3	1	8.9	13.0	9.9	10.4	–	–	–	–	–	–	–	–	–	–	–	–	68	83	76	76
VI	–	–	–	–	18.6	9.2	29.4	23	3.4	2	12.8	17.1	13.4	14.2	–	–	–	–	–	–	–	–	–	–	–	–	55	59	50	55
VII	–	–	–	–	20.8	10.4	30.0	26	5.9	30	14.1	18.9	14.5	15.5	–	–	–	–	–	–	–	–	–	–	–	–	55	65	55	58
VIII	–	–	–	–	22.1	11.9	30.1	13	6.8	31	14.7	20.5	16.0	16.8	–	–	–	–	–	–	–	–	–	–	–	–	70	63	49	61
IX	–	–	–	–	17.3	7.5	27.6	4	2.0	15	9.6	15.7	11.4	12.0	–	–	–	–	–	–	–	–	–	–	–	–	67	68	49	61
X	–	–	–	–	13.1	3.0	20.6	3	-3.9	16	4.7	12.0	6.4	7.4	–	–	–	–	–	–	–	–	–	–	–	–	71	42	36	50
XI	–	–	–	–	6.5	2.1	15.1	8	-1.7	18	3.1	5.6	3.7	4.0	–	–	–	–	–	–	–	–	–	–	–	–	89	81	85	85
XII	–	–	–	–	-2.2	-7.9	5.9	12	-21.5	22	-5.7	-3.5	-5.5	-5.0	–	–	–	–	–	–	–	–	–	–	–	–	95	81	72	83
Rok	–	–	–	–	11.0	2.7	30.1	13.VIII	-21.5	22.XII	5.0	9.5	6.1	6.7	–	–	–	–	–	–	–	–	–	–	–	–	74	69	61	68

Laskowice Oławskie $\varphi = 51°03'$ $\lambda = 17°21'$

I	–	–	–	–	3.1	-1.9	9.8	22	-14.9	31	0.0	2.2	0.3	0.7	5.5	5.6	5.5	5.5	86	77	85	83	0.9	1.8	1.0	1.2	69	63	73	68
II	–	–	–	–	1.5	-3.6	8.0	12	-14.2	1	-2.0	0.2	-0.8	-0.8	4.5	5.1	5.1	4.9	83	80	85	83	0.9	1.3	0.8	1.0	85	89	70	81
III	–	–	–	–	3.6	-2.8	15.1	31	-7.0	15	-1.9	2.6	0.2	0.3	4.8	5.0	4.9	4.9	87	64	79	77	0.7	2.6	1.3	1.5	80	78	73	77
IV	–	–	–	–	16.0	5.4	27.6	23	0.2	2	8.2	14.5	10.2	10.8	9.1	8.3	9.2	8.9	82	54	73	70	2.1	10.3	3.9	5.4	69	70	59	66
V	–	–	–	–	15.7	6.9	23.0	19	-1.1	1	9.7	14.2	10.4	11.2	10.4	10.4	11.0	10.6	85	65	86	79	1.9	6.4	1.9	3.4	78	79	69	75
VI	–	–	–	–	20.4	9.3	30.8	16	3.0	3	13.5	19.3	14.4	15.4	12.2	11.6	12.5	12.1	76	51	74	67	3.9	12.3	4.7	7.0	63	66	55	61
VII	–	–	–	–	21.6	10.5	32.6	26	4.5	11, 30	14.2	20.4	15.4	16.4	13.9	13.0	14.2	13.7	85	55	80	73	2.6	11.7	3.6	6.0	59	63	62	61
VIII	–	–	–	–	23.2	12.8	31.9	13	7.7	10	15.6	21.7	16.5	17.6	14.7	14.3	15.2	14.7	82	55	80	72	3.2	12.3	3.8	6.4	66	75	5.0	6.4
IX	–	–	–	–	18.6	7.5	31.0	4	0.8	15	10.1	17.0	11.7	12.6	11.1	11.5	11.4	11.3	88	62	83	78	1.7	8.8	2.8	4.4	72	65	51	63
X	–	–	–	–	13.4	3.7	22.8	3	-3.4	23	5.4	12.1	7.1	7.9	9.1	10.2	9.6	9.6	97	72	92	87	0.3	4.5	0.8	1.9	81	54	59	65
XI	–	–	–	–	6.7	2.4	17.1	8	-3.7	26	3.6	6.2	4.0	4.4	7.4	7.9	7.5	7.6	91	82	91	88	0.7	2.0	0.9	1.2	89	85	73	82
XII	–	–	–	–	-1.2	-6.6	5.4	13	-19.3	22	-4.9	-2.1	-4.0	-3.8	4.0	4.4	4.1	4.2	85	80	84	83	0.7	1.2	0.8	0.9	82	79	68	76
Rok	–	–	–	–	11.9	3.6	32.6	26.VII	-19.3	22.XII	6.0	10.7	7.1	7.7	8.9	8.9	9.2	9.0	86	66	83	78	1.6	6.3	2.2	3.4	74	72	64	70

Grabowiec — $H_s = 210 m$ — $h_w = 15 m$ — 1962

MIESIĄC	ROZKŁAD WIATRU °D, °mD: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n): Temperatura T: Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v: v > 10	v > 15	◉	●	Opad R: R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	[illegible]
I	7.5	4.3	1.5	3.3	·	·	2.5	4.0	29.5	4.2	21	4.8	20	5.2	6	6.6	5	4.5	24	5.1	12	2	—	21	·	3	1	·	13	12	7	·	·	—	·
II	6.5	3.7	0.5	1.0	11.5	2.4	3.5	2.4	11	4.1	13.5	6.9	14.5	7.1	17	7.4	6	5.1	31	8.0	12	4	—	26	·	9	1	·	20	14	8	·	·	—	·
III	9	5.6	6.5	3.8	6	1.8	5.5	3.5	17.5	3.5	2.5	3.8	9.5	6.2	16.5	4.2	20	3.3	25	8.4	12	5	15	26	·	2	·	2	19	11	7	·	2	—	·
IV	8	2.8	7.5	4.3	6	3.2	7	3.5	18.5	3.8	10	3.1	6.5	3.0	11.5	5.5	15	3.1	65	17.2	11	·	·	·	4	1	1	2	11	11	8	3	1	—	3
V	8	2.2	0.5	3.0	2	1.8	5	1.9	10	3.0	11.5	4.9	25	4.0	11	2.8	20	2.7	130	18.6	14	·	·	1	·	3	·	·	17	20	18	5	4	·	4
VI	12	6.2	1	2.5	·	·	2	1.5	7.5	2.1	8.5	3.5	20	4.9	23	3.6	16	3.4	111	40.1	4	·	·	·	4	3	·	1	10	10	6	4	·	·	1
VII	7.5	2.9	0.5	3.0	1	1.0	2.5	2.2	8	2.8	10.5	3.1	23	3.5	18	3.0	22	2.4	48	15.2	22	·	·	·	4	1	·	·	12	11	10	1	1	·	5
VIII	0.5	4.0	·	·	2	1.5	7	2.1	11.5	2.7	12.5	3.2	29	4.0	11.5	5.0	19	2.8	50	9.2	3	·	·	·	7	2	·	2	10	12	10	·	2	·	3
IX	2	2.2	2.5	2.0	7	1.6	2.5	2.8	13.5	3.1	18	3.3	26.5	3.5	5	4.1	13	2.7	55	24.1	18	·	·	·	2	1	·	3	11	12	8	2	6	·	1
X	2.5	2.8	3	3.3	4	1.4	8.5	1.8	11.5	1.8	4	3.5	20	2.9	11.5	2.7	28	1.7	3	1.7	14	·	·	9	·	·	·	3	9	3	1	·	18	·	·
XI	5	2.1	7	3.8	7	3.3	23.5	4.3	8.5	2.6	10.5	3.2	9	2.8	10.5	3.3	9	3.1	35	4.8	14	·	1	6	·	·	·	1	20	18	13	·	10	—	·
XII	14.5	3.4	6.5	3.8	3.5	3.1	4.5	3.8	18	4.2	8.5	4.0	18.5	2.9	9	3.8	10	3.2	15	4.4	18	11	16	29	·	·	·	·	17	12	5	·	5	—	·
Rok	83	3.5	37	2.8	50	1.8	74	2.8	165	3.2	131	3.9	221.5	4.2	150.5	4.3	183	3.2	592	40.1	4. VI	22	—	118	21	25	3	14	169	146	101	15	49	—	17

Namysłów — $H_s = 151 m$ — $h_w = 12,6 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◉	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	[illegible]
I	1	2.0	7.5	3.3	1.5	2.7	9.5	1.8	9	2.0	33	2.7	22	2.5	6.5	3.9	3	2.5	24	7.3	24	1	3	19	·	2	·	—	—	13	7	·	4	14	·
II	2.5	5.0	18.5	3.1	4	1.9	1.5	2.3	2	1.5	15.5	4.0	25.5	5.6	11.5	7.1	3	3.9	42	12.6	17	4	8	25	·	5	4	—	—	16	8	1	·	19	1
III	2.5	3.6	18.5	4.0	17.5	2.1	11	2.4	6.5	1.2	14.5	1.6	7.5	1.9	10	6.2	5	2.7	56	15.3	12	·	6	25	·	2	1	—	—	12	8	3	1	9	·
IV	2.5	2.6	1.5	1.0	3.5	1.3	15	1.4	14	1.6	19.5	2.2	15.5	1.7	17.5	2.5	1	1.9	57	18.2	26	·	·	·	8	1	1	—	—	10	8	2	·	·	2
V	4	2.1	2.5	1.8	2	1.2	11	2.4	6.5	2.5	18	2.7	13	3.5	17	3.5	19	2.3	101	26.6	14	·	·	1	·	1	·	—	—	21	13	2	3	·	2
VI	12	2.2	9.5	2.6	6	1.2	5.5	1.3	10.5	1.1	6	1.4	21.5	1.5	12	2.1	7	1.6	13	4.3	28	·	·	·	10		·	—	—	7	4	·	·	·	1
VII	5.5	1.3	4	1.1	3.5	1.0	3.5	1.1	14	1.5	16	1.7	25.5	1.6	6	1.7	15	1.3	88	48.1	22	·	·	·	7	·	·	—	—	15	11	2	2	·	6
VIII	·	·	·	·	·	·	3	2.0	7.5	2.3	27.5	2.2	31	2.5	7	2.7	17	1.9	64	13.7	14	·	·	·	12	·	·	—	—	15	10	1	2	·	4
IX	2	6.8	·	·	9	1.4	8.5	1.9	7	1.6	19	2.1	18.5	1.6	20	2.4	6	1.9	69	24.0	18	·	·	·	3	1	1	—	—	9	8	2	3	·	
X	0.5	1.0	1.5	1.3	15	1.3	19.5	1.3	6.5	1.2	4	1.5	16.5	1.7	6.5	1.3	23	1.0	32	14.8	31	·	·	7	·	·	·	—	—	6	6	1	19	·	·
XI	1.5	1.7	8.5	1.8	18	1.9	13	2.0	5.5	1.4	13	1.3	11	1.6	8.5	2.1	11	1.5	62	15.3	1	·	·	8	·	·		—	—	13	11	3	6	3	·
XII	·	·	3	1.3	19	1.3	12	1.6	10	2.1	15	1.9	13.5	1.3	6.5	1.3	14	1.3	31	11.3	15	10	16	26	·		·	—	—	12	8	1	8	16	·
Rok	34	2.4	75	1.8	99	1.4	113	1.8	99	1.7	201	2.1	221	2.2	129	3.1	124	2.0	639	48.1	22 VII	15	33	111	40	12	7	—	—	149	102	18	48	61	16

Przedbórz — $H_s = 235 m$ — $h_w = 13 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◉	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	[illegible]
I	3	10.0	5	6.2	1	5.0	10	3.3	37	3.8	20.5	4.3	14.5	5.2	1	9.0	1	4.4	25	5.9	25	2	8	24	·	1	·	1	14	14	8	·	1	15	—
II	5	4.0	9	3.8	7	4.1	6	3.2	11	4.8	9	7.3	24	5.9	4	7.5	9	4.7	42	11.5	16	4	12	26	·	4	·	·	16	16	9	1	1	23?	—
III	8	4.6	13	3.6	12	4.0	12	4.1	1	3.0	4	4.5	15	5.1	8	9.4	20	3.8	48	13.4	5	6	11	25	·	4	·	4	17	12	9	2	3	22	—
IV	8	3.8	9.5	4.7	4.5	5.2	11.5	3.8	20	4.3	4.5	3.1	10.5	5.5	8.5	4.9	13	3.8	51	15.1	26	·	·	2	4	4	·	4	9	11	9	1	1	·	—
V	·	·	8	2.4	3	4.7	7	2.9	14.5	3.1	10.5	3.3	26	4.9	8	3.2	16	3.1	121	16.7	14	·	·	2	·	2	·		14	23	18	5	·	·	—
VI	6.5	4.7	4	4.2	2	2.0	3	3.0	9.5	2.5	8	4.4	23.5	4.4	16.5	4.4	17	3.3	73	27.8	4	·	·	·	6	1	·	5	8	9	8	2	·	·	—
VII	5	4.2	5	3.8	·	·	6	2.8	17	2.6	10	3.4	15	3.8	13	3.3	22	2.5	107	46.8	22	·	·	·	5	·		5	6	12	11	3	·		—
VIII	·	·	3	2.3	3	2.7	9.5	2.8	14.5	2.7	24	3.4	16	4.6	4	3.2	19	2.7	75	18.2	15	·	·	·	7	·		2	9	17	11	3	1	·	—
IX	1	3.0	5	2.2	4.5	2.9	7.5	2.3	15.5	2.4	16.5	3.0	16	4.9	7	3.6	17	2.6	58	25.2	17	·	·	·	2	1	·	5	12	11	6	2	4	·	—
X	5.5	3.2	7.5	3.0	3	3.0	15	2.8	15	2.1	12	3.7	8	3.9	4	4.2	23	2.3	10	5.8	28	·	·	9	·	·	·	7	9	4	4	·	14	·	—
XI	6	3.3	12	5.3	12	4.5	22	4.3	5.5	2.2	11.5	3.3	6	3.3	7	3.1	8	3.6	39	9.8	15	·	·	9	·	·	·	1	21	12	9	·	1	3	—
XII	1	3.0	17	3.9	9	3.0	5	5.8	22	3.3	9	4.9	15	2.9	2	3.0	13	3.1	26	6.6	13	11	14	30		·	·		19	9	6	·	2	18	—
Rok	49	3.6	98	3.8	61	3.4	114.5	3.4	182.5	3.1	139.5	4.0	189.5	4.5	83	4.9	178	3.3	675	46.8	22. VII	23	45	127	24	17	·	34	154	150	108	19	28	81?	—

Laskowice Oławskie — $H_s = 135 m$ — $h_w = 13,5 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◉	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	[illegible]
I	6.5	5.8	3	5.2	·	·	3	3.0	24.5	4.6	29.5	4.8	14.5	5.1	11	5.7	1	4.9	31	10.0	24	2	4	16	·	4	·	2	13	12	8	1	5	8	·
II	5.5	6.6	4.5	4.9	11	4.0	4	3.8	10.5	4.2	10	4.6	19	8.2	17.5	7.9	2	6.0	27	7.2	12	2	10	20	·	10	3	·	14	15	7	·	2	14	2
III	10	7.0	10.5	2.9	7	3.7	15.5	3.6	12.5	3.5	4.5	3.1	8.5	7.1	14.5	5.2	10	4.0	54	16.5	31	·	6	25	·	6	1	1	19	12	7	3	5	9	·
IV	6.5	3.5	11.5	3.9	4	5.1	10	6.4	14.5	4.4	11	4.2	9.5	4.5	11	4.1	12	3.9	54	16.7	26	·	·	·	7	6	1	2	13	11	9	2	·	·	3
V	3.5	3.6	4.5	2.6	2.5	3.0	11	3.2	15	2.6	15.5	3.3	22	4.1	12	3.5	7	3.1	96	26.7	14	·	·	1	·	2	·	·	11	23	14	3	·	·	2
VI	9	4.2	3	2.7	2	2.5	7	2.4	9	3.1	9.5	2.8	28.5	3.7	18	3.7	4	3.3	17	4.9	16	·	·	·	8	4	·	1	10	10	4	·	·	·	3
VII	8.5	2.3	3	1.8	5.5	1.7	5	3.0	13.5	3.1	16	2.9	21	2.9	11.5	2.4	9	2.4	38	7.6	13	·	·	·	7	3	·	3	9	15	11	·	·	·	4
VIII	4.5	2.0	1.5	1.3	5.5	3.1	7	2.8	14.5	3.3	20.5	3.4	28.5	3.7	7	2.9	4	3.1	54	12.8	14	·	·	·	8	1	·	2	9	14	9	2	·	·	3
IX	3	2.3	2	3.2	12.5	2.8	10.5	2.5	11.5	3.5	17	3.5	23.5	3.4	7	3.1	3	3.1	54	18.4	17	·	·	·	4	1	·	3	10	13	7	2	5	·	·
X	3	2.0	5.5	1.9	14.5	2.3	15.5	2.5	9	2.2	5.5	2.4	13.5	3.3	12.5	3.3	14	2.2	25	14.2	31	·	·	7	·	·	·	4	12	11	5	1	18	·	·
XI	4.5	1.4	8	5.1	13.5	3.7	20.5	5.1	10.5	3.1	9	2.9	10.5	3.2	8.5	3.0	5	3.5	54	12.0	1	·	·	7	·	1	·	·	18	15	9	1	6	·	·
XII	8	2.6	10	4.4	10.5	3.2	11	2.5	13.5	3.7	9	3.2	14.5	3.4	9.5	3.1	7	3.0	21	7.9	15	10	14	26	·	·	·	1	16	13	5	·	5	16	·
Rok	72.5	3.6	67	3.3	88.5	2.9	120	3.4	158.5	3.4	157	3.4	213.5	4.4	140	4.0	78	3.5	525	26.7	14.V	14	34	102	34	38	5	19	154	164	95	15	46	47	17

Suchedniów I — φ = 51°03′ — λ = 20°50′ — 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	P_{0m}	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.7	-3.8	6.8	20	-25.8	31	-1.8	0.5	-1.4	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	83	67	56	69
II	–	–	–	–	-0.2	-6.5	4.6	13	-23.3	1	-4.6	-1.2	-3.4	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	90	89	79	86
III	–	–	–	–	2.0	-7.6	14.1	31	-20.8	19	-5.5	0.7	-3.0	-2.7	–	–	–	–	–	–	–	–	–	–	–	–	77	70	66	72
IV	–	–	–	–	15.9	4.3	27.1	23	-0.5	8	7.3	14.4	8.6	9.7	–	–	–	–	–	–	–	–	–	–	–	–	65	69	46	60
V	–	–	–	–	15.0	5.8	23.6	8	-2.6	1	9.1	13.7	9.2	10.3	–	–	–	–	–	–	–	–	–	–	–	–	72	85	53	70
VI	–	–	–	–	19.1	7.5	30.3	23	1.3	8	12.8	17.4	12.6	13.8	–	–	–	–	–	–	–	–	–	–	–	–	57	66	47	57
VII	–	–	–	–	21.3	9.6	29.6	22	4.2	2	14.1	19.8	13.8	15.4	–	–	–	–	–	–	–	–	–	–	–	–	56	64	58	59
VIII	–	–	–	–	22.3	10.6	30.8	13	3.6	27	14.5	21.0	14.8	16.3	–	–	–	–	–	–	–	–	–	–	–	–	55	62	40	52
IX	–	–	–	–	17.5	6.5	27.0	4	0.9	27	9.5	16.2	10.3	11.6	–	–	–	–	–	–	–	–	–	–	–	–	60	62	38	53
X	–	–	–	–	13.5	1.3	19.7	1	-6.3	16	3.4	12.7	4.3	6.2	–	–	–	–	–	–	–	–	–	–	–	–	55	41	40	45
XI	–	–	–	–	6.3	1.8	14.4	5, 8	-3.3	18	2.8	5.5	3.5	3.8	–	–	–	–	–	–	–	–	–	–	–	–	89	80	81	83
XII	–	–	–	–	-2.1	-8.2	4.3	13	-20.0	29	-5.5	-3.1	-5.9	-5.1	–	–	–	–	–	–	–	–	–	–	–	–	86	75	64	75
Rok	–	–	–	–	11.0	1.8	30.8	13.VIII	-25.8	31.I	4.7	9.8	5.3	6.3	–	–	–	–	–	–	–	–	–	–	–	–	70	69	56	65

Suchedniów II — φ = 51°02′ — λ = 20°50′

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	17.0	6.5	26.7	4	0.4	15	9.4	15.5	10.6	11.5	–	–	–	–	–	–	–	–	–	–	–	–	61	58	49	56
X	–	–	–	–	13.1	1.2	19.7	1	(-6.0)	16	3.6	12.2	4.5	6.2	–	–	–	–	–	–	–	–	–	–	–	–	59	51	46	52
XI	–	–	–	–	6.2	1.3	15.1	5	-3.5	18	2.5	5.3	3.2	3.6	–	–	–	–	–	–	–	–	–	–	–	–	90	84	87	87
XII	–	–	–	–	-2.4	-8.1	4.2	13	-20.0	24	-5.6	-3.7	-5.8	-5.2	–	–	–	–	–	–	–	–	–	–	–	–	90	78	23	80
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Krasnystaw — φ = 50°59′ — λ = 23°10′

I	–	–	–	–	1.8	-3.1	7.4	22	-19.1	31	-1.4	0.3	-1.2	-0.9	–	–	–	–	–	–	–	–	–	–	–	–	82	67	74	74
II	–	–	–	–	-0.4	-6.6	2.8	13, 16	-13.5	1	-4.4	-1.9	-3.6	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	89	89	81	86
III	–	–	–	–	1.3	-6.4	11.8	5	-19.0	26	-4.5	-0.2	-2.8	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	80	70	64	71
IV	–	–	–	–	16.3	5.3	26.1	22	-0.4	2, 30	7.5	14.8	9.9	10.5	–	–	–	–	–	–	–	–	–	–	–	–	60	56	43	53
V	–	–	–	–	16.2	7.0	23.5	28	-0.6	1	10.0	14.7	10.7	11.5	–	–	–	–	–	–	–	–	–	–	–	–	71	80	55	69
VI	–	–	–	–	19.8	9.3	28.8	16	3.5	6, 7	13.1	17.9	13.3	14.4	–	–	–	–	–	–	–	–	–	–	–	–	65	71	56	64
VII	–	–	–	–	21.2	10.8	27.9	26	6.3	2, 3	14.9	19.5	15.1	16.2	–	–	–	–	–	–	–	–	–	–	–	–	63	67	52	61
VIII	–	–	–	–	22.8	12.0	30.3	13	6.4	27	15.1	21.1	16.5	17.3	–	–	–	–	–	–	–	–	–	–	–	–	55	60	37	51
IX	–	–	–	–	18.1	7.6	28.0	5	2.2	15	9.9	16.3	11.6	12.4	–	–	–	–	–	–	–	–	–	–	–	–	61	70	40	57
X	–	–	–	–	13.4	2.1	19.5	4	-4.4	17	4.2	12.6	6.3	7.4	–	–	–	–	–	–	–	–	–	–	–	–	76	58	42	59
XI	–	–	–	–	7.3	2.4	19.5	1	-2.1	18	3.7	6.3	4.4	4.7	–	–	–	–	–	–	–	–	–	–	–	–	90	81	76	82
XII	–	–	–	–	-2.4	-7.8	3.9	13	-21.8	22	-5.6	-3.7	-5.4	-5.0	–	–	–	–	–	–	–	–	–	–	–	–	81	77	73	77
Rok	–	–	–	–	11.3	2.7	30.3	13.VIII	-21.8	22.XII	5.2	9.8	6.2	6.8	–	–	–	–	–	–	–	–	–	–	–	–	73	70	58	67

Wojcieszów Górny — φ = 50°57′ — λ = 15°55′

I	–	–	–	–	3.2	-3.0	11.1	22	-18.8	31	-0.7	1.4	-0.3	0.0	4.8	5.0	4.9	4.9	8.0	7.2	7.8	7.7	1.3	2.1	1.5	1.6	6.3	6.2	5.8	6.1
II	–	–	–	–	1.1	-5.2	6.7	12, 13	-19.7	1	-2.8	-0.4	-1.6	-1.6	4.2	4.6	4.5	4.4	8.3	7.5	8.0	7.9	0.9	1.5	1.2	1.2	8.8	8.1	7.1	8.0
III	–	–	–	–	2.6	-4.6	12.4	30	-11.7	15	-2.7	1.5	-1.5	-1.0	4.3	4.3	4.3	4.3	8.1	5.9	7.5	7.2	1.0	2.8	1.4	1.7	7.3	7.0	6.1	6.8
IV	–	–	–	–	14.5	4.0	26.4	23, 25	-2.3	11	6.2	12.8	7.8	8.6	7.8	8.1	8.1	8.0	8.1	5.6	7.6	7.1	2.3	8.6	3.0	4.6	5.0	6.2	4.9	5.4
V	–	–	–	–	14.5	5.2	22.8	8	-3.4	1	8.0	13.0	9.2	9.8	9.1	9.5	9.8	9.5	8.3	6.4	8.3	7.7	1.9	6.1	2.1	3.4	7.3	7.2	6.7	7.1
VI	–	–	–	–	19.1	8.0	29.1	16	0.4	8	11.0	17.5	12.8	13.5	11.0	11.0	11.5	11.2	8.0	5.3	7.5	6.9	2.7	10.4	3.9	5.7	4.3	5.9	5.2	5.1
VII	–	–	–	–	19.8	9.3	31.3	26	2.4	9	12.2	18.1	13.5	14.3	12.7	12.9	13.4	13.0	8.8	6.2	8.5	7.8	1.7	8.8	2.5	4.3	5.5	6.8	5.2	5.8
VIII	–	–	–	–	20.9	10.7	29.5	13	7.0	10, 30	13.6	19.7	14.0	15.3	13.3	14.2	13.7	13.7	8.4	6.2	8.5	7.7	2.4	9.4	2.4	4.7	6.1	7.3	3.9	5.8
IX	–	–	–	–	17.5	6.7	29.2	4	2.2	15, 20	9.2	16.1	10.7	11.7	10.3	11.4	10.8	10.8	8.8	6.3	8.5	7.9	1.7	7.7	2.5	4.0	6.2	5.5	3.2	5.0
X	–	–	–	–	13.7	4.4	24.4	4	-1.7	22	5.4	12.4	6.9	7.9	8.6	10.4	9.7	9.4	9.3	7.2	8.9	8.5	0.7	4.9	1.2	2.3	5.2	4.1	4.3	4.5
XI	–	–	–	–	6.0	1.6	16.6	8	-4.4	21	2.8	5.0	3.4	3.6	6.6	7.0	6.7	6.8	8.6	7.9	8.4	8.3	1.2	2.1	1.4	1.6	7.4	7.2	7.2	7.3
XII	–	–	–	–	-1.8	-7.2	8.3	9	-19.9	27	-5.5	-3.1	-5.1	-4.7	3.5	3.9	3.7	3.7	7.9	7.6	8.2	7.9	1.0	1.4	0.8	1.1	6.6	6.6	6.9	6.7
Rok	–	–	–	–	10.9	2.5	31.3	26.VII	-19.9	27.XII	4.7	9.5	5.8	6.6	8.0	8.5	8.4	8.3	8.4	6.6	8.1	7.7	1.6	5.5	2.0	3.0	6.3	6.5	5.5	6.1

Suchedniów I $H_s = 272\,m$ $h_w = 13{,}5\,m$ 1962

Miesiąc	Rozkład wiatru (n_D, v_{mD}) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Liczba dni (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◐	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R
I	4	4.0	2	3.0	·	·	·	·	12.5	3.2	24	2.6	32.5	3.0	5	3.3	13	2.6	42	8.1	14, 27	2	8	23	·	·	·	1	13	12	9	·	·	17	·
II	7	2.6	4	1.8	7	1.9	1	2.0	1.5	5.3	16	4.3	19	3.7	12.5	4.1	16	2.8	63	16.2	12	4	14	25	·	1	·	1	20	21	12	2	2	28	1
III	17	2.8	3.5	3.6	2.5	4.2	3	5.0	8	3.1	10	3.0	8.5	3.2	9.5	2.6	31	2.1	76	17.2	16	9	12	26	·	·	·	4	18	17	10	1	3	23	·
IV	8.5	2.4	3	2.7	1	7.0	5.5	5.1	9.5	3.9	9	2.8	12	2.2	8.5	3.6	33	2.0	54	9.9	27	·	·	2	5	·	·	5	9	16	10	·	·	·	1
V	2.5	2.4	0.5	1.0	1	2.5	2.5	3.4	6	2.8	6	2.9	24	3.2	7.5	2.3	43	1.6	158	37.2	14	·	·	2	·	·	·	1	12	25	21	3	3	·	3
VI	8.5	3.5	·	·	·	·	·	·	2	2.5	1.5	2.7	32	2.6	17	2.3	29	1.8	59?	23.4	1	·	·	·	6	·	·	7	10	14	9	2	·	·	1
VII	3	1.8	0.5	3.0	·	·	·	·	2	2.5	3.5	2.6	38	2.3	12	2.3	34	1.5	113	55.0	22	·	·	·	5	·	·	4	11	18	14	2	·	·	7
VIII	·	·	·	·	1	2.5	1	2.5	6	2.4	8.5	2.6	33	2.4	1.5	3.7	42	1.4	51	13.2	15	·	·	·	9	·	·	5	5	15	12	1	3	·	2
IX	2.5	2.8	0.5	1.0	1	3.0	1.5	3.7	3	1.3	10	2.5	28	2.6	4.5	3.5	39	1.5	54	16.2	17	·	·	·	2	·	·	8	9	16	10	2	4	·	1
X	7.5	1.9	3	1.5	4.5	2.4	3.5	2.4	2.5	2.2	3.5	2.3	13	3.0	4.5	2.1	51	1.1	2	0.8	14	·	·	11	·	·	·	11	7	5	·	·	12	·	·
XI	4	1.1	7	3.0	10.5	3.5	12	3.8	6.5	3.1	8	2.9	10.5	2.5	3.5	1.3	28	2.0	38	6.0	15	·	1	8	·	·	·	1	21	20	12	·	4	2	·
XII	6.5	2.2	4.5	2.4	3	2.7	0.5	3.0	7.5	2.5	11	3.0	14.5	2.7	2.5	2.2	43	1.4	33	6.9	15	11	14	28	·	·	·	1	16	16	8	·	2	18	·
Rok	71	2.3	28.5	1.9	31.5	2.5	30.5	2.6	67	2.9	111	2.8	265	2.8	88.5	2.8	402	1.8	735?	55.0	22. VII	26	49	125	27	1	·	49	151	195	127	13	33	88	16

Suchedniów II $H_s = 278\,m$ $h_w = 15{,}4\,m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	3	1.8	2.5	1.6	3	2.7	2	3.5	10	2.9	11	3.6	18	2.9	17.5	3.3	23	2.3	53	15.4	17	·	·	·	1	·	·	4	5	15	10	2	5	·	1
X	5	1.8	6	1.8	6.5	1.8	2.5	2.6	5	2.0	3.5	2.6	9.5	3.2	10	3.3	45	1.3	3	1.0	14	·	·	10	·	·	·	8	9	4	1	·	13	·	·
XI	6	1.7	5	3.1	16	2.7	8	3.1	5	2.5	4.5	2.7	10.5	2.9	5	3.1	30	1.8	41	6.3	15	·	1	11	·	·	·	·	22	18	11	·	4	1	·
XII	10.5	2.6	8.5	2.2	2	1.8	1	2.0	13	4.6	4.5	4.4	11.5	3.0	12	2.8	30	2.2	26	6.5	13	11	15	29	·	·	·	·	19	14	7	·	4	16	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Krasnystaw $H_s = 190\,m$ $h_w = 12{,}0\,m$ I–X, $14{,}8\,m$ XI–XII

I	7.5	2.1	4.5	2.2	0.5	1.0	4.5	1.8	14.5	1.6	42	2.7	13.5	2.7	6	3.3	·	2.4	17	4.3	13	2	8	23	·	·	·	1	15	13	7	·	·	–	–
II	7	1.8	9	2.2	7	2.9	6	1.9	9	4.9	11.5	6.6	23	6.4	6.5	6.6	5	4.5	31?	6.2	12	6	14	28	·	9	2	·	20	19	12?	·	2	26	–
III	7.5	3.4	7.5	3.5	12.5	1.8	14	3.7	8	2.2	15.5	3.3	12	4.4	9	3.0	7	3.0	55	21.2	16	4	11	28	·	5	·	·	14	12	9	1	6	19	–
IV	2	3.0	5.5	4.7	14	2.5	14	2.5	9.5	2.3	14	2.9	11	3.8	3	5.7	17	2.5	39	13.0	6	·	·	2	4	1	·	6	5	10	8	1	2	·	–
V	1.5	3.0	0.5	2.0	7.5	3.1	9	2.1	5	1.2	31.5	4.3	26	2.9	7	2.4	5	3.0	104	22.1	15	·	·	1	·	2	·	1	11	19	18	3	4	·	–
VI	4	2.5	7.5	4.3	7	3.0	6	4.0	8.5	2.3	23	3.7	14.5	3.2	10.5	2.3	9	2.9	88	25.4	1	·	·	·	10	1	·	2	13	12	11	3	·	·	–
VII	·	·	3	2.3	1	1.0	3	1.7	5	1.2	31	3.0	26	3.3	5	2.0	19	2.2	96	22.2	16	·	·	·	4	1	·	5	10	15	14	4	2	·	–
VIII	3	2.0	5	2.0	4	3.5	1	2.0	7	2.6	32	4.0	28	4.0	8	2.9	5	3.3	41	7.9	1	·	·	·	8	·	·	3	4	12	10	·	4	·	–
IX	1	3.0	1	1.0	9	2.2	3	2.3	1	7.0	44.5	3.8	11.5	4.5	1	3.0	18	2.9	47	18.4	5	·	·	·	2	·	·	4	7	15	10	1	7	·	–
X	1	4.0	·		11.5	1.7	10.5	1.6	9	2.3	26	2.9	12	3.7	4	1.0	19	2.0	3	1.7	14	·	·	9	·	·	·	3	9	3	2	·	22	·	–
XI	7.5	2.5	7	3.9	13	7.9	22.5	5.1	5.5	1.8	11	5.7	10.5	4.0	8	2.2	5	4.4	49	10.0	15	·	·	5	·	6	1	2	22	16	13	1	8	1	–
XII	10.5	2.1	10.5	3.9	4.5	2.9	4.5	2.9	16.5	3.5	13	5.8	10.5	3.0	13	3.0	10	3.1	15	3.3	14	11	16	30	·	1	1	2	19	16	8	·	3	16	–
Rok	52.5	2.4	61	2.7	91.5	2.8	98	2.6	98.5	2.7	295	4.1	198.5	3.8	81	3.1	119	3.0	585?	25.4	1. VI	23	49	126	28	26	4	29	149	162	122	14	60	–	–

Wojcieszów Górny $H_s = 358\,m$ $h_w = 23\,m$

I	6	4.1	4.5	3.7	3	2.3	0.5	2.0	14	3.3	24	3.9	19	3.0	5	3.8	17	2.8	56	14.8	26	3	6	19	·	2	·	4	12	13	10	2	1	15	1
II	11	2.9	3	2.3	3	1.3	·	·	2.5	7.2	16.5	5.6	10.5	3.0	9.5	5.0	28	2.8	60	10.8	12	3	10	25	·	1	·	·	14	19	14	1	2	23	·
III	17	2.5	1	2.0	4	2.0	·	·	5.5	2.8	14.5	3.0	6.5	3.7	6.5	2.3	38	1.6	50	12.1	31	1	10	27	·	·	·	2	12	13	7	3	4	25?	·
IV	9.5	1.8	0.5	2.0	3	1.3	1	2.0	6.5	3.0	16.5	3.3	9.5	3.0	14.5	2.6	29	1.8	56	17.2	28	·	·	2	4	·	·	8	8	15	12	1	1	1?	1
V	5.5	2.7	·	·	·	·	·	·	5	2.2	17	2.8	14.5	2.6	14	3.0	37	1.6	94	26.7	14	·	·	2	·	·	·	·	14	22	16	1	2	1?	2
VI	11	2.1	·	·	·	·	1	2.0	0.5	2.0	4.5	2.9	11.5	3.7	22.5	2.8	39	1.6	40	13.6	16	·	·	·	7	·	·	6	8	10	8	1	·	·	1
VII	3	2.3	·	·	2	1.5	·	·	4	2.2	8	2.9	13	2.8	12	2.8	51	1.2	77	19.3	16	·	·	·	5	·	·	1	9	17	13	2	2	·	9
VIII	4	2.2	2	4.5	2.5	2.0	1	2.5	3.5	2.1	17.5	2.5	5	2.3	16.5	2.1	41	1.3	61	15.1	14	·	·	·	4	·	·	1	6	16	11	2	·	·	1
IX	1	1.0	·	·	·	·	3	1.7	16	2.1	12.5	2.5	8.5	2.6	13	1.9	36	1.3	66	21.8	16	·	·	·	3	·	·	5	6	11	8	3	1	·	·
X	3	2.0	·	·	·	·	2	2.0	11	1.5	7	1.6	6	1.3	8	2.1	56	0.7	46	16.3	31	·	·	3	·	·	·	12	10	12	8	1	10	·	·
XI	9	1.7	·	·	1	2.0	2	1.0	15.5	4.8	9.5	3.9	6	2.3	3	1.3	44	1.7	32	9.6	1	·	1	8	·	1	·	1	18	13	6	·	9	6	·
XII	11.5	1.4	6.5	2.0	4	1.5	·	·	6.5	3.1	16.5	2.6	12	2.8	4	1.2	32	1.5	46	12.4	16	11	15	25	·	·	·	5	16	15	9	1	1	25	·
Rok	91.5	2.2	17.5	1.4	22.5	1.2	10.5	1.1	90.5	3.0	164	3.1	122	2.8	128.5	2.6	448	1.7	684	26.7	14. V	18	42	111	23	4	·	45	133	176	122	18	33	96?	15

Otawa-Zwierzyniec $\varphi = 50°57'$ $\lambda = 17°18'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																		
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.5	-1.8	10.4	22	-14.9	31	-0.1	2.4	0.4	0.8	–	–	–	–	–	–	–	–	–	–	–	–	74	66	76	72
II	–	–	–	–	2.0	-3.5	8.0	12	-12.5	1	-1.8	0.2	-0.8	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	88	94	72	85
III	–	–	–	–	3.9	-2.8	15.6	31	-6.2	8, 14, 15	-1.8	2.6	0.3	0.4	–	–	–	–	–	–	–	–	–	–	–	–	70	76	65	70
IV	–	–	–	–	16.3	6.2	28.1	24	0.7	2	8.2	14.5	10.5	10.9	–	–	–	–	–	–	–	–	–	–	–	–	68	74	52	65
V	–	–	–	–	16.1	7.3	23.0	19	-0.9	1	9.6	14.0	10.8	11.3	–	–	–	–	–	–	–	–	–	–	–	–	70	79	73	74
VI	–	–	–	–	21.0	10.1	31.2	23	3.6	6	13.4	19.3	14.9	15.6	–	–	–	–	–	–	–	–	–	–	–	–	54	65	53	57
VII	–	–	–	–	22.0	11.1	31.9	26	7.6	30	14.1	20.5	15.7	16.5	–	–	–	–	–	–	–	–	–	–	–	–	61	61	65	62
VIII	–	–	–	–	24.0	13.1	32.4	13	8.5	31	15.6	22.0	16.8	17.8	–	–	–	–	–	–	–	–	–	–	–	–	61	67	44	57
IX	–	–	–	–	19.1	8.2	31.9	4	3.6	15	10.5	17.3	12.1	13.0	–	–	–	–	–	–	–	–	–	–	–	–	66	59	35	53
X	–	–	–	–	13.8	4.7	23.1	1	-1.9	23	6.0	12.4	7.9	8.6	–	–	–	–	–	–	–	–	–	–	–	–	79	54	47	60
XI	–	–	–	–	6.9	2.5	17.2	8	-2.8	26	3.7	6.3	4.2	4.6	–	–	–	–	–	–	–	–	–	–	–	–	87	85	69	80
XII	–	–	–	–	-0.8	-6.3	5.4	12, 13	-18.8	22	-4.7	-2.0	-3.8	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	88	75	73	79
Rok	–	–	–	–	12.3	4.1	32.4	13.VIII	-18.8	22.XII	6.1	10.8	7.4	7.9	–	–	–	–	–	–	–	–	–	–	–	–	72	71	60	68

Bodzentyn $\varphi = 50°57'$ $\lambda = 20°57'$

I	–	–	–	–	–	-3.7	–	–	-22.3	31	-1.6	0.5	-1.2	-0.9	–	–	–	–	–	–	–	–	–	–	–	–	75	67	72	71
II	–	–	–	–	–	-6.3	–	–	-20.8	1	-4.2	-1.3	-3.1	-2.9	–	–	–	–	–	–	–	–	–	–	–	–	89	90	85	88
III	–	–	–	–	1.7	-6.9	13.4	31	-18.1	19	-4.7	0.4	-3.1	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	77	77	58	71
IV	–	–	–	–	16.0	4.9	26.2	22, 23	0.4	2, 8	8.2	14.3	9.4	10.3	–	–	–	–	–	–	–	–	–	–	–	–	65	66	46	59
V	–	–	–	–	15.3	6.5	22.6	8	-2.0	1	9.2	13.5	9.9	10.6	–	–	–	–	–	–	–	–	–	–	–	–	81	86	71	79
VI	–	–	–	–	18.9	8.2	29.6	23	3.2	7	12.7	17.0	12.7	13.8	–	–	–	–	–	–	–	–	–	–	–	–	54	74	53	60
VII	–	–	–	–	21.5	9.9	30.0	26	3.7	5	13.6	19.6	13.8	15.2	–	–	–	–	–	–	–	–	–	–	–	–	61	70	55	62
VIII	–	–	–	–	22.1	10.8	30.4	13	5.0	27	14.6	20.4	14.9	16.2	–	–	–	–	–	–	–	–	–	–	–	–	58	68	55	60
IX	–	–	–	–	17.6	6.7	26.8	4	0.6	26	9.0	16.0	10.7	11.6	–	–	–	–	–	–	–	–	–	–	–	–	59	58	35	51
X	–	–	–	–	13.0	2.1	21.5	1	-4.5	16	4.3	12.1	5.2	6.7	–	–	–	–	–	–	–	–	–	–	–	–	60	42	33	45
XI	–	–	–	–	6.0	1.6	14.5	5	-2.3	18	2.6	5.4	3.4	3.7	–	–	–	–	–	–	–	–	–	–	–	–	86	84	76	82
XII	–	–	–	–	-2.5	-9.0	3.4	12	-24.9	22	-5.5	-3.4	-5.9	-5.2	–	–	–	–	–	–	–	–	–	–	–	–	84	73	75	77
Rok	–	–	–	–	–	2.1	30.4	13.VIII	-24.9	22.XII	4.8	9.5	5.6	6.4	–	–	–	–	–	–	–	–	–	–	–	–	71	71	60	67

Silniczka $\varphi = 50°55'$ $\lambda = 19°46'$

I	–	–	–	–	2.2	-4.1	8.7	22	-18.9	31	-1.0	1.3	-1.1	-0.5	5.1	5.1	5.1	5.1	8.6	7.5	8.7	8.3	0.9	1.8	0.9	1.2	79	67	62	69
II	–	–	–	–	0.3	-5.7	5.4	13	-18.5	3	-3.8	-0.9	-2.3	-2.3	4.2	4.6	4.7	4.5	8.7	7.9	8.8	8.5	0.6	1.3	0.7	0.9	91	86	78	85
III	–	–	–	–	2.2	-6.7	14.6	31	-16.3	26	-4.2	1.3	-2.5	-2.0	4.2	4.9	4.7	4.6	8.9	7.0	8.7	8.2	0.5	2.2	0.6	1.1	81	78	70	76
IV	–	–	–	–	15.8	3.9	26.8	23	-1.0	6	7.1	14.4	8.5	9.6	8.7	8.0	9.1	8.6	8.5	5.2	8.0	7.2	1.7	10.1	2.5	4.8	79	83	66	76
V	–	–	–	–	15.2	5.9	22.8	8	-2.7	1	9.2	13.0	9.7	10.4	10.4	10.1	11.0	10.5	8.8	6.8	8.9	8.2	1.5	5.4	1.4	2.8	80	84	86	83
VI	–	–	–	–	19.1	8.2	30.0	23	2.9	2	12.8	17.5	12.4	13.8	12.1	11.1	12.7	12.0	8.0	5.7	8.6	7.4	3.3	10.4	2.2	5.3	67	73	65	68
VII	–	–	–	–	21.0	9.8	30.3	26	4.0	30	13.7	19.3	13.9	15.2	13.8	12.6	13.9	13.4	8.7	5.8	8.7	7.7	2.1	10.1	2.3	4.8	66	76	73	72
VIII	–	–	–	–	22.5	10.8	31.5	7	4.5	27	14.9	21.0	15.6	16.8	14.7	14.9	15.7	15.1	8.5	6.0	8.7	7.7	2.5	10.8	2.3	5.2	77	79	54	70
IX	–	–	–	–	17.5	6.1	28.3	4	0.0	15	9.4	16.0	10.3	11.5	10.8	11.3	11.3	11.1	9.0	6.3	8.9	8.1	1.3	7.7	1.6	3.5	79	72	50	67
X	–	–	–	–	13.3	1.6	20.3	1	-5.9	16	4.2	12.4	5.1	6.7	8.3	9.5	8.5	8.8	9.6	6.5	9.4	8.5	0.3	5.3	0.5	2.0	83	50	55	63
XI	–	–	–	–	6.4	1.8	15.1	8	-2.4	17	3.0	5.6	3.8	4.0	7.2	7.7	7.4	7.4	9.3	8.3	9.1	8.9	0.6	1.8	0.7	1.0	86	82	88	85
XII	–	–	–	–	-2.3	-8.6	5.9	12	-23.5	22	-5.8	-3.0	-5.7	-5.0	3.8	4.2	3.9	4.0	8.8	8.2	8.9	8.6	0.5	1.0	0.5	0.7	91	88	74	84
Rok	–	–	–	–	11.1	1.9	31.5	7.VIII	-23.5	22.XII	5.0	9.8	5.6	6.5	8.6	8.7	9.0	8.8	8.8	6.8	8.8	8.1	1.3	5.7	1.4	2.8	80	76	68	75

Kraśnik Lubelski $\varphi = 50°55'$ $\lambda = 22°12'$

I	–	–	–	–	0.5	-3.6	5.0	22	-19.2	31	-2.1	-0.6	-1.6	-1.5	–	–	–	–	–	–	–	–	–	–	–	–	70	64	64	66
II	–	–	–	–	-1.0	-6.4	2.9	7, 13	-13.6	25	-4.6	-2.2	-3.4	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	87	84	87	86
III	–	–	–	–	0.9	-5.4	11.5	31	-13.6	21	-4.0	-0.3	-2.5	-2.3	4.3	4.9	4.6	4.6	8.8	7.8	8.6	8.4	0.5	1.3	0.7	0.8	83	74	59	72
IV	–	–	–	–	15.7	5.8	26.0	22	-0.7	8	8.0	14.2	9.8	10.4	9.1	9.6	9.0	9.2	8.4	6.2	7.5	7.4	2.1	8.1	3.8	4.7	64	58	41	54
V	–	–	–	–	14.9	6.7	21.9	20	-2.0	1	9.3	13.3	10.4	10.8	10.9	11.4	11.1	11.1	9.1	7.4	8.6	8.4	1.2	4.5	1.8	2.7	80	89	65	78
VI	–	–	–	–	18.2	9.7	28.3	16	2.5	6	12.4	16.7	13.3	13.9	12.5	12.3	12.6	12.5	8.5	6.5	8.1	7.7	2.6	8.1	3.4	4.7	63	74	56	64
VII	–	–	–	–	20.5	11.0	27.7	26	6.7	29	13.7	18.8	14.8	15.5	13.8	14.1	13.8	13.9	8.7	6.5	8.1	7.8	2.1	8.1	3.3	4.5	61	72	58	64
VIII	–	–	–	–	21.9	12.7	29.3	13	7.3	31	14.8	20.2	16.4	17.0	15.2	15.5	15.6	15.4	8.9	6.6	8.3	7.9	1.9	8.8	3.3	4.7	66	67	46	60
IX	–	–	–	–	17.0	7.6	26.1	5	2.6	15	9.2	15.4	11.3	11.8	10.8	11.9	11.9	11.5	9.2	6.9	8.8	8.3	1.0	6.2	1.8	3.0	63	71	41	58
X	–	–	–	–	12.3	3.4	18.4	1, 2	-1.8	26	4.4	11.2	7.1	7.4	–	–	–	–	–	–	–	–	–	–	–	–	70	60	35	55
XI	–	–	–	–	6.6	1.8	17.6	1	-2.2	18	3.0	5.4	3.7	4.0	7.2	7.5	7.2	7.3	9.3	8.4	8.9	8.9	0.6	1.8	1.0	1.1	93	83	80	85
XII	–	–	–	–	-2.8	-8.3	3.1	13	-21.1	22	-6.0	-4.4	-6.0	-5.6	3.7	4.0	3.8	3.8	8.8	8.5	8.7	8.7	0.5	0.6	0.5	0.5	9.0	8.1	6.5	7.9
Rok	–	–	–	–	10.4	2.9	29.3	13.VIII	-21.1	22.XII	4.8	9.0	6.1	6.5	–	–	–	–	–	–	–	–	–	–	–	–	74	73	58	68

Oława-Zwierzyniec $H_S = 137\ m$ $h_w = 10\ m$ 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD Suma	OPAD Max	OPAD Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R 10
I	7	2.7	1	2.0	·	·	13.5	2.1	13.5	2.3	30	1.9	4.5	2.6	9.5	2.2	14	1.8	33	8.2	24	3	4	17	·	·	·	2	13	14	7	·	1	8	·
II	8.5	2.2	4.5	1.1	4.5	1.6	8	1.6	4	2.5	15.5	4.1	17.5	5.2	10.5	3.3	11	2.9	35	7.4	17	2	9	23	·	5	3	·	16	16	9	·	·	16	·
III	10.5	3.2	5	1.4	3.5	2.7	23	2.7	3.5	2.0	7.5	1.9	4.5	2.7	16.5	3.4	19	2.0	65	18.1	12	·	5	25	·	·	·	2	15	14	9	3	5	9	·
IV	7	2.0	5	1.8	·	·	12	1.9	7.5	2.2	15.5	2.5	9	2.7	16	1.8	18	1.7	50	16.8	26	·	·	·	8	·	·	4	10	14	9	1	·	·	2
V	2.5	1.2	1.5	1.3	3	2.0	8	2.1	3.5	1.9	22	2.2	4.5	3.3	21	3.3	27	1.8	101	30.6	14	·	·	1	·	1	·	·	15	22	14	3	1	·	3
VI	7.5	2.7	0.5	2.0	2.5	1.2	7.5	1.9	4	1.9	7	2.4	10.5	3.8	27.5	2.4	23	1.9	18	4.7	1	·	·	·	9	·	·	2	9	7	5	·	·	·	1
VII	·	·	1	2.0	1.5	2.0	3.5	2.1	5.5	2.3	17	2.0	7.5	2.4	26	1.9	31	1.4	75	36.6	22	·	·	·	8	·	·	3	12	15	11	1	·	·	7
VIII	0.5	2.0	1	1.0	2	2.2	4	1.4	3.5	3.6	19	2.4	16.5	2.7	14.5	2.6	32	1.6	36	7.5	14	·	·	·	13	·	·	1	9	13	8	·	·	·	3
IX	1	2.0	·	·	9	2.2	14.5	1.7	3.5	3.1	13	3.0	9	3.4	17	2.3	23	1.8	56	22.8	17	·	·	·	4	1	·	5	7	15	7	2	3	·	·
X	1	3.0	3.5	1.4	7	1.9	23	1.8	2.5	2.0	3	2.3	2	1.5	18	2.0	33	1.2	34	17.2	31	·	·	5	·	·	·	6	12	16	7	1	18	·	·
XI	1	2.0	7	2.3	4	2.0	26.5	3.0	4	1.6	14	1.9	5.5	2.1	8	1.9	20	1.8	56	12.7	1	·	·	8	·	·	·	2	19	13	9	1	2	·	·
XII	8.5	1.6	6.5	1.7	7.5	1.6	6.5	1.5	9	3.2	13.5	2.5	5	2.3	5.5	2.0	31	1.4	19	6.2	15	10	14	25	·	·	·	2	19	11	5	·	3	15	·
Rok	55	2.0	36.5	1.5	44.5	1.6	150	2.0	64	2.4	177	2.4	96	2.9	190	2.4	282	1.8	578	36.6	22.VII	15	32	104	42	7	3	29	156	170	100	12	33	48	16

Bodzentyn $H_S = 270\ m$ $h_w = 14\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD Suma	OPAD Max	OPAD Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R 10
I	1.5	3.0	4.5	2.8	·	·	1.5	5.0	10	4.8	47.5	4.2	16.5	4.0	10.5	5.2	1	4.2	44	10.4	12	2	–	26	·	·	·	2	12	15	9	1	·	–	·
II	2	6.2	5.5	4.3	9.5	3.4	4.5	2.4	6.5	6.4	20	5.8	16.5	6.4	15.5	7.9	4	5.5	56	16.1	12	5	–	26	·	5	2	·	21	16	9	2	3	28	·
III	6	6.3	8	5.2	6.5	2.9	14	3.0	8	2.7	5	3.7	10.5	5.7	19	5.5	16	3.7	56	20.8	16	9	13	28	·	3	1	5	17	13	10	1	3	23	·
IV	1	3.0	10	2.4	5.5	2.9	10	5.0	8.5	3.6	19.5	3.0	9	4.4	13.5	3.9	13	3.1	62	16.4	26	·	·	·	5	2	·	3	7	11	9	2	·	·	1
V	3.5	1.6	6.5	2.5	4	2.6	6	2.4	4	2.2	27	3.6	17.5	4.1	15.5	2.9	9	2.9	153	23.1	14	·	·	1	·	2	1	·	19	25	22	6	2	·	2
VI	9.5	4.8	3.5	1.9	1	2.0	·	·	2	2.2	25.5	3.8	14	3.2	20.5	4.5	14	3.3	122	62.3	4	·	·	·	6	1	·	5	10	11	6	3	·	·	1
VII	2.5	2.8	1.5	4.0	·	·	3.5	1.6	4	2.9	27.5	2.9	18	3.3	19	2.6	17	2.4	137	38.6	22	·	·	·	5	1	·	3	9	13	11	4	1	·	5
VIII	·	·	3	2.0	1	1.0	3.5	2.9	4.5	3.2	32	3.0	14	3.3	9	2.6	26	2.1	63	13.7	3	·	·	·	9	·	·	2	7	12	10	1	2	·	4
IX	2.5	2.0	1.5	1.7	0.5	2.0	5	3.4	4.5	2.3	23	2.8	19.5	2.4	9.5	2.6	24	1.9	61	21.2	18	·	·	·	2	·	·	9	7	13	9	2	8	·	·
X	7	2.2	7.5	2.1	6.5	2.5	8.5	1.8	2	2.0	12	3.2	7.5	2.5	9	1.9	33	1.5	3	1.0	14	·	·	10	·	·	·	9	7	3	1	·	8	·	·
XI	6	1.8	7.5	3.0	15.5	2.7	15.5	2.3	4	1.6	13	2.9	8	2.2	9.5	1.8	11	2.1	38	8.8	15	·	1	9	·	·	·	2	19	13	11	·	12	3	·
XII	5	3.1	10	2.6	5	2.7	8	3.4	3	4.2	21.5	4.3	14.5	3.1	12	3.2	14	2.9	34	7.5	13	12	16	29	·	·	·	2	17	11	8	·	5	18	·
Rok	46.5	3.1	69	2.9	55	2.1	80	2.8	61	3.2	273.5	3.6	165.5	3.7	162.5	3.7	182	3.0	829	62.3	4.VI	28	–	129	27	14	4	42	152	156	115	22	44	–	13

Silniczka $H_S = 215\ m$ $h_w = 14\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD Suma	OPAD Max	OPAD Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R 10
I	4	6.8	3.5	5.1	·	·	3.5	3.3	18	2.6	27	4.2	14.5	5.8	6.5	6.0	16	3.7	40	6.3	24	5	6	22	·	3	·	·	12	15	10	·	1	17	·
II	3	2.7	6.5	3.7	8.5	3.7	7.5	3.0	8	3.6	9	7.2	16.5	7.1	15	7.4	10	4.8	27	7.2	12	5	14	25	·	7	·	·	18	19	7	·	1	21	1
III	12	6.0	11	2.9	11	3.9	12.5	3.5	2	1.2	4.5	4.0	9.5	6.8	3.5	4.3	27	3.1	54	17.5	12	8	14	26	·	3	·	1	17	16	8	2	2	21	·
IV	10	4.2	9.5	3.5	8	4.8	10	5.0	9.5	4.1	6	4.0	8.5	5.2	13.5	4.4	15	3.7	60	20.4	26	·	·	1	5	5	·	1	15	15	9	1	1	·	2
V	4	3.0	7	2.0	6	2.2	9.5	2.7	8	2.6	10	2.6	20.5	5.7	10	2.6	18	2.7	157	20.6	14	·	·	2	·	1	·	·	19	27	21	6	·	·	7
VI	14	3.8	8	2.8	4.5	2.1	8.5	1.9	1	4.0	4.5	3.7	21	4.6	15.5	3.8	13	3.1	82	26.6	4	·	·	·	6	1	·	·	11	11	7	3	·	·	1
VII	7	2.6	2.5	1.8	5	2.3	6	2.4	4.5	1.7	9	3.3	18	3.2	18	3.1	23	2.1	78	25.8	27	·	·	·	5	·	·	·	16	15	11	2	·	·	9
VIII	4	2.5	3.5	2.0	1.5	1.7	10	3.3	2.5	3.1	6.5	3.5	32.5	3.8	8.5	2.8	19	2.7	70	14.3	3	·	·	·	7	1	·	1	12	12	9	2	2	·	5
IX	1	4.0	3	2.5	8	3.3	5.5	2.5	7.5	2.6	11	3.7	19	4.0	9	4.6	26	2.6	48	18.5	17	·	·	·	2	·	·	4	13	13	7	2	3	·	1
X	7	2.6	5	2.7	11	2.3	21	2.3	0.5	3.0	4	4.0	11.5	3.5	6	3.9	27	2.0	9	6.0	28	·	·	12	·	·	·	3	10	10	2	·	16	·	·
XI	9	2.4	6	4.9	23	3.9	18.5	3.8	4.5	2.2	10.5	3.0	8.5	3.2	4	4.0	6	3.3	47	14.5	15	·	·	9	·	·	·	·	21	15	9	1	3	4	·
XII	6.5	4.2	14.5	3.7	9	2.6	6	3.4	9	4.8	12.5	3.9	14.5	3.6	4	3.0	17	3.0	25	8.1	16	12	15	29	·	·	·	·	20	14	7	·	3	18	·
Rok	81.5	3.7	80	3.1	95.5	2.7	118.5	3.1	80	3.0	114.5	3.9	194.5	4.7	113.5	4.2	217	3.1	697	26.6	4.VI	30	49	126	25	21	·	10	184	182	107	19	32	81	26

Kraśnik Lubelski $H_S = 250\ m$ $h_w = 13.5\ m$ I–XI, $h_w = 14.4\ m$ XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD Suma	OPAD Max	OPAD Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R 10
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	27	7.8	29	2	10	27	·	–	–	1	10	9	5	·	2	25	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6	16	28	·	–	–	·	18	–	–	–	·	28	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	39	10.7	16	3	17	28	·	–	–	1	15	15	9	1	2	25	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	28	7.6	27	·	·	4	4	–	–	6	9	13	9	·	1	·	2
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	126	21.2	15	·	·	1	·	–	–	·	16	25	18	4	1	·	6
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	134	54.6	4	·	·	·	6	–	–	2	11	14	9	4	·	·	2
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	92	32.9	18	·	·	·	4	–	–	2	9	19	14	2	2	·	9
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	59	19.4	5	·	·	·	6	–	–	3	8	11	11	2	3	·	5
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	53	23.4	18	·	·	·	2	–	–	3	8	16	9	1	6	·	2
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	2	1.2	14	·	·	8	·	–	–	4	7	6	1	·	14[2]	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	51	10.8	15	·	1	6	·	–	–	·	20	16	12	1	6	2	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	19	5.2	18	11	19	31	·	–	–	1	16	14	5	·	6	17	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	54.6	4.VI	22	63	133	22	–	–	23	147	–	–	–	43[2]	97	26

Swieradów-Zdrój $\varphi = 50°54'$ $\lambda = 15°20'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PREŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{a.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.6	-2.8	7.0	21	-15.5	31	-1.0	-0.1	-0.6	-0.6	4.6	4.8	4.6	4.7	76	75	75	75	1.0	1.6	1.4	1.3	7.3	8.7	7.6	7.9
II	–	–	–	–	-0.4	-5.3	5.0	12	-13.5	26	-3.7	-1.6	-2.8	-2.7	4.0	4.1	4.2	4.1	82	80	82	81	0.8	1.1	0.9	0.9	8.7	8.8	7.5	8.3
III	–	–	–	–	1.0	-5.0	11.0	11	-10.0	14	-3.4	0.0	-2.6	-2.2	3.9	4.3	3.8	4.0	79	69	77	75	1.0	2.0	1.1	1.4	7.8	7.6	7.0	7.5
IV	–	–	–	–	11.8	4.0	25.2	24	-1.8	7	6.4	10.5	6.6	7.5	6.9	7.2	7.0	7.0	72	60	73	68	3.6	7.3	3.4	4.8	6.5	6.8	5.7	6.3
V	–	–	–	–	11.9	4.8	20.4	19	-3.5	1	7.5	10.6	7.4	8.2	8.0	8.1	8.5	8.2	77	64	81	74	2.6	5.4	2.1	3.4	7.5	7.6	7.0	7.4
VI	–	–	–	–	16.9	7.7	27.4	16	-0.5	6	11.5	15.6	11.5	12.5	9.6	9.7	10.3	9.9	70	54	73	66	5.0	9.0	3.9	6.0	5.5	6.0	5.8	5.8
VII	–	–	–	–	17.7	9.4	28.6	26	3.8	9	13.0	16.5	12.0	13.4	11.6	11.7	11.6	11.6	77	63	84	75	4.0	8.0	2.4	4.8	6.2	6.9	6.5	6.5
VIII	–	–	–	–	19.1	10.9	27.4	13	6.4	9.30.31	14.3	18.0	13.4	14.8	12.7	13.0	12.3	12.7	77	63	79	73	4.0	8.1	3.4	5.2	6.0	5.6	4.9	5.5
IX	–	–	–	–	15.5	7.4	26.0	4	3.2	25	10.1	14.2	10.6	11.4	9.7	10.3	9.9	10.0	79	65	78	74	3.1	6.7	3.4	4.4	5.9	5.8	4.3	5.3
X	–	–	–	–	12.0	5.0	21.8	4	-0.5	21	6.5	11.0	7.6	8.2	8.2	9.3	8.8	8.8	82	70	83	78	1.9	4.6	2.0	2.8	5.8	5.2	4.7	5.2
XI	–	–	–	–	4.1	0.6	14.4	7, 8	-7.4	25	1.7	3.4	2.0	2.3	5.9	6.4	6.0	6.1	83	80	83	82	1.4	1.9	1.3	1.5	8.0	8.1	8.3	8.1
XII	–	–	–	–	-2.7	-7.3	5.3	8	-20.2	22	-5.6	-4.0	-5.4	-5.1	3.3	3.6	3.3	3.4	77	73	76	75	1.0	1.3	1.0	1.1	7.4	6.8	6.5	6.9
Rok	–	–	–	–	9.0	2.4	28.6	26. VII	-20.2	22. XII	4.8	7.8	5.0	5.6	7.4	7.7	7.5	7.5	7.8	6.8	7.9	7.5	2.4	4.8	2.2	3.1	6.9	7.0	6.3	6.7

Jelenia Góra $\varphi = 50°54'$ $\lambda = 15°48'$

I	975.3	996.2	951.4	1018.1	3.8	-3.7	11.0	22	-21.4	31	-0.9	1.8	-0.2	0.1	4.9	5.1	4.9	5.0	80	73	78	77	1.4	2.1	1.6	1.7	7.6	8.1	7.1	7.6
II	975.5	993.0	946.2	1018.6	1.1	-6.5	6.5	12	-21.5	1	-3.5	-0.4	-2.0	-2.0	4.2	4.7	4.5	4.5	85	76	83	81	0.8	1.4	1.0	1.1	8.8	8.6	7.6	8.3
III	969.6	986.8	949.2	1012.3	2.7	-5.0	13.0	30	-13.9	15	-3.0	1.4	-1.5	-1.2	4.4	4.6	4.5	4.5	86	66	79	77	0.8	2.4	1.1	1.4	8.5	8.0	7.2	7.9
IV	973.4	985.9	947.2	1014.8	14.5	2.9	26.3	23	-3.6	11	5.7	12.5	7.4	8.2	7.8	7.4	8.2	7.8	84	55	78	72	1.8	8.8	2.8	4.5	7.1	7.5	5.9	6.8
V	973.1	979.2	964.2	1014.4	14.1	4.1	22.2	8	-4.0	1	7.7	12.3	8.7	9.4	9.2	9.2	9.8	9.4	87	64	86	79	1.5	5.7	1.6	2.9	8.4	8.4	7.7	8.2
VI	979.2	989.3	970.2	1020.0	19.0	7.1	29.7	23	-0.9	8	11.1	17.1	12.6	13.4	11.1	10.6	11.8	11.2	81	53	78	71	2.6	10.2	3.4	5.4	5.6	7.1	6.4	6.4
VII	975.3	985.7	960.7	1015.9	19.8	8.0	31.4	26	2.2	4	11.9	18.0	13.1	14.0	12.9	12.7	13.1	12.9	91	62	86	80	1.3	8.9	2.3	4.2	6.5	7.9	6.5	7.0
VIII	976.5	984.0	963.8	1017.0	21.4	9.7	30.1	13	3.4	31	13.0	19.6	13.8	15.0	13.7	14.1	14.1	14.0	90	63	89	81	1.5	9.2	1.9	4.2	6.6	7.5	5.4	6.5
IX	976.4	986.6	960.8	1017.4	18.0	4.9	29.5	4	-1.2	15	8.3	16.1	9.7	11.1	10.1	10.8	10.6	10.5	91	61	87	80	1.4	8.5	2.1	4.0	6.7	6.8	4.1	5.9
X	981.3	993.3	967.9	1023.2	14.0	1.8	24.8	3	-6.2	24	3.3	12.9	5.6	6.8	7.9	9.4	9.0	8.8	97	65	95	86	0.3	6.5	0.5	2.4	6.1	5.1	4.7	5.3
XI	974.3	992.5	956.2	1016.5	5.7	0.5	15.6	8	-6.9	24	2.2	4.9	2.9	3.2	6.6	7.1	6.7	6.8	91	81	88	87	0.9	2.0	1.1	1.3	8.4	8.2	7.7	8.1
XII	974.5	1002.3	933.2	1018.2	-2.5	-10.7	8.3	12	-26.1	21	-7.6	-3.6	-7.0	-6.3	3.4	4.0	3.4	3.6	88	81	86	85	0.6	1.1	0.6	0.8	8.1	7.5	7.2	7.6
Rok	975.4	1002.3	933.2	1017.2	11.0	1.1	31.4	26. VII	-26.1	21. XII	4.0	9.4	5.3	6.0	8.0	8.3	8.4	8.2	88	67	84	80	1.2	5.6	1.7	2.8	7.4	7.6	6.5	7.2

Sobótka $\varphi = 50°54'$ $\lambda = 16°45'$

I	–	–	–	–	4.1	-1.5	10.5	22	-15.7	31	0.9	2.5	1.2	1.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	1.7	-3.6	6.5	8	-13.7	1	-1.3	0.5	-0.7	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	2.9	-3.0	14.4	31	-7.2	14	-0.4	1.9	-0.4	0.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	15.1	6.3	27.1	24	-1.1	7	9.8	13.9	10.3	11.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15.0	7.2	22.1	8	-0.7	1	10.2	13.5	10.6	11.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	19.9	10.6	30.0	16	2.4	6	13.8	18.3	15.0	15.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.0	12.0	31.3	26	7.4	30	14.8	19.6	15.7	16.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	22.9	13.8	31.1	13	8.4	10	16.5	21.3	17.3	18.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	18.6	8.8	31.0	4	4.1	26	11.7	16.8	13.2	13.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	13.4	5.5	23.4	3	-1.3	16	7.3	12.1	8.8	9.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.4	1.8	16.3	7	-1.7	25	3.2	5.6	3.8	4.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-0.6	-6.3	6.6	7, 12	-18.4	22	-3.9	-2.2	-3.5	-3.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	11.7	4.3	31.3	26. VII	-18.4	22. XII	6.9	10.3	7.6	8.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Olesno $\varphi = 50°53'$ $\lambda = 18°25'$

I	–	–	–	–	2.0	-3.5	7.3	20	-18.2	31	-0.9	1.2	-0.8	-0.3	5.1	5.5	5.2	5.3	85	80	86	84	0.8	1.4	0.8	1.0	7.2	7.9	6.7	7.3
II	–	–	–	–	0.8	-5.6	6.9	13	-15.2	2, 3	-3.3	-0.7	-2.0	-2.0	4.3	4.7	4.9	4.6	86	80	87	84	0.7	1.2	0.7	0.9	8.0	8.0	8.0	8.3
III	–	–	–	–	3.0	-4.5	14.6	31	-9.6	25	-2.8	1.8	-1.0	-0.8	4.6	4.8	5.0	4.8	88	67	83	79	0.6	2.5	0.9	1.3	7.7	7.8	6.5	7.3
IV	–	–	–	–	15.5	5.2	27.7	23	-1.0	7	8.1	14.0	9.3	10.2	8.7	8.7	9.6	9.0	80	58	80	73	2.6	9.5	2.8	5.0	7.1	7.1	5.8	6.7
V	–	–	–	–	15.0	6.0	22.1	8, 19	-2.4	1	8.8	13.1	9.9	10.4	10.3	10.4	11.0	10.6	89	69	88	82	1.3	5.3	1.5	2.7	7.9	7.8	6.6	7.4
VI	–	–	–	–	19.3	8.5	29.9	16	1.6	3	12.6	17.7	13.7	14.4	12.2	11.6	12.6	12.1	81	57	79	72	3.1	10.1	3.9	5.7	5.6	7.1	5.6	6.1
VII	–	–	–	–	20.9	9.8	31.1	26	5.3	29	13.9	19.3	14.6	15.6	13.7	13.8	14.3	13.9	86	62	85	78	2.4	9.3	2.7	4.8	6.6	6.7	5.7	6.3
VIII	–	–	–	–	23.2	11.7	31.8	7	5.8	31	14.9	21.7	15.7	17.0	14.8	14.9	15.5	15.1	87	58	86	77	2.4	12.0	2.6	5.7	6.1	6.5	4.9	5.8
IX	–	–	–	–	17.8	7.6	29.7	4	1.2	15	9.6	16.2	11.9	12.4	11.0	12.2	11.9	11.7	92	68	86	82	1.3	7.1	2.6	3.7	6.8	6.4	3.0	5.4
X	–	–	–	–	13.2	3.6	22.7	3	-2.8	23	5.5	12.2	6.9	7.9	9.1	10.3	9.6	9.7	97	72	9.4	8.8	0.3	4.5	0.7	1.8	6.9	5.0	3.5	5.1
XI	–	–	–	–	6.4	1.3	18.8	8	-4.0	24	2.9	5.8	3.6	4.0	7.2	7.7	7.5	7.5	9.4	8.2	9.2	8.9	0.5	2.1	0.6	1.1	8.5	8.3	7.7	8.2
XII	–	–	–	–	-2.1	-7.4	5.4	13	-19.2	22	-5.4	-3.1	-4.8	-4.5	4.0	4.4	4.1	4.2	91	8.5	8.9	8.8	0.4	0.8	0.5	0.6	8.6	7.8	6.9	7.8
Rok	–	–	–	–	11.2	2.7	31.8	7. VIII	-19.2	22. XII	5.3	9.9	6.4	7.0	8.8	9.1	9.3	9.1	8.8	7.0	8.6	8.1	1.4	5.5	1.7	2.9	7.2	7.3	5.9	6.8

Świeradów-Zdrój $H_s = 549\ m$ $h_w = 13{,}5 m$ 1962

MIESIĄC	ROZKŁAD WIATRU ^0D, ^vmD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v v>10	v>15	◉	●	Opad R R≥0.1	R≥1.0	R≥10.0	═	▦	R/10
I	7	1.7	·	·	·	·	6.5	3.8	20	6.7	28.5	4.8	13.5	3.6	12.5	3.4	5	4.3	132	27.3	26	2	7	23	·	7	·	2	17	21	16	4	1	27	·
II	5.5	3.5	4.5	2.6	3	1.7	3.5	1.0	11.5	4.3	13	6.1	18	4.3	20	4.3	5	4.0	132	17.9	12	3	13	26	·	3	·	2	21	20	16	6	1	28	1
III	4	3.6	1	1.0	2	2.2	2.5	2.4	19.5	5.1	18	2.8	10.5	2.6	23.5	2.6	12	2.8	101	25.8	12	·	14	27	·	2	·	1	19	17	13	3	3	31	·
IV	2	1.7	0.5	1.0	6	4.0	1.5	5.0	37	3.4	17.5	2.5	8	2.0	10.5	2.6	7	2.8	84	16.4	28	·	·	4	1	2	·	5	13	17	14	3	3	3	1
V	1	1.0	·	·	1	1.0	1	3.0	17	2.4	31.5	2.4	24.5	2.3	12	2.2	5	2.2	149	23.3	14	·	·	2	·	·	·	·	11	26	21	5	2	2	4
VI	4	1.0	·	·	·	·	·	·	15	2.6	23.5	2.1	18	2.6	21.5	1.9	8	2.0	51	19.6	28	·	·	1	4	·	·	3	9	13	8	1	·	·	4
VII	0.5	2.0	·	·	·	·	0.5	1.0	20.5	2.5	21.5	1.9	34	2.7	11	1.7	5	2.2	136	25.5	15	·	·	·	2	·	·	3	14	17	15	6	1	·	7
VIII	·	·	·	·	·	·	2	1.5	19	2.7	38.5	2.7	21	2.7	6.5	1.5	6	2.4	89	17.6	24	·	·	·	2	·	·	3	7	16	14	3	3	·	3
IX	0.5	1.0	·	·	·	·	4	1.2	25.5	4.0	24	3.5	17	2.7	14	3.2	5	3.1	85	19.4	23	·	·	·	2	1	·	8	7	15	10	4	2	·	1
X	3	3.2	1	4.0	·	·	9	3.3	28	4.0	19.5	2.5	6.5	1.9	14	2.3	12	2.7	44	12.6	27	·	·	1	·	3		11	11	14	9	2	7	·	·
XI	1	2.5	5	1.7	·	·	8	7.1	23	5.8	11.5	3.4	12.5	2.2	7	2.3	22	3.1	43	16.7	1	·	5	16	·	6	·	·	17	18	10	1	9	14	·
XII	0.5	2.0	1	1.0	3.5	3.7	7	3.2	18.5	4.5	15.5	3.6	13	2.8	10	2.8	24	2.6	79	19.5	16	9	19	30	·	3	·	3	13	16	12	3	3	31	·
Rok	29	1.9	13	0.9	15.5	1.0	45.5	2.7	254.5	4.0	262.5	3.2	196.5	2.7	162.5	2.6	116	2.8	1125	27.3	26. I	14	58	130	11	27	·	41	159	210	158	41	35	136	21

Jelenia Góra $H_s = 342\ m$ $H_b = 343{,}9\ m$ $h_w = 16\ m$

I	2	4.0	4	2.2	5	2.5	14.5	2.6	4	3.2	14.5	5.4	23	5.3	9	6.2	17	3.6	43	12.5	26	4	5	21	·	6		1	15	15	9	1	·	16	·
II	2.5	3.0	3.5	4.1	10	4.6	4.5	2.6	·	·	3.5	7.3	25.5	7.0	14.5	5.3	20	4.3	41	6.9	13	6	9	27		8	2	1	20	19	12		2	22	·
III	4	4.1	6.5	2.3	13	3.0	7	3.1	1.5	3.3	2	4.5	15	4.7	12	4.2	32	2.4	44	13.6	31	2	10	27	·	1	·	·	20	14	7	1	1	14	·
IV	1.5	2.7	3	2.5	8	2.7	16.5	4.6	8	6.1	8	3.7	18	4.5	9	3.6	18	3.5	58	16.2	28	·	·	7	4	2	·	3	16	16	12	3	3	1	2
V	·	·	3	2.3	2	3.5	9	2.3	5.5	2.5	6.5	4.0	18.5	5.1	11.5	3.7	37	2.3	102	28.8	14	·	·	5	·	·	·	·	18	23	16	2	2	1	3
VI	2	3.2	1	2.0	3	2.3	5.5	1.5	7.5	2.0	8.5	4.2	21.5	4.2	17	3.9	24	2.6	47	14.9	16	·	·	1	6	·	·	2	13	12	10	1	1	·	4
VII	2.5	1.8	1.5	1.7	2.5	2.0	3.5	1.9	3	1.8	8.5	3.5	20	4.0	17.5	3.7	34	2.1	71	18.9	16	·	·	·	3	·	·	·	11	16	13	2	4	·	8
VIII	0.5	1.0	3.5	2.4	1.5	2.0	8.5	1.6	3	2.3	10.5	4.3	25.5	4.0	5	3.5	35	2.1	58	13.2	14	·	·	·	5	1	·	1	8	16	11	2	8	·	4
IX	·	·	3	3.0	4.5	3.0	12	2.4	3	2.7	9.5	6.0	20.5	4.4	10.5	3.1	27	2.6	87	37.2	16	·	·	2	3	1	·	3	9	11	10	2	13	·	1
X	1.5	1.3	2	3.8	7	3.0	6.5	1.8	5	1.7	2.5	1.8	11	3.7	11.5	2.7	46	1.4	41	21.3	31	·	·	10	·	·	·	9	11	13	6	1	17	·	·
XI	1	3.0	2.5	2.4	12	3.4	23.5	5.8	2	3.2	3	3.2	9.5	4.3	6.5	2.8	30	2.9	36	11.9	1		1	13	·	3	·	·	20	14	8	1	8	8	·
XII	8.5	1.6	2.5	2.4	2.5	2.6	10	3.8	3	6.0	8.5	4.4	11	4.4	6	3.9	41	2.1	42	14.7	16	17	19	26	·	·	·	2	18	18	8	1	7	25	·
Rok	26	2.1	36	2.6	71	2.9	121	2.8	45.5	2.9	85.5	4.4	219	4.6	130	3.9	361	2.7	670	37.2	16. IX	29	44	139	21	22	2	22	179	187	122	17	66	87	22

UWAGA. Kierunki i prędkości wiatru - wg anemometru.

Sobótka $H_s = 204\ m$ $h_w = 14\ m$

I	2	3.0	1.5	2.0	3.5	1.4	5	2.9	6	2.8	24.5	3.2	31	3.7	11.5	3.2	8	3.0	35	9.7	24	2	4	16	·	·	·	–	–	10	6	·	2	–	·
II	5.5	1.8	1.5	1.3	3	1.7	8.5	2.5	5.5	4.4	7.5	4.7	33	5.8	12.5	5.5	7	4.2	–	–	–	2	11	23	·	5	1?	–	–	–	–	–	2	–	·
III	4.5	3.6	6	1.3	5	2.0	17.5	2.2	4.5	2.6	5	2.9	24	3.0	17.5	3.7	9	2.5	–	–	–	·	7	26	·	·	·	–	–	–	–	–	3	–	·
IV	5	2.5	1	2.0	6	2.5	8	2.5	9.5	4.9	13.5	2.7	24.5	3.4	18.5	3.5	4	3.1	38	11.1	26	·	·	1	6	1	·	–	–	13	10	1	·	–	2
V	1	2.0	·	·	4	1.6	7	1.5	6	2.0	10.5	2.8	44	3.1	12.5	3.1	8	2.5	103	21.1	13	·	·	1	·	·	·	–	–	19	15	3	2	·	2
VI	2.5	2.4	·	·	0.5	3.0	5.5	2.0	6.5	2.5	4	2.5	48.5	2.9	19.5	2.9	3	2.7	18	6.2	1	·	·	·	7	·	·	–	–	6	4	·	·	·	2
VII	0.5	2.0	0.5	2.0	3	1.5	25	2.6	5.5	2.7	8.5	3.3	46	2.7	12.5	2.6	14	2.2	99	49.6	16	·	·	·	5	·	·	–	–	14	11	2	1	·	6
VIII		·	·	·	·	·	3.5	1.7	8.5	2.6	10.5	2.6	48.5	2.9	14	3.1	8	2.5	26	8.3	14	·	·	·	8	·	·	–	–	11	7	·	2	·	3
IX	0.5	1.0	·	·	6.5	2.0	9	1.8	8	2.4	13	3.5	35	3.2	12	2.5	6	2.6	41	12.9	17		·	·	6	·	·	–	–	9	7	2	8	·	1
X	·	·	1	1.0	6	1.6	11.5	2.0	10.5	1.8	1.5	4.0	34	2.6	11.5	2.4	17	1.9	35	19.4	31	·	·	1	·	·	·	–	–	10	6	1	10	·	·
XI	·	·	3.5	1.3	7	1.4	14	2.2	7.5	3.3	5.5	2.4	29.5	3.2	9	2.4	14	2.2	54	15.6	1	·	1	8	·	1	·	–	–	11	10	1	6	–	·
XII	3	1.0	3	1.0	6	1.8	10.5	1.9	5.5	3.3	7	6.4	31.5	3.2	14.5	2.5	12	2.5	19	6.2	17	10	14	25	·		·	–	–	12	6	·	22	–	·
Rok	24.5	1.6	18	1.0	50.5	1.7	102.5	2.2	83.5	2.9	111	3.4	429.5	3.3	165.5	3.1	110	2.7	–	49.6	16. VII	14	37	101	32	7	1?	–	–	–	–	–	58	–	16

Olesno $H_s = 238\ m$ $h_w = 13\ m$

I	4.5	4.9	3	3.0	3.5	2.3	0.5	1.0	15.5	4.1	39.5	3.3	13.5	4.1	10	4.8	3	3.6	42	6.7	25	2	7	28	·	1	·	1	13	13	11	·	1	–	·
II	7.5	5.3	5.5	2.1	10	2.2	2	2.5	10.5	2.8	14.5	3.8	14	6.1	16	7.4	4	4.4	39	7.8	16	5	10	28	·	3	1	1	17	16	11	·	3	–	·
III	12	4.7	12.5	2.1	10.5	2.0	12	2.0	9.5	1.8	11.5	2.5	8.5	4.2	10.5	5.3	6	2.9	56	16.1	31	·	8	27	·	2	·	1	17	14	8	3	8	–	·
IV	9.5	2.8	9	2.4	2.5	3.4	8	2.0	11.5	3.0	16	3.0	11.5	3.5	11	4.6	11	2.7	54	16.7	26	·	·	1	7	1	·	3	12	14	10	1	2	·	1
V	2.5	1.8	2.5	1.6	3.5	1.7	6.5	1.8	6	1.7	20	2.3	19.5	4.5	19.5	4.4	13	2.8	119	21.7	14	·	·	2	·	3	·	1	8	29	23	4	3	·	3
VI	12	3.3	2.5	2.0	2.5	1.6	3.5	1.6	4	1.2	8	2.0	25	3.0	24.5	3.3	8	2.6	27	8.5	1	·	·	·	6	·	·	1	11	10	5	·	·	·	2
VII	10	2.2	2.5	1.4	3	1.3	4.5	1.4	6.5	1.7	18.5	2.2	21	2.5	16	2.6	11	2.0	61	11.4	27	·	·	·	5	·	·	3	12	13	10	2	2	·	8
VIII	1	5.5	1	1.0	2	1.2	8.5	1.4	9	1.8	21	2.3	24	3.7	16.5	4.3	10	2.6	36	9.2	7	·	·	·	9	·	·	3	10	11	8	·	6	·	6
IX	5.5	3.0	1.5	1.7	6.5	1.8	10.5	1.6	9	2.0	19.5	2.7	18	3.6	11.5	3.5	8	2.5	73	23.2	18	·	·	·	7	·	·	6	7	12	7	2	7	·	1
X	5.5	1.8	3	2.2	10	1.3	17.5	1.5	9	1.7	10	2.0	6.5	2.8	18.5	2.8	13	1.7	18	5.3	31	·	·	9	·	·	·	9	10	8	6	·	15	·	·
XI	9	1.4	5	2.4	13.5	2.4	17.5	2.0	10.5	2.3	11.5	2.5	9.5	3.3	6.5	2.5	7	2.1	60	13.6	20	·	1	12	·	·	·	1	20	16	9	2	10	·	·
XII	5	2.3	12.5	2.0	9	2.3	9	1.9	9	3.6	22	3.7	13	2.6	9.5	2.2	4	2.6	36	11.5	15	9	17	31	·	1	·	3	18	16	9	1	8	–	·
Rok	84	3.2	60.5	2.0	76.5	2.0	100	1.7	110	2.3	212	2.7	184	3.7	170	4.0	98	2.7	621	23.2	18. IX	16	43	138	34	11	1	33	155	172	117	15	65	–	21

Cieplice Śl.-Zdrój $\varphi = 50°52'$ $\lambda = 15°41'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.8	-3.3	10.4	22	-20.9	31	-0.8	2.3	0.3	0.5	–	–	–	–	–	–	–	–	–	–	–	–	76	70	81	76
II	–	–	–	–	1.2	-6.5	6.2	7, 12	-22.0	1	-3.3	-0.4	-2.2	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	84	89	81	85
III	–	–	–	–	3.0	-5.6	12.9	31	-14.1	15	-3.5	1.5	-1.3	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	77	81	77	78
IV	–	–	–	–	14.1	2.9	26.6	23	-4.0	11	6.4	12.4	7.6	8.5	–	–	–	–	–	–	–	–	–	–	–	–	64	79	63	69
V	–	–	–	–	14.1	4.5	22.3	8	-3.2	6	8.3	12.5	9.0	9.7	–	–	–	–	–	–	–	–	–	–	–	–	85	92	86	88
VI	–	–	–	–	19.0	6.7	30.3	16	-0.8	8	11.7	17.3	12.4	13.4	–	–	–	–	–	–	–	–	–	–	–	–	57	77	65	66
VII	–	–	–	–	20.0	8.6	31.6	26	4.4	9, 30	12.6	18.1	12.8	14.1	–	–	–	–	–	–	–	–	–	–	–	–	62	81	73	72
VIII	–	–	–	–	21.5	9.5	30.2	13	3.7	10	13.8	19.7	13.5	15.1	–	–	–	–	–	–	–	–	–	–	–	–	70	82	67	73
IX	–	–	–	–	18.0	4.6	29.5	4	-2.3	15	8.6	16.2	10.4	11.4	–	–	–	–	–	–	–	–	–	–	–	–	63	74	61	66
X	–	–	–	–	14.5	1.3	24.6	3, 4	-5.9	24	3.0	13.1	6.3	7.2	–	–	–	–	–	–	–	–	–	–	–	–	57	49	47	51
XI	–	–	–	–	6.3	-0.3	18.1	8	-6.9	24	2.1	5.2	2.9	3.3	–	–	–	–	–	–	–	–	–	–	–	–	82	85	80	82
XII	–	–	–	–	-2.4	-10.4	8.8	9	-23.5	22	-7.4	-3.9	-6.9	-6.3	–	–	–	–	–	–	–	–	–	–	–	–	89	77	74	80
Rok	–	–	–	–	11.1	1.0	31.6	26.VII	-23.5	22.XII	4.3	9.5	5.4	6.2	–	–	–	–	–	–	–	–	–	–	–	–	72	78	71	74

Słupia Nowa $\varphi = 50°52'$ $\lambda = 21°05'$

I	–	–	–	–	1.2	-3.6	5.9	1	-19.4	31	-2.1	-0.1	-1.2	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	80	6.6	70	72
II	–	–	–	–	-0.5	-6.0	4.8	13	-15.8	1	-4.4	-2.0	-3.1	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	91	89	83	88
III	–	–	–	–	1.0	-5.4	12.2	31	-13.5	21	-4.1	-0.2	-2.4	-2.3	–	–	–	–	–	–	–	–	–	–	–	–	75	71	71	72
IV	–	–	–	–	15.2	6.0	25.9	23	0.1	2	8.6	13.8	9.6	10.4	–	–	–	–	–	–	–	–	–	–	–	–	67	68	50	62
V	–	–	–	–	14.4	6.8	22.3	8	-2.2	1	9.4	12.9	9.8	10.5	–	–	–	–	–	–	–	–	–	–	–	–	85	83	62	77
VI	–	–	–	–	18.0	9.6	28.9	23	2.6	7	13.1	16.2	12.9	13.8	–	–	–	–	–	–	–	–	–	–	–	–	54	65	59	59
VII	–	–	–	–	20.5	10.6	28.1	22	5.7	5	14.2	18.9	14.2	15.4	–	–	–	–	–	–	–	–	–	–	–	–	53	62	55	57
VIII	–	–	–	–	21.8	13.1	29.4	13	8.7	10	15.5	20.2	16.0	16.9	–	–	–	–	–	–	–	–	–	–	–	–	52	61	46	53
IX	–	–	–	–	17.2	8.3	26.4	4	2.1	25	10.4	15.5	11.9	12.4	–	–	–	–	–	–	–	–	–	–	–	–	66	63	48	59
X	–	–	–	–	12.7	3.8	19.3	2	-1.7	16	5.6	11.7	7.3	8.0	–	–	–	–	–	–	–	–	–	–	–	–	64	42	39	48
XI	–	–	–	–	6.0	1.5	13.8	1	-2.4	18	2.6	5.0	3.5	3.6	–	–	–	–	–	–	–	–	–	–	–	–	90	88	85	88
XII	–	–	–	–	-2.5	-7.9	4.0	4	-20.2	22	-6.1	-3.9	-5.6	-5.3	–	–	–	–	–	–	–	–	–	–	–	–	89	75	76	80
Rok	–	–	–	–	10.4	3.1	29.4	13.VIII	-20.2	22.XII	5.2	9.0	6.1	6.6	–	–	–	–	–	–	–	–	–	–	–	–	72	6.9	[illegible]	3

Świdnica $\varphi = 50°51'$ $\lambda = 16°29'$

I	–	–	–	–	3.6	-1.4	10.3	22	-16.2	31	0.7	2.2	0.7	1.1	–	–	–	–	–	–	–	–	–	–	–	–	83	6.8	7.8	7.6
II	–	–	–	–	1.8	-3.7	7.6	12	-16.8	1	-1.6	0.2	-0.7	-0.7	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.5	8.1	8.7
III	–	–	–	–	3.3	-3.7	13.9	31	-8.8	9	-1.4	1.9	-0.5	-0.1	–	–	–	–	–	–	–	–	–	–	–	–	77	77	73	76
IV	–	–	–	–	15.3	5.4	27.4	24	-0.9	11	8.3	13.5	9.2	10.0	–	–	–	–	–	–	–	–	–	–	–	–	67	71	68	69
V	–	–	–	–	15.3	6.6	23.3	8	-0.8	1	10.1	13.4	10.1	10.9	–	–	–	–	–	–	–	–	–	–	–	–	71	77	85	78
VI	–	–	–	–	19.9	9.9	29.7	24	1.8	6	13.8	18.4	14.0	15.0	–	–	–	–	–	–	–	–	–	–	–	–	54	63	55	57
VII	–	–	–	–	20.9	10.7	31.9	26	5.4	9	15.1	19.6	14.1	15.7	–	–	–	–	–	–	–	–	–	–	–	–	57	65	62	61
VIII	–	–	–	–	22.9	12.4	31.3	13	6.5	10	16.4	21.3	15.7	17.3	–	–	–	–	–	–	–	–	–	–	–	–	56	65	49	57
IX	–	–	–	–	18.6	8.4	30.8	4	3.3	15	11.3	17.0	12.0	13.1	–	–	–	–	–	–	–	–	–	–	–	–	67	61	41	56
X	–	–	–	–	13.9	4.9	25.3	3	-2.6	22	6.7	12.7	8.3	9.0	–	–	–	–	–	–	–	–	–	–	–	–	62	52	53	56
XI	–	–	–	–	6.6	1.9	17.9	8	-2.4	24	3.3	5.8	4.1	4.3	–	–	–	–	–	–	–	–	–	–	–	–	83	78	75	79
XII	–	–	–	–	-0.6	-6.8	7.3	7	-20.8	24	-4.8	-2.3	-4.1	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	80	70	74	75
Rok	–	–	–	–	11.8	3.7	31.9	26.VII	-20.8	24.XII	6.5	10.3	6.9	7.6	–	–	–	–	–	–	–	–	–	–	–	–	71	6.9	6.6	6.9

Kielce $\varphi = 50°51'$ $\lambda = 20°37'$

I	983.7	1002.6	960.7	1017.6	1.4	-4.2	7.0	20	-17.0	31	-2.1	0.3	-1.6	-1.3	4.9	5.2	5.0	5.0	9.0	8.1	8.8	8.6	0.5	1.3	0.7	0.8	8.0	7.3	7.2	7.5
II	982.3	999.8	954.2	1016.3	-0.1	-5.5	4.9	13	-14.8	3	-4.2	-1.4	-2.6	-2.7	4.1	4.5	4.7	4.4	8.9	8.1	9.0	8.7	0.5	1.1	0.5	0.7	9.1	8.9	8.3	8.8
III	977.7	994.5	958.7	1011.4	1.8	-6.5	13.8	31	-17.9	19	-4.7	0.6	-2.5	-2.3	4.2	4.8	4.7	4.6	9.0	7.2	8.7	8.3	0.4	1.9	0.6	1.0	8.1	7.9	7.8	7.9
IV	981.5	994.8	957.0	1013.6	16.0	4.7	26.8	23	-0.9	8	7.8	14.3	9.0	10.0	8.9	8.5	9.2	8.9	8.3	5.6	7.9	7.3	2.1	9.5	2.8	4.8	7.1	7.4	5.6	6.7
V	980.9	987.6	966.2	1013.3	15.0	6.2	23.5	8	-2.7	1	9.0	13.1	9.6	10.3	10.6	10.5	10.8	10.6	8.9	7.0	8.9	8.3	1.2	5.2	1.5	2.6	7.9	8.5	7.4	7.9
VI	985.8	994.8	972.0	1018.0	19.1	8.2	29.9	23	2.4	8	12.9	17.2	12.4	13.7	11.8	11.1	12.0	11.6	7.8	5.7	8.2	7.2	3.8	10.0	2.9	5.6	6.0	6.9	5.9	6.3
VII	982.9	993.3	970.4	1014.7	21.0	9.9	29.2	26	5.3	10	13.5	19.2	14.0	15.2	13.6	13.7	14.0	13.8	8.7	6.2	8.6	7.8	2.1	9.1	2.4	4.5	6.6	7.4	5.7	6.6
VIII	984.3	992.0	974.6	1016.1	22.4	10.9	30.7	7	5.1	31	14.5	20.5	15.2	16.4	14.6	15.1	15.3	15.0	8.7	6.4	8.7	7.9	2.1	9.6	2.3	4.7	6.5	7.3	6.9	6.9
IX	984.6	997.2	970.2	1016.8	17.5	6.6	27.4	4	0.0	15	9.4	15.8	11.0	11.8	10.8	11.6	11.5	11.3	9.0	6.6	8.6	8.1	1.3	7.2	2.1	3.5	6.9	7.1	4.4	6.1
X	990.0	1003.1	977.3	1023.0	13.3	2.3	19.9	2	-5.3	16	3.9	12.3	5.8	7.0	8.1	9.7	8.8	8.9	9.6	6.7	9.3	8.5	0.3	4.9	0.8	2.0	6.1	4.5	4.5	5.0
XI	984.3	998.6	969.5	1017.5	6.5	1.8	14.7	8	-2.0	17	2.9	5.6	3.6	3.9	7.3	7.8	7.3	7.5	9.4	8.4	9.1	9.0	0.5	1.8	0.7	1.0	8.8	8.7	8.3	8.6
XII	983.4	1010.6	946.0	1017.8	-2.5	-8.6	3.6	12	-24.5	22	-5.8	-3.6	-5.8	-5.2	3.9	4.2	3.9	4.0	9.0	8.4	8.8	8.7	0.4	0.8	0.5	0.6	8.5	8.0	6.8	7.8
Rok	983.4	1010.6	946.0	1016.4	11.0	2.2	30.7	7.VIII	-24.5	22.XII	4.8	9.5	5.7	6.4	8.6	8.9	8.9	8.8	8.9	7.0	8.7	8.2	1.3	5.3	1.5	2.7	7.5	7.5	6.6	7.2

Cieplice Śl.-Zdrój $H_s = 345 m$ $h_w = 13,6$ 1962

Miesiąc	Rozkład wiatru °D, °mD: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R: Suma	Max	Data	Liczba dni (n) – Temperatura T: Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v: ≥ 10	> 15	◷	●	Opad R: ≥ 0.1	≥ 1.0	≥ 10.0	═	⊠	R/K
I	4	1.2	1.5	1.3	3.5	1.1	6	20	5	70	20	8.2	16	4.1	14	8.0	23	4.3	29	8.3	26	5	5	16	·	9	5	2	17	12	8	·	3	16	·
II	3	3.7	7	2.1	9	2.2	2.5	1.4	1.5	1.7	10	9.1	17.5	9.5	13.5	8.1	20	5.0	40	11.5	12	5	10	26	·	7	6	1	20	16	12	1	4	23	·
III	2.5	2.8	5	4.6	6.5	3.5	5	7.6	·	·	3.5	7.8	13	4.4	17.5	4.4	40	2.7	39	11.8	31	6	8	28	·	7	1	2	21	13	5	2	3	15	·
IV	3	2.7	7.5	4.8	7	3.1	7	10.1	8.5	4.9	7	4.8	14	4.2	14	5.6	22	3.9	50	16.7	28	·	·	5	4	5	2	1	13	17	12	1	3	·	1
V	2.5	2.4	2.5	1.0	8	3.6	3.5	2.4	3	3.0	19.5	3.3	12.5	4.4	15.5	5.2	26	2.7	97	27.8	14	·	·	4	·	2	·	·	25	17	14	2	2	1	3
VI	9	3.7	6	3.2	2.5	1.8	9	1.8	5.5	2.0	4.5	3.0	14	4.8	19.5	6.6	20	3.3	65	40.4	16	·	·	1	7	3	1	1	14	10	7	1	–	·	2
VII	3	2.8	4	2.4	6	1.5	8.5	1.2	6.5	1.8	6	4.7	14	4.4	17	5.0	28	2.4	87	32.1	15	·	·	·	5	1	·	2	15	14	12	2	–	·	5
VIII	7	2.3	1	2.0	4	1.2	8	1.9	2	3.0	16	6.9	11	5.0	13	5.2	31	3.0	64	13.5	14	·	·	·	4	4	·	1	13	14	12	3	2	·	4
IX	2	1.0	6	2.8	4	2.5	6.5	4.8	1.5	2.0	14.5	7.1	14.5	4.0	12	4.2	29	3.0	71	31.5	16	·	·	2	4	3	2	4	12	11	6	2	3	·	1
X	3	2.7	5.5	3.7	8.5	2.6	7.5	2.1	7	2.3	2	2.0	2.5	4.0	11	4.5	46	1.6	38	18.3	31	·	·	12	·	·	·	12	11	8	6	1	7	·	·
XI	2	1.0	7	2.3	12	2.5	18	9.6	6	4.9	2	3.5	9	3.8	4	5.0	30	3.5	31	10.4	1	·	1	15	·	4	3	·	19	12	8	1	4	4	·
XII	5	2.2	8.5	2.3	6	2.6	4	4.5	8	5.8	8	10.4	4	8.8	7.5	5.2	42	2.9	31	8.8	16	17	20	26	·	5	3	2	20	15	6	·	3	25	·
Rok	46	2.4	61.5	2.7	77	2.4	85.5	4.1	54.5	3.2	113	5.9	142	5.1	158.5	5.6	357	3.2	642	40.4	16.VI	33	44	135	24	50	23	28	200	159	108	16	–	84	16

Słupia Nowa $H_s = 307 m$ $h_w = 15 m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◷	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R/K
I	6.5	4.7	1	3.0	·	·	0.5	6.0	9.5	6.3	34	5.3	21	4.5	13.5	3.7	7	4.5	60	16.4	13	2	8	23	·	3	·	2	12	13	7	3	4	8	·
II	12.5	4.4	2.5	2.4	4.5	2.6	4	4.0	8	3.6	17.5	6.0	7.5	4.3	21.5	5.2	6	4.4	53	15.5	12	5	14	26	·	4	1	·	22	19	10	1	4	28	1
III	18	5.8	3	2.0	0.5	4.0	3.5	3.1	18.5	4.6	11.5	4.7	5	3.2	16	4.3	17	3.7	38	7.1	5	6	17	26	·	2	·	2	17	20	10	·	4	23	·
IV	6	4.1	1	2.0	1.5	2.0	7.5	7.2	19	4.0	10	4.4	7.5	3.4	22.5	3.6	15	3.4	44	10.5	13	·	·	·	4	2	·	5	11	15	12	1	2	·	4
V	9.5	2.9	·	·	2.5	1.6	7	3.7	11.5	2.6	19	3.1	9	3.5	20.5	3.4	14	2.7	130	22.5	14	·	·	1	·	1	1	1	14	27	22	3	4	·	4
VI	20	4.3	1.5	2.7	·	·	2	1.5	3.5	2.4	12	2.6	11.5	2.7	30.5	2.9	9	2.8	99	38.8	4	·	·	·	4	·	·	3	10	14	8	3	1	·	2
VII	6.5	2.3	2	1.0	·	·	1	1.0	6	2.7	14	2.8	27.5	2.4	23	2.6	13	2.1	81	16.8	19	·	·	·	4	·	·	2	6	17	11	3	1	·	6
VIII	2	1.5	·	·	1.5	1.7	2.5	3.4	15.5	2.1	23	3.7	17.5	2.4	17	3.2	14	2.5	37	11.0	3	·	·	·	5	·	·	6	6	13	9	1	3	·	5
IX	2.5	2.4	2	1.8	1.5	1.7	·	·	9	3.1	19	4.0	17	3.5	12	3.4	27	2.4	93	34.9	18	·	·	·	2	·	·	6	9	14	11	2	5	·	·
X	8.5	2.1	0.5	2.0	4	1.9	6.5	2.1	13	3.2	16.5	3.7	6.5	2.4	12.5	2.4	25	2.0	1	0.5	19	·	·	5	·	1	·	6	6	2	·	·	10	·	·
XI	3.5	2.9	2	2.5	11.5	2.9	16.5	3.6	13.5	2.8	8.5	3.2	9.5	3.1	18	2.8	7	2.8	46	9.1	15	·	1	12	·	·	·	·	23	20	13	·	14	4	·
XII	20	2.5	3	2.5	4	1.8	1	1.0	7.5	4.1	12.5	5.5	11	2.9	10	2.7	24	2.4	24	5.9	13	11	16	31	·	·	·	1	17	15	7	·	5	18	·
Rok	115.5	3.3	18.5	1.8	31.5	1.7	52	3.0	134.5	3.5	197.5	4.1	150.5	3.2	217	3.4	178	3.0	706	38.8	4.VI	24	56	124	19	13	2	34	153	189	120	17	57	81	22

Świdnica $H_s = 230 m$ $h_w = 14 m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◷	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R/K
I	5.5	2.5	·	·	·	·	3.5	3.6	9	5.5	43.5	5.9	12	5.6	12.5	5.0	7	5.0	23	7.7	26	2	4	15	·	7	3	·	13	12	6	·	1	–	·
II	7.5	2.8	2.5	2.2	2.5	2.2	7	2.4	3.5	4.9	19	7.1	22.5	7.7	15.5	5.9	4	5.5	30	5.5	27	1	10	23	·	5	5	·	18	21	10	·	4	–	·
III	12	3.5	9	2.9	5	1.0	10	4.2	5.5	2.6	14.5	4.2	7.5	5.5	11.5	4.7	18	3.1	55	19.5	31	·	8	26	·	2	1	1	15	14	7	2	2	–	·
IV	8.5	2.1	5.5	2.3	3.5	4.4	8	3.9	5.5	4.3	18.5	5.8	13.5	4.9	10	3.8	17	3.5	48	15.2	26	·	·	1	5	4	2	2	14	12	8	1	2	–	2
V	9	2.7	·	·	2.5	1.8	4	1.9	5.5	2.7	22	3.1	22.5	3.8	13.5	3.4	14	2.7	97	19.4	14	·	·	1	·	1	·	·	18	16	14	3	·	·	1
VI	7	3.6	1.5	3.3	2.5	2.0	6	1.7	6	1.7	13.5	3.7	28	3.1	16.5	3.7	9	2.8	26	14.2	19	·	·	·	7	·	·	4	8	6	4	1	·	·	1
VII	6.5	3.0	4	2.1	2	2.2	2	1.0	4.5	2.8	18.5	4.2	22	2.5	10.5	3.0	23	2.2	79	32.9	16	·	·	·	5	1	1	·	11	16	12	2	1	·	7
VIII	0.5	2.0	3	1.7	·	·	3.5	1.3	5.5	1.9	31.5	2.9	20.5	3.4	3.5	3.1	25	2.1	43	19.1	14	·	·	·	8	·	·	2	8	16	8	1	·	·	3
IX	1	2.0	0.5	2.0	1.5	2.0	11.5	3.0	4	2.6	18	5.0	20	3.9	13.5	3.1	20	2.9	47	14.4	18	·	·	·	5	2	·	6	6	9	8	2	6	·	·
X	6	1.8	4	2.1	1	3.0	14	1.3	9.5	2.3	13.5	3.7	10.5	3.2	11.5	4.4	23	2.1	37	18.3	31	·	·	4	1	·	·	7	9	13	7	1	8	·	·
XI	0.5	2.0	7.5	1.7	3.5	2.9	14.5	3.6	11	4.3	16.5	2.8	9	3.4	10.5	2.1	17	2.5	51	14.8	1	·	1	6	·	1	·	2	20	14	11	1	3	–	·
XII	11.5	2.2	1.5	3.0	6	1.3	2	1.0	7.5	4.1	19	5.4	9.5	3.7	7	3.6	29	2.5	16?	–	–	10	14	25	·	3	·	2	18	12	5	·	·	–	·
Rok	75.5	2.5	39	1.9	30	1.9	86	2.4	77	3.3	248	4.5	192.5	4.2	136	3.8	206	3.1	552?	32.9	16.VII	13	37	101	31	26	12	26	158	161	100	14	27	–	14

Kielce $H_s = 268 m$ $H_b = 270,1 m$ $h_w = 21,1 m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◷	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R/K
I	2	5.0	3.5	3.9	2.5	3.0	0.5	4.0	25	3.8	34	3.6	17	4.1	5.5	4.4	3	3.7	43	8.6	25	3	9	23	·	·	·	·	16	17	12	·	·	27	·
II	6	3.2	2.5	2.6	8.5	3.4	9	3.3	12.5	3.7	12.5	4.9	19	5.4	10	6.0	4	4.2	62	12.8	12	4	14	26	·	1	1	·	23	21	10	2	·	28	1
III	3	5.0	4.5	4.7	11	2.9	13.5	3.4	19	3.2	4.5	3.1	11	5.4	17.5	3.1	9	3.2	67	16.1	16	8	10	26	·	1	·	3	22	17	12	3	1	28	·
IV	2.5	2.0	7.5	3.1	8.5	3.0	8	6.4	14	4.0	13.5	3.0	14	3.0	9	4.3	13	3.2	60	10.2	6	·	·	3	4	1	·	2	11	17	11	1	·	·	2
V	·	·	·	·	5	2.3	11	2.7	14.5	2.8	22	2.2	21	3.8	11.5	2.8	8	2.6	169	25.6	8	·	·	2	·	2	·	·	17	26	24	5	2	·	5
VI	7	3.6	5	3.0	·	·	1	1.5	5.5	2.5	12	3.1	35.5	2.6	15	3.6	9	2.6	79	36.4	4	·	·	·	6	·	·	4	11	11	8	3	·	·	1
VII	4	2.2	3	3.0	2.5	2.4	2.5	2.0	4.5	2.6	23	2.6	33	2.8	8.5	2.4	12	2.3	91	27.0	22	·	·	·	5	1	·	2	11	16	12	3	1	·	5
VIII	0.5	4.0	0.5	4.0	1	1.0	5	3.5	10	3.2	21	2.9	40	3.3	2	1.8	13	2.7	59	15.9	4	·	·	·	9	·	·	·	13	17	10	1	4	·	5
IX	0.5	3.0	2.5	2.8	6.5	2.0	10.5	2.6	9	3.5	22.5	3.5	24	2.8	1.5	3.3	13	2.6	50	14.0	18	·	·	·	3	·	·	4	10	12	8	2	4	·	·
X	1.5	3.3	4	2.5	7.5	2.3	14	2.6	7.5	2.4	8.5	3.5	15	2.8	1	4.0	34	1.7	5	2.0	19, 28	·	·	10	·	·	·	7	8	5	2	·	15	·	·
XI	3	2.0	4	3.4	15.5	3.7	23.5	3.4	3.5	3.9	11	2.4	12.5	2.4	4	2.5	13	2.6	45	12.3	15	·	·	8	·	·	·	·	20	18	10	1	6	2	·
XII	3	4.0	8.5	3.5	6	2.4	4	4.1	14	3.3	13	4.3	15.5	2.4	7	2.6	22	2.5	40	9.4	13	13	15	31	·	·	·	1	17	16	6	·	3	18	·
Rok	33	3.1	45.5	3.0	74.5	2.4	102.5	3.3	139	3.2	197.5	3.3	257.5	3.4	92.5	3.4	153	2.8	770	36.4	4.VI	28	48	129	27	6	1	23	179	193	125	21	36	103	19

Święty Krzyż $\varphi = 50°51'$ $\lambda = 21°03'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.9	-5.2	3.4	20	-17.4	30	-3.6	-2.3	-3.4	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.5	6.9	7.7
II	–	–	–	–	-2.6	-7.1	2.4	13	-14.1	1	-6.1	-4.2	-4.7	-4.9	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.8	8.1	8.6
III	–	–	–	–	-1.0	-6.2	9.8	31	-10.6	17	-5.2	-2.3	-4.1	-3.9	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.2	7.1	7.3
IV	–	–	–	–	13.1	5.4	24.9	22	-1.7	8	6.9	11.3	8.2	8.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.7	6.1	6.5
V	–	–	–	–	12.5	5.7	20.8	8	-3.6	1	7.3	10.7	8.2	8.6	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.3	7.5	7.9
VI	–	–	–	–	15.8	8.8	26.5	23	0.9	7	11.1	14.2	11.5	12.1	–	–	–	–	–	–	–	–	–	–	–	–	5.4	7.1	7.4	6.6
VII	–	–	–	–	18.3	10.3	25.9	22, 26	5.3	5	12.4	16.8	13.0	13.8	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.9	6.5	6.6
VIII	–	–	–	–	19.8	12.2	27.7	13	6.9	31	13.5	18.2	15.0	15.4	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.7	4.8	5.9
IX	–	–	–	–	15.1	7.1	24.7	4	1.6	22	8.6	13.1	10.3	10.6	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.5	3.5	5.0
X	–	–	–	–	11.0	4.6	16.9	4	0.1	21	5.9	9.8	6.6	7.2	–	–	–	–	–	–	–	–	–	–	–	–	4.0	3.3	2.4	3.2
XI	–	–	–	–	4.4	-0.1	11.8	8	-6.6	24	1.5	3.1	1.7	2.0	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.8	7.5	8.0
XII	–	–	–	–	-3.5	-8.4	5.1	8, 9	-19.0	26	-6.9	-5.3	-6.4	-6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.7	6.6	7.0
Rok	–	–	–	–	8.5	2.3	27.7	13.VIII	-19.0	26.XII	3.8	6.9	4.7	5.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.9	6.2	6.7

Strzyżów $\varphi = 50°51'$ $\lambda = 24°02'$

I	–	–	–	–	1.4	-3.9	7.9	22	-17.3	31	-1.9	0.3	-1.7	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	-1.0	-7.1	2.6	13	-13.6	1	-4.6	-2.1	-4.0	-3.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	0.5	-6.6	10.1	5	-20.0	21	-4.7	-0.5	-3.4	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	16.3	5.4	26.5	21, 24	-1.4	2	7.3	14.9	9.9	10.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	17.3	7.2	25.7	27	-0.9	4	10.3	15.5	11.2	12.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	19.7	9.6	28.7	20	3.1	6	13.6	18.3	13.6	14.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.3	10.4	28.3	27	6.2	2, 3	14.8	19.8	14.3	15.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	22.9	11.9	31.0	13	5.4	27	15.1	21.4	16.1	17.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	18.2	7.5	29.3	5	1.7	25	10.0	17.0	11.3	12.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	13.8	2.0	20.1	2	-4.6	17	3.9	13.0	6.2	7.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	7.8	2.2	19.1	1	-3.7	18	3.4	6.6	4.3	4.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-2.3	-8.0	3.4	11	-20.0	21	-5.5	-3.5	-5.6	-5.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	11.3	2.6	31.0	13.VIII	-20.0	21.III, 21.XII	5.1	10.1	6.0	6.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Szklarska Poręba $\varphi = 50°50'$ $\lambda = 15°32'$

I	–	–	–	–	2.1	-3.5	8.7	1	-19.8	31	-1.6	0.1	-0.9	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.2	7.3	8.0
II	–	–	–	–	-0.4	-7.1	5.2	7	-18.6	1	-4.4	-2.1	-3.5	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.8	7.9	8.6
III	–	–	–	–	1.2	-7.2	9.9	11	-15.3	14	-4.8	-0.2	-3.1	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.0	7.1	7.9
IV	–	–	–	–	11.2	1.4	24.4	24	-4.2	11	5.9	10.0	5.2	6.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.7	6.6	7.2
V	–	–	–	–	11.5	3.9	19.8	19	-2.7	5	7.3	10.0	6.7	7.7	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.4	7.7	8.1
VI	–	–	–	–	16.7	6.4	27.1	16	-0.9	8	11.1	14.9	10.3	11.6	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.5	7.8	7.3
VII	–	–	–	–	17.4	7.6	28.9	26	3.7	9	12.2	15.9	11.1	12.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.8	7.9	7.5
VIII	–	–	–	–	18.9	9.4	27.3	13	3.7	31	13.6	17.3	12.3	13.9	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.9	5.4	6.6
IX	–	–	–	–	15.6	5.4	25.8	4	-0.9	25	8.9	13.8	8.6	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.2	4.5	6.0
X	–	–	–	–	12.9	2.6	22.4	3, 4	-3.3	22	4.5	11.7	5.6	6.8	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.8	4.8	4.9
XI	–	–	–	–	4.1	-0.5	15.2	7	-9.4	25	1.2	3.2	1.3	1.8	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.8	7.9	7.9
XII	–	–	–	–	-2.4	-9.8	6.1	9	-21.6	24	-6.8	-3.8	-6.8	-6.0	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.6	5.7	6.6
Rok	–	–	–	–	9.1	0.7	28.9	26.VII	-21.6	24.XII	3.9	7.6	3.9	4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.6	6.7	7.2

Lipowa $\varphi = 50°50'$ $\lambda = 21°27'$

I	–	–	–	–	1.2	-3.5	6.0	20	-19.1	31	-1.8	0.2	-1.3	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	6.2	7.8	7.5
II	–	–	–	–	-0.5	-5.2	5.0	13	-13.6	1	-3.9	-1.7	-2.3	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.6	9.4	9.1
III	–	–	–	–	1.0	-5.5	11.0	31	-16.1	27	-4.1	-0.1	-2.0	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.9	8.5	8.2
IV	–	–	–	–	16.1	5.4	26.5	23	0.3	2, 3, 8	7.5	14.5	9.7	10.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15.1	6.6	23.2	8	-2.2	1	9.1	13.4	10.1	10.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	18.6	9.0	28.0	16, 23	2.7	2	13.2	16.8	12.9	14.0	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.6	5.4	5.8
VII	–	–	–	–	21.3	10.4	28.5	26	5.1	5	14.3	19.5	14.6	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.3	6.2	6.0
VIII	–	–	–	–	22.1	11.8	30.0	13	5.2	27	14.8	20.7	16.2	17.0	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.5	6.9	6.4
IX	–	–	–	–	17.0	7.5	26.5	4, 5	1.3	25	10.2	15.7	11.2	12.1	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.5	5.8	6.0
X	–	–	–	–	12.6	2.7	18.0	4	-3.7	16	5.0	11.9	6.1	7.3	–	–	–	–	–	–	–	–	–	–	–	–	7.0	4.8	5.6	5.8
XI	–	–	–	–	6.3	1.8	14.0	1	-1.7	18	2.5	5.3	3.8	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.7	9.3	9.0
XII	–	–	–	–	-2.4	-8.7	4.0	17	-24.1	22	-5.9	-3.6	-5.4	-5.1	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.2	8.5	8.4
Rok	–	–	–	–	10.7	2.7	30.0	13.VIII	-24.1	22.XII	5.1	9.4	6.1	6.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Święty Krzyż $H_s = 575\,m$ $h_w = 24\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU (°D, °mD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Max < 10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	◐	●	Opad R ≥ 0.1	R ≥ 10	R ≥ 100	≡	⊞	R ≥ 10
I	7	6.4	6.5	11.0	2	3.0	4	8.4	21	12.6	18.5	10.6	16.5	9.6	10.5	7.4	7	9.2	17[2]	4.1	27	3	16	30	·	19	16	·	13	10	7	·	14	4	·
II	14.5	10.9	3.5	5.0	5	3.6	4.5	10.7	6	10.4	9.5	11.9	11	13.5	11	10.1	19	8.1	106[2]	17.8	16	5	23	28	·	15	10		22	21	17	3	15	28	·
III	13.5	6.4	10.5	10.7	7	11.6	4	4.2	18	6.7	9	8.7	4	5.1	5	12.2	22	6.2	–	–	–	5	21	28	·	10	8	2	16	–	–	–	15	24	·
IV	14	5.7	11	4.2	·	·	4.5	11.4	22.5	11.5	5.5	5.2	5	4.5	9.5	7.1	18	6.2	45	8.9	27	·	·	6	·	10	5	3	11	16	10	·	12	1	1
V	12.5	4.0	1.5	3.0	1	1.0	3	5.2	15.5	5.5	9.5	4.5	17.5	6.6	14.5	4.7	18	4.1	166	26.3	14	·	·	3	·	4	3	·	16	25	23	6	15	1	3
VI	19.5	8.9	5	5.6	·	·	1	3.0	10	3.8	7.5	5.3	19.5	5.1	14.5	5.0	13	5.0	126	53.0	4	·	·	·	2	5	4	·	12	13	10	3	6	·	2
VII	14.5	4.6	1	2.0	3	1.3	1.5	5.7	13	3.4	12	4.8	14.5	6.2	14.5	4.2	19	3.6	100	17.5	18	·	·	·	3	4	1	1	9	15	10	5	7	·	7
VIII	2.5	1.6	1.5	3.3	3.5	2.9	3.5	6.0	20.5	5.4	12.5	4.0	21.5	4.7	15.5	5.3	12	4.2	41	10.7	3	·	·	·	3	6	4	2	5	14	10	1	4	·	5
IX	1.5	4.7	3	2.2	4.5	3.9	6	6.1	15.5	6.2	14	8.3	13.5	4.4	18	5.2	14	4.8	67	22.4	18	·	·		·	8	3	6	6	15	10	2	9	·	·
X	11.5	5.0	3.5	2.4	2	4.0	11	5.1	13.5	5.6	6	5.8	7	6.4	12.5	4.4	26	3.7	3	1.5	19	·	·	·	·	6	3	13	2	6	1	·	13	·	·
XI	1.5	3.4	9	3.7	13.5	4.9	12.5	10.8	19.5	8.5	3	1.3	3	2.3	7.5	3.7	7	5.4	58	11.0	15	·	4	18	·	9	5	1	17	20	15	1	24	9	·
XII	9.5	3.8	3	5.0	1.4	2.2	2	4.5	20	9.9	4	6.5	11.5	6.6	16	4.5	13	5.0	42	6.7	17	11	23	31	·	8	5	3	17	18	14	·	14	25	·
Rok	135.5	5.4	5.9	4.8	55.5	3.2	57.5	6.8	195	7.5	111	6.4	144.5	6.2	149	6.2	188	5.5	–	53.0	4. VI	24	87	144	8	104	67	31	146	–	–	–	148	92	18

Strzyżów $H_s = 185\,m$ $h_w = 12{,}5\,m$

I	1	3.0	8	3.9	·	·	8	4.1	10	3.2	22	3.9	29	3.2	7	2.6	8	3.2	18	3.6	25	2	7	28	·	1	·	–	–	10	6	·	2	–	–
II	4	3.2	9	4.0	8	3.9	12	4.1	5	5.2	11	9.7	9	5.1	20	6.0	6	5.1	40	8.1	13	8	16	28	·	7	2	–	–	15	12	·	4	25[2]	–
III	6	4.0	10	3.7	11	2.5	20	5.9	3	6.7	4	1.5	11	6.5	14	2.8	14	3.7	45	8.6	13	4	15	27	·	5	1	–	–	12	12	·	3	27	–
IV	7	4.0	6	3.2	19	2.9	16	5.3	6	3.2	10	3.5	6	2.5	8	6.8	12	3.4	29	8.4	7	·	·	4	5	3	·	–	–	8	7	·	4	·	–
V	8	2.1	4	2.5	7	2.6	7	3.0	2	4.0	17	3.9	18	4.9	15	3.3	15	3.0	77	14.8	11	·	·	3	1	3	2	–	–	16	11	3	4	·	–
VI	1.9	2.9	9	2.3	6	2.0	3	3.0	1	1.0	9	2.2	16	3.6	19	2.3	8	2.4	62	25.7	1	·	·	·	8	·	·	–	–	10	10	1	·	·	–
VII	1.5	2.8	4	1.2	4	1.2	3	2.3	5	1.8	11	3.1	19	2.3	21	3.1	11	2.3	67	22.7	18	·	·	·	5	·	·	–	–	10	9	3	·	·	–
VIII	8	1.6	3	1.0	7	1.9	5	3.2	11	2.4	6	3.7	29	2.7	11	3.0	13	2.2	42	9.2	20	·	·	·	11	·	·	–	–	10	10	·	3	·	–
IX	3	2.0	5	2.0	16	1.8	6	2.3	7	5.1	5	3.6	30	2.9	10	3.1	8	2.6	40	11.4	5	·	·	·	3	1	1	–	–	12	9	1	5	·	–
X	5	2.6	7	2.0	14	2.5	8	3.5	3	4.0	2	4.5	15	4.5	16	2.8	23	2.4	2	1.6	20	·	·	11	·	1	·	–	–	3	1	·	16	·	–
XI	5	3.0	1.5	5.1	18	4.4	27	5.6	·	·	4	5.2	10	2.5	5	2.4	6	4.2	45	9.0	10	·	·	7	·	7	·	–	–	11	11	·	9	·	–
XII	1.2	3.2	1.2	4.0	4	3.5	9	3.6	10	5.5	7	5.4	17	3.1	12	2.8	10	3.4	7	1.5	20	10	16	30	·	1	·	–	–	10	3	·	2	–	–
Rok	9.3	2.9	9.2	2.9	11.4	2.4	12.4	3.8	6.3	3.5	10.8	4.2	20.9	3.6	15.8	3.4	13.4	3.2	47.4	25.7	1. VI	24	54	138	33	29	6	–	–	127	101	8	5.2	–	–

Szklarska Poręba $H_s = 640\,m$ $h_w = 13\,m$

I	1	1.5	2	2.2	6.5	1.5	1.5	2.0	8.5	5.1	23.5	4.2	23	3.5	15	3.7	12	3.2	133[3]	30.5[3]	24	3	7	25	·	3	·	2	18	17	13	5	1	26[2]	·
II	2	2.0	2	2.0	4	1.2	5.5	3.0	3	4.8	9	4.8	25	3.6	15.5	4.2	18	2.9	131	37.1	12	5	14	28	·	2	·	1	22	18	14	5	·	28	1
III	5.5	2.4	4	1.1	5.5	2.0	7.5	1.5	7.5	2.9	12	3.5	7	2.2	16	2.7	28	1.7	84	22.5	30	10	14	28	·	·	·	1	16	14	4	3	–	31	·
IV	1	2.0	2.5	2.2	6	1.8	11	1.4	15	3.3	18	4.6	17	2.6	11.5	1.9	8	2.6	94	19.4	28	·	·	14	·	2	·	2	15	16	14	3	3	3	2
V	1.5	1.0	1	1.0	4.5	1.4	6.5	1.5	11.5	2.5	25	2.7	26.5	2.4	6.5	1.5	10	2.0	[illegible]	34.9	14	·	·	4	·	1	·	·	19	24	20	5	·	1	3
VI	2.5	2.8	3.5	2.0	3	1.3	10	1.2	21.5	1.7	11	2.7	16.5	2.9	15	2.9	7	2.1	48	13.5	28	·	·	2	4	·	·	1	13	12	10	1	–	·	3
VII	1.5	1.7	3	1.3	3.5	1.0	12.5	1.0	11.5	1.5	19	2.3	23.5	2.5	6.5	1.8	12	1.6	128	22.2	13	·	·	·	2	·	·	1	15	16	16	5	·	·	6
VIII	·	·	2	1.0	2	1.0	2	1.5	10.5	1.2	22	3.3	29	3.2	13.5	2.1	12	2.3	97	24.2	5	·	·	·	1	·	·	1	10	15	12	3	2	·	3
IX		·	0.5	1.0	3	1.0	7	1.1	11.5	2.6	14.5	4.0	27	2.6	10.5	1.6	16	2.1	95	21.1	16	·	·	1	1	1	·	4	10	12	8	4	·	·	·
X	2	1.5	·		1.6	1.1	14.5	1.0	14	1.1	14.5	2.2	6	1.3	7	1.3	19	1.0	38[2]	–	–	·	·	9	·	·	·	13	12	7[3]	5[3]	1[2]	–	·	·
XI	2	1.5	1	3.0	3	1.0	21	1.2	18.5	7.0	11	3.1	8.5	3.4	4	2.0	21	2.6	34	10.0	1	·	5	20	·	4	3	1	19	14	7	·	7	10[2]	·
XII	·	·	1	2.0	1	1.0	12	1.0	29	1.3	20	3.4	14	2.2	1	4.0	15	1.7	89	19.8	16	13	17	31	·	2	·	4	15	17	11	3	5	31	·
Rok	19	1.4	22.5	1.6	58	1.3	111	1.4	162	2.9	199.5	3.4	223	2.7	122	2.5	178	2.2	1116[2]	37.1	12. II	31	57	162	8	15	3	31	184	182[3]	134[3]	36[3]	–	130[2]	18

Lipowa $H_s = 245\,m$ $h_w = 16{,}5\,m$

I	1	4.0	·	·	4	6.5	·	·	3.1	5.5	14.5	4.3	21.5	3.4	14	6.1	7	4.7	19	4.6	27	2	7	24	·	–	–	1	16	11	7	·	–	15	·
II	1.2	4.8	2	2.5	11	3.1	6.5	2.6	9.5	6.8	9	6.8	18.5	7.6	10.5	9.5	5	5.5	–	–	–	2	13	27	·	–	–	·	22	–	–	–	–	23	1
III	17	4.9	4	4.0	7	2.4	13	3.6	2.4	2.9	·	·	5.5	7.3	12.5	5.4	10	3.7	–	–	–	5	13	28	·	–	–	·	21	–	–	–	–	22	·
IV	6	2.3	7	3.0	8	3.5	13	6.5	16	3.0	8	3.0	5	2.6	19	4.6	8	3.6	44	10.0	6	·	·	·	3	–	–	–	–	11	8	1	–	·	2
V	8.5	2.3	1	4.0	2	1.5	8	4.9	10	1.5	14	2.6	15	6.5	26.5	4.0	8	3.5	126	22.4	8	·	·	1	·	–	–	–	–	23	21	4	–	·	6
VI	14.5	1.7	1.5	2.0	2	2.0	·	·	5	1.2	6	2.0	19.5	3.8	22.5	3.3	19	2.2	123	41.3	4	·	·	·	6	–	–	3	9	11	8	3	–	·	3
VII	9.5	1.9	0.5	4.0	·	·	1	1.0	8	1.6	9.5	1.7	25	2.9	25.5	2.7	14	2.0	72	23.7	18	·	·	·	5	–	–	2	10	11	8	2	–	·	6
VIII	3.5	2.1	0.5	1.0	1	2.0	·	·	12.5	2.8	14	2.6	21.5	4.4	12	4.0	23	2.6	73	18.0	3	·	·	·	5	–	–	2	6	10	9	4	–	·	3
IX	3	3.7	1	2.0	5	2.0	3.5	1.4	13.5	2.8	10.5	3.9	21	2.5	14.5	3.5	18	2.3	58	18.9	18	·	·	·	2	–	–	5	8	18	8	2	–	·	·
X	3.5	1.7	9.5	2.3	3.5	1.2	13.5	1.6	7	1.6	2.5	3.2	10.5	2.1	7	3.6	3.6	1.3	2	0.7	14	·	·	9	·	–	–	5	8	9	·	·	–	·	·
XI	7.5	2.1	2	2.5	9	5.2	3.0	4.8	8.5	2.6	6	2.2	6.5	3.4	12.5	1.8	8	3.3	32[2]	5.2	12	·	1	7	·	–	–	·	23	16	13	·	–	3	·
XII	13.5	3.0	8	4.2	3	1.3	1	2.0	1.9	7.8	11.5	3.8	8	2.6	13	3.9	16	3.7	11	2.6	18	11	14	3.0	·	–	–	·	20	13	6	·	–	18	·
Rok	9.9.5	2.9	3.7	2.6	55.5	2.6	89.5	2.4	16.9	3.3	105.5	3.0	177.5	4.1	189.5	4.4	172	3.2	–	41.3	4. VI	20	48	126	21	–	–	–	–	–	–	–	–	81	21

Częstochowa $\varphi = 50°49'$ $\lambda = 19°06'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	$P_{a.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	985.0	1004.5	961.4	1017.9	2.3	−3.1	8.4	20	−17.3	31	−1.2	1.4	−1.0	−0.4	5.0	5.4	5.0	5.1	86	79	85	83	0.8	1.5	0.9	1.1	7.5	7.5	6.3	7.1
II	984.0	1001.3	954.7	1017.1	0.6	−5.2	5.7	7	−16.2	3	−3.6	−1.0	−2.0	−2.2	4.1	4.6	4.7	4.5	85	80	86	84	0.8	1.2	0.8	0.9	9.1	9.2	8.2	8.8
III	978.9	995.7	960.7	1011.4	3.2	−4.5	15.3	31	−9.6	19	−3.2	1.8	−0.9	−0.8	4.5	5.1	5.0	4.9	89	70	83	81	0.5	2.2	1.0	1.2	7.5	7.4	6.4	7.1
IV	982.6	995.2	956.5	1014.1	16.0	5.5	27.9	22, 23	−0.1	8	7.5	14.3	9.6	10.7	9.0	9.0	9.3	9.1	85	59	77	74	1.8	9.3	3.5	4.9	7.0	7.0	5.5	6.5
V	982.1	988.4	968.0	1013.6	15.7	6.6	23.2	8	−2.2	3	8.8	13.4	10.3	10.7	10.3	10.3	10.8	10.5	90	68	85	81	1.2	5.7	2.1	3.0	7.5	8.0	6.6	7.4
VI	987.4	996.8	977.3	1018.7	19.9	9.4	30.7	23	2.8	2	12.4	18.0	13.8	14.5	12.1	11.6	12.5	12.1	81	56	78	72	2.8	10.5	4.1	5.8	5.8	7.1	5.8	6.2
VII	984.2	994.1	971.6	1015.0	21.5	10.6	31.0	26	6.8	11	13.3	19.4	14.8	15.6	13.4	13.0	14.0	13.5	86	59	83	76	2.2	10.1	3.1	5.1	6.2	6.9	5.7	6.3
VIII	985.6	993.2	973.3	1016.5	23.1	12.2	31.3	7	6.9	31	14.4	21.3	15.8	16.8	14.6	14.8	15.4	14.9	88	59	85	77	1.9	11.4	2.7	5.3	6.4	6.7	4.5	5.9
IX	985.9	993.7	971.4	1017.3	17.8	7.6	28.7	4	2.2	15	9.3	15.9	10.9	11.8	10.9	11.6	11.5	11.3	92	65	87	81	1.1	7.3	1.9	3.4	7.2	6.8	3.8	5.9
X	991.0	1004.0	977.4	1023.0	14.1	3.8	23.6	1	−3.2	22	5.1	12.7	7.1	8.0	8.8	10.2	9.5	9.5	97	70	91	86	0.3	4.9	0.9	2.0	6.8	4.9	4.1	5.3
XI	985.0	1000.3	968.6	1017.3	6.7	1.8	18.3	8	−2.2	24	2.9	5.8	3.7	4.0	7.1	7.9	7.4	7.5	93	84	92	90	0.6	1.8	0.7	1.0	8.8	8.5	8.8	8.7
XII	984.5	1012.1	942.3	1017.8	−1.4	−6.9	8.0	13	−18.6	22	−5.5	−2.9	−4.6	−4.4	3.8	4.3	4.0	4.0	87	82	87	85	0.5	1.0	0.6	0.7	8.5	7.6	7.9	8.0
Rok	984.7	1012.1	942.3	1016.7	11.6	3.2	31.3	7.VIII	−18.6	22.XII	5.0	10.0	6.5	7.0	8.6	9.0	9.1	8.9	88	69	85	81	1.2	5.6	1.9	2.9	7.4	7.3	6.1	6.9

Szrenica $\varphi = 50°48'$ $\lambda = 15°31'$

I	857.6	870.6	837.4	–	−2.7	−7.4	5.0	5	−18.6	30	−5.2	−4.3	−5.2	−5.0	3.9	4.0	3.9	3.9	92	90	92	91	0.4	0.6	0.4	0.5	9.1	9.0	8.5	8.9
II	860.0	871.7	832.1	–	−5.4	−10.2	−0.6	7	−15.8	25	−8.4	−6.9	−7.8	−7.7	3.1	3.6	3.3	3.3	94	95	93	94	0.2	0.2	0.2	0.2	9.2	9.1	8.8	9.0
III	851.8	866.9	837.1	–	−4.2	−9.6	5.6	5	−16.2	14	−8.1	−5.7	−7.3	−7.1	3.2	3.8	3.3	3.4	91	89	88	89	0.3	0.4	0.4	0.4	9.1	8.9	8.6	8.9
IV	859.1	874.4	835.4	–	4.5	−0.1	17.1	24	−7.0	7	1.6	3.4	1.8	2.2	5.3	5.8	5.8	5.6	80	78	85	81	2.3	2.9	1.7	2.3	7.8	8.4	8.0	8.1
V	859.4	865.3	848.3	–	5.5	0.1	14.1	19	−8.7	1	1.6	4.0	2.3	2.6	6.5	7.1	7.0	6.9	94	87	9.5	9.2	0.5	1.3	0.4	0.7	9.2	9.1	8.3	8.9
VI	866.3	874.1	857.0	–	10.6	3.6	21.5	16	−4.7	6	5.7	8.7	6.4	6.8	8.2	8.6	8.6	8.5	8.6	7.5	8.6	8.2	1.7	3.7	1.6	2.3	7.0	7.9	6.9	7.3
VII	863.6	872.4	846.0	–	11.2	5.6	22.8	26	−0.5	4	7.6	9.7	7.4	8.0	9.4	9.9	9.6	9.6	9.0	8.3	9.1	8.8	1.4	2.7	1.0	1.7	7.4	8.4	7.1	7.6
VIII	865.1	871.3	855.4	–	12.9	7.0	20.8	13	2.6	31	8.8	11.2	9.1	9.6	10.2	10.8	10.0	10.3	8.9	7.6	8.6	8.4	1.6	2.9	1.8	2.1	7.8	8.5	7.0	7.8
IX	863.6	870.9	850.3	–	9.6	3.3	20.2	4	−1.0	23	5.1	7.4	5.6	5.9	7.7	8.4	7.7	7.9	8.8	8.3	8.5	8.5	1.4	2.5	1.7	1.9	7.7	7.9	5.4	7.0
X	862.2	878.3	853.1	–	8.1	2.2	16.8	2	−4.2	30	4.0	6.7	4.0	4.7	6.2	7.0	6.8	6.7	7.7	7.4	8.3	7.8	2.3	3.5	1.6	2.5	5.5	5.5	5.2	5.4
XI	857.9	873.4	840.9	–	0.0	−4.0	12.5	7	−10.1	23	−2.5	−1.5	−2.3	−2.2	5.0	5.3	5.1	5.1	9.5	9.4	9.6	9.5	0.3	0.4	0.3	0.3	9.0	8.7	9.0	8.9
XII	855.6	879.5	822.8	–	−4.5	−9.8	6.6	6	−22.6	23	−7.8	−6.5	−7.8	−7.5	2.9	3.2	2.9	3.0	8.2	8.2	8.2	8.2	0.8	0.9	0.8	0.8	7.8	7.6	7.1	7.5
Rok	860.6	879.5	822.8	–	3.8	−1.6	22.8	26.VII	−22.6	23.XII	0.2	2.2	0.5	0.8	6.0	6.5	6.2	6.2	8.8	8.4	8.8	8.7	1.1	1.8	1.0	1.3	8.0	8.2	7.5	7.9

Szczawno-Zdrój $\varphi = 50°48'$ $\lambda = 16°16'$

I	–	–	–	–	2.3	−2.7	7.6	20, 22	−18.7	31	−0.5	1.0	−0.5	−0.1	4.9	4.9	4.8	4.9	8.0	7.3	7.9	7.7	1.3	1.9	1.4	1.5	7.2	7.3	7.6	7.4
II	–	–	–	–	0.3	−4.9	5.8	12	−18.1	1	−3.1	−1.0	−2.1	−2.1	4.3	4.6	4.5	4.5	8.5	8.0	8.4	8.3	0.8	1.2	1.0	1.0	8.9	8.8	8.8	8.8
III	–	–	–	–	2.0	−4.0	11.8	31	−9.7	9	−2.1	1.0	−1.4	−1.0	4.6	4.8	4.6	4.7	8.4	7.0	8.1	7.8	0.9	2.0	1.0	1.3	8.2	8.0	7.1	7.8
IV	–	–	–	–	13.7	5.1	26.1	23	−0.7	11	8.4	12.4	8.1	9.2	7.8	7.8	7.9	7.8	7.2	5.8	7.4	6.8	4.1	8.4	3.5	5.3	6.2	7.6	6.8	6.9
V	–	–	–	–	14.0	6.0	22.1	19	−1.7	1	9.1	12.4	9.2	10.0	8.7	8.7	9.3	8.9	7.5	6.1	7.9	7.2	3.1	6.2	2.6	4.0	7.5	8.2	8.6	8.1
VI	–	–	–	–	18.9	9.0	29.3	16	1.6	4	13.1	17.3	12.6	13.9	10.4	10.0	10.8	10.4	6.7	5.0	7.1	6.3	5.7	11.2	4.4	7.1	5.0	7.0	6.2	6.1
VII	–	–	–	–	19.7	10.4	30.3	26	4.8	9	14.6	18.4	12.9	14.7	12.4	11.7	12.3	12.1	7.4	5.5	8.2	7.0	4.6	10.2	3.0	5.9	6.5	7.6	6.3	6.8
VIII	–	–	–	–	21.5	11.9	30.8	13	7.3	31	15.9	20.1	14.6	16.3	13.0	12.7	13.1	12.9	7.1	5.4	7.8	6.8	5.3	11.6	3.7	6.9	5.9	7.6	4.8	6.1
IX	–	–	–	–	17.0	8.0	28.7	4	1.8	15	11.2	15.7	11.1	12.3	10.4	9.9	10.0	10.1	7.9	5.8	7.7	7.1	3.3	8.9	3.8	5.3	6.6	6.9	5.3	6.3
X	–	–	–	–	13.0	5.4	23.7	4	0.2	16, 21, 22	7.4	11.9	7.7	8.7	8.9	9.3	9.2	9.1	8.4	6.8	8.6	7.9	1.8	5.5	1.7	3.0	4.8	5.1	4.5	4.8
XI	–	–	–	–	5.2	1.6	16.1	8	−4.1	24	2.7	4.5	3.1	3.4	6.6	6.8	6.6	6.7	8.7	7.9	8.4	8.3	1.1	2.1	1.3	1.5	8.8	8.5	8.5	8.6
XII	–	–	–	–	−2.3	−7.5	4.2	12	−19.8	22	−5.4	−3.7	−5.0	−4.8	3.5	3.7	3.5	3.6	8.0	7.6	7.9	7.8	1.0	1.3	1.0	1.1	8.0	7.0	8.0	7.7
Rok	–	–	–	–	10.4	3.2	30.8	13.VIII	−19.8	22.XII	5.9	9.2	5.9	6.7	8.0	7.9	8.0	8.0	7.8	6.5	8.0	7.4	2.8	5.9	2.4	3.7	7.0	7.5	6.9	7.1

Karpacz $\varphi = 50°46'$ $\lambda = 15°45'$

I	932.1	949.8	910.1	–	2.0	−3.4	8.5	1	−15.4	31	−1.2	0.1	−0.7	−0.6	4.6	4.8	4.8	4.7	7.9	7.7	7.9	7.8	1.2	1.6	1.3	1.4	7.2	7.5	7.3	7.3
II	931.9	947.7	904.6	–	−1.2	−6.9	3.7	11	−14.9	26	−4.6	−3.0	−4.0	−3.9	4.0	4.4	4.1	4.2	9.0	8.8	8.9	8.9	0.5	0.6	0.6	0.6	9.1	8.0	7.6	8.2
III	926.6	942.2	909.2	–	0.0	−6.3	8.5	30	−12.2	14	−4.4	−1.3	−3.4	−3.1	3.9	4.3	4.2	4.1	8.5	7.4	8.4	8.1	0.7	1.5	0.7	1.0	7.8	7.4	7.2	7.5
IV	931.5	944.1	906.6	–	10.3	2.9	24.0	24	−2.9	7	5.8	9.1	5.8	6.6	7.0	7.3	7.2	7.2	7.7	6.8	8.0	7.5	3.1	5.9	2.8	3.9	6.4	7.5	6.0	6.6
V	931.5	936.8	922.4	–	10.9	3.8	19.2	8, 19	−5.4	1	6.4	9.5	6.8	7.4	8.1	8.3	8.5	8.3	8.3	7.0	8.5	7.9	1.8	4.1	1.7	2.5	8.1	8.7	7.8	8.2
VI	937.4	946.3	929.2	–	15.7	7.2	26.6	16	−0.5	6	10.3	14.0	10.9	11.5	9.7	9.9	10.2	9.9	7.5	6.1	7.5	7.0	3.8	7.3	3.5	4.9	5.3	7.1	6.5	6.3
VII	934.2	943.2	919.2	–	16.3	8.9	28.2	26	4.3	9	11.9	15.3	11.4	12.5	11.4	11.8	11.7	11.6	8.1	6.8	8.6	7.8	3.0	6.3	2.1	3.8	5.9	7.3	6.4	6.5
VIII	935.2	942.2	924.7	–	18.3	10.6	25.9	13	6.3	9, 31	13.5	17.1	13.1	14.2	12.0	12.9	12.1	12.3	7.7	6.6	7.9	7.4	3.9	7.1	3.3	4.7	6.7	7.5	5.1	6.4
IX	934.8	943.4	921.1	–	14.2	7.0	25.2	4	1.8	23	9.3	12.8	10.0	10.5	9.7	10.1	9.6	9.8	8.3	6.9	7.9	7.7	0.4	5.5	3.3	3.1	6.7	7.0	3.8	5.8
X	938.9	950.7	926.4	–	11.0	4.0	19.8	3	−1.2	30	5.8	9.4	6.8	7.2	8.0	9.2	8.5	8.6	8.5	7.8	8.5	8.3	1.5	3.3	1.7	2.2	4.5	4.8	4.8	4.7
XI	931.6	948.5	914.5	–	3.5	−0.8	13.2	7	−7.9	25	0.8	2.2	1.0	1.2	6.0	6.4	6.2	6.2	9.0	8.8	9.1	9.0	0.8	1.1	0.7	0.9	8.1	8.3	7.9	8.1
XII	930.8	956.3	893.5	–	−2.8	−8.1	7.5	9	−19.9	22	−5.6	−4.5	−5.8	−5.4	3.7	3.9	3.6	3.7	8.7	8.5	8.7	8.6	0.7	0.9	0.6	0.7	7.0	7.3	7.2	7.2
Rok	933.0	956.3	893.5	–	8.2	1.6	28.2	26.VII	−19.9	22.XII	4.0	6.7	4.3	4.8	7.3	7.8	7.6	7.6	8.3	7.4	8.3	8.0	1.8	3.8	1.9	2.5	6.9	7.4	6.5	6.9

Częstochowa $H_s = 261\,m$ $H_b = 262{,}7\,m$ $h_w = 21{,}5\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU %D, v m/s																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr v				Opad R						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min < -10°	Max < 0°	Min < 0°	Max > 25°	n ≥ 10	n ≥ 15	◐	●	n ≥ 0.1	n ≥ 1.0	n ≥ 10.0	≈	⊠	n ≥ 20
I	5.5	6.6	4.5	3.7	·	·	·	·	12.5	3.2	4.8	2.9	16	2.6	6.5	3.1	·	3.2	44	8.3	25	2	6	24	·	1	·	3	13	15	12	·	·	17	·
II	6	3.4	5	3.2	13.5	1.8	2.5	1.8	10.5	2.6	15	4.7	17.5	4.9	11	4.8	3	3.6	49	10.1	12	5	11	25	·	3	·	·	22	20	11	1	2	21	1
III	14	3.8	9	2.6	11	1.9	9	1.9	17	1.4	7.5	2.4	14.5	3.0	8	3.7	3	2.5	62	16.2	12	·	9	24	·	·	·	3	14	16	12	2	4	19	·
IV	11.5	1.6	5	3.3	10	2.0	5.5	1.6	19	2.5	13	2.3	11	2.8	11	3.7	4	2.4	51	11.8	26	·	·	1	7	·	·	5	11	13	8	3	1	·	2
V	1.5	1.3	1	2.0	3.5	1.7	5	1.5	14.5	2.1	13.5	3.1	37.5	3.0	10.5	1.9	6	2.4	115	15.3	20	·	·	2	·	1	·	·	12	26	22	2	1	·	2
VI	18.5	3.2	4	1.1	2	1.8	1.5	1.3	6.5	2.1	12.5	2.2	30	3.1	11	2.5	4	2.6	60	19.4	1	·	·	·	7	1	·	1	10	10	8	4	·	·	1
VII	11.5	1.4	5	1.8	1	1.0	·	·	10.5	2.2	14.5	2.2	28.5	2.2	16	1.9	6	1.9	82	19.3	27	·	·	·	5	1	1	5	10	16	12	2	·	·	6
VIII	3.5	2.6	0.5	2.0	0.5	2.0	6.5	1.7	4	3.6	29	2.6	40.5	2.7	4.5	1.6	4	2.4	75	24.1	15	·	·	·	9	·	·	1	7	16	10	2	1	·	5
IX	3	2.3	1	2.0	13.5	1.3	2.5	2.4	8	2.2	25	3.4	24.5	2.3	8.5	2.2	4	2.3	66	30.6	17	·	·	·	4	1	·	4	11	10	7	2	5	·	·
X	9.5	1.5	5.5	2.0	14.5	1.3	13.5	1.4	2.5	2.0	12	2.1	20	2.0	5.5	1.5	10	1.5	14	8.2	28	·	·	9	·	·	·	8	11	8	2	·	12	·	·
XI	10	1.3	4	2.5	12.5	2.4	22.5	1.3	6	1.3	17	2.8	7.5	1.7	3.5	1.3	7	1.7	74	24.4	20	·	·	10	·	1	·	1	23	17	10	2	5	4	·
XII	8	2.8	9.5	3.1	10	1.8	·	·	12.5	2.2	3.0	2.5	11.5	1.7	8.5	2.2	3	2.3	33	9.3	15	9	13	29	·	·	·	1	20	19	5	·	3	18	·
Rok	102.5	2.6	5.4	2.4	9.2	1.6	68.5	1.2	123.5	2.3	23.7	2.8	25.9	2.7	104.5	2.5	5.4	2.4	72.5	30.6	17.IX	16	39	124	32	9	1	32	164	186	119	20	34	79	17

Szrenica $H_s = 1323\,m$ $H_b = 1363{,}6\,m$ $h_w = 19{,}8\,m$

I	11	14.4	2	10.2	5	12.4	1	20.0	5.5	13.2	48.5	16.7	8.5	13.9	9.5	11.3	2	14.7	111	16.4	24	6	25	31	·	28	27	1	16	23	16	3	27	31	·
II	11	13.1	14	11.8	1.5	9.3	6.5	9.0	3.5	14.4	16.5	16.2	11.5	11.9	18.5	19.1	1	14.2	135	27.1	12	16	28	28	·	26	15	·	23	24	18	4	26	28	·
III	8.5	10.9	15.5	9.7	14.5	11.0	4	22.1	11	12.0	23.5	10.3	5	10.6	9	12.5	2	11.1	115	27.0	30	16	25	31	·	23	14	·	26	24	15	4	26	31	·
IV	4	9.5	9	6.7	9	7.9	9	9.8	14	13.8	23	14.5	14	10.6	8	11.3	·	11.4	90	16.4	28	·	11	20	·	26	20	1	20	19	16	2	18	26	2
V	3	8.8	6.5	6.9	4.5	6.9	0.5	2.0	10	10.4	38	8.8	21.5	8.1	8	8.0	1	8.4	167	24.9	12	·	4	10	·	27	9	·	23	28	23	6	28	12	4
VI	11	10.6	11.5	10.7	3	4.7	1.5	3.0	8	8.9	23.5	9.4	18	8.6	10.5	6.0	3	8.5	72	16.3	28	·	·	9	·	24	8	·	15	16	10	3	14	4	4
VII	5	5.6	8.5	6.5	7.5	5.2	·	·	7.5	10.5	36	9.5	19.5	8.9	7	5.8	2	8.2	163	22.9	16	·	·	1	·	20	7	·	14	22	17	7	20	·	8
VIII	1.5	7.0	1	3.0	2	2.0	·	·	7	11.3	5.6	11.4	17.5	9.9	7	8.6	1	10.4	105	21.5	5	·	·	·	·	27	11	·	15	18	16	2	22	·	4
IX	4.5	6.9	4	4.1	2.5	4.6	7	10.7	12.5	10.4	33.5	11.9	15	10.3	10	8.4	1	10.0	120	26.0	16	·	·	6	·	24	14	2	13	20	11	4	20	3	·
X	8.5	7.1	12	6.1	11.5	2.8	7	8.3	21.5	8.2	17	9.1	4	8.4	6.5	7.1	5	6.8	68	20.4	31	·	1	12	·	21	7	10	13	21	12	3	16	2	·
XI	4	4.5	13	6.9	8.5	5.4	12	18.9	25.5	14.1	17	10.0	5	9.4	4	6.2	1	10.9	61	11.9	1	1	18	25	·	22	12	·	22	26	15	1	30	24	·
XII	4	7.2	6	5.3	17.5	11.3	8	3.8	7	8.7	23.5	13.0	14	10.3	11	5.7	2	9.3	77	15.3	16	14	26	31	·	20	11	2	17	18	14	2	21	31	·
Rok	76	8.8	10.3	7.3	8.7	7.0	56.5	9.0	13.3	11.3	35.6	11.7	153.5	10.1	10.9	9.2	21	10.3	1284	27.1	12.II	53	138	204	·	288	155	16	217	259	183	41	268	192	22

UWAGA. Kierunki i prędkości wiatru - wg anemografu

Szczawno-Zdrój $H_s = 415\,m$ $h_w = 13\,m$

I	8	4.8	·	·	·	·	1	1.0	1.4	5.9	3.7	9.0	1.3	5.5	2	4.0	1.8	5.7	34	6.5	26	2	4	18	·	11	5	4	19	11	9	·	1	15	·
II	8	3.0	6	2.0	4	1.8	·	·	10	2.5	9	11.0	15	8.2	16	7.8	16	5.0	42	7.6	27	3	11	25	·	8	4	·	22	16	11	·	3	24	·
III	9	2.4	5	2.6	1	2.0	3	5.0	10	4.4	7	4.0	9	5.0	6	3.2	4.3	2.0	42	18.0	31	·	9	26	·	4	·	2	21	11	5	1	5	16	·
IV	5	1.6	4	1.5	4	2.2	5	2.2	11	4.5	14	5.3	15	2.7	3	3.0	2.9	2.3	46	14.5	26	·	·	1	3	3	1	4	16	12	10	1	2	·	1
V	2	2.0	2	2.0	2	1.5	·	·	2	3.0	14	2.6	2.2	4.5	8	3.2	4.1	1.9	66	16.0	13	·	·	1	·	2	·	·	20	17	10	2	1	·	4
VI	7	3.9	·	·	2	1.5	·	·	3	2.0	6	1.8	2.2	3.0	11	2.4	3.9	1.6	28	7.3	19	·	·	·	6	·	·	5	12	7	6	·	·	·	2
VII	2	1.5	1	1.0	·	·	·	·	3	1.7	8	2.5	2.5	2.4	6	1.3	4.8	1.0	55	20.8	16	·	·	·	5	·	·	·	12	13	11	1	1	·	4
VIII	1	1.0	1	1.0	·	·	·	·	4	1.8	2.1	3.6	2.5	3.2	2	1.5	3.9	1.8	33	12.1	5	·	·	·	5	1	·	1	10	10	7	1	2	·	3
IX	·	·	2	1.5	2	2.0	·	·	6	1.2	1.8	5.0	2.0	2.3	2	2.0	4.0	1.7	39	14.7	18	·	·	·	3	2	1	5	12	10	7	1	5	·	·
X	1	1.0	3	1.3	·	·	·	·	6	1.8	9	2.2	7	1.4	3	1.7	6.4	0.5	37	15.2	31	·	·	·	·	·	·	14	11	12	8	1	12	·	·
XI	1	1.0	3	1.7	·	·	3	3.7	10	2.4	1.5	2.5	12	2.2	8	1.4	3.8	1.3	41	10.9	1	·	1	11	·	·	·	1	23	12	9	1	6	8	·
XII	3	2.0	8	2.4	·	·	·	·	6	5.0	31.5	5.2	15	3.8	18.5	2.1	11	3.4	26	5.4	16	9	14	28	·	5	1	3	22	13	8	·	2	27	·
Rok	47	2.0	3.5	1.4	1.5	0.9	1.2	1.0	8.5	3.0	18.9.5	4.6	20.0	3.7	8.5.5	2.8	4.2.6	2.4	48.9	20.8	16.VII	14	3.9	110	22	3.6	12	3.9	200	144	101	9	40	90	14

Karpacz $H_s = 700\,m$ $H_b = 708{,}0\,m$ $h_w = 16\,m$

I	1	3.5	1	3.0	·	·	2	4.0	2.0	6.5	1.2	4.7	7	3.2	2.2	4.5	2.8	3.5	8.7	16.4	12	3	7	24	·	8	4	2	16	18	13	2	3	29	·
II	2.5	6.6	3	2.0	·	·	1	10.0	6	15.5	1	17.0	·	·	29.5	7.5	4.1	4.3	10.0	33.5	12	7	15	27	·	7	4	1	19	20	15	2	5	28	·
III	4.5	3.2	3	1.7	2	1.5	3.5	11.7	6.5	5.0	3.5	3.6	5.5	4.0	21.5	3.3	4.3	2.2	10.1	22.5	30	5	18	29	·	1	1	2	16	21	12	4	5	31	·
IV	4.5	2.4	0.5	2.0	4.5	3.4	10.5	4.7	10	10.3	8.5	4.9	4.5	3.1	13	2.3	3.4	2.9	10.1	22.3	28	·	·	12	·	6	2	3	12	17	16	3	6	14	1
V	3	2.0	2	2.5	1	2.0	1.5	2.3	5.5	3.4	7.5	2.3	16.5	2.2	14	2.9	4.2	1.4	14.7	38.4	14	·	·	5	·	·	·	·	16	23	17	4	2	4	4
VI	5	2.9	1	3.0	2	3.0	3	2.8	4.5	3.1	4.5	2.4	8	3.6	2.2	3.5	4.0	1.8	9.2	43.7	16	·	·	1	4	·	·	1	12	12	10	3	1	·	4
VII	6.5	2.7	1	1.5	·	·	1	1.0	9	3.4	12	3.7	11.5	2.8	11	3.0	4.1	1.7	14.1	53.7	16	·	·	·	1	2	1	2	12	18	17	2	2	·	5
VIII	1.5	3.3	0.5	5.0	0.5	5.0	8.5	5.4	10	3.2	12.5	4.4	11	3.6	12.5	4.2	3.6	2.5	7.0	12.6	13	·	·	·	1	2	·	1	11	17	13	2	3	·	5
IX	5	1.7	1	1.5	1.5	5.0	7	7.0	9	4.9	10	4.8	8	3.9	14.5	3.3	3.4	2.6	9.6	25.9	16	·	·	·	1	4	·	4	9	14	10	4	3	·	·
X	0.5	4.0	·	·	1	5.0	2	4.0	1.5	3.3	3.5	4.0	5	2.5	8.5	2.6	7.1	0.7	8.0	22.9	6	·	·	4	·	·	·	13	13	15	11	3	7	·	·
XI	0.5	1.0	·	·	2.5	7.4	6.5	11.6	12.5	11.6	3	2.7	4	2.5	1[illegible]	2.9	4.9	3.2	4.3	12.3	1	·	6	2.0	·	4	2	·	19	16	9	1	10	17	·
XII	2	2.0	·	·	·	·	1	8.0	4	5.0	4.5	8.0	4.5	2.9	13	3.5	6.4	1.4	5.1	8.3	9	11	16	31	·	1	·	4	16	19	11	·	5	31	·
Rok	36.5	2.9	1.3	1.8	1.5	2.7	47.5	6.0	98.5	6.3	82.5	5.2	85.5	2.9	193.5	3.6	5.2.3	2.4	110.9	53.7	16.VII	26	62	153	7	35	14	33	171	210	154	30	52	154	19

Dobrogoszcz $\varphi = 50°46'$ $\lambda = 17°01'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA t										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{m.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.6	−1.2	11.2	22	−17.8	31	0.5	2.4	0.7	1.1	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.6	6.8	6.8
II	–	–	–	–	1.7	−3.9	8.2	12	−17.9	1	−1.6	0.2	−0.8	−0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.8	7.3	8.1
III	–	–	–	–	3.2	−2.9	14.4	31	−7.5	2, 3	−1.4	2.3	−0.3	0.1	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.1	6.6	7.0
IV	–	–	–	–	15.5	5.6	27.2	22, 24	0.7	1	8.2	14.4	9.6	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.3	6.2	6.5
V	–	–	–	–	15.2	6.8	22.4	8	−0.3	1	9.7	13.6	10.3	11.0	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.5	7.0	7.3
VI	–	–	–	–	20.0	9.2	29.4	16	1.8	8	13.3	18.6	13.9	14.9	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.8	5.0	5.4
VII	–	–	–	–	21.3	10.2	31.8	26	4.7	9	14.3	19.9	14.6	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.7	6.5	6.1
VIII	–	–	–	–	23.6	12.0	31.7	13	7.0	31	15.5	21.8	15.7	17.2	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.9	4.6	5.7
IX	–	–	–	–	18.8	8.6	31.0	4	2.9	27	11.1	17.1	12.4	13.2	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.7	4.7	5.7
X	–	–	–	–	13.8	5.0	25.1	4	−1.8	22	6.6	12.6	7.7	8.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.5	5.5	5.7
XI	–	–	–	–	6.6	1.7	16.9	8	−2.7	26	2.9	5.9	3.5	4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	8.2	6.8	7.6
XII	–	–	–	–	−1.2	−7.0	6.4	12	−20.9	24	−4.6	−2.2	−4.5	−4.0	–	–	–	–	–	–	–	–	–	–	–	–	2.4	7.5	6.7	7.2
Rok	–	–	–	–	11.8	3.7	31.8	26.VII	−20.9	24, XII	6.2	10.6	6.9	7.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.8	6.1	6.6

Werbkowice $\varphi = 50°45'$ $\lambda = 23°46'$

I	–	–	–	–	1.4	−3.7	6.7	22	−17.7	31	−1.8	0.1	−1.5	−1.2	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.8	7.2	8.0
II	–	–	–	–	−1.1	−7.0	2.7	13	−14.1	28	−5.1	−2.3	−3.8	−3.8	–	–	–	–	–	–	–	–	–	–	–	–	9.0	9.0	7.7	8.6
III	–	–	–	–	0.8	−6.7	11.2	5	−18.3	21	−4.7	−0.3	−3.3	−2.9	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.7	7.6	7.9
IV	–	–	–	–	16.1	5.0	26.8	24	−1.3	30	7.0	14.8	9.5	10.2	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.4	4.8	5.7
V	–	–	–	–	16.7	6.8	24.2	27	−0.8	2, 3	9.6	15.0	11.0	11.6	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.9	6.4	7.3
VI	–	–	–	–	19.2	8.9	27.8	16	3.1	7	12.9	17.8	13.6	14.5	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.8	6.6	6.4
VII	–	–	–	–	21.0	9.6	28.8	27	5.4	30	14.0	19.4	14.5	15.6	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.9	5.6	6.3
VIII	–	–	–	–	22.9	10.9	30.8	7, 13	5.1	27	14.4	21.5	15.7	16.8	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.3	4.9	5.8
IX	–	–	–	–	18.0	7.0	29.4	5	1.7	25	9.4	16.7	11.4	12.3	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.7	5.2	5.8
X	–	–	–	–	13.9	1.2	20.0	4	−5.8	17	3.5	12.8	6.2	7.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	5.3	3.7	5.6
XI	–	–	–	–	7.8	1.7	19.4	1	−4.1	18	3.2	6.6	4.0	4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.3	7.6	8.2
XII	–	–	–	–	−2.6	−8.0	2.9	1, 11	−19.8	21, 22	−5.9	−3.6	−5.6	−5.2	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.9	6.8	7.8
Rok	–	–	–	–	11.2	2.1	30.8	7.13.VIII	−19.8	21.22.XII	4.7	9.9	6.0	6.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.2	6.2	7.0

Śnieżka $\varphi = 50°44'$ $\lambda = 15°44'$

I	830.4	842.3	810.0	–	−3.5	−8.7	4.8	5	−18.3	30	−6.1	−5.6	−6.0	−5.9	3.4	3.6	3.4	3.5	8.6	8.9	8.6	8.7	0.6	0.6	0.7	0.6	8.4	8.7	8.4	8.5
II	828.8	844.4	806.2	–	−6.6	−11.6	−1.8	8	−18.1	25	−9.4	−8.4	−9.1	−9.0	2.7	3.0	2.9	2.9	8.6	8.9	9.0	8.8	0.4	0.3	0.3	0.3	8.8	8.9	8.0	8.6
III	824.9	839.6	810.9	–	−5.5	−11.5	3.9	11	−17.7	17	−9.8	−7.1	−8.7	−8.6	2.8	3.4	3.1	3.1	8.7	8.9	8.8	8.8	0.3	0.4	0.3	0.3	9.1	8.6	8.3	8.7
IV	832.9	849.2	809.5	–	3.1	−1.9	15.1	25	−8.9	7	0.0	1.6	0.5	0.6	4.9	5.6	5.5	5.3	8.2	8.3	8.6	8.4	1.8	2.1	1.5	1.8	7.5	8.0	7.6	7.7
V	833.1	839.2	822.1	–	3.4	−1.5	9.8	8	−9.8	1	−0.4	1.6	1.1	0.8	5.8	6.4	6.5	6.2	9.5	9.1	9.5	9.4	0.3	0.7	0.3	0.4	8.7	9.3	8.5	8.8
VI	840.2	848.0	829.9	–	7.8	1.9	17.4	23	−7.1	6	3.5	5.7	5.0	4.8	7.4	8.1	7.9	7.8	8.9	8.4	8.7	8.7	1.0	1.9	1.5	1.5	7.1	8.0	6.9	7.3
VII	837.8	846.6	819.0	–	8.9	4.3	19.3	26	−2.2	4	5.6	7.2	6.3	6.4	8.4	8.8	8.8	8.7	9.1	8.9	9.0	9.0	1.0	1.5	1.0	1.2	7.4	8.4	6.8	7.5
VIII	839.5	845.5	831.0	–	10.8	5.4	19.5	13	0.6	26	7.2	8.8	8.1	8.0	9.1	9.9	9.5	9.5	8.9	8.7	8.7	8.8	1.4	1.7	1.6	1.6	7.4	8.2	6.2	7.3
IX	837.6	845.2	824.1	–	7.5	2.0	17.0	4	−2.1	23	3.8	5.3	4.3	4.4	7.0	7.6	7.4	7.3	8.7	8.5	8.8	8.7	1.2	1.8	1.3	1.4	7.6	7.4	6.0	7.0
X	841.2	852.5	827.7	–	6.7	0.9	15.4	4	−6.6	21	3.5	4.9	3.2	3.7	5.4	6.4	6.3	6.0	7.2	7.5	8.2	7.6	3.0	2.7	1.8	2.5	5.1	5.3	5.9	5.4
XI	831.7	846.2	814.8	–	−0.9	−5.2	11.2	7	−11.5	23	−3.3	−2.6	−3.2	−3.1	4.7	4.7	4.4	4.6	9.3	9.1	8.9	9.1	0.3	0.6	0.6	0.5	8.5	8.6	8.8	8.6
XII	828.7	852.2	796.9	–	−5.4	−11.0	6.7	7	−23.9	23	−8.3	−7.3	−8.5	−8.2	2.8	2.9	2.6	2.8	8.2	7.8	7.8	7.9	0.7	1.0	0.9	0.9	7.3	7.0	6.5	6.9
Rok	833.9	852.5	796.9	–	2.2	−3.1	19.5	13.VIII	−23.9	23.XII	−1.1	0.3	−0.6	−0.5	5.4	5.9	5.7	5.7	8.6	8.6	8.7	8.6	1.0	1.3	1.0	1.1	7.7	8.0	7.3	7.7

Zamość $\varphi = 50°44'$ $\lambda = 23°15'$

I	990.1	1009.2	970.7	1017.6	2.3	−2.8	7.4	2.2	−17.4	31	−1.1	1.1	−0.8	−0.4	5.3	5.5	5.2	5.3	9.1	8.1	8.8	8.7	0.5	1.4	0.7	0.9	8.1	6.9	6.8	7.3
II	988.3	1005.5	960.3	1016.3	−0.8	−6.2	2.8	1.3	−13.9	2.5	−4.4	−1.8	−3.6	−3.4	4.1	4.5	4.4	4.3	8.9	8.3	9.1	8.8	0.5	0.9	0.4	0.6	8.9	8.8	8.1	8.6
III	984.4	1001.2	966.0	1011.9	1.4	−6.0	13.0	5	−16.4	21	−4.1	0.2	−2.7	−2.3	4.4	4.9	4.7	4.7	9.0	7.6	8.8	8.5	0.5	1.5	0.6	0.9	7.8	8.0	7.5	7.8
IV	987.8	1001.1	966.1	1014.1	16.7	5.4	26.8	2.4	−0.8	8	7.6	15.4	9.8	10.6	8.9	9.2	8.2	8.1	8.4	5.5	7.6	7.2	2.0	9.9	3.5	5.1	5.3	5.2	4.4	5.0
V	986.7	994.8	971.6	1012.9	16.6	7.2	24.5	14, 28	−0.6	2	9.8	15.2	10.8	11.6	11.4	11.7	11.9	11.7	9.1	6.7	8.9	8.2	1.1	6.6	1.5	3.1	6.6	7.4	5.3	6.4
VI	990.8	999.6	981.6	1016.9	19.5	9.6	28.8	2.3	3.3	7	13.3	18.0	13.7	14.7	13.2	13.4	13.5	13.4	8.4	6.4	8.3	7.7	2.7	8.7	2.8	4.7	6.1	6.7	5.1	6.0
VII	988.3	998.7	976.3	1014.3	21.3	11.0	28.9	2.7	7.2	4, 30	14.2	19.8	15.1	16.1	14.2	14.2	14.8	14.4	8.7	6.2	8.5	7.8	2.3	9.5	2.6	4.8	6.0	6.6	4.9	5.8
VIII	990.3	998.3	981.5	1016.2	23.2	12.3	31.1	1.3	6.2	2.7	14.9	21.7	16.6	17.4	15.6	15.8	16.5	16.0	9.1	6.1	8.6	7.9	1.6	10.9	2.9	5.1	5.5	6.2	4.0	5.2
IX	990.8	1004.4	976.8	1017.0	18.1	8.2	28.9	5	3.6	25, 26	10.0	16.6	11.8	12.6	11.3	12.1	12.4	11.9	9.1	6.5	8.9	8.2	1.4	7.6	1.8	3.6	5.3	6.5	5.0	5.6
X	996.3	1009.7	982.8	1023.2	13.7	2.4	19.9	2	−4.4	17	3.7	12.8	6.6	7.4	2.9	3.9	3.1	3.0	9.6	6.6	9.1	8.4	0.4	5.3	0.9	2.2	6.3	5.7	3.5	5.2
XI	991.6	1004.6	978.1	1018.7	7.5	2.0	19.6	1	−2.8	18	3.4	6.5	4.1	4.5	7.6	8.1	7.8	7.8	9.5	8.4	9.4	9.1	0.4	2.1	0.6	1.0	8.1	8.1	8.1	8.1
XII	989.7	1016.1	949.9	1017.7	−2.1	−7.3	4.6	1.3	−18.3	2.2	−5.6	−3.3	−5.0	−4.7	3.9	4.4	4.1	4.1	9.1	8.8	9.0	9.0	0.4	0.7	0.5	0.5	8.0	7.8	7.8	7.9
Rok	989.6	1016.1	949.9	1016.4	11.4	3.0	31.1	13.VIII	−18.3	22.XII	5.1	10.2	6.4	7.0	8.0	8.5	8.5	8.3	9.0	7.1	8.8	8.3	1.2	5.4	1.6	2.7	6.8	7.0	5.9	6.6

Dobrogoszcz $H_s = 175\,m$ h_w = 15,5 m I–II, 11,5 m III–XII 1962

MIESIĄC	ROZKŁAD WIATRU ºD, VmD																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Wiatr v				Opad R					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R
I	7.5	4.7	·	·	·	·	2.5	1.4	21.5	5.3	36.5	5.7	8.5	4.5	15.5	5.2	1	5.2	16	5.5	26	2	3	15		8	2	1	11	13	5	·	2	3	-
II	4	4.5	7	1.9	4	1.2	3	2.5	10.5	2.3	19	7.2	12.5	11.4	20	6.9	4	5.8	24	3.7	27	3	11	21	·	8	4	·	14	19	10	·	1	17	·
III	7	2.3	1	5.0	4.5	1.2	9	1.8	21.5	2.6	2	4.5	12	4.8	14	4.9	22	2.5	58	17.0	12	·	7	24		3	1	1	11	10	6	3	1	8	
IV	6.5	2.2	3.5	3.4	4.5	2.9	9.5	3.1	18	3.6	14.5	5.8	4.5	3.8	19	6.3	10	3.9	38	19.1	26	·	·	·	7	8	1	3	13	12	8	1	·	·	1
V	5.5	2.7	3	1.5	7.5	1.6	6	2.2	9	1.4	10	3.8	13.5	4.2	23.5	6.7	15	3.3	98	24.4	14	·	·	1	·	4	2	·	12	24	14	3	·	·	1
VI	13.5	4.4	2	3.0	2	2.5	3.5	1.4	12.5	1.7	5.5	1.8	8.5	5.4	34.5	4.7	8	3.5	37	21.7	16	·	·	·	7	4	·	3	4	7	5	1	·	·	2
VII	6	3.8	4	1.8	6	1.7	4.5	1.8	11.5	2.2	12	5.5	14.5	3.8	22.5	3.1	12	2.8	85	22.7	11	·	·	·	6	2	·	1	9	15	12	3	·	·	4
VIII	1	2.0	1	3.0	0.5	1.0	10.5	1.6	15	2.4	14.5	3.8	19	4.3	25.5	4.1	6	3.2	53	16.8	5	·	·	·	8	3	·	1	4	10	7	2	·	·	1
IX	2.5	3.4	·	·	5	3.9	7	3.1	11	3.4	17.5	5.0	13	5.2	18	5.1	16	3.7	69	25.5	18		·	·	4	4	·	3	8	13	8	2	2	·	·
X	4.5	3.8	1.5	3.0	7	2.1	8.5	2.8	21.5	2.6	7	5.2	3	3.7	21	4.1	19	2.7	41	16.0	31	·	·	3	1	2	·	7	11	13	6	2	8	·	·
XI	5.5	1.8	13	2.4	4.5	6.6	15	3.8	12	3.0	11	3.5	6	4.1	15	3.5	8	3.1	65	20.4	1	·	1	8	·	2	·	2	17	13	12	2	3	·	·
XII	3	4.7	4.5	2.1	1.5	2.3		·	25	3.0	13.5	7.3	6	5.0	36.5	2.1	3	3.3	17	4.2	18	11	14	27	·	4	2	3	15	12	6	·	·	15	·
Rok	66.5	3.4	40.5	2.3	47	2.2	79	2.1	189	2.8	163	4.9	121	5.0	265	4.7	124	3.6	601	25.5	18. IX	16	36	99	33	52	12	25	129	161	99	19	17	43	9

Werbkowice $H_s = 204\,m$ $h_w = 14\,m$

I	15	4.4	6.5	3.5	1	3.0	2.5	3.8	15.5	2.8	28	3.9	31	5.7	7	5.6	·	4.4	17	4.0	25	2	10	26	·	4	·	·	18	12	5	·	·	25	–
II	8	4.8	3	6.3	7	2.4	6	2.6	10.5	3.0	9.5	8.4	18.5	6.5	17.5	7.3	4	5.3	22	5.3	25	8	15	27	·	9	1	·	18	17	8	·	·	28	–
III	9.5	4.7	8.5	4.2	11	2.4	14	3.2	11.5	2.9	7	3.6	10.5	7.9	14	4.9	7	3.9	39	10.6	16	7	16	27	·	3	·	1	18	15	9	1	2	27	–
IV	5	5.4	10	2.5	20	2.7	8.5	2.6	10.5	3.1	14.5	3.3	9	3.5	7.5	5.7	5	3.2	28	8.6	6	·	·	3	4	1	·	6	9	9	7	·	2	2	–
V	7	2.1	1	3.0	6	2.0	5	2.8	7	2.5	22.5	4.4	19	4.0	16.5	3.9	9	3.2	69	13.0	11	·	·	4	·	3	2	1	14	18	13	2	4	·	–
VI	14	3.6	6.5	2.5	3	1.7	2.5	2.4	1	2.5	11	3.9	23	3.5	20	3.3	9	3.0	59	21.2	1	·	·	·	6	·	·	2	13	13	10	1	·	·	–
VII	12	2.6	1.5	1.3	4	1.4	4	1.5	7.5	2.3	21.5	2.9	21	3.2	15.5	3.4	6	2.6	63	29.4	18	·	·	·	4		·	4	10	14	9	3	1	·	–
VIII	3.5	2.9	7	1.9	1	2.0	8	1.9	7	2.6	27	2.9	21.5	3.0	10	3.6	8	2.5	32	7.1	1	·	·	·	10	·	·	3	8	13	9	·	4	·	–
IX	0.5	12.0	9.5	1.5	3.5	1.6	2.5	2.0	11.5	2.2	30	3.6	20	3.6	5.5	5.0	7	2.9	31	9.5	5	·	·	·	2	2	·	6	7	12	5	·	5	·	–
X	10.5	2.9	8	1.6	10	1.3	8	2.3	5.5	1.9	17	3.2	13	4.0	10	2.9	11	2.4	5	2.8	29	·	·	13	·	1	·	3	9	5	2	·	15	·	–
XI	3.5	2.7	8	2.7	17.5	3.0	29	2.9	2.5	2.0	12	5.5	8	3.4	7.5	3.7	2	3.3	50	11.3	10	·	·	7	·	1	·	2	21	16	9	2	5	3	–
XII	10	2.4	10.5	3.8	1.5	2.3	8.5	2.1	13.5	2.8	18.5	3.7	16.5	3.5	9	3.8	5	3.1	6	1.6	16	10	18	30	·	1	·	3	18	15	2	·	2	23	–
Rok	85	4.2	80	2.9	85.5	2.2	98.5	2.5	103.5	2.6	218.5	4.1	211	4.3	140	4.4	73	3.3	421	29.4	18. VII	27	59	137	26	25	3	31	163	159	88	9	40	108	–

Śnieżka $H_s = 1603\,m$ $H_b = 1610,6\,m$

I	4	6.5	4.5	18.4	1	14.0	0.5	10.0	2	11.2	37.5	20.1	22	18.6	21.5	18.2	·	18.3	132	18.5	26	6	27	30	·	31	30	1	22	26	23	5	28	31	·
II	6.5	18.6	2	17.0	2.5	7.2	9	9.6	0.5	12.0	11	22.4	16	13.2	36.5	18.9	·	16.8	164	19.2	14	19	28	28	·	28	24	1	21	24	21	8	26	28	·
III	20	13.5	3	9.3	3.5	2.8	2	9.0	4.5	16.2	26.5	13.9	12	11.9	20.5	8.6	1	11.7	128	20.1	30	19	25	31	·	27	21	1	24	25	21	4	28	31	·
IV	17	11.1	2.5	12.4	1.5	8.0	6.5	7.7	10.5	10.9	24	16.8	17	13.2	11	11.4	·	12.8	139	27.6	28	·	17	21	·	29	21	2	19	18	16	4	23	28	2
V	4.5	9.1	0.5	0.6	·	·	·		4	9.4	24.5	13.5	37	11.9	21.5	12.6	1	12.1	134	27.8	14	·	7	23	·	26	24	·	22	27	17	4	19	12	1
VI	14.5	10.0	·	·	·	·	·	·	2	14.0	17.5	10.5	21	11.9	32	10.2	3	10.4	96	33.3	16	·	4	14	·	27	13	·	13	15	9	3	20	6	6
VII	10	9.8	1	3.0	·	·	·	·	1	16.5	25.5	11.0	33	11.9	18.5	8.8	4	10.2	116	36.8	16	·	·	4	·	27	16	·	12	19	15	2	23	·	8
VIII	2.5	14.8	·	·	·	·	1	6.0	4.5	14.8	37.5	15.2	32.5	15.6	11	14.0	4	14.5	52	11.4	13	·	·	·	·	29	28	·	12	16	12	1	23	·	5
IX	4	13.0		·	·	·	1.5	6.0	11	8.9	35.5	17.0	10	15.4	26	11.8	2	13.6	72	18.5	16	·	·	10	·	28	25	1	12	16	11	3	21	2²	·
X	20.5	7.9	3.5	6.1	1.5	5.0	3	4.3	25	7.3	17.5	11.7	5.5	8.4	14.5	12.1	2	8.7	85	30.9	6	·	3	16	·	26	14	10	12	17	11	3	19	6	2
XI	22	9.8	5.5	8.5	·	·	3.5	7.7	20.5	19.3	22	16.6	8	9.6	7.5	10.4	1	13.4	126	26.5	1	4	20	26	·	27	20	·	21	27	24	3	30	25	·
XII	15.5	10.8	6.5	17.6	4.5	12.3	5.5	12.0	8	9.0	20.5	18.5	11.5	11.2	17	12.4	4	12.6	89	10.2	16	17	26	31	·	28	22	3	14	19	17	1	21	31	·
Rok	141	11.2	29	7.7	14.5	4.1	32.5	6.0	93.5	12.5	299.5	15.6	225.5	12.7	237.5	12.4	22	12.9	1333	36.8	16. VII	65	157	234	·	333	258	19	204	249	197	41	281	200²	24

Zamość $H_s = 219\,m$ $H_b = 218,8\,m$ $h_w = 14\,m$

I	1	4.0	4.5	4.3	2.5	4.2	·	·	9	2.7	38.5	3.5	28	3.1	9.5	2.6	·	3.2	30	6.3	13	2	6	24	·	·	·	1	15	17	10	·	·	21	·
II	6	3.7	5.5	3.4	11.5	3.8	8	2.4	6	2.3	11.5	9.3	18	5.1	15.5	5.4	2	4.8	51	9.0	12	6	15	27	·	7	5	·	19	21	13	·	·	28	·
III	5.5	6.5	3.5	3.0	21.5	2.1	9.5	3.7	11	3.0	6	2.8	16	4.5	14	3.3	6	3.2	60	18.8	16	5	13	25	·	2	·	1	19	19	11	1	2	30	·
IV	4.5	4.8	6	3.0	20	2.0	11	2.8	8.5	2.9	10.5	3.2	14	3.0	7.5	4.5	8	2.7	45	12.9	30	·	·	3	5	1	·	7	7	8	7	2	1	·	2
V	5	1.7	3.5	1.9	1	2.0	9	2.4	4.5	2.0	17	3.3	24	3.5	19	2.4	10	2.5	139	21.3	8	·	·	2	·	3	1	1	9	21	15	7	3	·	6
VI	13	3.6	5	1.8	2	2.0	·	·	·	·	11	2.5	20	3.6	29	1.8	10	2.4	72	24.3	1	·	·	·	8	·	·	5	10	11	9	2	·	·	4
VII	6	2.3	7	1.3	2	2.0	5	1.8	5	1.7	15.5	2.2	28.5	2.2	14	3.0	10	2.0	76	20.2	18	·	·	·	5	·	·	5	10	14	12	2	1	·	4
VIII	6.5	1.2	1	1.0	2	1.0	6	2.7	2	2.5	13	2.8	31	2.7	10.5	1.5	21	1.8	46	8.7	3	·	·	·	12	·	·	4	4	15	10	·	4	·	4
IX	·	·	4.5	1.8	5.5	2.4	6	2.0	6.5	3.1	18	3.8	31.5	2.7	7	4.2	11	2.6	50	22.9	5	·	·	·	2	1	1	5	9	16	7	1	6	·	2
X	2	[illegible]	4	1.6	4	2.8	14	1.7	4.5	1.9	7	4.0	15.5	2.5	11	2.7	31	1.6	3	1.6	19	·	·	8	·	·	·	6	6	4	2	·	15	·	·
XI	8.5	1.2	4	2.5	20	4.2	23	3.9	4.5	1.7	8.5	3.1	11.5	2.8	6	2.4	4	3.1	52	9.9	16	·	·	6	·	·	·	3	19	19	11	·	5	1	·
XII	14	2.1	10	3.0	8	2.2	5	1.9	8.5	3.3	15.5	3.5	20	2.5	5	2.2	7	2.5	16	4.1	15	10	17	30	·	2	·	3	21	16	5	·	2	23	·
Rok	72	2.7	58.5	2.4	100	2.6	96.5	2.1	70	2.3	172	3.7	258	3.2	148	3.0	120	2.7	640	24.3	1. VI	23	51	125	32	16	7	41	148	181	112	15	39	103	22

Zamość-Zamczysko $\varphi = 50°44'$ $\lambda = 23°15'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA t										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0,m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	17.8	7.5	28.8	5	0.6	26	10.2	16.0	11.3	12.2	11.1	12.0	12.0	11.7	88	67	88	81	1.8	6.9	1.8	3.5	5.0	5.2	4.8	5.0
X	–	–	–	–	13.3	1.5	19.3	2	–5.6	16	3.3	12.3	5.9	6.8	2.5	10.1	8.7	8.8	95	71	91	86	0.5	4.5	0.8	1.9	6.4	5.8	3.2	5.1
XI	–	–	–	–	7.5	1.4	19.5	1	–5.2	18	3.1	6.3	3.8	4.2	7.2	7.9	7.5	7.5	92	81	91	88	0.6	2.3	0.7	1.2	8.2	8.3	8.4	8.3
XII	–	–	–	–	–2.4	–7.8	4.7	13	–21.9	23	–5.6	–3.7	–5.1	–4.9	3.9	4.4	4.2	4.2	91	88	91	90	0.3	0.6	0.3	0.4	8.2	8.3	7.9	8.1
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Zdanów $\varphi = 50°43'$ $\lambda = 21°33'$

I	–	–	–	–	0.7	–4.4	5.2	20	–18.5	31	–2.4	–0.7	–2.0	–1.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.3	6.5	6.7
II	–	–	–	–	–0.6	–6.1	5.0	13	–13.4	25	–4.4	–2.2	–2.7	–3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.1	8.2	8.3
III	–	–	–	–	0.9	–5.0	11.1	31	–12.2	21	–4.3	–0.4	–2.5	–2.4	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.5	6.4	6.7
IV	–	–	–	–	15.9	5.3	26.4	23	–1.1	7	7.6	14.5	9.4	10.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15.0	6.5	22.9	8	–1.7	1	9.0	13.5	9.7	10.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	18.6	9.0	29.0	23	2.5	2	12.7	16.9	12.8	13.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.0	10.4	28.6	26	5.3	5	14.0	19.5	14.1	15.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	22.1	12.0	29.0	13	7.0	31	14.8	20.6	15.7	16.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	17.1	7.1	26.4	4	1.8	15	9.5	15.6	11.1	11.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	12.7	3.5	19.1	2	–1.9	23	5.0	11.0	6.7	7.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.4	1.7	14.6	1	–2.4	18	2.6	5.2	3.6	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.4	8.0	7.9
XII	–	–	–	–	–2.9	–8.3	2.7	6	–21.4	22	–6.2	–4.2	–5.5	–5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.6	6.4	6.8
Rok	–	–	–	–	10.6	2.6	29.0	23.VI, 13.VIII	–21.4	22. XII	4.8	9.1	5.9	6.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Janów Lubelski $\varphi = 50°43'$ $\lambda = 22°25'$

I	–	–	–	–	1.5	–3.3	6.9	22	–16.8	31	–1.4	1.0	–1.1	–0.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–0.2	–5.8	3.9	7	–12.3	25	–3.4	–0.9	–2.9	–2.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	1.5	–5.4	12.9	5, 31	–11.8	20, 21	–2.5	0.7	–2.2	–1.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	16.0	5.8	26.1	23	–1.4	8	9.5	15.4	9.4	10.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15.1	6.8	22.3	28	–0.9	1, 4	10.5	14.4	10.2	11.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	18.5	9.2	28.9	16, 23, 24	3.1	6, 7	13.3	17.6	13.2	14.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	20.8	10.6	27.7	26	6.2	10, 29	13.6	19.4	15.0	15.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	17.1	7.5	26.9	5	1.1	15	9.2	16.4	12.0	12.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	13.0	2.7	19.1	2, 4	–4.1	17	5.2	12.5	6.7	7.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	7.1	1.9	18.9	1	–2.1	17, 18	3.3	6.3	3.9	4.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–3.1	–7.6	3.9	13	–19.1	22	–5.7	–3.8	–5.7	–5.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–19.1	22. XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Sokołowsko $\varphi = 50°41'$ $\lambda = 16°14'$

I	–	–	–	–	0.3	–4.9	5.4	22	–17.0	31	–2.5	–1.2	–2.3	–2.1	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.5	8.5	8.6
II	–	–	–	–	–0.8	–7.5	4.1	21	–19.8	1	–4.4	–2.2	–3.7	–3.5	–	–	–	–	–	–	–	–	–	–	–	–	9.4	9.2	8.1	8.9
III	–	–	–	–	0.8	–6.8	9.1	31	–15.4	15	–4.6	–0.1	–3.4	–2.9	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.0	6.5	7.7
IV	–	–	–	–	12.5	2.4	25.0	24	–3.7	11	5.7	10.7	5.8	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.7	6.2	6.8
V	–	–	–	–	12.6	3.5	19.8	19	–4.8	1	7.1	10.9	7.1	8.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	8.5	7.3	7.8
VI	–	–	–	–	17.3	6.5	27.2	16	–0.4	8	10.8	15.7	10.4	11.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.9	5.6	5.9
VII	–	–	–	–	18.2	8.1	29.0	26	1.4	9	12.0	16.9	11.5	13.0	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.2	5.8	6.4
VIII	–	–	–	–	20.3	9.0	29.5	13	3.7	31	12.8	18.9	12.5	14.2	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.0	4.6	5.9
IX	–	–	–	–	15.9	5.2	27.2	4	0.4	15	8.0	14.1	9.0	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.7	4.3	6.0
X	–	–	–	–	12.5	3.0	21.3	4	–4.1	22	3.9	10.9	5.4	6.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.0	4.6	5.3
XI	–	–	–	–	4.3	0.5	15.3	8	–8.9	24	1.6	3.0	2.0	2.2	–	–	–	–	–	–	–	–	–	–	–	–	9.2	9.1	9.3	9.2
XII	–	–	–	–	–3.4	–10.1	2.7	16	–21.1	22	–7.5	–5.1	–7.5	–6.9	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.0	7.9	8.1
Rok	–	–	–	–	9.2	0.7	29.5	13.VIII	–21.1	22. XII	3.6	7.7	3.9	4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.6	6.6	7.2

Zamość-Zamczysko $H_s = 212\,m$ $h_w = 14{,}5\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU nD, vmD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◉	●	Opad R R > 0.1	R > 1.0	R > 10.0	≡	⊞	R f0
I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
V	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	·	·	2	2.0	6	1.3	5.5	1.7	12.5	3.1	23.5	3.4	21.5	3.9	4	4.9	15	2.8	38	16.7	5	·	·	·	2	·	·	8	6	11	7	1	8	·	2
X	3.5	2.4	5.5	3.2	12.5	2.7	11.5	1.8	1	2.5	12	3.8	15.5	3.9	10.5	3.2	21	2.4	5	2.2	19	·	·	13		·	·	4	7	4	2	·	15	·	·
XI	1.5	2.0	8.5	4.6	22	5.8	15.5	5.2	4.5	3.3	12	2.8	7.5	3.9	11.5	3.2	7	4.1	44	9.4	16		·	8	·	3	·	3	20	18	10	·	6	1	·
XII	11	2.6	9.5	3.6	9.5	2.5	8	2.9	5.5	4.4	18	4.3	17.5	3.3	5	3.3	9	3.1	16	3.2	14	10	19	30	·	·	·	2	23	15	6	·	2	23	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Zdanów $H_s = 236\,m$ $h_w = 15\,m$

I	8	8.1	1.5	7.0	·	·	0.5	1.0	22.5	4.0	28	4.3	20.5	4.6	7	6.2	5	4.5	25	6.3	25	2	9	30	·	3	·	2	13	9	6	·	3	—	—
II	9.5	5.8	9.5	3.2	10.5	3.8	4.5	3.8	6	6.1	9.5	7.1	17	6.2	14.5	8.9	3	5.7	26	6.2	12	1	14	27	·	8	2	·	18	13	11	·	·	—	—
III	20.5	5.0	8	4.0	8	3.1	12	4.2	10.5	3.3	3	4.5	10	6.8	10	4.8	11	4.0	37	9.5	16	4	16	28	·	4	·	4	15	15	11	·	3	—	—
IV	17	3.6	11.5	3.6	8	4.0	7.5	6.2	11	4.4	8.5	3.4	6.5	4.1	7	5.7	13	3.6	31	7.0	27	·	·	4	4	3	2	—	—	11	8	·	—	·	—
V	11	3.5	3	1.5	4.5	2.4	5	3.8	7.5	4.3	11.5	4.4	16	3.9	15.5	4.0	19	3.1	114	21.4	14	·	·	1	·	3	1	—	—	25	20	3	3	·	—
VI	17.5	4.3	2	4.7	0.5	1.0	3	1.1	3	1.7	6	2.8	15	4.2	25	3.7	18	2.9	108	41.4	4	·	·	·	6	2	·	—	—	9	7	3	·	·	—
VII	11	2.3	2	1.7	0.5	3.0	5	2.2	5.5	2.5	8	2.8	20.5	3.3	20.5	2.8	20	2.2	73	21.0	18	·	·	·	4	·	·	—	—	13	9	3	1	·	—
VIII	6	2.1	1	1.0	4.5	2.8	3	1.8	4.5	4.2	10	2.4	29	3.6	15	3.5	20	2.5	55	23.8	5	·	·	·	7	3	·	—	—	12	6	2	1	·	—
IX	2	2.8	6	2.4	3.5	3.1	4.5	1.9	5	2.1	15.5	3.6	23	3.7	11.5	4.0	19	2.6	61	20.0	18	·	·	·	2	·	·	—	—	12	8	2	4	·	—
X	8.5	3.5	6.5	1.7	8.5	1.9	4	2.8	1	1.0	5.5	3.7	15.5	3.4	7.5	3.1	36	1.8	1	0.4	14	·	·	7	·	1	·	—	—	4	·	·	10	·	—
XI	13	4.6	4.5	5.8	21.5	4.7	15	4.6	1.5	4.0	2.5	5.8	10	4.7	6	3.2	16	3.8	47	13.8	15	·	1	7	·	1	·	2	19	13	10	1	12	—	—
XII	19	4.7	7	3.8	2.5	4.2	3.5	4.0	9.5	5.8	8	3.9	15.5	3.4	9	4.3	19	3.4	15	4.2	14	11	19	30	·	3	·	3	14	11	5	·	4	—	—
Rok	143	4.2	62.5	3.4	72.5	2.8	67.5	3.1	87.5	3.6	116	4.1	198.5	4.3	148.5	4.5	199	3.3	593	41.4	4.VI	18	59	134	23	31	5	—	—	147	101	14	—	—	—

Janów Lubelski $H_s = 230\,m$ $h_w = 20{,}1\,m$

I	4	3.5	4	1.3	1	2.0	12	1.8	44	2.0	9	1.8	9	1.9	3	2.0	7	1.8	30	8.0	25	2	9	27	·	·	·	—	—	11	8	·	—	—	—
II	5	1.6	3	2.0	13	1.4	4	5.5	12	3.0	11	3.1	30	3.6	2	6.5	4	2.9	26	8.0	20	2	13	26	·	3	·	—	—	16	10	·	—	—	—
III	6	2.0	11.5	2.4	21	2.1	1	2.0	13	2.4	7	3.7	11	2.9	4.5	3.0	18	2.0	42	8.2	12	6	17	27	·	1	·	—	—	12	11	·	—	—	—
IV	12	1.2	10	1.5	16	2.4	5	1.8	19	2.0	4	3.0	11	3.5	·	·	13	1.8	24	7.0	6	·	·	5	4	·	·	—	—	8	7	·	—	·	—
V	8	1.4	1	1.0	15	1.4	5	2.2	17	2.6	5	1.4	27	1.9	3	2.0	12	1.6	119	17.5	15	·	·	3	·	1	·	—	—	24	20	4	—	·	—
VI	9	1.9	3	1.3	3	1.3	·	·	9	3.3	9	2.7	29	1.6	12	1.8	16	1.6	93	30.2	4	·	·	·	3	·	·	—	—	11	10	3	—	·	—
VII	8	1.1	2	1.0	1	1.0	4	1.2	16	1.3	12	1.8	30	1.6	5	1.0	15	1.2	90	28.0	19	·	·	·	4	·	·	—	—	14	11	3	—	·	—
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	51	22.5	5	·	·	·	—	—	—	—	—	7	6	2	—	·	—
IX	2	2.5	9	1.3	7	1.3	8	1.2	22	2.2	6	2.1	18	2.4	2	2.0	16	1.6	53	19.0	19	·	·	·	2	·	·	—	—	13	10	1	—	·	—
X	17	1.5	14	1.2	14	1.4	1	1.0	8	2.2	5	3.4	12	2.1	1	4.0	21	1.4	1	0.3	20	·	·	9	·	·	·	—	—	2	·	·	—	·	—
XI	4	1.2	8	5.1	32	2.7	3	1.3	7	2.6	2	1.5	14	2.1	11	3.2	9	2.4	58	13.8	25	·	1	6	·	·	·	—	—	15	11	2	—	—	—
XII	9	2.6	13	2.0	6	2.0	4	4.8	18	2.6	15	1.6	14	1.7	9	1.6	5	1.9	28	12.0	14	11	23	31	·	·	·	—	—	9	7	1	—	—	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	615	30.2	4.VI	21	63	134	—	—	—	—	—	142	111	16	—	—	—

Sokołowsko $H_s = 570\,m$

I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	60	13.0	26	5	10	26	·	—	—	·	21	19	10	1	2	31	·
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	70	12.2	12	8	13	27	·	—	—	·	20	21	15	1	·	28	·
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	70	22.8	31	6	13	29	·	—	—	1	17	20	9	2	·	31	·
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	61	10.8	28	·	·	8	·	—	—	4	16	14	12	2	1	4	2
V	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	120	28.4	14	·	·	5	·	—	—	·	16	25	18	3	·	1	2
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	60	25.2	19	·	·	1	5	—	—	3	7	11	9	1	·	·	3
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	80	18.4	27	·	·	·	2	—	—	1	13	16	12	3	·	·	4
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	37	6.2	31		·	·	3	—	—	2	11	16	11	·	1	·	4
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	68	17.6	18	·	·	·	2	—	—	5	10	14	11	3	2	·	·
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	51	23.7	31	·	·	6	·	—	—	10	12	13	6	2	8	·	·
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	58	15.7	1	·	4	16	·	—	—	·	25	18	11	1	7	12	·
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	50	8.2	17	17	20	31	·	—	—	2	21	19	10	·	1	31	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	785	28.4	14.V	36	60	149	12	—	—	28	189	206	134	19	22	138	15

Grodków $\varphi = 50°41'$ $\lambda = 17°23'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA t										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.7	-2.2	11.7	22	-19.0	31	-0.1	2.3	0.3	0.7	5.3	5.8	5.4	5.5	8.3	7.7	8.3	8.1	1.1	1.7	1.2	1.3	7.0	6.3	6.8	6.7
II	–	–	–	–	2.0	-4.3	8.5	12	-15.2	1	-1.8	0.2	-1.2	-1.0	4.5	5.0	4.9	4.8	8.1	8.0	8.3	8.1	1.0	1.3	1.0	1.1	8.2	8.9	6.8	8.0
III	–	–	–	–	3.7	-2.8	15.5	31	-6.3	15	-1.5	2.5	0.0	0.2	4.9	5.1	5.1	5.0	8.8	6.8	8.1	7.9	0.7	2.4	1.1	1.4	7.4	7.2	5.7	6.8
IV	–	–	–	–	16.0	5.9	27.5	23	1.2	2	8.4	14.5	9.8	10.6	9.0	8.2	8.8	8.7	8.0	5.3	7.1	6.8	2.4	10.2	4.1	5.6	7.0	6.7	6.3	6.7
V	–	–	–	–	15.9	6.8	23.2	8	-0.3	1	9.7	14.1	10.4	11.2	10.1	10.0	10.7	10.3	8.3	6.2	8.3	7.6	2.1	6.7	2.2	3.7	6.6	7.4	7.3	7.1
VI	–	–	–	–	20.5	10.0	30.3	16	3.2	6	13.5	16.9	14.3	15.2	12.2	11.9	12.7	12.3	7.6	5.3	7.5	6.8	3.9	11.4	4.1	6.5	5.5	6.1	5.5	5.7
VII	–	–	–	–	21.6	11.0	32.3	26	6.4	30	14.4	20.2	15.0	16.2	13.9	13.6	14.4	14.0	8.3	5.7	8.4	7.5	2.9	10.8	3.0	5.6	5.5	5.5	6.4	5.8
VIII	–	–	–	–	23.8	12.2	31.7	13	6.8	31	15.7	22.1	15.9	17.4	14.6	14.5	15.3	14.8	8.1	5.5	8.3	7.3	3.4	12.8	3.0	6.4	6.1	6.5	4.7	5.8
IX	–	–	–	–	18.8	7.8	31.7	4	2.6	27	10.2	17.1	11.4	12.5	10.8	11.3	11.0	11.0	8.6	6.1	8.3	7.7	2.1	9.3	2.8	4.7	6.7	6.4	3.8	5.6
X	–	–	–	–	14.0	4.2	24.0	3	-2.9	22	5.7	12.7	7.1	8.2	9.0	10.3	9.4	9.6	9.5	7.1	9.1	8.6	0.5	5.0	1.0	2.2	6.5	5.4	4.4	5.4
XI	–	–	–	–	7.2	2.5	17.3	8	-1.8	24	3.4	6.2	4.3	4.6	7.3	8.2	7.5	7.7	9.2	8.4	8.9	8.8	0.7	1.8	1.1	1.2	8.5	8.9	6.7	8.0
XII	–	–	–	–	-0.8	-6.8	6.0	12	-19.6	22	-5.2	-2.0	-4.2	-3.9	4.0	4.6	4.3	4.3	8.6	8.1	8.7	8.5	0.5	1.0	0.6	0.7	8.7	8.0	7.7	8.1
Rok	–	–	–	–	12.2	3.7	32.3	26.VII	-19.6	22.XII	6.0	10.7	6.9	7.6	8.8	9.0	9.1	9.0	8.4	6.7	8.3	7.8	1.8	6.2	2.1	3.4	7.0	6.9	6.0	6.6

Sandomierz $\varphi = 50°41'$ $\lambda = 21°45'$

I	992.7	1012.0	970.8	1017.8	1.4	-3.7	6.5	22	-17.4	31	-1.7	0.2	-1.5	-1.1	4.9	5.0	4.8	4.9	8.7	7.8	8.5	8.3	0.7	1.4	0.8	1.0	7.5	6.5	6.8	6.9
II	991.0	1008.2	962.0	1016.3	0.0	-5.3	6.2	13	-12.1	25	-3.9	-1.4	-2.5	-2.6	3.9	4.3	4.4	4.2	8.4	7.6	8.4	8.1	0.8	1.3	0.8	1.0	8.6	9.1	8.0	8.6
III	986.6	1003.8	968.0	1011.7	2.1	-4.7	13.4	5	-11.5	21	-3.6	0.7	-1.5	-1.5	4.3	4.7	4.8	4.6	8.7	6.9	8.3	8.0	0.6	2.0	0.9	1.2	7.7	7.3	6.9	7.3
IV	990.1	1003.2	966.2	1014.3	16.9	6.0	27.2	23	-0.6	8	7.9	15.2	10.6	11.1	8.8	8.4	8.7	8.6	8.2	5.2	6.9	6.8	2.2	10.4	4.9	5.8	6.1	5.9	4.7	5.6
V	989.3	996.8	975.4	1013.3	16.0	7.2	23.0	8	-1.5	1	9.3	14.2	10.7	11.2	10.9	11.2	11.4	11.2	9.1	6.8	8.7	8.2	1.0	5.6	1.8	2.8	8.1	8.4	6.6	7.7
VI	993.8	1003.1	983.8	1017.7	19.0	9.8	29.4	16	3.2	6	12.7	17.5	13.8	14.4	12.6	12.2	12.7	12.5	8.4	6.2	7.8	7.5	2.7	9.3	4.0	5.3	5.5	6.9	5.3	5.9
VII	991.1	1001.7	979.1	1014.8	21.6	11.3	28.7	26	7.4	5	13.8	20.2	15.3	16.2	13.9	13.9	14.3	14.0	8.8	5.9	8.2	7.6	2.0	10.3	3.4	5.2	6.0	5.6	5.4	5.7
VIII	992.7	1000.5	982.9	1016.2	23.0	12.7	30.0	7, 13	6.3	31	14.5	21.4	17.0	17.5	15.0	15.3	15.9	15.4	8.9	6.1	8.1	7.7	1.8	10.8	3.9	5.5	6.2	6.3	4.5	5.7
IX	993.2	1006.2	979.4	1017.2	17.8	7.9	27.5	4	2.6	15	9.2	16.2	11.7	12.2	10.7	11.9	11.9	11.5	9.1	6.6	8.6	8.1	1.2	7.2	2.3	3.6	5.6	6.6	4.8	5.7
X	998.7	1012.2	986.2	1023.2	13.1	3.3	20.4	2	-3.8	16	4.5	11.6	7.2	7.6	8.3	10.0	9.2	9.2	9.5	7.2	8.8	8.5	0.4	4.0	1.2	1.9	6.9	5.6	3.1	5.2
XI	993.4	1007.7	978.6	1018.1	6.8	2.0	16.1	1	-2.3	18	3.1	5.8	4.1	4.3	7.2	7.7	7.5	7.5	9.2	8.2	9.0	8.8	0.6	1.9	0.9	1.1	9.0	8.5	8.7	8.7
XII	992.3	1019.3	950.7	1017.8	-2.3	-7.6	3.9	13	-21.1	22	-5.7	-3.7	-5.1	-4.9	3.6	4.0	3.8	3.8	8.5	8.2	8.4	8.4	0.6	0.9	0.7	0.7	7.5	7.5	7.2	7.4
Rok	992.1	1019.3	950.7	1016.5	11.3	3.2	30.0	7.13.VIII	-21.1	22.XII	5.0	9.8	6.6	7.0	8.7	9.0	9.1	8.9	8.8	6.9	8.3	8.0	1.2	5.4	2.1	2.9	7.1	7.0	6.0	6.7

Opole $\varphi = 50°40'$ $\lambda = 17°58'$

I	995.9	1015.6	972.1	1018.3	2.8	-2.3	9.2	20	-17.5	31	-0.8	1.5	-0.3	0.0	5.1	5.6	5.2	5.3	8.5	8.0	8.4	8.3	0.9	1.5	1.0	1.1	7.3	7.9	7.3	7.5
II	995.4	1013.1	966.9	1018.0	1.7	-4.8	8.5	12, 13	-15.2	3	-3.3	-0.4	-1.6	-1.7	4.2	4.7	4.7	4.5	8.5	7.7	8.4	8.2	0.8	1.4	0.9	1.0	8.2	8.8	6.4	7.8
III	989.8	1007.1	970.3	1012.1	3.9	-3.6	16.0	31	-8.1	15	-2.6	2.1	-0.4	-0.3	4.6	5.0	5.1	4.9	8.7	6.9	8.2	7.9	0.7	2.4	1.1	1.4	7.6	7.6	6.1	7.1
IV	993.0	1004.9	967.9	1014.6	16.4	5.6	28.0	23	0.8	2	8.0	14.7	9.8	10.6	8.8	8.3	8.8	8.6	8.1	5.4	7.3	6.9	2.4	10.3	4.0	5.6	7.1	7.0	6.1	6.7
V	992.7	998.6	981.1	1014.1	16.2	6.5	24.0	8	-2.1	1	9.5	13.9	10.4	11.0	10.5	10.9	11.0	10.8	8.7	6.9	8.6	8.1	1.5	5.5	1.9	3.0	7.6	8.2	7.4	7.7
VI	998.0	1007.7	987.6	1019.2	20.8	9.5	31.6	23	2.9	6	13.4	18.9	14.8	15.5	12.5	12.2	12.2	12.3	7.9	5.5	7.1	6.8	3.5	11.2	5.5	6.7	5.9	7.0	6.0	6.3
VII	994.5	1003.8	981.9	1015.6	21.9	10.8	32.0	26	5.8	30	14.1	20.1	15.4	16.2	13.7	14.4	13.9	14.0	8.5	6.1	7.9	7.5	2.6	9.9	3.8	5.4	6.1	6.2	6.3	6.2
VIII	995.7	1003.1	982.2	1016.7	24.1	12.5	31.8	13	6.8	31	15.3	22.3	16.8	17.8	14.6	15.0	15.2	14.9	8.3	5.6	7.9	7.3	3.1	12.7	4.2	6.7	6.9	6.9	5.7	6.5
IX	996.0	1007.2	981.4	1017.4	18.7	7.6	30.9	4	0.5	15	9.9	16.8	11.9	12.6	10.9	12.5	11.3	11.6	8.8	5.6	8.2	7.9	1.7	8.0	3.1	4.3	6.8	6.7	4.0	5.8
X	1001.3	1013.3	988.6	1023.2	13.6	3.8	23.8	3	-3.4	22	5.3	12.3	7.1	8.0	9.0	10.6	9.6	9.7	9.7	7.4	9.3	8.8	0.3	4.4	0.8	1.8	7.7	5.5	4.0	5.7
XI	995.1	1011.5	979.0	1017.2	6.8	2.3	17.4	8	-2.9	24	3.1	6.0	3.9	4.2	7.2	7.9	7.4	7.5	9.2	8.3	9.1	8.9	0.6	2.0	0.8	1.1	8.1	8.2	8.3	8.2
XII	995.4	1022.9	955.2	1018.2	-1.5	-2.3	6.2	13	-21.7	22	-5.6	-2.8	-4.8	-4.5	3.8	4.5	4.0	4.1	8.8	8.5	8.7	8.7	0.5	0.8	0.6	0.6	7.6	7.6	6.6	7.3
Rok	995.2	1022.9	955.2	1017.0	12.1	3.4	32.0	26.VII	-21.7	22.XII	5.5	10.4	6.9	7.4	8.7	9.3	9.0	9.0	8.6	6.9	8.3	7.9	1.6	5.8	2.3	3.2	7.2	7.3	6.2	6.9

Lubliniec $\varphi = 50°40'$ $18°41'$

I	–	–	–	–	2.2	–	8.2	20	–	–	-1.5	1.3	-0.9	-0.5	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.1	6.8	7.0
II	–	–	–	–	0.6	-5.5	6.3	13	-16.1	3	-3.4	-0.7	-2.2	-2.1	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.9	7.3	8.5
III	–	–	–	–	3.2	-4.4	15.1	31	-9.6	14	-2.5	2.3	-1.0	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.7	6.5	7.1
IV	–	–	–	–	15.7	5.6	29.3	22	0.4	2, 3	8.6	14.5	9.3	10.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15.2	6.3	22.5	8	-2.2	3	9.7	13.5	9.9	10.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	19.9	9.1	30.6	16	2.6	2	13.1	18.7	13.7	14.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.1	10.4	30.8	26	6.3	30	14.6	20.0	14.6	16.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	23.1	12.0	31.3	7	5.9	31	15.5	22.3	15.6	17.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	17.5	7.4	28.8	4	1.7	15	10.2	16.3	10.9	12.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	13.2	4.1	23.0	3	-2.3	22	6.3	12.7	6.8	8.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.7	2.2	18.7	8	-2.0	24	3.4	6.3	3.8	4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.0	8.0	8.2
XII	–	–	–	–	-2.1	-7.6	7.6	13	-19.2	22	-5.3	-2.7	-4.8	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	9.1	7.6	8.3	8.3
Rok	–	–	–	–	11.4	–	31.3	7.VIII	-19.2	22.XII	5.7	10.4	6.3	7.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Grodków $H_s = 176\,m$ $h_w = 13{,}5\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU °D, v m/s N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Max < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15			Opad R ≥ 0.1	≥ 1.0	≥ 10.0			
I	7.5	37	0.5	30	1	10	3.5	26	15	32	38	3.5	11	4.2	12.5	42	4	3.5	29	6.2	24	1	4	18	·	1	·	·	9	12	9	·	3	15	·
II	7	29	4	20	8.5	25	1	2.5	10	26	13.5	5.2	18.5	5.4	19.5	45	2	4.0	23	4.5	18	5	10	22	·	3	1	·	16	13	9	·	·	17	·
III	10.5	34	8	28	5.5	24	7.5	4.0	9.5	22	14	2.5	12.5	3.0	22.5	34	3	2.9	62	19.7	12	·	7	25	·	2	·	1	13	14	9	2	6	10	
IV	9	27	6.5	22	2	4.0	4	4.5	16.5	38	15	3.2	15	3.5	20	36	2	3.3	36	11.8	4	·	·	·	7	1	·	3	13	12	8	1	1	·	1
V	7	13	1	1.0	1	4.0	3.5	21	10	2.5	19.5	1.8	25.5	2.5	18.5	36	7	2.3	120	29.8	14	·	·	1	·	·	·	2	13	24	16	3	·	·	2
VI	10.5	3.0	1	1.0	2	2.0	3.5	16	3.5	24	10	2.0	24	2.8	27.5	3.0	8	2.4	28	8.8	16	·	·	·	8	·	·	5	7	9	7	·	·	·	1
VII	6	1.4	3	1.0	1.5	2.3	4	2.0	5.5	1.7	20.5	2.2	18.5	1.9	2.0	2.1	14	1.7	70	15.1	2	·	·	·	7	·	·	5	8	15	12	2	·	·	7
VIII	7.5	1.7	2.5	1.0	0.5	1.0	2	1.5	8.5	1.7	15.5	2.7	28.5	2.2	17	2.8	11	2.0	39	7.2	24	·	·	·	11	·	·	2	7	12	9	·	2	·	4
IX	4.5	1.0	1.5	1.0	6.5	2.4	4	1.4	8	1.3	19	2.3	20.5	2.5	15	3.1	11	2.0	66	26.6	18	·	·	·	4	·	·	5	8	10	6	2	8	·	·
X	5	2.6	4.5	1.7	6	1.5	7	1.0	12.5	1.5	5	2.3	10.5	1.6	22.5	2.1	20	1.4	34	23.6	31	·	·	4	·	·	·	10	12	10	3	1	21	·	·
XI	4.5	1.6	8.5	1.6	5.5	2.6	1.6	6.2	8	1.8	12	2.3	11.5	2.8	12	1.9	12	2.6	49	12.1	19	·	·	8	·	2	·	·	18	14	9	1	10	1	·
XII	5.5	2.6	4	1.8	3.5	2.1	4	1.5	10	2.2	19	2.8	14.5	2.2	12.5	2.4	20	1.9	29	5.0	17	10	14	27	·	·	·	2	19	12	9	·	8	16	·
Rok	84.5	2.3	4.5	1.7	43.5	2.3	6.0	2.6	117	2.2	201	2.7	210.5	2.9	219.5	3.1	114	2.5	585	29.8	14.V	16	35	105	37	9	1	35	143	157	106	12	59	59	15

Sandomierz $H_s = 202\,m$ $H_b = 200{,}3\,m$ $h_w = 20{,}1\,m$

I	4.5	6.4	4	4.8	·	·	·	·	13	4.0	4.9	4.1	15	4.4	7.5	4.4	·	4.3	27	6.8	25	2	8	28	·	3	·	2	14	13	7	·	3	25	·
II	10.5	4.5	6	3.3	10	3.0	4	2.8	6	4.4	18	6.1	17	5.6	11.5	6.5	1	4.9	43	9.4	17	2	14	27	·	8	3	·	20	19	13	·	·	28	1
III	16	4.2	11	4.8	4.5	3.2	13.5	2.7	11.5	2.5	14.5	2.9	9.5	5.4	9.5	3.8	3	3.5	56	19.7	16	3	10	27	·	7	2	1	17	17	13	1	·	26	·
IV	11	3.4	13.5	2.7	4.5	3.2	15	2.6	10.5	4.0	15	4.4	7	3.9	9.5	5.2	4	3.5	46	21.5	11	·	·	3	4	2	·	5	8	9	7	1	1	·	1
V	11	2.8	4	1.8	1.5	1.7	4	3.0	3.5	2.8	2.7	3.7	2.2	3.5	13	2.7	7	3.0	114	14.6	24	·	·	2	·	3	2	1	15	26	18	4	5	·	5
VI	22.5	3.2	2	1.8	1.5	1.7	2.5	1.8	1.5	2.0	11	3.2	19	3.9	2.4	3.5	6	3.1	104	38.2	4	·	·	·	6	4	1	3	7	11	9	3	·	·	3
VII	9	2.4	4	2.8	·	·	1	1.5	8	1.9	2.5	2.9	19	3.2	20	2.6	7	2.5	74	33.0	18	·	·	·	4	·	·	2	7	12	10	2	2	·	6
VIII	7.5	1.6	1.5	1.3	2	2.5	6	1.1	3	2.7	22	3.2	3.0	3.3	12	2.7	9	2.5	30	7.6	5	·	·	·	8	1	·	2	6	10	6	·	4	·	2
IX	5	1.6	3.5	2.4	5	2.0	4	2.1	6.5	1.8	24.5	3.2	2.7	3.1	10.5	3.1	4	2.7	52	17.8	18	·	·	·	2	·	·	6	10	14	8	2	4	·	2
X	12	2.3	6.5	2.2	7	1.6	13.5	1.4	5	1.2	14.5	3.3	14.5	2.6	11	3.0	9	2.1	3	0.8	14	·	·	8	·	·	·	6	7	8	·	·	14	·	·
XI	11	3.1	6.5	4.6	18.5	4.0	20.5	3.8	3	2.3	11	4.2	8.5	3.5	7	3.4	4	3.6	56	18.0	15	·	·	7	·	·	·	·	21	16	12	1	9	3	·
XII	13	3.3	12	6.0	4	3.1	2.5	2.4	15.5	2.7	24.5	3.6	12.5	3.0	7	2.7	2	3.5	17	4.1	18	11	15	31	·	1	·	2	15	12	4	·	7	17	·
Rok	13.3	3.2	7.4.5	3.2	58.5	2.2	86.5	2.1	87	2.7	256	3.7	201	3.8	142.5	3.6	56	3.3	622	38.2	4.VI	18	47	133	24	29	8	30	147	167	107	14	49	99	20

Opole $H_s = 176\,m$ $H_b = 177{,}9\,m$ $h_w = 13{,}5\,m$

I	5.5	7.2	0.5	9.0	·	·	1.5	2.3	3.9	3.8	2.0	3.1	1.3	3.8	10.5	4.2	3	3.8	42	9.3	25	2	5	19	·	8	2	·	14	14	10	·	1	9	·
II	7	4.4	4	2.8	8.5	2.2	2	1.2	15.5	2.6	4	5.9	19.5	6.6	18.5	4.6	5	4.1	36	5.9	5	5	9	24	·	6	4	1	15	20	11	·	2	18	·
III	2.0	4.7	1.0	2.6	3	1.7	10.5	2.8	15.5	2.2	2.5	2.6	8	5.9	21.5	2.6	2	3.2	41	12.4	12	·	7	25	·	5	2	2	12	14	10	1	2	11	·
IV	8	2.9	9	2.6	2.5	3.6	13.5	4.4	20.5	2.8	8	2.5	10.5	3.6	18	3.2	·	3.2	2.6	6.9	4	·	·	·	8	3	·	4	14	13	8	·	·	·	1
V	2.5	1.8	1.5	1.0	0.5	1.0	4	1.9	14	1.9	19	1.8	27.5	3.5	2.4	2.7	·	2.5	146	28.6	13	·	·	2	·	2	·	·	14	2.5	22	5	3	·	6
VI	9	3.1	3	1.8	·	·	1	2.0	5	1.6	6.5	1.9	3.4	2.8	26.5	3.4	5	2.7	21	9.4	1	·	·	·	8	1	1	2	9	8	4	·	·	·	2
VII	2.5	1.8	2	1.0	0.5	2.0	2	2.2	12	2.1	18	1.8	2.8	2.0	21	2.0	7	1.8	69	10.0	2	·	·	·	8	·	·	4	9	15	15	1	1	·	8
VIII	·	·	2.5	1.0	1	1.5	2	2.8	8	3.6	16.5	2.4	44.5	2.6	13.5	2.0	5	2.4	54	17.3	17	·	·	·	14	1	·	1	8	12	8	2	3	·	4
IX	1	2.0	·	·	9.5	1.3	5	2.1	16.5	2.1	15.5	2.4	16	2.6	15.5	2.5	11	2.0	57	18.9	18	·	·	·	5	·	·	4	9	9	8	3	3	·	·
X	·	·	5	2.0	5.5	1.0	8.5	1.4	11	1.7	2.5	3.0	15.5	2.2	2.6	1.7	19	1.4	33	17.4	31	·	·	6	·	·	·	5	9	9	6	1	23	·	·
XI	0.5	4.0	11.5	2.5	1.5	2.3	2.0	2.8	7.5	4.3	7	2.3	16	2.0	11	1.7	15	2.1	55	13.6	15	·	1	7	·	·	·	1	21	15	10	2	6	·	·
XII	1.6	2.7	9.5	2.4	1	1.5	5.5	3.9	2.2	3.8	5	2.5	10	2.0	4	2.1	2.0	2.3	36	8.6	15	10	17	28	·	2	·	1	15	18	8	·	9	16	·
Rok	7.2	2.9	58.5	2.4	33.5	1.5	75.5	2.5	186.5	2.7	174.5	2.7	242.5	3.3	210	2.7	92	2.6	615	28.6	13.V	17	39	111	43	28	9	25	149	172	120	15	53	54	21

Lubliniec $H_s = 256\,m$ $h_w = 12{,}5\,m$

I	1.1	4.0	2.5	2.6	·	·	1.5	1.3	3.4.5	1.9	2.3.5	2.5	9.5	4.2	7.5	5.9	3	2.8	5.7	7.9	24	–	5	–	·	1	·	·	10	17	12	·	·	–	·
II	10.5	2.5	5	2.5	6	2.8	1.5	1.3	12	1.9	9	4.1	17.5	5.6	14.5	6.6	8	3.7	47	8.5	12	4	13	2.6	·	5	·	·	18	20	10	·	3	–	·
III	1.6	4.4	7	3.5	13.5	1.4	14.5	1.7	10	1.8	6.5	3.4	11	2.9	8.5	2.9	6	2.5	62	15.0	5	·	8	2.4	·	2	·	·	12	19	11	2	·	–	·
IV	1.4	1.9	5.5	2.5	8	2.4	3	1.8	14.5	2.4	8.5	2.8	12	2.4	12.5	4.0	12	2.2	51	12.6	2.6	·	·	·	7	1	·	–	–	12	10	1	·	·	·
V	3.5	1.6	2	1.8	8.5	1.2	4	1.1	9.5	2.0	13	1.4	19.5	3.6	14	5.2	19	2.2	125	15.4	2.0	·	·	2	·	2	1	–	–	23	21	4	1	·	3
VI	1.3	4.1	3	1.2	4.5	2.1	3	2.3	9.5	1.4	4	1.6	2.4	3.2	2.0	3.5	9	2.7	49	18.0	1	·	·	·	6	2	·	–	–	13	6	2	·	·	2
VII	1.5	1.6	6.5	1.3	4	1.2	6.5	1.5	14	1.2	1.2	1.5	17	1.9	11	2.4	7	1.5	66	10.4	27	·	·	·	6	·	·	–	–	19	14	1	·	·	5
VIII	3.5	1.0	5	2.3	6	1.4	7.5	1.7	13.5	1.7	15.5	2.7	27.5	2.7	13.5	3.3	1	2.4	65	27.5	15	·	·	·	9	1	·	–	–	16	9	1	2	·	5
IX	1.0	1.9	1	1.0	1.3	1.7	5	1.6	18	2.2	13.5	3.0	15.5	2.9	10	2.6	4	2.2	60	24.6	17	·	·	·	4	1	·	–	–	14	8	2	4	·	·
X	1.1	1.3	6	3.0	12.5	1.3	17.5	1.4	14.5	1.7	4	3.2	12	2.6	10.5	2.8	5	1.8	31	15.6	6	·	·	7	·	·	·	–	–	7	3	1	2.2	·	·
XI	8.5	1.6	4.5	3.9	14.5	2.1	2.2.5	1.6	10.5	1.3	9	4.9	7	2.9	7.5	2.1	6	1.8	55	16.4	15	·	1	10	·	·	·	1	22	17	9	1	7	–	·
XII	11.5	2.2	1.0	3.0	5.5	2.9	5	1.2	11.5	3.9	19.5	3.2	15	2.9	6	2.1	9	2.6	39	10.4	15	10	17	28	·	1	1	·	19	14	8	1	7	–	·
Rok	127.5	2.3	58	2.4	96	1.7	31.5	1.5	172	2.0	138	2.6	187.5	3.2	135.5	3.6	89	2.4	707	27.5	15.VIII	–	44	–	32	16	2	–	–	191	121	16	46	–	15

Ostroszowice $\varphi = 50°39'$ $\lambda = 16°38'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.7	-2.4	9.7	22	-15.4	31	-0.5	1.2	-0.1	0.1	–	–	–	–	–	–	–	–	–	–	–	–	74	67	79	73
II	–	–	–	–	0.8	-4.3	5.7	12	-12.9	1	-2.7	-0.8	-1.6	-1.7	–	–	–	–	–	–	–	–	–	–	–	–	90	91	86	89
III	–	–	–	–	2.5	-3.8	13.4	31	-8.4	19	-2.5	1.1	-1.2	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	77	74	70	74
IV	–	–	–	–	13.9	5.1	25.9	23, 24	0.1	11	7.3	12.2	8.7	9.2	–	–	–	–	–	–	–	–	–	–	–	–	67	71	67	68
V	–	–	–	–	14.5	5.9	21.3	31	-1.7	1	8.8	12.5	9.2	9.9	–	–	–	–	–	–	–	–	–	–	–	–	75	79	77	77
VI	–	–	–	–	18.9	9.2	28.8	16	2.4	6	12.9	17.4	12.8	14.0	–	–	–	–	–	–	–	–	–	–	–	–	54	60	52	55
VII	–	–	–	–	20.0	10.4	30.7	26	4.0	9	13.9	18.4	13.3	14.7	–	–	–	–	–	–	–	–	–	–	–	–	58	67	61	62
VIII	–	–	–	–	22.2	11.7	29.9	13	6.4	10	15.1	20.5	14.6	16.2	–	–	–	–	–	–	–	–	–	–	–	–	57	68	52	59
IX	–	–	–	–	17.7	7.8	29.5	4	1.1	15	10.0	15.9	11.5	12.2	–	–	–	–	–	–	–	–	–	–	–	–	67	62	51	60
X	–	–	–	–	13.2	4.5	23.9	4	-1.9	22	6.3	11.9	7.5	8.3	–	–	–	–	–	–	–	–	–	–	–	–	63	54	64	60
XI	–	–	–	–	5.4	1.6	16.7	8	-5.1	24	2.5	4.6	3.2	3.4	–	–	–	–	–	–	–	–	–	–	–	–	82	82	83	82
XII	–	–	–	–	-1.5	-7.6	7.4	7	-18.8	21	-5.5	-3.2	-5.2	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	80	71	76	76
Rok	–	–	–	–	10.9	3.2	30.7	26.VII	-18.8	21.XII	5.5	9.3	6.1	6.8	–	–	–	–	–	–	–	–	–	–	–	–	70	70	68	69

Szczekociny $\varphi = 50°38'$ $\lambda = 19°49'$

I	–	–	–	–	2.0	-3.6	9.1	22	-23.2	31	-1.5	1.1	-0.8	-0.5	–	–	–	–	–	–	–	–	–	–	–	–	88	71	75	78
II	–	–	–	–	-0.4	-5.5	5.9	13	-17.0	3	-4.1	-1.6	-2.7	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	83	83	88	85
III	–	–	–	–	1.7	-6.0	13.8	31	-14.5	21	-4.5	0.6	-2.5	-2.2	–	–	–	–	–	–	–	–	–	–	–	–	84	65	70	73
IV	–	–	–	–	15.4	4.4	26.5	24	0.3	2	6.9	13.6	9.0	9.6	–	–	–	–	–	–	–	–	–	–	–	–	60	57	65	61
V	–	–	–	–	14.9	6.4	22.9	8	-2.1	1	8.9	13.4	9.7	10.4	–	–	–	–	–	–	–	–	–	–	–	–	77	74	85	79
VI	–	–	–	–	19.3	8.6	30.7	23	2.4	2	12.9	17.5	12.5	13.8	–	–	–	–	–	–	–	–	–	–	–	–	59	56	59	58
VII	–	–	–	–	21.1	9.9	30.1	26	4.5	30	14.1	19.4	14.2	15.5	–	–	–	–	–	–	–	–	–	–	–	–	56	55	68	60
VIII	–	–	–	–	22.4	10.9	31.5	7	4.9	29, 31	14.7	21.4	15.4	16.7	–	–	–	–	–	–	–	–	–	–	–	–	62	51	57	57
IX	–	–	–	–	17.8	6.8	28.5	4	1.2	15	9.8	16.3	10.4	11.7	–	–	–	–	–	–	–	–	–	–	–	–	65	58	49	57
X	–	–	–	–	12.9	2.3	19.7	1	-5.1	16	4.5	12.0	5.6	6.9	–	–	–	–	–	–	–	–	–	–	–	–	78	48	56	61
XI	–	–	–	–	6.2	1.7	15.8	8	-2.6	17	2.6	5.4	3.6	3.8	–	–	–	–	–	–	–	–	–	–	–	–	88	82	85	85
XII	–	–	–	–	-2.5	-8.1	5.3	12	-20.1	26	-5.8	-3.5	-5.5	-5.1	–	–	–	–	–	–	–	–	–	–	–	–	73	75	61	70
Rok	–	–	–	–	10.9	2.3	31.5	7.VIII	-23.2	31. I	4.9	9.6	5.7	6.5	–	–	–	–	–	–	–	–	–	–	–	–	73	65	68	69

Skroniów $\varphi = 50°38'$ $\lambda = 20°16'$

I	–	–	–	–	1.5	-3.6	7.6	22	-18.9	31	-1.7	0.7	-1.3	-0.9	5.0	5.0	5.0	5.0	9.0	7.6	8.6	8.4	0.6	1.6	0.8	1.0	8.2	6.8	7.6	7.5
II	–	–	–	–	-0.1	-4.9	5.5	7	-13.4	1	-3.7	-1.4	-2.4	-2.5	4.1	4.5	4.6	4.4	8.6	8.0	8.7	8.4	0.7	1.1	0.7	0.8	9.5	9.1	8.6	9.1
III	–	–	–	–	1.7	-5.6	13.1	31	-14.4	20	-4.1	0.5	-2.4	-2.1	4.2	4.8	4.7	4.6	8.8	7.3	8.8	8.3	0.5	1.8	0.6	1.0	8.0	7.5	7.1	7.5
IV	–	–	–	–	15.9	5.1	26.3	24	0.2	2	7.6	14.2	8.9	9.9	8.8	8.7	9.1	8.9	8.3	5.7	7.9	7.3	2.1	9.3	2.8	4.7	6.9	6.8	5.4	6.4
V	–	–	–	–	14.8	6.7	21.9	8	-1.1	3	9.1	13.3	9.8	10.5	10.4	10.4	10.9	10.6	8.8	6.9	8.8	8.2	1.5	5.5	1.6	2.9	8.2	8.4	7.4	8.0
VI	–	–	–	–	18.8	8.6	29.2	23	2.8	2	12.7	17.1	13.0	14.0	11.9	11.4	12.3	11.9	8.0	5.8	8.0	7.3	3.2	9.6	3.3	5.4	6.0	7.4	6.6	6.7
VII	–	–	–	–	21.0	10.3	29.0	26	6.6	5	13.9	19.3	14.0	15.3	13.8	13.3	14.1	13.7	8.6	6.0	8.7	7.8	2.3	9.5	2.1	4.6	6.3	7.3	6.4	6.7
VIII	–	–	–	–	22.3	11.6	31.0	13	6.1	31	14.7	21.1	15.4	16.6	14.7	14.8	15.2	14.9	8.7	6.0	8.6	7.8	2.2	10.9	2.5	5.2	5.8	6.2	5.2	5.7
IX	–	–	–	–	17.6	6.9	27.4	4	1.3	15	9.4	16.2	10.9	11.8	10.7	11.2	11.3	11.1	8.9	6.2	8.6	7.9	1.4	8.0	2.0	3.8	6.5	6.6	4.4	5.8
X	–	–	–	–	12.5	2.9	17.6	1	-4.3	24	4.2	11.5	6.1	7.0	8.7	9.7	8.9	8.9	9.6	7.1	9.2	8.6	0.3	4.1	0.8	1.7	7.9	5.1	4.5	5.8
XI	–	–	–	–	6.4	1.9	16.1	8	-1.8	23, 24	2.7	5.4	3.5	3.8	7.2	7.8	7.5	7.5	9.5	8.5	9.3	9.1	0.4	1.7	0.5	0.9	8.2	8.0	8.7	8.3
XII	–	–	–	–	-2.3	-8.2	6.0	7	-24.0	22	-5.9	-3.4	-5.4	-5.0	3.8	4.1	4.0	4.0	9.0	8.1	9.0	8.7	0.4	1.0	0.5	0.6	8.5	7.9	7.6	8.0
Rok	–	–	–	–	10.8	2.6	31.0	13.VIII	-24.0	22.XII	4.9	9.5	5.8	6.5	8.6	8.8	9.0	8.8	8.8	6.9	8.7	8.1	1.3	5.3	1.5	2.7	7.5	7.3	6.6	7.1

Staszów $\varphi = 50°34'$ $\lambda = 21°10'$

I	–	–	–	–	1.5	-4.7	7.3	20	-16.7	31	-2.2	0.3	-1.4	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.6	7.1	7.1
II	–	–	–	–	0.1	-5.7	5.5	13	-12.7	2	-3.5	-1.4	-2.3	-2.4	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.9	9.3	9.2
III	–	–	–	–	1.9	-6.4	13.5	31	-19.5	19	-4.5	0.7	-2.2	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.6	7.2	7.4
IV	–	–	–	–	16.4	4.8	26.3	23	-1.1	8	7.8	15.0	9.3	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.7	4.7	5.8
V	–	–	–	–	15.8	6.0	24.4	19	-2.9	1	9.3	14.0	9.9	10.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.4	6.4	7.5
VI	–	–	–	–	19.0	7.4	29.4	16	1.2	9	12.8	17.1	12.8	13.9	–	–	–	–	–	–	–	–	–	–	–	–	5.4	7.5	5.7	6.2
VII	–	–	–	–	21.4	9.5	29.6	26	4.5	5	13.9	19.8	14.1	15.5	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.9	5.6	6.1
VIII	–	–	–	–	22.8	10.5	29.8	13	3.4	31	14.3	21.4	15.5	16.7	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.5	4.6	5.5
IX	–	–	–	–	17.8	5.4	27.1	4	-1.2	15	8.4	16.2	10.8	11.6	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.4	5.0	6.0
X	–	–	–	–	12.9	1.4	18.8	2	-6.3	16	3.6	11.3	5.1	6.3	–	–	–	–	–	–	–	–	–	–	–	–	7.0	5.1	4.8	5.6
XI	–	–	–	–	7.2	2.1	15.9	4	-1.9	17, 18	3.1	6.1	4.0	4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.4	9.1	8.6
XII	–	–	–	–	-2.2	-8.7	3.8	12	-22.9	29	-5.7	-3.4	-5.6	-5.1	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.0	7.8	8.1
Rok	–	–	–	–	11.2	1.8	29.8	13.VIII	-22.9	29.XII	4.8	9.8	5.8	6.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.2	6.4	6.9

Ostroszowice $H_s = 375$ m $h_w = 12{,}5$ m 1962

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v>10	v>15	⟨thunderstorm⟩	●	Opad R>0.1	R>1.0	R>10.0	═	⊞	R ⟨hail⟩
I	5	1.8	·	·	·	·	3	6.3	5.5	7.4	23	10.3	28	9.9	25.5	5.1	3	7.7	40	7.6	12, 28	2	4	17	·	—	—	·	12	15	6	·	·	8	·
II	7.5	5.1	2	2.0	6	1.2	1	2.0	·	·	10.5	12.8	23.5	6.5	25.5	6.0	8	5.9	49	9.4	12	2	12	23	·	—	—	·	19	18	13	·	2	22	·
III	13	3.9	1.5	2.0	·	·	3	2.0	11.5	5.3	10	6.0	15.5	3.5	32.5	3.3	6	3.7	45	15.1	31	·	9	25	·	—	—	·	15	15	6	2	2	16	·
IV	6	1.8	·	·	1	3.0	2.5	4.2	12	6.4	15	8.0	18.5	5.4	24	2.8	11	4.3	38	7.7	26	·	·	·	3	—	—	1	12	14	12	·	2	·	1
V	0.5	7.0	1	1.0	·	·	4	2.1	7	2.4	14	2.5	25	3.2	36.5	2.8	5	2.7	86	20.6	13	·	·	1	·	—	—	·	14	24	16	2	·	·	3
VI	11	4.0	·	·	·	·	1	1.0	1	5.0	6	4.8	20	3.6	37	3.0	14	3.0	80	55.1	16	·	·	·	6	—	—	3	8	10	8	1	·	·	3
VII	9	1.7	3	1.5	·	·	1.5	4.0	1	3.5	13.5	4.3	30	3.6	25	2.1	10	2.6	57	16.6	16	·	·	·	4	—	—	1	11	17	10	1	·	·	4
VIII	3	1.3	·	·	·	·	1	1.0	2.5	3.6	9.5	7.1	40.5	4.2	23.5	2.1	13	3.2	29	5.1	14	·	·	·	6	—	—	1	10	14	9	·	1	·	6
IX	1.5	3.0	·	·	·	·	3	2.8	12.5	3.0	13	6.3	26.5	4.8	23.5	2.7	10	3.6	59	18.3	17	·	·	·	4	—	—	4	8	13	8	2	1	·	·
X	4	2.5	5	1.8	·	·	3	2.3	11.5	1.8	9.5	4.7	21	3.3	26	2.7	13	2.5	30	14.1	31	·	·	6	·	—	—	7	14	17	4	1	9	·	·
XI	6.5	1.8	3.5	2.0	·	·	3.5	4.4	18.5	5.3	15	5.0	15	4.4	22	2.8	6	3.7	53	16.4	1	·	2	10	·	—	—	1	18	18	11	1	5	3	·
XII	4.5	3.0	·	·	·	·	2	1.5	5.5	3.6	17.5	7.4	17.5	5.3	27	2.4	19	3.5	36	5.4	31	9	15	28	·	—	—	3	17	22	13	·	5	26	·
Rok	71.5	3.1	16	0.9	7	0.4	28.5	2.8	88.5	3.9	156.5	6.6	261	4.8	328	3.2	118	3.9	602	55.1	16.VI	13	42	110	23	—	—	21	158	197	116	10	27	75	17

Szczekociny $H_s = 262$ m $h_w = 14$ m

I	4	5.8	·	·	2	5.0	8.5	3.9	17	4.6	26.5	5.8	11.5	5.1	5.5	4.6	18	4.1	34	6.3	25	2	5	27	·	2	·	1	17	11	10	·	4	12	·
II	6.5	4.7	3.5	4.4	7	4.0	3.5	5.0	6	7.8	14.5	8.6	17	6.6	8	6.8	18	5.1	34	9.8	12	4	14	24	·	6	2	1	19	15	10	·	—	24	·
III	10.5	5.7	4.5	4.0	10	3.5	9	3.7	4.5	4.1	5	5.2	8.5	6.5	8	5.2	33	3.1	41	15.9	12	7	13	27	·	2	·	2	16	15	6	2	1	20	·
IV	5	4.4	4.5	4.8	6	4.9	11	5.5	4	5.1	9	5.0	11.5	4.9	12	4.7	27	3.5	77	24.5	13	·	·	·	5	2	·	4	10	16	10	3	1	·	1
V	3.5	2.4	1.5	2.3	2.5	4.2	7	3.3	5.5	5.3	14	5.2	20.5	4.8	9.5	3.4	29	3.0	145	13.6	20	·	·	2	·	1	1	1	18	23	20	8	·	·	3
VI	5.5	4.0	3.5	4.3	2.5	3.0	4.5	3.2	1	3.0	10.5	4.2	16	4.1	16.5	5.5	30	2.9	89	32.3	1	·	·	·	6	3	·	2	11	9	7	3	·	·	2
VII	7.5	2.9	2	2.5	1.5	4.0	2	3.2	3.5	5.7	13	4.0	15	3.0	7.5	3.2	41	1.9	99	17.5	3	·	·	·	6	1	·	3	11	16	15	2	1	·	9
VIII	4	2.9	1	4.0	3	2.3	6	3.5	5.5	5.5	12.5	4.3	21	5.0	6	2.8	34	2.7	55	13.0	15	·	·	·	9	1	·	2	6	12	9	1	1	·	5
IX	2.5	3.4	1.5	4.0	7	4.2	5.5	4.4	9	5.9	18.5	4.8	12.5	3.9	4.5	4.8	29	3.1	50	20.7	17	·	·	·	3	4	·	7	11	10	7	2	2	·	·
X	2.5	2.8	4.5	3.1	15	3.3	8	3.2	1	6.0	6.5	5.8	11	4.0	3.5	3.6	41	2.1	10	5.6	28	·	·	11	·	·	·	5	11	5	4	·	8	·	·
XI	4	3.2	6	4.2	18.5	4.4	6.5	3.4	4.5	4.3	7.5	5.4	5.5	4.3	2.5	3.8	35	2.6	47	13.0	15	·	1	10	·	3	·	1	22	15	10	1	2	3	·
XII	8.5	4.1	5.5	3.3	5	3.8	7.5	3.7	7	7.1	11.5	5.4	10.5	3.0	5.5	4.8	32	2.9	18	5.4	13	11	15	29	·	4	·	·	14	12	5	·	1	18	·
Rok	64	3.9	38	3.4	80	3.9	79	3.8	58.5	5.4	149	5.3	160.5	4.6	89	4.4	367	3.1	699	32.3	1.VI	24	48	130	29	29	3	29	166	159	113	22	—	77	20

Skroniów $H_s = 256$ m $h_w = 16{,}5$ m

I	3	8.7	6.5	4.5	0.5	2.0	1	2.0	14.5	2.1	32	3.6	19	4.7	10.5	5.0	6	3.7	32	7.0	25	2	8	24	·	1	·	·	16	13	9	·	1	19	·
II	4.5	5.2	5	3.0	11	4.2	6	2.9	2	3.0	10	9.0	15.5	7.4	18	8.6	12	5.6	28	5.8	12	4	13	24	·	7	4	·	23	16	6	·	·	24	·
III	8	6.6	9	4.1	11	2.2	13.5	3.0	4	2.2	4.5	3.4	10.5	6.6	13.5	4.0	19	3.2	37	11.4	12	5	13	27	·	3	·	2	19	15	10	1	·	20	·
IV	6	4.2	6	4.6	6.5	3.6	9.5	4.5	6	2.2	10.5	2.7	11	4.9	17.5	5.1	17	3.4	43	10.4	6	·	·	·	4	3	2	3	8	12	9	1	·	·	2
V	6	2.8	1.5	2.3	2.5	2.8	6.5	3.4	6	2.7	12	3.2	28	4.4	13.5	4.1	17	3.1	155	14.2	9	·	·	2	·	1	·	·	14	22	19	6	·	·	4
VI	10	4.4	4	3.7	2.5	2.2	3.5	2.7	2	2.5	1	2.0	18	4.2	27	4.8	22	3.2	84	40.5	4	·	·	·	5	1	·	1	13	9	9	2	·	·	2
VII	4	3.8	2.5	2.8	0.5	2.0	3.5	2.3	·	·	9	2.8	23	4.0	17.5	3.1	33	2.2	91	15.6	15	·	·	·	4	1	1	2	11	16	14	3	·	·	9
VIII	1	2.0	2	3.5	1.5	2.7	4.5	2.9	3	3.3	7.5	4.0	29	4.7	11.5	4.1	33	2.7	52	15.5	5	·	·	·	9	·	·	2	4	12	7	2	3	·	3
IX	2	3.8	2	2.8	7.5	3.5	4.5	2.4	3	2.3	11.5	5.3	22.5	4.2	11	5.5	26	3.0	47	13.5	18	·	·	·	3	1	·	6	11	9	7	2	4	·	·
X	4	2.2	3.5	2.7	15	2.4	17.5	2.2	·	·	4	3.2	10	3.8	11	4.4	28	2.1	4	2.1	28	·	·	11	·	·	·	4	11	4	2	·	15	·	·
XI	7	1.1	5.5	5.1	28.5	4.3	10	3.4	2	3.0	3.5	3.6	13	3.8	8.5	2.5	12	3.1	49	13.0	15	·	1	9	·	·	·	1	20	16	11	1	13	5	·
XII	8	4.4	12.5	4.4	5.5	3.1	7.5	2.3	2	3.0	9	5.2	21.5	3.2	8	3.8	19	3.0	25	10.3	13	11	15	30	·	·	·	1	18	12	7	1	3	18	·
Rok	63.5	4.1	60	3.6	92.5	2.9	87.5	2.8	44.5	2.2	114.5	4.0	221	4.7	167.5	4.6	244	3.2	647	40.5	4.VI	22	50	127	25	18	7	22	168	156	110	19	39	86	20

Staszów $H_s = 193$ m $h_w = 16{,}2$ m

I	2	11.0	6	5.5	·	·	17.5	2.1	6.5	2.0	11	1.8	16	3.3	8	4.9	26	2.3	31	8.2	25	4	9	27	·	2	·	1	14	13	8	·	2	24	·
II	7	3.9	7	3.1	11	5.5	1	4.0	1	5.0	9.5	4.8	10.5	5.1	16	6.9	21	3.9	32	6.8	16	4	14	26	·	6	·		25	14	8	·	2	24	·
III	8.5	6.1	12	4.0	7	4.7	11	3.3	3	2.7	1	3.0	10	4.6	6.5	3.7	34	2.7	35	6.6	12	7	12	27	·	2	·	4	18	16	11	·	3	24	·
IV	3.5	4.4	9	3.9	6.5	6.4	13.5	4.4	2.5	4.0	7	2.9	5	3.0	10	5.6	33	2.8	42	14.6	6	·	·	2	4	3	·	6	9	14	8	1	2	·	2
V	4	2.2	4	2.5	3	2.0	5	4.6	3.5	2.6	4.5	2.0	9	4.9	15	4.3	45	1.9	123	18.8	21	·	·	3	·	2	·	·	14	26	21	3	3	·	3
VI	11.5	4.4	3.5	2.3	·	·	5	1.8	·	·	2	2.5	11	3.5	25	4.3	32	2.4	94	32.9	4	·	·	·	6	1	·	1	8	10	9	3	·	·	3
VII	1	4.0	6	3.0	2	1.5	5.5	3.2	3.5	1.9	4.5	2.8	17	2.6	17.5	2.6	36	1.6	91	25.3	19	·	·	·	4	·	·	3	9	14	11	3	·	·	7
VIII	1	6.0	2	2.0	3.5	2.9	4.5	3.1	6	2.2	4	2.0	16	3.6	14	3.9	42	1.8	38	10.0	16	·	·	·	9	1	·	3	5	10	6	1	4	·	4
IX	1	3.0	2	2.5	9	2.7	4	2.5	2.5	2.8	9.5	2.4	9.5	2.4	15.5	4.1	37	1.8	66	22.0	18	·	·	1	3	·	·	6	9	12	7	2	3	·	1
X	4	1.8	8	2.9	10	2.0	4	2.5	1	1.0	2.5	2.0	6.5	3.4	7	4.0	50	1.2	1	0.3	31	·	·	14	·	·	·	5	10	2	·	·	18	·	·
XI	6.5	2.6	8.5	4.2	27	4.6	6	4.3	1	2.0	3	2.7	8	2.2	5	2.6	25	2.7	48	11.9	15	·	·	6	·	·	·	1	20	20	11	1	10	2	·
XII	7	5.6	16.5	4.2	3.5	4.1	10	3.6	6	3.1	5	2.0	11.5	2.2	10.5	4.1	23	2.8	18	5.6	16	11	16	30	·	1	·	1	18	13	4	·	8	17	·
Rok	57	4.6	84.5	3.3	82.5	3.0	87	3.3	36.5	2.4	63.5	2.6	130	3.4	150	4.2	404	2.3	614	32.9	4.VI	26	51	136	26	19	·	31	159	164	104	14	55	91	20

Poturzyn $\varphi = 50°34'$ $\lambda = 23°56'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{s.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.0	–	6.2	22	–	–	-1.9	0.1	-1.8	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	93	77	69	80
II	–	–	–	–	-1.7	-7.0	2.2	13	-13.4	1	-5.1	-2.7	-4.0	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	94	85	88	89
III	–	–	–	–	0.1	-6.5	11.2	5	-16.8	21	-4.4	-0.9	-3.2	-2.9	–	–	–	–	–	–	–	–	–	–	–	–	76	75	76	76
IV	–	–	–	–	15.5	5.1	25.7	24	-0.7	2	7.2	14.5	9.5	10.2	–	–	–	–	–	–	–	–	–	–	–	–	50	47	51	49
V	–	–	–	–	16.6	7.3	23.9	14	-1.2	2	9.9	14.8	11.2	11.8	–	–	–	–	–	–	–	–	–	–	–	–	65	75	60	67
VI	–	–	–	–	18.7	9.8	28.0	16	2.5	7	13.1	17.5	13.5	14.4	–	–	–	–	–	–	–	–	–	–	–	–	54	68	67	63
VII	–	–	–	–	20.1	10.5	28.8	27	6.3	3	13.8	19.1	14.4	15.4	–	–	–	–	–	–	–	–	–	–	–	–	60	78	60	66
VIII	–	–	–	–	21.9	11.7	29.6	13	6.0	31	14.8	20.9	15.8	16.8	–	–	–	–	–	–	–	–	–	–	–	–	56	65	51	57
IX	–	–	–	–	17.5	7.4	28.0	5	1.2	25	9.7	16.6	11.4	12.3	–	–	–	–	–	–	–	–	–	–	–	–	56	69	48	58
X	–	–	–	–	13.3	2.2	19.0	2	-4.4	16	4.0	12.6	6.5	7.4	–	–	–	–	–	–	–	–	–	–	–	–	68	52	39	53
XI	–	–	–	–	7.3	1.8	18.7	1	-4.6	18	3.1	6.3	3.8	4.2	–	–	–	–	–	–	–	–	–	–	–	–	83	85	75	81
XII	–	–	–	–	-2.8	-8.0	2.9	12	-18.2	21, 22	-5.9	-3.9	-5.6	-5.2	–	–	–	–	–	–	–	–	–	–	–	–	83	79	76	79
Rok	–	–	–	–	10.6	–	29.6	13. VIII	–	–	4.9	9.6	6.0	6.6	–	–	–	–	–	–	–	–	–	–	–	–	70	71	63	68

Tarnobrzeg $\varphi = 50°34'$ $\lambda = 21°40'$

I	–	–	–	–	1.7	-3.5	7.1	22	-17.0	31	-1.5	0.5	-1.2	-0.8	5.1	5.3	5.0	5.1	90	82	86	86	0.6	1.3	0.8	0.9	79	67	70	72
II	–	–	–	–	0.3	-5.1	6.7	13	-12.4	25	-3.7	-1.2	-2.4	-2.4	4.2	4.6	4.7	4.5	89	82	86	86	0.6	1.0	0.6	0.7	90	87	88	88
III	–	–	–	–	2.6	-4.8	14.5	5	-13.8	20	-3.7	1.2	-1.5	-1.4	4.6	5.0	5.1	4.9	94	72	88	85	0.3	2.0	0.6	1.0	78	75	67	73
IV	–	–	–	–	17.1	5.8	28.1	23	0.0	8	8.0	15.6	10.5	11.2	8.9	8.6	8.9	8.8	82	52	71	68	2.1	10.8	4.4	5.8	60	56	42	53
V	–	–	–	–	16.0	7.4	22.6	8	-0.9	1	9.3	14.2	10.9	11.3	11.0	11.0	11.4	11.1	92	67	86	82	1.0	5.7	2.0	2.9	83	84	70	79
VI	–	–	–	–	19.3	9.8	29.6	16	3.5	6	12.6	17.8	14.3	14.8	12.4	11.8	12.6	12.3	82	59	76	72	2.8	10.2	4.5	5.8	63	72	58	64
VII	–	–	–	–	21.9	11.5	30.1	26	8.0	9, 30	14.0	20.4	15.8	16.5	13.8	12.9	14.3	13.7	86	54	79	73	2.4	11.7	3.9	6.0	65	63	58	62
VIII	–	–	–	–	23.5	12.7	30.3	7, 13	6.3	31	14.6	21.7	17.3	17.7	14.9	14.5	16.0	15.1	88	56	80	75	2.0	12.3	4.1	6.1	59	61	46	55
IX	–	–	–	–	18.2	7.8	27.6	4	2.1	25	9.2	16.5	11.9	12.4	10.6	11.2	11.7	11.2	90	62	84	79	1.3	8.3	2.6	4.1	63	67	45	58
X	–	–	–	–	13.1	2.9	20.5	2	-3.9	16	4.0	11.3	6.9	7.3	8.1	9.9	9.1	9.0	97	73	90	87	0.4	3.8	1.0	1.7	80	59	31	57
XI	–	–	–	–	7.2	2.4	15.7	1	-1.7	18	3.4	6.2	4.2	4.5	7.4	8.1	7.6	7.7	93	84	90	89	0.6	1.9	0.9	1.1	88	83	84	85
XII	–	–	–	–	-2.1	-8.0	3.7	13	-20.1	22	-5.7	-3.3	-5.2	-4.8	3.9	4.3	4.0	4.1	93	86	91	90	0.3	0.8	0.5	0.5	87	81	75	81
Rok	–	–	–	–	11.6	3.2	30.3	7.13. VIII	-20.1	22. XII	5.0	10.1	6.8	7.2	8.7	8.9	9.2	8.9	90	69	84	81	1.2	5.8	2.2	3.1	75	71	61	69

Biłgoraj $\varphi = 50°33'$ $\lambda = 22°43'$

I	–	–	–	–	2.0	-3.3	7.4	22	-16.8	31	-1.1	1.3	-0.9	-0.4	–	–	–	–	–	–	–	–	–	–	–	–	73	66	63	67
II	–	–	–	–	-0.2	-6.0	4.0	7	-12.2	25	-3.7	-1.0	-3.2	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	90	86	83	86
III	–	–	–	–	2.0	-5.6	12.1	5	-15.7	20	-3.3	1.2	-2.2	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	78	69	71	73
IV	–	–	–	–	16.8	4.7	27.3	23	-2.3	30	8.0	16.1	9.4	10.7	–	–	–	–	–	–	–	–	–	–	–	–	51	46	29	42
V	–	–	–	–	16.2	6.6	23.9	14, 28	-1.2	4, 5	9.9	15.3	10.8	11.7	–	–	–	–	–	–	–	–	–	–	–	–	72	59	48	60
VI	–	–	–	–	19.3	8.7	29.1	16	2.8	9	13.0	18.0	14.0	14.8	–	–	–	–	–	–	–	–	–	–	–	–	55	59	47	54
VII	–	–	–	–	21.2	10.2	30.3	27	5.0	30	14.1	20.0	15.5	16.3	–	–	–	–	–	–	–	–	–	–	–	–	58	52	51	54
VIII	–	–	–	–	23.2	11.6	31.1	7, 13	5.0	31	15.4	21.9	16.8	17.7	–	–	–	–	–	–	–	–	–	–	–	–	55	46	41	47
IX	–	–	–	–	18.0	7.2	28.1	5	0.0	15	10.1	17.0	12.1	12.8	–	–	–	–	–	–	–	–	–	–	–	–	51	55	44	50
X	–	–	–	–	13.6	1.6	20.6	2	-5.8	16, 17	3.7	12.8	5.4	6.8	–	–	–	–	–	–	–	–	–	–	–	–	66	46	30	48
XI	–	–	–	–	7.6	2.3	18.6	1	-2.1	18	4.2	6.9	4.4	5.0	–	–	–	–	–	–	–	–	–	–	–	–	88	81	85	85
XII	–	–	–	–	-2.1	-7.3	3.4	11	-18.3	22	-5.5	-3.0	-5.0	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	75	81	69	75
Rok	–	–	–	–	11.5	2.6	31.1	7.13. VIII	-18.3	22. XII	5.4	10.5	6.4	7.2	–	–	–	–	–	–	–	–	–	–	–	–	68	62	55	62

Nisko $\varphi = 50°31'$ $\lambda = 22°09'$

I	–	–	–	–	2.6	-3.3	7.8	20	-17.7	31	-1.0	1.4	-0.9	-0.3	–	–	–	–	–	–	–	–	–	–	–	–	79	67	54	67
II	–	–	–	–	0.3	-5.5	3.8	13	-13.4	25	-3.8	-1.2	-2.7	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	87	98	82	89
III	–	–	–	–	2.7	-5.4	14.6	5	-15.0	21	-3.8	1.3	-1.9	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	77	72	65	71
IV	–	–	–	–	17.5	5.0	27.8	23	-1.8	30	8.7	16.3	9.6	10.9	–	–	–	–	–	–	–	–	–	–	–	–	53	54	38	48
V	–	–	–	–	16.5	6.9	23.5	8	-1.5	1	9.9	14.8	10.6	11.5	–	–	–	–	–	–	–	–	–	–	–	–	78	84	56	73
VI	–	–	–	–	19.9	9.0	29.9	23	3.6	7	13.5	18.4	13.2	14.6	–	–	–	–	–	–	–	–	–	–	–	–	53	79	51	61
VII	–	–	–	–	22.4	10.7	30.2	27	5.7	30	14.4	20.4	14.8	16.1	–	–	–	–	–	–	–	–	–	–	–	–	55	68	60	61
VIII	–	–	–	–	23.9	12.0	30.9	13	6.4	29	15.2	22.2	16.4	17.6	–	–	–	–	–	–	–	–	–	–	–	–	62	57	39	53
IX	–	–	–	–	18.5	7.5	28.7	5	1.3	15	9.8	17.0	11.5	12.4	–	–	–	–	–	–	–	–	–	–	–	–	54	69	45	56
X	–	–	–	–	13.8	1.8	21.0	2	-5.6	17	3.9	12.6	5.7	7.0	–	–	–	–	–	–	–	–	–	–	–	–	66	48	23	46
XI	–	–	–	–	7.3	2.2	17.4	1	-1.7	17	3.4	6.4	4.3	4.6	–	–	–	–	–	–	–	–	–	–	–	–	89	81	75	82
XII	–	–	–	–	-1.9	-7.7	4.8	13	-18.7	22	-5.6	-3.1	-5.4	-4.9	–	–	–	–	–	–	–	–	–	–	–	–	71	78	73	74
Rok	–	–	–	–	12.0	2.8	30.9	13. VIII	-18.7	22. XII	5.3	10.5	6.3	7.1	–	–	–	–	–	–	–	–	–	–	–	–	69	71	55	65

Poturzyn — $H_s = 240\ m$ — $h_w = 14{,}7\ m$ — 1962

MIESIĄC	ROZKŁAD WIATRU °D, %D																				OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Date	Temperatura T				Wiatr v				Opad R							
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min ≤ -10°	Max ≤ 0°	Min ≤ 0°	Max ≥ 25°	≥ 10 m/s	≥ 15 m/s			≥ 0,1 mm	≥ 1,0 mm	≥ 10,0 mm					
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	11	38	15	–	9	–	·	–	–	·	13	8	3	·	1	22	–		
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7	18	27	·	–	–	·	22	–	–	–	2	28	–		
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6	17	29	·	–	–	1	15	–	–	–	1	30	–		
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	25	9.5	6	·	·	3	4	–	–	8	3	7	7	·	1	·	–		
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	67	14.0	11	·	·	3	·	–	–	·	9	14	12	2	2	·	–		
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	66	34.1	1	·	·	·	5	–	–	5	13	11	7	1	·	·	–		
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	·	·	·	3	–	–	1	11	–	–	–	·	·	–		
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	34	68	20	·	·	·	5	–	–	4	5	11	9	·	2	·	–		
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	21	4.7	22	·	·	·	1	–	–	4	10	11	8	·	4	·	–		
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4	1.8	29	·	·	10	·	–	–	4	10	4	1	·	11	·	–		
XI	5.5	3.1	6	4.9	17.5	5.7	28	5.4	4.5	4.2	13	4.7	6	4.0	5.5	4.2	4	4.7	35	6.0	16	·	·	6	·	2	·	4	22	11	9	·	11	·	–		
XII	13	3.8	9	5.2	5.5	3.1	12.5	3.0	10.5	3.3	15	3.3	15.5	4.3	7	4.6	5	3.6	6	2.9	16	10	18	30	·	·	·	3	20	7	2	·	3	18	–		
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	62	–	18	–	–	34	153	–	–	–	38	98	–		

Tarnobrzeg — $H_s = 175\ m$ — $h_w = 15{,}2\ m$

I	3.5	7.3	5.5	3.9	·	·	·	·	11.5	4.0	3.2	3.5	2.9	3.4	5.5	4.5	6	3.5	26	5.4	25	2	8	24	·	–	–	1	14	23	6	·	·	20	·		
II	10	3.2	6	1.7	7.5	3.2	5.5	5.1	3	4.7	12	8.8	20.5	6.2	10.5	9.2	9	5.2	36	6.2	17	2	12	26	·	–	–	·	20	21	12	·	3	28	1		
III	14.5	3.6	6.5	4.7	8.5	2.1	8	4.3	13	3.4	5	3.8	12	4.4	10.5	3.3	15	3.1	53	18.2	16	3	8	26	·	–	–	2	18	21	12	1	12	24	·		
IV	5	2.4	10.5	1.8	5	1.9	7.5	4.5	9	6.7	13.5	4.0	12	3.4	9.5	4.5	18	3.0	35	8.8	27	·	·	·	5	–	–	6	6	13	8	·	5	·	6		
V	10	1.6	6.5	1.3	0.5	6.0	2.5	3.6	4.5	3.0	11.5	2.0	29.5	4.0	10	2.6	18	2.3	13.0	18.8	8	·	·	1	·	–	–	·	18	25	19	6	4	·	8		
VI	16	2.6	1	1.0	·	·	1	1.0	3.5	1.6	6	3.1	19	4.9	17.5	3.6	26	2.5	9.5	36.0	1	·	·	·	6	–	–	1	10	12	9	2	3	·	3		
VII	8.5	2.1	6	2.8	2.5	2.0	2	4.0	5.5	2.6	12.5	3.3	3.4	3.6	14	3.0	8	2.9	10.2	37.5	18	·	·	·	4	–	–	2	7	15	11	4	4	·	7		
VIII	7.5	1.3	3	2.2	1	5.0	2	3.8	12	2.1	17.5	3.3	3.6	4.3	10	3.2	4	3.2	38	13.6	5	·	·	·	10	–	–	2	5	10	5	1	16	·	3		
IX	1	2.0	2.5	3.4	12.5	2.7	2	4.0	8.5	3.1	18	3.9	28.5	3.6	10	4.0	7	3.2	60	22.2	18	·	·	·	3	–	–	4	8	13	9	2	8	·	2		
X	1.3	2.3	11.5	2.4	13.5	2.1	9	2.6	4	3.0	6.5	3.2	20	2.7	6.5	4.0	9	2.6	2	0.8	31	·	·	10	·	–	–	2	8	7	·	·	22	·	·		
XI	1.5	3.2	2.5	3.6	9.5	5.2	34.5	6.3	4	5.2	5	5.8	11.5	5.1	6	3.3	2	5.0	57	21.0	15	·	·	6	·	–	–	·	21	20	12	1	12	2	·		
XII	13.5	2.8	11.5	4.7	8	2.9	3.5	2.3	10.5	5.4	17.5	5.8	17.5	4.2	5	3.9	6	4.0	17	6.4	14	11	16	30	·	–	–	·	19	16	4	·	12	17	·		
Rok	117.5	2.9	73	2.8	68.5	2.8	77.5	3.5	8.9	3.7	157	4.2	269.5	4.2	115	4.1	128	3.4	651	37.5	18.VII	18	44	123	28	–	–	20	154	196	107	17	101	91	3.0		

Biłgoraj — $H_s = 190\ m$ — $h_w = 19\ m$

I	2	3.0	3	2.3	·	·	3	1.7	2.6	1.2	1.9	1.7	1.4	2.1	8	2.1	1.8	1.4	38	7.2	25	3	6	24	·	·	·	1	13	16	10	·	·	–	–		
II	1.0	1.4	1	2.0	1.2	1.1	6	1.3	7	6.6	5	6.2	1.6	3.2	1.3	9.1	1.4	3.3	47	12.5	12	4	1.3	28	·	5	2	·	19	19	11	1	·	–	–		
III	1.2	2.8	9	1.2	1.4	1.5	1.9	2.7	9	1.2	2	1.0	9	4.0	4	4.2	1.5	2.0	69	18.8	16	6	7	25	·	1	·	1	16	16	12	2	1	–	–		
IV	1	1.0	4	2.2	1.2	2.4	1.6	2.1	7	2.6	6	1.8	1.1	3.1	5	3.2	2.8	1.7	43	16.3	6	·	·	3	5	1	1	8	3	9	8	1	1	·	–		
V	6	1.5	·	·	2	1.0	6	1.3	8	1.2	9	4.4	2.0	2.6	1.1	1.4	3.1	1.5	118	19.5	20	·	·	5	·	1	·	1	7	18	15	5	·	·	–		
VI	8	3.0	2	1.5	4	1.0	1	2.0	4	1.2	5	1.8	2.0	1.8	1.9	2.0	2.7	1.4	80	23.1	4	·	·	·	9	·	·	4	9	13	11	2	·	·	–		
VII	5	1.4	·	·	·	·	3	1.0	8	1.1	9	1.8	2.3	1.5	8	1.1	3.7	0.8	133²	40.2	23	·	·	·	4	·	·	6	5	15	11	4	1	·	–		
VIII	3	1.0	3	1.3	1	1.0	4	1.2	7	1.4	7	1.4	2.6	1.5	4	1.2	3.8	0.8	42	11.2	16	·	·	·	12	·	·	5	3	10	8	1	1	·	–		
IX	·	·	·	·	7	1.3	10	1.3	9	1.2	11	1.8	2.1	1.7	·	·	3.2	1.0	83	31.2	5	·	·	·	2	·	·	7	7	13	11	2	2	·	–		
X	5	1.4	1	1.0	2	1.0	8	1.4	3	1.0	3	3.0	9	2.2	1	2.0	6.1	0.6	4	2.0	19	·	·	11	·	·	·	6	3	4	1	·	12	·	–		
XI	5	1.4	6	2.0	1.3	3.0	2.8	2.4	1	1.0	3	2.7	1.0	1.5	5	2.0	1.9	1.8	6.4	15.6	25	·	·	5	·	·	·	1	19	16	11	2	5	–	–		
XII	1.4	1.4	7	1.7	5	1.1	9	1.4	7	1.4	1.2	1.3	1.3	1.2	4	2.2	2.2	1.1	15	8.1	16	1.1	1.3	3.0	·	·	·	1	18	15	4	·	·	–	–		
Rok	71	1.6	36	1.3	7.2	1.2	11.3	1.6	9.6	1.8	9.1	2.4	19.2	2.2	8.2	2.5	34.2	1.4	736²	40.2	23.VII	24	39	131	32	8	3	41	122	164	113	20	23	–	–		

Nisko — $H_s = 164\ m$ — $h_w = 16\ m$

I	2	4.0	5.5	1.7	0.5	3.0	0.5	1.0	3.6	2.7	1.7	2.8	25.5	3.1	6	3.8	·	2.7	31	6.5	25	3	6	24	·	·	·	4	14	14	11	·	·	16	·		
II	8.5	4.1	2.5	2.6	1.8	2.9	5.5	2.3	8	6.6	5.5	8.1	2.7	5.2	8	10.3	1	5.1	49	12.0	12	2	1.2	26	·	7	4	·	19	17	11	2	·	26	2		
III	8	3.5	7.5	3.0	1.8	1.7	12.5	4.1	1.6	3.2	3	2.8	9	4.4	1.8	3.0	1	3.1	64	18.0	16	5	6	26	·	2	1	3	16	18	12	2	1	22	·		
IV	4	1.7	9.5	1.5	19.5	3.0	11.5	3.2	15.5	3.5	7	2.1	1.7	3.5	5	5.1	1	3.0	25	8.5	28	·	·	2	5	1	·	9	8	13	6	·	1	·	1		
V	7	1.6	2	2.5	6	2.7	6.5	2.2	8.5	1.8	1.7	2.3	34.5	3.4	11.5	2.5	·	2.6	9.5	10.0	25	·	·	2	·	2	1	2	16	24	19	1	3	·	4		
VI	9.5	2.2	·	·	5	2.2	2	1.5	5	1.6	7	2.1	23.5	3.5	3.7	3.1	1	2.9	93	36.5	4	·	·	·	9	2	·	5	10	9	9	2	·	·	1		
VII	6	2.0	6	1.2	6	2.5	4	1.2	12.5	1.6	1.2	1.8	30.5	2.6	1.6	2.0	·	2.1	111	30.0	19	·	·	·	8	·	·	2	9	15	14	5	1	·	7		
VIII	4.5	1.2	2	1.0	8.5	1.4	10	1.4	3.5	2.3	11.5	1.6	39.5	2.5	13.5	1.9	·	2.0	48	21.0	5	·	·	·	13	·	·	3	5	9	6	1	2	·	2		
IX	4	1.0	1	1.0	14.5	2.2	3.5	2.7	12.5	2.2	1.1	1.7	31.5	3.1	5	4.7	7	2.4	5.5	16.0	18	·	·	·	4	1	·	6	10	11	10	1	2	·	2		
X	12.5	1.2	8	1.4	1.7	2.4	1.0	2.1	7	1.6	9	2.9	17.5	2.8	1.1	3.1	1	2.3	3	1.0	14,19,31	·	·	13	·	1	·	6	4	3	3	·	1.1	·	·		
XI	6	2.0	1	2.0	2.6	5.2	2.5	4.4	4.5	1.6	4.5	2.3	1.1	3.0	1.2	2.4	·	3.8	5.6	16.2	15	·	·	5	·	2	1	·	18	14	12	1	6	·	·		
XII	1.3	2.8	9.5	2.4	2.5	2.5	9.5	2.4	16.5	4.4	9	3.6	20.5	3.2	7.5	2.3	·	3.0	18	9.0	14	1.2	1.5	3.0	·	1	·	4	15	11	6	·	4	17	·		
Rok	8.5	2.3	54.5	2.1	146.5	2.6	100.5	2.4	145.5	2.8	113.5	2.8	28.7	3.4	150.5	3.7	1.2	2.9	648	36.5	4.VI	22	39	128	39	19	7	44	144	158	119	15	31	81	19		

Korfantów $\varphi = 50°29'$ $\lambda = 17°36'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.2	−2.9	8.9	22	−21.0	31	−1.1	1.9	0.2	0.3	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.1	6.5	6.4
II	–	–	–	–	1.3	−4.7	8.6	12	−13.5	4	−2.8	0.0	−1.5	−1.4	–	–	–	–	–	–	–	–	–	–	–	–	7.8	8.1	7.1	7.7
III	–	–	–	–	3.3	−2.9	15.3	31	−6.9	14	−1.1	2.3	−0.1	0.3	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.7	5.3	6.7
IV	–	–	–	–	15.7	5.6	28.2	21	1.4	2	10.0	14.2	10.7	11.4	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.9	6.1	6.1
V	–	–	–	–	15.4	6.4	22.8	8	−0.7	1	10.2	13.7	10.6	11.3	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.2	6.5	6.8
VI	–	–	–	–	20.4	8.8	30.8	23	3.0	6	14.0	19.0	14.6	15.6	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.7	5.3	4.8
VII	–	–	–	–	21.2	10.7	31.5	26	6.3	5	14.8	20.1	15.4	16.4	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.9	6.1	5.8
VIII	–	–	–	–	23.9	12.2	31.2	13	6.8	29	16.1	22.3	16.6	17.9	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.6	4.5	5.1
IX	–	–	–	–	18.5	7.4	31.1	4	1.3	15	10.3	16.8	12.2	12.9	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.0	3.4	5.1
X	–	–	–	–	13.3	3.9	23.1	3	−3.2	22	6.1	12.4	7.0	8.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	4.3	5.0	5.6
XI	–	–	–	–	6.6	1.9	16.4	9	−2.0	21, 25	3.1	6.0	3.9	4.2	–	–	–	–	–	–	–	–	–	–	–	–	9.5	8.5	8.0	8.7
XII	–	–	–	–	−1.4	−7.4	7.0	13	−22.0	24	−5.4	−2.7	−4.6	−4.3	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.1	7.6	7.9
Rok	–	–	–	–	11.8	3.2	31.5	26.VII	−22.0	24.XII	6.2	10.5	7.1	7.7	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.3	6.0	6.4

Otmuchów $\varphi = 50°28'$ $\lambda = 17°10'$

I	–	–	–	–	4.0	−2.4	10.6	22	−22.3	31	0.0	2.8	0.9	1.2	5.0	5.3	5.1	5.1	7.7	6.9	7.6	7.4	1.6	2.6	1.7	2.0	6.8	7.0	7.9	7.2
II	–	–	–	–	1.6	−5.6	8.1	12	−20.4	2	−2.4	0.2	−1.6	−1.4	4.3	4.6	4.6	4.5	8.1	7.2	7.9	7.7	1.1	1.9	1.2	1.4	8.9	9.5	8.0	8.8
III	–	–	–	–	3.6	−3.1	15.6	31	−7.7	15	−1.9	2.5	0.2	0.2	4.6	5.0	5.1	4.9	8.4	6.6	7.9	7.6	0.9	2.7	1.4	1.7	8.0	8.2	6.0	7.4
IV	–	–	–	–	15.6	5.0	27.6	24	−0.1	10	8.6	14.5	9.6	10.6	8.1	8.0	8.5	8.2	7.4	5.2	7.0	6.5	3.6	10.6	4.2	6.1	7.7	6.9	6.3	7.0
V	–	–	–	–	15.8	6.3	23.6	8	−1.8	5	9.7	14.0	10.7	11.3	10.2	10.1	10.7	10.3	8.3	6.7	8.2	7.7	2.1	6.5	2.5	3.7	7.4	8.7	7.9	8.0
VI	–	–	–	–	20.4	9.3	31.5	23	3.4	2, 6	13.1	19.0	14.2	15.1	11.8	11.2	12.6	11.9	7.4	4.9	7.5	6.6	4.0	12.4	4.2	6.9	5.6	6.0	6.0	5.9
VII	–	–	–	–	21.0	10.2	31.3	26	3.6	9	14.4	19.9	14.3	15.7	13.2	13.0	13.2	13.1	8.0	5.7	7.9	7.2	3.4	11.0	3.4	5.9	5.7	6.3	6.5	6.2
VIII	–	–	–	–	24.1	11.3	32.0	13	4.0	31	15.5	22.7	16.3	17.7	14.5	13.8	14.7	14.3	8.1	5.0	7.9	7.0	3.4	14.3	4.1	7.3	6.6	7.1	5.1	6.3
IX	–	–	–	–	18.7	7.4	31.4	4	0.4	15	10.3	17.1	12.2	13.0	11.0	11.6	11.3	11.3	8.6	6.2	8.1	7.6	2.1	9.0	3.5	4.9	6.6	5.9	4.1	5.5
X	–	–	–	–	14.2	4.0	25.0	4	−3.8	22	5.7	13.1	7.2	8.3	8.6	10.0	9.3	9.3	9.2	6.8	8.9	8.3	0.9	5.8	1.2	2.6	8.0	5.9	5.1	6.3
XI	–	–	–	–	7.0	1.7	18.6	8	−3.9	28	2.7	6.0	4.0	4.2	6.8	7.4	7.1	7.1	9.0	7.7	8.6	8.4	0.8	2.6	1.3	1.6	8.3	9.0	8.4	8.6
XII	–	–	–	–	−1.0	−7.7	8.4	13	−19.0	24	−5.2	−2.5	−4.8	−4.3	3.8	3.9	3.9	3.9	8.4	7.2	8.4	8.0	0.8	1.6	0.8	1.1	8.2	7.6	8.1	8.0
Rok	–	–	–	–	12.1	3.0	32.0	13.VIII	−22.3	31. I	5.9	10.8	6.9	7.6	8.5	8.7	8.8	8.7	8.2	6.3	8.0	7.5	2.1	6.8	2.5	3.8	7.3	7.3	6.6	7.1

Kudowa-Zdrój $\varphi = 50°27'$ $\lambda = 16°16'$

I	–	–	–	–	1.5	−3.8	8.2	22	−15.6	31	−1.4	0.4	−1.4	−1.0	5.2	5.3	5.1	5.2	9.0	8.1	8.8	8.6	0.6	1.3	0.7	0.9	8.3	8.0	7.7	8.0
II	–	–	–	–	0.2	−6.1	5.1	12, 13	−17.4	2	−3.4	−0.9	−2.6	−2.4	4.2	4.6	4.5	4.4	8.5	7.8	8.5	8.3	0.8	1.2	0.8	0.9	8.9	9.0	8.2	8.7
III	–	–	–	–	2.8	−5.1	13.2	31	−14.4	15	−3.6	1.7	−1.6	−1.3	4.4	4.9	4.7	4.7	8.9	6.8	8.3	8.0	0.6	2.3	0.9	1.3	7.7	7.4	6.8	7.3
IV	–	–	–	–	14.5	3.9	27.1	23	−2.5	11	6.6	13.2	8.0	9.0	7.8	7.7	7.9	7.8	8.0	5.4	7.4	6.9	2.4	9.4	3.4	5.1	6.8	7.0	5.7	6.5
V	–	–	–	–	14.7	4.6	21.7	19	−3.7	1	7.5	12.4	8.7	9.3	9.6	9.6	10.2	9.8	9.1	6.7	8.9	8.2	1.0	5.4	1.3	2.6	8.4	8.3	7.6	8.1
VI	–	–	–	–	19.3	6.9	29.2	16	0.1	3	11.9	17.6	12.2	13.5	11.6	11.2	11.9	11.6	8.0	5.4	8.0	7.1	2.9	10.5	3.0	5.5	5.3	5.8	4.8	5.3
VII	–	–	–	–	20.4	8.9	31.3	26	2.8	9	12.9	19.0	13.5	14.7	13.4	12.8	13.4	13.2	8.9	5.9	8.6	7.8	1.8	9.9	2.3	4.7	6.6	7.1	6.5	6.7
VIII	–	–	–	–	22.6	9.1	33.7	13	3.4	31	13.8	20.8	13.9	15.6	14.1	14.0	13.9	14.0	8.9	5.7	8.6	7.7	1.9	11.3	2.3	5.2	5.4	6.3	3.7	5.1
IX	–	–	–	–	17.6	5.0	28.8	4	−1.1	15	8.3	16.0	10.5	11.3	10.4	11.2	10.6	10.7	9.3	6.3	8.4	8.0	0.9	7.9	2.7	3.8	6.5	6.5	4.4	5.8
X	–	–	–	–	13.7	2.2	22.6	2, 3, 4	−4.7	22	3.7	12.9	5.7	7.0	7.7	9.4	8.6	8.6	9.3	6.4	9.1	8.3	0.5	6.3	0.9	2.6	6.0	4.8	4.5	5.1
XI	–	–	–	–	5.1	1.3	16.3	8	−5.6	24	2.6	4.3	3.2	3.3	6.6	7.0	6.9	6.8	6.7	6.2	8.6	8.5	1.1	1.7	1.2	1.3	8.9	8.8	8.8	8.8
XII	–	–	–	–	−3.1	−8.8	3.3	12, 13	−20.0	28	−6.4	−4.0	−5.9	−5.6	3.5	3.7	3.6	3.6	8.4	7.7	8.4	8.2	0.6	1.1	0.6	0.8	8.6	7.6	8.3	8.2
Rok	–	–	–	–	10.8	1.5	33.7	13.VIII	−20.0	28.XII	4.4	9.4	5.4	6.2	8.2	8.4	8.4	8.3	8.8	6.7	8.5	8.0	1.3	5.7	1.7	2.9	7.3	7.2	6.4	7.0

Góra Św. Anny $\varphi = 50°27'$ $\lambda = 18°10'$

I	–	–	–	–	1.4	−3.0	9.0	20	−16.6	31	−1.6	0.1	−1.0	−0.9	5.2	5.6	5.5	5.4	9.2	8.8	9.3	9.1	0.4	0.8	0.4	0.5	–	–	–	–
II	–	–	–	–	−0.6	−5.4	4.3	17	−13.0	1	−3.4	−1.7	−2.1	−2.3	4.3	4.9	4.8	4.7	8.9	8.9	9.1	9.0	0.5	0.7	0.5	0.6	–	–	–	–
III	–	–	–	–	2.0	−4.9	14.3	31	−8.5	14	−2.0	0.5	−1.1	−0.9	5.0	5.6	5.3	5.3	9.2	8.5	9.3	9.0	0.5	1.1	0.5	0.7	–	–	–	–
IV	–	–	–	–	14.4	6.2	26.7	25	0.4	30	8.9	13.3	8.3	9.7	7.6	7.8	9.4	8.3	7.8	5.6	8.4	7.3	3.2	9.3	2.5	5.0	–	–	–	–
V	–	–	–	–	14.4	6.4	21.1	19	−2.0	1	9.5	12.3	10.0	10.4	10.2	10.4	10.2	10.3	8.5	7.3	8.2	8.0	1.9	4.4	2.4	2.9	–	–	–	–
VI	–	–	–	–	–	9.7	–	–	1.4	2	12.5	17.1	13.8	14.3	11.9	11.7	12.2	11.9	7.9	6.0	7.5	7.1	3.3	9.2	4.6	5.7	–	–	–	–
VII	–	–	–	–	20.0	11.4	28.3	26	6.4	6	13.5	17.9	15.4	15.6	13.0	12.6	13.4	13.0	8.4	6.2	7.7	7.4	2.9	8.6	4.4	5.3	–	–	–	–
VIII	–	–	–	–	22.5	13.3	29.9	7, 13	8.9	31	15.0	20.9	16.7	17.3	13.9	13.8	15.2	14.3	8.1	5.6	8.0	7.2	3.4	11.6	4.1	6.4	–	–	–	–
IX	–	–	–	–	17.1	8.4	28.8	4	4.2	20	10.2	15.1	12.4	12.5	10.8	11.2	10.6	10.9	8.6	6.8	7.5	7.6	2.0	6.7	4.5	4.4	–	–	–	–
X	–	–	–	–	13.2	5.3	22.0	4	0.0	22	6.6	11.4	8.2	8.6	9.3	10.1	9.6	9.7	9.4	7.5	8.7	8.5	0.6	4.0	1.6	2.1	–	–	–	–
XI	–	–	–	–	6.0	1.4	16.3	8	−3.6	24	2.7	5.0	3.2	3.5	7.0	7.6	7.1	7.2	9.2	8.5	9.0	8.9	0.7	1.7	0.9	1.1	–	–	–	–
XII	–	–	–	–	−2.6	–	5.9	13	–	–	−5.4	−3.5	−5.6	−5.0	4.0	4.4	3.9	4.1	9.1	8.9	8.8	9.0	0.4	0.6	0.5	0.5	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	5.5	9.0	6.5	6.9	8.5	8.8	8.9	8.7	8.7	7.4	8.5	8.2	1.6	4.9	2.2	2.9	–	–	–	–

Korfantów $H_s = 200\,m$ $h_w = 12{,}5\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T. Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◑	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	33	9.1	26	3	5	18	·	—	—	5	14	12	7	·	1	14	—
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	18	5.3	18	5	11	24	·	—	—	2	17	17	6	·	·	17	—
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	37	14.5	12	·	8	26	·	—	—	3	13	11	7	1	1	9	—
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	30	12.1	4	·	·	·	6	—	—	6	12	11	7	1	·	·	—
V	4	2.5	0.5	1.0	0.5	0.3	6.5	2.0	10.5	1.6	12.5	2.3	10	3.2	20.5	3.0	28	1.8	145	28.6	14	·	·	1	·	1	·	1	7	25	21	5	·	·	—
VI	10.5	3.4	0.5	1.0	2.5	2.2	7	1.8	3.5	3.7	5.5	3.7	16.5	3.3	27	3.7	17	2.7	15	11.0	1	·	·	·	7	·	·	6	7	6	3	1	·	·	—
VII	3	2.8	·	·	1	1.0	2.5	2.6	6.5	2.8	16.5	1.8	29	2.5	26.5	2.8	8	2.3	61	23.3	22	·	·	·	7	·	·	6	12	15	10	1	·	·	—
VIII	3	2.2	1	1.5	4.5	3.1	5.5	1.7	11	3.6	16	2.8	27	3.3	10	4.2	15	2.7	44	13.0	7	·	·	·	12	2	·	6	6	10	8	1	2	·	—
IX	0.5	4.0	0.5	1.0	4	1.6	16.5	2.0	8	1.9	13.5	3.0	23.5	4.0	12.5	3.4	11	2.6	78	28.5	18	·	·	·	4	2	·	6	7	10	7	3	5	·	—
X	1	4.0	1	1.0	6	2.0	21.5	2.5	10	2.3	8.5	2.0	19	2.7	14	2.9	12	2.2	43	24.9	31	·	·	5	·	·	·	6	11	9	5	1	11	·	—
XI	0.5	3.0	7	2.9	4.5	2.4	23.5	4.1	6	5.9	6	2.7	25	2.6	10.5	2.4	7	3.0	54	12.8	19	·	1	10	·	2	·	·	23	14	12	2	4	3	—
XII	4.5	1.4	1.5	1.7	3.5	1.8	8	1.8	5.5	4.1	16	3.5	13.5	3.1	21.5	2.6	19	2.2	24	5.3	30	10	16	27	·	2	·	1	18	17	8	·	4	15	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	582	28.6	14.V	18	41	111	36	—	—	48	147	157	101	16	28	58	—

Otmuchów $H_s = 211\,m$ $h_w = 11\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	5	2.2	0.5	1.0	1.5	1.0	0.5	2.0	7	2.5	14.5	2.5	26	3.0	22	3.9	16	2.5	30	7.8	26	1	4	18	·	1	·	1	10	13	7	·	2	10	—
II	7	3.1	5.5	1.7	9.5	1.4	·	·	1.5	1.3	3	4.0	21	4.3	19.5	4.4	17	2.8	28	4.6	12	6	10	23	·	3	·	·	21	15	10	·	2	19	—
III	6.5	2.8	5.5	2.6	15.5	2.0	2	2.0	4	1.8	5	2.7	7	2.0	19.5	2.7	28	1.7	44	16.0	12	·	8	23	·	·	·	1	14	12	7	1	1	8	—
IV	6	2.7	8	1.6	5.5	2.4	2.5	2.4	7	3.1	2	2.2	19.5	2.5	16.5	2.8	23	1.9	33	6.1	4	·	·	1	7	·	·	4	17	12	9	·	3	·	—
V	6	1.7	2	1.0	7.5	1.4	2.5	1.4	·	·	1.5	3.0	25	2.4	22.5	2.7	26	1.6	134	31.2	14	·	·	3	·	·	·	·	15	25	20	3	·	·	—
VI	14	2.7	1.5	1.7	4	2.0	2	1.5	1	1.5	5	1.3	12.5	3.0	27	2.9	23	1.9	21	5.5	1	·	·	·	8	·	·	5	12	8	7	·	·	·	—
VII	5	1.5	2.5	1.0	3.5	1.1	1	1.5	2	1.0	2.5	2.0	17.5	2.2	15	2.1	44	1.0	78	44.5	17	·	·	·	5	·	·	3	11	16	10	2	3	·	—
VIII	6.5	2.2	4	1.7	2.5	1.4	3	1.3	0.5	3.0	2	1.7	23	2.6	22.5	2.9	29	1.7	30	7.0	7	·	·	·	12	·	·	1	7	13	8	·	4	·	—
IX	4	1.6	3.5	1.6	3.5	1.7	0.5	2.0	2	1.5	3	4.5	17	2.1	19.5	2.4	37	1.3	64	27.5	17	·	·	·	5	·	·	7	8	11	5	2	7	·	—
X	13	1.7	6.5	1.3	12.5	1.2	1.5	1.0	·	·	1.5	1.3	9	1.6	16	2.0	33	1.0	43	21.6	31	·	·	7	·	·	·	6	14	11	6	1	20	·	—
XI	4.5	1.7	14	1.8	5.5	2.1	6.5	2.8	2	3.5	3	1.8	11	2.0	14.5	1.6	29	1.3	59	13.0	1	·	·	10	·	·	·	·	21	13	12	1	9	·	—
XII	8	1.5	2	1.5	·	·	1.5	2.3	5.5	2.6	4	3.1	13.5	3.0	23.5	1.8	35	1.4	23	6.2	31	10	14	27	·	·	·	2	20	14	8	·	1	15	—
Rok	85.5	2.1	55.5	1.5	71	1.5	23.5	1.7	32.5	1.8	47	2.5	202	2.6	238	2.7	340	1.7	587	44.5	17.VII	17	36	112	37	4	·	30	170	163	109	10	52	52	—

Kudowa-Zdrój $H_s = 385\,m$ $h_w = 13{,}5\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	2	2.8	7	1.5	0.5	1.0	0.5	1.0	11	2.8	5.5	1.7	43.5	2.1	4	2.4	19	1.7	58	17.8	12	4	8	22	·	—	—	·	17	15	12	1	7	16	·
II	6	1.8	9	1.9	5.5	2.4	1	3.0	3	2.0	5	2.5	26.5	1.9	4	1.8	24	1.4	85	17.3	16	5	11	28	·	—	—	·	19	19	15	3	10	28	·
III	3.5	1.3	13.5	1.8	7	3.4	1	2.0	3.5	1.7	3.5	2.3	20	1.8	2	1.2	39	1.2	63	16.2	31	4	8	27	·	—	—	1	15	13	9	2	3	23	·
IV	5	1.8	14	2.3	8.5	4.2	1	6.0	8	2.8	1	2.0	26	2.4	1.5	1.7	25	1.9	31	10.7	26	·	·	2	7	—	—	2	11	13	7	1	1	·	1
V	2.5	1.8	12.5	1.6	2	2.0	·	·	2.5	1.8	3	1.3	32	1.8	4.5	2.6	34	1.2	108	21.9	14	·	·	3	·	—	—	·	16	25	17	3	6	·	2
VI	3	1.0	9.5	1.8	2	3.5	·	·	1	3.0	·	·	24	2.2	5.5	2.0	45	1.1	20	8.7	11	·	·	·	6	—	—	2	5	7	4	·	·	·	2
VII	8	1.1	11	1.3	1	3.0	·	·	2	2.0	·	·	23.5	1.9	5.5	2.4	42	0.9	45	11.0	11		·	·	5	—	—	·	13	14	10	1	1	·	2
VIII	5.5	2.0	7.5	1.4	·	·	·	·	·	·	·	·	24.5	2.5	8.5	2.4	47	1.1	29	6.1	5	·	·	·	7	—	—	4	3	13	8	·	1	·	2
IX	8.5	1.7	10	1.9	3	3.3	·	·	4	1.5	2.5	1.8	15	2.4	8	1.6	39	1.1	66	17.2	18	·	·	3	3	—	—	4	9	14	10	2	9	·	·
X	4.5	1.3	7.5	1.9	2	4.0	·		·	·	1.5	1.0	12.5	2.1	5	1.5	60	0.7	38	24.6	31	·		7	·	—	—	8	9	7	6	1	9	·	·
XI	5.5	1.3	11.5	2.4	11	4.3	1	3.5	5	2.2	2.5	1.0	7.5	1.3	2	1.5	44	1.2	55	13.1	-1	·	1	12	·	—	—	·	22	13	10	1	3	·	·
XII	4.5	1.6	7.5	1.8	7.5	2.2	0.5	1.0	2	3.8	5	1.5	16.5	2.0	3.5	1.4	46	1.0	52	16.2	15	14	21	29	·	—	—	·	19	16	14	1	3	28	·
Rok	58.5	1.6	120.5	1.8	50	2.8	5	1.4	42	2.0	29.5	1.3	271.5	2.0	54	1.9	464	1.2	650	24.6	31.X	27	49	133	28	—	—	21	158	169	122	16	53	95	9

Góra Św. Anny $H_s = 370\,m$ $h_w = 16\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	11	5.9	4	5.1	2	2.5	7	2.5	42	6.0	7	2.2	14.5	3.8	2.5	2.0	3	4.7	58	11.4	25	2	11	25	·	8	3	—	—	14	10	3	2	12	·
II	12.5	3.4	2.5	2.4	12.5	1.6	6	1.8	11	6.5	5	6.9	15	8.3	17.5	5.4	2	4.8	27	3.6	19	3	15	28	·	6	4	—	—	20	10	·	2	28	1
III	22	3.8	11.5	3.1	15	2.8	5.5	1.5	15.5	3.0	2	8.0	7	3.9	11.5	5.8	3	3.5	74	16.0	17	·	15	25	·	5	·	—	—	17	11	2	2	17	·
IV	14.5	3.3	4.5	1.6	6.5	2.5	4	5.5	26.5	6.6	3.5	4.4	16	3.9	14.5	3.9	·	4.5	44	8.4	4	·	·	·	4	6	3	—	—	15	10	·	1	·	·
V	13	1.5	5.5	1.3	4.5	2.3	3.5	1.4	21.5	2.4	11	1.8	21	4.4	10	2.8	3	2.5	171	20.1	13	·	·	2	·	2	·	—	—	26	24	7	2	·	4
VI	15.5	3.6	1.5	1.7	7.5	1.3	1.5	1.7	13.5	2.3	6	4.0	27	3.4	17.5	4.4	·	3.3	57	26.2	1	·	·	·	—	2	·	—	—	12	7	2	1	·	1
VII	11	2.4	3	1.5	2	1.5	1.5	1.7	18.5	2.8	10.5	2.9	22.5	3.2	23	3.0	1	2.8	63	16.6	22	·	·	·	4	·	·	—	—	15	12	1	1	·	6
VIII	6.5	1.4	4.5	1.1	3	3.3	4	1.4	21.5	3.5	6	3.0	33.5	3.2	13	3.6	1	3.0	42	12.2	7	·	·	·	7	1	1	—	—	13	8	1	2	·	5
IX	6.5	3.5	1	3.0	13.5	2.7	9	2.4	19.5	4.1	10	4.0	24.5	2.8	4	1.8	2	3.1	95	41.3	17	·	·	·	2	2	·	—	—	13	8	3	6	·	1
X	14	2.3	3.5	2.6	24.5	1.4	9.5	2.1	13.5	2.5	4.5	1.4	9	2.7	11.5	2.2	3	2.0	41	17.8	31	·	·	·	·	1	·	—	—	9	6	2	16	·	·
XI	20	2.0	9	1.1	16	4.4	13	4.2	10	4.3	·	·	16.5	1.9	5.5	2.1	·	2.9	68	15.4	15	·	2	13	·	3	·	—	—	17	14	3	14	4	·
XII	21	2.2	8	2.6	12	1.1	9	3.7	7	7.0	7	5.4	12	1.8	17	2.4	·	2.8	27	4.3	10	—	19	—		3	2	—	—	16	8	·	4	23	·
Rok	167.5	2.9	58.5	2.3	119	2.3	73.5	2.5	220	4.2	72.5	3.7	218.5	3.6	147.5	3.3	18	3.3	767	41.3	17.IX	—	62	—	—	39	13	—	—	187	128	24	53	84	18

Busko-Zdrój $\varphi = 50°27'$ $\lambda = 20°43'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.8	-3.4	7.4	20	-16.4	31	-1.8	0.7	-1.2	-0.9	5.0	5.4	5.1	5.2	90	82	88	87	0.6	1.3	0.7	0.9	7.3	6.5	6.5	6.8
II	–	–	–	–	0.3	-4.8	5.7	12	-12.0	1	-3.4	-1.2	-2.3	-2.3	4.4	5.0	4.8	4.7	91	87	92	90	0.4	0.8	0.4	0.5	9.2	8.7	8.8	8.9
III	–	–	–	–	2.2	-4.7	13.5	31	-10.7	21	-2.8	1.1	-1.8	-1.3	4.7	5.3	5.0	5.0	90	78	90	86	0.5	1.6	0.6	0.9	6.8	7.2	6.4	6.8
IV	–	–	–	–	16.2	6.1	26.4	23	-0.3	2	8.9	14.5	10.0	10.8	9.1	8.9	8.9	9.0	80	57	74	70	2.8	9.2	4.2	5.4	5.1	5.6	4.6	5.1
V	–	–	–	–	15.5	7.0	22.0	8	-1.9	1	10.0	13.5	10.4	11.1	11.0	11.0	11.3	11.1	88	73	88	83	1.5	5.0	1.7	2.8	7.4	8.2	6.3	7.3
VI	–	–	–	–	19.3	9.7	29.7	23	2.5	2	12.8	17.2	13.7	14.4	12.7	12.2	12.6	12.5	83	63	78	75	2.8	8.9	3.9	5.2	5.5	7.1	5.3	6.0
VII	–	–	–	–	21.5	11.3	29.4	26	7.4	9	14.1	19.7	15.1	16.0	13.8	13.6	14.2	13.9	85	60	82	76	2.5	10.0	3.3	5.3	6.0	7.0	5.8	6.3
VIII	–	–	–	–	22.8	12.7	30.1	7	6.5	31	14.8	21.5	16.6	17.4	15.1	15.5	15.5	15.4	89	61	81	77	2.0	10.8	3.7	5.5	5.1	5.8	4.5	5.1
IX	–	–	–	–	18.0	7.9	27.8	4	2.4	25	9.7	16.3	11.6	12.3	10.8	11.8	11.6	11.4	90	65	85	80	1.4	7.6	2.4	3.8	6.3	5.9	3.3	5.2
X	–	–	–	–	12.8	3.8	17.7	1	-2.4	24	5.1	11.3	7.3	7.8	8.6	9.7	9.3	9.2	95	72	89	84	0.5	3.9	1.0	1.8	7.2	5.4	4.1	5.6
XI	–	–	–	–	6.9	2.3	16.3	4	-1.8	17, 23, 24	3.2	5.9	3.9	4.2	7.4	8.0	7.6	7.7	94	85	92	90	0.5	1.8	0.7	1.0	7.7	8.1	8.5	8.1
XII	–	–	–	–	-1.8	-7.2	4.9	12	-18.8	22	-5.4	-3.0	-5.1	-4.6	3.9	4.2	4.0	4.0	89	82	89	87	0.5	1.0	0.5	0.7	8.0	7.9	7.3	7.7
Rok	–	–	–	–	11.3	3.4	30.1	7.VIII	-18.8	22.XII	5.4	9.8	6.5	7.0	8.9	9.2	9.2	9.1	89	72	86	82	1.3	5.2	1.9	2.8	6.8	7.0	6.0	6.6

Tomaszów Lubelski $\varphi = 50°27'$ $\lambda = 23°25'$

I	–	–	–	–	1.9	-3.9	7.5	22	-17.9	31	-1.8	0.7	-1.2	-0.9	4.8	5.3	4.9	5.0	85	80	85	83	0.8	1.4	0.9	1.0	8.2	7.4	7.3	7.6
II	–	–	–	–	-1.0	-7.4	2.6	13	-15.1	25	-5.3	-2.2	-4.0	-3.9	3.5	4.4	3.8	3.9	81	82	81	81	0.7	1.0	0.8	0.8	9.2	9.1	9.2	9.2
III	–	–	–	–	1.0	-7.0	13.8	5	-21.4	21	-4.5	-0.2	-3.2	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.2	8.1	8.3
IV	–	–	–	–	16.0	4.1	26.0	24	-1.5	30	7.2	14.6	8.8	9.8	8.4	8.3	8.9	8.5	8.2	5.4	7.8	7.1	2.0	9.8	2.8	4.9	6.2	5.7	5.2	5.7
V	–	–	–	–	16.5	6.7	24.2	14	-0.9	2	9.6	14.6	10.0	11.0	11.0	11.9	11.5	11.5	8.9	7.0	9.1	8.3	1.3	5.5	1.2	2.7	7.9	8.0	7.3	7.7
VI	–	–	–	–	19.1	8.9	28.4	25	2.9	6, 7	13.2	17.3	12.7	14.0	12.9	12.8	12.9	12.9	8.3	6.6	8.6	7.8	2.9	8.4	2.3	4.5	6.6	7.7	7.3	7.2
VII	–	–	–	–	20.9	10.4	30.0	27	5.5	30	14.3	19.4	13.9	15.4	14.1	14.2	14.1	14.1	8.6	6.4	8.8	7.9	2.5	8.8	2.0	4.4	6.4	7.2	6.7	6.8
VIII	–	–	–	–	22.9	11.3	31.0	13	4.9	27	15.2	21.4	15.6	17.0	15.7	16.3	15.9	16.0	8.9	6.5	8.9	8.1	1.8	10.0	2.1	4.6	6.1	6.8	6.0	6.3
IX	–	–	–	–	18.0	7.4	28.6	5	0.6	26	9.9	16.1	11.2	12.1	11.0	12.0	11.8	11.6	8.9	6.7	8.8	8.1	1.5	7.0	1.9	3.5	5.8	6.8	6.4	6.3
X	–	–	–	–	13.6	1.6	19.2	2	-5.0	16	4.0	12.3	5.5	6.8	7.4	9.7	8.2	8.4	8.8	6.7	8.8	8.1	1.1	4.9	1.1	2.4	7.3	6.2	4.2	5.9
XI	–	–	–	–	7.4	1.3	18.9	1	-4.5	18	2.8	5.9	3.6	4.0	6.8	7.7	7.2	7.2	8.9	8.2	8.8	8.6	0.8	2.0	0.9	1.2	8.9	8.2	8.0	8.4
XII	–	–	–	–	-2.4	-7.8	4.7	13	-19.3	22	-6.1	-3.8	-5.4	-5.2	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.3	8.9	8.7
Rok	–	–	–	–	11.2	2.1	31.0	13.VIII	-21.4	21.III	4.9	9.7	5.6	6.4	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.5	7.0	7.3

Kłodzko $\varphi = 50°26'$ $\lambda = 16°39'$

I	979.4	998.0	955.2	1019.0	2.2	-3.1	8.9	22	-13.6	31	-1.0	0.7	-0.7	-0.4	5.1	5.1	5.0	5.1	8.5	7.8	8.4	8.2	1.0	1.5	1.0	1.2	8.4	8.2	7.6	8.1
II	978.9	995.8	94.94	1018.8	0.5	-5.7	6.5	12, 13	-20.3	2	-3.3	-1.1	-2.1	-2.2	4.3	4.7	4.7	4.6	8.6	8.1	8.6	8.4	0.7	1.1	0.8	0.9	8.9	9.1	9.0	9.0
III	972.8	989.8	954.1	1012.2	2.5	-4.5	14.7	31	-12.7	14	-3.4	1.2	-0.9	-1.0	4.5	4.7	4.8	4.7	8.8	6.8	8.0	7.9	0.6	2.2	1.1	1.3	8.1	7.9	7.2	7.7
IV	976.5	989.2	950.9	1014.7	14.4	4.4	26.6	23	-0.1	1.1	6.0	12.9	8.8	9.1	7.8	7.7	8.1	7.9	8.4	5.6	7.2	7.1	1.9	8.9	3.9	4.9	7.6	7.3	6.6	7.2
V	976.4	982.2	966.7	1014.4	14.8	5.7	22.5	8	-1.3	5	8.1	13.1	9.6	10.1	9.6	9.4	10.3	9.8	8.7	6.2	8.4	7.8	1.4	6.2	2.0	3.2	8.2	8.7	8.0	8.3
VI	982.1	991.7	972.9	1019.3	19.1	8.1	28.4	23	1.7	8	11.6	17.6	13.2	13.9	11.5	11.0	12.1	11.5	8.0	5.3	7.7	7.0	2.9	10.6	3.7	5.7	5.7	6.2	5.6	5.8
VII	978.5	987.9	965.7	1016.0	20.6	9.3	29.8	26	3.4	9	12.5	19.0	14.0	14.9	13.0	12.4	13.2	12.9	8.8	5.7	8.2	7.6	1.9	10.3	3.2	5.1	6.3	7.4	6.6	6.8
VIII	979.8	986.8	965.9	1017.2	23.1	10.4	31.1	13	3.1	31	13.6	21.4	14.7	16.1	13.7	13.2	14.1	13.7	8.7	5.2	8.3	7.4	2.1	13.0	2.8	6.0	6.2	7.2	4.1	5.8
IX	979.9	989.9	965.7	1017.8	17.9	6.4	28.9	12	-0.9	15	8.5	16.1	11.2	11.8	10.2	11.0	10.7	10.6	9.1	6.3	8.2	7.9	1.5	8.2	3.2	4.3	7.1	6.4	4.9	6.1
X	984.7	996.1	971.5	1023.4	13.1	3.3	23.7	4	-4.4	22, 23	4.5	11.9	6.6	7.4	8.3	9.8	9.2	9.1	9.6	7.1	9.3	8.7	0.4	5.1	0.8	2.1	7.7	5.0	5.7	6.1
XI	978.1	994.8	960.3	1017.1	5.4	1.3	15.8	8	-5.3	24	2.5	4.6	3.2	3.4	6.7	7.2	7.1	7.0	9.0	8.3	8.9	8.7	0.9	1.7	1.0	1.2	8.4	8.9	8.0	8.4
XII	978.3	1005.4	937.6	1018.7	-2.7	-8.2	4.0	13	-19.4	28	-6.2	-4.2	-5.5	-5.4	3.8	4.0	3.9	3.9	9.1	8.4	9.0	8.8	0.4	0.8	0.5	0.6	8.5	7.5	7.8	7.9
Rok	978.8	1005.4	937.6	1017.6	10.9	2.3	31.1	13.VIII	-20.3	2.II	4.4	9.4	6.0	6.4	8.2	8.4	8.6	8.4	8.8	6.7	8.4	8.0	1.3	5.8	2.0	3.0	7.6	7.5	6.8	7.3

Świerklaniec $\varphi = 50°26'$ $\lambda = 18°57'$

I	–	–	–	–	2.3	-2.8	8.2	22	-19.6	31	-1.0	1.4	-0.6	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.3	7.4	8.0
II	–	–	–	–	0.4	-5.3	5.0	12	-18.0	3	-3.6	-0.9	-2.3	-2.3	–	–	–	–	–	–	–	–	–	–	–	–	9.5	9.1	8.0	8.9
III	–	–	–	–	2.9	-5.0	14.9	31	-13.6	21	-3.5	1.5	-1.8	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.8	6.4	7.6
IV	–	–	–	–	15.5	4.9	27.2	23	-0.2	6	7.7	14.0	9.1	10.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.8	6.0	7.2
V	–	–	–	–	15.3	7.0	22.1	8	-1.9	3	9.0	13.3	10.1	10.6	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.2	8.0	8.3
VI	–	–	–	–	19.2	8.9	30.0	23	0.6	2	13.0	17.9	13.5	14.5	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.7	7.1	6.7
VII	–	–	–	–	20.4	10.3	29.6	26	5.0	30	14.0	19.3	14.6	15.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.6	6.3	7.0
VIII	–	–	–	–	23.2	11.4	31.0	7	5.4	31	14.9	21.4	15.3	16.7	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.1	4.8	6.6
IX	–	–	–	–	17.8	6.9	27.7	4	0.1	15	9.6	16.0	10.4	11.6	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.5	3.9	6.4
X	–	–	–	–	13.7	3.3	22.2	3	-3.9	16	4.9	12.5	6.7	7.7	–	–	–	–	–	–	–	–	–	–	–	–	9.1	6.9	4.3	6.8
XI	–	–	–	–	6.3	1.6	17.9	8	-2.0	24	2.8	5.6	3.4	3.8	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.9	8.3	8.9
XII	–	–	–	–	-2.2	-7.7	7.1	13	-20.7	21	-5.8	-3.3	-5.3	-4.9	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.1	8.1	8.1
Rok	–	–	–	–	11.2	2.8	31.0	7.VIII	-20.7	21.XII	5.2	9.9	6.1	6.8	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.8	6.6	7.5

Busko-Zdrój $H_s = 440 m$ $h_w = 14 m$ 1962

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v>10	v>15	◷	●	Opad R≥0.1	R≥1.0	R≥10.0	═	⊞	R/10
I	7	7.2	5	4.4	1	1.0	4	3.5	23.5	4.8	22.5	4.1	21.5	4.2	4.5	6.3	4	4.2	37	9.0	25	2	8	24	·	7	·	2	12	16	9	·	·	18	-
II	8.5	5.9	8.5	2.1	10	4.8	4.5	2.4	6	2.3	12	8.4	22	5.2	11.5	8.7	1	5.4	26	5.5	12	2	13	26	·	9	3	·	23	14	8	·	1	22	·
III	12.5	7.9	13	4.2	10	2.6	17	3.3	14	2.7	2.5	2.6	12	5.4	12	3.3	·	4.1	35	5.3	12	3	11	25	·	6	1	5	16	14	9	·	4	20	·
IV	9	3.6	14.5	4.0	5	3.4	16	4.7	15.5	4.3	11	3.0	6.5	3.9	10.5	4.4	2	3.9	57	18.6	6	·	·	1	2	6	1	9	5	16	11	1	2	·	1
V	7.5	2.7	1	5.0	6	2.5	7	3.7	10	2.8	19	4.0	19	5.7	15.5	4.0	8	3.6	80?	10.0	10	·	·	2	·	3	2	·	15	28	20	1	3	·	4
VI	13	3.2	9.5	3.3	4.5	1.3	4	1.6	6	1.5	6.5	2.8	18	3.8	24.5	4.8	4	3.3	87	33.0	4	·	·	·	6	3	·	3	8	15	8	2	1	·	2
VII	22.5	2.0	0.5	2.0	11	1.8	0.5	4.0	14.5	1.7	8.5	2.2	22.5	2.4	11	2.0	2	2.0	87	19.5	7	·	·	·	5	·	·	4	9	18	14	3	·	·	10
VIII	4	2.0	7	3.1	9.5	1.7	8	2.5	13	2.8	10.5	3.0	26.5	3.3	10.5	3.8	4	2.8	65	32.5	5	·	·	·	9	1	1	3	4	13	7	3	1	·	3
IX	3	3.0	4	3.2	10.5	3.4	10	2.1	10	2.8	18	3.2	15.5	3.4	11	4.0	8	2.9	41	14.0	18	·	·	·	4	1	1	7	6	20	8	1	3	·	1
X	7	1.9	8	3.1	19	2.5	10	1.9	4	1.6	10.5	2.4	12.5	2.7	7	3.1	15	2.1	3	1.4	31	·	·	7	·	·	·	5	7	8	1	·	14	·	-
XI	8.5	2.1	10.5	3.5	26.5	3.9	14	4.2	2.5	1.6	9.5	1.9	8	2.0	6.5	2.0	4	3.0	42?	10.3	•15		·	6	·	2	·	2	20	17	11	1	8	·	·
XII	8.5	2.7	11	4.0	7.5	2.7	5	3.8	12	5.0	10	4.3	22	2.3	8	2.4	9	2.9	28	5.8	14	10	15	31	·	2	·	1	16	16	11	·	6	17	·
Rok	111	3.7	92.5	3.5	120.5	2.6	100	3.1	131	2.8	140.5	3.5	206	3.7	132.5	4.1	61	3.4	588?	33.0	4.VI	17	47	122	28	40	9	41	141	195	117	12	43	77	21

Tomaszów Lubelski $H_s = 273 m$ $h_w = 12 m$

I	2	2.5	4.5	3.2	1.5	3.0	4.5	3.6	15	2.7	39.5	3.5	20	3.2	5	3.2	1	3.2	32	8.3	25	3	8	29	·	·	·	·	16	14	10	·	–	19	·
II	8.5	4.4	8	2.0	11.5	3.0	3.5	2.3	4.5	3.9	13	6.2	17.5	5.2	15.5	4.7	2	4.2	61	15.2	12	8	14	28	·	6	·	·	24	19	12	2	–	28	·
III	6	8.5	15.5	4.6	13	2.7	12	5.1	7.5	3.1	13	4.2	9	6.3	14	3.5	3	4.3	47	10.8	16	7	18	29	·	4	1	1	21	16	11	1	–	31	·
IV	6.5	2.8	22	4.1	9	4.0	9	4.1	10	4.6	14	4.7	14	5.4	4.5	4.1	1	4.4	42	12.8	6	·	·	4	4	2	·	4	9	9	7	1	–	1	·
V	7	2.6	4.5	3.1	3	2.3	5.5	4.7	7.5	3.7	19.5	4.7	22	4.2	24	3.9	·	4.0	119	14.8	8	·	·	3	·	2	·	·	13	19	16	7	–	·	5
VI	16.5	3.8	6.5	3.8	3	5.7	·	·	0.5	4.0	16.5	5.1	15.5	4.5	31.5	4.2	·	4.4	124	41.7	1	·	·	·	6	1	·	1	13	15	12	4	–	·	5
VII	15	3.1	1	2.0	3	2.3	3	3.3	4.5	2.2	22.5	4.4	19	4.2	24	3.2	1	3.6	91	27.6	18	·	·	·	5	·	·	2	11	15	14	2	–	·	4
VIII	4	2.0	5	2.4	6	2.7	5	4.6	5	5.1	24.5	4.4	24	4.0	14.5	3.4	5	3.5	38	12.0	16	·	·		9	·		·	6	13	8	1	–	·	4
IX	2	1.5	9	2.4	4	3.2	7.5	2.7	9	5.1	25	3.7	27.5	3.9	1	3.0	5	3.4	45	14.5	5	·	·	·	2	1	·	4	11	14	8	1	–	·	1
X	14	2.5	5	2.4	12.5	3.0	14	2.7	2.5	2.8	15.5	4.2	12	3.8	8.5	2.7	9	2.8	5	1.8	19	·	·	12	·	-	·	1	9	5	2	-	–	·	·
XI	5	2.4	9.5	3.7	30	4.3	13.5	4.4	2.5	1.6	12.5	4.2	7	2.1	8	2.5	2	3.6	52	13.8	16	·	·	10	·	2	·	1	22	16	11	1	–	·	
XII	16	3.0	5.5	3.5	5	2.0	6	3.5	12.5	3.8	20	4.0	14	2.7	9	2.5	5	3.2	21	6.0	16	10	17	30	·	·	·	1	24	16	8	·	–	13	·
Rok	102.5	3.3	96	3.1	101.5	3.2	83.5	3.4	81	3.6	235.5	4.4	201.5	4.1	159.5	3.4	34	3.7	677	41.7	1.VI	28	57	145	26	18	1	15	179	171	119	20	–	92	19

Kłodzko $H_s = 316 m$ $H_b = 317,3 m$ h_w = 15,0 m I–XI, 13,6 m XII

I	9	4.7	2	4.0	·	·	2.5	5.2	22.5	6.9	15	3.6	17.5	3.5	9.5	4.0	15	4.0	26	6.4	26	5	8	19	·	7	·	·	17	18	6	·	·	15	·
II	19	2.8	3	2.3	0.5	1.0	·	·	10.5	5.3	5	5.5	15.5	4.8	14.5	4.9	16	3.4	44	9.3	12	4	11	25	·	4	2	·	21	20	11	·	2	23	
III	19	3.3	6	3.0	0.5	2.0	2	3.8	9	5.0	5	3.4	6	3.0	12.5	4.3	33	2.4	57	16.6	12	3	9	25	·	·	·	1	18	12	8	3	3	21	·
IV	9.5	3.2	7	2.4	2.5	3.2	2.5	5.2	14.5	5.1	8	3.9	9	4.0	11	4.4	26	3.1	26	7.5	26		·	1	5	3	1	3	16	13	7	·	1	·	3
V	3.5	2.3	5	1.4	·	·	·	·	3.5	4.0	12.5	3.4	23	3.6	9.5	0.9	36	1.9	105	24.4	14	·	·	3	·	·	·	·	18	22	16	3	·	·	2
VI	15	3.7	3	2.0	·	·	0.5	5.0	4	3.0	1.5	3.3	16.5	4.3	14.5	2.3	35	2.0	53	26.8	16	·	·	·	6	1	·	4	9	9	6	2	·	·	3
VII	8	2.4	0.5	1.0	1	2.0	·	·	9	3.8	5	3.1	24	3.4	2.5	1.8	43	1.7	30	6.7	13	·	·	·	6	·	·	2	13	15	8	·	·	·	5
VIII	3.5	1.9	·	·	·	·	·	·	3.5	3.9	9.5	4.4	26.5	3.8	7	2.4	43	1.9	53	13.0	14	·	·	·	9	1	·	2	6	13	11	1	3	·	5
IX	2	2.5	0.5	3.0	0.5	3.0	1	2.0	13.5	4.7	8	4.4	8.5	4.0	11	3.0	45	2.0	67	20.9	17	·	·	1	3	1	·	2	10	10	7	3	9	·	·
X	9.5	2.3	3	2.0	·	·	0.5	3.0	6	4.5	2	2.8	8.5	2.5	7.5	2.5	56	1.1	41	20.4	31	·	·	6	·	1	·	4	12	9	5	1	17	·	·
XI	7.5	2.0	2.5	2.0		·	3	4.2	18.5	6.0	6.5	3.3	10	3.2	4	2.0	38	2.3	61	24.1	1	·	1	13	·	3	·	1	19	13	10	1	6	8	·
XII	14	2.6	9.5	3.4	1.5	3.7	1.5	3.7	12	6.8	9	4.8	9.5	3.3	9	2.2	27	2.7	23	5.0	31	13	20	28		4	3	1	20	18	12	·	3	26	·
Rok	119.5	2.8	42	2.2	6.5	1.2	13.5	2.7	126.5	4.9	87	3.8	174.5	3.6	112.5	2.9	413	2.4	586	26.8	16.VI	25	49	121	29	25	6	20	179	172	107	14	44	93	18

Świerklaniec $H_s = 284 m$ $h_w = 13,5 m$

I	5.5	4.1	2	3.0	·	·	2	1.0	11	3.6	48.5	5.1	12.5	4.1	11.5	4.0	·	4.5	52	8.8	25	2	5	22	·	3	·	–	–	14	10	·	1	17	·
II	5.5	3.0	6.5	2.8	8	2.5	5	2.2	4	5.5	19	5.6	20	6.7	14	6.3	2	4.9	45	7.0	19	4	10	27	·	5	3	–	–	19	13	·	3	28	·
III	10	3.8	6	3.8	9.5	2.5	7	3.2	7	2.6	17	3.1	16	3.4	13.5	2.8	7	2.9	64	13.6	12	4	8	25	·	1	·	–	–	20	13	1	2	21	·
IV	5.5	2.5	3	2.8	4	2.5	8.5	2.9	11.5	4.6	15.5	3.0	22.5	3.2	17.5	3.3	2	3.2	84	19.6	13	·	·	1	6	·	·	–	–	16	11	3	1	·	1
V	1	2.5	·	·	1.5	2.3	6.5	2.4	4	2.5	24	3.5	39	3.9	16	3.0	1	3.4	148	22.4	13	·	·	2	·	2	·	–	–	24	20	5	3	·	3
VI	4	3.4	0.5	1.0	0.5	3.0	2.5	2.2	·	·	10.5	2.6	42.5	3.2	27.5	3.2	2	3.0	71	33.2	1	·	·	·	6	·	·	–	–	13	10	1	·	·	·
VII	1.5	3.3	2	2.0	1	2.0	1	3.0	5	2.6	19.5	3.5	41	3.0	20	2.4	2	2.8	112	47.2	17	·	·	·	5	·	·	–	–	15	10	2	·	·	5
VIII	1.5	2.7	2	2.0	1	3.0	2	2.8	4.5	3.8	17	3.5	53.5	3.3	9.5	2.1	2	3.1	69	32.0	15	·	·	·	11	·	·	–	–	14	9	1	1	·	4
IX	1.5	3.7	3	3.5	12	2.1	·	·	2.5	2.2	27	4.4	31	3.4	11	3.5	2	3.4	52	14.7	18	·	·	·	2	·	·	–	–	13	10	2	8	·	·
X	2	3.5	5	2.2	15.5	2.2	10.5	2.5	1.5	2.0	15.5	3.0	25	3.3	14	2.8	4	2.7	27	9.5	6	·	·	9	·	·	·	–	–	6	3	·	16	·	·
XI	3	2.8	5.5	3.2	10.5	2.0	17	2.9	7.5	2.0	12.5	3.6	19.5	3.0	14.5	2.8	·	2.8	76	16.5	15	·	2	9	·	·	·	–	–	19	13	3	5	5	·
XII	12	2.9	5.5	3.4	1	2.0	0.5	3.0	1	3.5	31	4.8	23	2.8	18	2.4	1	3.4	47	11.4	13	11	16	31	·	3	·	–	–	19	10	1	2	19	·
Rok	53	3.2	41	2.5	64.5	2.2	62.5	2.3	59.5	2.9	257	3.8	345.5	3.6	187	3.2	25	3.3	847	47.2	17.VII	21	41	126	30	14	3	–	–	192	132	19	42	90	13

Duszniki-Zdrój $\varphi = 50°24'$ $\lambda = 16°24'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o,m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.9	-3.9	9.8	20	-14.7	31	-2.5	0.8	-1.9	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	73	83	83	80
II	–	–	–	–	-0.8	-6.7	4.4	12	-19.7	2	-4.2	-1.6	-3.5	-3.1	–	–	–	–	–	–	–	–	–	–	–	–	88	95	83	89
III	–	–	–	–	1.1	-6.0	9.1	31	-13.7	14	-4.5	0.3	-2.7	-2.4	–	–	–	–	–	–	–	–	–	–	–	–	78	75	71	75
IV	–	–	–	–	12.8	3.7	24.7	23	-0.9	11	6.4	11.5	6.3	7.6	–	–	–	–	–	–	–	–	–	–	–	–	67	62	49	59
V	–	–	–	–	13.0	4.8	20.9	19	-3.0	1	7.6	11.4	7.7	8.6	–	–	–	–	–	–	–	–	–	–	–	–	75	69	64	69
VI	–	–	–	–	17.7	7.7	27.4	24	-0.2	6	12.0	16.5	11.2	12.7	–	–	–	–	–	–	–	–	–	–	–	–	48	55	51	51
VII	–	–	–	–	18.8	9.7	30.1	26	4.5	9	12.6	17.6	12.0	13.6	–	–	–	–	–	–	–	–	–	–	–	–	60	50	52	54
VIII	–	–	–	–	21.2	10.7	29.2	13	4.7	31	13.9	19.9	13.2	15.0	–	–	–	–	–	–	–	–	–	–	–	–	59	63	34	52
IX	–	–	–	–	16.0	6.1	27.9	4	0.8	26	8.8	14.9	9.5	10.7	–	–	–	–	–	–	–	–	–	–	–	–	65	59	33	52
X	–	–	–	–	11.9	3.4	21.5	4	-1.4	22	4.9	11.3	5.5	6.8	–	–	–	–	–	–	–	–	–	–	–	–	51	50	48	50
XI	–	–	–	–	4.0	0.4	15.5	8	-5.8	24	1.5	3.4	2.0	2.2	–	–	–	–	–	–	–	–	–	–	–	–	80	86	90	85
XII	–	–	–	–	-3.7	-9.0	3.5	9	-19.3	22	-6.7	-4.5	-6.4	-6.0	–	–	–	–	–	–	–	–	–	–	–	–	72	72	76	73
Rok	–	–	–	–	9.5	1.7	30.1	26.VII	-19.7	2.II	4.2	8.5	4.4	5.4	–	–	–	–	–	–	–	–	–	–	–	–	68	68	61	66

Polanica-Zdrój $\varphi = 50°24'$ $\lambda = 16°30'$

I	–	–	–	–	2.4	-3.5	10.2	22	-14.1	31	-1.0	1.2	-0.8	-0.4	5.1	5.2	5.0	5.1	86	76	85	82	0.9	1.7	1.0	1.2	77	76	71	75
II	–	–	–	–	0.4	-5.2	6.4	12	-15.6	2	-3.6	-1.0	-2.2	-2.2	4.3	4.8	4.8	4.6	89	82	89	87	0.5	1.0	0.6	0.7	87	89	86	87
III	–	–	–	–	2.3	-5.0	13.6	31	-12.6	15	-3.6	1.1	-1.4	-1.3	4.4	4.8	4.7	4.6	88	69	82	80	0.6	2.0	1.0	1.2	81	76	64	74
IV	–	–	–	–	14.2	4.1	25.8	23	-0.5	11	6.9	12.7	7.9	8.9	8.0	8.1	8.1	8.1	80	59	76	72	2.4	8.3	3.2	4.6	67	69	56	64
V	–	–	–	–	14.7	5.2	22.0	8	-1.5	1	8.2	13.0	8.9	9.8	9.6	9.4	10.2	9.7	87	63	88	79	1.5	6.1	1.4	3.0	76	78	71	75
VI	–	–	–	–	19.1	8.0	28.6	16	1.1	3	12.0	17.3	12.5	13.6	11.4	11.1	11.9	11.5	79	55	79	71	3.0	10.0	3.2	5.4	55	64	50	56
VII	–	–	–	–	20.3	9.7	30.8	26	4.2	9	13.0	19.0	13.7	14.8	12.9	12.4	12.8	12.7	85	57	81	74	2.4	10.4	3.2	5.3	64	67	61	64
VIII	–	–	–	–	22.6	10.5	30.7	13	4.0	31	14.2	21.1	14.3	16.0	13.7	13.6	14.1	13.8	84	54	85	74	2.8	11.8	2.3	5.6	60	65	33	53
IX	–	–	–	–	17.7	6.4	29.8	4	0.1	15	8.6	16.4	10.8	11.6	10.5	11.4	10.7	10.9	93	64	84	80	1.1	8.2	2.9	4.1	66	62	41	56
X	–	–	–	–	12.8	3.2	23.3	3	-3.5	22	4.4	11.9	6.1	7.1	8.4	10.2	9.1	9.2	97	74	95	89	0.3	4.5	0.5	1.8	71	60	53	61
XI	–	–	–	–	5.2	1.2	16.1	8	-4.3	24	2.3	4.5	3.1	3.2	6.8	7.4	7.2	7.1	92	85	92	90	0.8	1.5	0.8	1.0	87	87	87	87
XII	–	–	–	–	-2.7	-8.2	5.0	13	-17.5	22,23,28	-6.4	-3.9	-5.7	-5.4	3.7	4.1	3.8	3.9	90	85	90	88	0.4	0.8	0.4	0.5	91	75	78	81
Rok	–	–	–	–	10.8	2.2	30.8	26.VII	-17.5	22,23,28.XII	4.6	9.4	5.6	6.3	8.2	8.5	8.5	8.4	88	69	86	81	1.4	5.5	1.7	2.9	74	72	63	70

Wolbrom $\varphi = 50°23'$ $\lambda = 19°45'$

I	–	–	–	–	1.4	-5.2	8.4	22	-20.2	31	-2.7	0.6	-1.6	-1.3	–	–	–	–	–	–	–	–	–	–	–	–	81	68	69	73
II	–	–	–	–	-0.7	-7.1	5.0	13	-18.9	3	-4.7	-2.2	-3.6	-3.5	–	–	–	–	–	–	–	–	–	–	–	–	100	89	86	92
III	–	–	–	–	1.1	-7.1	13.0	31	-17.4	26	-4.8	-0.3	-3.3	-2.9	–	–	–	–	–	–	–	–	–	–	–	–	82	79	78	80
IV	–	–	–	–	14.4	3.9	24.9	24	-0.9	2	7.4	13.0	8.0	9.1	–	–	–	–	–	–	–	–	–	–	–	–	69	68	59	65
V	–	–	–	–	14.2	5.6	21.8	8	-2.6	1	8.9	12.6	9.3	10.0	–	–	–	–	–	–	–	–	–	–	–	–	78	85	69	77
VI	–	–	–	–	18.4	8.0	28.8	23	1.6	2	12.6	16.9	11.9	13.3	–	–	–	–	–	–	–	–	–	–	–	–	64	74	51	63
VII	–	–	–	–	20.3	9.2	29.1	26	2.5	5, 6	14.2	18.9	13.7	15.1	–	–	–	–	–	–	–	–	–	–	–	–	58	70	55	61
VIII	–	–	–	–	22.1	10.4	30.1	7	3.6	31	14.9	20.7	14.7	16.7	–	–	–	–	–	–	–	–	–	–	–	–	67	65	48	60
IX	–	–	–	–	17.1	6.0	26.3	4	0.8	15	9.5	16.0	9.8	11.3	–	–	–	–	–	–	–	–	–	–	–	–	74	61	39	58
X	–	–	–	–	13.0	2.7	18.8	1	-4.0	22	4.5	11.9	6.0	7.1	–	–	–	–	–	–	–	–	–	–	–	–	70	53	52	58
XI	–	–	–	–	5.6	2.6	14.7	8	-2.6	23, 24	2.6	4.7	3.5	3.6	–	–	–	–	–	–	–	–	–	–	–	–	86	88	87	87
XII	–	–	–	–	-2.8	-8.4	3.8	12	-20.9	26	-6.2	-3.8	-5.5	-5.2	–	–	–	–	–	–	–	–	–	–	–	–	84	88	82	85
Rok	–	–	–	–	10.3	1.7	30.1	7.VIII	-20.9	26.XII	4.7	9.1	5.2	6.0	–	–	–	–	–	–	–	–	–	–	–	–	76	74	65	72

Ząbkowice $\varphi = 50°22'$ $\lambda = 19°17'$

I	–	–	–	–	2.1	-4.1	8.5	22	-20.3	31	-2.1	1.2	-1.1	-0.8	5.0	5.2	5.0	5.1	91	76	85	84	0.5	1.7	0.9	1.0	74	73	59	69
II	–	–	–	–	0.2	-5.7	6.7	12	-15.3	3	-3.9	-1.4	-2.7	-2.7	4.1	4.5	4.6	4.4	88	80	88	85	0.6	1.1	0.6	0.8	90	86	81	86
III	–	–	–	–	2.4	-5.4	14.7	31	-12.0	20	-3.7	1.0	-2.1	-1.7	4.3	4.7	4.7	4.6	88	69	84	80	0.5	2.2	0.9	1.2	68	76	58	67
IV	–	–	–	–	15.3	4.9	26.6	24	-1.6	2	7.9	13.7	8.8	9.8	8.9	8.6	9.1	8.9	82	60	80	74	2.4	9.0	2.9	4.8	62	67	54	61
V	–	–	–	–	15.0	6.1	22.2	19	-1.8	1	8.7	12.9	9.9	10.4	10.3	10.4	10.8	10.5	91	70	87	83	1.2	5.1	1.8	2.7	77	85	69	77
VI	–	–	–	–	18.8	8.7	28.8	16, 23	0.6	2	12.5	17.1	12.7	13.8	12.1	11.2	12.4	11.9	81	58	82	74	3.1	9.9	3.1	5.4	56	67	60	61
VII	–	–	–	–	20.6	10.2	29.9	26	5.0	30	13.7	19.0	14.2	15.3	13.6	12.9	13.9	13.5	86	59	85	77	2.4	9.8	2.6	4.9	58	67	49	58
VIII	–	–	–	–	22.7	11.9	31.8	7	4.3	31	14.8	20.8	15.5	16.6	14.9	14.9	15.2	15.0	87	62	86	78	2.3	10.5	2.7	5.2	64	60	42	55
IX	–	–	–	–	17.7	7.1	29.0	4	1.7	20, 21	9.7	15.8	11.0	11.9	11.1	12.0	11.7	11.6	91	69	88	83	1.4	6.7	1.9	3.3	64	62	42	56
X	–	–	–	–	13.4	3.9	22.6	4	-3.3	22	5.2	12.4	6.8	7.8	8.8	10.8	9.6	9.7	97	75	95	89	0.2	4.1	0.6	1.6	61	41	41	48
XI	–	–	–	–	6.5	1.9	18.5	7	-3.0	17, 24	2.7	5.6	3.5	3.8	7.2	7.8	7.6	7.5	95	85	95	92	0.4	1.9	0.5	0.9	85	83	80	83
XII	–	–	–	–	-2.3	-8.0	6.0	13	-18.0	29	-5.9	-3.6	-5.2	-5.0	3.8	4.3	4.0	4.0	91	86	90	89	0.4	0.7	0.4	0.5	72	78	73	74
Rok	–	–	–	–	11.0	2.6	31.8	7.VIII	-20.3	31.I	5.0	9.5	5.9	6.6	8.7	8.9	9.0	8.9	89	71	87	82	1.3	5.2	1.6	2.7	69	70	59	66

Duszniki - Zdrój $H_S = 540\ m$ $h_W = 16\ m$ 1962

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	3.5	3.7	5.5	6.0	1.5	3.7	1.5	1.7	3.5	3.0	32.5	4.6	24	5.8	2	2.5	19	3.8	35	5.1	25	4	9	25	·	4	·	1	18	18	12	·	1	22	·
II	26	2.0	6.5	2.1	6	3.2	6.5	4.4	2.5	4.8	8	4.9	9.5	3.3	4	3.6	15	2.5	105	32.0	16	5	15	27	·	2	1	·	20	19	15	2	9	28	·
III	20	2.1	2	13.0	16	2.2	2	5.5	10	2.4	3	1.7	6.5	2.0	4.5	4.0	29	1.9	69	16.6	5	5	12	27	·	1	·	2	17	17	9	4	5	31	·
IV	13.5	2.1	4	3.1	24.5	2.6	9.5	2.3	6.5	7.7	1.5	2.0	9.5	2.5	3	2.3	18	2.3	50	12.6	26	·	·	2	·	2	·	7	10	12	10	1	2	·	1
V	12	1.8	1	2.0	12	2.2	4.5	2.0	6.5	2.0	20	1.8	23.5	1.8	5.5	1.8	8	1.7	147	24.8	15	·	·	3	·	·	·	1	14	24	19	3	·	·	1
VI	27	1.8	10.5	2.2	13.5	1.6	1	1.0	2	1.5	12	1.8	16	1.5	4	1.5	4	1.7	39	10.6	11	·	·	1	5	·	·	8	10	9	7	1	·	·	4
VII	12	1.2	·	·	4	1.0	6	1.7	9.5	1.1	13.5	1.1	32	1.6	14	1.6	2	1.4	53	10.3	13	·		·	3		·	4	10	16	14	1	·	·	3
VIII	3	2.7	·	·	·		12	1.4	13.5	1.1	37.5	1.7	5	1.0	5	1.0	17	1.2	69	31.2	5	·	·		5		·	5	8	14	11	1	1	·	5
IX	1	3.0		·	·	·	12	1.5		·	21	1.8	2	1.0	1	3.0	53	0.7	87	21.4	17		·	·	2	·	·	6	9	15	13	3	·	·	·
X	7	1.2	·	·	·		5	1.8	·	·	14.5	1.6	1.5	1.0		·	65	0.5	40	22.8	31	·	·	6	·	·		13	13	8	5	1	11	·	1
XI	16	2.0	1	2.0		·	14	3.6	3	2.0	20	3.3					36	1.7	62	17.2	1	·	6	19	·	1		1	22	11	10	1	17	11	·
XII	24	2.2	·	·	1	2.0	·	·	7	3.6	40	3.2	1	2.0	2	2.0	18	2.3	64	14.2	15	12	21	31	·	1	1	3	17	18	12	2	16	31	·
Rok	165	2.2	30.5	2.5	78.5	1.5	74	2.2	64	2.4	223.5	2.5	130.5	2.0	45	1.9	284	1.8	820	32.0	16.II	26	63	141	15	11	2	51	168	181	137	20	62	123	15

Polanica - Zdrój $H_S = 400\ m$ $h_W = 11{,}3\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	4	4.0	2.5	2.8	4	2.0	2	3.5	9.5	4.2	20	5.0	16.5	4.0	9.5	3.4	25	3.0	49	21.6	12	4	8	21	·	1	·	1	14	15	10	1	1	16	·
II	11	2.8	3	2.3	·	·	·	·	3	6.7	7	6.1	17.5	4.2	16.5	3.2	26	2.7	80	24.6	12	4	10	26	·	2	·	·	21	19	15	2	7	28	·
III	8.5	4.4	5.5	2.2	4	2.2	2.5	5.6	2.5	3.6	5	5.4	7.5	3.1	12.5	3.3	45	1.9	62	16.5	12	5	9	26	·	·		2	16	15	8	3	6	25	·
IV	3	2.3	7	2.7	3	2.3	5	3.6	6.5	8.3	11	3.7	11.5	2.9	11	2.6	32	2.3	35	12.5	26	·	·	2	2	2	·	4	14	12	7	1	·	·	1
V	4.5	1.8	·	·	1	3.0	1	2.0	1	4.0	9.5	3.3	25.5	3.1	10.5	2.1	40	1.6	115	25.8	13	·	·	3	·		·	·	14	20	18	4	2	·	2
VI	9.5	2.7	2	1.0	3	2.7	1	1.0	2	2.5	3.5	3.7	12.5	2.9	17.5	2.8	39	1.6	35	9.6	11	·			6			4	7	8	5		1	·	4
VII	4	2.2	1	2.0	·	·	1.5	2.0	3	3.0	5.5	4.1	27.5	2.9	8.5	2.2	42	1.5	26	4.9	13	·	·	·	5	·	·	2	10	12	6	·	2	·	4
VIII	2.5	2.4	·	·	·	·	1	1.0	3.5	4.3	5.5	4.4	29	3.0	5.5	2.2	46	1.6	38	9.3	24	·		·	8	·	·	3	3	10	10	·	6	·	4
IX	2	1.5	1	2.0	·	·	1	1.0	7	3.7	7	4.7	21.5	2.6	7.5	2.0	43	1.5	51	15.7	17		·	·	4	·	·	5	9	12	8	2	9	·	·
X	6.5	2.3	2	2.5	·	·	3	2.3	1	1.0	2	3.0	8	2.2	5.5	2.2	65	0.7	39	22.0	31		·	7	·	·	·	8	14	6	4	1	19	·	·
XI	4	2.5	6	2.7	3	4.0	11	3.5	10	4.5	7	2.9	9	3.4	1	2.0	39	1.9	55	17.9	1	·	2	15	·	·	·	·	22	13	11	1	9	11	·
XII	14.5	2.0	3.5	3.3	1	2.0	1	4.0	5	4.8	7.5	3.7	14	3.6	4.5	2.6	42	1.7	35	6.2	9	12	20	28	·	1	·	1	20	15	12	·	8	31	·
Rok	74	2.6	33.5	2.0	19	1.5	30	2.5	54	4.2	90.5	4.2	200	3.2	110	2.6	484	1.8	620	25.8	13.V	25	49	128	25	6	·	30	164	157	114	15	70	111	15

Wolbrom $H_S = 373\ m$ $h_W = 13.5\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	5.5	6.3	2	2.5	1	2.0	·	·	8	2.7	27.5	3.4	26	5.3	5	5.0	18	3.5	51	9.5	28	4	8	26	·	4		1	13	14	13	·	–	18	·
II	5	4.2	3	2.7	10	3.6	·	·	3	5.0	12.5	8.1	18	7.6	9.5	9.5	23	4.9	62	16.1	17	6	14	27	·	8	3	·	24	21	15	1	–	28	·
III	8	5.6	9	4.2	11.5	3.9	3.5	2.3	4	3.5	9.5	5.4	9.5	4.6	5	4.4	33	2.9	64	14.6	12	10	16	27	·	5	·	2	19	16	13	2	–	23	·
IV	6	2.8	2.5	3.2	4	3.8	11	4.3	5	4.6	10	4.8	9.5	4.1	11	5.0	31	2.8	83	25.0	6	·	·	2	·	2	·	4	10	16	12	2	–	·	1
V	1	2.0	·	·	4	3.5	2.5	3.0	6.5	4.7	6	4.7	20	5.7	3	3.3	50	2.2	162	17.6	9	·	·	3	·	3	·	·	16	25	21	6	–	·	4
VI	9.5	3.3	·	·	4	2.5	1	3.0	1	4.0	6	2.2	22	3.8	10.5	3.7	36	2.1	87	25.8	1, 4	·	·	·	5	3	·	2	10	13	7	3	–	·	2
VII	3	1.0	2	1.0	2	2.0	1	3.0	2.5	2.6	5.5	2.8	26	2.9	12	1.8	39	1.4	139	74.3	22	·	·	·	4	·	·	5	10	15	13	3	–	·	7
VIII	1	1.0	1	3.0	2	3.5	7.5	3.9	4	1.8	4.5	3.5	33	3.5	4	5.0	36	2.1	59	14.8	5		·	·	6	·	·	2	7	17	10	1	–	·	6
IX	1	3.0	1	1.0	9.5	2.3	2.5	4.4	5	2.2	11	5.0	15	3.5	9	3.2	36	2.0	55	15.6	18	·	·	·	2	2	·	6	9	12	10	2	–	·	·
X	4	2.8	4	2.2	16	2.4	5	1.8	1.5	4.0	4	3.9	9.5	3.4	3	2.0	46	1.4	13	3.4	28	·	·	10	·	·	·	5	10	6	5	·	–	·	·
XI	5	2.2	1	2.0	16	2.9	10	2.9	3	6.0	4	2.5	12	2.5	1	3.0	38	1.7	61	9.7	15	·	2	12	·	·	·	2	23	18	12	·	–	6	·
XII	3	4.7	6.5	2.3	13.5	2.4	4	3.5	1	6.0	1.5	4.3	30.5	3.6	1	6.0	32	2.2	38	8.4	13	11	21	31	·	1	·	1	21	18	8	·	–	18	·
Rok	52	3.2	32	2.0	93.5	2.9	48	2.7	44.5	3.9	102	4.2	231	4.2	74	4.3	418	2.4	874	74.3	22.VII	31	61	138	17	28	3	30	172	191	139	20	–	93	20

Ząbkowice $H_S = 314\ m$ $h_W = 14\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	3.5	5.4	3	2.8	·	·	1	3.0	3	2.5	21	2.3	31	2.3	16.5	2.9	14	2.2	44	6.8	11	3	5	25	·	·	·	·	12	17	13	·	5	16	·
II	6.5	4.2	7	2.2	9	3.4	3	1.8	1	2.5	12.5	5.0	17.5	4.0	15.5	4.9	12	3.5	43	5.1	5	4	13	25	·	3	1	·	20	18	13	·	7	23	·
III	21	3.0	4.5	3.1	16	2.4	4	2.0	2.5	1.6	6	2.0	9	3.5	10	3.8	20	2.2	62	12.3	12	7	12	26	·	·	·	3	15	17	12	2	3	20	·
IV	10.5	2.3	3.5	2.7	6.5	3.1	12	2.2	4.5	2.1	5.5	3.0	8.5	3.5	14	3.1	25	2.0	54	10.4	6	·	·	5	6	·	·	5	9	15	8	1	3	·	·
V	10	1.6	3	1.2	5.5	1.5	4	2.2	2.5	2.5	7.5	3.1	23.5	2.7	15	2.6	22	1.8	139	17.8	31	·	·	3	·	·	·	·	14	23	21	5	3	·	2
VI	12	2.2	5	1.2	4.5	2.0	0.5	2.0	0.5	2.0	3	3.8	15	3.8	23.5	2.9	26	2.0	71	37.4	1	·	·	·	6	·	·	2	12	13	6	2	·	·	2
VII	10	2.0	5.5	1.7	4	1.5	2	2.0	2.5	2.8	7.5	2.8	17.5	2.3	21	2.1	23	1.6	87	28.7	22	·	·	·	4	·	·	4	7	14	13	2	·	·	3
VIII	3	2.3	4.5	1.7	6.5	2.7	5	2.6	0.5	2.0	3.5	2.4	24.5	3.4	13.5	2.0	32	1.8	71	17.0	15		·	·	7	1		2	7	15	10	4	3	·	2
IX	8	1.8	3	1.3	14	2.8	2.5	2.0	4	2.4	10.5	3.1	15.5	2.4	14.5	2.1	18	1.9	49	16.0	18		·	·	3	·	·	7	10	10	7	2	3	·	2
X	7.5	1.5	6.5	2.8	11.5	2.1	5.5	2.0	·	·	1	4.0	17	2.2	11	1.7	33	1.3	18	6.4	28	·	·	6	·	·	·	10	9	7	4	·	15	·	·
XI	8	1.2	7	1.7	22	1.9	4.5	2.3	·	·	3.5	1.9	6.5	1.3	7.5	1.5	31	1.1	76	15.2	15		2	10	·	·	·	2	21	18	12	2	11	4	·
XII	8	1.9	12	3.4	7	1.3	1	1.0	1.5	2.3	10.5	3.4	9.5	1.5	8.5	1.9	35	1.5	44	10.2	13	11	17	29	·	·	·	2	16	18	10	1	3	18	
Rok	108	2.4	64.5	2.2	106.5	2.1	45	2.1	22.5	1.9	92	3.1	195	2.7	170.5	2.6	291	1.9	758	37.4	1.VI	25	49	129	26	4	1	37	152	185	129	21	56	81	11

Miechów $\varphi = 50°22'$ $\lambda = 20°02'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.1	−38	9.2	22	−18.6	31	−1.8	1.0	−1.0	−0.7	–	–	–	–	–	–	–	–	–	–	–	–	74	67	66	69
II	–	–	–	–	0.0	−5.3	5.9	13	−12.3	1, 2	−4.0	−1.6	−2.8	−2.8	–	–	–	–	–	–	–	–	–	–	–	–	94	84	76	85
III	–	–	–	–	1.5	−5.5	13.3	31	−15.5	26	−4.2	0.3	−2.4	−2.2	–	–	–	–	–	–	–	–	–	–	–	–	80	72	62	71
IV	–	–	–	–	15.2	4.7	25.9	23	0.4	2	7.0	13.3	9.2	9.7	–	–	–	–	–	–	–	–	–	–	–	–	64	67	43	58
V	–	–	–	–	14.7	6.2	22.5	8	−1.9	1	8.7	13.1	9.9	10.4	–	–	–	–	–	–	–	–	–	–	–	–	79	81	65	75
VI	–	–	–	–	18.5	8.3	28.4	16	1.4	2	12.4	16.6	12.7	13.6	–	–	–	–	–	–	–	–	–	–	–	–	62	71	56	63
VII	–	–	–	–	20.6	9.8	29.0	26	3.5	5	13.6	19.3	13.8	15.1	–	–	–	–	–	–	–	–	–	–	–	–	61	67	54	61
VIII	–	–	–	–	22.6	10.8	30.9	7	3.5	31	14.3	21.1	15.3	16.5	–	–	–	–	–	–	–	–	–	–	–	–	58	60	43	54
IX	–	–	–	–	17.5	5.9	26.9	4	0.2	20	8.7	15.9	10.4	11.4	–	–	–	–	–	–	–	–	–	–	–	–	67	65	40	57
X	–	–	–	–	12.6	2.6	18.6	1	−4.9	16	3.7	11.4	6.1	6.8	–	–	–	–	–	–	–	–	–	–	–	–	78	53	43	58
XI	–	–	–	–	6.2	1.8	16.8	8	−2.6	24	2.4	5.2	3.5	3.6	–	–	–	–	–	–	–	–	–	–	–	–	83	82	81	82
XII	–	–	–	–	−2.2	−7.8	4.6	12	−20.6	29	−6.1	−3.2	−5.4	−5.0	–	–	–	–	–	–	–	–	–	–	–	–	74	81	72	76
Rok	–	–	–	–	10.8	2.3	30.9	7.VIII	−20.6	29.XII	4.6	9.4	5.8	6.4	–	–	–	–	–	–	–	–	–	–	–	–	73	71	58	67

Tarnogród $\varphi = 50°22'$ $\lambda = 22°45'$

I	–	–	–	–	2.1	−2.6	8.1	22	−15.6	31	−1.2	1.0	−1.0	−0.6	–	–	–	–	–	–	–	–	–	–	–	–	76	60	60	65
II	–	–	–	–	−0.4	−5.4	3.1	13	−13.8	25	−4.0	−1.4	−3.2	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	84	87	86	86
III	–	–	–	–	1.6	−5.9	12.4	5	−17.6	21	−3.3	0.6	−2.8	−2.1	–	–	–	–	–	–	–	–	–	–	–	–	73	68	71	71
IV	–	–	–	–	16.4	5.5	26.3	22	−0.4	30	9.0	15.3	9.5	10.8	–	–	–	–	–	–	–	–	–	–	–	–	45	48	27	40
V	–	–	–	–	16.3	7.6	23.4	14	−0.4	1, 2	10.8	14.8	10.5	11.6	–	–	–	–	–	–	–	–	–	–	–	–	70	73	58	67
VI	–	–	–	–	18.8	9.8	28.3	16, 23	3.8	6, 7	13.4	17.4	13.3	14.4	–	–	–	–	–	–	–	–	–	–	–	–	54	66	53	58
VII	–	–	–	–	20.7	11.1	29.8	27	7.1	30	14.8	19.8	14.8	16.0	–	–	–	–	–	–	–	–	–	–	–	–	52	58	47	52
VIII	–	–	–	–	22.9	12.7	30.3	7, 13	7.1	31	15.6	21.8	16.3	17.5	–	–	–	–	–	–	–	–	–	–	–	–	46	55	32	44
IX	–	–	–	–	17.8	8.0	26.9	5	2.6	15, 25	10.2	17.0	11.6	12.6	–	–	–	–	–	–	–	–	–	–	–	–	41	45	47	44
X	–	–	–	–	13.1	2.4	20.0	2	−4.8	16	4.6	12.6	5.8	7.2	–	–	–	–	–	–	–	–	–	–	–	–	50	34	26	37
XI	–	–	–	–	7.4	2.4	18.6	1	−2.4	26	3.6	6.6	4.1	4.6	–	–	–	–	–	–	–	–	–	–	–	–	88	77	77	81
XII	–	–	–	–	−2.0	−7.4	4.7	14	−19.7	22	−5.4	−3.3	−5.4	−4.9	–	–	–	–	–	–	–	–	–	–	–	–	84	76	77	79
Rok	–	–	–	–	11.2	3.2	30.3	7.13.VIII	−19.7	22.XII	5.7	10.2	6.1	7.0	–	–	–	–	–	–	–	–	–	–	–	–	64	62	55	60

Lądek-Zdrój $\varphi = 50°21'$ $\lambda = 16°53'$

I	–	–	–	–	2.1	−3.6	10.5	22	−15.3	31	−1.6	0.5	−0.9	−0.7	5.0	5.0	4.9	5.0	87	77	82	82	0.8	1.6	1.1	1.2	80	79	77	79
II	–	–	–	–	−0.1	−6.5	5.5	12	−15.8	26	−3.9	−1.6	−2.9	−2.8	4.1	4.5	4.5	4.4	86	81	87	85	0.7	1.0	0.7	0.8	9.9	9.4	8.2	9.2
III	–	–	–	–	2.1	−5.8	11.6	31	−14.6	14	−4.1	0.6	−2.2	−2.0	4.3	4.5	4.5	4.4	89	68	83	80	0.6	2.2	0.9	1.2	8.9	8.2	7.5	8.2
IV	–	–	–	–	13.4	4.1	26.1	24	−0.2	3.0	6.7	12.0	7.4	8.4	7.7	7.4	7.9	7.7	79	58	77	71	2.6	8.3	3.0	4.6	8.3	7.8	6.2	7.4
V	–	–	–	–	14.0	5.2	21.2	8	−1.1	1, 5	7.9	12.2	8.7	9.4	9.0	8.8	9.7	9.2	84	63	85	77	1.9	5.9	1.8	3.2	8.1	8.8	8.1	8.3
VI	–	–	–	–	18.5	7.6	27.9	23	1.6	8	11.4	16.5	12.1	13.0	11.4	11.2	11.3	11.3	82	56	80	73	2.7	9.4	3.0	5.0	6.8	8.0	6.9	7.2
VII	–	–	–	–	19.6	9.5	29.4	26	4.1	9	12.6	18.1	13.3	14.3	12.6	12.7	12.6	12.6	85	61	82	76	1.2	8.8	3.1	4.4	7.2	8.4	7.0	7.5
VIII	–	–	–	–	18.8	10.4	29.9	13	4.1	31	14.0	20.4	13.8	15.5	13.9	13.7	13.6	13.7	86	57	85	76	2.3	10.9	2.5	5.2	6.9	7.3	3.7	6.0
IX	–	–	–	–	17.0	6.7	27.2	4	0.8	20	8.9	15.0	10.8	11.4	10.1	10.9	10.2	10.4	88	66	81	78	1.8	7.0	3.4	4.1	6.7	6.7	4.9	6.1
X	–	–	–	–	13.0	3.4	22.3	4	−2.9	22	4.7	11.9	6.2	7.2	8.4	9.6	9.0	9.0	95	70	93	86	0.5	5.0	0.7	2.1	6.0	5.0	5.5	5.5
XI	–	–	–	–	4.8	1.0	14.9	8	−5.9	24	2.2	4.0	2.8	3.0	6.5	7.0	6.9	6.8	89	84	90	88	1.0	1.5	0.9	1.1	9.2	9.1	8.9	9.1
XII	–	–	–	–	−3.2	−8.8	3.6	16	−19.3	28	−6.7	−4.6	−6.1	−5.9	3.5	3.8	3.7	3.7	88	83	89	87	0.5	0.8	0.5	0.6	8.5	8.4	7.6	8.2
Rok	–	–	–	–	10.0	1.9	29.9	13.VIII	−19.3	28.XII	4.3	8.8	5.2	5.9	8.0	8.3	8.2	8.2	86	69	84	80	1.4	5.2	1.8	2.8	7.9	7.9	6.8	7.5

Bytom $\varphi = 50°21'$ $\lambda = 18°55'$

I	–	–	–	–	2.4	−2.6	8.4	22	−18.9	31	−0.8	1.5	−0.3	0.0	5.3	5.4	5.1	5.3	88	77	83	83	0.7	1.6	1.1	1.1	7.8	7.5	6.2	7.2
II	–	–	–	–	0.6	−4.7	6.8	13	−15.4	3	−3.4	−0.9	−1.8	−2.0	4.4	4.7	4.9	4.7	89	81	89	86	0.5	1.1	0.6	0.7	8.6	8.7	8.0	8.4
III	–	–	–	–	3.0	−3.6	15.1	31	−7.9	14, 17	−2.6	1.6	−0.7	−0.6	4.8	5.1	5.1	5.0	91	72	84	82	0.5	2.1	1.0	1.2	7.6	7.3	6.3	7.1
IV	–	–	–	–	15.6	5.7	27.5	24	1.0	6	8.1	14.1	9.9	10.5	8.9	8.3	9.1	8.8	81	56	75	71	2.4	9.6	3.8	5.3	6.1	6.5	5.6	6.1
V	–	–	–	–	15.5	6.8	22.7	28	−1.1	1	9.2	13.2	10.6	10.9	10.4	10.2	10.9	10.5	88	68	84	80	1.5	5.5	2.3	3.1	7.5	7.7	2.1	7.4
VI	–	–	–	–	19.8	9.6	30.6	23	0.6	2	12.9	17.7	13.5	14.4	12.1	11.3	12.4	11.9	79	56	79	71	3.6	10.6	3.9	6.0	5.3	6.7	5.6	5.9
VII	–	–	–	–	21.5	11.1	30.6	26	7.0	30	14.2	19.3	14.8	15.8	13.7	13.0	14.0	13.6	84	59	83	75	2.8	10.0	3.2	5.3	5.5	6.7	5.3	5.8
VIII	–	–	–	–	23.9	12.7	31.6	7	7.3	31	15.3	21.6	16.1	17.3	14.9	14.4	15.3	14.9	85	57	83	75	2.7	12.3	3.3	6.1	6.3	6.1	4.0	5.5
IX	–	–	–	–	18.3	7.8	29.2	4	4.4	20	10.1	16.5	11.5	12.4	11.4	11.8	11.8	11.7	92	64	87	81	1.3	7.7	2.1	3.7	6.8	5.6	3.2	5.2
X	–	–	–	–	14.2	4.6	23.7	4	−4.4	22	6.2	12.5	7.8	8.6	9.3	10.1	9.9	9.8	96	70	91	86	0.4	5.0	0.9	2.1	7.8	5.8	4.3	6.0
XI	–	–	–	–	6.9	2.1	18.7	7	−1.7	24, 28	3.4	5.8	4.2	4.4	7.4	7.8	7.8	7.7	94	83	93	90	0.5	2.0	0.7	1.1	8.8	8.2	8.3	8.4
XII	–	–	–	–	−1.6	−6.4	8.8	13	−17.8	22	−5.0	−3.1	−4.2	−4.1	3.9	4.2	4.2	4.1	88	83	88	86	0.6	0.9	0.6	0.7	8.3	7.9	7.7	8.0
Rok	–	–	–	–	11.7	3.6	31.6	7.VIII	−19.9	31, 1	5.6	10.0	6.8	7.3	8.9	8.9	9.2	9.0	88	69	85	81	1.5	5.7	2.0	3.1	7.2	7.1	6.0	6.8

Miechów $H_s = 292\ m$ $h_w = 16.5\ m$ 1962

MIESIĄC	ROZKŁAD WIATRU (D, VmD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v > 15	◔	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	[illegible]
I	4	7.5	4	6.1	0.5	5.0	3.5	2.0	10.5	2.6	15.5	3.8	29	4.7	14	5.2	12	3.9	23	3.8	25	2	6	23	·	2	·	2	12	11	8	·	1	18	·
II	8	5.4	2.5	5.2	11.5	3.9	4.5	3.0	3	2.8	9.5	5.6	22	6.3	14	8.1	9	5.1	25	3.9	12	5	13	24	·	7	3	·	19	17	10	·	2	25	1
III	10.5	6.2	6.5	5.3	12	3.3	14.5	2.7	5	2.2	2	5.5	10	5.0	14.5	4.4	18	3.4	37	9.9	12	5	12	26	·	2	·	3	15	18	11		3	24	·
IV	9.5	5.2	4	4.5	6.5	3.2	11	3.8	8.5	3.1	6	4.4	10	4.2	20.5	5.1	14	3.7	84	33.0	13	·	·	·	3	1		5	6	14	10	2	1	·	1
V	4	3.9	3	3.8	2.5	2.8	6	3.1	4.5	3.2	8.5	3.6	24	4.8	16.5	3.9	24	3.0	148	29.3	14	·	·	3	·	2	1	·	11	26	21	4			4
VI	10.5	5.0	3	4.2	3	2.0	3	3.0	1	2.0	5.5	3.6	15.5	3.9	24.5	4.3	24	3.0	90	34.0	4	·	·	·	5	1	·	2	13	13	8	4	·	·	1
VII	9	3.3	4.5	3.4	2.5	1.8	4	2.8	2	2.5	10.5	3.2	15.5	3.5	22	4.0	23	2.6	145	72.2	22		·		4	2	·	4	10	16	13	3			9
VIII	2.5	2.2	·		2	2.2	6	3.0	4	2.2	6	3.3	18.5	4.3	22	4.1	32	2.4	42	12.5	5		·	·	9	2	·	1	5	13	9	1	3	·	4
IX	3.5	2.9	1.5	2.0	6.5	3.2	2	3.8	3.5	2.7	11.5	4.1	13.5	4.3	14	4.5	34	2.4	47	21.2	18	·	·	·	2	·	·	6	9	12	7	2	5	·	1
X	3.5	2.3	4.5	3.8	10.5	2.7	11	2.6	2	2.2	2	4.0	10.5	4.0	14	3.1	35	1.9	9	4.0	28	·	·	11	·	·	·	5	9	10	3	·	16	·	·
XI	5	3.5	4.5	3.8	23.5	3.6	15	3.2	2.5	2.8	3	3.3	15	3.0	10.5	4.0	11	3.0	64	12.9	15	·	1	7	·	·	·	1	21	20	11	1	9	7	·
XII	10	4.0	11.5	3.3	9.5	3.1	6.5	2.7	4.5	2.7	7	4.7	12.5	4.2	14.5	2.9	17	2.8	33	11.4	13	11	15	29	·	·	·	2	15	18	8	1	2	18	·
Rok	80	4.3	49.5	3.8	90.5	3.1	87	3.0	51	2.6	87	4.1	196	4.4	201	4.5	253	3.1	747	72.2	22.VII	23	47	123	23	19	4	31	145	188	119	18	42	92	21

Tarnogród $H_s = 217\ m$ $h_w = 15.9\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	[illegible]
I	3	2.7	3	2.7	2	3.0	·		15	3.0	27	2.5	25	2.1	3	2.0	15	2.1	31	10.5	25	2	6	20	·	·	·	–	–	13	8	1	3	8	·
II	5	2.8	1	2.0	3	2.0	2	2.5	6	3.8	9	3.9	23	4.2	9	5.6	26	2.7	40	7.5	12	3	15	27	·	4	·	–	–	18	9	·	2	28	·
III	11	4.3	4	5.5	5	1.2	2	3.0	9	2.1	9	2.0	11	4.3	3	4.0	39	1.9	49	9.2	16	3	12	25	·	3	·	–	–	15	12	·	9	23	·
IV	5	3.2	4	2.0	5	1.6	1	2.0	16	3.2	5	1.8	13	2.2	3	4.7	38	1.5	42	13.8	6	·	·	1	4	·	·	–	–	9	8	2	3	·	·
V	4	2.0	2	3.0	1	1.0	1	2.0	8	2.3	9	2.2	16	3.5	6	2.0	46	1.3	104	18.2	20	·	·	2	·	1	·	–	–	21	19	5	6	·	4
VI	14	3.0	5	1.8	6	1.5		·	1	2.0	4	3.2	15	2.4	5	2.6	40	1.4	82	25.5	1	·	·	·	7	·	·	–	–	13	10	2	4	·	2
VII	7	2.9	1	2.0	2	1.0	·	·	6	1.5	6	2.2	20	1.8	7	2.0	44	1.0	100	27.2	19	·	·	·	4	·	·	–	–	16	13	2	4	·	3
VIII	2	1.0	1	1.0	·	·	1	1.0	12	1.9	4	2.5	22	1.6	3	2.3	48	0.9	59	15.0	5	·	·	·	11	·	·	–	–	13	9	1	12	·	4
IX	·	·	·	·	·	·	1	1.0	6	2.5	4	3.0	22	2.3	3	3.7	54	1.0	56	27.2	5	·	·	·	2	·	·	–	–	10	6	2	6	·	1
X	3	1.3	1	2.0	6	1.3	6	2.0	5	1.8	5	2.0	13	2.1	4	3.0	50	0.9	1	0.2	1, 2, 31	·	·	9	·	·	·	–	–	5	·	·	19	·	·
XI	6	1.5	2	4.0	13	2.1	22	2.0	2	1.5	9	3.0	8	2.5	4	2.5	24	1.6	58	13.0	25	·	·	4	·	·	·	–	–	17	11	2	16	·	·
XII	9	1.8	6	1.8	1	2.0	3	1.3	15	2.1	7	3.4	16	1.9	·4	3.0	32	1.4	30	6.8	30	11	16	30	·	·	·	–	–	20	6	·	14	14	·
Rok	69	2.2	30	2.3	44	1.4	39	1.4	101	2.3	98	2.6	204	2.6	54	3.1	456	1.5	652	27.2	19.VII, 5.IX	19	49	118	28	8	·	–	–	170	111	17	98	73	14

Lądek-Zdrój $H_s = 460\ m$ $h_w = 13.5\ m$ I–XI, $h_w = 12.7\ m$ XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	[illegible]
I	2	1.8	3.5	1.4	3	1.2	1.5	4.3	20	4.5	39	3.7	8.5	2.1	1.5	3.0	14	3.0	55	12.5	28	5	6	19	·	5	1	1	18	15	11	2	·	19	·
II	9.5	1.3	7	1.6	0.5	1.0	1	1.0	11.5	3.0	27.5	2.3	10	3.4	6	1.9	11	2.0	64	10.2	24	5	13	27	·	3	3	·	21	22	14	1	3	28	·
III	9	1.6	11.5	1.3	7	1.0	3	4.2	18.5	2.5	8.5	2.3	7	1.6	8.5	2.0	20	1.5	64	20.6	12	6	9	26	·	1	·	2	22	21	10	2	2	30	·
IV	0.5	1.0	5	1.5	7.5	1.5	12	3.2	14	3.8	19.5	3.0	5	1.4	3.5	1.3	23	2.0	56	9.7	11	·	·	1	3	3	1	3	17	14	12	·	1	1	·
V	0.5	2.0	2.5	1.2	10.5	1.0	8	1.1	24.5	1.8	16	2.0	2.5	1.8	0.5	1.0	28	1.1	152	40.8	14	·	·	2	·	·	·	·	17	25	19	3	·	·	1
VI	5.5	1.7	8.5	1.3	13	1.2	4	1.0	10	1.8	14	1.9	4.5	2.3	0.5	2.0	30	1.1	53	13.9	3	·	·	·	6	·	·	·	14	12	10	1	·	·	2
VII	·	·	2	1.2	9	1.1	6.5	1.3	13.5	1.7	16	2.0	1.5	1.3	0.5	2.0	44	0.8	50	15.6	17	·	·	·	4	·		1	15	17	11	1	·	·	3
VIII	0.5	1.0	1	1.0	5	1.0	4	1.0	21	2.0	16	2.4	6.5	1.8	1	2.0	38	1.1	75	29.7	14	·	·	·	6	·	·	2	5	15	10	2	·	·	5
IX	1.5	1.0	3	1.7	9.5	1.0	11.5	1.6	22	2.1	9	3.9	2.5	4.2	1	1.0	30	1.4	92	24.7	17	·	·	·	2	1	·	3	13	13	11	3	4	·	·
X	1	1.0	5.5	1.8	11.5	1.0	8.5	1.0	11	1.4	7.5	1.3	1	1.0	·	·	47	0.6	56	26.4	31	·	·	3	·	·	·	9	11	10	7	2	9	·	·
XI	0.5	4.0	1.5	2.0	14	1.1	13	1.9	14	2.6	7	2.4	1	1.0	·	·	39	1.1	77	24.2	1	·	3	14	·	·	·	·	23	16	13	2	6	11	·
XII	1.5	2.3	6.5	1.6	16.5	1.1	6	2.2	16	3.0	12	3.4	1.5	2.7	·	·	33	1.5	35	6.7	31	14	21	30	·	·	·	2	20	18	13	·	2	31	·
Rok	32	1.6	57.5	1.5	107	1.1	79	2.0	196	2.5	192	2.6	51.5	2.0	23	1.4	357	1.4	829	40.8	14.V	30	52	122	21	13	5	23	196	197	141	19	27	120	11

Bytom $H_s = 300\ m$ $h_w = 22.0\ m$ I–VII, $h_w = 16.3\ m$ VIII–XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	[illegible]
I	7.5	3.9	2.5	3.6	·	·	·	·	6.5	3.2	50.5	2.8	9.5	3.2	12.5	2.2	4	2.7	46	7.8	11	2	5	22	·	·	·	·	11	12	11	·	1	19	·
II	9.5	2.7	4.5	1.8	12	3.1	1.5	2.3	9.5	4.1	12	4.2	13.5	4.3	14.5	4.3	7	3.4	48	9.6	5	3	11	26	·	2	2	·	18	19	12	·	2	28	1
III	13.5	3.9	9.5	2.4	10.5	2.9	4	2.0	8	2.0	9.5	3.5	8	3.7	10	3.6	20	2.5	56	14.8	12	·	9	24	·	2	·	1	11	17	11	2	5	19	1
IV	15	1.5	7.5	2.5	5	4.2	2.5	3.0	12	2.8	10	3.2	5.5	3.5	14.5	3.2	18	2.2	61	10.5	13	·	·	·	6	·	·	4	9	13	13	2	5	·	·
V	3	1.8	3.5	2.4	6	2.7	3	1.8	5	3.4	11	2.9	13	2.9	18.5	2.4	30	1.8	145	24.0	13	·	·	2	·		·	·	11	20	19	5	5	·	3
VI	14.5	3.3	3.5	2.7	0.5	3.0	1	3.0	1.5	1.7	3.5	2.7	16.5	3.6	21	3.4	28	2.3	60	35.0	1	·	·	·	7	·	·	2	8	10	7	1	·	·	2
VII	8	2.0	2	2.5	·	·	0.5	4.0	1	5.0	13	3.3	18.5	2.5	20	2.8	30	1.9	67	18.0	22	·	·	·	6	·		4	9	13	12	2	·	·	3
VIII	4.5	1.3	0.5	2.0	1	1.0	4	2.9	3.5	4.1	7.5	3.5	21	3.2	15	2.6	36	1.8	88	39.6	15	·	·	·	13	·	·	2	7	13	10	3	2	·	4
IX	1	3.0	1	1.0	11	3.5	0.5	2.0	3.5	3.4	19.5	3.6	16.5	3.6	12	3.5	25	2.5	53	14.0	18	·	·	·	4	·	·	8	8	14	10	2	9	·	1
X	5	2.6	4.5	3.8	14.5	2.7	7	1.9	1.5	2.0	8	2.6	7	2.6	14.5	2.4	31	1.7	16	8.8	28	·	·	6	·			3	10	4	2	·	13	·	·
XI	6.5	2.4	6.5	2.8	19.5	2.4	9	2.2	0.5	3.0	8.5	2.9	12	2.3	25	2.1	20	1.9	78	17.5	20		1	10	·	·	·	·	21	15	13	3	10	–	
XII	7	2.3	13	2.9	8	2.8	7	2.0	1	5.0	14	3.2	12.5	1.7	9.5	2.1	16	2.0	50	14.0	13	8	17	29	·		·	·	17	13	8	2	7	25	·
Rok	95	2.6	58.5	2.5	88	2.4	40	2.3	53.5	3.3	167	3.2	158.5	3.1	169.5	2.9	265	2.2	768	39.6	15.VIII	13	43	119	36	4	2	24	140	163	128	22	59	–	15

Chorzelów $\varphi = 50°21'$ $\lambda = 21°27'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{a.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.1	-3.0	7.4	20	-15.7	31	-1.2	1.1	-0.9	-0.5	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.4	6.4	6.6
II	–	–	–	–	0.5	-4.6	6.7	13	-13.1	25	-3.3	-1.1	-1.9	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.7	8.7	8.7
III	–	–	–	–	2.4	-4.8	14.4	5	-15.3	20	-3.8	1.2	-1.5	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.3	6.0	6.9
IV	–	–	–	–	17.1	5.2	27.3	23	-0.1	8	8.5	15.7	9.8	11.0	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.0	3.9	5.2
V	–	–	–	–	16.3	7.0	23.3	8	-1.6	1	9.8	14.6	10.4	11.3	–	–	–	–	–	–	–	–	–	–	–	–	7.4	8.1	5.5	7.0
VI	–	–	–	–	19.2	9.0	29.5	16	3.4	7	13.0	17.6	13.5	14.4	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.5	5.5	6.4
VII	–	–	–	–	21.9	11.0	29.8	27	7.7	4	14.0	20.2	14.9	16.0	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.5	5.9	5.9
VIII	–	–	–	–	23.8	12.1	31.5	13	5.3	31	15.0	22.2	16.6	17.6	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.3	3.5	5.1
IX	–	–	–	–	18.8	7.4	29.1	4	0.9	15	10.0	17.1	11.7	12.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.4	4.3	5.6
X	–	–	–	–	13.3	1.6	20.0	2	-5.1	16	3.4	11.6	5.6	6.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	5.8	2.9	5.7
XI	–	–	–	–	7.8	2.3	16.6	8	-1.6	18	3.6	7.0	4.3	4.8	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.1	8.2	8.3
XII	–	–	–	–	-1.9	-7.9	4.6	1	-20.9	29	-5.5	-3.3	-5.0	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.6	7.5	7.8
Rok	–	–	–	–	11.8	2.9	31.5	13.VIII	-20.9	29.XII	5.3	10.3	6.5	7.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.1	5.7	6.6

Prudnik $\varphi = 50°19'$ $\lambda = 17°34'$

I	–	–	–	–	3.6	-3.1	9.5	1, 20	-14.9	31	-1.1	2.2	0.0	0.3	4.7	5.0	4.9	4.9	7.8	6.8	7.7	7.4	1.4	2.5	1.5	1.8	6.4	5.9	6.6	6.3
II	–	–	–	–	1.1	-5.4	8.5	12	-17.4	1	-2.9	-0.2	-2.3	-1.9	4.1	4.6	4.3	4.3	8.0	7.4	7.9	7.8	1.0	1.7	1.2	1.3	7.6	8.5	7.2	7.8
III	–	–	–	–	3.0	-3.2	14.6	31	-9.0	15	-1.1	1.9	-0.5	0.0	4.6	4.8	4.6	4.7	7.8	6.8	7.4	7.3	1.3	2.5	1.6	1.8	6.9	7.1	6.3	6.8
IV	–	–	–	–	15.1	6.6	26.5	23	0.4	30	9.2	13.9	9.1	10.3	8.0	7.4	7.9	7.8	6.9	5.0	6.8	6.2	4.3	10.5	4.2	6.3	6.3	6.4	5.6	6.1
V	–	–	–	–	15.4	6.2	22.9	8	-1.4	3	10.2	13.8	9.7	10.8	9.6	10.0	10.0	9.9	7.6	6.3	8.2	7.4	3.1	6.4	2.4	4.0	6.5	7.4	5.9	6.6
VI	–	–	–	–	19.6	9.1	31.1	23	1.5	2	13.7	18.2	12.8	14.4	11.7	11.5	12.0	11.7	7.2	5.4	7.8	6.8	4.8	10.9	3.5	6.4	5.0	6.3	5.1	5.5
VII	–	–	–	–	21.1	10.0	31.0	26	5.4	9	14.9	19.4	14.0	15.6	14.0	14.1	13.5	13.9	8.1	6.3	8.4	7.6	3.3	9.1	2.9	5.1	5.3	6.5	5.6	5.8
VIII	–	–	–	–	23.8	12.0	30.7	13	4.5	31	16.4	22.2	15.5	17.4	14.6	14.7	14.6	14.6	7.8	5.5	8.2	7.2	4.2	12.8	3.2	6.7	5.5	6.4	3.3	5.1
IX	–	–	–	–	18.6	7.3	31.0	4	2.4	28	10.8	16.8	11.6	12.7	10.5	11.0	10.3	10.6	8.1	6.1	7.7	7.3	2.9	9.3	4.1	5.5	5.8	6.0	4.2	5.3
X	–	–	–	–	13.6	3.4	24.3	3	-2.9	22	5.9	12.6	6.8	8.0	8.6	9.8	8.9	9.1	9.0	6.8	8.9	8.2	1.0	5.5	1.2	2.6	6.7	4.7	5.6	5.7
XI	–	–	–	–	6.5	2.1	17.4	8	-3.6	28	3.2	5.7	3.9	4.2	6.6	7.3	7.1	7.0	8.4	7.8	8.5	8.2	1.3	2.3	1.3	1.6	7.9	9.2	8.2	8.4
XII	–	–	–	–	-1.1	-7.6	6.6	7	-22.8	22	-5.0	-2.2	-4.9	-4.2	3.7	4.0	3.7	3.8	7.9	7.3	7.9	7.7	1.0	1.6	1.0	1.2	7.2	6.8	7.3	7.1
Rok	–	–	–	–	11.7	3.1	31.1	23. VI	-22.8	22. XII	6.2	10.4	6.3	7.3	8.4	8.7	8.5	8.5	7.9	6.5	8.0	7.5	2.5	6.3	2.3	3.7	6.4	6.8	5.9	6.4

Sielec $\varphi = 50°19'$ $\lambda = 20°25'$

I	–	–	–	–	2.5	-4.1	8.5	22	-19.8	31	-2.6	1.1	-1.1	-0.9	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.6	7.3	7.5
II	–	–	–	–	0.5	-4.6	6.0	12, 13	-13.4	3	-3.4	-1.0	-2.1	-2.2	–	–	–	–	–	–	–	–	–	–	–	–	9.5	8.4	9.0	9.0
III	–	–	–	–	2.5	-5.3	15.0	31	-13.5	26	-3.5	1.4	-2.1	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.4	6.5	7.1
IV	–	–	–	–	16.5	4.7	27.0	19, 22	0.0	2	8.1	15.0	8.7	10.1	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.5	4.9	5.9
V	–	–	–	–	15.8	6.1	23.1	8	-3.1	1	9.5	14.4	9.9	10.9	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.7	6.8	7.9
VI	–	–	–	–	19.5	8.5	29.5	16	2.9	9	12.9	18.2	13.0	14.3	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.1	7.0	6.9
VII	–	–	–	–	21.8	10.2	30.7	26	5.0	5	14.4	20.3	14.0	15.7	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.3	6.2	6.7
VIII	–	–	–	–	23.1	11.1	31.2	7	4.1	31	15.0	21.7	15.5	16.9	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.6	5.9	6.2
IX	–	–	–	–	18.3	6.2	28.4	4	0.9	15	9.6	16.9	10.4	11.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.0	4.2	6.1
X	–	–	–	–	12.6	2.4	18.1	7	-4.4	24	4.1	11.5	5.9	6.8	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.0	4.0	5.7
XI	–	–	–	–	7.1	1.8	17.8	8	-2.4	17	2.8	6.2	3.8	4.2	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.6	8.4	8.5
XII	–	–	–	–	-1.6	-7.8	5.6	12	-20.8	29	-5.8	-2.5	-5.2	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.5	8.3	8.4
Rok	–	–	–	–	11.6	2.4	31.2	7.VIII	-20.8	29. XII	5.1	10.3	5.9	6.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.5	6.5	7.1

Bystrzyca Kłodzka $\varphi = 50°18'$ $\lambda = 16°39'$

I	–	–	–	–	2.1	-2.8	9.6	22	-14.8	31	-1.1	0.7	-0.8	-0.5	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.1	7.5	7.7
II	–	–	–	–	0.2	-6.4	6.4	12	-18.5	26	-3.9	-1.4	-2.2	-2.4	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.2	8.0	8.2
III	–	–	–	–	2.2	-4.6	10.9	31	-12.6	14	-3.5	0.9	-1.3	-1.3	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.7	6.6	7.0
IV	–	–	–	–	14.2	4.0	26.5	23	-0.7	30	6.5	12.7	7.9	8.8	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.3	5.6	6.1
V	–	–	–	–	14.8	5.9	22.5	8	-1.3	5	8.5	12.9	9.4	10.0	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.8	7.0	7.4
VI	–	–	–	–	19.4	8.1	29.9	23	0.7	3	12.3	17.6	12.9	13.9	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.2	5.5	5.8
VII	–	–	–	–	20.5	9.7	30.0	26	3.3	9	13.1	18.9	13.8	14.9	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.8	6.1	6.3
VIII	–	–	–	–	23.6	10.5	31.4	13	4.2	31	14.8	21.6	14.6	16.4	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.2	3.5	5.1
IX	–	–	–	–	18.0	6.2	28.5	12	-1.1	15	9.0	16.2	10.7	11.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	5.8	3.5	5.5
X	–	–	–	–	13.2	3.0	23.5	4	-4.7	22	4.5	12.1	6.2	7.2	–	–	–	–	–	–	–	–	–	–	–	–	7.5	4.5	5.6	5.9
XI	–	–	–	–	5.1	1.4	15.0	8	-5.3	26	2.5	4.3	3.0	3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.3	7.6	8.2
XII	–	–	–	–	-2.8	-8.4	4.1	16	-21.3	22	-6.7	-4.3	-5.6	-5.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	6.5	7.3	7.4
Rok	–	–	–	–	10.9	2.2	31.4	13.VIII	-21.3	22.XII	4.7	9.4	5.7	6.4	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.7	6.2	6.7

Chorzelów $H_s = 170\,m$ $h_w = 16\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU (%, %mD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < 10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	> 15	☾	●	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	≡	▦	≈
I	1.5	2.0	7	4.4	0.5	0.5	0.5	2.0	35.5	2.1	17.5	1.6	14	2.7	3.5	1.9	13	2.1	31	9.5	25	2	8	22	·	·	·	2	12	13	10	·	1	23	·
II	12.5	4.6	4	2.1	12.5	2.2	1	2.0	12	2.7	4.6	3.9	15.5	3.2	10	6.6	12	3.1	26	4.8	12	2	12	26	·	3	·	·	20	15	10	·	1	27	·
III	15.5	3.5	13.5	3.7	8	2.1	8	2.6	14	1.9	5	3.8	9	4.0	3	2.7	17	2.5	47	11.0	16	5	10	23	·	3	1	5	15	15	12	1	7	24	·
IV	3.5	1.1	13.5	2.0	6.5	2.3	8	2.3	16.5	2.5	6	2.7	6	1.2	12	3.0	18	1.8	25	6.8	28	·	·	1	7	·	·	7	7	12	7		2	·	1
V	9	1.2	7	1.4	1	2.0	2	3.0	4	1.2	11	2.0	16	3.2	10	2.3	33	1.4	118	12.6	8	·	·	2	·	1	·	1	12	25	16	5	6		3
VI	14	2.9	5	1.6	1	1.0	·	·	1.5	1.0	5.5	1.5	13.5	2.3	15.5	2.5	34	1.6	113	41.5	4	·	·	·	6	·	·	1	10	10	7	3	·		3
VII	5.5	1.4	4.5	1.7	4	1.2	1	1.0	2	1.0	1.2	1.2	14	2.0	14	1.5	36	0.9	111	36.8	18	·	·	·	6	·	·	4	10	15	14	4	2	·	5
VIII	1	1.0	3	1.0	4	1.8	·	·	5	2.4	9.5	1.5	15.5	2.1	1.2	2.9	43	1.1	28	10.1	16	·	·	·	12	·	·	3	3	9	6	1	1	·	2
IX	1	1.0	3.5	1.3	4.5	1.7	6.5	1.1	5.5	1.1	1.5	1.8	18.5	1.4	7.5	3.0	28	1.1	46	16.6	18	·	·	·	5	·	·	6	6	12	6	2	3	·	·
X	3	1.0	1.0	1.2	8	1.0	·	·	·	·	5	1.5	8.5	1.5	3.5	2.6	5.5	0.6	3	1.6	31	·	·	12	·	·	·	2	7	11	1	·	2.4	·	·
XI	4	2.9	1.5	2.0	2.5	2.0	12.5	2.0	3	2.7	5	2.2	6.5	2.3	8	1.8	11	1.8	56	18.7	15	·	·	6	·	·	·	2	20	20	13	1	7	2	·
XII	6.5	2.4	18.5	2.7	3	2.0	1.5	2.3	17.5	3.5	1.0	1.8	8	1.9	5	3.4	2.3	2.0	32	7.5	14	11	1.5	31	·	·	·	·	15	16	6	·	4	17	·
Rok	7.7	2.5	10.4.5	2.1	7.8	1.6	4.1	1.5	116.5	1.8	10.6	2.1	14.5	2.3	10.4	2.8	32.3	1.7	636	41.5	4.VI	20	45	123	36	7	1	33	137	173	108	17	58	93	14

Prudnik $H_s = 265\,m$ $h_w = 14{,}0\,m$

	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < 10°	Max < 0°	Min < 0°	Max > 25°	> 10	> 15	☾	●	≥ 0.1	≥ 1.0	≥ 10.0	≡	▦	≈
I	7.5	5.7	0.5	1.0	1.5	1.0	3	2.8	2.0	5.5	1.2	4.2	2.0	5.8	11.5	4.5	17	4.1	34	2.1	26	4	4	17	·	7	5	4	11	15	7	·	2	14	·
II	9	4.7	3	3.3	2	2.8	4.5	2.4	3.5	6.4	4	9.6	2.2	9.1	15	7.3	21	5.2	36	4.7	14	4	11	24	·	8	5	1	15	21	13	·	2	22	·
III	7.5	2.6	3.5	3.9	4	2.9	11	2.4	8	3.9	8.5	3.8	8	2.8	25.5	5.8	17	3.7	44	13.1	12	·	8	24	·	3	·	4	16	16	8	1	2	19	·
IV	7	2.6	6	2.0	4.5	2.4	8	4.1	16.5	8.1	4.5	4.9	22.5	5.0	11	6.4	10	4.6	33	10.5	4	·	·	·	7	8	2	6	12	13	9	1	1	·	·
V	9.5	2.4	1	2.5	5.5	2.1	3.5	3.4	11	3.6	11	3.1	22.5	4.7	15	3.6	14	3.0	189	31.5	13	·	·	3	·	2	·	1	9	26	22	7	1	·	7
VI	13.5	3.5	0.5	2.0	2	3.0	6	3.2	3	3.3	2.5	2.6	2.8	4.6	19.5	4.2	15	3.3	37	17.9	1	·	·	·	6	3	·	7	10	9	7	1	·	·	3
VII	9	2.4	1.5	3.0	2.5	2.4	3	2.2	9	2.3	1.0	3.2	19.5	3.4	16.5	2.7	22	2.2	69	34.6	17	·	·	·	5	·	·	6	11	15	9	2	·	·	8
VIII	4	2.8	1	3.0	1	1.5	5	1.7	4	6.8	1.5	3.2	2.2	4.5	11	4.9	3.0	2.7	43	8.5	3.7	·	·	·	12	3	1	3	4	11	7	·	1	·	6
IX	1.5	0.3	2.5	2.0	6.5	2.4	4	2.1	1.2	3.8	9.5	5.9	18.5	4.8	14.5	3.4	21	2.9	81	34.2	17	·	·	·	4	3	·	6	6	10	9	2	4	·	·
X	7	2.4	1	2.0	6	3.5	12	2.6	3.5	3.0	·	·	16	3.1	11.5	3.8	3.6	1.9	50	28.1	31	·	·	4	·	·	·	10	14	12	4	2	9	·	·
XI	3	2.8	4	3.6	6	2.4	16.5	2.6	1.4	4.2	4	1.4	26.5	3.2	7	1.9	9	2.7	58	11.7	19	·	1	7	·	2	·	·	20	16	11	1	7	3	·
XII	4	2.5	2.5	2.0	5.5	1.5	6	2.1	9.5	8.0	6.5	5.2	10.5	3.3	21.5	3.2	27	2.7	33	7.4	30	10	14	25	·	3	1	5	17	16	10	·	3	18	·
Rok	82.5	3.3	27	2.5	4.7	2.3	62.5	2.6	11.4	4.9	87.5	3.9	2.3.6	4.5	179.5	4.3	23.9	3.2	707	34.6	17.VII	18	38	104	34	4.2	1.4	5.3	145	180	116	17	3.2	7.6	24

Sielec $H_s = 202\,m$ $h_w = 16{,}7\,m$

	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < 10°	Max < 0°	Min < 0°	Max > 25°	> 10	> 15	☾	●	≥ 0.1	≥ 1.0	≥ 10.0	≡	▦	≈
I	2	6.0	3	1.0	1	1.0	1	1.0	·	·	1.3	2.9	1.4	3.4	1.0	7.0	4.9	1.8	28	7.0	24	3	6	23	·	2	·	·	16	11	7	·	1.0	1.3	·
II	·	·	4	1.1	9	2.8	·	·	1.5	7.3	10.5	7.0	1.7	5.9	5	3.6	3.7	2.8	22	5.3	5	4	12	24	·	8	2	·	21	14	6	·	4	1.8	1
III	4.5	4.1	4.5	4.7	9	3.0	·	·	·	·	1	3.0	8	5.0	11	3.4	5.5	1.6	35	7.7	16	5	10	26	·	1	·	3	16	13	8	·	9	2.0	·
IV	2	7.0	5	3.4	4	5.2	2.5	3.4	1	1.0	9	3.7	10	2.6	5.5	3.5	5.1	1.5	57	21.0	6	·	·	·	6	1	·	6	8	12	8	2	2	·	·
V		·	2	1.0	4	1.8	·	·	2	1.0	5	3.1	21.5	4.8	4.5	4.3	5.4	1.6	124	13.8	13	·	·	2	·	3	2	1	18	2.6	19	5	4	·	5
VI	1.5	3.7	·	·	·	·	·	·	·	·	4	3.9	13.5	3.3	8	3.9	6.3	1.1	84	32.5	1	·	·	·	6	2	·	1	11	9	7	2	·	·	2
VII	2	2.5	1.5	1.0	0.5	1.0	1	2.0	·	·	7.5	1.9	16	1.9	4.5	1.6	6.0	0.7	115	44.8	22	·	·	·	6	1	·	2	13	14	13	3	2	·	4
VIII	1	1.0	1	2.0	6	1.3	2	5.0	0.5	1.0	7.5	2.2	21.5	3.1	2.5	2.4	5.1	1.2	43	14.2	5	·	·	·	11	3	1	1	7	10	8	1	7	·	2
IX	·	·	1	1.0	5	3.4	1	1.0	·	·	1.0	2.6	1.3	3.0	5	3.0	5.5	1.1	44	16.0	18	·	·	·	5	·	·	7	11	11	8	2	9	·	1
X	1	1.0	4.5	1.2	7.5	1.9	·	·	·	·	1	4.0	6.5	2.9	3.5	3.4	6.9	0.6	5	1.8	1.5	·	·	11	·	1	·	7	10	6	2	·	1.5	·	·
XI	1	1.0	1	6.5	28.5	3.2	0.5	9.0	·	·	5	4.1	7.5	4.3	0.5	2.0	4.6	1.8	55	12.2	15	·	·	6	·	4	·	2	23	18	9	1	6	4	·
XII	5.5	1.9	6	1.8	7	2.7	3	3.3	2	3.0	7.5	4.2	11.5	2.8	3.5	1.9	4.7	1.4	32	7.5	14	11	1.5	3.0	·	·	·	2	23	17	7	·	5	1.7	·
Rok	20.5	2.4	33.5	2.1	81.5	2.3	11	2.1	7	1.1	81	3.6	160	3.6	63.5	3.3	63.7	1.4	644	44.8	22.VII	23	43	122	34	2.6	5	3.2	177	161	102	16	7.3	7.2	15

Bystrzyca Kłodzka $H_s = 370\,m$ $h_w = 12{,}3\,m$

	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < 10°	Max < 0°	Min < 0°	Max > 25°	> 10	> 15	☾	●	≥ 0.1	≥ 1.0	≥ 10.0	≡	▦	≈
I	11.5	4.7	·	·	·	·	5	5.5	4.3	6.0	.9	3.2	2.5	3.0	4	3.8	1.8	4.2	38	17.0	12	3	6	18	·	5	·	1	16	14	8	1	·	3	–
II	20.5	4.4	1	2.0	·	·	1.5	4.7	1.4	5.7	4	8.8	9.5	6.8	15.5	3.9	1.8	4.0	65	24.2	12	7	12	25	·	4	1	·	17	18	11	2	2	2.7	–
III	2.2	5.0	3.5	3.0	0.5	1.0	3.5	3.4	2.0	4.4	3	3.5	0.5	1.0	9	3.3	3.1	2.8	65	15.5	5	4	1.0	2.3	·	3	·	2	14	14	7	3	4	1.7	–
IV	13.5	3.0	2.5	3.6	·	·	4.5	3.0	2.3	6.1	7.5	4.9	6	4.9	9	3.9	2.4	3.4	34	6.7	11	·	·	1	3	3	·	5	12	13	10	·	1		–
V	3	2.8	2.5	1.8	1	2.5	3.5	1.7	20.5	4.0	6.5	4.0	11.5	6.0	2.5	3.8	4.2	2.2	112	30.0	14	·	·	2	·	·	·	·	13	22	14	3	1	·	–
VI	14.5	4.9	5.5	2.6	1.5	2.7	1.5	2.3	6.5	3.3	3	3.0	10.5	5.5	11	2.5	3.6	2.3	34	11.4	11	·	·	·	6	1	·	4	9	9	7	1	·	·	–
VII	6	3.3	0.5	1.0	·	·	5	3.2	18.5	3.3	1.3	5.2	7	5.0	6	2.6	3.7	2.3	39	6.6	16	·	·	·	5	1	·	·	10	14	10	·	1	·	–
VIII	0.5	2.0	1	1.0	·	·	·	·	14	4.6	1.3	4.2	13.5	3.5	6	3.1	4.5	2.0	20	4.7	14	·	·	·	12	2	·	2	5	11	9	·	1	·	–
IX	4.5	2.3	1	2.0	0.5	2.0	1.5	5.0	2.4	5.2	3	4.3	4	6.8	6.5	2.5	4.5	2.2	56	20.6	17	·	·	3	3	1	1	6	8	12	9	2	7	·	–
X	13.5	2.6	1.5	4.0	·	·	1	3.5	1.4	2.7	4	2.4	1.5	1.7	5.5	2.4	5.2	1.2	41	23.2	31	·	·	5	·	·	·	7	11	8	4	1	1.2	·	–
XI	1.4	2.6	0.5	4.0		·	3.5	4.7	2.8	6.1	6	4.8	2.5	2.4	6.5	2.6	2.9	3.1	64	24.4	1	·	2	11	·	3	·	·	20	14	10	1	2	6	–
XII	18.5	4.5	0.5	1.0	0.5	1.0	1	5.0	22.5	6.1	1.5	2.0	5	3.2	7.5	3.3	3.6	2.9	42	15.1	15	14	18	29	·	2	1	2	16	20	10	1	1	2.2	–
Rok	14.2	3.5	2.0	2.2	4	0.8	31.5	3.5	24.8	4.8	7.3.5	4.2	7.4	4.2	8.9	3.1	4.1.3	2.7	610	30.0	14.V	28	48	117	29	2.5	3	2.9	151	169	109	15	3.2	7.5	–

Głuchołazy $\varphi = 50°18'$ $\lambda = 17°23'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.5	-2.9	10.4	22	-15.8	31	-0.6	2.0	0.2	0.4	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.1	7.4	6.6
II	–	–	–	–	0.7	-5.0	7.8	12	-14.3	1	-2.9	-0.8	-2.0	-1.9	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.3	7.0	8.0
III	–	–	–	–	2.5	-4.4	14.5	31	-8.9	9, 27	-2.3	1.7	-1.3	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.5	6.9	6.9
IV	–	–	–	–	14.8	5.2	26.8	22	0.0	10	8.6	13.8	9.1	10.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.2	6.4	6.6
V	–	–	–	–	14.8	5.7	23.8	8	-0.9	1	9.4	13.2	9.2	10.2	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.3	7.3	7.4
VI	–	–	–	–	19.1	9.0	30.1	16	2.1	2	13.2	17.3	12.4	13.8	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.9	5.9	5.9
VII	–	–	–	–	20.7	10.3	32.4	26	5.6	9	14.6	18.9	13.6	15.2	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.4	5.8	5.9
VIII	–	–	–	–	23.6	12.2	30.4	13	6.5	31	16.1	21.5	15.0	16.9	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.8	3.9	4.9
IX	–	–	–	–	17.9	7.8	30.3	4	2.0	27	10.9	16.1	11.5	12.5	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.9	4.1	5.3
X	–	–	–	–	12.8	4.4	24.0	3	-0.8	22	6.2	11.7	7.3	8.1	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.3	5.0	5.3
XI	–	–	–	–	6.0	1.5	16.5	8	-5.3	23	2.8	5.2	3.5	3.8	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.2	8.5	8.2
XII	–	–	–	–	-1.8	-7.0	7.5	13	-18.2	22	-5.0	-3.2	-5.0	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.6	7.5	7.5
Rok	–	–	–	–	11.2	3.1	32.4	26.VII	-18.2	22.XII	5.9	9.8	6.1	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.6	6.3	6.5

Gliwice $\varphi = 50°18'$ $\lambda = 18°40'$

I	–	–	–	–	2.1	-2.8	7.3	20	-18.9	31	-1.1	1.5	-0.6	-0.2	5.3	5.7	5.2	5.3	8.8	8.2	8.6	8.5	0.7	1.4	0.8	1.0	6.8	7.2	6.8	6.9
II	–	–	–	–	0.5	-5.0	6.2	12	-16.1	3	-3.4	-0.8	-1.8	-2.0	4.4	5.0	4.9	4.8	8.0	8.4	8.6	8.3	0.6	0.9	0.7	0.7	9.1	8.1	7.8	8.3
III	–	–	–	–	3.1	-3.5	14.7	31	-9.4	25	-2.6	1.9	-0.4	-0.4	4.7	5.5	5.4	5.2	8.9	7.5	8.7	8.4	0.5	1.8	0.8	1.0	7.4	7.3	6.2	7.0
IV	–	–	–	–	15.2	–	26.4	24	–	–	7.8	14.1	9.8	10.4	8.9	8.5	9.0	8.6	8.3	5.8	7.6	7.2	2.1	9.3	3.9	5.1	6.1	5.9	5.3	5.8
V	–	–	–	–	15.2	6.8	22.0	8	-1.1	1	9.0	13.3	10.3	10.7	10.4	10.4	11.0	10.6	8.9	6.8	8.6	8.1	1.3	5.5	1.9	2.9	7.2	7.5	7.1	7.3
VI	–	–	–	–	19.4	9.3	29.6	16	1.0	2	12.8	18.2	13.8	14.6	12.3	11.9	12.7	12.3	8.1	5.6	7.8	7.2	3.1	10.4	3.8	5.8	4.8	6.3	5.8	5.6
VII	–	–	–	–	21.1	10.6	30.0	26	6.1	5	13.8	19.4	15.1	15.8	13.7	13.7	13.9	13.8	8.6	6.1	8.0	7.6	2.2	9.4	3.7	5.1	5.7	6.7	5.8	6.1
VIII	–	–	–	–	23.6	12.3	31.3	7	6.4	31	15.0	22.0	16.1	17.3	14.5	14.7	15.5	14.9	8.5	5.6	8.4	7.5	2.7	12.4	3.2	6.1	5.9	5.6	4.3	5.3
IX	–	–	–	–	18.2	7.4	28.7	4	2.6	20	9.8	16.5	11.4	12.3	11.1	12.3	11.6	11.7	9.0	6.7	8.5	8.1	1.4	7.2	2.3	3.6	6.3	6.2	3.6	5.4
X	–	–	–	–	13.7	4.4	22.5	4	-1.9	22	5.7	12.8	7.6	8.4	9.0	11.1	9.9	10.0	9.5	7.6	9.3	8.8	0.4	4.2	0.8	1.8	7.4	5.0	4.5	5.6
XI	–	–	–	–	6.8	2.3	17.8	8	-2.1	21	3.2	5.9	4.0	4.3	7.2	8.0	7.6	7.6	9.2	8.4	9.2	8.9	0.7	2.0	0.8	1.2	7.9	8.1	7.9	8.0
XII	–	–	–	–	-1.9	-7.0	7.5	13	-17.5	22	-5.3	-2.9	-4.7	-4.4	3.9	4.4	4.1	4.1	8.9	8.4	8.8	8.7	0.5	0.8	0.5	0.6	7.6	7.5	6.4	7.2
Rok	–	–	–	–	11.4	–	31.3	7.VIII	-18.9	31. I	5.4	10.2	6.7	7.2	8.8	9.3	9.2	9.1	8.7	7.1	8.5	8.1	1.4	5.4	1.9	2.9	6.8	6.8	6.0	6.5

Mielec $\varphi = 50°18'$ $\lambda = 21°27'$

I	996.8	1014.8	974.2	1018.2	1.6	-2.5	8.0	20	-16.9	31	-0.9	1.3	-0.5	-0.1	5.0	5.3	5.0	5.1	8.5	7.7	8.2	8.1	0.9	1.7	1.1	1.2	7.8	6.8	6.8	7.1
II	995.1	1012.3	966.4	1016.7	0.5	-4.4	7.0	13	-12.3	1	-3.1	-0.9	-1.8	-1.9	4.2	4.6	4.7	4.5	8.5	7.9	8.5	8.3	0.7	1.2	0.8	0.9	9.0	8.9	9.0	9.0
III	990.3	1007.2	971.6	1011.7	2.7	-5.1	14.8	5	-18.8	20	-3.7	1.4	-1.2	-1.2	4.5	5.2	5.1	4.9	8.7	7.4	8.5	8.2	0.7	1.9	0.9	1.2	7.6	7.5	7.1	7.4
IV	993.6	1006.2	969.6	1014.1	17.3	5.3	27.8	23	0.3	30	8.5	15.6	10.1	11.1	8.5	8.4	8.7	8.5	7.7	5.1	7.2	6.7	3.0	10.9	4.2	6.0	6.6	6.9	5.7	6.2
V	993.1	1000.2	977.7	1013.6	16.4	7.2	23.4	8	-2.2	1	9.8	14.5	11.0	11.6	10.9	10.7	11.1	10.9	8.8	6.4	8.3	7.8	1.4	6.5	2.4	3.4	8.0	8.8	6.6	7.8
VI	997.6	1006.9	987.6	1018.0	19.7	9.2	29.8	23	2.9	7	13.0	17.9	14.2	14.8	12.4	12.2	12.7	12.4	8.0	6.0	7.7	7.2	3.3	9.9	4.4	5.9	6.3	8.0	5.9	6.7
VII	994.7	1005.3	983.0	1014.9	22.2	11.3	30.5	27	5.8	30	14.2	20.4	15.7	16.5	13.9	13.0	14.2	13.7	8.5	5.5	7.9	7.3	2.5	11.6	3.9	6.0	6.3	6.8	6.2	6.4
VIII	996.3	1003.5	987.2	1016.4	24.1	12.6	32.1	13	6.4	31	15.3	22.4	17.5	18.7	15.0	14.5	15.7	15.1	8.5	5.5	7.7	7.2	2.7	13.3	4.8	6.9	6.4	6.9	5.1	6.1
IX	996.9	1009.6	983.0	1017.5	18.8	7.7	28.6	4	1.6	25	10.1	16.9	12.2	12.8	10.6	11.2	11.5	11.1	8.6	6.0	8.1	7.6	2.1	8.9	3.2	4.7	6.4	7.5	4.8	6.2
X	1002.2	1015.5	989.1	1023.2	13.3	1.7	19.8	2	-5.4	16	3.4	11.8	5.9	6.8	7.8	9.7	8.7	8.7	9.6	7.0	9.1	8.6	0.4	4.4	0.8	1.9	7.5	5.8	3.4	5.6
XI	996.7	1011.3	998.2	1017.8	7.9	2.5	16.8	8	-1.4	18	3.8	7.0	4.4	4.9	7.5	8.2	7.6	7.8	9.1	8.0	8.9	8.7	0.9	2.5	1.0	1.5	8.8	8.3	9.2	8.8
XII	996.1	1023.4	955.1	1017.9	-1.9	-7.6	4.0	14	-19.4	29	-5.0	-3.2	-4.7	-4.4	3.9	4.1	4.0	4.0	8.6	8.0	8.6	8.4	0.6	1.0	0.7	0.8	8.4	8.4	8.2	8.3
Rok	995.8	1023.4	955.1	1016.5	11.9	3.2	32.1	13.VIII	-19.4	29.XII	5.4	10.4	6.9	7.4	8.7	8.9	9.1	8.9	8.6	6.7	8.2	7.8	1.6	6.2	2.4	3.4	7.4	7.6	6.5	7.2

Spalona $\varphi = 50°17'$ $\lambda = 16°33'$

I	–	–	–	–	-0.6	-5.2	4.4	22	-16.3	31	-3.1	-2.1	-3.0	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.3	8.6	8.5
II	–	–	–	–	-2.5	-7.5	2.7	12	-15.3	1	-5.5	-3.8	-4.6	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	8.8	9.6	8.5	9.0
III	–	–	–	–	-1.2	-6.7	7.8	5	-14.0	14	-4.6	-2.3	-3.8	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.2	7.1	7.9
IV	–	–	–	–	10.1	3.2	22.3	23	-3.0	30	5.6	8.8	5.9	6.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.5	6.3	7.0
V	–	–	–	–	10.9	3.8	17.6	8, 19	-5.1	1	6.0	9.0	6.7	7.1	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.4	8.1	8.2
VI	–	–	–	–	15.0	7.1	25.2	24	-0.3	6	10.5	13.6	10.5	11.3	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.0	6.1	6.4
VII	–	–	–	–	16.2	8.9	25.4	26	3.7	4	11.7	15.0	11.4	12.4	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.0	6.3	6.7
VIII	–	–	–	–	18.9	10.6	27.0	13	6.2	30	13.6	17.4	13.3	14.4	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.3	4.3	6.0
IX	–	–	–	–	14.2	6.5	24.1	4	1.9	20	8.5	12.2	9.6	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.6	4.7	5.9
X	–	–	–	–	10.9	3.9	19.9	2, 4	-1.4	30	6.6	9.5	6.4	7.2	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.0	5.5	5.3
XI	–	–	–	–	–	-1.1	–	–	-7.3	23	0.3	1.2	0.5	0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.9	9.3	9.2	9.1
XII	–	–	–	–	-3.1	-8.8	7.2	9	-21.5	23	-6.8	-5.9	-6.6	-6.5	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.6	7.6	7.9
Rok	–	–	–	–	–	1.7	27.0	13.VIII	-21.5	23.XII	3.6	6.0	3.9	4.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.6	6.9	7.3

Głuchołazy

$H_s = 344\ m$ $h_w = 10{,}0\ m$ I–IX, $h_w = 12{,}7\ m$ X–XII **1962**

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
	ROZKŁAD WIATRU (°D, v mD)																		OPAD R			LICZBA DNI (n) Temperatura T				Wiatr v				Opad R					
I	0.5	4.0	1	1.0	·	·	3.5	1.9	10	3.8	29.5	3.9	21.5	2.6	13	4.7	14	3.0	43	8.7	28	3	5	19	·	3	1	2	8	13	9	·	3	14	·
II	4	4.4	3	1.0	5	1.2	3	1.0	5.5	5.8	10	4.8	16	3.2	23.5	4.2	14	3.1	40	5.3	24	2	11	25	·	3	·	·	17	18	11	·	1	23	·
III	5	5.9	4	2.0	4	1.5	6	1.0	8.5	1.4	18	2.5	9.5	1.7	23	2.5	15	1.9	51	16.8	12	·	10	25	·	1	·	2	13	14	7	1	1	20	·
IV	3.5	1.8	6.5	1.4	4.5	1.8	7.5	3.9	12	4.8	19	1.7	14.5	1.8	12.5	2.4	10	2.2	58	11.6	28	·	·	·	7	3	·	6	15	14	11	1	1	·	·
V	·	·	1.5	1.3	6.5	1.4	3	1.3	3	1.7	17.5	1.9	34.5	1.8	6	2.0	21	1.4	194	43.4	14	·	·	2	·	·	·	1	10	26	22	6	1	·	5
VI	5	3.3	·	·	4	3.0	1	3.0	8.5	1.2	22.5	2.2	25	2.3	18	2.8	6	2.2	34	16.7	1	·	·	·	6	·	·	6	10	10	7	1	·	·	1
VII	0.5	3.0	·	·	2	2.0	6	2.3	5	1.2	25	1.8	27.5	1.6	8	2.6	19	1.4	52	24.4	17	·	·	·	5	·	·	3	7	12	9	1	·	·	2
VIII	·	·	1	3.0	1	4.0	1.5	9.7	12	2.7	33	1.9	27.5	2.0	6	2.8	11	2.0	44	13.3	14	·	·	·	12	1	·	2	3	11	9	1	·	·	4
IX	·	·	1	1.0	2	3.0	3	2.3	11	1.6	17.5	3.1	25	2.1	9.5	1.9	21	1.7	99	50.5	17	·	·	·	4	·	·	7	9	12	7	2	3	·	·
X	2	1.0	10	2.6	3.5	2.3	1	1.0	13	1.8	5	1.2	11.5	1.1	17	1.7	30	1.2	64?	—	—	·	·	1	·	·	·	10	11	13	8	3	10	·	·
XI	1.5	1.0	0.5	1.0	0.5	3.0	12.5	4.4	10	4.7	12	1.8	10.5	1.3	9.5	1.6	33	1.7	75	19.5	1	·	1	11	·	2	·	1	19	15	12	2	4	8	·
XII	1.5	1.3	2	1.5	2	1.5	3	1.7	7	4.9	8.5	3.1	7.5	1.3	15.5	1.5	46	1.2	34	8.6	16	11	16	27	·	·	·	2	18	17	9	·	1	26?	·
Rok	23.5	2.1	30.5	1.3	35	2.1	51	2.8	105.5	3.0	217.5	2.5	230.5	1.9	161.5	2.6	240	1.9	788?	50.5	17.IX	16	43	110	34	13	1	42	140	175	121	18	25	91?	12

Gliwice

$H_s = 220\ m$ $h_w = 13\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	7	2.4	5	1.2	0.5	1.0	1	1.0	16.5	1.5	41.5	2.1	9.5	2.5	9	2.7	3	2.0	44	9.0	11	2	6	20	·	·	·	1	12	13	10	·	1	11	·
II	11.5	2.1	7	1.7	11	1.1	3.5	1.0	9.5	2.0	14	4.9	11.5	5.5	12	5.6	4	3.2	48	8.5	16	4	11	25	·	4	2	·	19	17	11	·	3	25	·
III	20.5	2.6	9	1.3	11	1.1	12.5	1.3	9	1.2	11.5	1.6	25	2.8	10	3.8	7	1.8	56	13.2	12	·	8	25	·	·	·	3	14	15	11	1	3	13?	·
IV	16.5	1.4	6.5	1.2	5	1.3	10.5	1.7	12	1.8	13	2.9	5.5	1.8	14	2.4	7	1.8	49	9.8	26	·	·	—	5	·	·	7	10	13	9	·	·	·	·
V	15.5	1.4	6.5	1.0	4.5	1.2	9.5	1.4	9.5	1.9	18	1.5	12.5	4.2	14	2.5	3	1.9	164	32.3	31	·	·	2	·	2	·	·	10	25	18	6	·	·	5
VI	23	2.3	10.5	1.2	1	1.5	4	1.0	5.5	1.5	11.5	1.7	8.5	2.5	20	2.0	6	1.8	63	30.6	1	·	·	·	6	·	·	5	10	14	8	2	·	·	2
VII	21.5	1.3	6	1.2	4	1.0	3	1.0	7	1.2	17.5	2.2	9	1.7	18	1.4	7	1.4	71	26.1	17	·	·	·	4	·	·	5	10	16	13	3	·	·	6
VIII	10	1.4	4.5	1.0	6	1.2	9	1.1	10.5	1.8	8.5	2.6	14.5	1.9	23	1.7	7	1.5	73	34.1	15	·	·	·	11	·	·	4	5	14	11	1	2	·	3
IX	9.5	1.7	3.5	1.6	6.5	1.5	8	1.2	13	1.3	16.5	3.6	15	2.0	13	1.9	5	1.9	67	24.0	17	·	·	·	3	·	·	10	10	15	10	2	4	·	1
X	18.5	1.2	5.5	1.2	20	1.0	12.5	1.0	10	1.0	8.5	2.3	7	2.4	7	1.6	4	1.3	25	10.0	28	·	·	4	·	·	·	6	11	9	4	1	11	·	·
XI	11	1.1	9.5	1.5	15.5	1.4	17.5	1.4	7	2.0	11.5	2.6	3	1.7	13	1.7	2	1.6	85	16.0	15	·	1	8	·	·	·	1	19	19	13	3	5	6	·
XII	15.5	1.6	14	1.6	6	1.6	14.5	1.1	12	2.3	19	4.3	4	1.2	6	1.7	2	2.1	50	14.2	13	10	17	28	·	2	·	2	18	15	9	1	6	27	·
Rok	180	1.7	87.5	1.3	91	1.2	105.5	1.2	121.5	1.6	191	2.7	102.5	2.5	159	2.4	57	1.9	795	34.1	15.VIII	16	43	—	29	8	2	44	148	185	127	20	35	82?	17

Mielec

$H_s = 168\ m$ $H_b = 170{,}2\ m$ $h_w = 24\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	1.5	8.0	6	4.3	·	·	12	4.7	26	5.3	24	3.8	15.5	5.0	5	6.4	3	4.6	29	8.0	25	2	8	20	·	1	·	1	15	13	11	·	1	17	·
II	7.5	3.8	5.5	2.9	12.5	4.2	5	2.9	7.5	6.0	9	6.6	23	6.3	9	6.6	5	5.0	32	6.5	12	2	13	24	·	7	4	·	20	17	11	·	1	21	·
III	8.5	4.2	16	4.8	9.5	3.5	16	4.4	10	4.2	3	3.3	9.5	7.8	8.5	4.3	12	4.0	55	16.7	16	5	10	24	·	6	·	4	19	15	11	1	2	23	·
IV	7.5	3.0	10	2.8	5.5	5.0	10	5.6	14.5	4.4	6.5	4.4	11	3.9	9	5.2	16	3.5	26	9.7	6	·	·	·	6	5	·	6	8	9	6	·	1	·	2
V	6.5	2.8	6	1.9	5	1.9	9.5	2.7	7	2.4	12	3.2	22	4.4	6	3.8	19	2.6	117	11.6	21	·	·	3	·	3	·	·	16	26	18	3	3	·	3
VI	12	4.2	6	3.2	1	1.0	5.5	1.5	3.5	2.3	8.5	3.6	24	4.1	9.5	4.8	20	2.9	103	33.3	4	·	·	·	8	2	·	·	11	11	10	3	1	·	3
VII	4.5	1.8	8	3.2	4	1.8	6	2.0	6.5	2.3	12	2.7	22.5	3.0	13.5	3.2	16	2.3	95	33.1	18	·	·	·	8	1	·	2	12	14	12	4	1	·	7
VIII	4	2.1	4.5	2.6	6	2.1	8	2.7	9.5	2.8	9.5	2.5	27	4.2	5.5	4.5	19	2.6	23	8.9	16	·	·	·	13	1	·	1	7	8	6	·	3	·	3
IX	·	·	5.5	2.0	7	3.3	5.5	2.6	14	2.8	14	3.6	18	4.2	7	4.0	19	2.7	50	17.7	18	·	·	·	4	·	·	3	9	8	7	2	3	·	1
X	3.5	2.3	8.5	2.4	11.5	2.4	2.5	1.2	2.5	3.2	5.5	3.6	10	3.9	1	6.0	48	1.4	3	2.0	31	·	·	14	·	·	·	6	8	3	2	·	20	·	·
XI	7	2.6	9.5	3.2	29	4.6	13.5	4.8	2	4.5	6.5	3.8	12.5	3.4	3	3.0	7	3.7	56	16.8	15	·	·	6	·	2	·	·	21	17	12	1	6	3	·
XII	10.5	4.4	17.5	3.5	3.5	3.0	8.5	5.2	13	6.0	9	3.5	13	3.2	4	3.1	14	3.5	37	7.3	14	11	14	30	·	2	·	·	20	18	8	·	6	18	·
Rok	73	3.3	103	3.1	94.5	2.7	102	3.4	116	3.8	119.5	3.7	208	4.4	81	4.6	198	3.2	626	33.3	4.VI	20	45	121	39	30	4	23	166	159	114	14	48	82	19

Spalona

$H_s = 790\ m$ $h_w = 13{,}5\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	66	19.2	12	6	16	29	·	—	—	·	22	21	14	2	8	30?	·
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	72	23.6	12	9	19	28	·	—	—	·	19	19	13	1	9	28	·
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	102	22.1	30	4	21	29	·	—	—	·	19	17	10	5	7	31	·
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	41	6.5	26	·	·	14	·	—	—	3	14	11	11	·	7	11?	1
V	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	145	27.6	13	·	·	5	·	—	—	·	15	21	17	6	8	3	2
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	38	10.6	11	·	·	1	1	—	—	1	9	13	7	1	2	·	3
VII	1	2.0	9.5	1.6	10.5	1.7	6	2.6	14.5	3.1	25	3.6	13.5	3.5	1	2.5	12	2.5	66	15.9	13	·	·	·	1	·	·	·	11	19	14	2	6	·	4
VIII	·	·	2.5	1.0	1.5	1.0	8	1.9	12	2.6	34	3.7	27.5	3.8	0.5	2.0	7	3.0	35	9.9	7	·	·	·	1	·	·	·	5	13	8	·	1	·	4
IX	2.5	1.0	4.5	1.9	1.5	1.7	12	1.6	16	3.0	24.5	3.8	12	2.7	5	2.1	12	2.4	74	21.5	17	·	·	·	·	·	·	5	10	14	12	2	6	·	·
X	1	1.0	12.5	1.4	12.5	1.4	13.5	1.7	18.5	2.6	13	3.5	2	2.2	5	2.6	15	1.8	39	24.7	31	·	·	4	·	·	·	8	11	13	4	1	10	·	·
XI	1.5	1.7	16.5	2.8	2.5	2.8	14.5	3.7	12.5	4.0	21.5	4.0	1.5	4.0	0.5	1.0	19	2.8	79	21.4	1		—	19	·	·	·	·	25	17	12	2	13	12	·
XII	·	·	19	3.2	7.5	1.7	12.5	2.4	11	5.3	13.5	7.0	7.5	6.9	2	2.0	20	3.4	68	17.0	23	12	20	31	·	3	·	2	20	20	12	1	13	31	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	825	27.6	13.V	31	—	160	3	—	—	19	180	198	134	23	90	146?	14

Olkusz $\varphi = 50°17'$ $\lambda = 19°34'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.2	-3.8	9.3	22	-18.8	31	-1.6	1.2	-1.0	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	-0.1	-5.7	6.2	13	-14.9	3	-4.2	-0.9	-3.0	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	1.6	-6.3	13.4	31	-15.0	26	-3.2	0.8	-2.7	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	14.7	4.7	26.0	24	0.6	2	8.7	13.7	8.7	10.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	14.7	6.0	21.6	8	-2.2	1, 2	9.5	13.3	9.8	10.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	18.5	8.7	29.4	16	0.6	2	12.6	16.8	12.7	13.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	20.4	10.1	29.5	26	5.5	30	14.6	18.8	14.2	15.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	22.8	11.6	31.1	7	5.0	31	15.2	21.1	15.8	17.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	17.4	6.8	28.1	4	2.5	25	9.5	15.7	10.8	11.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	13.4	3.5	21.8	4	-3.3	22	5.2	12.0	6.1	7.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.0	1.5	17.3	8	-3.1	24	2.4	5.0	3.1	3.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-2.8	-8.2	5.7	13	-17.8	26	-6.4	-4.0	-5.8	-5.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	10.7	2.4	31.1	7.VIII	-18.8	31.I	5.2	9.5	5.7	6.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Borusowa $\varphi = 50°17'$ $\lambda = 20°47'$

I	–	–	–	–	2.0	-3.6	7.4	20	-15.8	31	-1.8	0.8	-1.0	-0.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	0.6	-4.2	7.7	13	-11.0	25	-3.2	-1.1	-1.7	-1.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	2.4	-4.9	14.0	31	-17.4	26	-3.6	1.2	-1.3	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	16.5	5.4	26.3	23	0.0	2	7.7	14.6	10.2	10.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15.6	7.0	22.6	8	-0.9	1	9.1	13.9	10.9	11.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	18.7	9.0	29.3	24	3.4	7	12.6	16.9	13.9	14.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.5	10.7	29.7	26	6.5	30	14.0	20.1	15.2	16.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	23.6	12.0	30.8	7	5.4	31	14.9	21.7	17.0	17.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	18.2	7.3	28.5	4	2.1	15, 25	10.0	16.7	12.1	12.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	12.6	3.0	17.8	7	-4.1	16	4.0	11.0	6.4	7.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	7.4	2.3	16.8	8	-2.2	24	3.1	6.7	4.4	4.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-1.5	-7.4	3.9	13, 14	-19.2	29	-5.3	-2.7	-4.6	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	11.5	3.0	30.8	7.VIII	-19.2	29.XII	5.1	10.0	6.8	7.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Zakrzów $\varphi = 50°16'$ $\lambda = 18°09'$

I	–	–	–	–	2.7	-2.3	7.6	22	-17.9	31	-1.0	1.8	-0.4	0.0	–	–	–	–	–	–	–	–	–	–	–	–	70	73	85	76
II	–	–	–	–	1.1	-5.0	5.8	12	-16.7	3	-3.4	0.0	-1.6	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	91	90	74	85
III	–	–	–	–	3.5	-3.2	15.2	31	-7.8	20	-2.3	2.1	-0.1	-0.1	–	–	–	–	–	–	–	–	–	–	–	–	85	77	67	76
IV	–	–	–	–	15.6	5.1	26.9	24	1.0	3	8.3	14.7	9.2	10.4	–	–	–	–	–	–	–	–	–	–	–	–	66	63	61	63
V	–	–	–	–	15.4	6.4	22.6	19	-0.9	1	9.9	14.1	10.0	11.0	–	–	–	–	–	–	–	–	–	–	–	–	81	78	83	81
VI	–	–	–	–	20.2	9.1	30.7	24	1.7	2	13.0	19.1	13.3	14.7	–	–	–	–	–	–	–	–	–	–	–	–	55	52	55	54
VII	–	–	–	–	21.6	10.2	29.9	26	5.7	30	14.5	20.0	15.0	16.1	–	–	–	–	–	–	–	–	–	–	–	–	57	66	68	64
VIII	–	–	–	–	24.0	11.7	30.9	7	6.3	29	15.7	22.2	15.9	17.4	–	–	–	–	–	–	–	–	–	–	–	–	52	36	33	40
IX	–	–	–	–	18.2	7.3	29.3	4	0.1	15	10.4	17.0	11.6	12.6	–	–	–	–	–	–	–	–	–	–	–	–	71	58	45	58
X	–	–	–	–	13.8	3.9	22.9	4	-2.9	23	6.3	12.9	7.4	8.5	–	–	–	–	–	–	–	–	–	–	–	–	80	57	45	61
XI	–	–	–	–	7.1	2.0	20.2	7	-2.8	28	3.0	6.0	3.9	4.2	–	–	–	–	–	–	–	–	–	–	–	–	85	77	84	82
XII	–	–	–	–	-1.7	-7.4	6.7	13	-18.3	22	-5.6	-2.5	-5.0	-4.5	–	–	–	–	–	–	–	–	–	–	–	–	79	78	68	75
Rok	–	–	–	–	11.8	3.2	30.9	7.VIII	-18.3	22.XII	5.7	10.6	6.6	7.4	–	–	–	–	–	–	–	–	–	–	–	–	73	67	64	68

Długopole $\varphi = 50°15'$ $\lambda = 16°38'$

I	–	–	–	–	1.6	-3.1	8.0	22	-14.0	31	-1.1	0.2	-1.1	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	79	85	87	84
II	–	–	–	–	0.0	-6.0	5.7	12	-18.7	26	-4.1	-1.7	-2.3	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	92	95	91	93
III	–	–	–	–	1.6	-5.5	9.5	31	-13.7	14	-3.9	0.5	-1.8	-1.8	–	–	–	–	–	–	–	–	–	–	–	–	83	77	69	76
IV	–	–	–	–	13.5	3.9	25.0	23, 24	-0.9	30	6.1	12.1	7.8	8.4	–	–	–	–	–	–	–	–	–	–	–	–	84	82	69	78
V	–	–	–	–	14.3	5.4	21.2	31	-2.1	1	8.7	12.4	9.2	9.8	–	–	–	–	–	–	–	–	–	–	–	–	76	84	77	79
VI	–	–	–	–	18.6	8.2	28.5	23	-0.1	3	11.9	16.9	12.6	13.5	–	–	–	–	–	–	–	–	–	–	–	–	63	65	57	62
VII	–	–	–	–	19.7	9.4	28.8	26	3.0	9	12.9	18.4	13.9	14.8	–	–	–	–	–	–	–	–	–	–	–	–	70	69	65	68
VIII	–	–	–	–	22.8	10.7	29.9	13	4.0	21	14.6	21.0	14.6	16.2	–	–	–	–	–	–	–	–	–	–	–	–	60	69	36	55
IX	–	–	–	–	17.4	6.1	27.8	12	-0.7	15	8.9	15.5	10.6	11.4	–	–	–	–	–	–	–	–	–	–	–	–	69	64	43	59
X	–	–	–	–	13.0	3.1	22.6	4	-4.2	22	4.8	11.8	6.5	7.4	–	–	–	–	–	–	–	–	–	–	–	–	74	60	62	65
XI	–	–	–	–	4.8	1.2	14.6	8	-6.4	24	2.5	3.8	2.9	3.0	–	–	–	–	–	–	–	–	–	–	–	–	92	92	82	89
XII	–	–	–	–	-3.0	-8.8	4.0	16	-22.0	22	-6.6	-4.4	-5.7	-5.6	–	–	–	–	–	–	–	–	–	–	–	–	86	82	76	81
Rok	–	–	–	–	10.4	2.0	29.9	13.VIII	-22.0	22.XII	4.5	8.9	5.6	6.2	–	–	–	–	–	–	–	–	–	–	–	–	77	77	68	74

Olkusz — $H_s = 360m$ — $h_w = 16{,}5m$ — 1962

MIESIĄC	ROZKŁAD WIATRU (%D, %D) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	☁	●	Opad R ≥ 0.1	≥ 10	≥ 100	≡	⊞	Ra
I	3	4.0	0.5	3.0	2	5.0	0.5	3.0	8.5	2.4	2.5	2.9	34.5	3.0	10	3.4	9	2.7	53	10.9	27	3	5	23	·	·	·	–	–	16	11	1	·	16	
II	6.5	3.8	2.5	3.4	13	3.2	2.5	1.0	2	1.0	8.5	5.2	29.5	5.4	6.5	2.8	13	3.6	65	16.1	16	4	12	27	·	3	1	–	–	17	12	1	1	26	1
III	6.5	4.4	8	3.9	18.5	2.1	6.5	1.4	4	2.1	4	2.4	14	2.5	9.5	2.3	22	2.0	78	19.1	16	9	13	27	·	1	·	–	–	15	10	2	·	29	·
IV	11	2.0	2.5	2.4	12.5	1.8	9.5	2.5	8.5	2.6	6	2.6	16	2.5	9	2.7	15	2.0	91	31.3	13	·	·	·	4	·	·	–	–	14	12	2	·	·	2
V	6.5	1.0	1.5	1.0	9	1.4	6	1.6	5	1.5	4	2.6	30.5	3.6	10.5	2.3	20	2.0	137	19.3	20	·	·	3	·	1	·	–	–	23	18	6	·	·	1
VI	10	1.4	1.5	1.7	7	2.1	·	·	3	1.3	3.5	3.6	23.5	3.9	20.5	2.9	21	2.2	70	25.6	1	·	·	·	6	2	·	–	–	10	7	2	·	·	2
VII	5.5	2.1	1	1.0	5.5	1.5	1.5	1.7	4	3.0	12	2.0	20.5	2.2	21	2.1	22	1.6	130	39.3	17	·	·	·	5	·	·	–	–	14	13	4	·	·	5
VIII	0.5	1.0	4	2.0	7	2.3	3	2.7	4	3.4	9	2.0	28	2.4	7.5	1.9	30	1.6	62	12.5	15	·	·	·	9	·	·	–	–	15	9	2	2	·	2
IX	2.5	1.6	2.5	1.8	11	3.5	4	1.0	5.5	2.9	5.5	2.7	22	3.3	13	2.6	24	2.1	71	17.8	18	·	·	·	2	1	·	–	–	13	9	3	5	·	·
X	7.5	2.0	7	1.9	21.5	1.8	5	1.3	1	3.0	6	2.7	6.5	2.7	8.5	2.6	30	1.4	26	8.0	5	·	·	10	·	·	·	–	–	8	6	·	6	·	·
XI	6.5	1.9	6	4.5	30.5	2.5	4.5	2.6	6.5	2.4	8.5	2.5	11.5	2.0	2	2.2	14	2.1	76	11.4	22	·	2	13	·	·	·	–	–	17	15	2	7	4	·
XII	3.5	3.0	1.5	1.7	2.0	2.9	1	1.0	1.0	2.6	5.5	3.3	1.5	3.2	5.5	2.9	3.1	1.9	52	13.4	15	13	18	30	·	·	·	–	–	17	12	1	4	19	·
Rok	69.5	2.4	38.5	2.4	157.5	2.5	4.4	1.6	6.2	2.4	97.5	2.9	251.5	3.1	123.5	2.6	251	2.1	911	39.3	17.VII	29	50	133	26	8	1	–	–	179	134	26	25	96	13

Borusowa — $H_s = 170m$ — $h_w = 16m$

I	6	5.5	2	3.0	·	·	0.5	2.0	22.5	3.3	9	3.3	21	4.4	5	4.3	27	2.8	24	6.4	25	4	6	22	·	·	·	–	–	11	8	·	1	16	·
II	8.5	4.9	·	·	14	2.1	2	1.5	7.5	4.1	4.5	9.9	23.5	6.2	12	6.8	12	4.5	13	3.0	19	3	11	24	·	7	2	–	–	10	7	·	·	19	·
III	10	2.7	3.5	1.6	20.5	2.7	4	3.8	5	2.6	1	2.0	11	3.4	3	5.3	35	1.8	21	4.4	23	4	8	24	·	1	·	–	–	10	9	·	5	21	·
IV	11	2.7	·	·	8.5	2.9	6.5	5.2	6	3.3	2	2.0	16	4.0	5	6.0	35	2.3	52	22.0	13	·	·	·	4	2	1	–	–	9	7	2	·	·	·
V	10	2.1	·	·	·	·	·	·	2	4.5	1	7.0	28.5	4.4	6.5	2.3	4.5	1.9	107	17.4	8	·	·	2	·	2	1	–	–	24	19	2	1	·	4
VI	15	3.1	4.5	2.7	1.5	1.0	1.5	1.0	·	·	5.5	2.7	11.5	3.9	23.5	3.5	27	2.3	84	32.8	1	·	·	·	6	1	1	–	–	10	10	2	2	·	2
VII	13.5	1.6	3	2.3	1.5	1.3	2	2.0	0.5	4.0	3.5	3.1	21.5	2.9	14.5	2.8	33	1.6	84	25.2	18	·	·	·	4	1	·	–	–	15	12	2	1	·	6
VIII	6	2.3	2	2.0	2	1.8	2	3.2	3	4.7	7	2.6	23	4.0	12	4.2	36	2.2	46	16.2	6	·	·	·	12	2	·	–	–	9	6	2	4	·	2
IX	3	5.3	1	1.5	4	3.6	1	3.0	3	3.0	12	4.1	18.5	4.6	10.5	4.0	37	2.4	46	18.9	18	·	·	·	3	3	·	–	–	10	8	2	10	·	2
X	2.5	2.2	4.5	2.0	9.5	2.3	2	2.0	·	·	·	·	12.5	3.1	8	3.4	5.4	1.1	2	1.0	31	·	·	8	·	·	·	–	–	2	1	·	2.6	·	·
XI	7	1.6	1	1.0	2.4	3.3	4.5	4.9	3.5	1.4	·	·	12.5	3.0	5.5	2.5	32	1.9	48	12.0	15	·	·	5	·	·	·	–	–	15	11	1	–	2	·
XII	5.5	2.1	4.5	2.8	7	2.1	·	·	1.6	3.2	1.5	7.0	15.5	2.7	5	3.0	38	1.7	26	4.8	31	11	14	28	·	·	·	–	–	16	7	·	–	17	·
Rok	9.8	3.0	2.6	1.6	92.5	1.9	2.6	2.4	6.9	2.8	4.7	3.6	21.5	3.9	110.5	4.0	411	2.2	553	32.8	1.VI	22	39	113	29	19	5	–	–	141	105	13	–	75	16

Zakrzów — $H_s = 217m$ — $h_w = 13{,}0m$ I–VII, $16{,}4m$ VIII–XII

I	13	3.8	3	3.7	·	·	2.5	2.4	3.8	3.6	8.5	5.6	1	2.0	12	3.9	15	3.2	32	10.9	11	2	3	20	·	·	·	1	17	12	10	1	1	3	·
II	19	3.4	·	·	2	1.5	0.5	1.0	18.5	3.8	6	4.8	4	3.2	18	5.9	16	3.4	23[2]	4.1	19	6	9	25	·	2	1	·	17	12	8	·	2	18	·
III	14.5	5.0	4.5	3.8	8.5	1.6	1.5	2.0	10.5	2.9	7.5	3.0	3.5	3.0	17.5	4.6	25	2.7	41	13.1	12	·	7	23	·	2	·	·	20	11	9	1	6	8	·
IV	7	3.0	2	2.5	5.5	1.9	4.5	2.6	2.5	3.3	3	4.2	2	1.5	2.2	3.9	19	2.6	31	5.2	4	·	·	·	7	·	·	5	12	14	12	·	·	·	·
V	14	2.8	1	2.0	2	1.0	1.5	1.3	2.2	2.2	2.5	3.0	1	4.0	2.0	3.7	29	1.9	17.5	29.2	13	·	·	1	·	1	·	·	18	23	21	7	·	·	5
VI	19.5	2.6	2	2.0	7	1.6	0.5	1.0	9	1.4	0.5	1.0	6	2.7	29.5	3.5	16	2.2	42	26.0	1	·	·	·	7	1	·	8	9	8	3	1	1	·	1
VII	14	2.1	·	·	2.5	2.2	1	2.0	13.5	2.4	4	2.0	9	2.1	2.0	2.8	29	1.6	52	34.6	17	·	·	·	6	·	·	4	11	13	9	1	1	·	2
VIII	18	1.6	0.5	1.0	0.5	1.0	3.5	1.7	9.5	2.8	6.5	2.0	16	2.4	21.5	1.9	17	1.7	51	25.4	15	·	·	·	14	1	·	6	2	11	9	1	2	·	4
IX	5.5	2.6	·	·	4.5	2.5	3.5	2.1	12.5	2.5	12.5	2.5	12	2.2	21.5	2.5	18	2.0	81	37.4	17	·	·	·	3	·	·	4	10	12	9	2	11	·	·
X	9	2.1	3	1.3	8	1.2	3.5	1.1	14.5	2.2	3	3.3	7	1.9	21	2.1	24	1.5	36	18.4	31	·	·	5	·	·	·	5	13	5	2	·	21	·	·
XI	9.5	2.2	4	2.2	6.5	2.0	3.5	2.4	13.5	1.8	1.5	2.0	2	2.0	19.5	2.6	30	1.5	53[2]	15.0	15	·	·	6	·	·	·	19	1	13	10	1	5	1	·
XII	22	2.2	3	1.7	3	1.3	1	1.0	18	4.8	5	4.0	·	·	13	2.1	28	2.1	31	8.8	16	10	15	26	·	1	·	3	17	12	8	·	8	17	·
Rok	16.5	2.8	2.3	1.7	5.0	1.5	2.7	1.7	20.4.5	2.8	6.0.5	3.1	6.3.5	2.2	23.5.5	3.3	266	2.2	648[2]	37.4	17.IX	18	34	106	37	8	1	55	147	146	110	15	58	47	12

Długopole — $H_s = 420m$ — $h_w = 20m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	56	22.9	12	2	7	20	·	–	–	·	18	16	10	1	1	–	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	77	26.4	12	6	13	24	·	–	–	·	25	18	11	2	1	–	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	68	15.2	5	5	13	25	·	–	–	2	18	16	6	3	1	–	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	35	7.3	11	·	·	1	·	–	–	2	18	16	10	·	·	–	·
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	121	34.0	14	·	·	3	·	–	–	·	15	22	15	3	·	·	1
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	43	18.6	11	·	·	1	6	–	–	1	11	10	8	1	·	·	2
VII	9.5	2.6	2.5	1.8	2	2.0	3	4.2	22.5	3.0	9.5	3.3	4	2.0	6	1.7	34	1.7	35	13.3	13	·	·	·	5	·	·	·	11	16	9	1	·	·	5
VIII	7	3.0	2	2.0	1.5	2.0	8	3.2	21	3.0	13	3.0	4.5	2.9	4	3.5	32	2.0	26	6.5	14	·	·	·	8	·	·	·	4	9	7	·	·	·	4
IX	12	2.3	0.5	2.0	·	·	6	3.8	19.5	3.6	6	3.0	2.5	4.0	2.5	3.6	41	1.8	69	29.6	17	·	·	1	3	·	·	5	8	16	11	2	3	·	·
X	16.5	1.8	3	2.0	0.5	1.0	3.5	2.6	18.5	2.3	3	2.0	·	·	1	2.5	47	1.0	48	25.1	31	·	·	7	·	·	·	8	16	7	4	2	8	·	·
XI	16.5	3.6	0.5	3.0	·	·	4	4.5	2.6	6.7	9	3.6	·	·	3	3.0	31	3.2	83	32.2	1	·	3	14	·	5	·	·	22	15	11	1	7	–	·
XII	21.5	4.3	3	3.3	·	·	6.5	3.2	2.3	3.9	5	3.7	2.5	2.2	4.5	3.2	27	2.7	42	13.0	15	13	20	30	·	1	·	1	21	16	10	1	1	–	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	703	34.0	14.V	26	56	126	22	–	–	19	187	177	112	17	22	–	12

Leżajsk $\varphi = 50°15'$ $\lambda = 22°26'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.0	−2.3	8.9	22	−16.5	31	−0.6	1.3	−0.3	0.0	5.2	5.4	5.1	5.2	8.5	7.9	8.2	8.2	0.9	1.5	1.1	1.2	8.0	6.7	6.4	7.0
II	–	–	–	–	0.2	−5.0	4.0	13	−12.5	25	−3.6	−1.3	−2.6	−2.5	4.1	4.8	4.5	4.5	8.5	8.5	8.6	8.5	0.7	0.9	0.7	0.8	9.1	9.5	8.5	9.0
III	–	–	–	–	2.4	−4.8	13.8	5	−15.7	21	−3.4	1.0	−1.7	−1.4	4.4	5.4	4.9	4.9	8.5	8.2	8.7	8.5	0.7	1.5	0.7	1.0	8.0	7.7	7.2	7.6
IV	–	–	–	–	17.3	5.5	26.8	22, 23	−1.1	30	7.6	15.6	10.3	11.0	8.8	9.7	9.5	9.3	8.4	5.7	7.6	7.2	1.8	9.1	3.6	4.8	5.0	5.5	3.8	4.8
V	–	–	–	–	16.8	7.8	24.1	14	−0.8	1	10.1	14.9	11.1	11.8	11.1	11.4	11.5	11.3	8.8	6.7	8.5	8.0	1.5	6.2	2.1	3.3	7.6	8.3	6.8	7.6
VI	–	–	–	–	19.8	10.1	29.7	23	3.4	6	13.4	17.8	14.3	15.0	13.2	12.8	12.9	13.0	8.3	6.2	7.7	7.4	2.9	9.2	4.2	5.4	6.0	7.4	6.3	6.6
VII	–	–	–	–	21.8	11.8	30.9	27	7.1	30	14.4	19.8	15.5	16.3	13.6	13.5	14.1	13.7	8.3	5.9	7.9	7.4	2.9	10.2	3.8	5.6	5.9	6.6	5.8	6.1
VIII	–	–	–	–	24.1	12.8	31.7	13	7.0	1	15.2	22.1	17.4	18.0	15.1	15.7	16.0	15.6	8.6	6.0	7.9	7.5	2.4	11.6	4.3	6.1	4.9	6.3	3.7	5.0
IX	–	–	–	–	18.8	8.4	28.3	5	2.1	15	10.0	17.0	12.2	12.8	10.9	11.7	12.0	11.5	8.8	6.2	8.4	7.8	1.8	8.4	2.6	4.3	5.2	6.2	5.3	5.6
X	–	–	–	–	13.9	2.8	19.9	2	−4.7	17	4.0	12.4	6.8	7.5	8.0	10.1	8.7	8.9	9.5	6.9	8.6	8.3	0.5	4.7	1.4	2.2	6.1	4.6	2.6	4.4
XI	–	–	–	–	7.6	2.5	17.2	1	−1.9	18	3.5	6.0	4.3	4.5	7.6	8.5	7.9	8.0	9.6	9.0	9.4	9.3	0.4	1.2	0.5	0.7	9.2	8.6	7.7	8.5
XII	–	–	–	–	−1.3	−7.1	6.0	13	−17.2	27	−5.2	−3.2	−4.9	−4.6	3.7	4.2	3.8	3.9	8.4	8.2	8.2	8.3	0.7	0.9	0.8	0.8	8.0	8.2	7.4	7.9
Rok	–	–	–	–	12.0	3.5	31.7	13.VIII	−17.2	27. XII	5.4	10.3	6.9	7.4	8.8	9.4	9.2	9.1	8.7	7.1	8.3	8.0	1.4	5.4	2.2	3.0	6.9	7.1	6.0	6.7

Katowice $\varphi = 50°14'$ $\lambda = 19°02'$

I	983.2	1000.7	959.9	1018.8	2.3	−3.4	8.6	22	−17.7	31	−1.4	1.5	−0.7	−0.3	5.1	5.2	5.0	5.1	8.8	7.5	8.3	8.2	0.7	1.8	1.1	1.2	7.5	7.7	7.6	7.6
II	981.9	998.6	953.1	1017.6	0.4	−5.1	6.9	12	−14.4	3	−3.5	−1.2	−2.0	−2.2	4.2	4.5	4.6	4.4	8.6	7.8	8.6	8.3	0.7	1.2	0.8	0.9	9.4	8.6	8.5	8.8
III	976.3	992.9	959.3	1011.7	2.7	−4.8	14.7	31	−11.0	21	−3.5	1.4	−1.3	−1.2	4.4	4.9	4.9	4.7	8.9	7.0	8.4	8.1	0.5	2.2	1.0	1.2	7.8	8.2	6.6	7.5
IV	980.3	992.1	954.3	1014.4	15.2	4.9	26.6	23	0.1	2, 3	7.8	13.3	9.3	9.9	8.6	8.6	8.7	8.6	8.0	6.0	7.4	7.1	2.4	8.5	3.7	4.9	6.6	7.5	6.0	6.7
V	980.0	985.9	966.2	1014.0	15.1	6.2	22.0	19	−3.4	3	9.3	13.3	10.3	10.8	10.2	9.9	10.7	10.3	8.6	6.5	8.4	7.8	1.8	5.9	2.2	3.3	7.8	8.4	7.7	8.0
VI	985.1	994.0	975.8	1018.9	19.1	9.0	29.2	16, 23	0.7	2	12.7	17.4	13.4	14.2	12.0	11.2	12.0	11.7	7.9	5.5	7.6	7.0	3.3	10.2	4.1	5.9	6.1	7.5	6.6	6.7
VII	981.9	991.5	969.9	1015.3	21.0	10.5	30.1	26	5.3	5	14.2	19.2	14.9	15.8	13.6	13.3	13.7	13.5	8.3	6.0	8.0	7.4	2.8	9.6	3.6	5.3	6.1	7.3	5.7	6.4
VIII	983.4	990.3	971.8	1016.8	23.2	11.7	30.9	7	5.7	31	15.2	21.7	16.0	17.2	14.8	14.4	15.0	14.7	8.4	5.6	8.2	7.4	2.8	12.3	3.6	6.2	6.5	6.5	5.2	6.1
IX	983.5	994.4	970.1	1017.6	17.9	6.8	28.4	4	1.7	15, 25	9.8	16.1	11.2	12.1	11.0	11.5	11.4	11.3	9.0	6.4	8.5	8.0	1.5	7.5	2.4	3.8	7.3	6.4	3.8	5.8
X	988.2	1000.5	974.6	1022.9	13.7	3.9	22.3	4	−3.3	22	5.5	12.6	7.7	8.4	8.9	10.2	9.8	9.6	9.6	7.0	9.1	8.6	0.4	5.0	0.9	2.1	7.9	4.7	4.7	5.8
XI	982.1	997.1	966.6	1017.1	6.6	1.6	18.0	7	−2.9	18	2.8	5.8	3.8	4.0	7.2	7.7	7.6	7.5	9.4	8.2	9.3	9.0	0.5	2.2	0.6	1.1	8.1	8.2	8.6	8.3
XII	981.6	1008.9	940.8	1017.6	−1.8	−7.0	7.9	13	−17.9	29	−5.5	−3.0	−4.5	−4.4	3.8	4.2	4.0	4.0	8.7	8.3	8.6	8.5	0.6	0.9	0.6	0.7	7.3	7.8	7.5	7.5
Rok	982.3	1008.9	940.8	1016.9	11.3	2.9	30.9	7.VIII	−17.9	29. XII	5.3	9.8	6.5	7.0	8.6	8.8	9.0	8.8	8.7	6.8	8.4	8.0	1.5	5.6	2.0	3.0	7.4	7.4	6.5	7.1

Kolbuszowa $\varphi = 50°14$ $\lambda = 21°47'$

I	–	–	–	–	2.1	−2.6	8.2	20	−16.9	31	−1.1	1.1	−0.9	−0.4	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.2	7.3	7.4
II	–	–	–	–	0.0	−5.1	4.0	13	−12.9	25	−3.7	−1.4	−2.4	−2.5	–	–	–	–	–	–	–	–	–	–	–	–	9.7	9.2	9.2	9.4
III	–	–	–	–	2.1	−5.6	13.5	31	−19.0	20	−3.8	1.0	−2.2	−1.8	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.0	7.5	7.8
IV	–	–	–	–	16.7	4.9	27.3	23	−0.8	30	8.1	15.5	9.3	10.6	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.1	6.0	6.2
V	–	–	–	–	16.2	6.8	23.7	8	−1.2	1	9.7	14.4	10.2	11.1	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.5	6.8	7.9
VI	–	–	–	–	19.0	8.7	28.8	23	2.6	9	13.1	17.0	12.9	14.0	–	–	–	–	–	–	–	–	–	–	–	–	6.7	8.2	6.7	7.2
VII	–	–	–	–	21.7	10.2	29.9	27	4.1	30	14.3	20.0	14.5	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.1	6.3	6.6
VIII	–	–	–	–	23.6	11.3	31.2	13	3.6	29	15.4	22.1	16.0	17.4	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.1	5.1	6.2
IX	–	–	–	–	18.3	7.5	27.6	5	−0.5	15	10.0	16.6	11.6	12.4	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.9	6.0	6.3
X	–	–	–	–	13.4	1.2	19.4	2	−6.5	16	3.2	12.1	5.0	6.3	–	–	–	–	–	–	–	–	–	–	–	–	7.3	5.7	3.2	5.4
XI	–	–	–	–	7.5	2.1	15.7	4	−2.0	18	3.4	6.5	4.0	4.5	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.0	8.4	8.4
XII	–	–	–	–	−1.8	−8.0	5.0	14	−19.2	23	−5.2	−3.4	−5.0	−4.6	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.3	7.8	8.0
Rok	–	–	–	–	11.6	2.6	31.2	13.VIII	−19.2	23.XII	5.3	10.1	6.1	6.9	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.5	6.7	7.2

Głubczyce $\varphi = 50°12'$ $\lambda = 17°49'$

I	–	–	–	–	2.7	−2.7	10.0	20	−16.3	31	−1.1	1.5	−0.6	−0.2	5.5	5.9	5.6	5.7	9.3	8.5	9.2	9.0	0.4	1.1	0.5	0.7	–	–	–	–
II	–	–	–	–	1.2	−5.3	6.9	13	−15.1	3	−3.3	−0.4	−2.0	−1.9	4.6	5.0	5.0	4.9	9.2	8.2	9.0	8.8	0.4	1.1	0.5	0.7	–	–	–	–
III	–	–	–	–	3.2	−3.2	15.7	31	−8.6	25	−2.4	1.8	−0.5	−0.4	4.8	5.5	5.4	5.2	9.1	7.6	8.7	8.5	0.5	1.7	0.8	1.0	–	–	–	–
IV	–	–	–	–	15.6	5.2	27.1	23, 24	1.2	2, 3	7.6	14.2	9.1	10.0	8.6	8.7	9.0	8.8	8.2	5.8	7.8	7.3	2.3	9.0	3.2	4.8	–	–	–	–
V	–	–	–	–	16.2	6.4	22.5	19	−1.0	1	9.3	13.6	10.1	10.8	10.3	10.4	10.8	10.5	8.6	6.6	8.5	7.9	1.7	5.8	1.9	3.1	–	–	–	–
VI	–	–	–	–	20.1	9.0	30.9	23	1.3	2	13.0	18.7	13.4	14.6	12.2	12.0	12.6	12.3	7.8	5.4	8.1	7.1	3.5	11.0	3.2	5.9	–	–	–	–
VII	–	–	–	–	21.6	10.1	30.0	26	4.8	9	14.2	19.8	14.6	15.8	13.4	13.6	13.9	13.6	8.2	5.9	8.3	7.5	3.0	10.1	3.1	5.4	–	–	–	–
VIII	–	–	–	–	24.3	11.9	31.0	7, 13	6.9	31	15.0	23.0	15.8	17.4	14.4	15.7	15.1	15.1	8.4	5.5	8.3	7.4	2.8	13.0	3.1	6.3	–	–	–	–
IX	–	–	–	–	18.4	7.2	29.5	4	0.7	27	9.8	16.7	10.8	12.0	10.7	11.6	11.1	11.1	8.7	6.2	8.5	7.8	1.9	8.3	2.3	4.2	–	–	–	–
X	–	–	–	–	13.9	4.0	23.9	4	−2.4	23	5.6	12.8	6.9	8.0	8.8	10.5	9.4	9.6	9.4	7.2	9.2	8.6	0.6	5.1	0.8	2.2	–	–	–	–
XI	–	–	–	–	6.6	1.9	18.0	7	−3.2	28	2.7	5.6	3.6	3.9	7.0	7.7	7.4	7.4	9.3	8.3	9.2	8.9	0.5	1.9	0.7	1.0	–	–	–	–
XII	–	–	–	–	−1.4	−6.8	5.7	13	−17.8	22	−5.4	−2.6	−4.7	−4.4	3.9	4.3	4.1	4.1	9.0	8.0	8.9	8.6	0.4	1.1	0.5	0.7	–	–	–	–
Rok	–	–	–	–	11.9	3.1	31.0	7.13. VIII	−17.8	22. XII	5.4	10.4	6.4	7.2	8.7	9.2	9.1	9.0	8.8	6.9	8.6	8.1	1.5	5.8	1.7	3.0	–	–	–	–

Leżajsk $H_s = 190\,m$ $h_w = 15{,}7\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU nD, vnD: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n) Temperatura T: Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v: v≥10	v>15	◔	●	Opad R: R≥0.1	R≥1.0	R≥10.0	≡	⊞	R/R
I	2	5.0	5.5	3.1	0.5	4.0	·	·	20	4.7	38.5	5.1	24	3.9	0.5	6.0	2	4.5	33	7.7	25	2	5	19	·	3	·	3	14	16	10	·	·	18	·
II	6.5	2.8	1.5	4.0	11.5	3.0	6.5	4.5	4.5	8.2	12.5	9.2	21	6.3	15	5.9	5	5.5	42	10.4	12	1	14	27	·	9	5	·	21	19	9	1	·	28	·
III	5.5	3.8	6	4.2	12	5.1	12	2.3	12	2.9	10.5	5.2	11	5.3	13	4.0	11	3.6	40	10.3	16	4	9	26	·	5	·	3	19	16	9	1	3	28	·
IV	2.5	2.6	6	2.2	11	3.0	13.5	2.9	16	3.0	12	4.7	14	4.2	4	5.5	11	3.1	35	8.2	28	·	·	1	5	2	·	9	4	13	9	·	4	·	·
V	8	1.6	1.5	1.3	3	3.3	2.5	2.0	10.5	2.5	19	3.9	26.5	4.3	8	2.6	14	2.8	94	14.7	20	·	·	2	·	2	1	1	14	23	18	1	3	·	6
VI	7	3.7	1.5	1.7	3	1.3	1	3.0	3.5	2.3	19	4.1	30.5	3.3	16.5	2.5	8	2.9	77	23.2	1, 4	·	·	·	10	·	·	3	11	11	9	2	1	·	3
VII	8	2.1	5.5	1.6	6	1.8	2	1.5	6	2.3	20.5	3.0	25.5	3.5	13.5	2.4	6	2.5	106	32.5	19	·	·	·	6	1	·	4	11	15	14	3	3	·	7
VIII	2	2.0	1	3.0	10	2.3	1	1.0	7	2.5	17	2.3	31	3.5	6	1.8	18	2.2	32	11.2	16	·	·	·	13	·	·	5	5	10	8	1	3	·	4
IX	1	2.0	·	·	8.5	1.6	1.5	1.3	8.5	3.0	26.5	3.0	25.5	3.0	0.5	4.0	18	2.2	59	35.3	5	·	·	·	4	·	·	6	11	12	8	1	3	·	3
X	4.5	1.4	6.5	1.9	6	1.6	10	2.0	3.5	2.1	16	3.2	12.5	2.6	6	2.2	28	1.6	3	1.1	19	·	·	8	·	·	·	7	4	3	1	·	20	·	·
XI	3.5	2.4	4.5	4.7	24	4.7	16.5	3.1	1.5	1.7	14.5	3.6	8	3.7	10.5	2.1	7	3.3	49	12.1	15	·	·	3	·	1	·	·	20	15	10	2	7	1	·
XII	7.5	2.0	9	3.0	5	2.6	6.5	1.8	7.5	6.4	20.5	4.5	18.5	2.7	5.5	2.4	13	2.9	39	12.8	16	10	13	31	·	2	1	1	19	13	5	1	8	17	·
Rok	58	2.6	48.5	2.6	100.5	2.9	73	2.1	100.5	3.5	226.5	4.3	248	3.9	99	3.4	141	3.1	609	35.3	5. IX	17	41	117	38	25	7	42	153	166	110	13	55	92	23

Katowice $H_s = 284\,m$ $H_b = 284{,}1\,m$ $h_w = 20\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	R/R
I	8.5	4.5	3	4.2	2.5	4.8		·	9.5	5.8	38	5.6	23.5	6.0	7	4.9	1	5.4	42	8.1	11	3	5	24	·	6		·	15	17	11	·	1	16	·
II	8	6.2	9	4.2	9	3.3	4.5	3.0	2	2.5	17	6.6	18	6.1	14.5	5.3	2	5.2	35	5.9	12	4	11	27	·	4	2	·	23	21	11	·	4	26	·
III	5.5	5.2	18.5	5.1	10	3.9	5.5	3.4	14.5	2.7	9.5	4.6	11.5	5.2	12	4.3	6	4.0	58	10.7	12	3	9	26	·	1	·	1	18	18	13	1	4	17	·
IV	9	4.7	14.5	3.4	7.5	3.0	3	3.5	11	4.5	13.5	5.2	15	4.6	8.5	4.8	8	3.9	66	19.8	10	·	·	·	5	4	·	4	11	16	13	2	3	·	·
V	6	2.2	7.5	2.7	3	1.7	4.5	2.8	7.5	3.0	13	4.3	26	4.5	20.5	4.5	5	3.6	180	21.0	13	·	·	1	·	2	·	·	14	23	18	9	6	·	2
VI	11	4.1	12	3.3	3.5	2.9	15	2.0	8.5	1.6	5.5	2.8	22.5	3.4	19.5	3.5	6	3.0	62	33.0	1	·	·	·	6	1	·	2	12	11	9	1	1	·	3
VII	8	4.0	8	2.4	6.5	2.5	4	2.2	3.5	3.0	7	3.9	28.5	4.0	18.5	3.1	9	3.1	100	48.9	17	·	·	·	4	·	·	3	10	15	13	2	2	·	6
VIII	2.5	4.2	3	1.8	3	2.8	10	2.8	7	2.1	10.5	5.5	31	3.7	16	3.2	10	3.1	73	19.4	15	·	·	·	9	4	1	2	6	15	11	2	7	·	5
IX	6	3.4	2.5	1.4	8	2.8	5.5	2.8	6.5	3.5	20.5	4.9	29	4.7	5	3.9	7	3.8	56	16.1	17	·	·	·	2	2	·	6	11	14	8	2	5	·	1
X	10	3.0	9.5	2.8	11.5	2.4	11	2.4	7	1.9	16.5	3.5	13.5	3.3	6	3.2	8	2.6	29	12.8	6	·	·	6	·	·	·	4	11	9	3	1	20	·	·
XI	7.5	3.0	6.5	3.7	11.5	3.7	21	3.2	3	2.8	12.5	4.1	11	3.3	8	3.1	9	3.1	92	17.8	15	·	1	10	·	·	·	1	21	19	14	4	13	7	·
XII	4	4.2	14.5	3.9	12	3.8	6.5	2.4	3.5	4.0	26	5.6	11	3.6	9.5	3.4	6	3.9	43	11.2	13	10	16	28	·	4	·	2	18	22	10	1	7	22	·
Rok	86	4.1	108.5	3.2	88	3.1	77	2.5	83.5	3.1	189.5	4.7	240.5	4.4	145	3.9	77	3.7	836	48.9	17. VII	20	42	122	26	28	3	25	170	200	134	25	73	88	17

UWAGA. Kierunki i prędkości wiatru - wg. anemometru.

Kolbuszowa $H_s = 208\,m$ $h_w = 16{,}1\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	R/R
I	3	4.7	4.5	4.3	·	·	2.5	5.0	36.5	5.0	22	3.1	16.5	3.3	3	4.3	5	4.0	32	10.9	25	2	8	20	·	3	·	·	14	14	9	1	·	11	–
II	7.5	3.9	3	2.7	10.5	4.7	7	2.5	8.5	7.2	12.5	7.2	16	6.3	11	8.7	8	5.4	45	9.1	12	2	14	26	·	7	4	·	25	20	12	·	1	28	–
III	6.5	7.1	9	3.6	10	3.6	6	3.3	15	3.8	4	2.1	10.5	5.5	10	3.4	22	3.1	45	11.5	16	6	11	25	·	2	·	2	20	16	9	1	·	23	–
IV	2.5	4.2	7	2.0	10.5	3.7	7	4.7	11.5	5.7	11	3.4	10	3.1	8.5	4.8	22	3.0	19	5.2	28	·	·	1	6	4	·	4	8	10	5	·	1	·	–
V	2	1.7	0.5	3.0	2.5	2.6	4	2.5	8.5	2.7	16.5	3.4	20.5	3.4	10.5	2.3	28	2.1	100	13.5	20	·	·	2	·	2	1	·	15	27	18	2	·	·	–
VI	7	3.3	0.5	2.0	2	3.5	1	1.0	·	·	15	3.0	22.5	2.8	17	4.1	25	2.3	129	39.6	4	·	·	·	8	·	·	1	13	12	10	6	·	·	–
VII	5	3.9	4	2.6	2.5	1.2	1.5	2.0	3	1.6	17.5	2.4	26.5	2.6	7	2.6	26	1.8	73	21.5	18	·	·	·	5	·	·	3	11	18	12	2	1	·	–
VIII	1.5	3.3	1.5	2.0	2.5	3.6	4	3.0	5	4.4	14	2.8	23.5	3.6	3	1.6	38	1.9	37	12.9	16	·	·	·	12	·	·	·	4	10	9	1	1	·	–
IX	3	2.7	4.5	2.2	5	3.1	4.5	1.7	10.5	3.3	17.5	3.0	18.5	2.4	1.5	5.0	25	2.1	58	14.2	5	·	·	1	3	·	·	4	9	13	7	3	3	·	–
X	6.5	3.0	4	3.2	10.5	3.1	·	·	3.5	2.1	6.5	4.6	8	2.8	3	2.8	51	1.4	4	1.7	19	·	·	13	·	·	·	6	7	4	2	·	13	·	–
XI	8	2.8	4.5	5.1	27	5.3	9.5	3.8	4.5	3.2	11	3.0	10.5	2.6	3	2.0	12	3.4	63	15.4	15	·	·	5	·	1	1	·	19	15	13	2	4	2	–
XII	13.5	3.1	7	2.9	4	3.1	1.5	2.3	18.5	5.9	12.5	2.9	12	2.5	5	2.5	19	2.9	50	11.8	14	11	15	30	·	2	1	·	17	19	11	2	2	18	–
Rok	66	3.6	50	3.0	87	3.1	48.5	2.6	125	3.7	160	3.4	195	3.4	82.5	3.7	281	2.8	655	39.6	4. VI	21	48	123	34	21	7	20	162	178	117	20	26	82	–

Głubczyce $H_s = 290\,m$ $h_w = 13\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	R/R
I	12	4.8	·	·	·	·	·	·	15	4.5	24	5.4	11	2.5	4	4.9	27	3.2	37	7.0	29	2	4	20	·	5	·	–	–	13	9	·	1	7	–
II	18.5	4.8	·	·	·	·	·	·	8.5	3.4	6.5	5.5	16	4.4	3.5	7.4	31	2.9	28	4.2	24	7	10	24	·	4	·	–	–	15	11	·	·	25	–
III	17	3.5	2	4.8	3	1.7	0.5	1.0	8.5	1.9	11	2.6	12.5	2.6	6.5	4.8	32	2.0	43	11.3	12	·	9	23	·	2	·	–	–	13	8	1	1	16	–
IV	8.5	3.5	·	·	3	1.3	·	·	15.5	3.9	7.5	4.7	14.5	2.2	3	4.2	38	1.9	30	7.8	4	·	·	·	7	3	·	–	–	15	8	·	2	·	–
V	5	3.0		·	·	·	·	·	15.5	1.9	5.5	2.4	12	2.6	·	·	55	1.0	206	27.0	13	·	·	2		·	·	–	–	24	21	8	·	·	–
VI	8	3.4	·	·	0.5	3.0	1	2.0	9	1.9	5.5	3.2	18.5	2.7	4.5	4.0	43	1.5	41	24.9	1	·	·	·	6	·	·	–	–	11	5	1	·	·	–
VII	1.5	2.3	0.5	1.0	1	1.0	3.5	2.1	8.5	2.6	6	2.9	10.5	2.9	1.5	1.3	60	0.9	56	25.0	17	·	·	·	8	·	·	–	–	14	10	1	·	·	–
VIII	2.5	3.6	1.5	2.7	·	·	1	2.0	9.5	2.7	8.5	3.4	7	2.4	4	2.2	59	1.0	50	12.0	15	·	·	·	14	1	·	–	–	12	11	1	·	·	–
IX	3	3.0	·	·	·	·	·	·	15.5	3.8	9.5	4.1	11	2.4	1	3.0	50	1.5	100	40.6	17	·	·	·	3	1	·	–	–	11	9	3	5	·	–
X	5.5	1.2	0.5	1.0	2	1.5	1.5	1.7	7.5	1.7	·	·	11	2.7	1	3.0	64	0.6	42	17.5	31	·	·	4	·	·	·	–	–	10	4	2	10	·	–
XI	8	1.8	·	·	·	·	2	1.5	11.5	3.2	5.5	2.8	2.5	1.6	2.5	3.2	58	0.9	94	17.3	15	·	2	10	·	·	·	–	–	16	10	3	5	9	–
XII	11.5	2.8	0.5	2.0	·	·	·	·	6.5	7.3	12.5	5.6	3	3.7	4	2.0	55	1.8	23	7.2	31	9	13	28	·	3	·	–	–	14	7	·	1	23	–
Rok	101	3.1	5	1.0	9.5	0.7	9.5	0.9	131	3.2	102	3.6	129.5	2.7	35.5	3.3	572	1.6	750	40.6	17. IX	18	38	111	38	19	·	–	–	168	113	20	25	80	–

Goszyce $\varphi = 50°11'$ $\lambda = 20°08'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.4	-3.2	9.2	22	-15.8	31	-1.2	1.1	-0.4	-0.2	5.1	5.8	5.4	5.4	88	84	87	86	0.7	1.1	0.7	0.8	–	–	–	–
II	–	–	–	–	0.2	-5.0	6.0	12, 13	-12.2	2	-3.7	-1.4	-2.2	-2.4	4.3	4.8	4.7	4.6	88	86	88	87	0.5	0.8	0.7	0.7	9.4	8.3	7.7	8.5
III	–	–	–	–	1.8	-5.0	14.0	31	-13.8	21	-3.8	0.6	-1.6	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.2	7.1	7.1
IV	–	–	–	–	15.6	5.5	25.8	23	0.9	3	8.1	14.1	9.9	10.5	9.0	10.0	10.0	9.7	82	65	81	76	2.2	7.6	2.9	4.2	–	–	–	–
V	–	–	–	–	15.1	6.7	22.7	8	-1.4	1	9.6	13.3	10.5	11.0	10.5	10.2	11.2	10.9	86	72	87	82	1.8	5.2	1.9	3.0	7.4	8.6	6.7	7.6
VI	–	–	–	–	18.7	9.2	28.8	16, 24	2.8	2	12.7	17.1	13.7	14.3	12.4	12.3	12.5	12.4	82	62	78	74	2.9	8.8	3.9	5.7	4.8	6.8	5.2	5.6
VII	–	–	–	–	20.9	10.8	30.1	26	6.1	5	14.1	19.5	15.3	16.0	13.5	14.1	14.5	14.0	83	62	82	76	2.8	9.2	3.1	5.0	5.3	5.7	6.1	5.7
VIII	–	–	–	–	22.8	12.4	31.0	7	6.5	27, 29	14.9	21.3	17.0	17.6	14.8	15.6	15.7	15.4	86	62	80	76	2.4	10.5	3.9	5.6	4.6	5.5	4.0	4.7
IX	–	–	–	–	17.6	7.2	27.7	4	1.4	15	9.4	16.2	12.1	12.4	10.7	11.6	12.0	11.4	89	64	84	79	1.5	7.6	2.5	3.9	5.8	5.9	3.3	5.0
X	–	–	–	–	12.1	3.6	17.9	1	-3.5	16	4.7	11.2	7.3	7.6	8.3	10.0	9.3	9.2	93	75	89	86	0.5	3.5	1.1	1.7	6.7	4.9	4.5	5.4
XI	–	–	–	–	6.5	1.7	16.4	8	-2.3	24	2.6	5.6	3.8	4.0	6.8	7.6	7.4	7.3	90	82	90	87	0.7	2.0	0.8	1.2	7.9	7.9	8.1	8.0
XII	–	–	–	–	-2.0	-7.1	5.3	12	-20.3	29	-5.6	-3.3	-4.6	-4.5	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.3	7.9	7.7
Rok	–	–	–	–	11.0	3.1	31.0	7.VIII	-20.3	29.XII	5.2	9.6	6.7	7.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Horyniec $\varphi = 50°11'$ $\lambda = 23°21'$

I	–	–	–	–	1.9	-4.4	7.7	22	-15.0	31	-1.7	0.9	-1.7	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.1	5.4	6.3
II	–	–	–	–	-0.7	-7.0	3.3	13	-14.9	25	-4.7	-1.6	-3.7	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.8	8.4	8.7
III	–	–	–	–	1.7	-6.4	11.7	5, 6	-20.5	19	-3.8	0.6	-2.8	-2.2	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.3	7.6	7.6
IV	–	–	–	–	16.3	4.2	26.2	22, 24	-2.8	2	8.3	15.1	8.7	10.2	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.6	3.6	4.4
V	–	–	–	–	16.9	6.4	24.7	14, 20	-3.2	4	10.2	15.5	10.2	11.5	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.8	5.6	6.6
VI	–	–	–	–	19.2	8.4	28.9	22	2.6	8	13.4	17.4	12.7	14.0	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.6	5.6	6.0
VII	–	–	–	–	20.8	9.5	29.8	27	4.2	3, 10	14.2	19.3	13.5	15.1	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.9	5.6	5.7
VIII	–	–	–	–	22.9	10.8	29.6	7, 13	3.5	31	15.0	21.6	15.4	16.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.2	3.6	4.7
IX	–	–	–	–	17.9	6.2	27.9	5	-1.0	15	9.6	16.5	10.4	11.7	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.8	4.9	5.4
X	–	–	–	–	13.6	0.6	19.6	4	-6.1	16	3.2	12.7	4.4	6.2	–	–	–	–	–	–	–	–	–	–	–	–	6.0	4.8	2.5	4.4
XI	–	–	–	–	8.0	1.7	19.6	1	-4.2	17	3.6	6.6	4.0	4.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.8	7.3	7.9
XII	–	–	–	–	-2.3	-7.5	4.0	14	-17.7	29	-5.5	-3.2	-5.0	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.4	8.2	8.5
Rok	–	–	–	–	11.4	1.9	29.8	27.VII	-20.5	19. III	5.2	10.1	5.5	6.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.5	5.7	6.3

Trzebinia $\varphi = 50°10'$ $\lambda = 19°28'$

I	–	–	–	–	2.8	-3.1	9.5	22	-16.9	31	-0.7	1.8	-0.8	-0.1	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.5	6.7	6.7
II	–	–	–	–	0.2	-5.1	6.2	12	-13.5	25	-3.6	-1.3	-2.2	-2.3	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.1	8.0	8.4
III	–	–	–	–	2.0	-4.6	14.2	31	-10.1	19	-2.1	1.0	-1.5	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.4	5.8	6.7
IV	–	–	–	–	15.1	6.1	26.0	24	0.5	3	9.2	13.7	9.6	10.5	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.0	4.4	5.4
V	–	–	–	–	14.9	6.8	22.0	8, 19	-1.8	1	9.9	13.0	10.4	10.9	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.1	6.6	6.8
VI	–	–	–	–	18.9	9.2	29.9	16	1.1	2	12.5	17.5	13.1	14.0	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.9	4.9	5.3
VII	–	–	–	–	20.8	11.2	29.9	26	6.7	2	13.9	18.7	15.1	15.7	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.0	5.1	5.0
VIII	–	–	–	–	23.0	12.8	31.4	7	6.6	31	15.4	21.5	16.7	17.6	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.9	4.0	4.7
IX	–	–	–	–	17.8	7.9	28.6	4	2.6	25	10.3	15.9	11.9	12.5	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.4	3.0	4.6
X	–	–	–	–	13.2	4.9	20.2	4	-0.7	16	6.5	12.2	7.6	8.5	–	–	–	–	–	–	–	–	–	–	–	–	5.6	3.7	3.7	4.3
XI	–	–	–	–	6.2	2.3	15.7	7	-2.5	23	3.3	5.1	3.7	4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.8	7.0	7.0
XII	–	–	–	–	-2.4	-7.2	6.5	13	-16.9	22	-5.3	-3.5	-4.8	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.5	6.3	6.7
Rok	–	–	–	–	11.0	3.4	31.4	7.VIII	-16.9	31.I, 22.XII	5.8	9.6	6.6	7.2	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.1	5.5	6.0

Biały Kościół $\varphi = 50°10'$ $\lambda = 19°50'$

I	–	–	–	–	1.5	-3.6	7.6	22	-16.7	31	-1.6	0.6	-1.3	-0.9	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.3	7.5	7.5
II	–	–	–	–	-0.8	-5.9	4.1	12	(-12.9	25	-4.2	-1.8	-2.8	-2.9	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.1	7.1	7.8
III	–	–	–	–	1.5	-5.1	12.2	5	-11.1	27	-3.1	-0.1	-1.8	-1.7	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.2	6.9	7.1
IV	–	–	–	–	14.4	5.9	24.9	24	-0.3	3	8.5	12.8	9.6	10.1	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.5	4.9	5.4
V	–	–	–	–	14.2	6.4	21.9	8	-1.8	1	8.6	12.6	9.6	10.1	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.2	7.1	7.8
VI	–	–	–	–	18.2	9.6	28.0	23	1.4	2	12.6	16.3	12.9	13.7	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.8	5.8	6.3
VII	–	–	–	–	19.7	11.3	29.0	27	6.2	6	14.0	18.7	14.9	15.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.2	6.0	6.1
VIII	–	–	–	–	22.0	13.1	30.0	7	7.1	31	15.4	20.6	16.4	17.2	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.9	5.1	5.6
IX	–	–	–	–	16.9	7.8	26.8	4	3.6	26	10.1	15.2	11.8	12.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.1	4.5	5.9
X	–	–	–	–	12.1	4.9	18.9	11	0.2	16	6.0	11.1	7.5	8.0	–	–	–	–	–	–	–	–	–	–	–	–	6.5	4.9	4.7	5.4
XI	–	–	–	–	5.5	1.3	14.8	7, 8	-3.1	23, 24	2.2	4.4	3.0	3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.3	8.7	8.6
XII	–	–	–	–	-2.5	-7.1	4.9	12	-17.8	22	-5.6	-3.7	-5.0	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.7	7.8	8.1
Rok	–	–	–	–	10.2	3.2	30.0	7.VIII	-17.8	22.XII	5.2	8.9	6.2	6.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.9	6.3	6.8

Goszyce $H_s = 260\ m$ $h_w = 14{,}5\ m$ 1962

MIESIĄC	ROZKŁAD WIATRU (n D, v m/s) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	◔	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	5	5.8	3	4.7	·	·	2.5	1.8	28.5	2.6	19.5	4.3	12	4.8	4.5	5.4	18	3.1	19	3.7	29	2	7	22	·	2	·	–	–	14	8	·	·	7	·
II	2	2.5	13	3.5	4	6.0	1	4.0	9.5	6.5	9	7.7	15.5	8.7	10	7.6	20	5.0	43	5.4	12, 16	4	13	25	·	8	3	·	19	21	13	·	1	25	1
III	9.5	5.1	19.5	3.6	2.5	1.4	4	2.0	7.5	2.7	4.5	4.9	6	5.5	9.5	3.5	30	2.6	46	9.8	15	4	12	26	·	2	·	3	15	14	11	·	·	23	·
IV	6.5	2.0	6.5	4.8	12	3.7	7.5	3.1	8	3.7	7.5	3.6	12	5.7	10	5.5	20	3.2	46	14.6	6	·	·	·	2	2	1	–	–	13	9	2	·	·	1
V	6	1.5	3	2.7	5	3.4	7	2.1	13	2.5	12.5	2.5	15.5	7.5	10	2.7	21	2.8	129	15.0	13	·	·	2	·	2	1	1	17	24	16	5	·	·	5
VI	15.5	2.8	1	2.0	7	2.1	2	2.0	3.5	5.9	11.5	4.1	13.5	4.4	17	5.2	19	3.1	74	31.8	1	·	·	·	6	2	·	5	11	12	8	2	·	·	2
VII	4	3.8	2	3.5	2	3.8	1.5	4.0	8	1.6	16	2.3	22.5	4.1	17	3.1	20	2.6	104	23.9	18	·	·	·	5	·	·	5	10	17	9	6	1	·	8
VIII	3.5	3.7	4.5	2.9	8	2.4	2.5	1.8	14.5	2.7	13	3.3	23	4.1	9	3.9	15	2.8	25	10.7	5	·	·	·	9	·	·	6	4	9	4	1	2	·	1
IX	0.5	7.0	2	2.0	11	2.9	2	1.5	14.5	3.3	10.5	3.6	11.5	4.4	8	4.1	30	2.3	45	19.1	18	·	·	·	1	·	·	8	6	11	5	2	6	·	1
X	2.5	1.0	12.5	2.2	14	2.4	4	2.0	6	2.4	6.5	4.2	6	4.0	3.5	2.4	38	1.6	4	2.2	31	·	·	6	·	·	·	8	9	5	1	·	15	·	·
XI	4.5	2.2	14	3.8	21	3.4	6	2.8	9.5	2.6	7	4.6	4	3.0	2	5.0	22	2.5	77	15.2	15	·	1	7	·	·	·	3	21	15	10	2	10	6	·
XII	5.5	3.8	16	3.1	7.5	3.4	4.5	4.3	13.5	2.7	15	3.6	6	4.3	3	3.3	22	2.6	43	16.1	15	11	16	29	·	·	·	2	18	18	7	1	4	19	·
Rok	65	3.4	97	3.2	94	2.9	44.5	2.6	136	3.3	132.5	4.1	147.5	5.0	103.5	4.3	275	2.8	655	31.8	1 VI	21	49	117	23	18	5	–	–	173	101	21	39	80	19

Horyniec $H_s = 240\ m$ $h_w = 12\ m$ I – VII, $h_w = 15\ m$ VIII – XII

I	1	3.0	2.5	3.4	2.5	3.4	0.5	1.0	16	2.5	12	3.6	26	3.2	1.5	3.0	31	2.1	31	8.0	25	6	8	28	·	·	·	2	9	14	9	·	1	21	–
II	6.5	3.2	2.5	2.2	7	2.3	5	2.4	6	4.8	8.5	8.0	13	5.1	9.5	4.5	26	3.1	37	7.7	12	6	16	28	·	5	4	1	20	20	11	·	1	28	–
III	2.5	2.4	3.5	4.1	15	2.6	6.5	2.5	6	2.3	1.5	3.0	14.5	5.5	5.5	3.7	38	2.1	69	22.6	16	9	11	25	·	2	·	3	20	15	9	2	·	31	–
IV		·	2	3.5	14	2.1	3.5	2.0	12.5	2.7	5.5	2.0	18	2.9	3.5	4.6	31	1.7	26	8.7	6			4	4		·	11	5	9	5	·	1	1	–
V	2	2.0	1	1.0	1.5	2.0	2	2.0	5.5	1.6	8.5	4.7	24	4.0	5.5	2.9	43	1.8	87	14.6	29	·	·	5	·	2	·	1	12	18	13	4	4	·	–
VI	6.5	2.6	1.5	1.7	3.5	2.3	3	1.3	3	1.7	3.5	2.4	24.5	2.5	5.5	2.0	40	1.3	95	17.6	1	·	·	·	7	·		4	10	15	14	4	·	·	–
VII	1.5	2.0	4.5	1.7	2	2.2	1.5	2.6	4	1.6	7.5	2.5	20	2.9	11	3.1	41	1.5	96	31.1	19	·	·	·	4	·	·	4	8	17	12	3	4	·	–
VIII	4.5	1.4	2.5	1.4	2.5	2.0	7	2.4	4.5	2.0	5.5	2.5	20	3.1	5.5	2.5	41	1.4	51	14.7	25		·		10	·	·	4	4	13	8	1	8	·	–
IX	1.5	1.3	2	2.0	4	2.2	4.5	1.8	10.5	3.2	4	2.8	23.5	2.9	2	4.0	38	1.6	48	9.2	5	·	·	1	1	·		5	9	14	10	·	3	·	–
X	3	1.8	5	1.8	6	1.8	4	2.2	2	2.0	3.5	3.1	17	2.9	0.5	2.0	52	1.1	3	1.8	19	·	·	14			·	11	4	3	2	·	10	·	–
XI	·	·	7	2.4	28	2.5	11.5	2.4	1.5	2.0	5.5	2.6	12.5	2.2	3	1.8	21	1.8	43	13.4	16	·	·	6	·	·	·	1	18	14	9	1	5	2	–
XII	4	2.2	13	3.0	3.5	1.3	10	2.7	5	3.4	10.5	3.5	16	2.8	7	2.5	24	2.1	32	8.2	31	10	18	31	·	·	·	1	22	17	8	·	3	18	–
Rok	32	1.8	47	2.4	89.5	2.2	59	2.1	76.5	2.5	76	3.4	229	3.3	60	3.0	426	1.8	618	31.1	19 VII	31	53	142	26	9	4	48	141	169	110	15	40	101	–

Trzebinia $H_s = 320\ m$ $h_w = 14{,}9\ m$

I	9	3.4	·	·	2.5	2.0	0.5	2.0	·	·	9.5	3.5	28.5	3.0	25	2.3	18	2.3	37	7.5	27	2	6	24	·	1	·	–	–	10	10	·	3	17	–
II	5	2.0	6.5	2.1	5.5	2.1	3	1.0	·	·	7	7.7	13.5	8.1	30.5	4.2	13	3.9	41	6.7	19	4	13	25	·	5	4	–	–	13	10	·	7	27	–
III	12	3.9	15.5	2.7	21.5	2.8	4.5	1.9	1	1.0	7.5	2.6	13	4.8	6	7.5	12	3.1	45	16.5	12	1	15	25	·	3	2	–	–	14	8	1	8	19	–
IV	9.5	2.3	8.5	2.7	12	2.4	10.5	1.8	10	1.2	12	3.6	7	3.6	13.5	3.6	7	2.5	78	23.9	6	·	·	·	4	2	·	–	–	13	9	3	1	·	–
V	6.5	1.2	2.5	1.8	10	1.9	5.5	1.9	2.5	1.0	15.5	2.3	18	3.5	21.5	2.5	11	2.1	148	22.6	13	·	·	1	·	2	1	–	–	24	18	6	1	·	–
VI	12.5	1.7	5.5	1.9	6	1.8	2	2.2	2.5	3.0	7	3.2	13	2.7	24.5	3.2	17	2.1	57	23.5	1	·		·	6	2	1	–	–	10	6	2	·	·	–
VII	7.5	2.1	4	1.6	7	1.7	2	1.2	2.5	1.0	12	2.7	33	2.2	17	2.2	8	2.0	170	57.0	17	·	·		5	·	·	–	–	14	13	6	1	·	–
VIII	1.5	1.7	2.5	2.0	9.5	2.7	5	1.8	1	9.0	14	1.9	20	1.9	17.5	2.2	22	1.7	64	11.7	7	·	·		10	·	·	–	–	14	12	2	3	·	–
IX	2	1.0	1.5	1.7	13.5	3.6	3.5	3.1	3.5	1.7	12.5	3.5	15.5	2.3	14	2.6	24	2.1	73	18.3	18	·			4	2	·	–	–	13	10	3	6	·	–
X	4	1.8	5	1.8	21.5	2.3	9.5	2.5	·	·	4.5	2.2	15.5	2.1	11	2.6	22	1.7	21	6.0	28	·	·	2	·	·	·	–	–	8	5	·	9	·	–
XI	3	2.0	8	2.6	28	3.1	10.5	2.2	0.5	2.0	9	2.1	7.5	2.8	4.5	2.4	19	2.1	77	14.5	15	·	2	10	·	1	·	–	–	17	14	2	10	8	–
XII	6	2.2	13.5	2.6	17	3.3	1.5	2.3	0.5	5.0	14	2.7	8.5	1.6	11	1.9	21	2.0	42	11.2	13	11	19	29	·	1	·	–	–	19	10	1	6	25	–
Rok	78.5	2.1	73	2.0	154	2.5	58	2.0	24	2.1	124.5	3.2	193	3.2	196	3.1	194	2.3	853	57.0	17 VII	18	55	116	29	19	8	–	–	169	125	26	55	96	–

Biały Kościół $H_s = 400\ m$ $h_w = 18{,}5\ m$

I	·	·	3	1.7	3	1.0	1	1.0	·	·	23	1.3	41	2.2	12	2.5	10	1.7	50	9.8	28	2	8	26	·	·	·	·	11	14	12	·	·	9²	·
II	11	1.0	·	·	10	1.0	·	·	·	·	4	2.2	44	3.8	10	2.9	5	2.7	79	11.3	17	3	15	27	·	5	3	2	18	18	17	1	1	28	1
III	18	2.2	8	4.2	13	1.2	7	1.0	·	·	5	1.0	30	2.0	8	1.0	4	1.8	86	11.7	13	2	16	27	·	2	1	2	18	16	15	3	1	25	·
IV	5	1.0	5	1.6	8	2.1	17	1.5	6	1.0	9	1.0	27	1.4	8	2.9	5	1.5	74	28.9	6	·	·	1	·	1	·	7	9	15	12	1	·	·	1
V	4	1.0	1	1.0	6	1.3	5	1.0	2	1.0	18.5	1.2	35.5	2.6	9	1.3	12	1.6	144	19.1	13	·	·	2	·	2	·	·	14	27	22	5	3	·	3
VI	3	1.0	8	1.0	10	1.3	4	1.0	4	1.0	9	1.3	25	2.2	22	1.8	5	1.5	76	21.7	1	·	·	·	5	·	·	1	8	11	7	3	·	·	3
VII	6	1.3	·	·	5	1.0	1	2.0	1	1.0	12	1.5	47	1.5	10	1.7	11	1.3	122	31.2	17	·	·	·	4	·		3	11	15	14	4	1	·	6
VIII	2	2.0	·	·	3.5	1.3	0.5	1.0	2	1.5	14	1.5	43.5	1.6	1.5	1.3	26	1.1	42	11.7	5	·	·	·	6	1	1	2	3	13	9	1	6	·	3
IX	·	·	1	2.0	12	1.4	·	·	3	1.0	10	1.5	44	1.7	5	2.0	15	1.4	60	19.1	18	·	·	·	1	·	·	6	9	11	8	2	5	·	1
X	2	1.0	6	1.2	25	1.1	4	1.0	4	1.0	10.5	1.0	22	1.5	2.5	1.0	17	1.0	19	12.4	6	·	·	·	·	·	·	8	10	9	4	1	13	·	·
XI	9	1.0	7	1.6	36	1.3	1	1.0	·	·	9	1.1	11	2.1	6	1.3	11	1.2	69	15.1	15	·	2	13	·	·	·	1	22	16	12	1	13	10	·
XII	11	1.3	6	1.2	9	1.9	3	1.3	2	1.0	11.5	1.2	22.5	2.2	8	1.8	20	1.3	56	14.1	13	11	18	29	·	·	·	1	19	20	10	1	4	20	·
Rok	71	1.1	45	1.3	140.5	1.3	43.5	1.0	24	0.7	135.5	1.3	392.5	2.1	102	1.8	141	1.5	877	31.2	17 VII	18	59	125	16	11	5	33	152	185	142	23	47	92²	18

Garlica Murowana $\varphi = 50°09'$ $\lambda = 19°56'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.4	-3.9	9.3	22	-15.9	31	-1.7	1.3	-0.9	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	75	63	62	67
II	–	–	–	–	0.2	-5.5	6.1	13	-12.5	1, 3	-4.0	-1.7	-2.4	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	96	81	80	86
III	–	–	–	–	1.7	-5.2	13.8	31	-11.3	21	-3.8	0.2	-1.7	-1.8	–	–	–	–	–	–	–	–	–	–	–	–	75	74	62	70
IV	–	–	–	–	15.2	5.4	25.4	24	-0.3	3	7.3	13.5	9.7	10.0	–	–	–	–	–	–	–	–	–	–	–	–	63	56	44	54
V	–	–	–	–	14.9	6.5	22.3	19	-0.8	1	8.9	13.0	10.1	10.5	–	–	–	–	–	–	–	–	–	–	–	–	84	81	64	76
VI	–	–	–	–	18.6	8.5	28.9	16	2.6	2	12.5	16.8	12.6	13.6	–	–	–	–	–	–	–	–	–	–	–	–	63	70	58	64
VII	–	–	–	–	20.7	10.1	29.9	26	4.6	5	13.5	19.1	14.6	15.4	–	–	–	–	–	–	–	–	–	–	–	–	66	66	57	63
VIII	–	–	–	–	22.7	11.6	31.0	7	4.7	31	14.5	21.1	15.5	16.6	–	–	–	–	–	–	–	–	–	–	–	–	67	62	34	54
IX	–	–	–	–	17.6	6.8	27.6	4	1.9	15	9.2	15.8	10.9	11.7	–	–	–	–	–	–	–	–	–	–	–	–	64	63	36	54
X	–	–	–	–	12.6	3.7	18.4	1	-2.4	22	4.7	11.3	6.9	7.4	–	–	–	–	–	–	–	–	–	–	–	–	69	52	40	54
XI	–	–	–	–	6.5	1.9	16.2	8	-2.3	24	2.9	5.4	3.7	3.9	–	–	–	–	–	–	–	–	–	–	–	–	85	82	79	82
XII	–	–	–	–	-1.9	-7.2	5.7	12	-17.6	26	-5.6	-3.2	-4.7	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	83	79	73	78
Rok	–	–	–	–	10.9	2.7	31.0	7.VIII	-17.6	26.XII	4.9	9.4	6.2	6.7	–	–	–	–	–	–	–	–	–	–	–	–	74	69	57	67

Lubaczów $\varphi = 50°09'$ $\lambda = 23°08'$

I	–	–	–	–	2.5	-4.1	8.3	22	-14.8	31	-1.7	1.2	-1.6	-0.9	–	–	–	–	–	–	–	–	–	–	–	–	84	74	56	71
II	–	–	–	–	-0.6	-6.3	3.6	13	-13.6	25	-4.4	-1.6	-3.2	-3.1	–	–	–	–	–	–	–	–	–	–	–	–	94	91	87	91
III	–	–	–	–	1.9	-6.2	13.2	31	-20.4	21	-4.2	0.7	-2.7	-2.2	–	–	–	–	–	–	–	–	–	–	–	–	86	81	72	80
IV	–	–	–	–	16.7	4.3	26.3	22	-2.6	30	7.0	15.2	9.1	10.1	–	–	–	–	–	–	–	–	–	–	–	–	67	65	30	54
V	–	–	–	–	17.1	6.7	24.8	14	-2.6	2	10.0	15.5	10.9	11.8	–	–	–	–	–	–	–	–	–	–	–	–	80	80	75	78
VI	–	–	–	–	19.6	8.9	28.3	16	3.2	2, 6	13.2	17.7	13.7	14.6	–	–	–	–	–	–	–	–	–	–	–	–	68	80	85	78
VII	–	–	–	–	21.0	10.1	30.4	27	5.4	3, 30	13.9	19.7	14.4	15.6	–	–	–	–	–	–	–	–	–	–	–	–	67	74	68	70
VIII	–	–	–	–	23.4	11.2	30.7	13	4.4	29	14.8	22.2	16.0	17.2	–	–	–	–	–	–	–	–	–	–	–	–	64	64	35	54
IX	–	–	–	–	18.5	6.6	28.0	5	-0.7	15	9.1	17.0	11.2	12.1	–	–	–	–	–	–	–	–	–	–	–	–	62	73	49	61
X	–	–	–	–	14.1	0.2	19.7	2, 4	-6.7	17	2.4	13.3	4.7	6.3	–	–	–	–	–	–	–	–	–	–	–	–	76	64	33	58
XI	–	–	–	–	7.8	2.0	18.2	1	-3.5	17	4.0	6.7	4.2	4.8	–	–	–	–	–	–	–	–	–	–	–	–	92	85	85	87
XII	–	–	–	–	-1.7	-7.7	4.3	13	-17.5	26	-5.4	-2.8	-4.9	-4.5	–	–	–	–	–	–	–	–	–	–	–	–	90	89	84	88
Rok	–	–	–	–	11.7	2.1	30.7	13.VIII	-20.4	21.III	4.9	10.4	6.0	6.8	–	–	–	–	–	–	–	–	–	–	–	–	78	77	63	73

Tychy $\varphi = 50°08'$ $\lambda = 18°59'$

I	–	–	–	–	2.7	-3.5	8.7	22	-18.1	31	-1.3	1.9	-0.5	-0.1	–	–	–	–	–	–	–	–	–	–	–	–	86	69	85	80
II	–	–	–	–	0.8	-5.4	7.6	12, 13	-13.8	3	-3.3	-0.6	-1.9	-1.9	–	–	–	–	–	–	–	–	–	–	–	–	98	86	90	91
III	–	–	–	–	2.9	-4.6	14.8	31	-10.1	25	-3.3	1.7	-1.1	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	75	81	65	74
IV	–	–	–	–	15.5	5.1	27.0	24	0.1	3	7.2	13.9	9.8	10.2	–	–	–	–	–	–	–	–	–	–	–	–	65	73	59	66
V	–	–	–	–	15.3	6.3	22.7	19	-1.9	1	8.8	13.7	10.9	11.1	–	–	–	–	–	–	–	–	–	–	–	–	80	82	84	82
VI	–	–	–	–	19.6	9.0	29.5	23	1.3	2	12.5	17.8	14.1	14.6	–	–	–	–	–	–	–	–	–	–	–	–	54	79	52	62
VII	–	–	–	–	20.8	10.5	30.5	26	5.8	5	13.7	19.4	15.2	15.9	–	–	–	–	–	–	–	–	–	–	–	–	61	72	58	64
VIII	–	–	–	–	23.4	11.7	32.0	7	5.9	29	14.7	22.3	16.7	17.6	–	–	–	–	–	–	–	–	–	–	–	–	57	61	49	56
IX	–	–	–	–	18.1	6.7	29.4	4	1.1	25	9.1	16.4	11.5	12.1	–	–	–	–	–	–	–	–	–	–	–	–	69	67	36	56
X	–	–	–	–	13.6	3.8	21.8	1	-3.5	23	5.0	12.5	7.5	8.1	–	–	–	–	–	–	–	–	–	–	–	–	84	54	52	63
XI	–	–	–	–	6.5	1.8	17.1	8	-2.0	23, 24	2.9	5.7	3.7	4.0	–	–	–	–	–	–	–	–	–	–	–	–	87	80	83	83
XII	–	–	–	–	-1.7	-6.9	8.2	13	-18.2	29	-5.1	-2.9	-4.3	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	90	75	85	83
Rok	–	–	–	–	11.3	2.9	32.0	7.VIII	-18.2	29.XII	5.1	10.2	6.8	7.2	–	–	–	–	–	–	–	–	–	–	–	–	76	73	66	72

Rybnik $\varphi = 50°06'$ $\lambda = 18°33'$

I	–	–	–	–	2.6	-1.9	7.9	22	-17.1	31	-0.5	1.9	0.2	0.4	–	–	–	–	–	–	–	–	–	–	–	–	82	81	85	83
II	–	–	–	–	1.0	-4.4	7.5	12, 13	-14.2	3	-2.8	0.0	-1.3	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	96	88	88	91
III	–	–	–	–	3.6	-3.5	15.0	31	-10.1	25	-2.4	2.3	0.1	0.0	–	–	–	–	–	–	–	–	–	–	–	–	86	82	69	79
IV	–	–	–	–	15.7	6.2	27.9	23	1.7	3, 6	8.5	14.5	10.2	10.8	–	–	–	–	–	–	–	–	–	–	–	–	68	71	63	67
V	–	–	–	–	15.6	7.3	22.9	19	-1.0	1	9.6	13.8	11.1	11.4	–	–	–	–	–	–	–	–	–	–	–	–	83	79	83	82
VI	–	–	–	–	19.9	10.1	29.9	16	1.2	2	12.7	18.5	14.7	15.2	–	–	–	–	–	–	–	–	–	–	–	–	65	68	73	69
VII	–	–	–	–	21.5	11.5	30.1	26	6.7	30	14.2	19.9	16.3	16.7	–	–	–	–	–	–	–	–	–	–	–	–	67	69	72	69
VIII	–	–	–	–	23.9	12.9	31.1	7	7.0	29, 30	15.5	22.6	17.6	18.3	–	–	–	–	–	–	–	–	–	–	–	–	60	61	68	63
IX	–	–	–	–	18.5	8.0	29.1	4	1.8	25	10.4	16.8	12.6	13.1	–	–	–	–	–	–	–	–	–	–	–	–	72	64	53	63
X	–	–	–	–	13.9	4.9	23.5	4	-2.1	22	6.2	13.1	7.9	8.8	–	–	–	–	–	–	–	–	–	–	–	–	87	60	64	70
XI	–	–	–	–	7.0	2.1	18.1	8	-1.9	21, 24	3.3	6.0	4.3	4.5	–	–	–	–	–	–	–	–	–	–	–	–	89	86	87	87
XII	–	–	–	–	-1.5	-6.0	7.5	13	-15.9	29	-4.5	-2.5	-4.0	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	92	85	75	84
Rok	–	–	–	–	11.8	3.9	31.1	7.VIII	-17.1	31.I	5.8	10.6	7.5	7.8	–	–	–	–	–	–	–	–	–	–	–	–	79	74	73	75

Garlica Murowana — $H_s = 270\,m$ — $h_w = 15{,}9\,m$ — 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min<-10°	Max<0°	Min<0°	Max≥25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	R
I	3	6.5	8	4.9	2.5	2.6	2.5	1.6	1.5	1.3	10.5	2.6	32.5	4.0	5.5	4.5	27	2.7	24?	4.0	11	3	8	26	·	-	·	3	12	12	8	·	1	17	·
II	4.5	4.0	6.5	4.2	12	3.7	5	4.2	2	12.0	5	6.9	25	4.4	6	5.9	18	3.8	24?	5.0	5	4	13	25	·	2	·	·	20	15	8	·	1	27	1
III	12.5	3.0	16	2.6	11	3.1	·	·	·	·	4	1.8	8.5	5.6	9	6.8	32	2.5	28	8.2	5	3	15	26	·	3	·	4	14	16	8	·	·	22	·
IV	10	4.0	7	2.6	5	1.7	8.5	2.5	2.5	2.4	7	3.4	16.5	2.7	10.5	3.6	23	2.3	72	30.2	6	·	·	1	2	·	·	6	9	14	10	1	·	·	2
V	6.5	1.1	3	2.0	5	1.9	3.5	2.4	2.5	3.2	7	2.6	25	3.8	11.5	2.5	29	1.9	126	17.3	13	·	·	1	·	·	·	1	14	24	19	2	1	·	3
VI	10.5	2.9	8	3.1	2.5	2.8	2.5	1.4	1.5	1.3	7	1.6	14	3.0	9	4.7	35	1.8	64	26.9	1	·	·	·	6	·	·	5	12	11	7	2	·	·	1
VII	9	1.8	2.5	1.2	5.5	1.5	3.5	2.4	3	1.8	8.5	1.8	18.5	2.4	11.5	2.1	31	1.4	139	38.1	22	·	·	·	4	·	·	3	10	15	10	5	·	·	7
VIII	6.5	2.0	3	1.8	2.5	1.4	1.5	1.7	1	2.0	6.5	2.3	25	2.7	5	4.4	42	1.4	41	20.0	5	·	·	·	9	·	·	1	3	12	7	1	5	·	2
IX	4	1.4	4.5	2.9	7	2.9	0.5	4.0	1.5	3.3	11.5	2.5	23	3.1	7	5.0	31	2.0	57	18.8	17	·	·	·	3	·	·	6	9	12	8	2	5	·	1
X	3	2.0	15	2.2	19.5	2.5	4	2.2	·	·	4.5	2.0	8	3.6	7	3.2	32	1.7	7	2.6	31	·	·	8	·	·	·	7	8	7	3	·	13	·	·
XI	6	2.2	20	2.5	21.5	3.0	6.5	3.3	·	·	5.5	3.7	11.5	3.0	2	3.2	17	2.3	72	15.9	15	·	1	10	·	·	·	2	20	17	13	1	12	5	·
XII	9.5	2.2	14.5	3.2	13.5	2.3	2	5.5	0.5	3.0	13.5	2.4	16.5	2.8	4	3.5	19	2.2	38	10.8	13	11	15	30	·	·	·	1	16	14	7	1	3	19	·
Rok	85	2.8	108	2.8	107.5	2.4	40	2.6	16	2.5	90.5	2.8	224	3.4	88	4.1	336	2.2	692?	38.1	22. VII	21	52	127	24	5	·	39	147	169	108	15	41	90	17

Lubaczów — $H_s = 214\,m$ — $h_w = 16\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min<-10°	Max<0°	Min<0°	Max≥25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	R
I	·	·	5	3.4	3	4.0	3	1.7	12	2.3	25	1.8	31	2.4	9	2.8	5	2.2	29	9.3	25	4	6	30	·	·	·	·	13	15	6	·	·	16	–
II	8.5	2.4	3	1.0	9.5	2.5	10.5	1.8	4	2.3	4	7.0	20	5.9	18.5	5.9	6	4.0	61	10.2	12	5	15	28	·	6	1	·	22	20	12	3	·	28	–
III	7.5	3.3	8	2.1	16	2.3	16	3.3	9.5	2.1	3.5	2.0	12	5.0	15.5	2.5	5	2.8	68	23.5	16	7	12	26	·	2	·	·	21	18	12	1	·	28	–
IV	2	1.0	6.5	2.3	11.5	2.0	13	2.7	10.5	2.5	6.5	2.1	19.5	2.1	10.5	3.1	10	2.1	32	14.0	6	·	·	4	5	·	·	3	5	10	5	1	1	·	–
V	11	1.5	1	1.0	3	1.0	3	3.3	8	1.4	8	2.7	39.5	2.5	14.5	1.9	5	2.0	97	15.4	20	·	·	4	·	1	·	·	17	17	13	2	2	·	–
VI	11.5	2.4	·	·	4	1.8	3	2.0	5	1.2	8	1.8	16.5	2.6	32	2.1	10	1.9	108	34.7	1	·	·	·	7	·	·		14	15	12	3	·	·	–
VII	5	1.6	7	1.4	2	1.5	4	1.0	7	1.3	7	2.0	29	2.5	15	2.4	17	1.7	89	21.3	19	·	·	·	4	·	·	·	15	13	13	4	2	·	–
VIII	6.5	1.4	0.5	2.0	2.5	1.2	6	1.6	4.5	1.8	6.5	1.8	25.5	2.2	19	2.4	22	1.5	52	12.0	25	·	·	·	11	·	·	2	2	14	9	1	8	·	–
IX	2	2.0	·	·	7	1.7	9	2.0	6	2.5	16	2.2	32.5	2.1	7.5	3.3	10	2.0	41	10.2	8	·	·	1	2	·	·	1	9	13	8	1	2	·	–
X	3	1.3	6	2.0	5	1.8	14	1.6	8	1.9	4	4.2	14.5	2.8	8.5	2.6	30	1.5	3	1.7	31	·	·	15	·	·	·	1	6	3	·	·	10	·	–
XI	2	1.5	7	1.7	6.5	3.0	43.5	3.3	2	2.0	5.5	1.6	14.5	2.3	6	1.9	3	2.6	58	12.7	25	·	·	4	·	·	·	·	23	14	12	2	3	·	–
XII	9	1.7	12	2.2	8	1.5	7	1.1	8	2.6	12	1.9	20	1.7	9	2.0	8	1.7	36	12.7	31	10	13	30	·	·	·	·	23	13	5	2	1	22	–
Rok	68	1.7	56	1.6	78	2.0	132	2.1	84.5	2.0	106	2.6	274.5	2.8	165	2.7	131	2.2	674	34.7	1. VI	26	46	142	29	9	1	7	170	165	107	20	29	94	–

Tychy — $H_s = 280\,m$ — $h_w = 15{,}5\,m$ I – IX; $16{,}3\,m$ X – XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min<-10°	Max<0°	Min<0°	Max≥25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	R
I	4	3.5	4	2.8	1	2.0	1	2.0	3.5	3.4	19.5	3.4	33	3.5	10	3.8	17	2.8	51	10.2	11	3	5	23	·	·	·	·	15	12	11	1	–	16	–
II	6.5	3.1	3.5	2.6	11.5	2.7	2	2.0	1	3.0	10.5	4.5	19	4.3	15	4.5	15	3.1	61	13.7	13	4	11	27	·	2	·	·	22	15	14	1	–	25	–
III	9	5.7	7	5.1	12	3.4	3	4.0	4.5	2.2	8	3.2	11.5	2.7	6	4.8	32	2.5	73	13.8	12	1	7	26	·	1	1	1	18	15	11	3	–	11	–
IV	5.5	2.2	3.5	3.4	0.5	3.0	5.5	4.3	7.5	2.9	7	2.9	9	3.2	16.5	4.3	35	2.0	102	27.1	10	·	·	·	7	1	·	4	13	14	10	5	–	·	–
V	1	3.0	2	2.0	6	2.5	3	3.3	1.5	2.0	7	2.6	18.5	3.2	17	3.8	37	1.9	220	33.0	14	·	·	2	·	·	·	·	18	21	20	7	–	·	–
VI	6.5	3.7	6	2.5	2	2.0	1	3.0	·	·	2	2.0	14	3.4	20.5	3.7	38	1.9	83	41.1	1	·	·	·	6	·	·	4	9	10	9	2	–	·	–
VII	4	2.2	1	3.0	2	2.5	·	·	2	2.0	9	2.8	23.5	2.6	13.5	3.0	38	1.6	158	69.3	17	·	·	·	5	·	·	2	10	15	13	5	–	·	–
VIII	2.5	2.4	2	2.0	3	2.3	4	3.5	·	·	5	4.4	13.5	3.1	18	3.2	45	1.6	65	14.8	15	·	·	·	11	·	·	4	9	13	12	2	–	·	–
IX	1.5	2.0	2	2.0	7	3.1	·	·	2	2.5	9.5	3.3	17.5	2.7	12.5	3.4	38	1.7	100	29.1	17	·	·	·	4	·	·	5	10	13	11	3	–	·	–
X	5	2.0	3	2.7	11.5	2.8	4.5	2.7	·	·	6	3.3	5	3.4	10	2.4	48	1.3	36	13.4	28	·	·	9	·	·	·	3	11	5	4	3	–	·	–
XI	1	2.0	4	2.5	13	3.2	14	2.8	·	·	7.5	3.5	9.5	3.1	5	2.2	36	1.8	121	24.8	15	·	·	7	·	·	·	·	19	14	13	5	–	3	–
XII	6	2.3	9.5	2.7	3.5	2.9	4.5	2.4	3	2.3	16.5	3.5	13	2.9	4	3.0	33	1.9	52	10.2	13	10	16	28	·	·	·	1	22	14	11	1	–	20	–
Rok	52.5	2.8	47.5	2.8	73	2.7	42.5	2.5	25	1.7	107.5	3.3	187	3.2	148	3.5	412	2.0	1122	69.3	17. VII	18	39	122	33	4	1	24	176	161	139	38	–	75	–

Rybnik — $H_s = 243\,m$ — $h_w = 11{,}5\,m$ I – VII; $17{,}2\,m$ VIII – XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min<-10°	Max<0°	Min<0°	Max≥25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	R
I	6	2.7	·	·	1	1.0	·	·	4.5	2.0	51	3.2	9.5	3.0	6	1.5	15	2.4	40	8.7	11	1	5	18	·	3	·	·	16	14	10	·	·	14	·
II	6	2.3	6.5	1.7	1	1.0	·	·	2.5	2.4	18.5	5.6	20	3.2	8.5	2.7	21	2.7	46	7.1	17	5	10	23	·	2	2	·	23	16	15	·	1	21	·
III	10.5	4.5	4.5	2.9	6	2.3	3	1.7	1	1.0	15	3.5	8	2.4	17	3.3	28	2.2	55	13.6	31	1	7	25	·	4	·	·	15	14	9	1	1	11	1
IV	5	1.2	3	3.3	2.5	2.4	1.5	1.3	9.5	2.5	18.5	3.6	15.5	2.7	7.5	1.2	27	1.8	55	10.6	13	·	·	·	7	2	1	3	12	12	11	1	1	·	·
V	2	1.5	3	1.3	2	1.5	·	·	3	2.0	37	2.5	15	2.7	8	2.4	23	1.8	207	43.2	13	·	·	1	·	·	·	·	13	21	16	9	1	·	3
VI	5	3.8	2	1.5	1	2.0	·	·	·	·	23	2.3	19	1.9	16	2.9	24	1.8	52	31.5	1	·	·	·	6	·	·	1	10	8	5	1	·	·	1
VII	1	1.0	4	2.0	0.5	2.0	4.5	1.8	2	1.0	22.5	2.4	18.5	2.0	10	2.2	30	1.4	76	58.4	17	·	·	·	8	·	·	2	13	8	6	1	·	·	2
VIII	2	1.5	2	4.0	2	1.0	7	2.0	6	1.5	20.5	3.0	10.5	2.1	12	2.0	31	1.5	100	34.2	5	·	·	·	13	·	·	1	9	11	10	3	1	·	4
IX	3	1.0	4	1.2	9	1.6	1	1.0	6	2.2	24	3.1	18.5	1.7	12.5	3.1	12	2.0	68	24.1	17	·	·	·	4	1	·	3	12	9	7	2	6	·	·
X	6	1.2	4	1.5	17	1.4	4	1.0	3	3.3	16	1.6	3	1.3	7	1.3	33	1.0	31	13.1	31	·	·	2	·	·	·	2	13	7	6	1	15	·	·
XI	4	1.8	9	1.6	13	1.2	12.5	1.6	3.5	1.6	14	3.3	7	1.9	6	1.3	21	1.4	121	24.2	15	·	1	10	·	2	·	1	23	16	13	4	–	3	·
XII	10	2.0	7	2.6	12.5	1.2	1.5	2.3	10	4.4	26	6.2	2	2.0	8	1.5	16	3.0	47	13.8	13	7	17	26	·	5	4	·	22	14	10	1	–	21	·
Rok	60.5	2.0	49	2.0	67.5	1.6	35	1.1	51	2.0	286	3.4	146.5	2.2	118.5	2.1	281	1.9	898	58.4	17. VII	14	40	105	38	19	7	13	181	150	118	24	–	70	11

Rzeszów-Jasionka $\varphi = 50°06'$ $\lambda = 22°03'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	993.3	1010.6	972.8	1018.7	2.3	−2.6	8.2	22	−15.7	31	−0.9	1.3	−0.4	−0.1	5.2	5.4	5.1	5.2	88	79	84	84	0.7	1.6	1.0	1.1	7.3	7.2	6.8	7.1
II	991.4	1008.7	963.5	1016.9	−0.1	−5.3	3.4	13	−13.5	25	−3.4	−1.4	−2.4	−2.4	4.2	4.6	4.6	4.5	87	81	88	85	0.6	1.0	0.6	0.7	8.8	9.0	8.5	8.8
III	986.6	1004.0	969.2	1012.0	2.1	−5.9	13.6	31	−20.2	20	−3.9	0.9	−2.0	−1.8	4.5	5.2	4.9	4.9	90	77	87	85	0.5	1.7	0.7	1.0	6.4	7.6	6.5	7.5
IV	990.1	1002.3	967.0	1014.5	16.9	4.6	26.7	24	−0.6	30	7.7	15.4	9.3	10.4	8.8	9.0	9.1	9.0	83	57	77	72	2.0	9.9	3.0	5.0	5.7	6.1	4.8	5.5
V	989.6	997.1	975.7	1013.9	16.4	6.7	23.5	14	−1.3	1	9.9	14.9	10.5	11.4	11.0	11.1	11.3	11.1	88	64	87	80	1.5	6.5	1.7	3.2	7.8	8.3	6.5	7.5
VI	993.7	1002.6	983.6	1017.8	19.3	9.1	28.6	16	3.2	9	12.9	17.8	13.4	14.4	13.1	12.9	13.5	13.2	85	63	85	78	2.4	9.2	2.7	4.8	6.3	7.2	6.0	6.5
VII	991.1	1001.5	979.2	1015.0	21.6	10.6	30.7	27	4.3	30	14.3	20.2	15.0	16.1	14.1	13.3	14.4	13.9	86	57	84	76	2.4	10.9	2.8	5.4	5.6	7.0	5.8	6.1
VIII	992.8	999.9	982.7	1016.5	23.9	11.4	31.1	13	4.8	1	15.2	22.3	16.7	17.8	15.4	15.5	16.0	15.6	89	59	84	77	2.0	12.1	3.3	5.8	5.4	6.3	4.4	5.4
IX	993.5	1005.5	980.2	1017.7	18.6	7.5	27.6	5	0.9	15	10.0	17.1	11.8	12.7	10.9	11.7	11.8	11.5	89	62	85	79	1.8	8.6	2.5	4.3	5.3	6.5	4.9	5.6
X	998.7	1011.9	986.1	1023.6	13.7	1.5	18.6	2	−6.1	16	3.6	12.4	5.4	6.7	7.9	10.2	8.5	8.9	95	71	92	86	0.4	4.4	0.7	1.8	7.0	5.4	2.9	5.1
XI	993.3	1008.2	979.6	1018.3	7.4	1.9	16.1	1	−2.1	18	3.4	6.2	4.2	4.5	7.4	8.2	7.7	7.8	93	85	92	90	0.6	1.6	0.7	1.0	8.6	8.1	8.1	8.3
XII	992.4	1019.2	952.6	1018.1	−1.6	−7.9	5.2	13	−18.5	29	−4.8	−3.3	−4.7	−4.4	3.9	4.2	4.1	4.1	87	84	88	86	0.6	0.9	0.6	0.7	7.7	8.4	8.7	8.3
Rok	992.2	1019.2	952.6	1016.9	11.7	2.6	31.1	13.VIII	−20.2	20. III	5.3	10.3	6.4	7.1	8.9	9.3	9.2	9.1	88	70	86	81	1.3	5.7	1.7	2.9	7.0	7.3	6.2	6.8

Racibórz $\varphi = 50°05'$ $\lambda = 18°13'$

I	994.6	1012.9	971.5	1018.9	3.3	−2.3	9.2	22	−16.0	31	−0.5	2.2	0.0	0.3	5.1	5.2	5.1	5.1	84	71	81	79	1.0	2.2	1.2	1.5	6.8	7.8	7.3	7.3
II	993.8	1010.5	963.6	1018.3	1.7	−4.9	7.4	12, 13	−14.3	3	−3.3	−0.1	−1.4	−1.6	4.3	4.5	4.7	4.5	85	73	82	80	0.8	1.7	1.1	1.2	8.6	8.2	7.5	8.1
III	987.8	1005.1	969.6	1012.0	3.8	−3.1	15.9	31	−7.3	26	−2.3	2.2	0.2	0.1	4.8	4.9	5.2	5.0	89	66	80	78	0.6	2.6	1.3	1.5	7.5	7.5	6.5	7.2
IV	991.3	1003.0	964.7	1014.6	16.2	5.7	28.3	23	1.3	3	7.7	14.8	10.0	10.6	8.4	7.9	8.8	8.4	79	51	71	67	2.4	10.9	4.2	5.8	6.7	6.1	5.6	6.1
V	991.1	996.9	979.5	1014.3	16.1	6.8	23.0	19	−0.7	1	9.4	13.9	10.7	11.2	10.3	9.9	10.9	10.4	85	63	84	77	1.8	6.5	2.2	3.5	7.6	7.6	7.1	7.4
VI	996.3	1005.7	986.0	1019.3	20.2	9.6	30.5	23	0.5	2	12.7	18.9	14.1	15.0	12.0	11.3	13.0	12.1	79	50	78	69	3.2	12.0	4.2	6.5	5.7	6.3	5.5	5.8
VII	992.9	1002.3	980.7	1015.7	21.9	10.3	31.1	26	5.0	9	13.9	19.9	15.1	16.0	13.4	13.6	13.9	13.6	84	59	80	74	2.7	10.3	3.6	5.5	6.1	6.4	6.0	6.2
VIII	994.2	1001.4	980.8	1017.0	24.7	12.0	33.3	7	5.7	29	14.8	23.0	16.2	17.6	14.6	14.7	15.7	15.0	85	52	84	74	2.5	14.2	3.0	6.6	6.0	6.2	4.7	5.6
IX	994.6	1005.3	980.8	1017.8	18.8	7.0	30.3	4	0.5	15	9.5	16.8	11.3	12.2	10.9	11.7	11.5	11.4	90	63	86	80	1.4	8.4	2.3	4.0	7.0	6.4	3.9	5.8
X	999.5	1011.1	986.0	1023.2	14.4	4.0	23.7	4	−2.1	22	5.7	12.9	7.1	8.2	8.9	10.3	9.5	9.6	94	70	91	85	0.6	5.3	0.9	2.3	7.7	5.2	4.3	5.7
XI	993.4	1009.2	976.7	1017.3	7.3	2.3	18.4	7	−1.9	24	2.8	6.2	3.9	4.2	6.9	7.6	7.2	7.2	90	79	88	86	0.7	2.5	1.1	1.4	8.5	8.5	8.6	8.5
XII	993.5	1021.3	951.6	1018.2	−1.2	−6.3	7.4	13	−16.7	22	−4.8	−2.5	−4.3	−4.0	3.9	4.2	4.0	4.0	85	78	85	83	0.7	1.3	0.8	0.9	7.6	7.8	6.7	7.4
Rok	993.6	1021.3	951.6	1017.2	12.3	3.4	33.3	7.VIII	−16.7	22. XII	5.5	10.7	6.9	7.5	8.6	8.8	9.1	8.8	86	65	82	78	1.5	6.5	2.2	3.4	7.2	7.0	6.1	6.8

Bieruń Stary $\varphi = 50°05'$ $\lambda = 19°05'$

I	988.9	1006.6	965.7	1018.9	3.3	−3.7	10.3	22	−17.0	31	−1.6	2.5	−0.8	−0.2	5.1	5.5	5.2	5.3	90	74	87	84	0.6	2.1	0.8	1.2	6.7	7.1	6.6	6.8
II	987.9	1005.1	958.4	1018.0	1.0	−5.3	7.7	12	−15.0	3	−3.1	−0.1	−2.5	−2.0	4.4	4.6	4.7	4.6	88	75	88	84	0.6	1.5	0.6	0.9	9.0	8.2	8.0	8.4
III	982.0	998.7	964.2	1011.8	3.4	−4.8	15.9	31	−11.2	21	−2.2	2.5	−1.7	−0.8	4.8	5.0	5.0	4.9	88	66	88	81	0.7	2.7	0.7	1.4	7.4	7.5	6.8	7.2
IV	985.7	997.6	959.8	1014.5	16.1	4.2	28.1	23	−1.2	3	8.4	15.0	8.0	9.8	9.0	8.6	8.9	8.8	81	56	82	73	2.5	10.6	2.2	5.1	6.5	6.4	4.2	5.7
V	985.5	991.9	970.6	1014.2	16.0	5.9	23.5	8, 19	−1.9	1	9.8	14.1	9.4	10.7	10.8	10.6	10.9	10.8	88	67	91	82	1.6	6.2	1.2	3.0	7.4	7.5	6.8	7.2
VI	990.6	1000.1	981.3	1019.1	20.0	8.6	30.9	16	2.1	2	12.9	18.6	12.3	14.0	12.7	12.4	12.7	12.6	83	58	86	76	2.8	10.7	2.2	5.2	5.5	6.3	4.8	5.5
VII	987.4	997.2	975.1	1015.6	21.7	10.2	31.1	26	4.9	30	14.7	20.3	13.8	15.6	14.4	14.7	14.0	14.4	85	62	87	78	2.6	9.9	2.1	4.9	5.3	6.2	4.9	5.5
VIII	988.7	995.8	976.8	1016.8	24.1	11.2	32.6	7	5.0	29, 31	15.5	22.5	15.4	17.2	15.9	15.7	15.8	15.8	89	59	89	79	1.9	12.5	2.1	5.5	5.6	5.4	4.3	5.1
IX	989.0	1000.4	976.1	1017.7	18.8	6.0	29.6	4	0.6	10	10.0	17.3	10.3	12.0	11.4	12.7	11.6	11.9	92	66	92	83	1.2	8.0	1.3	3.5	7.2	5.3	3.1	5.2
X	994.1	1006.8	979.8	1023.3	14.2	3.5	22.8	1	−3.9	24	5.3	13.5	6.2	7.8	9.0	10.5	9.3	9.6	97	69	95	87	0.3	5.5	0.5	2.1	8.6	5.1	5.2	6.3
XI	988.1	1003.2	972.9	1017.7	6.8	2.0	18.5	7	−1.9	24	3.2	5.9	3.4	4.0	7.3	7.9	7.6	7.6	94	84	95	91	0.5	1.9	0.4	0.9	8.8	8.2	8.8	8.6
XII	987.9	1014.9	946.8	1018.3	−1.5	−7.3	8.3	13	−19.0	29	−5.2	−2.5	−4.9	−4.4	4.0	4.4	4.1	4.2	89	83	89	85	0.5	1.0	0.5	0.7	8.6	8.0	7.8	8.1
Rok	988.0	1014.9	946.8	1017.2	12.0	2.5	32.6	7.VIII	−19.0	29. XII	5.6	10.8	5.7	7.0	9.1	9.4	9.2	9.2	89	68	89	82	1.3	6.0	1.2	2.8	7.2	6.8	5.9	6.6

Kraków-Czyżyny $\varphi = 50°05'$ $\lambda = 20°01'$

I	991.4	1009.2	968.2	1018.1	3.3	−4.2	11.2	22	−17.3	31	−1.7	2.2	−0.6	−0.2	4.9	5.3	5.1	5.1	88	72	83	81	0.7	2.2	1.1	1.3	7.2	6.7	7.6	7.2
II	990.2	1007.1	961.5	1017.1	0.8	−4.9	7.4	12	−14.0	3	−3.1	−0.9	−1.7	−1.8	4.3	4.5	4.6	4.5	85	77	84	82	0.7	1.4	1.0	1.0	9.1	8.4	8.1	8.5
III	984.8	1001.5	967.6	1011.6	2.6	−4.7	15.9	31	−13.9	26	−3.3	1.4	−1.2	−1.1	4.4	5.2	4.8	4.8	86	73	82	80	0.7	2.0	1.0	1.2	8.1	7.8	7.2	7.7
IV	988.4	1000.5	962.5	1014.4	16.0	4.9	26.0	22	−1.5	3	7.9	14.3	9.8	10.4	8.9	8.7	9.1	8.9	82	57	74	71	2.0	9.4	3.6	5.0	6.8	7.0	5.5	6.4
V	988.0	994.6	973.4	1013.6	15.9	6.7	23.5	8	−1.0	1	9.7	14.1	10.8	11.4	10.6	10.3	11.0	10.6	86	64	83	78	1.7	6.4	2.3	3.5	8.3	8.4	6.8	7.8
VI	992.9	1002.1	983.4	1018.3	19.5	9.1	30.3	23	3.3	2	13.2	17.7	13.7	14.6	12.4	11.9	12.5	12.3	79	58	77	71	3.5	9.8	4.0	5.8	5.8	7.4	5.9	6.4
VII	989.8	999.8	977.8	1015.1	21.7	10.8	31.1	26	5.6	5	14.3	20.1	15.4	16.3	13.8	12.7	14.2	13.6	83	55	80	73	2.8	11.5	3.5	5.9	6.3	7.0	5.6	6.3
VIII	991.3	998.3	979.9	1016.4	23.8	12.2	32.1	7	5.8	31	15.1	22.3	16.5	17.6	14.9	14.8	15.5	15.1	86	56	81	74	2.4	12.9	3.6	6.3	5.9	6.4	5.1	5.8
IX	991.6	1003.4	978.4	1017.2	18.7	6.8	28.7	4	0.8	27	9.5	16.9	11.6	12.4	10.8	11.7	11.7	11.4	90	62	85	79	1.3	8.4	2.4	4.0	6.2	6.3	4.1	5.5
X	996.7	1009.4	982.9	1022.9	13.1	3.4	19.0	1	−3.5	27	4.8	11.8	6.9	7.6	8.5	10.0	9.2	9.2	96	72	91	86	0.4	4.1	0.9	1.8	7.9	5.6	4.6	6.0
XI	990.8	1005.9	975.9	1017.1	7.2	2.0	17.9	5, 7	−2.2	24	3.0	6.2	4.2	4.4	7.1	7.8	7.7	7.5	92	82	91	88	0.6	2.2	0.9	1.2	8.4	8.3	8.5	8.4
XII	990.6	1017.7	949.8	1017.7	−1.2	−7.4	7.0	12	−21.9	29	−5.1	−2.6	−4.4	−4.1	3.8	4.2	4.0	4.0	83	80	84	82	0.8	1.1	0.8	0.9	8.2	8.3	8.3	8.3
Rok	990.5	1017.7	949.8	1016.5	11.8	2.9	32.1	7.VIII	−21.9	29. XII	5.4	10.3	6.8	7.3	8.7	8.9	9.1	8.9	86	67	83	79	1.5	6.0	2.1	3.2	7.4	7.3	6.4	7.0

Rzeszów-Jasionka $H_s = 200m$ $H_b = 201,7m$ $h_w = 21m$ 1962

MIESIĄC	ROZKŁAD WIATRU ⁿD, ᵛmD — N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R — Suma	Max	Data	LICZBA DNI (n) — Temperatura T — Min < −10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v — v ≥ 10	v ≥ 15	◔	●	Opad R — R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R
I	3	6.0	4.5	5.7	·	·	0.5	3.0	28.5	5.9	32	5.3	17	4.8	5.5	6.7	2	5.4	27	7.2	25	2	7	20	·	3	·	1	11	16	7	·	·	16	·
II	9.5	4.4	2	3.8	14	5.1	3.5	4.4	5.5	6.8	16	6.1	18.5	5.8	13	7.7	2	5.7	28	7.3	12	4	15	28	·	9	·	·	18	18	11	·	·	24	·
III	6	3.3	11	5.5	15.5	4.2	3	4.5	14	4.9	10	4.0	16.5	5.5	11	5.5	6	4.5	31	5.8	12	6	12	27	·	5	·	1	15	13	8	·	1	27	·
IV	0.5	3.0	8	3.6	17.5	3.5	1.5	4.0	21	4.8	11	3.9	10	5.6	7.5	7.1	13	3.9	22	7.4	28	·	·	2	4	5	1	6	7	10	5	·	1	·	1
V	5.5	3.9	2	1.8	8.5	3.2	2	3.0	7.5	3.7	20.5	3.0	33	4.7	6	3.9	8	3.5	111	11.7	15	·	·	4	·	2	2	·	15	25	18	3	5	·	4
VI	9	4.0	2.5	2.4	2.5	2.4	1.5	2.7	10.5	2.0	14.5	3.0	24	4.0	19.5	4.8	6	3.4	125	30.8	1	·	·	·	8	2	·	2	10	15	13	4	2	·	4
VII	6	3.6	3.5	2.9	5	1.8	1	1.0	5.5	3.3	23.5	2.4	26	3.4	13.5	4.2	9	2.9	61	29.3	19	·	·	·	5	1	·	2	10	17	9	2	2	·	7
VIII	4	3.6	2.5	2.0	9.5	2.7	2	1.0	9.5	3.5	25	2.5	24	4.6	7.5	4.3	9	3.1	36	8.3	1	·	·	·	12	2	·	2	4	14	8	·	7	·	5
IX	1.5	1.3	4	2.2	11	2.9	2	1.2	14.5	4.9	16	3.3	29.5	4.4	2.5	4.2	9	3.4	60	28.4	5	·	·	·	3	·	·	4	10	12	7	1	7	·	2
X	3	1.7	5.5	3.2	18	2.9	1	1.0	2.5	3.0	19.5	2.8	13.5	3.1	12	3.9	18	2.4	4	1.8	15	·	·	10	·	·	·	5	4	3	2	·	17	·	·
XI	5	3.4	7	4.3	40.5	5.3	1.5	3.0	5	4.7	11	4.6	10.5	4.7	6.5	3.5	3	4.6	50	11.1	15	·	·	5	·	3	·	·	18	17	11	1	6	2	·
XII	10	3.6	12	4.1	7	4.2	·	·	23	6.8	16	3.9	15	3.9	6	4.0	4	4.5	33	9.6	16	11	14	31	·	5	·	·	21	18	6	·	8	18	·
Rok	63	3.5	64.5	3.5	149	3.2	19.5	2.4	147	4.5	215	3.7	237.5	4.5	110.5	5.0	89	3.9	588	30.8	1.VI	23	48	127	32	37	3	23	143	178	105	11	56	87	23

UWAGA. *Kierunki i prędkości wiatru - wg anemometru*

Racibórz $H_s = 189m$ $H_b = 192,6m$ $h_w = 12,5m$

I	7.5	3.4	1	3.0	·	·	3	1.8	31.5	2.4	27	2.8	4.5	2.7	12.5	3.8	6	2.6	37	9.6	11	2	4	18	·	·	·	·	13	16	13	·	1	11	·
II	10	3.0	2.5	1.4	3.5	1.9	6	2.2	11.5	2.2	9.5	3.4	9	4.4	16	4.6	16	2.7	31	5.7	19	5	9	24	·	3	1	·	16	17	13	·	1	21	·
III	13.5	4.2	9	1.8	3	1.7	6	1.6	11	1.5	7	1.6	4.5	1.9	20	3.5	19	2.1	49	14.7	5	·	7	25	·	·	·	2	18	16	9	2	·	12	·
IV	15	1.6	2	2.0	4	2.2	5	1.7	19.5	2.7	10	2.3	6.5	2.2	14	3.1	14	2.0	41	9.0	6	·	·	·	8	·	·	4	9	14	9	·	·	·	·
V	13	1.4	3	1.5	1	1.0	5	1.5	13	2.0	11.5	1.8	11.5	3.0	17	2.2	18	1.6	215	34.0	13	·	·	1	·	·	·	·	10	22	20	9	1	·	6
VI	11.5	1.9	2	3.0	2	1.0	6	1.5	8	2.0	7	2.4	11.5	2.4	26	2.6	16	1.9	56	34.0	1	·	·	·	7	·	·	2	9	12	6	1	·		2
VII	13.5	1.6	2.5	1.8	·	·	4	1.4	11.5	1.7	15.5	2.2	3.5	2.4	26.5	1.6	16	1.5	60	37.2	17	·	·	·	8	·	·	4	7	14	7	1	·	·	5
VIII	5	1.5	1	1.5	0.5	1.0	12.5	1.3	14.5	2.2	12	2.0	5	1.7	18.5	2.0	24	1.4	43	12.7	15	·	·	·	14	1	·	2	6	13	8	1	1	·	5
IX	5.5	2.3	0.5	3.0	4.5	1.7	5	1.4	14	2.0	14	2.2	4.5	1.9	14	2.6	28	1.5	82	28.9	18	·	·	·	4	·	·	5	10	11	10	2	7	·	1
X	10.5	1.8	1.5	2.7	8	1.3	10.5	1.3	9	1.9	1.5	3.0	2	2.5	12	2.4	38	1.1	48	22.8	31	·	·	6	·	·	·	4	10	8	6	2	18	·	·
XI	8	2.0	8	2.1	3	1.8	17.5	1.5	9.5	1.5	4	2.1	1.5	1.7	12.5	2.1	26	1.3	121	25.0	15	·	·	8	·	·	·	·	21	19	12	4	7	7	·
XII	21	2.5	2.5	1.6	3	1.0	6.5	2.0	11	2.8	17.5	2.3	3	3.0	12.5	2.0	16	1.9	26	5.3	31	9	14	28	·	·	·	·	18	16	7	·	2	20	·
Rok	134	2.3	35.5	2.1	32.5	1.2	87	1.6	164	2.1	136.5	2.3	67	2.5	201.5	2.7	237	1.8	809	37.2	17.VII	16	34	110	41	4	1	23	147	178	120	22	38	71	19

Bieruń Stary $H_s = 236m$ $H_b = 239,0m$ $h_w = 30m$

I	3.5	3.6	1.5	2.3	·		·	·	0.5	3.0	36.5	3.5	16	3.4	8	3.8	27	2.5	42	6.0	11	3	5	25	·	·	·	·	13	16	12	·	·	18	·
II	4.5	3.2	5	2.9	2.5	2.0		·	·	·	14.5	5.3	17.5	5.0	14	4.8	26	3.2	54	8.5	16	4	10	25	·	3	3	·	18	19	13	·	1	24	·
III	9.5	4.5	9	4.0	5	2.5	5	2.6	·		8	3.4	8	4.8	10.5	4.7	38	2.3	55	12.7	12	3	6	27	·	2	1	2	17	14	10	2	1	17	·
IV	6	2.2	3.5	2.4	2.5	2.8	3.5	3.3	5	2.7	12	2.5	9	3.4	13.5	4.0	35	1.9	80	16.5	28	·	·	2	8	1	·	7	9	13	9	4	·	·	·
V	2	2.5	1.5	1.0	4.5	2.0	3	2.0	1	2.5	16	2.7	12.5	4.2	10.5	3.6	42	1.7	160	21.3	13	·	·	3	·	·	·	1	13	23	19	6	·	·	3
VI	4	5.5	3.5	3.6	2.5	1.8	0.5	1.0	1	2.0	9.5	3.5	14.5	3.1	15.5	4.1	39	2.0	62	23.4	1	·	·	·	6	1	·	6	12	14	6	3	·		2
VII	3	2.7	2	3.0	1	4.0	1	2.0	1	1.0	13	3.5	19.5	2.8	14.5	2.8	38	1.7	111	40.0	17	·	·	·	6	·	·	5	7	15	13	2	·	·	5
VIII	1	2.0	0.5	3.0	3	2.8	1.5	2.7	2	2.0	12.5	3.4	18.5	3.2	9	2.9	45	1.6	39	8.8	7	·	·	·	14	·	·	6	6	14	10	·	2	·	6
IX	3	2.3	3.5	2.1	6	2.8	1.5	2.0	·	·	13	5.0	17.5	3.2	11.5	3.1	34	2.1	$61^{?}$	19.0	17	·	·	·	4	·	·	6	7	11	9	2	4	·	1
X	0.5	2.0	4.5	2.0	17.5	2.6	1.5	2.7	·	·	5	3.5	12.5	2.2	6.5	2.5	45	1.3	21	9.1	28	·	·	8	·	·	·	3	11	10	5	·	19	·	·
XI	·	·	8.5	2.5	17	2.3	6.5	2.2	·		4.5	3.2	9.5	2.4	4	2.0	40	1.3	90	18.1	15	·	·	7	·	·	·	·	21	15	12	3	4	3	·
XII	2.5	2.6	11	2.3	7	1.9	1	2.0	0.5	3.0	15.5	4.3	5	2.6	4.5	3.3	46	1.5	49	12.7	13	11	16	28	·	·	·	1	19	19	11	1	3	20	·
Rok	39.5	2.8	54	2.6	68.5	2.3	25	1.9	11	1.4	160	3.6	160	3.4	122	3.5	455	1.9	$824^{?}$	40.0	17.VII	21	37	125	38	7	4	37	153	182	129	23	34	82	17

Kraków-Czyżyny $H_s = 213m$ $H_b = 213,4m$ $h_w = 25m$

I	2.5	7.8	5.5	3.0	3.5	4.1	3	2.0	1.5	3.3	7	2.9	41	4.2	15	5.2	14	3.5	37	7.8	27	3	5	24	·	1	·	1	13	16	11	·	3	16	·
II	5	4.0	12	4.1	7.5	3.0	0.5	1.0	2.5	3.6	9.5	6.8	27	5.4	12	6.6	8	4.6	41	6.9	17	5	10	23	·	4	·	·	21	22	11	·	1	19	1
III	9	5.7	26	4.3	9.5	3.9	3.5	2.3	1	3.0	5.5	4.8	18.5	4.2	17	4.4	8	4.0	37	8.8	12	3	11	25	·	3	·	3	18	18	9	·	1	22	·
IV	8	4.2	13	3.8	9	3.7	5.5	4.5	5	5.0	6.5	4.2	23.5	4.3	9.5	5.4	10	3.8	97	44.8	6	·	·	2	5	2	·	4	10	16	11	2	2	·	1
V	4.5	2.8	7.5	2.8	10.5	3.9	3.5	3.3	2	2.0	21.5	3.9	31.5	4.1	8	3.4	4	3.6	145	13.9	13, 21	·	·	1	·	1	·	·	16	26	19	8	2	·	3
VI	7	3.6	7.5	2.0	8.5	2.4	1	1.5	1	1.0	11.5	3.4	30	3.8	16.5	4.6	7	3.3	75	36.2	1	·	·	·	6	1	·	3	12	11	8	2	·	·	4
VII	4.5	2.8	3	2.7	4	2.6	2	3.0	3.5	4.3	20	2.9	32.5	3.4	10.5	2.6	13	2.7	153	39.8	17	·	·	·	6	·	·	3	11	17	14	4	2	·	11
VIII	3.5	3.6	7	2.3	6	2.8	2.5	2.8	1	6.0	18.5	3.4	34	3.5	7.5	3.8	13	2.9	45	20.5	5	·	·	·	11	·	·	2	6	12	6	2	4	·	3
IX	3.5	1.9	13.5	2.2	8	3.2	4	1.6	2.5	4.4	14	4.4	30	3.7	2.5	3.4	12	2.9	66	19.6	18	·	·	·	5	·	·	7	7	13	8	3	6	·	1
X	8	2.5	22	2.8	12.5	2.3	3	1.7	·	·	6	3.2	24.5	2.9	5	2.9	12	2.4	7	3.5	31	·	·	8	·	·	·	4	12	7	2	·	25	·	·
XI	3.5	2.1	30	3.6	14.5	3.4	2.5	1.8	1.5	3.7	8	3.4	21.5	3.6	5.5	3.1	3	3.3	84	17.8	15	·	1	8	·	·	·	1	21	18	13	3	14	7	·
XII	8	3.8	23	3.9	8.5	3.2	2.5	4.0	2	2.8	13	4.2	20	4.4	5	4.7	11	3.5	42	7.3	13	11	14	29	·	·	·	2	21	20	9	·	7	18	·
Rok	67	3.7	170	3.1	102	3.2	33.5	2.5	23.5	3.3	141	4.0	334	4.0	109	4.2	115	3.4	829	44.8	6.IV	22	41	120	33	12	·	30	168	196	121	24	67	82	24

UWAGA. *Kierunki i prędkości wiatru - wg anemometru*

Kraków - Chełm $\varphi = 50°04'$ $\lambda = 19°51'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.0	-3.3	10.1	22	-14.9	31	-1.3	1.7	-0.2	0.0	–	–	–	–	–	–	–	–	–	–	–	–	79	70	76	75
II	–	–	–	–	0.8	-4.6	7.0	12, 13	-14.1	3	-3.2	-1.1	-1.8	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	98	83	85	89
III	–	–	–	–	2.2	-5.0	14.2	31	-15.0	26	-3.9	0.7	-1.6	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	83	76	62	74
IV	–	–	–	–	15.4	5.2	25.3	23	-0.3	3	7.6	13.6	9.8	10.2	–	–	–	–	–	–	–	–	–	–	–	–	63	63	48	58
V	–	–	–	–	15.5	6.7	22.8	19	-0.7	1	9.0	13.6	10.6	11.0	–	–	–	–	–	–	–	–	–	–	–	–	84	78	71	78
VI	–	–	–	–	19.5	9.1	33.1	24	3.0	2	12.8	17.2	13.1	14.0	–	–	–	–	–	–	–	–	–	–	–	–	64	71	54	63
VII	–	–	–	–	21.0	10.6	30.5	26	6.2	6	13.7	19.5	15.0	15.8	–	–	–	–	–	–	–	–	–	–	–	–	59	64	58	60
VIII	–	–	–	–	23.4	12.2	31.9	7	5.2	31	14.8	21.6	16.3	17.2	–	–	–	–	–	–	–	–	–	–	–	–	58	56	39	51
IX	–	–	–	–	18.2	6.9	28.3	4	1.8	25	9.1	16.2	11.5	12.1	–	–	–	–	–	–	–	–	–	–	–	–	73	59	42	58
X	–	–	–	–	12.6	3.4	19.0	1	-2.8	22	4.6	11.4	6.9	7.4	–	–	–	–	–	–	–	–	–	–	–	–	93	54	44	64
XI	–	–	–	–	6.7	1.9	17.0	7	-2.3	24	2.9	5.4	3.8	4.0	–	–	–	–	–	–	–	–	–	–	–	–	87	76	82	82
XII	–	–	–	–	-1.5	-7.1	7.9	13	-20.3	23	-5.3	-3.1	-4.5	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	86	82	78	82
Rok	–	–	–	–	11.4	3.0	33.1	24. VI	-20.3	23. XII	5.1	9.7	6.6	7.0	–	–	–	–	–	–	–	–	–	–	–	–	77	69	62	69

Kraków, Obserw. Astr. UJ $\varphi = 50°04'$ $\lambda = 19°58'$

I	990.2	1007.8	967.3	1017.9	3.6	-2.8	11.1	22	-14.2	31	-1.2	2.5	0.0	0.3	5.2	5.3	5.3	5.3	90	72	85	82	0.6	2.3	1.0	1.3	76	71	77	75
II	989.0	1005.8	960.5	1016.7	1.2	-4.1	8.1	12	-11.5	3	-2.8	-0.7	-1.3	-1.5	4.6	4.8	5.1	4.8	90	82	90	87	0.6	1.2	0.7	0.8	91	89	92	91
III	983.6	1000.[illegible]	966.8	1011.0	3.1	-4.1	16.0	31	-12.1	26	-3.0	1.6	-0.6	-0.6	4.6	5.2	5.3	5.0	90	72	86	83	0.5	2.2	0.8	1.2	85	76	77	79
IV	987.1	999.2	962.1	1013.7	16.2	5.6	26.3	23	0.3	2, 3	8.2	14.3	10.4	10.8	8.9	8.7	9.6	9.1	81	58	75	71	2.3	9.3	3.8	5.1	66	66	68	67
V	986.8	993.2	972.8	1013.2	16.2	7.2	24.0	19	-0.1	1	9.7	14.2	11.2	11.6	10.7	10.7	11.3	10.9	87	67	83	79	1.6	6.1	2.4	3.4	83	81	74	79
VI	991.6	1000.8	982.2	1017.9	19.9	10.1	30.4	23	3.4	2	13.3	17.9	14.3	15.0	12.3	12.0	13.1	12.5	78	58	78	71	3.7	10.1	4.0	5.9	61	72	61	65
VII	988.7	998.3	976.8	1014.8	21.9	11.6	31.1	26	6.8	5	14.4	20.2	16.0	16.6	13.6	13.2	14.8	13.9	82	57	81	73	2.9	11.2	3.6	5.9	64	69	60	64
VIII	990.1	997.4	978.8	1016.1	24.1	13.0	33.0	7	7.1	31	15.6	22.5	17.1	18.1	15.1	15.2	16.5	15.6	84	56	83	74	2.8	12.8	3.3	6.3	64	67	62	64
IX	990.7	1003.6	977.4	1017.1	18.8	7.5	29.3	4	1.7	27	9.7	17.0	11.9	12.6	11.0	11.8	12.4	11.7	91	63	88	81	1.4	8.4	2.0	3.9	74	62	61	66
X	995.5	1007.9	981.7	1022.5	13.1	4.1	19.0	1	-2.3	27	5.0	11.8	7.4	7.9	8.7	10.7	9.8	9.7	97	77	94	89	0.3	3.4	0.7	1.5	79	57	52	63
XI	989.8	1005.9	974.4	1017.1	7.3	2.1	17.6	7	-1.6	18, 24	3.1	6.2	4.4	4.5	7.2	7.9	7.9	7.7	93	83	92	89	0.5	2.1	0.7	1.1	90	83	87	87
XII	989.5	1016.5	948.6	1017.6	-0.9	-6.3	7.1	12	-18.9	29	-4.9	-2.6	-3.8	-3.8	4.0	4.3	4.2	4.2	88	82	85	85	0.6	1.1	0.8	0.8	83	82	90	85
Rok	989.4	1016.5	948.6	1016.3	12.0	3.7	33.0	7. VIII	-18.9	29. XII	5.6	10.4	7.2	7.6	8.8	9.2	9.6	9.2	88	69	85	81	1.5	5.8	2.0	3.1	76	73	72	74

UWAGA. *Ciśnienie powietrza jest za niskie przeciętnie o około 0,5 mb.*

Kraków - Nowa Huta $\varphi = 50°04'$ $\lambda = 20°05'$

I	–	–	–	–	3.5	-3.5	11.3	22	-14.3	31	-1.4	2.1	-0.4	0.0	–	–	–	–	–	–	–	–	–	–	–	–	87	63	64	71
II	–	–	–	–	0.9	-4.6	7.3	13	-13.5	3	-3.1	-0.9	-1.8	-1.9	–	–	–	–	–	–	–	–	–	–	–	–	92	76	90	86
III	–	–	–	–	2.6	-4.8	15.1	31	-13.6	26	-3.2	1.2	-1.1	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	76	79	65	73
IV	–	–	–	–	15.7	5.1	25.7	23	0.0	3	8.2	14.0	9.7	10.4	–	–	–	–	–	–	–	–	–	–	–	–	71	67	49	62
V	–	–	–	–	15.5	6.6	23.2	8	-0.6	1	9.5	14.1	10.6	11.2	–	–	–	–	–	–	–	–	–	–	–	–	82	79	61	74
VI	–	–	–	–	18.9	8.9	29.9	23	3.3	2, 7	12.9	17.6	13.2	14.2	–	–	–	–	–	–	–	–	–	–	–	–	59	71	59	63
VII	–	–	–	–	21.5	10.5	31.3	26	4.4	5	14.5	19.7	15.2	16.2	–	–	–	–	–	–	–	–	–	–	–	–	61	67	59	62
VIII	–	–	–	–	23.7	11.7	32.5	7	5.0	29	15.0	22.1	16.5	17.5	–	–	–	–	–	–	–	–	–	–	–	–	60	59	39	53
IX	–	–	–	–	18.8	6.6	29.0	4	0.7	27	9.3	16.9	11.2	12.2	–	–	–	–	–	–	–	–	–	–	–	–	65	53	35	51
X	–	–	–	–	12.7	3.2	18.5	1	-3.9	27	4.5	11.3	6.7	7.3	–	–	–	–	–	–	–	–	–	–	–	–	71	53	41	55
XI	–	–	–	–	7.4	1.9	18.7	5	-2.1	18	3.0	6.2	4.1	4.4	–	–	–	–	–	–	–	–	–	–	–	–	87	79	82	83
XII	–	–	–	–	-1.3	-7.0	6.6	12	-20.8	29	-5.2	-2.8	-4.5	-4.2	–	–	–	–	–	–	–	–	–	–	–	–	81	81	81	81
Rok	–	–	–	–	11.7	2.9	32.5	7. VIII	-20.8	29. XII	5.3	10.1	6.6	7.2	–	–	–	–	–	–	–	–	–	–	–	–	74	69	60	68

Dębica $\varphi = 50°03'$ $\lambda = 21°24'$

I	–	–	–	–	3.0	-2.1	8.7	20	-16.8	31	-0.4	1.9	0.1	0.4	–	–	–	–	–	–	–	–	–	–	–	–	75	75	70	73
II	–	–	–	–	0.5	-4.8	7.5	13	-14.6	26	-3.4	-1.0	-2.2	-2.2	–	–	–	–	–	–	–	–	–	–	–	–	92	86	96	91
III	–	–	–	–	2.5	-4.6	14.9	31	-16.8	21	-3.2	1.3	-1.1	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	84	75	86	82
IV	–	–	–	–	16.8	5.4	27.1	23	-0.1	30	8.3	15.2	10.5	11.1	–	–	–	–	–	–	–	–	–	–	–	–	59	51	60	57
V	–	–	–	–	16.2	7.4	22.9	8	-0.2	1	9.8	14.3	10.8	11.4	–	–	–	–	–	–	–	–	–	–	–	–	79	77	75	77
VI	–	–	–	–	19.3	9.3	30.6	24	3.1	7	12.8	17.3	13.8	14.4	–	–	–	–	–	–	–	–	–	–	–	–	63	63	60	62
VII	–	–	–	–	21.8	11.6	31.7	22	6.3	30	14.1	20.1	15.5	16.3	–	–	–	–	–	–	–	–	–	–	–	–	57	62	69	63
VIII	–	–	–	–	24.3	12.4	31.4	13	5.8	31	15.5	22.6	17.2	18.1	–	–	–	–	–	–	–	–	–	–	–	–	54	43	52	50
IX	–	–	–	–	19.1	8.4	29.0	5	1.9	15	10.4	17.2	12.3	13.0	–	–	–	–	–	–	–	–	–	–	–	–	53	54	52	53
X	–	–	–	–	13.9	2.8	19.0	1	-5.0	16	4.3	12.4	6.5	7.4	–	–	–	–	–	–	–	–	–	–	–	–	67	52	47	55
XI	–	–	–	–	8.3	2.5	17.3	8	-1.0	17	3.8	6.9	4.6	5.0	–	–	–	–	–	–	–	–	–	–	–	–	87	80	87	85
XII	–	–	–	–	-1.5	-6.9	5.6	14	-17.7	26	-4.6	-2.8	-4.5	-4.1	–	–	–	–	–	–	–	–	–	–	–	–	85	81	84	82
Rok	–	–	–	–	12.0	3.4	31.7	22. VII	-17.7	26. XII	5.6	10.4	7.0	7.5	–	–	–	–	–	–	–	–	–	–	–	–	71	67	70	69

Kraków - Chełm $H_s = 225\,m$ $h_w = 12\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU °D. °mD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	≥ 15	☁	●	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	≡	⊞	≈
I	5	3.8	0.5	3.0	3.5	3.6	·	·	·	·	24.5	3.9	32	5.2	3.5	5.3	24	3.4	20	3.5	12	2	6	22	·	·	·	2	18	15	8	·	1	17	·
II	4	3.5	3.5	3.9	11.5	3.0	·	·	·	·	18	4.8	23.5	7.3	6.5	7.0	17	4.4	25	5.6	13	4	9	24	·	5	1	·	22	15	9	·	·	23	1
III	2	4.0	9	5.3	16.5	2.8	2	1.2	2.5	1.8	7	4.5	15	5.5	8	4.4	31	2.8	27	7.9	12	3	11	26	·	1	·	3	17	14	8	·	·	22	·
IV	3	1.7	3	2.7	12.5	3.2	1.5	2.0	3	3.7	9	3.9	21	4.6	7	4.4	30	2.5	85	38.0	6	·	·	1	2	·	·	7	11	17	10	2	2	·	1
V	1	3.0	3.5	1.7	7.5	2.7	2	1.0	3	4.7	15	3.9	29.5	5.2	3.5	3.4	28	2.9	136	15.6	28	·	·	1	·	2	·	1	14	27	20	4	·	·	5
VI	7.5	3.9	3.5	1.9	2	2.0	0.5	3.0	1	5.0	11.5	3.9	22.5	5.1	10.5	4.0	31	2.7	67	26.4	1	·	·	·	7	·	·	3	11	11	8	3	·	·	3
VII	2	2.5	·	·	5.5	2.6	0.5	5.0	1	3.0	13.5	3.2	33	3.6	5.5	3.0	32	2.2	184	59.8	17	·	·	·	4	·	·	4	11	14	13	4	·	·	7
VIII	1	3.0	2.5	1.4	5.5	2.6	1	2.0	1	5.0	9.5	4.0	35	4.8	3.5	3.9	34	2.7	35	12.2	5	·	·	·	11	·	·	3	5	12	8	1	2	·	5
IX	·	·	1	1.5	8	2.8	·	·	·	·	15.5	4.3	23.5	4.3	3	3.5	39	2.2	51	16.2	18	·	·	·	3	·	·	4	10	10	8	2	6	·	1
X	1	1.0	6	2.2	17.5	2.2	0.5	3.0	2	2.0	6	4.1	14.5	3.8	1.5	2.3	44	1.5	11	3.3	6	·	·	8	·	·	·	1	12	7	3	·	22	·	·
XI	·	·	5	3.1	2.9	2.6	2	4.0	·	·	8.5	3.4	16.5	4.3	1	4.0	28	2.3	81	16.9	15	·	1	6	·	·	·	2	21	18	13	1	8	7	·
XII	5	3.0	7	2.9	16	4.6	2	2.5	·	·	17	5.1	16.5	5.4	4.5	4.0	25	3.3	38	10.5	13	11	15	30	·	·	·	2	20	17	8	1	2	19	·
Rok	31.5	2.4	44.5	2.5	13.5	2.9	12	2.0	13.5	2.1	155	4.1	282.5	4.9	58	4.1	363	2.7	760	59.8	17.VII	20	42	118	27	8	1	32	172	177	116	18	43	88	23

Kraków, Obserw. Astr. UJ $H_s = 206\,m$ $H_b = 219{,}8\,m$ $h_w = 10\,m$

I	4	3.8	3	4.3	0.5	1.0	2.5	1.0	4.5	1.8	37	2.9	14.5	3.5	6	3.5	21	2.3	29	4.0	11	2	4	20	·	·	·	·	14	16	10	·	21	19	·
II	4	3.2	12	3.2	4.5	2.4	0.5	3.0	4.5	2.3	22.5	3.9	17	3.9	8	4.9	11	3.2	48	7.6	13	2	10	24	·	2	1	·	21	22	10	·	13	23	1
III	10	3.7	17.5	2.9	9	2.4	3	1.3	1.5	1.3	11.5	2.6	9.5	4.1	10	3.5	21	2.4	43	8.2	12	3	10	25	·	2	·	·	18	17	12	·	15	22	·
IV	5	2.0	12.5	2.2	5	2.5	5	4.5	4.5	3.4	16	2.9	16	3.0	11	3.9	15	2.5	91	40.7	6	·	·	·	6	·	·	4	13	16	10	2	4	·	3
V	4	1.6	6.5	2.2	5	2.5	5.5	2.5	4	1.5	23.5	3.1	21.5	2.6	7	2.1	16	2.1	141	15.5	13	·	·	1	·	1	·	1	15	24	20	6	·	·	4
VI	7	2.4	7	1.9	4	1.5	1.5	1.0	0.5	3.0	13.5	3.3	21	2.5	13.5	3.4	22	2.0	68	31.9	1	·	·	·	6	·	·	4	13	13	10	2	·	·	4
VII	3	1.3	3.5	1.6	2	1.5	2.5	2.4	4	2.9	20	2.0	18	2.4	10	1.8	30	1.4	148	57.9	17	·	·	·	7	·	·	3	10	16	13	4	1	·	8
VIII	4.5	2.0	4.5	2.0	6	2.7	1.5	4.7	3	1.7	16.5	2.9	18.5	2.8	3.5	2.9	35	1.7	38	13.8	5	·	·	·	12	·	·	·	6	10	7	2	5	·	3
IX	2	1.0	7.5	2.1	6	2.7	0.5	4.0	4.5	3.2	19.5	2.4	19.5	2.5	2.5	3.4	28	1.7	63	18.2	18	·	·	·	5	·	·	5	13	14	8	3	8	·	·
X	5.5	1.3	2.0	1.8	1.1	1.5	0.5	2.0	1	1.0	10.5	1.6	9.5	2.1	5	1.6	30	1.1	8	3.1	31	·	·	7	·	·	·	4	14	16	2	·	27	·	·
XI	7.5	1.4	2.4	2.6	8.5	2.5	·	·	2.5	3.2	13	2.5	10	2.5	5.5	2.2	19	1.9	86	17.6	15	·	·	6	·	·	·	·	21	19	13	3	15	5	·
XII	10.5	3.0	17	3.7	8	2.1	1.5	1.3	3	3.7	22.5	2.6	8	2.2	6.5	2.3	16	2.3	49	8.3	13	10	14	29	·	·	·	·	20	19	10	·	17	19	·
Rok	6.7	2.2	13.5	2.5	6.9.5	2.1	2.4.5	2.3	3.7.5	2.4	226	2.7	183	2.8	88.5	3.0	264	2.0	812	57.9	17.VII	17	38	112	36	5	1	21	178	202	125	22	126	88	23

Kraków - Nowa Huta $H_s = 195\,m$ $h_w = 15{,}4\,m$

I	5	4.2	4.5	5.0	9	2.4	0.5	1.0	5	1.6	10.5	2.6	4.7.5	2.6	3	4.3	8	2.6	23	4.9	11	2	5	25	·	·	·	·	12	10	7	·	2	–	–
II	3	4.3	6.5	3.5	14	3.0	0.5	1.0	1.5	1.0	8	4.2	37	3.6	8.5	4.2	5	3.3	36	6.2	16	4	10	24	·	1	·	·	20	15	9	·	2	–	–
III	8.5	3.5	14.5	3.1	26.5	2.0	2.5	1.4	2.5	1.6	3	2.0	19	2.8	13.5	4.0	3	2.7	27	7.5	12	3	12	26	·	·	·	1	15	8	7	·	1	–	–
IV	4	2.6	6	3.7	17.5	2.9	3.5	3.0	5	2.6	8.5	2.6	30.5	2.8	6	4.2	9	2.7	72	34.8	6	·	·	·	3	·	·	4	9	12	9	2	2	·	–
V	6.5	1.8	7.5	1.5	11.5	1.8	0.5	1.0	6	1.2	12.5	2.3	34.5	2.5	11	2.0	3	2.0	137	14.8	25	·	·	2	·	·	·	1	13	23	21	5	5	·	–
VI	12.5	2.2	5.5	1.7	8.5	2.3	2	1.0	2	1.2	5.5	2.0	36.5	2.8	11.5	2.7	6	2.3	45	26.2	4	·	·	·	6	·	·	3	12	9	6	1	3	·	–
VII	5.5	1.9	2.5	2.6	11.5	1.8	·	·	3.5	3.7	9.5	2.7	43.5	2.1	9	2.6	8	2.1	108	26.2	18	·	·	·	6	·	·	3	10	15	13	4	2	·	–
VIII	3.5	1.7	3.5	1.7	10	1.8	2.5	2.0	3	2.0	12	2.0	37.5	3.1	8	2.2	13	2.2	29	14.8	16	·	·	·	12	·	·	1	3	11	7	1	4	·	–
IX	·	·	3.5	2.3	20.5	1.9	1.5	1.0	1.5	1.0	10	2.8	29.5	3.3	2.5	5.0	21	2.1	60	17.7	18	·	·	·	5	·	·	8	7	12	7	3	3	·	–
X	4.5	2.9	3.5	2.1	36.5	1.9	1	1.0	·	·	4	2.0	16	2.2	1.5	1.7	26	1.5	5[2]	2.0	31	·	·	8	·	·	·	8	11	4	2	·	19	·	–
XI	1.5	1.3	10	3.2	4.0	2.6	1.5	1.0	1	6.0	4	1.5	24	2.2	1	1.0	7	2.3	53[2]	–	–	·	·	7	·	·	·	1	21	17	11	·	6	–	–
XII	5.5	3.6	8.5	5.3	20	3.6	5.5	1.5	1.5	3.7	6.5	2.5	28.5	2.7	6	2.9	11	2.8	36	6.7	13	10	16	31	·	·	·	2	20	16	9	·	5	–	–
Rok	6.0	2.5	7.6	3.0	22.5.5	2.3	21.5	1.2	3.2.5	2.1	9.4	2.4	38.4	2.7	81.5	3.1	120	2.4	63.1[2]	34.8	6.IV	19	43	123	32	1	·	3.2	153	152	108	16	5.4	–	–

Dębica $H_s = 205\,m$ $h_w = 16{,}2\,m$

I	2.5	2.2	4	1.9	4	1.4	1.0	2.7	3.8.5	4.0	10.5	2.0	15	2.2	8.5	2.4	·	3.0	26	5.8	28	2	4	19	·	2	·	·	15	10	7	·	·	10	·
II	11.5	2.2	9.5	1.7	12.5	1.4	1	1.5	1.4	5.0	9.5	4.0	13.5	3.9	12.5	3.3	·	3.1	36	5.3	16	4	11	25	·	3	2	·	21	14	10	·	5	22	·
III	11.5	2.9	21	1.8	10	1.8	4.5	3.0	16	3.6	3	1.8	9.5	2.6	14.5	2.5	3	2.4	50	7.7	16, 22	5	10	24	·	·	·	1	22	17	13	·	6	20	·
IV	6	1.9	12.5	1.6	9.5	1.7	8.5	3.5	16.5	3.3	10.5	2.3	7.5	2.2	13	3.3	6	2.4	23	6.3	27	·	·	1	5	·	·	4	9	10	8	·	2	·	1
V	8.5	1.9	10.5	1.8	9	1.5	8.5	1.7	7	1.5	9.5	2.0	21.5	5.6	10.5	2.0	8	2.5	117[2]	13.4	21	·	·	1	·	3	2	·	16	26	21	1	1	·	3
VI	10.5	3.0	10.5	1.2	10	1.7	2.5	1.4	4.5	1.7	6.5	2.5	15.5	3.4	19	3.5	11	2.3	12.5	39.8	4	·	·	·	6	·	·	2	9	11	11	5	·	·	3
VII	9.5	1.5	7.5	1.7	7.5	1.3	7	1.8	2.5	2.4	10	2.4	17	2.4	19	2.2	13	1.8	88	21.5	18	·	·	·	6	·	·	2	10	16	15	3	·	·	5
VIII	7.5	1.5	13	1.4	14	1.5	6	1.8	8	1.8	6.5	1.7	16	2.6	13	2.6	9	1.8	28	14.5	16	·	·	·	13	·	·	4	2	10	7	1	1	·	4
IX	3	1.8	11	1.2	9.5	1.2	3.5	3.7	10.5	3.5	9.5	3.0	19.5	2.6	15.5	2.4	8	2.2	46	13.0	17	·	·	·	4	·	·	4	6	10	7	3	6	·	1
X	5.5	1.0	2.6	1.1	12.5	1.2	·	·	8	1.7	9.5	1.6	5	1.6	9.5	1.5	17	1.1	0	0.2	19, 31	·	·	10	·	·	·	8	11	2	·	·	19	·	·
XI	8.5	1.8	20.5	1.9	22	1.6	6	1.8	3.5	2.1	6.5	1.7	11.5	1.7	6.5	1.7	5	1.6	79	13.1	15	·	·	6	·	1	·	·	20	16	14	2	9	3	·
XII	9	1.7	21.5	1.6	9	1.7	4	2.5	12.5	6.0	15	3.2	10.5	3.7	5.5	2.8	6	2.9	47	15.4	14	10	13	30	·	2	1	·	22	16	10	1	5	18	·
Rok	9.3.5	2.0	167.5	1.6	129.5	1.5	61.5	2.5	141.5	3.0	106.5	2.4	162	2.9	147	2.5	86	2.3	665[2]	39.8	4.VI	21	38	116	34	11	5	25	163	158	123	16	5.4	73	17

Tarnów $\varphi = 50°02'$ $\lambda = 20°59'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	992.2	1009.7	970.5	1018.4	3.1	−2.4	8.8	20	−17.3	31	−0.6	2.0	0.3	0.5	4.8	4.9	4.8	4.8	80	69	75	75	1.2	2.4	1.7	1.8	7.3	6.6	7.4	7.1
II	990.6	1007.5	962.6	1017.0	0.6	−4.7	7.5	13	−13.2	25	−3.2	−1.1	−1.8	−2.0	4.1	4.4	4.5	4.3	82	77	83	81	0.9	1.4	1.0	1.1	9.0	8.0	8.6	8.5
III	985.4	1002.0	967.1	1011.6	2.5	−4.3	14.8	31	−13.4	27	−2.7	1.5	−1.0	−0.8	4.5	4.8	4.8	4.7	83	68	80	77	1.0	2.4	1.2	1.5	8.3	7.5	7.1	7.6
IV	989.0	1001.3	964.5	1014.2	16.5	5.9	26.7	23	0.2	30	8.7	15.0	10.2	11.0	8.5	8.4	8.7	8.5	75	54	71	67	3.1	10.3	4.4	5.9	6.5	6.9	5.6	6.3
V	988.7	995.9	974.6	1013.8	16.2	7.1	23.5	8	−1.2	2	10.1	14.3	10.6	11.4	10.8	10.5	10.8	10.7	85	64	83	77	1.9	6.3	2.4	3.5	7.6	8.6	6.5	7.6
VI	993.4	1002.3	983.8	1018.5	19.0	9.4	29.5	23	2.5	7	13.2	17.3	13.4	14.3	12.7	12.4	12.6	12.6	81	64	80	75	3.2	8.9	3.5	5.2	6.0	7.7	6.0	6.6
VII	990.4	1000.8	978.9	1015.2	21.4	11.2	29.6	26	7.4	9, 30	14.5	20.2	15.2	16.3	13.9	13.3	14.6	13.9	84	57	83	75	2.9	10.9	3.0	5.6	6.2	7.5	6.2	6.6
VIII	991.9	998.7	982.5	1016.6	23.8	12.6	30.7	13	6.7	29	15.9	22.3	16.8	18.0	15.3	15.3	15.7	15.4	84	58	81	74	2.9	12.3	3.9	6.4	6.3	6.5	4.6	5.8
IX	992.3	1004.7	979.1	1017.3	18.7	8.0	27.7	4	2.3	27	10.7	17.3	12.4	13.2	10.6	11.2	11.4	11.1	83	58	80	74	2.7	9.4	3.5	5.2	6.2	6.4	4.8	5.8
X	997.4	1010.1	983.8	1023.0	13.5	3.2	19.5	2	−3.4	16	4.9	12.4	6.7	7.7	8.3	9.9	9.1	9.1	94	69	90	84	0.6	4.8	1.0	2.1	7.0	5.4	3.7	5.4
XI	991.6	1006.4	977.5	1017.3	8.0	2.8	17.0	8	−1.7	24	3.9	6.9	4.9	5.2	2.2	7.9	7.6	7.6	88	79	86	84	1.0	2.7	1.3	1.7	7.9	8.5	8.7	8.4
XII	991.3	1018.3	950.6	1017.9	−1.4	−6.6	5.3	13	−17.5	26	−4.7	−2.7	−4.2	−4.0	3.7	4.0	3.9	3.9	81	77	82	80	0.9	1.3	0.9	1.0	8.0	8.4	7.6	8.0
Rok	991.2	1018.3	950.6	1016.7	11.8	3.5	30.7	13, VIII	−17.5	26, XII	5.9	10.4	7.0	7.6	8.7	8.9	9.0	8.9	83	66	81	77	1.9	6.1	2.3	3.4	7.2	7.3	6.4	7.0

Jakubowice $\varphi = 50°01'$ $\lambda = 17°51'$

I	–	–	–	–	2.3	−2.7	7.4	20	−15.9	31	−1.1	1.3	−0.7	−0.3	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.2	7.0	7.1
II	–	–	–	–	0.7	−5.0	5.0	13	−12.0	1, 26	−3.7	−0.9	−2.1	−2.2	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.5	6.9	8.1
III	–	–	–	–	2.5	−3.1	14.7	31	−7.6	9	−2.4	1.5	−0.6	−0.5	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.8	5.5	7.0
IV	–	–	–	–	14.9	5.6	26.5	23, 25	1.2	2	7.6	13.5	9.5	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.4	4.9	5.9
V	–	–	–	–	15.1	6.5	22.7	8	2.0	1, 3	9.6	13.3	10.2	10.8	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.3	7.5	7.9
VI	–	–	–	–	19.7	9.0	30.7	23	2.0	2	12.7	17.7	13.6	14.4	–	–	–	–	–	–	–	–	–	–	–	–	5.2	6.5	5.1	5.6
VII	–	–	–	–	21.2	10.2	29.8	26	4.7	5	13.5	19.8	14.9	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.8	5.6	6.2
VIII	–	–	–	–	23.9	11.4	30.3	7	4.8	31	14.6	22.0	16.4	17.4	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.3	4.3	5.5
IX	–	–	–	–	18.0	6.9	30.1	4	−0.1	15	9.0	16.2	11.3	12.0	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.4	4.0	5.6
X	–	–	–	–	13.4	3.8	24.4	4	−2.6	22	5.4	12.5	7.0	8.0	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.9	4.3	5.4
XI	–	–	–	–	6.4	1.4	17.8	7	−3.0	28	2.3	5.3	3.3	3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.8	8.4	8.7
XII	–	–	–	–	−1.7	−7.1	5.8	13	−16.1	23	−5.4	−3.0	−4.8	−4.5	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.1	6.1	7.4
Rok	–	–	–	–	11.4	3.1	30.7	23, VI	−16.1	23, XII	5.2	9.9	6.5	7.0	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.2	5.8	6.7

Ożańsk $\varphi = 50°01'$ $\lambda = 22°35'$

I	–	–	–	–	2.2	−2.4	8.8	22	−15.6	31	−0.7	1.1	−0.4	−0.1	5.2	5.8	5.2	5.4	8.6	8.6	8.5	8.6	0.8	1.0	0.9	0.9	7.9	6.3	6.1	6.8
II	–	–	–	–	−0.9	−5.6	2.8	13	−15.1	25	−4.1	−2.0	−2.9	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.6	8.7	8.9
III	–	–	–	–	1.3	−5.3	13.4	5, 6	−15.1	20	−3.7	0.0	−1.7	−1.8	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.4	7.0	7.4
IV	–	–	–	–	16.2	5.6	26.8	23	0.0	2	7.6	14.5	10.1	10.6	8.4	8.5	8.4	8.4	8.0	5.5	6.9	6.8	2.3	9.4	4.7	5.5	5.4	5.7	4.3	5.1
V	–	–	–	–	16.0	7.3	23.7	14	−0.8	1	10.0	14.5	11.0	11.6	11.1	11.3	11.3	11.2	8.8	6.7	8.4	8.0	1.5	5.9	2.2	3.2	7.6	7.3	6.4	7.1
VI	–	–	–	–	18.5	9.8	27.6	16, 23-25	2.7	6	13.1	17.1	13.8	14.4	13.1	12.9	12.9	13.0	8.4	6.6	8.0	7.7	2.7	8.0	3.8	4.8	6.4	6.9	6.2	6.5
VII	–	–	–	–	20.5	11.2	29.2	27	7.6	30	14.3	19.1	15.2	16.0	14.2	13.9	14.5	14.2	8.7	6.4	8.3	7.8	2.3	8.7	3.0	4.7	5.6	6.5	5.0	5.7
VIII	–	–	–	–	22.9	12.9	29.4	7, 13	6.0	31	15.4	21.6	17.4	18.0	15.5	15.6	16.0	15.7	8.7	6.1	8.0	8.6	2.3	10.9	4.2	5.8	5.4	6.2	3.7	5.1
IX	–	–	–	–	18.0	8.0	27.5	5	2.3	26	10.4	16.5	12.1	12.8	10.8	11.6	11.5	11.3	8.6	6.3	8.2	7.7	2.0	7.9	3.0	4.3	5.9	6.1	5.1	5.7
X	–	–	–	–	13.2	3.2	18.2	4	−4.2	24	5.0	11.9	7.2	7.8	8.4	9.9	9.0	9.1	9.3	7.0	8.6	8.3	0.6	4.2	1.4	2.1	5.6	5.7	3.2	4.8
XI	–	–	–	–	6.8	1.9	16.8	1	−1.7	18	3.2	5.6	3.8	4.1	7.5	8.1	7.7	7.8	9.5	8.8	9.4	9.2	0.4	1.3	0.6	0.8	8.8	8.3	7.5	8.2
XII	–	–	–	–	−2.2	−7.0	5.4	13, 14	−15.8	23	−5.0	−3.5	−4.7	−4.5	4.0	4.2	4.0	4.1	8.7	8.4	8.6	8.6	0.5	0.8	0.6	0.6	7.9	8.6	7.5	8.0
Rok	–	–	–	–	11.0	3.3	29.4	7, 13, VIII	−15.8	23, XII	5.5	9.7	6.7	7.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.0	5.9	6.6

Jarosław $\varphi = 50°01'$ $\lambda = 22°42'$

I	–	–	–	–	3.1	−2.1	9.8	22	−14.6	31	−0.3	1.7	0.2	0.4	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.4	6.6	7.5
II	–	–	–	–	−0.3	−4.9	3.7	13	−13.3	25	−3.8	−1.2	−2.5	−2.5	–	–	–	–	–	–	–	–	–	–	–	–	9.2	9.3	8.9	9.1
III	–	–	–	–	2.1	−4.4	14.4	31	−16.0	20	−3.4	0.8	−1.7	−1.5	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.5	7.3	8.0
IV	–	–	–	–	16.8	5.6	26.7	23	−0.2	30	7.4	15.1	10.8	11.0	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.5	4.1	4.9
V	–	–	–	–	16.8	8.1	25.5	14	0.2	1	10.2	15.3	11.8	12.3	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.5	6.9	7.3
VI	–	–	–	–	19.2	10.4	28.2	23	3.5	7	13.4	17.5	14.6	15.0	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.2	6.5	6.6
VII	–	–	–	–	21.1	11.9	30.0	27	7.8	30	14.7	19.7	16.0	16.6	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.1	5.6	6.2
VIII	–	–	–	–	23.6	13.2	30.9	13	6.9	1	15.5	22.3	17.8	18.4	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.7	4.0	5.4
IX	–	–	–	–	18.5	8.4	28.3	5	1.8	15	10.1	17.1	12.7	13.2	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.5	4.7	5.6
X	–	–	–	–	13.8	2.7	19.0	2	−4.4	16	4.2	12.4	7.5	7.9	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.7	2.7	5.1
XI	–	–	–	–	7.4	2.4	16.8	1	−2.1	18	3.5	6.2	4.3	4.6	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.5	7.9	8.4
XII	–	–	–	–	−1.5	−6.5	6.1	13	−16.0	29	−4.9	−3.0	−4.4	−4.2	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.9	8.3	8.5
Rok	–	–	–	–	11.7	3.7	30.9	13, VIII	−16.0	20 II, 29 XII	5.6	10.3	7.3	7.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.4	6.1	6.9

Tarnów $H_s = 209\,m$ $H_b = 209{,}1\,m$ $h_w = 13{,}6\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU °D, °mD																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C					Temperatura T				Wiatr v				Opad R					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	≥ 10 m/s	≥ 15 m/s	☁	●	0.1 ≤ R < 1.0	1.0 ≤ R < 10.0	R ≥ 10.0	▬	⊞	R ≥ 0
I	2	3.2	4	3.0	2	3.0	1.5	2.3	29.5	2.5	9	2.2	24	3.0	12	3.8	9	2.6	29	5.5	25	2	4	21	·	·	·	2	16	15	9	·	·	17	·
II	10.5	3.8	5	2.4	9.5	2.8	3.5	2.6	4.5	2.0	5	5.2	17	4.9	18	4.5	11	3.4	34	5.1	17, 19	3	12	25	·	2	·	·	18	20	10	·	1	23	·
III	11	3.0	10	3.8	10.5	2.1	15.5	2.5	12.5	2.8	1.5	2.3	5.5	3.8	12.5	4.0	14	2.6	40	6.2	23	4	15	23	·	1	·	1	17	18	10	·	2	24	·
IV	4.5	3.7	5.5	3.0	4.5	3.4	9	2.5	11	4.1	8	2.1	9.5	2.1	20	3.6	18	2.5	44	6.8	6	·	·	·	4	1	·	5	12	12	11	·	2	·	2
V	9.5	1.8	4.5	1.6	5.5	1.3	7	1.6	6.5	2.8	4	1.7	13.5	5.0	20.5	2.8	22	2.1	101	9.7	21	·	·	2	·	1	·	·	16	25	22	·	1	·	4
VI	17.5	2.1	5	2.3	1.5	1.0	3	1.8	3	1.5	0.5	1.0	11.5	3.3	28	2.8	20	2.0	139	71.4	4	·	·	·	6	·	·	3	12	12	9	3	·	·	4
VII	7	1.7	7	1.7	7	1.5	4	2.2	4.5	1.8	2	1.0	18.5	2.8	25	2.5	18	1.8	148	27.6	19	·	·	·	5	·	·	3	11	19	15	6	1	·	14
VIII	2.5	1.6	1.5	2.0	8.5	1.5	5.5	2.4	4	2.0	6.5	1.4	10	2.8	26.5	2.9	28	1.7	23	11.3	16	·	·	·	12	·	·	2	4	12	6	1	1	·	1
IX	·	·	2	1.5	11	1.9	5	1.8	10	1.9	7	1.9	15	3.1	19	3.1	21	1.9	51	16.3	17	·	·	·	6	·	·	5	11	10	7	2	5	·	1
X	1.5	2.3	5	2.6	1.5	1.7	8	1.5	·	·	1	1.5	8	2.9	10.5	1.9	44	1.1	6	3.7	31	·	·	8	·	·	·	6	9	4	2	·	16	·	·
XI	4	1.8	5	2.2	1.8	3.3	21.5	3.7	4.5	4.2	2	2.8	13	2.1	12	2.2	10	2.6	64	13.0	15	·	1	5	·	·	·	2	21	16	11	3	9	5	·
XII	8	2.6	15.5	3.2	8	1.9	7.5	3.7	9.5	3.9	8.5	2.8	10.5	2.6	13.5	2.4	12	2.6	30	9.0	14	9	13	30	·	·	·	1	19	13	8	·	3	18	·
Rok	78	2.3	70	2.4	10.1	2.1	9.1	2.4	99.5	2.5	55	2.2	156	3.2	217.5	3.0	227	2.2	709	71.4	4.VI	18	45	114	33	5	·	30	166	176	120	15	41	87	26

Jakubowice $H_s = 319\,m$ $h_w = 14\,m$

I	5	5.0	·	·	·	·	·	·	2.8	4.6	35.5	5.1	4.5	3.6	14	6.1	6	4.7	28	6.6	28	2	4	22	·	2	·	1	16	14	8	·	·	4	–
II	14.5	2.4	5.5	1.5	·	·	·	·	11	6.0	10	5.6	8.5	5.2	21.5	6.9	13	4.3	37	7.8	13	4	12	23	·	6	2	1	18	19	12	·	2	21	–
III	19	5.2	7	3.3	2.5	3.4	2	2.5	13.5	3.0	12	3.7	2.5	4.6	16.5	4.8	18	3.3	78	16.9	5	·	9	23	·	3	·	·	14	17	8	3	4	13	–
IV	9	3.0	1.5	3.0	4	1.9	4.5	2.0	15.5	5.1	11.5	4.4	8	3.3	21	4.9	15	3.4	34	10.0	4	·	·	·	6	4	·	7	11	13	8	1	1	·	–
V	7.5	2.2	5.5	2.3	5.5	2.1	7.5	2.6	7	2.3	12.5	2.6	8.5	2.9	22	3.1	22	2.0	18.2	34.2	13	·	·	·	·	·	·	1	20	24	20	7	1	·	–
VI	19	2.4	5	2.0	3.5	1.3	1.5	2.3	4	2.2	6	2.2	6.5	2.7	26.5	4.5	18	2.5	40[2]	27.0	1	·	·	·	6	1	·	5	11	9	5	1	·	·	–
VII	13	1.5	1	2.0	2	1.0	1.5	1.3	7	1.2	13.5	2.4	10	1.6	19	2.3	26	1.4	62	25.2	17	·	·	·	7	1	·	4	11	15	11	2	·	·	–
VIII	4	1.5	·	·	2	1.0	7	2.4	7.5	2.5	12.5	2.3	8	1.9	16	3.1	36	1.5	46	16.5	15	·	·	·	12	1	·	1	6	11	8	1	1	·	–
IX	5	1.2	1	1.5	4	1.1	·	·	18.5	2.6	9.5	3.4	4	1.5	17	2.8	31	1.6	57	19.8	17	·	·	1	4	·	·	7	10	11	7	2	7	·	–
X	12.5	2.1	2.5	1.0	3.5	1.0	0.5	1.0	10.5	2.0	5.5	1.0	1	3.0	16	3.6	41	1.3	46	18.8	31	·	·	2	·	·	·	9	11	7	4	2	16	·	–
XI	12.5	2.9	1	5.0	1	2.0	7.5	2.9	9.5	4.2	8	1.6	2.5	1.4	16	3.6	32	2.0	76	16.8	19	·	2	11	·	·	·	·	23	16	14	2	10	1	–
XII	24.5	3.0	·	·	·	·	·	·	11	4.3	16.5	3.9	1.5	1.0	11.5	4.5	28	2.6	29	6.9	31	8	15	29	·	3	·	3	17	19	8	·	4	16	–
Rok	145.5	2.7	30	1.8	28	1.2	27	1.4	143	3.3	153	3.2	65.5	2.7	217	4.2	286	2.6	715[2]	34.2	13.V	14	42	111	35	21	2	39	168	175	113	21	46	55	–

Ożańsk $H_s = 250\,m$ $h_w = 20{,}5\,m$

I	1	4.0	2	6.0	2.5	5.2	0.5	2.0	19	6.5	22	7.4	23.5	6.0	1.5	6.7	21	5.0	22	8.4	13	2	6	23	·	1.2	1	2	12	12	5	·	·	7[2]	·
II	3.5	8.6	3	4.3	12.5	4.5	3	5.0	2	7.0	8.5	10.3	25.5	11.6	4	9.8	22	6.6	17	4.3	12	3	15	28	·	10	7	·	22	15	6	·	1	28	·
III	0.5	6.0	2.5	8.4	13	6.1	4.5	5.1	7.5	4.1	6	6.7	13.5	8.6	5.5	6.5	40	3.8	24	4.3	12	5	19	27	·	5	1	2	17	16	7	·	·	24	·
IV	·	·	3	2.7	4.5	5.9	15.5	4.7	7	3.3	9	4.4	6	5.8	6	6.0	39	2.7	58	13.1	27	·	·	·	3	2	1	6	3	10	9	3	2	·	1
V	·	·	·	·	·	·	4	2.5	4.5	3.6	11.5	3.8	13.5	8.2	4.5	3.5	55	2.5	89	13.7	20	·	·	2	·	3	2	·	11	25	16	2	·	·	4
VI	·	·	1	2.0	0.5	4.0	0.5	4.0	1.5	4.0	11	5.3	18	5.9	7.5	4.1	50	2.3	118	34.8	1	·	·	·	6	1	·	1	8	13	12	5	2	·	3
VII	·	·	·	·	1	2.0	·	·	0.5	4.0	12.5	4.2	11.5	3.9	2.5	2.0	6.5	1.1	114	28.6	7	·	·	·	3	·	·	3	8	15	14	3	·	·	6
VIII	·	·	·	·	0.5	2.0	3	3.3	4	2.8	14.5	4.6	9.5	6.1	3.5	5.1	58	1.8	45	9.9	18	·	·	·	9	1	·	1	2	13	9	·	2	·	3
IX	·	·	·	·	·	·	3	3.3	5	6.0	12.5	5.4	21.5	4.8	3	7.3	45	2.6	49	14.0	8	·	·	·	2	3	·	2	6	9	8	2	9	·	2
X	·	·	1	4.0	3	3.0	1.1	4.1	1.5	2.7	9.5	6.1	9	5.3	1	8.0	57	1.9	4	1.7	19	·	·	6	·	1	·	6	6	3	2	·	10	·	·
XI	·	·	0.5	4.0	1.5	7.0	2.3	2.4	3.5	5.1	2.5	4.0	9.5	5.7	5	4.8	31	4.3	4.5	9.5	25	·	·	7	·	5	2	·	17	15	12	·	6	1	·
XII	1.5	3.3	2.5	2.8	6.5	4.2	·	·	5	12.0	1.5	7.7	12	4.8	2.5	4.4	48	3.0	24	6.5	30	9	15	31	·	5	3	·	20	12	5	·	4	16	·
Rok	6.5	1.8	15.5	2.8	5.9	3.7	6.8	3.4	6.1	5.1	134.5	5.8	17.3	6.4	46.5	5.7	531	3.1	609	34.8	1.VI	19	55	124	23	48	17	23	132	158	105	15	36	76[2]	19

Jarosław $H_s = 204\,m$ $h_w = 19\,m$

I	6	4.2	·	·	6	3.0	1.5	1.7	3.5	3.6	35.5	3.7	18.5	3.8	1.3	4.2	9	3.8	28	8.0	13	2	6	20	·	·	·	2	17	10	8	·	·	–	·
II	4.5	8.7	5	3.4	5	2.0	14	3.9	1	3.0	12	7.3	16	2.8	21.5	5.8	5	5.5	43	5.1	12	2	15	27	·	9	3	1	24	15	10	·	1	28	·
III	14	4.6	1	3.0	6	6.1	2.2	3.2	1.0	3.5	8	3.5	12	4.7	9	3.4	11	3.5	48	8.3	12	3	14	24	·	4	·	1	21	11	10	·	1	26[2]	·
IV	8.5	5.9	3	1.0	5.5	3.4	15.5	3.2	1.2	4.2	7.5	4.1	14.5	4.0	9.5	4.4	14	3.3	49	19.2	6	·	·	1	4	2	1	6	4	7	7	2	2	·	1
V	9.5	3.6	3	4.7	·	·	9	3.6	2	1.5	8	3.9	3.4	4.9	14.5	3.8	13	3.6	101	16.3	10	·	·	·	1	3	2	·	12	19	16	2	3	·	4
VI	21	5.5	1.5	4.0	1.5	4.3	1	2.0	2.5	2.6	7.5	3.0	24.5	3.9	14.5	3.6	16	3.6	125	44.7	1	·	·	·	7	4	·	1	9	15	12	4	2	·	3
VII	13.5	5.8	3	2.7	3.5	2.4	5.5	2.8	6.5	4.0	5.5	2.4	2.8	3.6	4.5	3.4	23	2.8	106	25.0	19	·	·	·	4	4	·	2	8	15	13	3	3	·	5
VIII	6	6.8	·	·	3	3.3	2	3.0	8	2.5	5	2.3	3.4	3.5	3	5.3	32	2.4	52	15.0	5	·	·	·	13	2	·	2	4	12	11	1	2	·	6
IX	4.5	3.0	·	·	2	2.0	2.5	2.7	7	2.1	12.5	4.3	2.8	3.5	8.5	4.6	20	2.7	47	15.0	8	·	·	·	2	2	1	3	8	12	8	2	5	·	3
X	6.5	4.3	·	·	4	2.0	1.2	3.1	1.1	2.3	2.5	4.1	1.7	4.0	9	2.4	3.1	2.1	3	1.1	19	·	·	9	·	1	·	6	6	5	2	·	13	·	·
XI	8.5	2.2	1.5	2.0	6	5.9	3.5	5.8	6	3.1	4.5	5.2	13.5	3.7	4	1.5	11	4.0	52	12.3	25	·	·	3	·	5	·	·	18	17	10	1	7	1[2]	·
XII	7.5	4.1	5	2.6	9	3.7	1.2	2.2	4	2.2	15.5	6.0	2.0	3.6	1.0	3.2	1.0	3.3	37	11.1	31	9	16	30	·	3	·	·	22	14	5	2	7	17	·
Rok	11.0	4.9	2.3	2.0	51.5	3.2	13.7	3.1	73.5	2.9	12.4	4.2	26.0	4.2	12.1	3.8	19.5	3.4	67.6	44.7	1.VI	16	51	114	31	39	7	24	153	152	112	17	46	–	22

Pszczyna $\varphi = 50°00'$ $\lambda = 18°55'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.8	-3.2	9.3	22	-18.4	31	-1.2	1.8	-0.4	0.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.8	6.9	6.5
II	–	–	–	–	0.5	-5.3	7.0	12	-15.1	3	-3.5	-1.0	-2.2	-2.2	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.1	8.1	8.5
III	–	–	–	–	2.8	-4.6	15.2	31	-11.5	25	-3.1	1.4	-1.3	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.2	6.6	6.9
IV	–	–	–	–	15.2	4.9	26.5	23, 24	0.6	6	7.8	13.7	9.3	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.9	5.0	5.7
V	–	–	–	–	15.2	6.2	22.5	31	-1.6	1	9.0	13.4	9.9	10.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.4	7.3	7.3
VI	–	–	–	–	19.5	9.1	30.1	16	1.9	2	12.2	17.6	13.3	14.1	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.9	5.5	5.5
VII	–	–	–	–	21.1	10.5	30.5	26	5.8	30	13.6	19.3	14.8	15.6	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.0	5.5	5.7
VIII	–	–	–	–	23.6	11.9	30.7	7	5.8	29	14.2	21.6	15.9	16.9	–	–	–	–	–	–	–	–	–	–	–	–	4.2	4.4	3.5	4.0
IX	–	–	–	–	18.8	6.8	28.9	4	0.2	25	9.3	16.7	11.5	12.2	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.1	3.3	4.5
X	–	–	–	–	13.4	2.9	23.5	4	-2.2	25	5.6	12.0	7.6	8.2	–	–	–	–	–	–	–	–	–	–	–	–	6.1	4.6	4.8	5.2
XI	–	–	–	–	6.2	1.4	18.5	7	-2.4	23	2.4	5.2	3.3	3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.5	8.9	8.3
XII	–	–	–	–	-1.9	-7.0	7.8	13	-19.3	29	-5.1	-3.1	-5.0	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.6	7.9	8.1
Rok	–	–	–	–	11.4	2.8	30.7	7.VIII	-19.3	29.XII	5.1	9.9	6.4	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.3	6.1	6.3

Czernichów $\varphi = 50°00'$ $\lambda = 19°41'$

I	–	–	–	–	3.5	–	11.8	25	–	–	-1.5	2.2	-0.4	0.0	–	–	–	–	–	–	–	–	–	–	–	–	8.7	6.5	8.4	7.9
II	–	–	–	–	1.0	–	7.2	7	–	–	-3.3	-0.4	-2.0	-1.9	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.1	9.5	8.9
III	–	–	–	–	3.0	-4.3	15.4	31	-12.2	26	-3.1	1.9	-0.7	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.1	8.2	7.7
IV	–	–	–	–	16.0	4.8	26.9	24	0.4	3	7.4	14.4	9.8	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.9	6.3	6.1
V	–	–	–	–	16.0	6.7	24.7	8	-0.2	1	9.5	14.7	10.8	11.4	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.4	8.0	7.7
VI	–	–	–	–	19.7	9.6	30.9	16	3.6	2	12.7	18.7	14.2	15.0	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.8	6.6	6.7
VII	–	–	–	–	22.0	11.0	31.3	26	5.6	6	14.5	21.0	16.2	17.0	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.1	6.7	6.3
VIII	–	–	–	–	24.4	12.5	33.3	7	6.0	31	15.1	23.6	17.2	18.3	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.8	6.5	6.0
IX	–	–	–	–	19.1	7.1	30.6	4	0.5	25	8.9	17.8	11.9	12.6	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.0	7.1	7.2
X	–	–	–	–	13.5	3.8	20.4	1	-2.2	22, 23	4.7	12.6	7.3	8.0	–	–	–	–	–	–	–	–	–	–	–	–	8.9	5.5	6.4	6.9
XI	–	–	–	–	7.1	1.7	18.2	7	-1.9	25	3.0	6.2	3.9	4.2	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.4	8.6	8.7
XII	–	–	–	–	-1.4	-6.7	7.0	13	-20.2	29	-5.2	-2.7	-4.3	-4.1	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.5	8.6	8.8
Rok	–	–	–	–	12.0	–	33.3	7.VIII	-20.2	29.XII	5.2	10.8	7.0	7.5	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.9	7.6	7.4

Wieliczka $\varphi = 50°00'$ $\lambda = 20°03'$

I	–	–	–	–	3.8	-2.4	11.4	22	-14.6	31	-0.3	2.6	0.4	0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.3	8.2	7.9
II	–	–	–	–	1.2	-4.4	8.2	12, 13	-11.7	25	-3.1	-0.3	-1.9	-1.8	–	–	–	–	–	–	–	–	–	–	–	–	9.4	9.0	9.3	9.2
III	–	–	–	–	3.0	-4.5	15.8	31	-13.6	26	-3.0	1.8	-0.8	-0.7	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.0	7.8	8.3
IV	–	–	–	–	15.9	6.2	26.1	19, 23	0.6	1	8.7	14.3	10.1	10.8	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.8	6.3	6.7
V	–	–	–	–	15.7	7.3	23.7	19	0.1	1	9.9	14.2	11.0	11.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	19.1	9.9	29.6	23	3.0	7	13.5	17.6	13.8	14.7	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.7	6.6	7.2
VII	–	–	–	–	21.4	11.7	31.0	26	7.1	30	15.0	19.9	15.3	16.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.5	7.0	7.1
VIII	–	–	–	–	23.9	13.3	32.5	7	6.4	27	16.4	22.6	17.3	18.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	18.7	7.9	30.0	4	2.1	27	10.6	17.1	12.1	13.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	12.8	3.8	19.4	1	-3.3	16	4.7	12.0	7.2	7.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	7.0	1.8	17.6	7	-2.0	24, 28	2.8	6.1	3.9	4.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-1.1	-6.7	6.6	12	-21.2	29	-4.9	-2.4	-4.0	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	11.8	3.7	32.5	7.VIII	-21.2	29.XII	5.9	10.5	7.0	7.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Bochnia-Chodenice $\varphi = 49°59'$ $\lambda = 20°24'$

I	–	–	–	–	3.7	-3.5	11.3	22	-15.0	30	-1.2	2.7	-0.1	0.3	4.9	5.3	5.3	5.2	8.4	7.0	8.4	7.9	1.0	2.5	1.1	1.5	7.3	6.4	7.5	7.1
II	–	–	–	–	1.0	-4.8	7.5	12	-14.0	25	-2.9	-0.6	-1.8	-1.8	4.5	4.5	4.7	4.6	8.8	7.7	8.6	8.4	0.7	1.5	0.9	1.0	9.1	8.4	9.1	8.9
III	–	–	–	–	2.9	-5.2	15.3	31	-16.8	27	-3.3	1.7	-1.0	-0.9	4.4	5.2	4.9	4.8	8.6	7.2	8.2	8.0	0.8	2.2	1.1	1.4	8.5	7.6	6.7	7.6
IV	–	–	–	–	16.0	4.3	26.0	23	-0.1	2	8.4	14.2	9.2	10.2	9.1	9.3	9.3	9.2	8.2	6.1	7.9	7.4	2.2	8.5	2.8	4.5	6.7	6.9	5.1	6.2
V	–	–	–	–	15.9	6.4	23.3	8	-1.0	2	9.9	13.9	10.1	11.0	11.0	10.7	11.0	10.9	8.8	6.8	8.8	8.1	1.5	5.7	1.7	3.0	7.9	9.0	6.7	7.9
VI	–	–	–	–	19.0	8.6	28.9	16, 23	3.2	7, 9	13.1	17.2	12.9	14.0	13.0	12.9	13.1	13.0	8.3	6.5	8.6	7.8	2.8	8.2	2.5	4.5	5.9	7.5	6.4	6.6
VII	–	–	–	–	21.5	10.5	31.0	26	4.6	5	14.5	19.9	14.7	16.0	14.1	13.5	14.8	14.1	8.4	5.8	8.7	7.6	2.6	10.4	2.2	5.1	6.5	7.1	6.1	6.6
VIII	–	–	–	–	23.6	11.4	31.3	7	4.9	29	15.4	22.2	16.1	17.4	15.5	15.5	15.9	15.6	8.8	5.8	8.6	7.7	2.2	12.0	2.8	5.7	6.0	6.2	3.6	5.3
IX	–	–	–	–	18.9	6.3	28.6	4	-0.3	27	9.8	17.2	11.3	12.4	10.8	11.6	11.6	11.3	8.9	6.0	8.7	7.9	1.8	8.9	2.4	4.4	6.7	6.0	3.4	5.4
X	–	–	–	–	13.0	2.2	19.6	1	-5.1	16	4.1	12.1	6.0	7.0	8.1	10.1	8.9	9.0	9.6	7.2	9.4	8.7	0.4	4.2	0.6	1.7	7.4	5.4	4.7	5.8
XI	–	–	–	–	7.3	1.3	18.9	8	-2.4	18	2.4	6.6	4.3	4.4	7.0	7.9	7.8	7.6	9.4	8.1	9.2	8.9	0.4	2.6	0.7	1.2	8.3	8.3	8.2	8.3
XII	–	–	–	–	-1.0	-7.5	8.2	9	-23.0	29	-5.4	-2.4	-4.4	-4.2	3.9	4.1	4.2	4.1	8.8	7.9	8.8	8.5	0.7	1.5	0.7	1.0	8.2	8.3	7.6	8.0
Rok	–	–	–	–	11.8	2.5	31.3	7.VIII	-23.0	29.XII	5.4	10.4	6.4	7.2	8.9	9.2	9.3	9.1	8.8	6.8	8.7	8.1	1.4	5.7	1.6	2.9	7.4	7.3	6.3	7.0

Pszczyna $H_S = 270\,m$ h_w = 18,0m I–VI, 16,3m VII–XII 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◔	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	11	2.1	·	·	·	·	·	·	7	2.0	54	2.5	5	1.8	13	2.5	3	2.3	52	7.5	11	3	5	22	-	1	·	1	11	14	13	·	1	8	·
II	11	2.9	7	1.9	5	2.0	2	1.0	5	1.6	34	2.4	5	2.4	7	1.6	8	2.0	43	5.0	12, 19	4	12	25	·	·	·	·	18	21	14	·	3	24	·
III	12	1.4	6	3.7	16	1.9	8	1.4	6	1.5	19	1.8	3	1.7	10	1.8	13	1.6	67	15.5	12	2	11	26	·	·	·	4	15	16	11	2	3	10	·
IV	4	1.8	7	1.3	7	1.6	9	1.6	8	1.8	28	2.1	3	2.3	9	1.9	15	1.5	81	21.2	6	·	·	·	6	·	·	8	12	9	8	4	3	·	·
V	3	2.0	·	·	3	1.3	7	1.4	2	1.5	42	1.7	7	1.6	17	1.8	12	1.5	203	25.0	13	·	·	2	·	·	·	·	11	25	18	7	1	·	4
VI	8	2.0	5	2.0	·	·	9	1.2	2	1.0	17	1.6	4.5	1.9	28.5	1.6	16	1.4	60	27.4	1	·	·	·	6	·	·	6	10	14	8	2	·	·	3
VII	11	1.5	4	1.2	·	·	1	1.0	1	1.0	17.5	2.0	13	1.7	34.5	1.3	11	1.4	78	31.4	17	·	·	·	5	·	·	4	7	13	10	2	·	·	9
VIII	5	1.2	9	1.4	2	1.0	1	2.0	·	·	19	2.1	5	2.0	42	1.3	10	1.4	59	11.6	15	·	·	·	14	1	·	9	3	14	10	3	1	·	6
IX	1	1.0	16	1.1	5	2.2	·	·	·	·	19	2.2	15	1.6	23	1.4	11	1.4	73	20.2	17	·	·	·	4	·	·	9	9	11	10	2	5	·	1
X	3	1.0	25	1.1	1	3.0	·	·	·	·	8	1.9	3	1.3	30	1.3	23	1.0	26	10.0	28	·	·	5	·	·	·	8	10	9	5	1	23	·	·
XI	6	1.2	30.5	1.3	5.5	1.6	5	1.6	1	1.0	12	2.7	·	·	20	1.1	10	1.3	111	23.8	15	·	2	11	·	·	·	1	19	15	14	4	16	5	·
XII	6.5	1.2	22.5	1.7	2	2.0	4	1.5	·	·	24	2.8	4	2.0	22	1.2	8	1.7	55	15.0	13	9	17	28	·	·	·	1	20	18	11	1	8	24	·
Rok	81.5	1.6	132	1.4	46.5	1.4	46	1.1	32	1.0	293.5	2.2	67.5	1.7	256	1.6	140	1.5	908	31.4	17.VII	18	47	119	35	2	·	51	145	179	132	28	64	71	23

Czernichów $H_S = 218\,m$ h_w = 16m I–X, 17m XI–XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	4	3.0	7	2.9	2	3.5	1	3.0	2.5	3.2	20.5	3.5	36	2.9	9	2.9	11	2.7	57	13.4	29	–	5	–	·	·	·	·	15	15	13	1	–	19	·
II	4	4.8	7	3.4	7	4.0	·	·	1.5	5.3	10.5	6.5	26.5	4.5	16.5	5.2	11	4.2	49	7.8	16	–	10	–		4	1	·	20	15	11	·	–	24	·
III	4	7.0	28	3.6	4	4.8	4	3.8	4	1.5	5.5	3.3	21.5	4.2	8	3.8	14	3.3	61	13.4	12	3	6	25	·	2		2	16	13	13	2	–	16	·
IV	·	·	12	2.9	10	2.2	·	·	6	3.0	13.5	2.7	24.5	3.0	16	3.7	8	2.7	84	35.1	6	·	·	·	8	1	·	7	13	14	11	3	8	·	2
V	·	·	5	3.2	·	·	2	2.5	5	2.4	27.5	2.6	36	3.6	10.5	3.2	7	2.9	157	18.0	13		·	1	·	2	·	1	19	24	20	6	·	·	4
VI	7	3.1	9.5	2.7	6	2.9	4.5	3.6	·	·	0.5	3.0	37.5	2.9	17	3.0	8	2.7	71	27.0	1	·		·	6	·	·	3	12	13	8	3		·	3
VII	4	2.0	6	1.7	4	2.0	3	3.0	0.5	4.0	9	2.3	46.5	2.5	14	2.4	6	2.2	185	53.0	17	·	·	·	10	·		2	9	14	12	4	4	·	9
VIII	·	·	6	2.3	3	2.0	·	·	1	2.0	7	3.4	47	2.3	18	2.4	11	2.1	34	11.0	5	·	·	·	15	·		2	7	12	9	1	6	·	2
IX	6	2.5	9	2.4	1	3.0	2	2.5	2	4.0	8	3.5	31	3.0	23	2.2	8	2.5	61	18.5	18	·	·	·	6	1	·	·	10	15	10	2	8	·	·
X	6	2.1	17	2.7	18	2.4	1	3.5	·	·	3	2.2	22	2.4	25	2.3	1	2.4	32	15.0	6	·	·	8	·	·	·	1	13	18	6	1	23	·	·
XI	16	2.4	17	3.0	23	2.6	3	2.0	·	·	6	3.3	16	2.4	8	2.5	1	2.6	75	9.0	22, 26	·	·	9	·	·	·	·	22	19	16	·	19	6	·
XII	7	2.4	13	4.7	15	2.9	·	·	·	·	10.5	2.9	35.5	2.2	9	2.3	3	2.7	62	13.0	13	10	14	29	·	1	·	·	20	21	13	2	8	19	·
Rok	58	2.4	136.5	3.0	93	2.7	20.5	2.0	22.5	2.1	121.5	3.3	380	3.0	174	3.0	89	2.8	928	53.0	17.VII	–	35	–	45	11	1	18	176	193	142	25	–	84	20

Wieliczka $H_S = 225\,m$ $h_w = 20{,}4\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	4.5	3.0	7.5	1.9	4	1.0	2	2.0	17.5	3.2	31	2.8	12	3.4	8.5	3.6	6	2.7	28	4.4	29	2	5	19	·	·	·	–	–	15	10	·	1	16	·
II	10.5	3.1	10	1.9	4.5	1.9	·	·	9	5.9	25.5	4.6	14.5	7.5	5	8.7	5	4.6	34	8.1	13	4	10	23	·	9	5	–	–	15	10	·	3	26	·
III	7	4.3	25	3.5	4.5	1.3	4.5	1.2	12.5	2.8	19	2.3	8	7.8	5.5	4.8	7	3.2	44	8.4	12	3	11	25	·	4	3	–	–	16	10	·	5	24	·
IV	5	2.1	15.5	1.7	5	1.6	7.5	1.8	12.5	3.2	16.5	2.9	17	3.2	8	2.2	3	2.4	95	38.6	6	·	·	·	5	1	1	–	–	11	9	2	3	·	2
V	3.5	1.6	13	1.7	6	1.2	2	1.8	8.5	2.0	26.5	3.8	21.5	3.5	7	1.8	5	2.6	142	14.3	25	·	·	·	·	3	3	–	–	25	23	5	1	·	2
VI	15.5	2.8	11.5	1.3	3	1.3	·	·	5.5	1.8	23.5	2.8	21	2.6	7	2.4	3	2.3	88	36.7	1	·	·	·	6	1	·	–	–	11	9	2	·	·	1
VII	2	1.5	13.5	1.3	1.5	1.3	2	1.2	12	2.2	27	2.1	23	2.6	5	2.2	7	1.9	183	79.3	17	·	·	·	5	·	·	–	–	16	12	4	·	·	9
VIII	1	2.0	12	1.4	4	1.5	3	1.0	15	3.2	31	2.1	17.5	3.8	4.5	3.7	5	2.4	29	12.2	16	·	·	·	12	2	1	–	–	11	8	1	2	·	3
IX	1.5	3.7	9	1.4	5.5	1.5	5.5	1.2	17.5	1.9	28.5	2.6	14	3.1	5.5	2.6	3	2.2	62	16.7	18	·	·	·	6	1	·	–	–	14	11	2	8	·	1
X	1	1.0	39.5	1.3	2.5	1.2	·	·	2	2.0	19.5	1.6	9	2.6	3.5	2.1	16	1.3	13	3.4	31	·	·	4	·	·	·	–	–	18	3	·	21	·	·
XI	5	1.2	38.5	1.5	11.5	1.4	·	·	1	2.0	10.5	2.2	15	2.6	6.5	1.4	2	1.7	89	14.5	15	·	1	6	·	·	·	–	–	16	13	4	15	8	·
XII	9	2.6	24	1.8	1.5	1.0	1.5	1.7	14	3.5	20	2.2	10.5	2.2	3.5	3.3	9	2.2	57	10.3	30	10	13	26	·	·	·	–	–	18	13	1	6	19	1
Rok	65.5	2.4	219	1.7	53.5	1.4	28	1.0	127	2.8	278.5	2.7	183	3.7	69.5	3.2	71	2.5	864	79.3	17.VII	19	40	103	34	21	13	–	–	186	131	21	65	93	19

Bochnia-Chodenice $H_S = 200\,m$ $h_w = 14{,}9\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	3.5	3.0	2.5	1.6	·	·	1.5	1.0	7	1.9	23	1.8	38.5	2.7	14	4.0	3	2.5	16	3.3	29	3	6	24	·	·	·	2	15	12	9	·	1	16	·
II	6.5	2.2	5.5	2.2	6	2.7	3	1.0	5.5	2.2	9.5	5.0	29.5	4.3	16.5	4.6	2	3.7	21	3.0	13	5	11	24	·	3	·	·	21	16	9	·	·	24	·
III	7.5	3.6	15	2.5	6.5	2.0	6	2.2	9.5	2.4	7.5	3.0	21	3.8	18	3.9	2	3.1	35	8.2	12	4	13	24	·	2	·	2	17	15	11	·	2	25	·
IV	3	2.3	5	1.9	11.5	1.9	7	2.8	5	3.0	15	2.6	30	3.2	12.5	3.4	1	2.8	86	40.4	6	·	·	1	2	1	·	7	11	11	10	3	1	·	1
V	4	1.9	3.5	1.9	4.5	1.3	5.5	1.6	2	2.0	12	2.4	45.5	3.5	14	2.3	2	2.7	116	14.9	14	·	·	2	·	2	1	1	16	26	19	4	1	·	4
VI	10.5	2.7	2.5	1.4	2.5	1.4	0.5	1.0	·	·	1	4.0	34	3.1	33	3.5	6	2.9	134	44.0	1	·	·	·	6	1	·	4	13	14	11	3	·	·	4
VII	2	1.8	5.5	1.7	·	·	3.5	2.0	3	2.2	12	2.2	40.5	2.8	23.5	2.1	3	2.3	166	50.0	18	·	·	·	5	·	·	3	13	14	11	5	·	·	10
VIII	2	2.0	4.5	1.6	5.5	1.8	4	1.2	2.5	3.0	5.5	2.8	42.5	2.7	21.5	3.0	5	2.5	26	11.4	16	·	·	·	11	1	1	3	3	11	4	1	2	·	3
IX	0.5	1.0	3.5	1.0	4.5	1.4	3.5	1.6	·	·	14.5	3.4	39.5	2.8	14	3.0	10	2.4	39	15.4	18	·	·	2	7	·	·	7	7	13	5	1	6	·	2
X	2.5	1.8	14.5	1.7	19.5	1.3	10	1.2	1	1.0	2.5	3.0	25	2.7	12	1.4	6	1.7	8	2.1	31	·	·	11	·	·	·	6	13	16	1	·	19	·	·
XI	0.5	2.0	13	1.5	14.5	1.8	16	2.5	3	2.2	3	3.0	33	2.2	7	1.6	·	2.1	69	13.0	15	·	1	12	·	·	·	1	22	18	11	3	11	9	·
XII	4	1.2	12.5	2.2	18.5	1.3	3.5	1.4	6	3.3	10	5.1	26	2.8	10.5	2.2	2	2.5	29	5.9	31	10	13	27	·	·	·	2	19	16	7	·	·	19	·
Rok	46.5	2.1	87.5	1.8	93.5	1.4	64	1.6	44.5	1.9	115.5	3.2	405	3.0	196.5	2.9	42	2.6	735	50.0	18.VII	22	44	127	31	10	2	38	170	182	108	20	43	93	24

Libertów $\varphi = 49°58'$ $\lambda = 19°53'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o,m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.0	-2.3	10.5	22	-14.9	31	-0.9	1.6	0.3	0.3	–	–	–	–	–	–	–	–	–	–	–	–	7.4	5.9	5.3	6.2
II	–	–	–	–	0.2	-4.9	6.7	12, 13	-13.3	2	-3.5	-1.6	-2.2	-2.4	–	–	–	–	–	–	–	–	–	–	–	–	9.5	8.2	7.8	8.5
III	–	–	–	–	2.6	-4.2	13.8	31	-11.4	21	-3.0	0.6	-1.1	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.6	5.4	6.9
IV	–	–	–	–	14.7	6.7	24.7	23	1.7	3, 14	8.3	13.0	10.3	10.5	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.1	4.3	5.5
V	–	–	–	–	14.8	7.3	22.0	8, 19	-0.4	1	8.9	13.1	10.6	10.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.6	5.9	7.0
VI	–	–	–	–	18.3	10.4	31.2	24	2.7	2	12.4	16.6	14.0	14.2	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.0	5.5	5.9
VII	–	–	–	–	20.4	12.0	29.9	26	7.5	4	14.1	18.6	15.7	16.0	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.1	6.2	5.9
VIII	–	–	–	–	22.9	13.7	31.5	7	9.2	31	15.6	21.5	17.9	18.2	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.3	4.0	4.8
IX	–	–	–	–	17.8	8.5	26.8	4	2.3	27	10.4	15.8	12.8	13.0	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.7	2.9	5.0
X	–	–	–	–	12.1	4.3	18.0	1	-3.1	16	5.3	10.9	8.2	8.2	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.3	4.4	5.5
XI	–	–	–	–	6.3	1.8	18.6	7	-2.6	24	2.7	5.0	3.8	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.4	7.8	8.2
XII	–	–	–	–	-1.7	-6.8	6.6	13	-17.2	23	-5.4	-3.3	-4.3	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.6	7.0	7.6
Rok	–	–	–	–	11.0	3.9	31.5	7 VIII	-17.2	23. XII	5.4	9.3	7.2	7.3	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.6	5.5	6.4

Jastrzębie-Zdrój $\varphi = 49°57'$ $\lambda = 18°34'$

I	–	–	–	–	2.6	-2.8	7.7	21	-17.6	31	-1.1	1.7	-0.4	0.0	5.1	5.7	5.2	5.3	8.6	8.1	8.5	8.4	0.8	1.4	0.9	1.0	5.7	6.5	6.4	6.2
II	–	–	–	–	1.1	-5.8	8.3	12	-16.2	26	-3.5	0.1	-2.1	-1.9	4.1	4.9	4.7	4.6	8.3	7.9	8.5	8.2	0.8	1.4	0.8	1.0	8.3	7.9	7.5	7.9
III	–	–	–	–	3.4	-4.2	15.0	31	-9.3	21	-2.5	2.5	-0.8	-0.4	4.6	6.0	5.2	5.3	8.6	8.0	8.7	8.4	0.8	1.7	0.9	1.1	7.3	7.0	6.9	7.1
IV	–	–	–	–	15.7	4.9	27.2	23	1.2	6	8.1	14.4	8.8	10.0	8.5	8.6	9.4	8.8	7.9	5.7	8.1	7.2	2.6	9.7	2.3	4.9	6.1	5.8	6.1	6.0
V	–	–	–	–	–	6.0	–	–	-1.0	1, 3	9.6	14.1	10.3	11.1	10.7	11.2	11.7	11.2	8.8	7.0	9.1	8.3	1.5	5.5	1.2	2.7	7.2	6.8	6.5	6.8
VI	–	–	–	–	–	8.5	–	–	1.8	2	12.6	18.3	12.6	14.0	12.7	13.0	13.4	13.0	8.4	6.1	8.9	7.8	2.5	9.3	1.7	4.5	6.2	6.1	5.8	6.0
VII	–	–	–	–	–	10.0	–	–	4.8	5	14.2	19.7	14.3	15.6	14.2	14.4	14.6	14.4	8.7	6.4	8.9	8.0	2.2	9.3	1.9	4.5	5.4	5.6	5.7	5.6
VIII	–	–	–	–	–	11.1	–	–	5.1	31	15.2	22.7	15.0	17.0	15.6	15.8	16.0	15.8	8.9	5.7	9.3	8.0	1.9	12.4	1.4	5.2	5.1	5.1	4.8	5.0
IX	–	–	–	–	–	6.3	–	–	1.6	15, 25	9.1	16.5	10.2	11.5	11.0	13.0	11.7	11.9	9.4	7.0	9.3	8.6	0.9	6.6	1.1	2.9	7.0	5.8	3.4	5.4
X	–	–	–	–	–	3.6	–	–	-2.3	22	5.1	12.6	6.2	7.5	8.8	10.6	9.5	9.6	9.7	7.4	9.7	8.9	0.3	4.6	0.3	1.7	7.7	5.2	4.6	5.8
XI	–	–	–	–	6.9	1.7	18.1	7, 8	-4.4	21	3.0	5.9	3.6	4.0	7.3	8.0	7.5	7.6	9.4	8.5	9.4	9.1	0.5	2.0	0.6	1.0	8.5	8.4	8.7	8.5
XII	–	–	–	–	-1.6	-6.5	8.7	13	-17.2	29	-4.8	-2.7	-4.6	-4.2	4.2	4.5	4.2	4.3	9.2	8.7	9.1	9.0	0.4	0.8	0.4	0.5	8.0	7.4	7.0	7.5
Rok	–	–	–	–	–	2.7	–	–	-17.6	31. I	5.4	10.5	6.1	7.0	8.9	9.6	9.4	9.3	8.8	7.2	9.0	8.3	1.3	5.4	1.1	2.6	6.9	6.5	6.1	6.5

Goczałkowice $\varphi = 49°57'$ $\lambda = 18°55'$

I	–	–	–	–	2.5	-3.7	8.8	22	-18.6	31	-1.2	1.3	-1.0	-0.5	5.2	5.5	5.0	5.2	8.9	8.1	8.5	8.5	0.7	1.4	0.9	1.0	6.3	6.9	6.7	6.6
II	–	–	–	–	0.4	-6.0	5.3	17	-15.9	3	-4.0	-1.2	-2.8	-2.7	4.3	5.0	4.8	4.7	9.0	8.8	9.3	9.0	0.4	0.7	0.4	0.5	9.6	8.0	7.4	8.3
III	–	–	–	–	2.6	-4.9	14.1	5	-12.5	25	-3.4	0.8	-1.2	-1.2	4.5	5.5	5.1	5.0	8.9	8.3	8.7	8.6	0.6	1.2	0.8	0.9	7.2	7.5	5.9	6.9
IV	–	–	–	–	14.7	5.4	26.7	21	0.5	2	8.0	12.9	9.3	9.9	8.7	8.4	8.8	8.6	8.1	6.1	7.5	7.2	2.5	8.2	3.6	4.8	6.2	5.4	5.1	5.6
V	–	–	–	–	15.1	6.9	21.6	19	-1.4	1	9.0	12.8	10.7	10.8	10.3	10.3	11.0	10.6	8.8	7.0	8.4	8.1	1.4	4.9	2.2	2.8	7.4	7.6	6.6	7.2
VI	–	–	–	–	19.3	9.8	29.9	16	2.2	2	12.4	17.1	14.2	14.5	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.6	5.9	5.9
VII	–	–	–	–	20.8	11.5	29.4	26	6.8	30	14.1	19.2	15.2	15.9	13.8	14.4	14.6	14.3	8.5	6.5	8.4	7.8	2.6	8.3	3.0	4.6	–	–	–	–
VIII	–	–	–	–	23.5	12.8	29.9	7, 13	6.7	29	15.4	21.7	17.3	17.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	18.1	6.9	27.9	4	-0.2	25	10.1	16.0	12.3	12.7	11.4	12.6	12.5	12.2	9.1	7.0	8.7	8.3	1.5	6.2	2.3	3.3	6.1	5.7	3.5	5.1
X	–	–	–	–	13.1	3.9	23.0	4	-3.0	22	5.7	12.1	7.2	8.0	9.1	11.3	9.9	10.1	9.7	8.0	9.6	9.1	0.3	3.2	0.5	1.3	6.0	5.1	4.7	5.3
XI	–	–	–	–	6.7	1.6	18.8	8	-2.6	24	2.8	5.6	3.8	4.0	7.2	8.1	7.8	7.7	9.5	8.8	9.6	9.3	0.4	1.7	0.4	0.8	8.4	7.9	7.9	8.1
XII	–	–	–	–	–	-7.1	–	–	-19.6	29	-4.9	-2.9	-4.6	-4.2	4.1	4.5	4.3	4.3	8.8	8.6	9.0	8.8	0.5	0.7	0.4	0.5	8.6	8.0	6.6	7.7
Rok	–	–	–	–	–	3.1	29.9	16 VI, 7, 13 VIII	-19.6	29. XII	5.3	9.6	6.7	7.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Wadowice $\varphi = 49°53'$ $\lambda = 19°31'$

I	–	–	–	–	3.9	-3.2	12.0	22	-14.2	31	-1.0	2.2	0.1	0.4	4.8	4.9	4.9	4.9	8.2	6.8	7.8	7.6	1.3	2.6	1.6	1.8	8.0	7.5	7.0	7.5
II	–	–	–	–	1.0	-5.8	7.9	13	-16.7	25	-3.6	-0.8	-2.3	-2.2	4.0	4.4	4.5	4.3	8.3	7.5	8.4	8.1	0.9	1.6	1.0	1.2	9.7	8.5	8.9	9.0
III	–	–	–	–	3.1	-5.0	15.8	5	-12.7	26	-3.2	1.3	-1.3	-1.1	4.4	5.0	4.9	4.8	8.6	7.1	8.3	8.0	0.8	2.2	1.1	1.4	8.6	8.3	6.4	7.8
IV	–	–	–	–	15.4	5.1	26.0	23, 24	1.1	8	8.2	13.6	8.8	9.9	8.2	8.0	8.7	8.3	7.6	5.7	7.5	6.8	3.0	9.4	3.1	5.2	7.1	7.0	4.7	6.3
V	–	–	–	–	15.5	6.4	22.9	19	-0.4	2, 3	9.9	13.7	10.1	11.0	10.1	10.0	10.6	10.2	8.1	6.4	8.4	7.6	2.4	6.3	2.1	3.6	8.0	8.5	7.5	8.0
VI	–	–	–	–	18.9	9.0	29.3	16	2.8	7	12.8	17.2	12.9	14.0	12.4	12.7	12.9	12.7	8.0	6.4	8.4	7.6	3.1	8.4	2.6	4.7	6.3	7.3	6.5	6.7
VII	–	–	–	–	21.2	10.2	30.5	26	4.7	6	14.1	19.5	14.6	15.7	13.3	13.4	14.2	13.6	8.3	6.1	8.5	7.6	3.0	10.1	2.6	5.2	6.8	7.4	6.6	6.9
VIII	–	–	–	–	24.1	12.0	32.5	7	6.5	31	15.7	22.5	16.4	17.8	14.2	14.2	15.2	14.5	7.9	5.3	8.1	7.1	3.8	13.9	3.8	7.2	6.5	6.6	4.6	5.9
IX	–	–	–	–	18.3	7.1	30.0	4	1.0	25	10.0	16.3	11.3	12.2	10.1	11.3	11.0	10.8	8.3	6.2	8.2	7.6	2.8	8.2	3.1	4.7	6.6	6.8	3.7	5.7
X	–	–	–	–	12.9	3.7	20.4	1	-1.0	27	4.8	12.2	6.9	7.7	8.3	10.4	9.4	9.4	9.4	7.3	9.3	8.7	0.5	4.2	0.7	1.8	6.7	5.7	5.0	5.8
XI	–	–	–	–	6.9	1.5	18.0	8	-2.8	24	2.6	5.9	3.6	3.9	6.8	7.6	7.4	7.3	9.2	8.1	9.1	8.8	0.7	2.3	0.7	1.2	8.6	8.4	8.5	8.5
XII	–	–	–	–	-0.9	-7.6	9.6	13	-18.8	26	-5.3	-2.4	-4.3	-4.1	3.6	4.2	3.9	3.9	8.3	8.0	8.2	8.2	0.9	1.4	1.0	1.1	8.6	8.3	7.8	8.2
Rok	–	–	–	–	11.7	2.8	32.5	7 VIII	-18.8	26. XII	5.4	10.1	6.4	7.1	8.4	8.8	9.0	8.7	8.4	6.7	8.4	7.8	1.9	5.9	2.0	3.3	7.6	7.5	6.4	7.2

Libertów — $H_s = 320\ m$ — $h_w = 15{,}9\ m$ — 1962

MIESIĄC	ROZKŁAD WIATRU nD, vmD — N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R — Suma	Max	Data	LICZBA DNI (n) — Temperatura T — Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v > 15	◔	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R (?)
I	1	2.0	4	3.5	4	2.8	2.5	1.6	7.5	3.3	23	3.4	46.5	3.4	4.5	6.9	·	3.5	23	5.1	11	2	6	20	·	·	·	2	11	10	9	·	·	—	·
II	5	3.6	13	1.8	6.5	2.0	1.5	1.7	6.5	5.5	14.5	4.6	28	4.0	8	4.3	1	3.6	32	5.4	13	4	12	26	·	5	1	·	21	18	10	·	6	—	·
III	13	4.1	23	3.2	13.5	1.7	5.5	2.1	3	2.0	9.5	2.3	16	4.1	7.5	2.5	2	2.9	32	9.0	12	2	16	25	·	2	·	1	11	13	6	·	7	—	·
IV	8	2.2	7.5	1.8	11.5	1.7	7	1.8	10	4.4	15.5	2.0	20.5	3.3	10	2.8	·	2.6	102	50.6	6	·	·	·	·	3	2	8	8	14	9	2	3	·	2
V	3	1.3	7	1.3	9.5	1.1	5.5	1.2	10	1.4	18	2.4	32.5	2.4	6.5	1.8	1	1.9	144	16.4	20	·	·	1	·	·	·	2	11	20	20	5	·	·	·
VI	9	2.9	2	1.0	5	1.2	3	1.0	3	1.0	11	1.5	36	2.5	13	2.8	8	2.0	83	30.3	1	·	·	·	4	·	·	4	10	9	9	4	1	·	3
VII	7.5	1.5	3	1.3	3.5	1.1	2.5	1.4	10	2.4	11	1.5	45	2.4	8.5	1.7	2	2.0	209	80.5	17	·	·	·	4	·	·	4	9	14	14	6	1	·	7
VIII	3	2.0	2.5	1.0	6.5	1.3	7.5	1.5	13.5	2.5	12.5	2.4	36	2.7	10.5	2.5	1	2.3	29	9.0	16	·	·	·	9	·	·	3	3	9	8	·	1	·	3
IX	3.5	1.3	9.5	1.3	9.5	1.6	4.5	1.0	13	2.0	19	2.8	26	3.2	2	2.5	3	2.2	61	21.2	18	·	·	·	2	1	·	7	7	11	11	2	6	·	·
X	9.5	1.4	21.5	1.8	14.5	1.6	5	1.4	2.5	1.0	9.5	1.6	23	2.3	5.5	1.7	2	1.7	8	4.2	31	·	·	2	·	·	·	9	13	6	3	·	17	·	·
XI	10.5	2.2	22.5	2.1	16	2.0	5.5	1.9	1.5	7.3	2	5.0	27	2.5	5	2.1	·	2.4	77?	20.2	26	·	2	12	·	·	·	2	20	17	12	2	16	—	·
XII	15	2.9	6.5	3.9	18	3.3	2.5	2.4	10	5.0	11	4.5	26.5	3.2	3.5	4.1	·	3.6	43	9.4	16	10	15	28	·	·	·	2	14	17	11	·	10	—	·
Rok	88	2.3	122	2.0	118	1.8	52.5	1.6	90.5	3.2	156.5	2.8	363	3.0	84.5	3.0	20	2.6	843?	80.5	17.VII	18	51	114	19	11	3	44	138	158	122	21	68	—	15

Jastrzębie-Zdrój — $H_s = 227\ m$ — $h_w = 12{,}5\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R (?)
I	3	2.5	4	1.8	1.5	1.3	·	·	1	1.0	47.5	2.3	20	2.0	13	1.4	3	2.0	46	7.8	11	2	6	23	·	·	·	—	—	15	11	·	·	13	·
II	6.5	1.2	13.5	1.5	3.5	1.3	1.5	1.0	2.5	5.2	17	4.0	13	2.3	19.5	1.7	7	2.1	52	8.6	17	7	10	24	·	2	·	—	—	19	13	·	·	26	·
III	10	1.6	21.5	1.7	4	1.5	5	1.2	1	1.0	7.5	1.5	6.5	1.7	30.5	1.4	7	1.4	76	16.3	31	·	8	26	·	·	·	—	—	17	11	2	1	20	·
IV	5	1.3	8.5	1.7	5	1.3	6.5	1.6	6.5	1.5	14	1.8	8.5	1.9	27	1.5	9	1.4	76	12.7	13	·	·	·	8	·	·	—	—	17	13	2	·	·	1
V	3	1.8	10.5	1.4	2	1.2	1.5	1.0	6	1.5	13.5	2.2	12.5	1.6	43	1.3	1	1.5	207	28.8	13	·	·	2	—	·	·	—	—	27	20	8	3	·	2
VI	8.5	1.4	12	1.3	1	1.5	3	1.5	0.5	1.0	4	2.9	5	2.6	44	1.5	12	1.4	52	33.7	1	·	·	·	—	·	·	—	—	12	6	1	1	·	1
VII	2.5	1.2	5.5	1.1	2	1.2	2.5	1.4	4	1.0	12.5	1.8	17	1.9	34	1.1	13	1.2	61	30.9	17	·	·	·	—	·	·	—	—	12	8	1	2	·	3
VIII	0.5	1.0	3.5	1.0	7.5	1.0	3.5	1.0	4.5	1.2	7.5	2.3	15.5	1.6	31.5	1.2	19	1.1	70	21.4	5	·	·	·	—	·	·	—	—	15	11	3	1	·	4
IX	0.5	2.0	6	1.3	6	1.3	·	·	3	1.0	16	2.2	14	1.6	31.5	1.2	13	1.3	77	24.0	17	·	·	·	—	·	·	—	—	14	12	2	7	·	1
X	4.5	1.0	17.5	1.3	9.5	1.5	·	·	2	1.0	1	2.0	11	2.0	26.5	1.1	21	1.0	35	13.0	31	·	·	9	—	·	·	—	—	11	7	1	18	·	·
XI	1.5	1.0	17.5	1.5	13	1.3	13.5	1.3	·	·	8.5	1.7	1.5	1.7	27.5	1.1	7	1.2	102	19.9	19	·	1	10	·	·	·	—	—	20	13	4	6	8	·
XII	10.5	1.5	17	1.6	2.5	1.0	3	1.2	5.5	1.2	11.5	2.5	12	2.3	15	1.2	16	1.4	47	14.3	13	10	17	28	·	·	·	—	—	18	11	1	4	25	·
Rok	56	1.5	137	1.4	57.5	1.3	40	0.9	36.5	1.4	160.5	2.3	136.5	1.9	343	1.3	128	1.4	901	33.7	1.VI	19	42	122	—	2	·	—	—	197	136	25	43	92	12

Goczałkowice — $H_s = 260\ m$ — $h_w = 10{,}0\ m$ I–V, $h_w = 16.7\ m$ VI–XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R (?)
I	7	4.9	3	3.7	·	·	0.5	7.0	8	7.3	25.5	6.7	28	5.4	4	5.0	17	4.8	28	5.4	11	4	5	23	·	6	·	2	13	14	9	·	1	15	·
II	7.5	5.1	6.5	3.9	5.5	3.4	·	·	2.5	8.4	14	8.1	18	5.5	7	6.1	23	4.3	19	4.9	12	6	13	27	·	6	4	·	18	17	8	·	5	24	·
III	12	6.3	15	3.5	6.5	2.5	·	·	3	8.8	12	5.4	8	4.1	4.5	5.1	32	3.1	40	11.6	12	5	10	27	·	4	·	1	15	13	8	1	6	18	1
IV	4.5	3.8	7	3.7	3.5	3.7	0.5	6.0	4	7.4	18	5.4	6	4.1	10.5	5.1	36	2.9	73	17.7	10	·	·	·	5	2	·	7	10	13	10	3	4	·	·
V	1.5	1.7	2	3.5	2	2.5	·	·	2.5	2.2	16	5.1	17.5	4.4	10.5	2.9	41	2.2	179	22.3	20	·	·	1	·	3	1	·	13	24	18	7	1	·	6
VI	7	4.5	1	3.0	2	3.0	·	·	1	4.0	5.5	8.1	19.5	3.5	18	2.8	36	2.3	41	24.7	1	·	·	·	6	2	1	4	12	11	5	1	·	·	2
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	80	23.6	17	·	·	·	6	—	—	—	—	12	11	3	·	·	4
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	51	15.0	7	·	·	·	11	—	—	—	—	11	10	2	1	·	3
IX	3	1.7	7	2.4	0.5	5.0	·	·	5.5	6.4	14.5	7.7	20.5	5.1	7	2.9	32	3.3	58	17.4	18	·	·	1	3	5	2	8	10	10	9	2	10	·	1
X	0.5	3.0	11.5	2.2	6.5	3.7	·	·	·	·	5.5	5.7	7.5	2.9	13.5	2.2	48	1.4	23	9.6	28		·	5	·	·	·	8	9	8	6	·	17	·	·
XI	3	2.0	16.5	2.8	7.5	3.1	2	2.0	0.5	12.0	10	6.0	11.5	3.2	3	2.3	36	2.1	99	15.5	15	·	·	12	·	2	·	1	19	17	14	3	7	7	·
XII	12	2.4	14.5	3.7	2.5	3.0	·	·	3	8.0	18.5	8.0	11.5	3.0	3	2.7	28	3.3	30	12.2	13	10	—	29	·	5	3	2	18	13	6	1	7	17	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	721	24.7	1.VI	25	—	125	31	—	—	—	—	163	114	23	59	81	17

Wadowice — $H_s = 260\ m$ — $h_w = 21{,}4\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R (?)
I	3	1.0	2	1.2	5	1.3	8	1.2	12.5	1.4	26.5	2.9	24.5	3.5	5.5	1.7	6	2.3	41	7.3	26	4	4	22	·	1	·	1	16	15	12	·	·	18	·
II	2	2.0	2	1.5	10	1.1	3.5	1.0	12.5	3.1	11	5.3	25	4.2	11	3.0	7	3.0	38	8.4	12	7	10	25	·	5	1	·	24	19	11	·	3	24	·
III	5	4.0	5	3.8	16.5	1.8	9	1.1	9	1.2	7.5	2.9	19.5	2.5	7.5	1.8	14	1.9	51	15.5	12	5	9	26	·	·	·	·	16	13	10	1	1	24	·
IV	4	1.0	4	3.0	4	2.0	12	1.2	17	1.6	9.5	2.3	28.5	2.4	2	1.2	9	1.8	119	45.5	6	·	·	·	4	·	·	5	12	16	10	5	2	·	2
V	1	2.0	1	1.0	6	1.2	10	1.2	12.5	1.2	20.5	1.9	23	2.7	4	1.4	15	1.5	176	20.0	20	·	·	2	·	·	·	1	16	27	20	9	·	·	1
VI	4.5	1.7	5	2.0	5	1.0	9	1.0	14	1.0	7.5	2.4	30	2.2	8	1.8	7	1.6	92	29.7	1	·	·	·	6	·	·	2	13	12	10	3	·	·	3
VII	3	1.0	1	1.0	6	1.3	9	1.0	10	1.1	20	1.5	29.5	1.9	5.5	1.0	9	1.3	129	51.3	18	·	·	·	5	·	·	2	14	14	13	2	·	·	6
VIII	2	1.0	1	1.0	9	1.6	14.5	1.0	14.5	1.5	16	2.0	26	2.8	1	4.0	9	1.7	28	5.6	15	·	·	·	11	1	·	2	6	14	9	·	1	·	1
IX	1	1.0	1.5	1.0	11.5	1.3	18.5	1.1	10	2.1	14.5	2.2	28.5	2.2	0.5	2.0	4	1.7	74	18.2	18	·	·	·	3	1	·	7	9	12	10	2	3	·	1
X	1.5	1.0	3	1.7	21	1.1	22.5	1.0	8	1.0	3.5	1.9	18.5	1.6	5	1.2	10	1.1	34	19.5	6	·	·	4	·	·	·	6	12	10	5	1	12	·	·
XI	1	1.0	5.5	1.0	22.5	1.3	9.5	1.0	5	1.4	3.5	1.9	15	1.5	1	1.0	27	0.9	90	13.9	23	·	1	10	·	1	·	2	22	15	15	3	8	9	·
XII	3	1.0	7.5	1.3	15.5	1.2	10.5	1.3	15	2.6	11	3.1	14.5	1.8	2	2.0	14	1.6	54	12.7	13	10	14	28	·	3	·	1	20	17	11	1	3	27	·
Rok	31	1.5	38.5	1.6	132	1.4	136	1.1	140	1.6	151	2.5	282.5	2.4	53	1.8	131	1.7	926	51.3	18.VII	26	38	117	29	12	1	29	180	184	136	27	33	102	14

Żarnowa $\varphi = 49°52'$ $\lambda = 21°50'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA t												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0,m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.2	-2.5	7.2	22	-15.6	31	-1.0	1.2	-0.3	-0.1	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.3	7.2	6.8
II	–	–	–	–	0.2	-5.6	4.7	17	-16.9	25	-3.3	-0.9	-2.3	-2.2	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.3	8.4	8.5
III	–	–	–	–	2.5	-4.6	13.9	6	-17.1	20	-3.2	1.3	-1.1	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.3	6.7	7.4
IV	–	–	–	–	16.3	5.5	26.4	22	-0.9	30	7.4	14.9	9.7	10.4	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.8	3.3	5.0
V	–	–	–	–	16.4	6.8	23.6	28	-1.9	2	9.6	14.8	10.5	11.4	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.6	6.2	7.4
VI	–	–	–	–	18.8	8.9	28.8	16	2.6	6, 7	12.0	17.2	12.9	13.8	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.2	5.7	6.3
VII	–	–	–	–	21.1	10.6	30.2	27	6.6	10	13.5	19.7	14.5	15.6	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.8	5.1	6.0
VIII	–	–	–	–	23.7	11.9	30.4	13	4.6	31	14.4	22.3	16.4	17.4	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.6	4.0	5.3
IX	–	–	–	–	18.4	8.1	26.7	5	1.7	15	10.2	17.0	12.1	12.8	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.9	4.2	5.4
X	–	–	–	–	13.7	2.6	19.2	2, 11	-4.6	16	4.3	13.0	6.4	7.5	–	–	–	–	–	–	–	–	–	–	–	–	7.4	4.6	3.5	5.2
XI	–	–	–	–	8.7	2.4	17.2	8	-1.3	18	4.2	7.4	4.8	5.3	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.3	7.7	7.7
XII	–	–	–	–	-1.6	-6.4	6.2	14	-15.2	24	-4.5	-3.0	-4.2	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.1	7.4	7.9
Rok	–	–	–	–	11.7	3.1	30.4	13.VIII	-17.1	20, III	5.3	10.4	6.6	7.2	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.7	5.8	6.6

Ochaby $\varphi = 49°51'$ $\lambda = 18°46'$

I	–	–	–	–	3.4	-2.3	10.8	22	-17.0	31	-0.2	2.2	0.3	0.6	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.3	7.4	7.0
II	–	–	–	–	0.9	-6.4	8.3	12	-18.8	25	-4.3	-0.8	-2.2	-2.4	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.3	7.6	8.3
III	–	–	–	–	3.1	-4.6	15.2	31	-11.9	19	-3.0	1.6	-0.5	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.5	5.8	6.9
IV	–	–	–	–	15.2	5.4	26.1	21, 24	0.7	29	8.5	13.7	9.5	10.3	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.0	5.4	6.3
V	–	–	–	–	15.3	6.8	22.7	19	-0.4	1	10.0	13.2	10.6	11.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.1	7.4	7.7
VI	–	–	–	–	19.3	9.2	29.2	23	3.0	2	13.1	17.5	13.4	14.4	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.8	6.6	6.6
VII	–	–	–	–	21.2	10.6	30.6	26	5.6	30	14.8	19.6	14.6	15.9	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.1	6.1	6.6
VIII	–	–	–	–	24.0	12.1	30.7	7	6.4	31	16.1	22.2	16.3	17.7	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.5	5.3	5.9
IX	–	–	–	–	18.6	7.2	29.4	4	0.5	25	10.6	16.8	11.9	12.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.9	4.0	5.8
X	–	–	–	–	13.2	3.5	23.4	4	-2.2	22	5.5	12.3	6.9	7.9	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.4	4.9	5.8
XI	–	–	–	–	6.8	1.8	19.4	8	-4.9	22	3.1	5.9	3.5	4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.8	8.7	8.8
XII	–	–	–	–	-1.4	-7.4	7.8	13	-19.8	29	-5.3	-2.6	-4.5	-4.2	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.2	8.0	8.3
Rok	–	–	–	–	11.6	3.0	30.7	7.VIII	-19.8	29, XII	5.7	10.1	6.6	7.2	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.4	6.4	7.0

Porąbka $\varphi = 49°49'$ $\lambda = 19°13'$

I	–	–	–	–	3.9	-1.7	12.2	22	-17.4	31	0.2	2.3	0.8	1.0	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.8	7.2	6.9
II	–	–	–	–	0.8	-5.3	7.1	13	-16.8	25	-3.7	-1.0	-2.1	-2.2	–	–	–	–	–	–	–	–	–	–	–	–	9.3	9.1	7.8	8.7
III	–	–	–	–	2.8	-4.7	14.9	5	-14.6	21	-3.3	1.3	-1.2	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.8	6.5	7.7
IV	–	–	–	–	14.9	5.6	26.3	24	0.8	7, 8	7.7	13.2	8.9	9.7	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.6	4.5	5.9
V	–	–	–	–	15.3	6.6	23.0	19	-0.1	1	9.4	13.4	9.8	10.6	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.4	7.6	7.9
VI	–	–	–	–	19.2	9.1	29.8	24	3.0	2, 3, 7	11.9	17.1	12.4	13.4	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.0	6.0	6.3
VII	–	–	–	–	21.2	11.1	30.5	26	6.5	6	13.4	19.9	14.2	15.4	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.5	6.5	6.4
VIII	–	–	–	–	24.4	12.5	32.0	15	7.1	31	14.8	22.5	16.2	17.4	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.2	5.0	5.0
IX	–	–	–	–	18.8	8.0	29.3	4	1.6	25	9.9	16.6	11.4	12.3	–	–	–	–	–	–	–	–	–	–	–	–	5.1	6.0	3.3	4.8
X	–	–	–	–	13.8	4.5	22.0	4	0.0	22, 23	5.5	12.8	7.1	8.1	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.2	4.1	5.2
XI	–	–	–	–	7.3	2.0	19.5	7, 8	-2.8	23	3.2	6.4	3.9	4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.0	7.4	7.8
XII	–	–	–	–	-1.1	-7.1	8.5	13	-19.0	22	-4.8	-2.6	-4.7	-4.2	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.7	6.5	7.4
Rok	–	–	–	–	11.8	3.4	32.0	15.VIII	-19.0	22.XII	5.4	10.2	6.4	7.1	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.1	6.0	6.7

Myślenice $\varphi = 49°49'$ $\lambda = 19°56'$

I	–	–	–	–	4.4	-2.4	11.0	22	-15.0	31	-0.5	3.1	0.7	1.0	5.0	4.8	5.0	4.9	8.3	6.3	7.6	7.4	1.3	3.2	1.8	2.1	6.6	6.0	7.4	6.7
II	–	–	–	–	1.1	-5.2	8.8	13	-18.0	25	-3.5	-0.6	-2.2	-2.1	4.3	4.4	4.6	4.4	8.8	7.6	8.8	8.4	0.7	1.6	0.8	1.0	8.8	7.9	9.0	8.6
III	–	–	–	–	3.1	-5.2	15.7	5	-15.4	21	-3.7	1.7	-1.3	-1.2	4.3	4.5	4.9	4.6	8.8	6.5	8.5	7.9	0.7	2.9	1.2	1.6	7.4	7.9	6.5	7.3
IV	–	–	–	–	15.4	4.7	26.0	23	0.0	7, 8	7.3	13.8	8.8	9.7	8.1	7.9	8.7	8.2	8.0	5.6	7.7	7.1	2.4	9.8	3.0	5.1	6.1	5.9	4.8	5.6
V	–	–	–	–	15.7	6.5	23.9	8	0.0	2	9.5	13.9	9.8	10.8	10.2	9.9	10.6	10.2	8.4	6.4	8.6	7.8	1.9	6.7	1.9	3.5	7.3	7.9	6.4	7.2
VI	–	–	–	–	18.8	8.9	29.3	23	2.5	7	12.1	17.0	12.4	13.5	12.2	13.0	12.6	12.6	8.4	6.7	8.5	7.9	2.5	8.0	2.4	4.3	6.3	7.1	6.2	6.5
VII	–	–	–	–	21.3	10.1	30.9	26	6.0	5	13.4	20.0	14.1	15.4	13.5	14.6	14.2	14.1	8.7	6.3	8.7	7.9	2.1	9.5	2.1	4.6	6.2	6.4	5.3	6.0
VIII	–	–	–	–	24.4	12.2	34.6	13	6.0	31	14.7	22.8	16.0	17.4	14.2	15.7	15.5	15.1	8.4	5.8	8.4	7.5	2.8	12.9	3.0	6.2	4.4	6.2	4.2	4.9
IX	–	–	–	–	18.8	7.1	29.0	4	2.0	25, 27	9.8	17.1	10.9	12.2	10.5	12.3	11.4	11.4	8.6	6.6	8.7	8.0	2.2	8.3	2.1	4.2	6.0	5.9	3.4	5.1
X	–	–	–	–	13.8	4.0	19.8	1, 2, 12	-0.6	17	5.0	12.6	6.7	7.7	8.3	10.9	9.3	9.5	9.3	7.5	9.3	8.7	0.7	4.0	0.7	1.8	5.3	4.5	4.8	4.9
XI	–	–	–	–	7.4	2.0	19.9	7	-2.3	18	3.1	6.2	3.7	4.2	7.0	7.5	7.6	7.4	9.1	8.0	9.3	8.8	0.8	2.8	0.7	1.4	7.2	7.9	8.5	7.9
XII	–	–	–	–	-1.1	-7.4	8.8	9	-18.8	22	-5.0	-2.6	-5.0	-4.4	3.7	3.8	3.8	3.8	8.4	7.5	8.5	8.1	0.9	1.7	0.8	1.1	7.7	7.2	7.9	7.6
Rok	–	–	–	–	11.9	2.9	34.6	13.VIII	-18.8	22.XII	5.2	10.4	6.2	7.0	8.4	9.1	9.0	8.8	8.6	6.7	8.6	8.0	1.6	6.0	1.7	3.1	6.6	6.7	6.2	6.5

Żarnowa — $H_s = 256\,m$ — $h_w = 18{,}3\,m$ — 1962

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	T Min < -10°	T Max < 0°	T Min < 0°	T Max > 25°	Wiatr v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	≡	⊞	R
I	10	4.1	·	·	·	·	6.5	2.2	38.5	5.1	15	4.8	10.5	3.3	10.5	2.6	2	4.2	39	9.3	27	2	6	21	·	5	·	1	12	12	10	·	·	8	·
II	18.5	3.7	8.5	2.7	6	1.8	1	1.0	21	5.3	2	6.0	12.5	3.9	12.5	5.4	2	4.1	48 ?	8.7	12	2	13	27	·	2	2	·	19	17	14	·	1	28	·
III	30.5	3.3	10.5	3.0	6	1.7	5.5	2.4	22.5	4.8	5	3.6	6	5.3	5	4.7	2	3.6	50	11.1	16	5	12	24	·	2	·	1	16	19	11	1	·	27	·
IV	13.5	3.3	9.5	1.8	7	2.9	10	2.8	18.5	4.6	5	5.7	7.5	3.0	8	4.2	11	3.1	27	8.7	27	·	·	2	4	3	·	6	6	10	6	·	2	·	·
V	20.5	2.0	5	2.0	4	1.0	9.5	2.3	12.5	3.5	14.5	3.9	6.5	2.6	9.5	4.2	11	2.5	120	12.6	11	·	·	1	·	1	·	·	14	28	21	3	5	·	3
VI	28	2.5	7	1.7	6	1.0	5.5	1.4	6.5	2.4	·	·	10	3.5	16	4.1	11	2.4	139	35.2	4	·	·	·	7	·	·	1	9	13	11	4	·	·	3
VII	16	2.1	14.5	2.1	9.5	1.1	6	2.1	15	1.8	4	2.5	11.5	3.0	9.5	2.7	7	2.0	125	33.2	16	·	·	·	5	·	·	2	9	18	12	4	2	·	4
VIII	13	1.5	15.5	1.2	9	1.4	9	2.1	12	4.2	3	4.3	8.5	2.5	15	2.5	8	2.1	37	9.7	16	·	·	·	11	1	·	5	6	10	8	·	7	·	3
IX	11.5	1.1	11.5	1.8	10	1.8	10	2.6	18	4.2	4	2.2	9	3.4	9	3.7	7	2.5	51	17.2	5	·	·	·	2	1	·	4	6	10	8	1	5	·	1
X	21.5	1.6	8.5	2.4	14	1.3	9	1.9	9	2.3	4	3.5	4	2.8	4	3.0	19	1.6	7	1.8	31	·	·	9	·	·	·	6	4	12	3	·	13	·	·
XI	28	2.1	3	1.3	7.5	1.3	11	2.7	18	3.7	10	2.4	4	2.2	3.5	1.9	5	2.3	63	12.4	15	·	·	5	·	1	1	1	17	20	12	1	4	2	·
XII	26.5	2.7	9.5	2.6	9	1.2	3	3.7	31	3.7	7	3.3	1	1.0	5	2.2	1	2.9	41	11.4	30	9	15	31	·	·	·	·	17	17	8	1	1	17	·
Rok	237.5	2.5	103	1.9	88	1.4	86	2.3	222.5	3.8	73.5	3.5	91	3.0	107.5	3.4	86	2.8	747 ?	35.2	4. VI	18	46	120	29	16	3	27	135	186	124	15	40	82	14

Ochaby — $H_s = 270\,m$ — $h_w = 18\,m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	T Min < -10°	T Max < 0°	T Min < 0°	T Max > 25°	Wiatr v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	≡	⊞	R
I	3	3.3	5	4.6	·	·	1	3.5	15.5	7.2	34	5.2	8	5.9	6.5	4.3	20	4.3	43	8.4	24	2	4	19	·	10	1	2	15	13	11	·	2	15	·
II	8	4.0	6	2.5	·	·	·	·	8	5.9	18.5	6.7	9.5	5.5	7	5.9	27	3.7	35	5.1	13	6	10	25	·	8	4	·	18	19	10	·	5	26	·
III	8	5.2	11	5.3	4.5	3.0	0.5	5.0	10	4.2	9	4.9	6	3.3	6	4.0	38	2.6	51	12.7	12	5	9	25	·	2	1	1	13	14	10	1	3	22	·
IV	7.5	1.7	8.5	2.1	4.5	4.2	0.5	2.0	12	6.1	15.5	4.7	8.5	4.4	9	4.9	24	3.1	82	21.4	10	·	·	·	6	9	1	7	13	16	11	2	3	·	1
V	5	2.3	4	2.5	4	1.4	2.5	2.2	12	2.7	20	4.0	6.5	4.7	9	3.2	30	2.2	205	30.7	20	·	·	2	·	1	·	·	15	27	22	9	·	·	5
VI	6	3.8	4.5	3.2	1.5	2.3	·	·	3.5	1.9	10.5	2.5	10	3.7	16	3.8	38	1.9	60	24.6	1	·	·	·	6	3	·	2	16	13	9	2	·	·	1
VII	3.5	2.1	3	2.8	2.5	3.6	2	1.2	11	1.8	17.5	3.5	9	3.6	13.5	3.9	31	2.1	49	16.0	18	·	·	·	7	1	·	3	10	11	9	2	·	·	5
VIII	1.5	2.7	5.5	1.5	4	1.2	0.5	1.0	6.5	2.9	18	5.0	13	3.8	8	3.2	36	2.2	84	27.2	3	·	·	·	14	2	1	1	8	15	10	3	·	·	4
IX	2	2.5	2.5	3.4	3.5	2.1	1	1.0	13.5	3.6	24.5	3.4	10	3.3	5	3.2	28	2.3	71	18.8	17	·	·	·	5	2	·	7	9	12	9	3	6	·	1
X	2.5	2.2	5.5	1.5	8.5	2.4	0.5	2.0	3	4.5	5.5	3.3	13	3.0	5.5	2.2	49	1.3	59	21.1	5	·	·	6	·	·	·	8	13	11	8	2	15	·	·
XI	3.5	2.4	9	2.3	8.5	2.4	2.5	2.8	8	3.0	15.5	3.2	4	3.0	8	2.6	31	1.8	109	17.9	19	·	1	11	·	·	·	1	24	18	15	4	7	10	·
XII	2.5	3.6	15	4.0	2.5	5.2	1.5	1.7	8.5	7.2	13.5	5.4	9	2.6	5.5	3.6	35	2.8	33	10.3	13	10	15	28	·	4	1	1	21	17	10	1	5	30	·
Rok	53	3.0	79.5	3.0	44	2.3	12.5	1.9	111.5	4.2	202	4.3	106.5	3.9	99	3.7	387	2.5	881	30.7	20. V	23	39	116	38	42	9	33	175	186	134	29	46	103	17

Porąbka — $H_s = 315\,m$ — $h_w = 17\,m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	T Min < -10°	T Max < 0°	T Min < 0°	T Max > 25°	Wiatr v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	≡	⊞	R
I	9	2.3	4	1.5	·	·	2.5	5.4	27	5.7	32.5	4.9	6	2.7	9	2.3	3	4.2	48	9.1	27	2	3	19	·	5	3	3	15	15	13	·	1	15	·
II	9	2.1	2	3.0	·	·	3.5	6.0	14	7.8	22.5	2.0	3	3.7	14	2.1	16	2.9	56	12.5	12	5	10	23	·	3	2	·	19	16	14	1	6	28	1
III	13	2.8	7	2.1	2	2.0	5	2.8	13.5	5.2	23.5	2.6	3	4.7	13	1.9	13	2.6	67	20.4	12	4	10	24	·	1	1	1	18	13	10	1	10	24	·
IV	8	1.8	5	1.8	1	1.0	4	5.1	14	4.9	26.5	3.9	8.5	1.2	13	1.9	10	2.8	118	42.5	6	·	·	·	8	3	·	8	11	17	9	4	6	·	1
V	9	1.2	·	·	1	1.0	5	1.6	8.5	1.7	31	2.2	6.5	1.5	10	1.0	22	1.3	249	29.1	14	·	·	1	·	·	·	1	18	25	20	12	1	·	3
VI	15	1.9	4	2.0	2	1.0	1	3.0	4	2.0	24	1.8	9	2.2	11	2.2	20	1.5	102	32.8	1	·	·	·	6	·	·	6	11	12	10	4	3	·	3
VII	11.5	1.7	5.5	1.4	·	·	1.5	3.7	5	1.4	39.5	2.5	6	1.5	14	1.5	10	1.8	104	37.5	18	·	·	·	6	·	·	5	14	13	10	3	1	·	5
VIII	12	2.2	2	2.0	·	·	0.5	7.0	5.5	5.7	40	2.4	13	1.8	6	1.3	14	2.1	43	8.1	15	·	·	·	13	1	1	5	6	15	12	·	·	·	4
IX	6	2.3	0.5	1.0	·	·	4	5.4	17.5	3.2	31.5	3.1	9	1.3	10.5	1.8	11	2.4	82	16.2	23	·	·	·	5	1	·	10	9	13	9	4	4	·	2
X	8.5	1.4	1	4.0	2	1.0	1	2.0	8.5	3.2	32.5	2.6	8	1.5	8.5	2.1	23	1.7	45	16.1	6	·	·	·	·	·	·	9	11	10	9	1	10	·	·
XI	8	1.9	3	1.7	1	1.0	4	3.0	13	2.4	15	2.2	2	1.0	7	1.7	37	1.2	107	19.3	20	·	1	10	·	·	·	3	20	16	15	5	13	9	·
XII	12.5	2.0	6.5	2.8	·	·	4.5	3.4	12.5	9.3	29	2.1	5	1.6	9	1.2	14	2.8	54	12.7	16	12	15	28	·	3	3	2	19	15	11	2	8	29	·
Rok	121.5	2.0	40.5	1.9	9	0.6	36.5	4.0	143	4.4	342.5	2.7	79	2.1	125	1.8	193	2.3	1075	42.5	6. IV	23	39	105	38	17	10	53	171	180	142	37	63	105	19

Myślenice — $H_s = 295\,m$ — $h_w = 16{,}8\,m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	T Min < -10°	T Max < 0°	T Min < 0°	T Max > 25°	Wiatr v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	≡	⊞	R
I	·	·	3	2.0	·	·	·	·	12	7.2	32.5	3.1	13.5	2.6	3	3.0	29	2.6	56	13.4	27	1	4	19	·	3	3	2	11	14	10	1	·	16	·
II	5	1.7	2.5	2.6	1	2.0	1	3.0	10	7.4	24	3.2	6	2.3	7.5	1.9	27	2.4	51	7.5	12	4	11	24	·	3	3	·	19	20	15	·	·	28	·
III	15	2.3	2	4.5	·	·	·	·	6	2.8	28	3.6	6	2.7	7	1.9	29	2.0	77	13.7	6	6	12	25	·	1	1	2	15	16	12	3	·	25	·
IV	7	2.9	·	·	·	·	1.5	2.0	4	4.0	41.5	3.0	7.5	2.3	3.5	1.3	25	2.1	137	72.6	6	·	·	·	4	·	·	7	8	15	10	2	4	·	2
V	2.5	2.0	·	·	·	·	·	·	3	2.0	35	2.6	12	2.3	0.5	2.0	40	1.4	138	18.0	31	·	·	·	·	·	·	2	14	24	20	7	·	·	3
VI	6.5	2.1	0.5	2.0	·	·	·	·	1	2.5	25.5	2.3	15.5	2.3	6	1.9	35	1.4	132	39.8	1	·	·	·	6	·	·	4	12	13	11	4	·	·	4
VII	4	1.8	·	·	·	·	·	·	2.5	2.0	33	2.1	17.5	2.0	3	1.7	33	1.3	187	72.2	17	·	·	·	5	·	·	3	9	17	14	4	1	·	7
VIII	3	1.7	·	·	·	·	·	·	5	3.1	39	2.2	13	1.7	2	3.0	31	1.4	33	9.9	16	·	·	·	11	1	1	5	2	12	7	·	1	·	4
IX	3.5	2.0	2.5	2.4	·	·	1	1.0	6	3.2	36	2.3	10	1.8	3	2.3	26	1.6	62	16.3	18	·	·	·	6	·	·	7	8	13	10	2	6	·	·
X	6.5	1.7	·	·	·	·	·	·	0.5	4.0	30	2.3	11.5	2.4	4.5	1.8	40	1.3	14	2.5	19	·	·	3	·	·	·	11	10	9	7	·	11	·	·
XI	5	1.8	2	3.0	3	2.0	1	2.0	4	4.0	20.5	2.6	4.5	1.9	1	1.0	49	1.1	106	19.7	15	·	1	7	·	1	1	3	19	14	13	5	3	8	·
XII	1.5	1.3	11	2.4	·	·	1.5	1.3	7.5	8.7	25	4.3	10.5	2.6	1	1.5	35	2.5	66	14.0	16	12	14	29	·	3	2	3	18	17	12	2	·	25	·
Rok	59.5	1.8	23.5	1.6	4	0.3	6	0.8	61.5	4.2	370	2.8	127.5	2.2	42	1.9	401	1.8	1059	72.6	6. IV	23	42	107	32	12	11	49	145	184	141	30	26	102	20

Aleksandrowice $\varphi = 49°48'$ $\lambda = 19°00'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	969.0	984.5	946.2	1019.0	3.4	−2.7	10.3	22	−17.7	31	−0.5	1.6	0.1	0.3	4.9	5.1	4.8	4.9	81	73	76	77	1.3	2.1	1.8	1.7	7.5	7.9	7.7	7.7
II	967.8	983.8	939.9	1018.2	0.2	−5.9	6.5	12	−16.6	1	−4.2	−1.9	−2.6	−2.8	4.0	4.5	4.6	4.4	86	83	89	86	0.7	1.0	0.6	0.8	8.6	8.6	8.2	8.5
III	962.1	978.5	944.9	1011.9	2.2	−4.9	14.7	5	−11.0	21	−3.6	0.4	−0.9	−1.2	4.4	4.8	4.9	4.7	89	74	81	81	0.6	1.9	1.4	1.3	8.5	8.6	7.3	8.1
IV	966.6	977.9	941.3	1014.6	14.1	5.0	24.7	24	0.4	29	7.9	12.3	9.2	9.6	8.4	8.7	8.3	8.5	80	65	73	73	2.8	7.3	4.1	4.7	7.4	7.2	5.9	6.8
V	966.5	972.6	953.5	1014.5	14.3	5.7	21.4	19	−1.2	1	9.0	12.1	9.6	10.1	10.0	10.2	10.3	10.2	85	73	85	81	1.7	4.6	2.1	2.8	8.3	8.7	7.9	8.3
VI	971.8	980.5	962.7	1019.5	18.1	9.0	28.4	23, 24	1.8	2	12.2	16.3	12.4	13.3	11.9	12.2	11.5	11.9	81	65	78	75	3.1	7.9	3.7	4.9	7.0	7.8	6.8	7.2
VII	968.7	977.6	956.9	1015.6	20.1	10.5	29.6	26	6.1	30	14.0	18.3	14.6	15.4	12.8	12.9	12.5	12.7	80	62	75	72	3.6	8.9	4.6	5.7	7.2	7.4	6.2	6.9
VIII	970.2	976.5	958.7	1017.1	23.1	12.0	29.7	15	6.4	31	16.0	21.3	16.0	17.3	14.3	15.0	14.1	14.5	78	59	77	71	4.2	11.0	4.4	6.5	6.2	7.1	6.2	6.5
IX	970.1	979.6	958.2	1018.0	17.4	7.3	28.0	4	0.3	25	10.3	15.4	11.7	12.3	10.3	11.4	10.5	10.7	83	67	77	76	2.9	7.0	3.9	4.6	6.4	7.2	4.0	5.9
X	974.4	985.9	960.6	1023.2	12.7	3.9	20.8	4	−0.8	25	6.1	11.5	7.4	8.1	8.8	10.4	9.5	9.6	92	77	90	86	1.0	3.7	1.1	1.9	5.9	5.3	4.5	5.2
XI	968.0	982.5	952.7	1017.2	6.5	1.5	17.8	8	−4.8	28	3.0	5.2	3.6	3.8	6.9	7.6	7.3	7.3	90	84	91	88	0.9	2.0	0.9	1.3	8.3	8.6	8.0	8.3
XII	967.3	994.1	927.7	1017.9	−1.6	−7.5	9.6	13	−18.5	22	−4.9	−3.3	−5.1	−4.6	3.7	4.1	4.0	3.9	84	83	89	85	1.0	1.0	0.6	0.9	7.5	8.3	7.6	7.8
Rok	968.5	994.1	927.7	1017.2	10.9	2.8	29.7	15.VIII	−18.5	22.XII	5.4	9.1	6.3	6.8	8.4	8.9	8.5	8.6	8.4	7.2	8.2	7.9	2.0	4.9	2.4	3.1	7.4	7.7	6.7	7.3

Leskowiec $\varphi = 49°48'$ $\lambda = 19°27'$

I	—	—	—	—	0.0	−4.4	6.3	22	−17.9	31	−2.9	−1.2	−2.5	−2.3	—	—	—	—	—	—	—	—	—	—	—	—	7.1	6.2	6.6	6.6
II	—	—	—	—	−2.9	−8.8	1.3	8	−18.4	1	−6.5	−4.3	−5.5	−5.4	—	—	—	—	—	—	—	—	—	—	—	—	8.7	8.3	8.9	8.6
III	—	—	—	—	−1.5	−6.6	10.4	5	−13.0	17	−4.8	−3.1	−4.5	−4.2	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.6	7.4	7.4
IV	—	—	—	—	10.6	4.4	23.0	24	−3.0	7	6.3	8.6	6.3	6.9	—	—	—	—	—	—	—	—	—	—	—	—	6.7	6.9	5.8	6.5
V	—	—	—	—	11.5	4.0	19.5	8	−4.3	1	6.3	8.7	7.1	7.3	—	—	—	—	—	—	—	—	—	—	—	—	7.1	8.2	7.7	7.7
VI	—	—	—	—	14.7	7.1	24.4	16, 24	−0.9	7	9.5	12.2	10.0	10.4	—	—	—	—	—	—	—	—	—	—	—	—	6.9	7.5	6.4	6.9
VII	—	—	—	—	16.8	9.4	25.6	27	4.0	4	11.7	15.1	11.9	12.6	—	—	—	—	—	—	—	—	—	—	—	—	6.0	6.4	5.9	6.1
VIII	—	—	—	—	20.2	12.0	27.4	15	6.6	31	14.3	17.7	14.7	15.4	—	—	—	—	—	—	—	—	—	—	—	—	5.5	5.9	5.2	5.5
IX	—	—	—	—	14.5	6.9	25.0	3	2.3	25	8.9	12.0	9.4	9.9	—	—	—	—	—	—	—	—	—	—	—	—	5.6	5.9	4.5	5.3
X	—	—	—	—	11.6	5.3	19.7	3	0.0	16	7.0	10.0	7.2	7.8	—	—	—	—	—	—	—	—	—	—	—	—	5.2	5.4	4.6	5.1
XI	—	—	—	—	5.2	−0.1	15.5	8	−6.0	24	1.6	3.0	1.8	2.0	—	—	—	—	—	—	—	—	—	—	—	—	7.9	8.0	7.9	7.9
XII	—	—	—	—	−3.4	−8.6	5.0	9	−21.9	23	−6.8	−5.2	−6.6	−6.3	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.0	7.1	7.3
Rok	—	—	—	—	8.1	1.7	27.4	15. VIII	−21.9	23. XII	3.7	6.1	4.1	4.5	—	—	—	—	—	—	—	—	—	—	—	—	6.8	6.9	6.5	6.7

Dynów $\varphi = 49°48'$ $\lambda = 22°14'$

I	—	—	—	—	2.2	−2.2	7.9	22	−13.1	31	−1.0	1.5	−0.5	−0.1	—	—	—	—	—	—	—	—	—	—	—	—	8.1	6.7	7.3	7.4
II	—	—	—	—	−0.2	−6.2	3.8	6	−15.8	25	−4.5	−0.9	−2.8	−2.8	—	—	—	—	—	—	—	—	—	—	—	—	8.8	7.6	9.1	8.5
III	—	—	—	—	2.1	−5.1	13.0	6	−18.1	20	−3.4	1.3	−1.5	−1.3	—	—	—	—	—	—	—	—	—	—	—	—	8.4	6.9	6.8	7.4
IV	—	—	—	—	16.6	5.1	26.2	22	−1.0	30	7.8	15.4	10.0	10.8	—	—	—	—	—	—	—	—	—	—	—	—	5.3	4.8	4.7	4.9
V	—	—	—	—	16.4	7.4	24.1	28	−0.9	1, 2	10.1	15.5	10.8	11.8	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.1	6.5	7.2
VI	—	—	—	—	18.9	8.8	28.7	16	3.1	9	12.8	17.7	13.2	14.2	—	—	—	—	—	—	—	—	—	—	—	—	5.8	6.4	6.9	6.4
VII	—	—	—	—	20.8	11.2	29.2	27	5.1	30	14.6	19.9	14.8	16.0	—	—	—	—	—	—	—	—	—	—	—	—	6.9	6.4	5.8	6.4
VIII	—	—	—	—	23.6	12.2	30.2	13, 15	5.1	29	15.2	22.8	16.9	18.0	—	—	—	—	—	—	—	—	—	—	—	—	6.3	5.2	5.3	5.6
IX	—	—	—	—	18.3	7.7	28.1	5	0.3	15	10.2	17.5	11.4	12.6	—	—	—	—	—	—	—	—	—	—	—	—	6.5	5.4	5.5	5.8
X	—	—	—	—	13.7	2.5	19.4	11	−5.4	16	4.8	13.3	6.5	7.8	—	—	—	—	—	—	—	—	—	—	—	—	6.8	4.5	3.5	4.9
XI	—	—	—	—	8.2	1.7	16.6	1	−3.5	18	2.9	6.9	4.1	4.5	—	—	—	—	—	—	—	—	—	—	—	—	8.8	7.4	7.9	8.0
XII	—	—	—	—	−2.1	−6.6	7.1	14	−15.0	23	−5.0	−3.3	−4.5	−4.3	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.8	7.9	8.0
Rok	—	—	—	—	11.5	3.0	30.2	13.15.VIII	−18.1	20. III	5.4	10.6	6.5	7.2	—	—	—	—	—	—	—	—	—	—	—	—	7.3	6.4	6.4	6.7

Przemyśl $\varphi = 49°48'$ $\lambda = 22°46'$

I	988.5	1004.7	968.3	1018.4	3.5	−2.3	10.6	22	−14.0	31	0.0	2.1	0.1	0.6	5.0	5.1	4.8	5.0	79	71	78	76	1.4	2.3	1.5	1.7	6.9	6.8	6.4	6.7
II	986.3	1003.6	958.9	1016.4	−0.1	−5.5	3.9	8, 13	−14.4	25	−3.8	−1.3	−2.4	−2.5	4.0	4.2	4.3	4.2	85	75	83	81	0.7	1.5	0.9	1.0	8.7	8.9	8.8	8.8
III	981.6	999.0	965.3	1011.4	2.5	−4.9	15.1	5	−18.1	20	−3.2	1.0	−1.1	−1.1	4.4	4.8	4.9	4.7	85	70	81	79	0.8	2.3	1.1	1.4	8.6	7.5	6.9	7.7
IV	985.6	997.9	963.5	1014.3	16.7	5.0	25.8	24	−1.3	30	7.3	15.2	10.3	10.8	8.5	8.8	9.0	8.8	83	53	72	69	2.0	9.9	4.7	5.4	5.1	5.2	3.4	4.6
V	984.8	992.7	972.1	1013.3	16.9	7.4	25.0	14	−2.4	3	10.2	15.5	11.4	12.1	11.6	12.4	12.3	12.1	91	69	89	83	1.2	5.9	1.6	2.9	6.7	7.8	5.6	6.7
VI	988.9	997.5	979.3	1017.4	19.0	9.8	28.2	23	2.9	7	12.8	17.6	14.0	14.6	13.4	14.0	13.8	13.7	88	69	84	80	2.0	7.9	3.0	4.3	5.1	6.8	6.3	6.1
VII	986.5	996.8	974.4	1014.7	20.8	11.6	30.7	27	7.1	30	14.6	19.4	15.2	16.1	14.9	15.5	15.2	15.2	89	70	88	82	1.9	7.7	2.3	4.0	5.0	6.8	4.4	5.4
VIII	988.4	995.0	979.9	1016.5	23.6	12.7	30.4	7	6.1	29	15.0	22.4	17.2	18.0	15.7	16.8	17.2	16.6	91	62	86	80	1.5	10.9	2.9	5.1	5.5	5.6	3.5	4.9
IX	989.0	1000.9	975.9	1017.6	18.6	8.0	28.6	5	1.4	15	10.4	17.1	12.2	13.0	11.2	12.3	12.0	11.8	89	64	85	79	1.8	8.1	2.5	4.1	5.3	5.7	4.5	5.2
X	993.8	1006.3	981.3	1023.0	13.8	3.4	18.4	2, 12	−3.4	16	4.9	12.5	7.2	8.0	8.3	10.1	9.4	9.3	93	70	90	84	0.7	4.7	1.1	2.2	6.4	5.3	7.4	4.7
XI	988.8	1002.4	975.1	1018.4	7.5	2.1	16.8	1	−3.3	18	3.3	6.2	4.5	4.6	7.5	8.2	7.9	7.9	94	85	92	90	0.5	1.7	0.7	1.0	9.1	8.7	7.4	8.4
XII	987.4	1014.1	947.6	1017.8	−1.3	−6.6	8.5	14	−15.4	26	−4.9	−2.8	−4.2	−4.0	3.8	4.1	4.0	4.0	86	79	85	83	0.7	1.2	0.8	0.9	7.7	7.6	7.7	7.7
Rok	987.5	1014.1	947.6	1016.5	11.8	3.4	30.7	27.VII	−18.1	20. III	5.6	10.4	7.0	7.5	9.0	9.7	9.6	9.4	88	70	84	81	1.3	5.3	1.9	2.8	6.7	6.9	5.6	6.4

Aleksandrowice $H_s = 398 m$ $H_b = 403,4 m$ $h_w = 20 m$ 1962

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◔	●	Opad R > 0.1	R > 1.0	R > 10.0	≡	⊠	R
I	4.5	3.4	4	2.4	2.5	2.8	7.5	4.2	13	9.4	24.5	7.5	17	5.7	6	4.1	14	5.3	56	8.6	28	3	4	19	·	15	5	·	17	17	14	·	1	15	·
II	7.5	3.3	1.5	3.0	5.5	2.6	4.5	2.0	7	9.7	15.5	8.4	18	6.2	10.5	5.9	14	5.0	56	8.0	13	5	12	27	·	8	5	·	20	23	16	·	2	28	·
III	10	3.6	8.5	5.1	5	4.6	9	2.8	20.5	8.3	8	4.6	14	5.2	6	3.8	11	4.7	73	15.7	12	3	16	23	·	11	2	1	20	19	12	2	5	25	·
IV	5	2.1	4	4.2	9	3.7	12.5	3.7	17	8.8	9.5	6.2	11.5	5.4	8.5	5.2	13	4.7	138	33.2	6	·	·	·	·	11	5	5	13	18	11	6	5	·	1
V	1.5	2.3	3.5	2.3	8	2.3	5.5	3.1	13	6.1	20	5.1	18	5.1	7.5	3.0	16	3.7	239	35.4	20	·	·	3	·	9	·	·	17	29	23	11		1	5
VI	4	2.4	2	2.5	6	3.5	4.5	2.2	11	3.3	9.5	6.2	31	3.5	10	3.6	12	3.2	91	30.5	1	·	·	·	5	4	·	1	16	15	12	2	·	—	4
VII	3	1.8	4	2.1	5	1.9	7	3.1	12	4.2	23.5	4.0	21.5	3.7	5	2.1	12	3.0	93	42.1	18	·	·	·	4	6	·	2	14	15	10	2	·	·	6
VIII	2.5	1.0	3	4.0	9	2.7	11	3.1	13	2.6	18	5.0	20.5	4.2	6	3.2	10	3.3	76	22.3	7	·	·	·	9	8	1	·	6	13	10	3	·	·	6
IX	1.5	2.7	3	3.0	11.5	2.9	11.5	3.3	16.5	6.2	22	6.1	15	4.0	5	1.9	4	4.3	96	25.8	17	·	·	·	1	11	1	7	10	13	10	4	3	·	2
X	6.5	1.8	5.5	2.9	11	2.7	18.5	2.5	5.5	5.6	12	3.5	15.5	3.2	5.5	2.5	13	2.6	57	18.2	5	·	·	4	·	1	1	7	10	10	10	2	17	·	·
XI	5	1.2	7.5	5.1	11.5	2.7	21	4.2	4	6.6	5	5.0	17	3.2	3	1.7	16	3.0	122	23.6	20	·	2	13	·	5	1	2	22	19	15	4	13	11	·
XII	2.5	1.2	7	5.1	14	4.1	7.5	4.1	14	12.3	8	8.9	11	4.0	2	3.8	27	4.5	53	13.7	13	12	15	29	·	11	3	2	19	17	11	1	5	29	
Rok	53.5	2.2	54.5	3.5	98	3.0	120	3.2	146.5	6.9	175.5	5.9	210	4.4	75	3.4	162	3.9	1150	42.1	18.VII	23	49	118	19	100	24	27	184	208	154	37	51	109	24

Leskowiec · $H_s = 870 m$ $h_w = 16 m$

I	7	5.4	1	2.0	4.5	4.8	12.5	6.5	19.5	10.3	18	7.3	13.5	7.1	12	9.1	5	7.3	69	21.8	28	3	14	27	·	14	6		10	11	10	2	12	—	·
II	5.5	12.7	3	4.0	1	11.0	16	5.9	6	7.7	6	13.6	8	5.8	16.5	7.8	22	5.8	90	17.7	21	9	24	28	·	10	5	·	22	18	17	1	20	—	1
III	2	5.5	4	3.2	15.5	5.5	17.5	5.1	18.5	8.7	4.5	8.7	1.5	12.0	10.5	8.8	19	5.5	92	20.0	16	9	20	29	·	10	5	2	15	19	15	2	17	—	·
IV	6	4.3	1.5	2.7	11.5	5.7	5	4.5	22	10.2	6	4.6	11.5	3.9	17.5	4.8	9	5.5	134	52.4	6	·	·	10	·	9	5	1	14	14	11	5	13	—	1
V	10.5	3.9	6	5.3	3	3.3	5.5	5.1	18.5	6.1	8.5	4.9	17.5	4.3	18.5	5.4	5	4.7	202	30.3	20	·	·	4	·	9	2	·	11	25	20	10	15	—	4
VI	15	3.8	6	3.3	7	5.7	5	4.0	4	3.5	4	6.4	18	6.4	26	6.4	5	5.1	152	34.2	4	·	·	2	·	8	4	·	15	13	13	6	11	—	4
VII	5	2.5	7	4.3	8	3.8	5.5	3.6	9	8.3	5.5	3.0	15.5	2.8	27.5	4.7	10	3.8	129	57.3	18	·	·	·	2	5	1	3	7	16	15	2	10		5
VIII	3.5	2.4	3.5	2.9	7.5	3.4	9.5	6.2	7.5	9.3	9	4.7	27.5	4.7	17	6.1	8	4.8	50	9.0	15	·	·	·	3	6	4	·	4	15	11		5	·	2
IX	3.5	2.4	2.5	3.2	9	5.7	11.5	5.0	14.5	7.4	10.5	6.8	17.5	4.1	14	6.7	7	5.2	102	20.2	17	·	·	·	·	9	3	6	6	11	10	4	9		2
X	1.5	3.0	3	4.0	10.5	2.2	10	3.8	14.5	5.4	8.5	2.6	14.5	2.2	14.5	5.0	16	3.1	54	19.8	6	·	·	·	·	4	2	10	9	10	10	1	13	·	·
XI	2	2.5	8	1.9	8	2.1	10.5	3.3	33	5.3	8	1.9	4.5	3.4	4	4.0	12	3.3	11.0	16.8	20	·	7	18	·	4	2	2	20	17	14	5	18	—	
XII	3	2.3	4	7.5	7	6.6	8.5	6.0	16.5	13.5	8.5	6.5	13.5	4.7	9	5.0	23	5.6	82	13.8	14	10	23	31	·	13	6	1	13	16	16	3	17	—	·
Rok	64.5	4.2	49.5	3.7	92.5	5.0	117	4.9	183.5	8.0	97	5.9	163	5.1	187	6.2	141	5.0	1266	57.3	18.VII	31	88	149	5	101	45	25	146	185	162	41	160	—	19

Dynów $H_s = 276 m$ $h_w = 17,5 m$

I	3	1.7	4	3.0	1	7.0	1	1.0	1	2.0	62	7.2	4	2.8	11	2.5	6	5.5	33	8.6	27	2	7	22	·	10	4	1	15	14	12	·	·	—	·
II	5	1.2	7	1.9	7	2.1	1	1.0	1	1.0	18	8.0	3	7.7	22	4.3	20	3.5	50	15.1	13	6	15	27	·	6	2	·	17	18	11	1	·	—	·
III	3	2.3	9	5.1	7	3.4	·	·	6	5.2	21	3.0	6	2.0	17	3.3	24	2.6	67	15.7	15	6	12	25	·	3	·	·	12	19	11	2	·	—	·
IV	4	1.0	3	1.3	2	2.5	4	4.0	9	6.0	18	2.8	4	1.2	9	2.8	37	1.8	37	13.6	27	·	·	1	4	2	1	8	4	7	6	1	·	—	·
V	3	1.0	3	1.0	·	·	·	·	4	1.5	27	2.0	9	4.6	13	1.6	34	1.4	103	20.4	10	·	·	2	·	·	·	·	11	21	15	3	1	·	6
VI	11	1.9	2	1.0	3	1.3	·	·	·	·	15	1.3	4	1.2	27	2.3	28	1.3	145	36.2	1	·	·	·	6	·	·	·	10	12	10	5	1	·	3
VII	4	1.2	1	1.0	1	1.0	1	1.0	3	1.3	22	1.5	10	1.3	13	1.4	38	0.8	90	24.4	19	·	·	·	5	·	·	2	10	13	10	3	2	·	5
VIII	·	·	·	·	·	·	·	·	2	1.0	24	1.7	12	1.7	10	2.5	45	0.9	35	12.2	16	·	·	·	10			·	3	11	8	1	3	·	3
IX	·	·	1	2.0	2	1.0	2	1.0	1	1.0	27	3.0	19	1.3	4	3.0	34	1.4	51	11.8	5	·	·	·	2	1		2	7	12	8	2	3	·	1
X	4	1.2	5	1.2	6	1.3	·	·	·	·	18	2.0	4	1.2	8	1.2	48	0.8	2	1.7	19	·	·	11	·	·	·	6	7	3	1	·	10	·	·
XI	5	1.2	6	1.0	12	1.0	5	1.4	3	5.7	17	2.2	5	1.4	6	1.0	31	1.1	68	11.4	25	·		7	·	·	·	·	16	13	11	2	2	—	·
XII	8	1.2	8	2.4	3	1.7	·	·	7	4.1	32	5.4	3	1.3	4	1.2	28	2.6	40	10.2	31	9	17	31	·	5	·	1	20	16	11	1	·	—	·
Rok	50	1.2	49	1.7	44	1.9	14	0.8	37	2.4	301	3.3	83	2.3	144	2.3	373	2.0	721	36.2	1.VI	23	51	126	27	27	7	20	132	159	114	21	22	—	18

Przemyśl $H_s = 237 m$ $H_b = 238,9 m$ $h_w = 20,6 m$

I	1	3.5	3.5	6.0	2	5.0	·	·	4	4.2	25.5	4.1	38	3.0	8	5.0	11	3.3	28	9.9	13	2	5	21	·		·	2	13	12	5	·	·	15	·
II	5	3.4	2	2.0	10	3.2	6	2.3	·	·	10.5	7.2	25	5.0	13.5	5.4	12	4.0	39	9.2	13	3	14	27	·	7	·	·	20	21	11	·	1	28	·
III	4.5	2.9	9	4.6	14	3.5	3.5	3.7	3.5	3.4	9.5	2.6	17	4.1	15	5.1	17	3.2	35	8.1	12	3	11	27	·	3	·	1	17	15	9	·	2	26	·
IV	3	3.5	11	2.7	12	3.1	6	3.0	7.5	2.3	10	3.5	19	3.3	8.5	4.6	13	2.8	32	16.7	6	·	·	2	4	1	·	7	6	10	6	1	2	·	·
V	9	2.3	4.5	3.1	1	5.0	1	3.0	6	3.1	10	3.6	43	3.0	11.5	3.5	7	2.8	116	20.0	20	·	·	3	·	2		1	10	23	16	4	4	·	7
VI	4	3.2	1.5	3.7	4	4.8	·	·	1	1.0	3.5	3.1	40	3.6	26	2.9	10	3.0	118	14.9	1	·	·	·	7	·	·	5	10	16	13	6	3		5
VII	3.5	2.1	3.5	3.0	3	2.7	3.5	1.9	1	1.0	8.5	2.5	35.5	2.8	15.5	3.5	19	2.2	105	28.1	18	·	·	·	5	·	·	4	8	18	14	2	1	·	7
VIII	2	3.2	0.5	2.0	4.5	3.3	2.5	4.4	3.5	3.7	13	3.0	37	3.1	6	3.2	24	2.3	56	17.9	22	·	·		11	·	·	4	3	15	10	1	7	·	9
IX	1	2.0	4	2.0	5.5	2.1	2.5	1.4	3.5	3.3	11.5	4.1	37.5	3.1	4.5	3.0	20	2.4	58	16.6	22	·	·	·	3			7	7	15	9	2	3	·	2
X	9	1.2	4	1.4	9	1.7	4.5	2.9	2	1.8	6	3.4	23.5	2.9	10	2.0	25	1.7	3	1.2	31	·	·	8	·	·	·	8	4	4	1	·	14	·	·
XI	3	2.7	6.5	3.0	17.5	3.1	16	2.1	3	2.0	7	3.1	14	2.8	6	2.8	17	2.2	57	10.8	16	·	·	5	·	·		·	19	16	10	2	10	1	·
XII	3.5	3.7	14.5	3.7	6.5	2.6	·	·	3	3.2	10.5	4.9	26	3.7	10	2.6	19	2.8	36	8.7	30	9	14	31	·	1	·	2	18	13	6		3	20	·
Rok	48.5	2.8	64.5	3.1	89	3.3	45.5	2.1	38	2.4	125.5	3.8	355.5	3.4	134.5	3.6	194	2.7	683	28.1	18.VII	17	44	124	30	14	·	41	135	178	110	18	50	90	30

Międzybrodzie Bialskie $\varphi = 49°47'$ $\lambda = 19°12'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T											ŚREDNIA PREŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.4	-1.9	11.3	22	-16.9	31	-0.1	2.1	0.5	0.8	4.8	4.6	4.8	4.7	76	63	73	71	1.5	2.8	1.9	2.1	7.2	7.7	7.9	7.6
II	–	–	–	–	0.8	-5.8	7.6	12	-18.7	25	-3.8	-0.9	-2.2	-2.3	4.2	4.4	4.6	4.4	85	75	84	81	0.7	1.5	0.9	1.0	8.6	8.4	8.7	8.6
III	–	–	–	–	2.5	-5.0	14.0	5	-15.3	26	-3.2	1.3	-1.4	-1.2	4.4	4.5	4.9	4.6	86	66	85	79	0.8	2.7	1.0	1.5	7.7	7.7	7.7	7.7
IV	–	–	–	–	13.9	5.1	24.6	20, 21	1.0	7, 8	7.5	12.4	8.9	9.4	7.8	7.7	8.4	8.0	76	59	75	70	3.0	8.4	3.5	5.0	6.8	6.9	6.8	6.8
V	–	–	–	–	14.5	6.4	21.6	19	0.2	3	9.3	13.0	10.1	10.6	9.9	10.2	10.6	10.2	83	68	85	79	2.1	5.4	2.1	3.2	7.9	8.3	8.2	8.1
VI	–	–	–	–	18.2	9.0	28.2	24	3.5	2, 7	12.2	16.7	12.6	13.5	11.9	12.3	12.4	12.2	81	64	82	76	2.9	8.2	2.8	4.6	6.6	8.0	6.7	7.1
VII	–	–	–	–	20.2	10.3	29.0	26, 27	5.6	30	14.0	18.8	14.9	15.6	12.9	13.0	13.1	13.0	80	61	77	73	5.0	9.5	4.2	6.2	6.5	7.5	6.0	6.7
VIII	–	–	–	–	–	11.5	–	–	6.0	31	14.4	21.9	16.2	17.2	14.1	14.7	14.6	14.5	85	56	79	73	2.6	11.7	4.1	6.1	5.5	6.2	4.1	5.3
IX	–	–	–	–	17.7	7.1	28.1	4	1.2	25	9.5	15.8	11.1	11.9	10.0	11.4	10.9	10.8	84	65	82	77	2.7	7.4	2.9	4.3	5.7	6.0	2.6	4.8
X	–	–	–	–	13.4	3.6	20.4	4	-1.3	23	4.7	12.1	7.0	7.7	8.2	10.5	9.4	9.4	94	74	93	87	0.6	4.1	0.8	1.8	7.3	4.6	4.3	5.4
XI	–	–	–	–	7.3	2.0	18.3	7	-3.3	24	3.3	6.1	4.0	4.4	7.2	7.9	7.6	7.6	92	83	92	89	0.8	2.2	0.8	1.3	8.4	7.8	7.5	7.9
XII	–	–	–	–	-1.5	-9.2	7.3	13	-23.7	22	-5.4	-3.1	-5.0	-4.6	3.7	4.1	3.8	3.9	85	80	85	83	0.7	1.1	0.8	0.9	7.5	7.7	6.7	7.3
Rok	–	–	–	–	–	2.8	–	–	-23.7	22, XII	5.2	9.7	6.4	6.9	8.3	8.8	8.8	8.6	84	68	83	78	2.0	5.4	2.2	3.2	7.1	7.2	6.4	6.9

Ciężkowice $\varphi = 49°47'$ $\lambda = 20°58'$

I	–	–	–	–	2.7	-3.1	9.5	20	-16.0	31	-1.6	1.5	-0.7	-0.4	4.8	4.8	4.8	4.8	83	69	80	77	0.9	2.3	1.2	1.5	5.5	5.7	6.5	5.9
II	–	–	–	–	1.0	-5.2	7.7	13	-13.0	24	-3.6	-0.9	-2.2	-2.2	4.0	4.3	4.5	4.3	82	74	83	80	0.9	1.5	0.9	1.1	8.4	8.3	8.5	8.4
III	–	–	–	–	2.9	-5.4	13.9	5, 31	-16.8	21	-3.8	1.6	-1.5	-1.3	4.2	4.8	4.9	4.6	83	67	84	78	0.8	2.5	0.9	1.4	7.5	7.4	7.1	7.3
IV	–	–	–	–	15.9	4.5	26.6	22	-1.0	30	6.7	14.3	9.4	10.0	8.2	8.5	9.2	8.6	83	56	77	72	1.9	9.5	3.2	4.9	5.6	7.4	4.3	5.8
V	–	–	–	–	16.1	6.3	23.6	8	-1.3	2	9.0	14.2	10.2	10.9	10.4	10.3	11.0	10.6	88	64	86	79	1.6	6.5	1.9	3.3	7.1	8.3	5.7	7.0
VI	–	–	–	–	18.8	8.6	29.2	16	2.5	7, 9	11.7	17.3	13.0	13.8	12.7	12.7	13.2	12.9	89	65	85	80	1.7	8.8	2.5	4.3	5.8	7.5	5.2	6.2
VII	–	–	–	–	21.4	10.1	29.8	26, 27	5.4	30	13.0	19.6	14.6	15.4	13.7	14.8	14.8	14.4	91	66	88	82	1.5	8.8	2.2	4.2	5.5	6.6	5.3	5.8
VIII	–	–	–	–	23.8	11.2	30.5	13	4.3	31	13.6	22.3	16.0	17.0	14.5	15.9	15.9	15.4	92	59	86	79	1.3	11.8	2.7	5.3	5.0	5.3	3.2	4.5
IX	–	–	–	–	18.8	7.2	28.2	4	0.6	26	8.9	17.2	11.8	12.4	10.2	11.7	11.8	11.2	89	61	85	78	1.7	8.9	2.5	4.4	6.4	5.9	4.8	5.7
X	–	–	–	–	13.9	2.4	20.5	2	-3.1	22	3.8	12.9	6.0	7.2	8.0	10.7	8.9	9.0	96	69	93	86	0.4	5.0	0.7	2.0	6.4	4.4	4.6	5.1
XI	–	–	–	–	8.3	2.8	17.5	1	-1.8	24	3.9	6.9	4.8	5.1	7.2	7.9	7.6	7.6	88	73	87	84	1.2	2.8	1.3	1.8	7.0	8.2	8.0	7.7
XII	–	–	–	–	-1.3	-7.3	4.9	8	-18.2	27	-5.4	-2.8	-4.6	-4.4	3.5	4.0	3.8	3.8	81	76	81	79	0.9	1.3	0.9	1.0	6.3	8.2	7.2	7.2
Rok	–	–	–	–	11.9	2.7	30.5	13, VIII	-18.2	27, XII	4.7	10.3	6.4	7.0	8.4	9.2	9.2	8.9	87	67	85	80	1.2	5.8	1.7	2.9	6.4	6.9	5.9	6.4

Rożnów $\varphi = 49°46'$ $\lambda = 20°41'$

I	–	–	–	–	3.3	-2.7	8.9	20	-15.8	31	-1.0	2.0	0.0	0.2	5.0	5.1	5.0	5.0	84	70	79	78	0.9	2.3	1.4	1.5	7.3	6.4	8.1	7.3
II	–	–	–	–	1.2	-5.2	8.3	12, 13	-15.0	25	-3.6	-0.9	-1.9	-2.1	3.7	4.2	4.2	4.0	77	73	78	76	1.1	1.6	1.3	1.3	9.5	8.3	9.0	8.8
III	–	–	–	–	3.1	-4.9	14.6	5	-14.3	27	-3.2	1.7	-1.1	-0.9	4.3	5.3	5.0	4.9	83	72	84	80	0.9	2.1	1.0	1.3	8.1	8.0	7.1	7.7
IV	–	–	–	–	16.0	5.5	26.5	23, 24	-0.1	30	8.0	14.2	9.7	10.4	8.3	8.3	8.6	8.4	78	56	73	69	2.7	9.6	4.1	5.5	6.2	6.4	5.0	5.9
V	–	–	–	–	15.8	7.0	23.7	8	0.0	2	9.4	13.4	10.6	11.0	10.3	10.3	10.9	10.5	85	68	84	79	1.8	5.7	2.3	3.3	7.7	8.4	6.7	7.6
VI	–	–	–	–	18.4	9.6	28.5	23, 24	1.4	7	12.2	16.5	13.1	13.7	12.4	12.3	13.0	12.6	85	66	83	78	2.5	8.2	2.8	4.5	6.4	7.5	6.4	6.8
VII	–	–	–	–	21.0	11.6	29.5	26	7.4	30	13.8	19.3	15.3	15.9	13.3	14.9	14.7	14.3	84	66	84	78	2.7	8.1	3.0	4.6	6.5	6.3	6.4	6.4
VIII	–	–	–	–	23.6	13.2	30.0	13, 15	7.0	31	15.3	22.0	17.5	18.1	14.7	15.8	16.3	15.6	84	60	81	75	2.9	11.5	4.0	6.1	6.1	5.5	4.5	5.4
IX	–	–	–	–	18.4	8.8	27.8	4	3.3	26	10.6	16.8	12.7	13.2	10.4	11.6	11.9	11.3	82	62	82	75	2.8	8.6	3.2	4.9	6.2	5.9	4.8	5.6
X	–	–	–	–	13.4	4.6	19.0	1, 2, 11	-1.1	22	5.5	12.4	7.4	8.2	8.7	10.5	9.7	9.6	95	72	93	87	0.5	4.3	0.8	1.9	8.2	4.9	5.6	6.2
XI	–	–	–	–	7.8	2.9	18.0	8	-2.0	23, 24	4.0	6.7	4.6	5.0	7.5	8.0	7.7	7.7	90	81	90	87	1.0	2.5	1.1	1.5	8.2	8.2	8.2	8.2
XII	–	–	–	–	-1.3	-6.7	5.6	13	-16.2	26	-5.0	-2.7	-4.4	-4.1	3.6	4.0	3.9	3.8	78	77	82	79	0.9	1.3	0.8	1.0	8.1	8.2	8.2	8.2
Rok	–	–	–	–	11.7	3.6	30.0	13, 15, VIII	-16.2	26, XII	5.5	10.1	7.0	7.4	8.5	9.2	9.2	9.0	84	69	83	79	1.7	5.5	2.2	3.1	7.4	7.0	6.7	7.0

Cieszyn $\varphi = 49°45'$ $\lambda = 18°38'$

I	–	–	–	–	3.7	-2.0	12.0	22	-16.0	31	-0.3	2.4	0.1	0.6	5.4	5.5	5.3	5.4	85	75	83	81	0.9	2.1	1.1	1.4	7.1	7.8	7.3	7.4
II	–	–	–	–	1.1	-5.8	8.4	12, 13	-19.0	1	-3.9	-0.3	-1.9	-2.0	4.1	4.9	4.8	4.6	83	81	86	83	0.8	1.2	0.7	0.9	8.8	8.7	7.6	8.4
III	–	–	–	–	3.6	-3.9	16.8	31	-11.8	26	-2.8	2.0	-0.2	-0.3	4.5	5.5	5.1	5.0	83	75	81	80	0.8	2.0	1.3	1.4	8.7	8.4	7.4	8.2
IV	–	–	–	–	15.7	5.7	27.0	23, 24	1.3	2	7.8	14.1	10.0	10.5	8.2	8.5	8.7	8.5	79	57	72	69	2.8	9.4	4.5	5.6	6.9	6.9	6.2	6.7
V	–	–	–	–	15.9	6.5	25.5	19	-0.8	3	9.3	13.4	10.3	10.8	10.2	10.9	11.0	10.7	86	72	86	81	1.7	5.2	2.0	3.0	7.6	8.4	7.1	7.7
VI	–	–	–	–	20.0	9.4	31.2	23	2.6	2	12.7	18.2	13.6	14.5	12.4	13.1	12.9	12.8	82	62	87	75	3.1	9.6	3.5	5.4	6.9	6.8	6.4	6.7
VII	–	–	–	–	21.7	10.9	31.9	26	5.9	6	14.2	20.2	14.9	16.0	13.5	14.6	14.4	14.2	83	62	84	76	2.9	9.9	3.0	5.3	7.2	7.1	6.7	7.0
VIII	–	–	–	–	24.8	12.8	31.7	15	6.8	31	15.2	23.0	16.9	18.0	14.7	15.9	15.8	15.5	84	58	82	75	2.9	12.9	3.8	6.5	6.3	6.6	6.0	6.3
IX	–	–	–	–	19.0	7.8	30.3	4	0.7	25	9.9	16.9	11.9	12.7	10.7	13.0	11.6	11.8	87	69	83	80	2.1	7.2	2.9	4.1	6.5	6.4	4.3	5.7
X	–	–	–	–	13.9	4.9	24.8	4	-0.9	25	6.1	12.8	7.6	8.5	9.0	11.0	9.9	10.0	93	75	93	87	0.7	4.5	0.7	2.0	6.4	6.3	5.2	6.0
XI	–	–	–	–	6.9	2.0	18.9	8	-4.7	22	3.3	5.8	4.0	4.3	6.9	7.5	7.4	7.3	88	80	89	86	1.2	2.5	1.1	1.6	8.3	8.6	8.2	8.4
XII	–	–	–	–	-1.1	-7.1	6.6	13	-17.1	22	-4.9	-2.3	-4.8	-4.2	3.7	4.2	3.8	3.9	80	78	82	80	0.8	1.3	0.8	1.0	8.9	8.8	7.9	8.5
Rok	–	–	–	–	12.1	3.4	31.9	26, VII	-19.0	1, II	5.6	10.5	6.9	7.5	8.6	9.6	9.2	9.1	84	70	84	79	1.7	5.6	2.1	3.1	7.5	7.6	6.7	7.3

Międzybrodzie Bialskie $H_s = 320\,m$ $h_w = 10\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU n_D, v_{mD}: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n) Temperatura T: Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v: v>10	v>15	◐	●	Opad R: R>0.1	R>1.0	R>10.0	≡	⊞	R FO
I	8	4.8	3	3.0	·	·	32.5	7.3	19	10.9	4.5	5.4	2	6.0	11	5.8	13	6.4	41	7.8	27	2	3	18	·	10	5	·	15	13	10	·	1	7	·
II	13	5.5	4	3.2	·	·	14	5.4	11	12.3	·		2	5.0	16	6.8	24	4.9	51	10.2	12	7	9	25	·	8	4	·	19	20	14	1	·	26	·
III	23.5	6.7	8	2.7	·	·	9	4.9	15.5	6.3	1.5	4.3	3	3.7	8.5	4.0	24	4.0	59	23.2	12	5	9	24	·	3	·	·	17	16	13	1	1	21	·
IV	11.5	4.1	9	3.6	·	·	16	5.8	11	9.6	2	7.5	4	4.2	7.5	5.4	29	3.9	121	47.8	6	·	·	·	·	6	1	2	11	18	11	4	6	·	1
V	10	3.5	13	2.7	2	2.0	23.5	4.7	7.5	5.5	2.5	5.2	5.5	4.2	4	3.0	25	3.0	236	27.7	20	·	·	·	·	1	·	·	16	27	23	11	·	·	5
VI	14	5.0	12	3.0	·	·	8	3.2	3	4.3	0.5	3.0	5	3.2	12.5	6.7	36	2.7	119	33.4	4	·	·	·	4	4	2	·	13	12	10	4	·	·	2
VII	11.5	3.9	3.5	2.7	·	·	21	4.0	2.5	5.4	1.5	2.3	1	6.0	11	3.4	41	2.1	119	44.2	18	·	·	·	4	·	·	2	13	12	10	4	·	·	5
VIII	7.5	4.5	2	3.0	1	5.0	16	3.3	4	9.5	·	·	4	5.0	10.5	4.3	48	2.2	46	11.9	3	·	·	·	—	1	1	2	6	15	12	1	1	·	6
IX	7.5	4.9	1.5	3.7	1	3.0	23.5	6.1	6.5	8.2	2	3.5	6	3.0	8	3.5	34	3.3	92	20.5	23	·	·	·	5	4	·	10	6	13	10	5	—	·	2
X	11	4.1	7.5	3.0	0.5	1.0	6.5	4.4	6	6.5	·	·	1	5.0	3.5	4.7	57	1.7	44	8.4	5	·	·	5	·	1	1	5	9	11	8	·	15	·	·
XI	13.5	3.7	7	2.9	1	1.0	10.5	6.4	11	8.0	0.5	5.0	·	·	7.5	6.9	39	3.1	100	17.5	20	·	1	11	·	5	3	·	17	19	16	4	4	9	·
XII	19	4.6	3.5	3.7	0.5	1.0	12.5	4.7	19.5	12.3	1	7.0	3	3.0	2	9.7	32	4.7	43	9.7	16	12	15	30	·	9	5	1	12	21	10	·	2	29	·
Rok	150	4.6	74	3.1	6	1.1	193	5.0	116.5	8.2	16	3.6	36.5	4.0	102	5.4	401	3.5	1071	47.8	6.IV	26	37	113	—	52	22	22	154	197	147	35	—	92	21

Ciężkowice $H_s = 280\,m$ $h_w = 15{,}9\,m$

I	1	1.0	1.5	1.0	·	·	0.5	2.0	28	1.7	13	1.2	10	1.6	3	1.7	36	0.9	41	7.8	29	2	6	23	·	—	—	5	11	16	10	·	—	14	—
II	6	2.0	·	·	1.5	1.7	0.5	1.0	7.5	1.3	8.5	2.5	12.5	2.0	12.5	3.4	35	1.4	49	7.9	17, 19	4	11	25	·	—	—	·	15	20	12	·	—	28	—
III	3.5	3.4	1.5	2.7	3	1.0	0.5	3.0	17	1.6	5	1.7	15	2.0	4.5	3.1	43	1.1	63	8.9	16	5	9	25	·	—	—	2	15	17	13	·	7	27	—
IV	1.5	2.3	4	1.1	2.5	2.0	3	4.0	16	2.0	6.5	1.3	11.5	2.5	5	3.2	40	1.2	80	25.4	7	·	·	3	4	—	—	3	9	14	10	2	3	·	—
V	0.5	2.0	·	·	·	·	1	1.5	11.5	1.3	20.5	1.7	13	2.3	1.5	2.0	45	0.9	101	10.2	25	·	·	2	·	—	—	2	12	27	21	1	1	·	—
VI	3.5	2.7	2	1.0	1.5	1.0	1	1.0	6	1.1	18	1.3	19	2.6	9	3.6	30	1.4	159	56.4	4	·	·	·	5	—	—	3	8	15	12	4	4	·	—
VII	2.5	1.6	1	1.0	·	·	·	·	13	1.2	18	1.0	20	1.8	2.5	2.6	36	0.9	109	40.6	18	·	·	·	5	—	—	3	4	17	13	3	·	·	—
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	33	15.0	16	·	·	·	11	—	—	4	2	10	7	1	3	·	—
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	63	17.0	17	·	·	·	5	—	—	6	5	13	8	3	6	·	—
X	5	1.1	1	1.5	3.5	1.1	4	1.0	3.5	1.0	4.5	1.4	5.5	1.5	11	1.8	55	0.6	10	2.4	15	·	·	10	·	—	—	9	8	8	4	·	18	·	—
XI	4	1.2	1.5	1.7	4.5	1.8	15.5	2.4	14	1.5	6.5	1.3	7.5	1.5	7.5	1.3	29	1.1	80	17.5	15	·	·	5	·	—	—	2	18	18	14	3	9	8	—
XII	15.5	2.4	1	1.0	2	1.0	1.5	3.0	20.5	2.9	10	1.5	5	2.2	6.5	1.8	31	1.5	60	14.1	14	9	16	31	·	—	—	1	12	19	12	2	2	21	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	848	56.4	4.VI	20	42	124	30	—	—	40	119	194	136	19	—	98	—

Rożnów $H_s = 300\,m$ $h_w = 20\,m$

I	2.5	4.6	1	1.0	1	1.0	27.5	2.0	24	3.5	6	2.2	12	2.8	11	3.6	8	2.6	28	6.4	28	2	4	21	·	·	·	1	14	14	9	·	1	16	·
II	3	2.3	·	·	3.5	1.9	16	1.6	7.5	4.7	3.5	7.0	16.5	9.2	21	4.7	13	4.2	36	5.8	19	2	9	27	·	5	3	·	20	22	15	·	2	27	·
III	7	5.7	3	3.2	5	1.4	17	1.5	16	3.7	3	2.3	5	6.2	12	6.2	25	2.7	50	10.1	12	5	8	26		3	1	1	17	16	9	1	5	25	·
IV	1	1.0	2.5	1.0	3	1.0	30	2.2	15.5	5.1	3	4.5	5.5	2.5	17.5	3.7	12	2.7	74	19.5	6	·	·	1	5	3	·	6	9	14	11	2	4	·	1
V	2.5	1.2	2	1.0	4.5	1.0	32.5	1.4	13	2.2	4	1.5	10.5	5.9	14	2.3	10	2.0	99	12.7	20	·	·	·	·	2	1	1	15	23	19	2	·	·	3
VI	8.5	3.2	2	2.0	11	1.1	23	1.3	1	1.0	4	1.8	13	2.5	21.5	3.4	6	2.0	140	41.7	4	·	·	·	5	1	·	3	12	12	10	4	1	·	3
VII	8	1.2	7.5	1.0	9	1.0	28.5	1.1	12	1.4	2	2.5	1.5	1.0	16.5	2.5	8	1.3	144	46.5	18	·	·	·	5	·	·	2	9	16	14	5	2	·	8
VIII	5.5	1.0	3	1.0	3.5	1.0	37	1.3	15	2.1	4	2.5	8	4.1	9	3.0	8	1.7	45	15.8	16	·	·	·	11	1	·	1	3	9	5	3	3	·	2
IX	1.5	1.7	1.5	1.7	·	·	21	1.3	22	2.7	8.5	2.9	9.5	3.8	7	2.9	19	1.9	56	18.5	18	·	·	·	5	1	·	5	5	10	7	2	6	·	1
X	7.5	1.0	5	1.0	6	1.0	22	1.0	7.5	1.5	3.5	1.3	5	1.8	10.5	1.7	26	0.9	7	2.6	15	·	·	3	·	·	·	3	9	5	2	·	18	·	·
XI	6	1.0	2	1.0	2	1.0	22.5	2.1	19	4.7	5	1.2	2.5	1.4	9	1.6	22	1.9	73	11.6	23	·	1	8	·	2	·	1	21	18	12	3	13	9	·
XII	9	1.6	3	1.3	5	1.4	16.5	2.7	17.5	6.0	2.5	4.4	9.5	3.1	14	1.9	16	2.6	57	13.0	14	9	13	31	·	3	1	1	18	17	12	2	4	25	·
Rok	62	2.1	32.5	1.3	53.5	1.1	293.5	1.6	170	3.2	49	2.8	98.5	3.7	163	3.1	173	2.2	809	46.5	18.VII	18	35	117	31	21	6	25	152	176	125	24	59	102	18

Cieszyn $H_s = 300\,m$ $h_w = 15{,}8\,m$

I	4.5	1.6	2	1.8	2	1.0	11.5	1.6	44.5	1.8	19.5	1.5	3	1.3	4	1.4	2	1.6	56	8.6	29	2	5	19	·	·	·	·	15	14	13	·	·	15	—
II	5.5	1.5	6	1.2	2	1.0	4	1.1	23	2.0	17	2.4	2.5	2.2	13	1.8	11	1.6	58	7.8	19	6	8	25	·	·	·	1	19	20	16	·	·	27	—
III	16.5	1.9	9.5	1.8	2	1.2	8.5	1.1	25.5	1.3	16	1.1	4	1.4	6	1.2	5	1.3	75	15.1	12	3	6	22	·	·	·	·	18	12	11	4	1	22	—
IV	1.5	1.0	3	1.0	8.5	1.2	10.5	1.7	26.5	1.6	10.5	1.6	6	1.3	6.5	1.3	17	1.2	68	15.1	10	·	·	·	8	·	·	6	15	17	11	2	2	·	—
V	2	1.0	2	1.0	1.5	1.3	12	1.2	30	1.2	20.5	1.2	3	1.5	7	1.0	15	1.0	222	32.4	20	·	·	2	1	·	·	·	16	24	19	8	·	·	—
VI	8.5	1.5	7	1.2	2	1.0	7	1.2	20.5	1.2	11.5	1.6	3	1.8	10.5	1.6	20	1.1	60	26.5	1	·	·	·	7	·	·	2	12	15	8	2	·	·	—
VII	7	1.3	2	1.0	1	1.0	9.5	1.2	32	1.3	13.5	1.4	3	2.0	9	1.2	16	1.1	86	25.2	18	·	·	·	6	·	·	·	14	16	13	3	·	·	—
VIII	0.5	1.0	1	1.0	1.5	1.0	11	1.2	43.5	1.6	13.5	1.7	3.5	1.4	3.5	1.1	15	1.3	59	17.2	5	·	·	·	15	·	·	·	7	15	10	2	·	·	—
IX	6.5	1.2	4.5	1.7	3.5	1.4	10.5	1.6	25.5	1.7	13.5	1.8	4	1.5	8	1.4	14	1.3	77	21.1	17	·	·	·	4	·	·	5	10	13	11	3	2	·	—
X	6.5	1.0	5.5	1.0	1	1.0	9	1.5	24.5	1.2	2.5	1.0	·	·	6	1.0	38	0.7	55	17.4	5	·	·	2	·	·	·	8	12	11	9	2	10	·	—
XI	8.5	1.1	5	1.7	3.5	1.0	6	1.5	15	2.0	12.5	1.4	3.5	1.1	10	1.0	26	1.0	111	22.4	20	·	1	12	·	·	·	1	19	18	16	3	4	10	—
XII	7	1.0	5.5	1.2	1	1.0	8.5	1.8	26.5	1.6	13.5	1.5	4	1.0	10	1.4	17	1.2	49	7.9	31	11	14	28	·	·	·	·	19	19	9	·	2	31	—
Rok	74.5	1.3	53	1.3	29.5	1.1	108	1.4	337	1.5	184	1.5	39.5	1.4	93.5	1.3	196	1.2	976	32.4	20.V	22	34	110	41	·	·	23	176	194	146	29	21	105	—

Cieszyn-Bobrek $\varphi = 49°45'$ $\lambda = 18°39'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA t										ŚREDNIA PREŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0,m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.6	−2.2	12.3	22	−16.3	31	−0.5	2.2	0.1	0.5	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.7	7.5	7.5
II	–	–	–	–	0.8	−6.7	9.0	12	−21.7	1	−4.2	−0.6	−2.5	−2.4	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.4	8.3	8.6
III	–	–	–	–	3.2	−4.8	15.8	31	−14.0	26	−3.1	1.8	−0.7	−0.7	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.1	7.5	8.1
IV	–	–	–	–	15.2	5.5	25.7	21	1.4	6	8.5	13.7	9.1	10.1	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.1	6.5	6.8
V	–	–	–	–	15.3	6.2	22.9	8, 28	−1.0	3	9.8	13.6	9.9	10.8	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.3	7.2	7.8
VI	–	–	–	–	19.4	8.8	30.6	16, 23	2.4	2	12.8	18.0	12.6	14.0	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.0	6.6	6.8
VII	–	–	–	–	21.3	10.6	31.2	26	5.1	30	14.9	19.9	14.3	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.0	6.5	6.8
VIII	–	–	–	–	24.3	11.8	31.4	15	6.2	29	16.1	22.9	15.8	17.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.4	5.9	6.1
IX	–	–	–	–	18.6	6.7	29.8	4	−0.3	25	10.2	17.0	10.8	12.2	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.2	4.2	5.5
X	–	–	–	–	13.5	3.8	23.2	4	−2.5	25	5.5	12.4	6.5	7.7	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.7	5.5	6.4
XI	–	–	–	–	6.8	2.0	18.8	7	−6.1	22	3.3	6.0	3.9	4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.8	8.5	8.5
XII	–	–	–	–	−1.3	−7.2	6.6	13	−19.0	22	−5.3	−2.4	−5.1	−4.5	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.1	7.5	8.0
Rok	–	–	–	–	11.7	2.9	31.4	15.VIII	−21.7	1. II	5.7	10.4	6.2	7.1	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.5	6.8	7.2

Klimczok $\varphi = 49°44'$ $\lambda = 19°00'$

I	–	–	–	–	0.8	–	5.3	1	–	–	−4.8	−2.1	−4.5	−4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.9	6.5	6.9
II	–	–	–	–	−4.2	–	0.5	12	–	–	−8.6	−5.7	−7.6	−7.4	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.5	7.5	7.7
III	–	–	–	–	−2.5	–	8.2	5	–	–	−7.2	−4.0	−5.9	−5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.2	6.8	7.3
IV	–	–	–	–	8.3	–	20.7	18	–	–	3.6	6.9	4.5	4.9	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.3	6.1	6.3
V	–	–	–	–	9.1	–	18.3	19	–	–	5.2	7.6	5.4	5.9	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.2	7.0	7.2
VI	–	–	–	–	12.8	–	24.8	16	–	–	7.9	11.2	8.5	9.0	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.0	5.0	5.7
VII	–	–	–	–	14.7	7.9	24.2	26	2.1	4	9.9	13.0	10.9	11.2	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.8	6.1	5.9
VIII	–	–	–	–	18.1	10.3	25.5	15	5.2	31	12.4	16.6	13.2	13.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.4	4.6	5.1
IX	–	–	–	–	12.3	5.4	23.0	4	0.0	22	7.2	10.2	8.3	8.5	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.4	3.1	4.8
X	–	–	–	–	10.4	4.5	23.1	9	−1.0	21	5.7	8.5	6.4	6.8	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.8	4.3	4.5
XI	–	–	–	–	3.4	−1.5	14.5	8	−7.7	25	0.1	1.8	0.2	0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.9	7.2	7.4
XII	–	–	–	–	−3.9	−10.2	2.6	7	−28.6	24	−7.7	−6.1	−7.9	−7.4	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.3	8.0	7.7
Rok	–	–	–	–	6.6	–	25.5	15.VIII	–	–	2.0	4.8	2.6	3.0	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.4	6.0	6.4

Maków Podhalański $\varphi = 49°44'$ $\lambda = 19°40'$

I	–	–	–	–	4.0	−4.7	10.3	22	−19.5	31	−2.2	3.0	−1.0	−0.3	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.2	6.9	6.3
II	–	–	–	–	1.3	−6.8	8.1	13	−18.9	25	−4.6	−0.1	−2.7	−2.5	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.7	8.8	8.4
III	–	–	–	–	3.2	−6.3	16.4	5	−18.0	26	−4.4	1.9	−2.1	−1.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	15.0	3.5	27.3	22	−1.9	2	6.4	13.7	8.2	9.1	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.3	5.0	5.4
V	–	–	–	–	15.6	6.0	23.4	8	−1.7	2	8.8	13.7	9.8	10.5	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.5	6.1	6.8
VI	–	–	–	–	18.7	8.2	29.5	16, 23	2.6	7	11.8	17.0	12.3	13.4	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.1	5.6	5.8
VII	–	–	–	–	21.4	9.7	30.8	26	5.0	2, 5, 30	13.4	19.8	13.9	15.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	24.2	11.0	32.0	15	5.0	31	14.1	22.8	15.6	17.0	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.3	3.9	4.3
IX	–	–	–	–	19.2	5.6	29.3	4, 12	0.3	27	8.6	17.8	10.5	11.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	14.7	2.6	23.3	3	−2.0	17	4.3	13.7	6.2	7.6	–	–	–	–	–	–	–	–	–	–	–	–	4.3	3.9	3.2	3.8
XI	–	–	–	–	7.9	1.1	19.4	7	−3.4	22	2.6	6.9	3.4	4.1	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.6	7.5	7.5
XII	–	–	–	–	−1.1	–	9.4	9	–	–	−6.0	−2.4	−5.8	−5.0	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.8	7.5	7.2
Rok	–	–	–	–	12.0	–	32.0	15.VIII	–	–	4.4	10.6	5.7	6.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Biecz $\varphi = 49°44'$ $\lambda = 21°15'$

I	–	–	–	–	2.2	−3.3	9.7	20	−16.1	31	−1.6	1.1	−1.0	−0.6	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.8	7.1	6.4
II	–	–	–	–	0.5	−5.7	7.6	13	−17.2	25	−3.6	−1.2	−2.8	−2.6	–	–	–	–	–	–	–	–	–	–	–	–	9.5	7.8	8.0	8.4
III	–	–	–	–	2.4	−5.9	12.8	31	−16.0	21	−3.3	1.1	−1.7	−1.4	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.0	6.4	7.4
IV	–	–	–	–	–	4.3	–	–	−1.7	30	7.3	14.2	8.9	9.8	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.7	4.7	5.4
V	–	–	–	–	–	6.1	–	–	−2.5	2	9.3	13.6	9.7	10.6	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.2	6.0	7.4
VI	–	–	–	–	–	8.0	–	–	2.0	7	12.0	16.9	12.6	13.5	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.2	6.6	6.6
VII	–	–	–	–	–	9.9	–	–	5.8	30	13.5	19.3	14.0	15.2	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.7	5.5	6.0
VIII	–	–	–	–	23.7	10.9	30.4	13	3.5	31	13.8	22.2	15.6	16.8	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.4	3.3	4.6
IX	–	–	–	–	18.3	6.6	26.3	4, 5, 12	0.2	26	9.2	16.8	11.9	12.4	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.5	4.5	5.3
X	–	–	–	–	13.8	2.0	20.5	3	−4.0	22	4.2	12.6	5.8	7.1	–	–	–	–	–	–	–	–	–	–	–	–	7.2	4.0	2.5	4.6
XI	–	–	–	–	8.1	2.5	17.3	1	−3.1	28	4.0	6.9	5.1	5.3	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.8	8.1	8.0
XII	–	–	–	–	−1.7	−7.3	4.8	14	−17.4	27	−5.1	−3.0	−4.5	−4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.3	8.1	8.3
Rok	–	–	–	–	–	2.3	–	–	−17.4	27.XII	5.0	10.0	6.1	6.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.6	5.9	6.5

Cieszyn-Bobrek $H_s = 300\,m$ $h_w = 14\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v>10	v>15	◑	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊞	R (R)
I	6.5	2.4	2.5	1.4	0.5	1.0	5.5	5.1	22.5	4.3	29.5	2.8	12	2.5	9	2.3	5	3.0	49	7.6	6	2	5	18	·	·	·	·	13	15	11	·	·	10	·
II	6.5	1.7	14.5	1.4	0.5	1.0	1	4.0	10.5	3.8	12	4.9	11	2.5	15	3.2	13	2.5	56	7.7	19	5	10	24	·	2	1	·	17	22	15	·	·	26	1
III	14	2.7	18	3.3	2	2.5	9	3.2	11.5	3.3	8.5	2.6	7	1.4	8	2.8	15	2.4	68	14.4	12	6	10	23	·	·	·	·	16	17	10	2	1	23	·
IV	5.5	1.5	13	1.7	2	2.0	9.5	3.1	14.5	4.5	10	2.4	10.5	3.1	15	2.3	10	2.4	74	15.8	10	·	·	·	7	1	·	5	16	18	12	3	1	·	·
V	7.5	1.5	7	1.6	1	1.0	8	2.4	9.5	2.2	21	3.1	11.5	1.9	12.5	1.5	15	1.8	221	31.4	20	·	·	3	·	·	·	·	13	26	19	10	·	·	6
VI	14	2.0	11.5	1.7	1	1.5	1.5	1.7	1.5	1.7	9.5	2.6	21.5	2.1	20.5	1.9	9	1.8	61	28.2	1	·	·	·	6	·	·	1	13	16	11	2	·	·	2
VII	12	1.3	8.5	1.9	·	·	5	2.1	7	1.6	20.5	2.6	12	2.5	12	1.6	16	1.7	95	23.3	18	·	·	·	5	·	·	3	11	17	12	4	·	·	8
VIII	5.5	1.5	4	1.3	2.5	1.0	2.5	1.0	8	2.7	17	3.8	15.5	2.5	10	1.8	28	1.7	65	21.8	5	·	·	·	14	·	·	1	7	16	12	2	·	·	5
IX	2	1.8	5.5	1.8	1	1.0	2	5.0	9.5	3.4	21.5	3.0	11	2.0	11.5	1.2	26	1.7	74	20.1	17	·	·	1	4	·	·	8	9	12	11	3	1	·	1
X	7.5	1.7	16	1.9	·	·	3.5	1.6	2	3.5	5.5	2.2	14.5	1.4	8	1.1	36	1.0	53	21.3	5	·	·	5	·	·	·	6	13	11	8	2	13	·	·
XI	6.5	1.0	16	1.5	1	1.5	17.5	2.9	8	2.6	11.5	1.3	5.5	1.3	8	1.2	16	1.5	110	22.4	20	·	2	12	·	·	·	1	21	19	16	3	9	10	·
XII	7	2.0	16.5	2.1	1.5	2.0	2.5	4.0	12.5	5.8	14.5	2.5	7.5	1.9	3	1.5	28	2.0	40	7.7	13	11	15	28	·	·	·	1	18	21	9	·	4	31	·
Rok	94.5	1.8	133	1.8	13	1.2	67.5	3.0	117	3.3	181	2.8	139.5	2.1	132.5	1.9	217	2.0	966	31.4	20.V	24	42	114	36	3	1	26	167	210	146	31	29	100	23

Klimczok $H_s = 1010\,m$ $h_w = 16{,}0\,m$ I–V, $h_w = 16{,}2\,m$ VI–XII

I	16	7.1	2	10.5	1	6.0	·	·	60	9.7	3	14.3	3	9.0		·	8	8.5	–	–	–	–	17	–	·	19	7	·	11	–	–	–	17	31	·
II	31	7.8	1	12.0	·	·	·	·	26	10.0	·	·	4	18.5	·	·	22	7.0	–	–	–	–	27	–	·	9	4	·	16	–	–	–	17	28	·
III	34	7.3	·	·	·	·	·	·	27	11.2	·	·	2	10.0	2	2.5	28	6.2	–	–	–	–	23	–	·	11	8	·	13	–	–	–	16	31	·
IV	26	5.8	·	·	1	4.0	·	·	30	7.9	·	·	9	3.0	5	3.6	19	4.9	–	–	–	–	3	–	·	5	3	2	11	–	–	–	12	25	·
V	20	3.2	·	·	·	·	0.5	2.0	33.5	4.9	8	4.8	3	8.3	4	6.0	24	3.4	–	–	–	–	2	–	·	2	·	·	11	–	–	–	16	6	2
VI	49	5.2	·	·	·	·	·	·	12	3.3	8	3.8	2	7.0	·	·	19	3.8	–	–	–	–	·	–	·	2	·	5	6	–	–	–	9	5	2
VII	20	4.0	·	·	·	·	·	·	7	6.3	23	6.0	5	4.4	·	·	38	3.0	103	40.7	18	·	·	·	·	·	·	2	7	16	14	4	11	·	3
VIII	17	3.9	·	·	1	9.0	·	·	24	6.5	15	4.9	2	4.0	3	2.3	31	3.4	63	16.6	15	·	·	·	1	3	·	1	3	13	10	2	6	·	4
IX	8	5.1	·	·	·	·	·	·	34	10.9	8	10.1	3	4.3	6	5.0	31	6.0	129	27.6	23	·	·	·	·	11	8	7	4	13	12	5	13	·	1
X	10	1.6	10	2.6	4.5	1.3	5.5	3.8	10	6.2	24	4.2	4.5	3.1	18.5	3.7	6	3.4	–	–	–	·	·	3	·	6	3	13	10	–	–	–	10	·	·
XI	8	3.2	7.5	2.7	1	5.0	10.5	4.6	29.5	4.6	18	7.5	·	·	6.5	3.6	9	4.4	–	–	–	·	11	18	·	5	4	2	16	–	–	–	17	15	·
XII	8.5	4.4	2.5	11.2	2	4.0	7	4.0	23	8.3	21.5	9.7	3.5	4.1	8	4.2	17	5.9	–	–	–	11	27	31	·	9	8	1	15	–	–	–	18	31	·
Rok	247.5	4.9	23	3.2	10.5	2.4	23.5	1.2	316	7.5	128.5	5.4	41	6.3	53	2.6	252	5.0	–	–	–	–	110	–	1	82	45	33	123	–	–	–	162	172	12

Maków Podhalański $H_s = 350\,m$ $h_w = 18\,m$

I	2	1.0	2	4.5	1.5	3.0	4.5	2.8	2.5	2.0	10.5	5.2	13	4.2	3	6.7	54	1.8	45	10.9	27	5	4	26	·	·	·	4	12	11	7	1	·	–	–
II	1.5	3.0	1.5	1.7	2	3.5	1	2.0	2	3.5	8.5	7.4	11	7.5	15.5	7.6	41	3.4	66	11.5	17	6	10	25	·	6	·	1	21	17	16	1	1	–	–
III	2	3.5	3	2.3	2	1.0	5	3.5	3	2.8	5	3.4	8.5	4.2	4.5	6.1	60	1.3	82	24.5	16	7	9	26	·	1	·	–	–	13	11	2	6	–	–
IV	·	·	3	5.3	8.5	3.6	5	2.7	5	2.2	12.5	5.2	15	4.7	4	4.5	37	2.5	132	74.1	6	·	·	5	6	1	·	9	10	14	9	3	8	·	–
V	2	2.5	1	2.0	5	4.2	10.5	4.5	5	3.6	7.5	3.3	1	1.0	·	·	61	1.3	152	25.0	20	·	·	2	·	·	·	2	11	24	20	5	8	·	–
VI	4	3.5	2	4.5	5	3.0	5	1.8	7.5	2.8	2.5	3.6	12.5	5.7	0.5	6.0	51	1.7	157	43.4	1, 4	·	·	·	6	·	·	9	11	12	12	3	5	·	–
VII	2	2.0	·	·	5	1.8	2•	2.5	3	1.3	7.5	3.9	4.5	3.2	4	2.2	65	0.8	135	50.5	18	·	·	·	5	·	·	–	–	9	9	4	7	·	–
VIII	1	1.0	·	·	8.5	2.1	6	3.1	2	3.8	6.5	3.9	6.5	3.8	2.5	2.4	60	1.1	51	11.9	15	·	·	·	13	1	·	9	4	11	10	1	5	·	–
IX	1	4.0	·	·	5	3.4	5	2.6	6	4.3	3	2.7	6	3.8	·	·	64	1.0	63	15.8	18	·	·	·	6	1	·	–	–	10	7	3	13	·	–
X	3	3.0	3	2.0	4	2.0	2	2.0	6	2.2	1	2.0	3	3.0		·	71	0.6	22	7.5	6	·	·	9	·	·	·	15	8	10	8	·	17	·	–
XI	·	·	2	4.5	5	3.4	4	3.8	3	3.7	4	5.2	3	3.7	·	·	69	0.9	91	15.2	23	·	1	11	·	·	·	3	18	16	14	2	15	–	–
XII	0.5	5.0	4	3.8	8	2.9	4	2.9	6.5	3.4	7.5	5.2	3	5.7	2.5	3.0	57	1.5	70	10.0	13, 31	–	15	–	·	2	·	–	–	15	15	2	3	–	–
Rok	19	2.4	21.5	2.6	59.5	2.8	54	2.8	51.5	3.0	76	4.2	87	4.2	36.5	3.2	690	1.5	1066	74.1	6.IV	–	39	–	36	12	·	–	–	162	138	27	88	–	–

Biecz $H_s = 260\,m$ $h_w = 16{,}1\,m$

I	3	4.0	2	6.0	·	·	·	·	18	6.7	29	4.6	9	3.9	16	5.4	16	4.3	30	7.4	29	2	7	24	·	3	·	2	12	15	7	·	·	17	·
II	10	4.8	1	2.0	5	2.6	1	2.0	1	4.0	16	5.4	9	5.5	19	6.4	22	3.9	30	7.8	19	3	10	26	·	3	·	·	18	21	10	·	·	28	·
III	10	5.9	9	5.8	3	2.3	1	4.0	13	5.8	13	4.9	1	2.0	19	5.3	24	3.9	27	7.0	12	5	9	25	·	4	·	1	16	17	7	·	1	23	·
IV	4	4.0	5	4.0	6	3.3	1	5.0	11	6.3	12	4.8	6	3.5	17	5.1	28	3.3	31	8.0	28	·	·	3	–	2	·	7	9	14	7	·	·	·	·
V	6	3.2	2	3.0	5	2.6	2	3.0	5	5.6	6	3.5	15	6.3	12	4.7	40	2.6	137	25.6	28	·	·	2	·	1	·	·	13	27	19	3	·	·	4
VI	10	5.5	3	2.7	1	3.0	·	·	1	7.0	2	2.5	10	5.5	29	4.4	34	2.9	159	43.0	4	·	·	·	–	3	·	3	12	16	11	6	1	·	3
VII	4	5.5	2	4.0	2	6.0	·	·	2	5.5	9	3.3	12	4.1	20	4.4	42	2.4	143	37.9	17	·	·	·	–	·	·	3	9	13	10	5	·	·	5
VIII			·	·	4	2.8		·	7	4.6	6	5.7	9	3.6	25	4.5	42	2.4	33	12.0	16	·	·	·	11	2	·	6	3	9	6	1	4	·	6
IX	5	3.6	1	2.0	3	4.3	·		11	5.5	8	5.0	13	3.8	13	5.2	36	2.8	65	21.3	5	·	·	·	3	·	·	8	8	10	7	3	7	·	1
X	2	3.5	5	3.2	5	3.6	2	3.0	4	3.5	5	3.6	8	3.0	5	4.6	57	1.4	4	2.3	30	·	·	11	·	·	·	7	5	4	2	·	14	·	·
XI	6	3.7	8	4.1	6	4.0	7	4.9	21	5.7	8	4.2	4	3.5	10	4.0	20	3.6	87	21.8	15	·	1	6	·	·		1	19	17	13	3	6	9	·
XII	17	4.3	8	4.1	4	2.0	·	·	8	7.1	21	5.0	4	3.5	12	4.7	19	3.7	42	10.6	30	10	17	31	·	2	·	1	20	18	6	2	3	17	·
Rok	77	4.0	46	3.4	44	3.0	14	1.8	102	5.6	135	4.4	100	4.0	197	4.9	380	3.1	788	43.0	4.VI	20	44	128	–	20	·	39	144	181	105	23	36	94	19

Jasło $\varphi = 49°44'$ $\lambda = 21°28'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA t												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																					
	P_m	Max	Min	$P_{o,m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.1	-3.0	7.4	23	-15.5	31	-1.7	0.9	-0.9	-0.6	4.7	4.9	4.9	4.8	84	74	83	80	0.9	1.9	1.0	1.3	6.5	5.5	6.2	6.1
II	–	–	–	–	0.5	-5.2	6.3	13	-18.1	25	-3.6	-0.9	-2.3	-2.3	4.1	4.4	4.3	4.3	83	76	81	80	0.8	1.4	1.0	1.1	8.8	7.9	7.5	8.1
III	–	–	–	–	2.7	-4.4	12.9	31	-13.9	20	-3.0	1.5	-0.8	-0.8	4.5	5.0	5.0	4.8	83	72	83	79	0.9	2.1	1.0	1.3	8.0	6.9	5.6	6.8
IV	–	–	–	–	16.7	5.1	27.6	23	-1.6	2	7.0	14.7	10.0	10.4	8.1	8.3	8.8	8.4	80	55	72	69	2.2	10.1	4.0	5.4	5.4	5.9	3.6	5.0
V	–	–	–	–	16.8	6.9	23.8	8	-2.0	2	9.1	14.6	10.9	11.4	10.7	11.3	11.1	11.0	89	67	84	80	1.2	6.0	2.3	3.2	7.7	7.8	6.2	7.2
VI	–	–	–	–	19.5	9.1	30.1	23	3.0	7	11.7	17.6	13.8	14.2	12.8	12.8	13.5	13.0	90	64	82	79	1.4	9.2	3.1	4.6	5.3	6.6	5.7	5.9
VII	–	–	–	–	21.9	10.8	31.3	27	6.3	30	13.5	20.1	15.4	16.1	13.9	14.1	14.8	14.3	89	61	84	78	1.7	10.3	2.9	5.0	5.7	5.9	5.3	5.6
VIII	–	–	–	–	24.3	12.0	31.6	13	4.3	31	14.0	22.9	17.3	17.9	14.7	15.4	16.4	15.5	91	56	82	76	1.5	13.2	3.8	6.2	4.6	5.4	4.0	4.7
IX	–	–	–	–	18.8	7.6	27.4	5	0.4	26	9.4	17.3	12.3	12.8	10.4	11.8	11.8	11.3	88	61	82	77	1.8	8.8	2.9	4.5	5.3	5.5	4.0	4.9
X	–	–	–	–	14.4	2.8	21.4	3	-3.9	22	4.3	13.1	6.8	7.8	7.9	10.1	8.9	9.0	91	67	88	82	0.8	5.3	1.2	2.4	5.7	4.0	2.0	3.9
XI	–	–	–	–	8.5	2.9	16.8	1, 8	-2.8	28	4.3	7.1	5.4	5.6	7.4	8.0	7.8	7.7	87	78	85	83	1.2	2.7	1.4	1.8	7.9	7.9	8.2	8.0
XII	–	–	–	–	-1.8	-6.6	4.4	14	-15.4	27	-4.9	-3.2	-4.4	-4.2	3.8	4.0	3.9	3.9	86	80	84	83	0.6	1.0	0.7	0.8	7.9	8.0	7.4	7.8
Rok	–	–	–	–	12.0	3.2	31.6	13. VIII	-18.1	25. II	5.0	10.5	7.0	7.4	8.6	9.2	9.3	9.0	87	68	82	79	1.2	6.0	2.1	3.1	6.6	6.4	5.5	6.2

Tęgoborze $\varphi = 49°43'$ $\lambda = 20°39'$

I	–	–	–	–	3.4	-2.5	9.2	20, 22	-15.0	31	-1.0	1.9	0.1	0.3	5.0	5.5	5.3	5.3	84	76	84	81	0.9	1.8	1.0	1.2	6.7	6.2	6.8	6.6
II	–	–	–	–	1.5	-5.2	8.7	12	-16.5	25	-3.2	-0.5	-1.9	-1.9	4.0	4.5	4.5	4.3	80	76	81	79	1.0	1.5	1.1	1.2	9.1	7.9	8.6	8.5
III	–	–	–	–	3.1	-4.8	13.9	31	-15.8	27	-3.2	2.0	-1.1	-0.8	4.4	5.3	5.0	4.9	85	75	86	82	0.8	2.0	0.9	1.2	8.5	8.1	6.9	7.8
IV	–	–	–	–	15.3	5.7	26.3	23	0.5	2	7.8	13.6	9.5	10.1	8.6	9.5	9.5	9.2	81	63	79	74	2.2	7.5	2.8	4.2	6.4	6.8	4.7	6.0
V	–	–	–	–	15.6	7.4	24.5	8	0.5	2	9.8	13.6	10.7	11.2	10.5	10.8	11.2	10.8	84	70	86	80	1.9	5.3	1.9	3.0	8.0	8.7	6.4	7.7
VI	–	–	–	–	18.6	9.6	30.9	19	2.3	7	12.4	16.9	13.2	13.9	12.3	13.1	13.0	12.8	84	68	84	79	2.7	7.8	2.9	4.5	6.8	7.5	7.0	7.1
VII	–	–	–	–	21.1	11.5	29.3	26	8.1	6	14.1	19.9	15.0	16.0	13.6	14.7	15.0	14.4	83	64	87	78	2.8	9.1	2.3	4.7	5.5	6.7	6.8	6.3
VIII	–	–	–	–	23.7	13.2	29.5	13	6.9	31	15.5	22.5	16.9	18.0	15.0	16.6	16.3	16.0	85	61	84	77	2.8	11.3	3.3	5.8	5.5	5.8	4.5	5.3
IX	–	–	–	–	18.8	8.6	27.9	5	2.8	27	10.9	17.1	12.4	13.2	11.0	13.4	12.6	12.3	85	69	86	80	2.5	6.9	2.3	3.9	6.5	6.3	4.7	5.8
X	–	–	–	–	14.1	4.6	19.3	3	0.0	17	5.9	12.9	7.5	8.4	8.9	11.6	9.8	10.1	94	77	92	88	0.5	3.6	0.8	1.6	7.7	4.7	4.1	5.5
XI	–	–	–	–	8.2	3.2	17.1	8	-1.7	23, 24	4.6	7.0	5.1	5.4	7.6	8.4	8.1	8.0	89	83	90	87	1.2	2.3	1.0	1.5	8.3	8.4	8.3	8.3
XII	–	–	–	–	-1.3	-7.0	4.7	13	-16.5	27	-4.9	-2.4	-4.2	-3.9	4.0	4.7	4.2	4.3	89	86	89	88	0.5	0.7	0.6	0.6	7.9	8.2	8.4	8.2
Rok	–	–	–	–	11.8	3.7	30.9	19. VI	-16.5	25.II, 27XII	5.7	10.4	6.9	7.5	8.7	9.8	9.5	9.3	85	72	86	81	1.6	5.0	1.7	2.8	7.2	7.1	6.4	6.9

Limanowa $\varphi = 49°42'$ $\lambda = 20°25'$

I	–	–	–	–	3.2	-4.7	7.6	21, 25	-20.0	31	-1.9	1.5	-1.0	-0.6	4.7	4.9	4.8	4.8	83	71	81	78	1.0	2.2	1.1	1.4	7.2	6.7	7.3	7.1
II	–	–	–	–	0.5	-7.6	7.0	13	-19.1	25	-4.2	-1.1	-3.2	-2.9	3.9	4.3	4.3	4.2	85	76	87	83	0.7	1.5	0.8	1.0	9.9	8.3	9.4	9.2
III	–	–	–	–	2.0	-7.3	12.7	5, 30	-20.0	26	-5.0	0.8	-3.2	-2.6	3.9	4.6	4.3	4.3	85	68	85	79	0.7	2.3	0.8	1.3	8.6	8.5	8.3	8.5
IV	–	–	–	–	14.7	2.8	25.8	23	-2.6	2	6.9	13.1	7.0	8.5	8.1	7.7	8.2	8.0	81	57	82	73	2.3	9.3	2.1	4.6	6.9	7.1	6.0	6.7
V	–	–	–	–	15.1	4.6	23.0	8, 19	-3.4	2	9.2	12.7	8.3	9.6	10.1	9.9	10.2	10.1	84	68	91	81	1.9	5.4	1.0	2.8	8.5	9.0	7.5	8.3
VI	–	–	–	–	17.8	6.8	28.9	23	0.2	9	12.4	16.1	11.0	12.6	12.2	12.4	12.1	12.2	82	67	90	80	2.9	7.6	1.5	4.0	7.2	8.3	7.7	7.7
VII	–	–	–	–	20.3	8.3	30.3	26	3.6	30	13.4	18.9	12.6	14.4	13.4	13.3	13.6	13.4	86	61	92	80	2.2	9.3	1.3	4.3	6.9	8.0	7.2	7.4
VIII	–	–	–	–	23.1	9.3	29.9	15	3.1	31	14.3	21.5	13.9	15.9	15.1	15.8	14.7	15.2	92	62	92	82	1.3	10.6	1.5	4.5	6.4	7.0	5.6	6.3
IX	–	–	–	–	18.4	4.6	27.9	4	-1.3	27	8.3	16.4	9.1	10.7	10.1	12.1	10.6	10.9	92	67	91	83	1.3	7.6	1.5	3.5	6.1	6.3	4.8	5.7
X	–	–	–	–	14.1	0.9	21.9	3	-4.4	23	3.1	13.2	3.8	6.0	7.5	10.6	7.9	8.7	96	70	97	88	0.4	5.1	0.3	1.9	6.1	5.1	3.6	4.9
XI	–	–	–	–	7.7	1.5	19.1	8	-5.7	17	3.0	6.4	3.7	4.2	7.0	7.9	7.5	7.5	91	81	92	88	0.8	2.4	0.7	1.3	8.7	8.3	8.4	8.5
XII	–	–	–	–	-1.4	-9.8	5.4	8, 13	-22.4	21	-6.2	-2.9	-5.7	-5.1	3.5	4.0	3.7	3.7	85	78	85	83	0.6	1.3	0.7	0.9	8.5	7.9	8.4	8.3
Rok	–	–	–	–	11.3	0.8	30.3	26. VII	-22.4	21.XII	4.4	9.7	4.7	5.9	8.3	9.0	8.5	8.6	87	69	89	82	1.3	5.4	1.1	2.6	7.6	7.5	7.0	7.4

Żywiec-Sporysz $\varphi = 49°41'$ $\lambda = 19°13'$

I	–	–	–	–	3.1	-2.7	8.8	22	-18.7	31	-0.8	2.1	-0.1	0.3	4.9	4.7	4.8	4.8	81	65	76	74	1.2	2.7	1.6	1.8	7.0	6.9	7.1	7.0
II	–	–	–	–	0.7	-6.6	5.0	12, 13	-19.3	1	-4.3	-0.8	-2.6	-2.6	3.9	4.3	4.4	4.2	84	72	83	80	0.8	1.6	0.9	1.1	8.9	8.1	8.8	8.6
III	–	–	–	–	3.2	-5.6	15.6	5	-16.9	21	-3.8	2.0	-1.7	-1.3	4.2	4.8	4.7	4.6	84	65	83	77	0.8	2.7	1.0	1.5	8.0	7.7	6.9	7.5
IV	–	–	–	–	14.9	4.3	26.9	23, 24	0.2	3	6.8	13.3	8.4	9.2	8.3	8.8	8.6	8.6	83	62	78	74	1.9	8.6	2.9	4.5	7.0	6.9	5.2	6.4
V	–	–	–	–	15.3	5.8	24.0	19	-0.6	5	8.9	13.3	9.9	10.5	10.0	10.6	10.7	10.4	86	70	86	81	1.6	5.4	2.0	3.0	7.3	8.1	7.1	7.5
VI	–	–	–	–	19.0	8.2	29.8	16, 23	2.2	9	11.4	16.8	12.5	13.3	12.3	12.7	12.9	12.6	87	64	86	79	1.8	8.5	2.3	4.2	6.2	7.6	5.7	6.5
VII	–	–	–	–	21.1	9.8	30.1	27	4.5	30	13.2	19.4	14.1	15.2	13.1	13.5	14.2	13.6	86	61	88	78	2.3	9.7	2.2	4.7	6.2	7.4	5.4	6.3
VIII	–	–	–	–	24.4	10.7	31.6	15	5.0	29	13.9	22.4	15.9	17.0	14.4	15.1	15.9	15.1	90	56	88	78	1.7	12.8	2.5	5.7	5.5	6.3	4.7	5.5
IX	–	–	–	–	18.3	6.0	29.1	4	-0.1	25	8.5	16.4	10.3	11.4	10.3	12.0	11.5	11.3	91	65	91	82	1.4	7.5	1.5	3.5	6.5	6.5	3.6	5.5
X	–	–	–	–	14.6	2.5	23.1	4	-3.3	22	3.7	13.4	6.4	7.5	7.9	10.6	9.4	9.3	97	70	96	88	0.3	5.4	0.4	2.0	5.4	4.7	3.7	4.6
XI	–	–	–	–	7.6	1.3	19.8	7	-4.0	22	2.6	6.6	3.4	4.0	7.1	7.9	7.4	7.5	9.4	8.1	9.3	8.9	0.5	2.7	0.7	1.3	8.3	8.5	8.0	8.3
XII	–	–	–	–	-1.6	-9.1	7.3	13	-24.4	22	-6.5	-3.3	-5.9	-5.4	3.6	4.1	3.7	3.8	8.6	8.1	8.6	8.4	0.5	1.0	0.6	0.7	8.0	8.0	7.4	7.8
Rok	–	–	–	–	11.7	2.0	31.6	15. VIII	-24.4	22.XII	4.5	10.1	5.9	6.6	8.3	9.1	9.0	8.8	8.7	6.8	8.6	8.0	1.2	5.7	1.6	2.8	7.0	7.2	6.1	6.8

Jasło — $H_s = 240\,m$ — $h_w = 15{,}8\,m$ — 1962

MIESIĄC	ROZKŁAD WIATRU °D, v=D N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v≥10	v≥15	●	●	Opad R ≥0.1	≥1.0	≥10.0	≡	⊞	⊠
I	2.5	3.4	2	3.0	1	1.0	1	3.0	4.7	7.2	3	2.3	8	3.5	13.5	4.6	15	4.9	37	6.2	27	1	7	25	·	6	·	3	10	18	10	·	1	14	·
II	8	3.0	3	2.0	3	2.7	0.5	3.0	1.5	7.4	1.5	4.3	1.3	6.1	2.1	5.6	19	4.2	43	8.1	17	4	12	27	·	8	·	·	17	20	11	·	·	2.8	·
III	9	4.6	4.5	4.6	2.5	3.4	1	5.0	2.5	5.9	1	2.0	5	4.7	2.0	4.8	25	3.7	60	12.5	16	6	7	25	·	2	·	3	13	18	10	1	1	2.4	·
IV	6.5	2.5	2.5	1.4	4	4.2	·	·	1.9	5.5	1	4.0	1.1	2.4	1.5	4.4	31	2.6	31	9.6	27	·	·	3	6	2	·	9	5	11	6	·	2	·	·
V	5.5	2.1	2.5	1.4	2	2.0	2	3.5	8	6.1	4	3.2	17.5	4.9	15.5	2.9	36	2.4	126	18.8	28	·	·	1	·	3	1	·	13	2.6	2.2	2	3	·	3
VI	1.0	2.4	2	2.0	·	·	·	·	3.5	3.3	0.5	1.0	20.5	3.4	23.5	3.5	30	2.1	123	26.8	4	·	·	·	10	·	·	5	11	15	12	4	2	·	1
VII	6	1.8	4	1.8	1	1.0	1	3.0	5	4.2	2.5	2.0	16	2.9	16.5	3.2	41	1.6	175	73.7	17	·	·	·	5	·	·	3	9	16	14	4	·	·	4
VIII	1.5	3.0	2.5	1.4	1	4.0	·	·	5	5.9	2	3.2	14.5	3.1	21.5	3.6	45	1.8	29	11.5	16	·	·	·	14	·	·	5	4	14	7	1	5	·	4
IX	1.5	1.0	·	·	1	5.0	·	·	9.5	5.7	5	3.3	15.5	2.8	22.5	2.4	35	2.0	52	17.7	5	·	·	·	3	·	·	9	7	14	7	1	6	·	1
X	4	2.4	·	·	1	4.0	·	·	6	4.3	·	·	8	2.0	21	2.0	53	1.1	7	3.9	31	·	·	7	·	·	·	10	5	5	2	·	12		·
XI	11.5	1.9	4	3.0	·	·	2.5	3.4	21.5	4.0	4	2.5	10	2.2	14.5	1.9	22	2.1	87	20.9	15	·	·	6	·	·	·	1	18	18	13	3	5	4	·
XII	10	2.6	1	2.0	·	·	·	·	2.4	7.2	1	2.0	5.5	2.3	22.5	2.8	29	3.0	53	13.9	30	10	18	30	·	3	·	2	20	19	8	3	2	17	
Rok	7.6	2.6	2.8	1.9	16.5	2.3	8	1.7	188.5	5.6	25.5	2.5	144.5	3.4	227	3.5	381	2.6	823	73.7	17.VII	21	44	124	38	24	1	50	132	194	122	19	39	87	13

Tęgoborze — $H_s = 272\,m$ — $h_w = 17{,}6\,m$

I	2	3.0	·	·	·	·	4	3.0	2.6	3.5	4	4.2	3	1.7	8	2.2	46	1.6	32	11.8	29	2	6	21	·	·	·	2	12	9	7	1	·	6	·
II	2	1.5	·	·	2	1.0	1	1.0	1.1	5.8	2	7.5	1.4	4.0	1.0	3.3	42	2.1	50	8.1	17	5	10	25	·	3	1	·	18	18	14	·	·	18	·
III	6	4.5	·	·	2	1.5	5	2.4	4	4.0	1	4.0	5	2.4	4	3.8	66	1.0	75	20.1	16	4	6	24	·	·	·	1	18	12	12	2	3	15	·
IV	·	·	1	2.0	2	1.0	3	3.7	2.6	4.6	1	2.0	9	2.3	5	2.2	43	1.9	69	22.3	6	·	·	·	3	1	·	5	8	11	11	2	·	·	1
V	1	2.0	·	·	·	·	2	3.0	2.2	2.8	1	4.0	9	2.4	1	2.0	57	1.1	108	13.5	20	·	·	·	·	·	·	1	15	2.4	20	2	·	·	2
VI	·	·	·	·	3	1.0	·	·	8	1.6	2	1.5	12	1.8	1	2.0	64	0.5	154	37.9	5	·	·	·	6	·	·	2	13	15	13	4	1	·	3
VII	·	·	·	·	·	·	·	·	1.3	1.9	1	2.0	7	1.7	·	·	72	0.4	169	65.8	17	·	·	·	5	·	·	4	10	15	14	4	·	·	5
VIII	·	·	·	·	1	1.0	·	·	2.5	2.5	1	2.0	5	1.6	1	1.0	60	0.8	62	26.5	6	·	·	·	13	1	·	2	3	9	6	3	2	·	2
IX	·	·	·	·	1	3.0	·	·	2.3	2.4	8	4.0	9	2.0	1	5.0	48	1.3	61	17.9	18	·	·	·	5	·	·	6	7	9	9	3	4	·	2
X	1	1.0	·	·	4	2.5	1	3.0	1.6	2.1	1	2.0	3	1.3	1	2.0	66	0.6	7	2.3	30	·	·	·	·	·	·	6	9	5	3	·	14	·	·
XI	·	·	·	·	3	2.7	1	2.0	2.7	3.8	·	·	1	3.0	1	1.0	57	1.3	8.3	13.2	23	·	·	6	·	·	·	1	21	13	12	2	5	4	·
XII	1	1.0	1	2.0	3	2.3	3	3.7	1.7	4.4	2	3.0	·	·	1	3.0	65	1.1	61	13.5	30	10	13	28	·	1	·	·	18	15	13	2	·	18	·
Rok	1.3	1.1	2	0.3	2.1	1.3	2.0	1.8	21.8	3.3	2.4	3.0	7.7	2.0	3.4	2.3	686	1.1	931	65.8	17.VII	21	35	104	32	6	1	30	152	155	134	25	29	61[2]	15

Limanowa — $H_s = 440\,m$ — $h_w = 16\,m$

I	3	2.5	2.5	2.2	7	3.6	2.5	3.0	6	3.0	3.5	3.0	19.5	4.0	23.5	3.6	3	3.3	31	7.0	29	6	4	25	·	·	·	·	13	12	8	·	·	2.4	·
II	7.5	2.8	·	·	4.5	3.1	1.4	3.0	3.5	2.6	5	6.2	18.5	11.4	2.7	5.4	4	5.4	46	7.6	17	7	10	27	·	7	4	·	23	21	11	·	2	2.8	·
III	4.5	3.7	6	3.2	5.5	3.3	21.5	3.0	4.5	2.9	7	2.4	12.5	5.6	25.5	3.7	6	3.4	60	13.6	16	8	12	27	·	1	1	·	21	18	12	1	7	2.9	·
IV	3	2.8	5	1.9	6	2.8	1.5	3.6	9	5.2	5	3.0	12	3.8	2.4	3.0	11	3.0	122	59.6	6	·	·	5	2	·	·	4	12	13	10	2	3	3	·
V	5.5	1.5	4	2.2	3.5	2.7	11	2.1	5	2.3	7	3.2	19.5	4.0	28.5	2.6	9	2.5	113	19.7	20	·	·	4	·	1	·	1	19	23	20	5	2	·	4
VI	6	2.2	1	3.0	2	2.8	5	2.5	1.5	2.0	6.5	2.4	19	3.7	3.9	3.4	10	2.8	199	49.2	3	·	·	·	5	·	·	·	17	13	12	5	1	·	5
VII	10	2.1	6	1.9	0.5	1.0	10	2.4	6.5	2.1	3.5	2.0	14	3.3	27.5	2.7	15	2.1	171	76.5	18	·	·	·	5	·	·	2	19	14	11	4	2	·	6
VIII	8	2.1	1	1.0	2	2.8	12.5	2.3	7	2.4	5	2.6	12	3.5	20.5	2.8	25	2.0	72	37.5	5	·	·	·	11	1	·	1	8	13	5	3	3	·	3
IX	4	1.5	3	2.7	1.5	2.7	1.5	2.6	9	2.3	6	2.7	15.5	3.7	22	3.1	14	2.4	68	14.1	18	·	·	3	4	·	·	4	8	12	9	4	5	·	·
X	1.6	1.9	5.5	2.1	3	2.7	1.6	2.5	3.5	2.4	8.5	2.1	6.5	3.0	22	2.5	12	2.0	8	2.4	30	·	·	13	·	·	·	8	7	7	3	·	12	·	·
XI	1.5	2.4	·	·	5	4.1	2.8	3.4	1.0	3.4	·	·	3.5	3.4	20.5	2.6	8	2.8	70	15.8	15	·	1	11	·	·	·	3	23	18	12	1	14	12	·
XII	1.1	2.5	2.5	2.2	8.5	3.6	9.5	3.8	4	3.5	1.0	2.3	1.0	3.5	28.5	2.8	9	2.7	53	13.6	14	12	16	31	·	·	·	1	22	19	8	2	1	31	·
Rok	93.5	2.3	36.5	1.9	49	2.9	182.5	2.8	69.5	2.8	67	2.7	162.5	4.4	308.5	3.2	126	2.9	1013	76.5	18.VII	33	43	146	27	10	5	24	192	183	121	27	52	127	18

Żywiec-Sporysz — $H_s = 360\,m$ — $h_w = 20{,}6\,m$

I	2.5	2.0	1.5	1.0	·	·	1.0	1.4	17.5	3.1	30.5	3.0	4	2.4	9	2.7	18	2.2	61	20.0	28	2	4	22	·	1	·	2	14	14	11	1	·	11	·
II	1.5	1.0	2	1.0	2.5	1.8	4	1.2	9	5.6	11	5.1	10.5	8.0	12.5	3.6	31	3.0	71	11.4	12	7	9	24	·	4	3	1	21	20	13	1	7	2.8	1
III	10.5	2.6	4.5	3.3	2.5	2.2	1	2.5	5	1.7	5	1.7	6	2.9	9.5	2.5	49	1.2	92	28.1	16	7	9	24	·	3	·	1	17	17	12	3	6	2.5	·
IV	2.5	2.6	1.5	1.0	3.5	1.1	4.5	1.8	8.5	3.5	6	2.7	8.5	2.1	8	2.5	47	1.2	90	38.1	6	·	·	·	7	·	·	6	9	13	7	3	5	·	1
V	2	1.0	2	1.0	·	·	1.5	1.0	10.5	1.5	1.3	2.5	9	1.8	9	1.5	46	0.9	162	32.1	20	·	·	2	·	·	·	1	14	2.6	17	8	6	·	4
VI	1.5	1.0	3	1.3	2.5	1.8	1.5	1.3	2.5	2.2	6.5	2.1	16	2.0	15.5	1.8	41	1.0	138	31.6	1	·	·	·	6	1	1	3	11	13	12	6	1.4	·	3
VII	1	1.0	0.5	1.0	2.5	1.0	3	1.5	6	2.0	1.3	1.7	12.5	1.6	10.5	1.8	44	0.9	73	41.5	18	·	·	·	6	·	·	3	9	14	11	1	3	·	7
VIII	·	·	2	1.0	1.5	1.0	5.5	1.2	6.5	2.4	13.5	2.7	13	2.0	6	1.8	45	1.1	39	10.6	15	·	·	·	16	2	2	2	4	14	10	1	3	·	5
IX	·	·	1	1.0	0.5	1.0	3.5	1.0	8	2.0	16.5	2.6	10.5	1.8	6	1.6	44	1.0	93	17.8	23	·	·	1	4	·	·	7	9	14	10	5	10	·	2
X	0.5	1.0	1	1.0	3.5	1.4	2	1.2	4.5	2.3	8	2.1	6.5	1.5	8	1.4	59	0.6	39	11.4	6	·	·	7	·	·	·	11	9	9	7	1	2.6	·	·
XI	·	·	4.5	1.0	5	1.5	4.5	1.6	7.5	1.8	2.5	3.8	4	1.9	2	1.8	60	0.6	114	23.9	20	·	1	10	·	·	·	2	22	17	14	3	1.3	10	·
XII	5.5	1.6	6.5	1.8	2.5	2.0	5	1.7	11	4.6	7	3.8	2	3.2	6.5	2.4	47	1.4	52	13.4	13	14	15	29	·	2	2	1	19	16	11	1	3	31	·
Rok	27.5	1.2	3.0	1.3	26.5	1.2	4.6	1.4	9.6.5	2.7	132.5	2.8	102.5	2.6	102.5	2.1	531	1.3	1024	41.5	18.VII	30	38	119	39	13	8	40	158	187	135	34	96	105	23

Krosno $\varphi = 49°41'$ $\lambda = 21°45'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.2	-3.8	6.4	23	-14.9	31	-1.8	0.0	-1.1	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.8	7.3	7.2
II	–	–	–	–	-0.4	-6.8	3.1	13, 21	-21.9	25	-4.2	-1.7	-3.1	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.2	8.1	8.3
III	–	–	–	–	1.8	-5.8	12.6	31	-17.7	20	-3.3	0.6	-1.3	-1.3	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.5	7.0	7.6
IV	–	–	–	–	17.1	4.2	26.4	23	-1.6	2,3,8,30	7.7	14.4	9.6	10.3	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.4	5.0	5.4
V	–	–	–	–	16.2	5.9	24.1	28	-2.6	2	9.0	14.8	10.9	11.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.4	7.3	7.4
VI	–	–	–	–	18.9	8.6	28.3	16	0.6	5	11.3	17.6	13.7	14.1	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.1	7.3	6.5
VII	–	–	–	–	20.6	10.1	29.3	27	5.3	30	13.2	19.4	15.5	15.9	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.1	5.9	6.1
VIII	–	–	–	–	23.3	11.5	29.7	13	3.3	31	13.4	22.2	17.6	17.7	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.5	5.9	5.8
IX	–	–	–	–	18.1	7.0	27.5	5	-0.1	27	9.2	16.6	12.5	12.7	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.1	5.6	5.9
X	–	–	–	–	14.0	2.3	19.9	3	-5.8	16	4.3	13.3	7.6	8.2	–	–	–	–	–	–	–	–	–	–	–	–	6.6	4.2	2.7	4.5
XI	–	–	–	–	8.5	2.2	16.9	6	-4.0	18	4.3	8.0	5.0	5.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.0	7.5	8.0
XII	–	–	–	–	-2.1	-7.1	5.6	14	-15.6	23	-5.0	-3.0	-4.6	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.6	8.7	8.7
Rok	–	–	–	–	11.4	2.4	29.7	13.VIII	-21.9	25. II	4.8	10.2	6.9	7.2	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.7	6.5	6.8

Bircza $\varphi = 49°41'$ $\lambda = 22°29'$

I	–	–	–	–	2.7	0.1	9.7	22	-14.2	31	-0.6	1.4	-0.1	0.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.4	6.7	6.8
II	–	–	–	–	-0.6	-6.6	3.5	13	-16.2	26	-4.6	-1.7	-3.0	-3.1	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.2	8.1	8.3
III	–	–	–	–	2.1	-5.7	13.8	6	-19.6	20	-3.6	0.8	-1.9	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.6	6.0	7.3
IV	–	–	–	–	15.9	3.4	25.4	22, 23	-1.4	2	6.9	14.4	8.9	9.8	–	–	–	–	–	–	–	–	–	–	–	–	5.4	4.8	3.9	4.7
V	–	–	–	–	16.2	6.5	25.2	28	-3.5	2	9.7	14.9	10.4	11.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.5	6.0	6.8
VI	–	–	–	–	18.1	8.3	28.1	16	1.8	9	12.3	16.4	12.8	13.6	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.5	6.4	6.3
VII	–	–	–	–	20.1	9.9	30.0	27	4.7	30	13.9	18.7	14.2	15.2	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.2	5.2	5.8
VIII	–	–	–	–	23.1	11.2	29.9	13	3.4	31	14.0	21.9	16.2	17.1	–	–	–	–	–	–	–	–	–	–	–	–	5.6	4.9	4.0	4.8
IX	–	–	–	–	18.0	6.8	27.4	5	-0.1	26	9.7	16.6	11.0	12.1	–	–	–	–	–	–	–	–	–	–	–	–	5.7	4.9	5.3	5.3
X	–	–	–	–	13.7	2.0	19.4	2	-5.0	17	4.0	12.5	5.7	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.4	4.3	3.6	4.8
XI	–	–	–	–	8.1	1.4	16.6	4	-4.7	18	3.0	6.4	4.2	4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.6	7.4	7.8
XII	–	–	–	–	-1.4	-7.2	7.9	14	-15.6	26	-4.9	-3.2	-4.6	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.2	6.8	7.7
Rok	–	–	–	–	11.3	2.5	30.0	27.VII	-19.6	20. III	5.0	9.9	6.7	6.8	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.4	5.8	6.4

Mszana Dolna $\varphi = 49°40'$ $\lambda = 20°05'$

I	–	–	–	–	2.8	-3.7	9.4	22	-17.3	31	-1.9	1.7	-0.6	-0.4	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.3	7.1	6.8
II	–	–	–	–	0.2	-7.0	4.4	7, 13	-23.3	25	-4.9	-1.2	-3.4	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	9.8	8.2	9.5	9.2
III	–	–	–	–	2.4	-7.0	14.4	5	-19.5	21	-5.1	1.3	-2.7	-2.3	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.5	7.5	7.7
IV	–	–	–	–	14.3	2.9	25.8	23	-1.2	2	6.1	12.8	7.7	8.3	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.1	5.2	6.3
V	–	–	–	–	14.9	5.7	22.4	19	-0.8	2	8.9	12.7	9.1	10.0	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.8	7.5	7.9
VI	–	–	–	–	17.8	7.4	29.6	16	1.2	7	11.4	16.4	12.1	13.0	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.9	6.7	7.0
VII	–	–	–	–	20.2	9.3	29.3	27	3.6	30	13.0	19.1	13.8	14.9	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.6	6.5	6.7
VIII	–	–	–	–	23.3	10.2	30.5	7	4.7	29	14.2	22.1	15.3	16.7	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.5	5.3	5.8
IX	–	–	–	–	18.2	5.5	27.6	4	-0.6	27	8.2	16.5	10.4	11.4	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.8	3.8	4.8
X	–	–	–	–	14.3	1.4	21.5	11	-3.9	17	3.1	13.6	5.4	6.9	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.3	3.7	4.2
XI	–	–	–	–	7.7	0.8	19.7	8	-3.2	18	2.0	6.7	3.2	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.3	8.6	8.3
XII	–	–	–	–	-2.0	-10.4	5.7	13	-24.8	21	-6.9	-3.3	-6.9	-6.0	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.3	6.9	7.3
Rok	–	–	–	–	11.2	1.3	30.5	7.VIII	-24.8	21.XII	4.0	8.9	5.2	6.1	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.1	6.5	6.8

Wisła $\varphi = 49°39'$ $\lambda = 18°52'$

I	–	–	–	–	2.1	-3.0	7.5	20	-18.1	31	-1.6	0.8	-0.7	-0.6	5.1	5.9	5.5	5.5	8.9	8.8	9.1	8.7	0.6	0.8	0.5	0.6	6.9	6.9	6.4	6.7
II	–	–	–	–	0.0	-7.3	6.1	10	-21.7	1	-5.1	-1.3	-3.1	-3.2	4.1	5.0	4.7	4.6	8.7	8.9	9.0	8.9	0.5	0.6	0.4	0.5	8.3	8.3	8.2	8.3
III	–	–	–	–	2.0	-6.4	13.2	31	-17.0	26	-4.5	0.6	-2.3	-2.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.5	6.6	7.2
IV	–	–	–	–	13.6	3.2	26.8	25	-1.7	2	6.3	12.6	7.2	8.3	7.9	9.2	8.3	8.5	8.3	6.7	8.2	7.7	2.1	7.4	2.3	3.9	6.3	6.2	5.9	6.1
V	–	–	–	–	14.3	5.1	21.9	31	-1.0	2, 5	8.6	12.2	9.1	9.8	10.1	11.0	10.5	10.5	8.9	7.8	9.0	8.6	1.3	4.3	1.4	2.3	7.4	8.6	7.7	7.9
VI	–	–	–	–	18.1	7.7	29.0	24	2.1	9	10.5	16.0	12.4	12.8	11.9	12.4	12.6	12.3	9.0	6.7	8.4	8.0	1.4	7.6	2.5	3.8	6.2	7.0	5.4	6.2
VII	–	–	–	–	20.0	9.7	29.4	27	4.2	6	12.4	18.5	14.1	14.8	12.9	14.0	14.0	13.6	8.9	6.6	8.7	8.1	1.8	8.3	2.4	4.2	5.8	6.3	5.4	5.8
VIII	–	–	–	–	23.0	10.5	30.3	15	4.4	31	13.1	22.0	15.4	16.5	14.0	15.3	15.3	14.9	9.2	5.8	8.6	7.9	1.3	12.0	2.5	5.3	4.1	5.3	4.9	4.8
IX	–	–	–	–	17.1	6.2	27.0	4	-0.2	25	8.4	15.6	10.0	11.0	10.4	12.2	11.4	11.3	9.2	7.1	9.2	8.5	1.2	6.2	1.4	2.9	5.0	6.1	3.6	4.9
X	–	–	–	–	13.4	2.8	21.9	1	-2.0	25	4.2	12.3	5.8	7.0	8.0	10.9	9.0	9.3	9.5	7.7	9.6	8.9	0.5	4.0	0.4	1.6	4.7	4.7	3.7	4.4
XI	–	–	–	–	6.8	1.0	17.1	8	-6.1	22	2.7	5.8	3.3	3.8	7.0	8.3	7.5	7.6	9.3	8.8	9.4	9.2	0.7	1.6	0.5	0.9	8.1	8.0	8.1	8.1
XII	–	–	–	–	-1.5	-8.8	5.8	13	-24.3	22	-6.3	-2.8	-5.9	-5.2	3.8	4.6	3.9	4.1	9.1	8.7	9.2	9.0	0.4	0.7	0.3	0.4	6.8	6.2	6.7	6.6
Rok	–	–	–	–	10.7	1.7	30.3	15.VIII	-24.3	22.XII	4.1	9.4	5.4	6.1	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.8	6.0	6.4

Krosno — $H_s = 282\,m$ — $h_w = 15\,m$ — 1962

Miesiąc	Rozkład wiatru (%D, %mD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Liczba dni (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	≥15	●	●	Opad R ≥0.1	≥1.0	≥10.0	■	■	■
I	1.5	6.0	·	·	6	5.0	4.5	5.1	5.0	8.4	4.5	2.6	8.5	4.6	11	6.2	7	6.5	20	6.7	13	1	8	28	·	11	·	1	14	13	5	·	·	15	·
II	9	4.9	·	·	10	3.0	2	4.5	13	11.0	3	7.3	13	5.2	15	6.2	19	4.9	27	7.7	13	6	14	28	·	6	2	·	16	17	7	·	3	28	·
III	12	5.0	7	5.9	10	4.2	5	4.6	24	6.7	2	3.0	6	5.1	8	6.0	19	4.4	30	8.1	12	7	11	25	·	3	·	1	15	15	10	·	2	26	·
IV	5.5	4.2	4	3.2	12	3.8	7.5	5.7	16.5	6.6	6	4.2	9	4.4	11.5	6.5	18	4.2	26	8.7	27	·	·	4	3	3	1	5	7	8	7	·	2	·	·
V	9	3.3	1.5	2.7	8	3.0	2.5	3.6	17	4.4	2.5	4.0	6	4.2	27.5	5.6	19	3.3	102	11.7	9	·	·	4	·	2	1	·	13	27	24	2	3	·	2
VI	10	4.7	·	·	6	2.3	1.5	3.3	4.5	5.3	1	3.0	5	6.2	3.5	4.0	27	3.3	161	49.3	4	·	·	·	6	·	·	4	9	16	14	6	3	·	3
VII	6.5	5.4	6	3.3	6	4.7	1	1.0	13	5.1	5	3.6	8	4.5	22.5	5.2	25	3.5	125	24.3	19	·	·	·	4	1	·	3	7	15	12	5	—	·	3
VIII	4	4.8	5	3.2	5	4.6	4.5	3.3	14	5.6	3	3.7	1	4.0	22.5	5.1	34	3.0	47	19.7	6	·	·	·	10	1	1	1	3	13	8	2	7	·	3
IX	1.5	5.3	1.5	6.0	8	3.8	8	3.3	12	7.2	6.5	4.1	5.5	4.1	18	5.0	29	3.4	39	12.4	5	·	·	1	2	4	1	6	11	16	7	1	10	·	1
X	7	3.4	1.5	4.7	5	2.8	8	3.2	11.5	4.7	5.5	5.3	3	4.0	15.5	4.3	36	2.5	8	2.1	19	·	·	9	·	1	·	8	5	13	3	·	11	·	·
XI	1.5	5.3	2	3.5	20	5.0	16.5	5.1	16.5	7.0	8	4.7	·	·	19.5	4.9	6	5.0	67	13.9	23	·	1	7	·	2	·	·	18	21	11	2	7	9	·
XII	12.5	4.7	8	3.5	8	4.2	1.5	4.0	28.5	8.8	4.5	4.4	1.5	5.3	14.5	4.3	14	5.1	40	12.3	30	10	18	30	·	8	1	1	21	14	6	1	4	19	·
Rok	8.0	4.8	36.5	3.0	10.4	3.9	62.5	3.9	220.5	6.7	51.5	4.2	66.5	4.3	220.5	5.3	258	4.1	692	49.3	4.VI	24	52	136	25	42	7	30	139	188	114	19	—	97	12

Bircza — $H_s = 300\,m$ — $h_w = 16\,m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	≥15	●	●	Opad R ≥0.1	≥1.0	≥10.0	■	■	■
I	·	·	4	5.2	2	9.0	·	·	10.5	4.8	33.5	3.4	20	4.7	10	3.1	13	3.5	25?	6.5	29	2	6	23	·	2	·	2	13	12	6	·	·	—	—
II	3	3.3	5	2.0	8	4.0	7	2.7	2	2.5	13	7.1	13.5	7.2	14.5	5.1	18	4.2	39	8.6	13	6	13	28	·	6	1	·	18	14	13	·	·	28	—
III	6	4.2	11.5	4.7	10	4.8	4	5.1	10.5	3.5	8	3.4	13.5	6.0	9.5	4.7	20	3.6	43	—	—	7	13	25	·	5	3	·	14	12	12	1	·	30	—
IV	5.5	3.0	4.5	2.4	8	5.5	6	4.0	9	3.9	8	4.4	8.5	4.4	6.5	4.3	34	2.6	39	12.5	6	·	·	6	3	3	1	7	4	7	7	2	1	·	—
V	1	2.0	2	1.5	2	4.0	1	1.0	4	6.2	5	3.6	3.4	3.4	16	2.5	28	2.3	109	18.1	10, 20	·	·	4	1	1	·	·	10	23	17	3	2	·	—
VI	1.3	2.5	·	·	5	1.6	1	6.0	·	·	4	3.0	21.5	3.4	14.5	4.6	31	2.2	155	38.9	4	·	·	·	5	·	·	4	10	14	11	6	·	·	—
VII	2.5	2.8	6	1.7	6	2.3	2	1.0	4	1.8	13	2.2	16	3.7	11.5	1.8	32	1.6	127	31.1	19	·	·	·	3	·	·	3	8	15	13	6	·	·	—
VIII	0.5	3.0	·	·	3	3.3	3	3.0	6.5	4.5	8	1.9	2.0	3.3	10	2.8	42	1.7	61	13.5	22	·	·	·	11	·	·	2	4	15	12	1	4	·	—
IX	1	2.0	2	2.0	7	3.1	1	2.0	3	5.3	19.5	3.0	1.8	3.6	4.5	3.0	34	2.0	57	14.2	7	·	·	1	2	1	·	5	7	10	9	3	5	·	—
X	1	1.0	7	1.9	11.5	1.9	2.5	2.0	1	3.0	10.5	3.6	1.3	3.1	3.5	2.7	43	1.5	5	2.1	15, 31	·	·	11	·	·	·	7	6	4	2	·	8	·	—
XI	·	·	4	2.5	14.5	3.8	2.3	3.3	6.5	3.8	7.5	3.5	16.5	2.7	·	·	18	2.6	69	13.0	16	·	·	10	·	·	·	·	16	14	12	3	2	2	—
XII	4	2.2	12	3.2	8.5	3.3	3.5	2.9	5	4.6	16	5.0	13.5	3.6	4.5	3.3	26	2.7	39	8.3	30	10	15	30	·	2	·	·	17	11	11	·	1	18	—
Rok	37.5	2.2	58	2.3	85.5	3.9	54	2.8	62	3.7	146	3.7	208	4.1	105	3.2	339	2.5	768?	38.9	4.VI	25	47	138	25	20	5	30	127	151	125	25	23	—	—

Mszana Dolna — $H_s = 410\,m$ — $h_w = 16\,m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	≥15	●	●	Opad R ≥0.1	≥1.0	≥10.0	■	■	■
I	5	2.2	2.5	1.4	2	1.5	4	2.5	8	3.8	24.5	3.4	5	4.5	18	2.8	24	2.3	39	8.0	27	4	4	23	·	·	·	3	14	13	9	·	·	25	—
II	5.5	2.5	0.5	3.0	0.5	3.0	0.5	3.0	3.5	4.1	8.5	4.8	15.5	4.9	21.5	3.1	28	2.6	44	7.6	19	8	10	26	·	3	·	·	23	18	14	·	·	28	—
III	7.5	3.6	4.5	2.6	·	·	·	·	3.5	4.9	8	3.5	4	4.2	22.5	2.5	43	1.7	55	14.0	15	8	11	25	·	·	·	3	20	15	10	2	1	28	—
IV	5	1.6	1.5	2.3	2.5	1.8	4	1.5	3.5	3.7	11.5	2.5	6	2.9	14	2.6	42	1.3	124	60.6	6	·	·	4	3	·	·	5	11	13	11	3	1	1	—
V	6.5	1.9	1	1.5	1.5	1.3	2	1.8	3.5	2.7	7	2.4	8.5	3.6	19	2.6	44	1.4	131	15.8	24	·	·	1	·	1	1	1	17	25	21	6	·	·	—
VI	1.0	1.8	0.5	2.0	·	·	1	2.0	0.5	2.0	5.5	1.9	6	3.0	25.5	2.3	41	1.2	237	59.5	4	·	·	·	5	·	·	5	15	13	13	5	·	·	—
VII	6.5	2.5	1.5	2.0	·	·	1	2.0	3	2.7	8.5	3.1	7.5	2.5	23	2.1	42	1.3	206	94.4	18	·	·	·	5	·	·	3	12	13	9	4	·	·	—
VIII	4.5	1.6	3.5	1.4	2.5	1.4	3	1.8	2.5	2.4	3	4.2	9	3.3	19	2.4	46	1.2	61	16.3	16	·	·	·	11	·	·	3	9	12	8	3	·	·	—
IX	2	2.0	1	2.5	2	2.8	2.5	2.4	·	·	5	2.3	11	2.0	19.5	1.9	47	1.0	62	16.5	18	·	·	2	5	·	·	9	4	11	11	3	4	·	—
X	5.5	2.7	1.5	3.0	2.5	2.4	·	·	1	2.0	5	2.0	4.5	2.3	21	2.0	52	1.0	10	3.3	6	·	·	12	·	·	·	14	9	8	5	·	3	·	—
XI	5.5	1.7	3	2.5	3	2.5	2	2.0	1.5	2.3	2	2.2	5	2.7	15	1.6	53	0.8	76	17.8	15	·	2	12	·	·	·	2	23	17	12	2	4	12	—
XII	1.5	2.3	5	2.5	1.5	2.0	2	2.0	5.5	2.8	1.2	3.9	5	1.9	8	3.1	39	1.6	44	8.7	14	15	15	31	·	2	·	2	15	17	11	·	·	31	—
Rok	78.5	2.2	26	2.2	18	1.6	22	1.8	36	2.7	100.5	3.0	87	3.2	226	2.4	501	1.4	1089	94.4	18.VII	35	42	136	29	6	1	50	172	175	134	28	13	125	—

Wisła — $H_s = 430\,m$ — $h_w = 14.5\,m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	≥15	●	●	Opad R ≥0.1	≥1.0	≥10.0	■	■	■
I	3	2.7	·	·	3	1.7	2.3	3.1	3.4	2.5	·	·	1.5	3.7	26.5	2.8	2	2.7	72	11.1	24	2	5	22	·	·	·	4	15	16	14	2	·	19?	·
II	2	2.0	·	·	·	·	15.5	3.0	9.5	2.4	1	2.0	5	2.2	4.8	2.9	3	2.7	99	14.8	13	7	11	26	·	·	·	2	20	21	15	4	·	28	·
III	7	2.7	0.5	3.0	2	1.5	14.5	1.8	24.5	2.7	·	·	·	·	43.5	2.4	1	2.4	91	21.3	16	8	10	24	·	·	·	1	19	17	12	3	·	25	·
IV	4	1.6	1	1.0	3	1.3	10.5	2.0	33.5	2.6	·	·	2.5	2.0	33.5	2.4	2	2.3	122	38.5	6	·	·	5	3	·	·	6	13	17	14	4	1	2	2
V	4.5	1.9	·	·	1	2.0	10.5	2.0	28	2.4	0.5	2.0	4	2.2	44.5	2.2	·	2.2	235	37.0	20	·	·	4	·	·	·	1	20	26	21	9	·	·	4
VI	8	2.8	·	·	2	2.0	7.5	2.0	14.5	1.8	·	·	4	2.0	52	2.4	2	2.2	138	58.7	4	·	·	·	5	·	·	5	14	14	12	5	·	·	·
VII	3.5	2.1	·	·	1	1.0	11	2.2	32	1.9	1	2.0	1	2.0	41.5	1.9	2	1.9	72	34.6	18	·	·	·	6	·	·	5	11	16	14	2	·	·	4
VIII	1	2.0	·	·	1	1.0	1.3	1.5	4.8	2.2	·	·	3	1.7	27	2.2	·	2.1	41	9.9	7	·	·	·	11	·	·	6	6	14	10	·	1	·	3
IX	5	1.8	1	1.0	1.5	1.3	11.5	1.6	3.3	2.4	·	·	4.5	2.2	29.5	1.8	4	1.9	84	20.1	23	·	·	1	2	·	·	10	8	14	13	3	2	·	·
X	3	2.0	·	·	1	1.0	2.1	1.1	2.2	1.8	2	1.0	1.5	1.7	39.5	2.0	3	1.6	58	20.3	5	·	·	5	·	·	·	13	10	10	9	2	10	·	·
XI	1.5	2.0	·	·	·	·	8	2.0	3.5	2.1	·	·	4	1.8	40.5	2.0	1	2.0	97	14.9	19	·	3	12	·	·	·	3	22	18	16	2	5	12	·
XII	6	1.8	·	·	0.5	4.0	21.5	2.3	2.7	2.6	·	·	2	1.5	3.6	2.2	·	2.3	67	13.8	16	11	16	30	·	·	·	2	15	13	10	1	2	31	·
Rok	4.8.5	2.1	2.5	0.4	16	1.4	167.5	2.0	34.1	2.3	4.5	0.6	33	1.9	46.2	2.3	20	2.2	1176	38.5	6.IV	28	45	129	27	·	·	58	172	196	169	37	21	109?	13

Luboń Wielki $\varphi = 49°39'$ $\lambda = 19°59'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.3	-6.0	3.7	19, 22	-17.8	31	-4.0	-2.7	-4.0	-3.7	–	–	–	–	–	–	–	–	–	–	–	–	84	72	84	80
II	–	–	–	–	-3.4	-8.7	-0.4	13	-15.9	1	-7.4	-5.0	-6.2	-6.2	–	–	–	–	–	–	–	–	–	–	–	–	97	90	96	94
III	–	–	–	–	-1.9	-7.6	10.7	5	-14.3	17	-6.3	-3.5	-5.3	-5.1	–	–	–	–	–	–	–	–	–	–	–	–	86	88	84	86
IV	–	–	–	–	8.7	2.9	20.5	21, 22	-4.6	7	4.7	7.6	5.6	5.9	–	–	–	–	–	–	–	–	–	–	–	–	76	82	70	76
V	–	–	–	–	10.5	3.2	18.5	8	-5.2	1	5.0	7.9	6.2	6.3	–	–	–	–	–	–	–	–	–	–	–	–	85	94	82	87
VI	–	–	–	–	13.2	6.5	25.2	16	-1.9	7	8.4	11.3	9.1	9.5	–	–	–	–	–	–	–	–	–	–	–	–	73	93	86	84
VII	–	–	–	–	16.0	8.6	25.4	27	3.6	6	10.5	14.4	11.3	11.9	–	–	–	–	–	–	–	–	–	–	–	–	78	85	75	79
VIII	–	–	–	–	19.2	10.9	27.4	15	5.2	31	12.7	17.4	13.6	14.3	–	–	–	–	–	–	–	–	–	–	–	–	71	79	66	72
IX	–	–	–	–	13.5	5.9	23.7	4	1.6	25	7.3	11.7	8.6	9.0	–	–	–	–	–	–	–	–	–	–	–	–	72	79	61	71
X	–	–	–	–	10.5	4.6	17.5	11	-1.3	16	6.1	9.1	6.7	7.2	–	–	–	–	–	–	–	–	–	–	–	–	55	55	42	51
XI	–	–	–	–	4.3	-0.6	14.3	8	-6.8	24	0.9	2.8	1.4	1.6	–	–	–	–	–	–	–	–	–	–	–	–	87	86	88	87
XII	–	–	–	–	-4.3	-9.5	3.5	8	-22.8	23	-7.6	-6.2	-7.1	-7.0	–	–	–	–	–	–	–	–	–	–	–	–	80	83	82	82
Rok	–	–	–	–	7.2	0.8	27.4	15.VIII	-22.8	23.XII	2.5	5.4	3.3	3.6	–	–	–	–	–	–	–	–	–	–	–	–	79	82	76	79

Zawoja $\varphi = 49°37'$ $\lambda = 19°31'$

I	–	–	–	–	2.5	-4.2	10.3	1	-18.5	31	-1.5	0.5	-1.1	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	61	64	67	64
II	–	–	–	–	-0.9	-7.8	4.5	13	-19.1	1	-5.9	-2.9	-4.2	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	81	80	88	83
III	–	–	–	–	0.4	-6.5	12.8	5	-14.0	21	-4.1	-1.1	-3.6	-3.1	–	–	–	–	–	–	–	–	–	–	–	–	72	78	70	73
IV	–	–	–	–	12.1	3.0	23.5	23	-4.0	3	6.7	10.3	6.0	7.2	–	–	–	–	–	–	–	–	–	–	–	–	63	67	53	61
V	–	–	–	–	12.5	3.7	19.1	6, 19, 28	-3.5	2	8.0	10.3	7.2	8.2	–	–	–	–	–	–	–	–	–	–	–	–	75	84	72	77
VI	–	–	–	–	15.6	6.6	26.3	23	-0.2	7	11.0	13.9	9.5	11.0	–	–	–	–	–	–	–	–	–	–	–	–	65	79	64	69
VII	–	–	–	–	17.9	8.2	27.3	27	2.6	2	12.9	16.5	11.2	13.0	–	–	–	–	–	–	–	–	–	–	–	–	62	71	55	63
VIII	–	–	–	–	21.5	10.0	28.7	15	3.6	31	15.2	18.2	13.4	15.3	–	–	–	–	–	–	–	–	–	–	–	–	49	64	50	54
IX	–	–	–	–	16.1	5.2	25.8	4	-0.1	25	8.9	14.2	9.1	10.3	–	–	–	–	–	–	–	–	–	–	–	–	53	60	34	49
X	–	–	–	–	12.8	3.1	20.2	2	-1.5	16	5.5	11.9	5.6	7.2	–	–	–	–	–	–	–	–	–	–	–	–	44	41	37	41
XI	–	–	–	–	6.1	0.0	16.5	8	-5.9	17	2.3	4.6	2.2	2.8	–	–	–	–	–	–	–	–	–	–	–	–	81	83	79	81
XII	–	–	–	–	-2.4	-9.1	7.2	9	-22.4	22	-6.1	-4.1	-6.0	-5.6	–	–	–	–	–	–	–	–	–	–	–	–	75	79	71	75
Rok	–	–	–	–	9.5	1.0	28.7	15.VIII	-22.4	22.XII	4.4	7.8	4.1	5.1	–	–	–	–	–	–	–	–	–	–	–	–	65	71	62	66

UWAGA. W okresie 1.I.–15.V.1962r. obserwacje w III terminie były dokonywane o 1 godzinę za wcześnie

Nowy Sącz $\varphi = 49°37'$ $\lambda = 20°42'$

I	981.8	997.4	959.6	1018.7	3.4	-3.1	8.6	20	-15.0	31	-1.3	2.3	-0.3	0.1	4.7	5.0	4.9	4.9	81	69	79	76	1.1	2.5	1.4	1.7	70	67	79	72
II	979.9	996.7	951.7	1017.1	1.3	-5.4	7.5	12	-14.0	25	-3.5	-0.6	-2.0	-2.0	4.1	4.4	4.4	4.3	84	74	82	80	0.8	1.6	1.1	1.2	96	81	87	88
III	974.5	991.8	956.5	1011.3	3.2	-4.9	16.2	5	-15.5	21	-3.2	2.1	-0.7	-0.6	4.4	5.0	5.0	4.8	85	69	81	78	0.9	2.6	1.2	1.6	88	78	77	81
IV	978.8	991.4	953.6	1014.4	15.9	4.7	26.6	22	-0.9	2	6.9	14.3	9.9	10.2	8.3	8.2	8.7	8.4	83	55	72	70	1.9	9.8	4.1	5.3	68	75	61	68
V	978.5	985.1	963.7	1013.9	16.1	6.6	23.4	8	-1.3	2	9.0	14.1	10.9	11.2	10.1	10.3	11.0	10.5	86	64	83	78	1.8	6.3	2.3	3.5	80	86	66	77
VI	983.3	992.2	973.2	1018.5	18.5	8.7	28.7	23	2.0	7	11.4	16.9	13.5	13.8	12.3	12.7	13.2	12.7	88	65	82	78	1.6	8.2	3.1	4.3	70	80	70	73
VII	980.3	990.7	968.5	1015.1	21.5	10.4	30.6	26	6.1	30	12.9	19.9	15.3	15.8	13.4	13.6	14.6	13.9	89	59	84	77	1.6	10.3	3.0	5.0	65	73	63	67
VIII	982.0	988.5	972.7	1016.6	24.2	11.7	30.8	13	4.1	31	13.7	22.7	17.1	17.6	14.4	15.8	16.1	15.4	91	57	82	77	1.5	12.5	3.7	5.9	62	72	49	61
IX	982.3	993.7	970.2	1017.6	19.1	7.1	29.0	4	1.3	15	8.9	14.0	12.2	11.8	10.1	11.3	11.7	11.0	89	59	82	77	1.7	9.6	3.0	4.8	65	63	45	58
X	987.1	994.4	972.8	1023.2	14.8	2.6	21.3	3	-3.8	22	3.9	13.5	6.9	7.8	8.1	10.7	9.3	9.4	96	69	92	86	0.3	5.2	0.9	2.1	83	44	32	53
XI	980.9	995.4	966.3	1017.0	8.7	2.7	18.7	8	-1.8	24	4.2	7.8	5.1	5.6	7.4	8.0	7.9	7.8	89	76	88	84	1.1	3.4	1.2	1.9	81	80	79	80
XII	980.5	1007.5	940.7	1018.0	-1.2	-8.0	6.1	13	-16.4	21	-5.5	-2.6	-4.8	-4.4	3.6	3.9	3.8	3.8	85	73	84	81	0.7	1.5	0.8	1.0	76	78	83	79
Rok	980.8	1007.5	940.7	1016.8	12.1	2.8	30.8	13.VIII	-16.4	21.XII	4.8	10.4	6.9	7.2	8.4	9.1	9.2	8.9	87	66	83	79	1.2	6.1	2.2	3.2	75	73	66	71

Istebna-Kubalonka $\varphi = 49°36'$ $\lambda = 18°54'$

I	–	–	–	–	-0.7	-5.2	4.4	20	-16.5	31	-3.5	-1.8	-3.2	-2.9	–	–	–	–	–	–	–	–	–	–	–	–	79	66	79	75
II	–	–	–	–	-2.1	-7.2	3.4	13	-16.7	1	-5.7	-3.3	-4.4	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	85	81	88	85
III	–	–	–	–	-0.1	-6.0	12.3	5	-12.6	17	-4.6	-1.7	-3.5	-3.3	–	–	–	–	–	–	–	–	–	–	–	–	79	76	74	76
IV	–	–	–	–	11.3	3.8	23.9	23	-2.1	2	5.8	9.6	6.5	7.1	–	–	–	–	–	–	–	–	–	–	–	–	68	62	54	61
V	–	–	–	–	11.5	4.2	18.6	19	-2.5	2	6.3	9.6	7.4	7.7	–	–	–	–	–	–	–	–	–	–	–	–	84	75	67	75
VI	–	–	–	–	15.7	7.3	27.0	24	-0.1	7	9.8	13.8	10.5	11.2	–	–	–	–	–	–	–	–	–	–	–	–	63	72	56	64
VII	–	–	–	–	17.8	9.8	27.5	27	4.4	5	11.7	16.0	12.3	13.1	–	–	–	–	–	–	–	–	–	–	–	–	64	63	57	61
VIII	–	–	–	–	21.1	11.5	28.5	15	5.2	31	13.7	19.3	14.8	15.6	–	–	–	–	–	–	–	–	–	–	–	–	41	51	39	44
IX	–	–	–	–	15.3	6.6	25.3	4	2.1	25	8.6	13.1	9.5	10.2	–	–	–	–	–	–	–	–	–	–	–	–	51	55	34	47
X	–	–	–	–	12.4	4.5	20.9	2	0.0	16	6.2	11.1	6.8	7.7	–	–	–	–	–	–	–	–	–	–	–	–	50	36	29	38
XI	–	–	–	–	4.5	0.1	14.8	7, 8	-5.1	24	1.1	3.3	1.6	1.9	–	–	–	–	–	–	–	–	–	–	–	–	84	84	78	82
XII	–	–	–	–	-4.1	-8.8	4.2	8	-20.2	23	-6.9	-5.3	-6.6	-6.4	–	–	–	–	–	–	–	–	–	–	–	–	75	70	79	75
Rok	–	–	–	–	8.6	1.7	28.5	15.VIII	-20.2	23.XII	3.5	7.0	4.3	4.8	–	–	–	–	–	–	–	–	–	–	–	–	69	66	61	65

Luboń Wielki $H_s = 1023 m$ $h_w = 15{,}1 m$ 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R/K
I	4.5	5.9	·	·	1	5.0	·	·	7.5	14.9	53	12.6	10.5	6.2	14.5	5.0	2	10.2	79	18.4	27	5	18	30	·	18	11	·	20	17	12	3	14	31	–
II	2	3.0	3	5.0	7	3.9	·	·	·	·	25	11.4	16	9.6	24	8.5	7	8.2	115	13.3	21	8	28	28	·	11	8	·	26	22	19	3	19	28	·
III	6.5	15.2	5.5	5.9	4.5	4.1	·	·	4.5	11.9	29	10.1	5	2.8	32	5.5	6	7.4	135	46.2	16	10	20	29	·	12	12	2	25	18	14	4	14	31	–
IV	8.5	3.8	7.5	4.9	·	·	1	9.0	5.5	9.6	28.5	10.1	3.5	5.3	33.5	5.3	2	6.8	133	56.4	6	·	1	11	·	7	5	2	16	17	13	4	16	22	1
V	8	3.5	·	·	1	7.0	·	·	3	7.0	30.5	6.8	19	5.5	22.5	4.0	9	4.9	162	17.8	20	·	1	5	·	3	·	·	22	28	24	6	19	3	6
VI	3.5	9.3	5	4.8	3	4.3	1	3.0	·	·	10.5	5.4	14.5	5.2	48.5	5.7	4	5.3	182	47.8	1	·	·	6	1	3	3	·	19	14	14	4	12	3	4
VII	8.5	4.4	1	5.0	·	·	·	·	1	12.0	19	7.0	16	4.2	42.5	3.8	5	4.5	185	66.3	18	·	·	·	1	2	1	3	21	17	12	4	9	·	7
VIII	1.5	3.0	3	3.0	2	5.0	1	5.0	4	9.2	28.5	7.2	21.5	4.7	25.5	4.4	6	5.2	65	18.6	15	·	·	·	2	3	3	·	12	17	10	2	9	·	4
IX	1.5	4.3	4	3.2	3	5.7	1	6.0	4.5	10.1	29	10.7	11.5	4.4	22.5	5.0	13	6.3	73	15.9	18	·	·	·	·	8	7	3	15	17	12	3	9	·	1
X	4	4.5	6	3.4	5	4.2	1	3.0	1	7.5	22	6.0	15.5	2.9	30.5	3.2	8	3.7	19	4.4	19	·	·	3	·	3	2	11	9	13	7	·	10	·	·
XI	4	3.2	8.5	3.7	3.5	4.1	3	7.3	7.5	8.0	28	4.4	4.5	2.6	21	3.6	10	3.9	80	11.6	23	·	11	17	·	3	1	2	25	19	14	4	17	15	·
XII	9.5	5.4	14.5	6.7	2	11.0	·	·	8	14.9	26	12.5	7	6.3	16	4.9	10	7.9	78	13.5	14	11	24	31	·	13	10	1	20	20	15	2	20	31	·
Rok	62	5.5	58	3.8	32	4.5	8	2.8	46.5	8.8	329	8.7	144.5	5.0	333	4.9	82	6.3	1306	66.3	18. VII	34	103	160	4	86	63	24	230	219	166	39	168	164	23

Zawoja $H_s = 670 m$ $h_w = 18 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R/K
I	5.5	1.5	2	2.0	0.5	2.0	1	1.0	10	6.0	28	3.0	8.5	1.8	5.5	1.9	32	2.0	77	20.3	27	3	6	24	·	3	3	2	11	16	10	2	·	13	·
II	7.5	2.5	·	·	·	·	0.5	1.0	5.5	8.2	13	1.8	5	3.2	13.5	2.9	39	1.7	75	13.7	5	7	12	28	·	1	1	·	21	21	14	2	·	28	·
III	18	2.5	2.5	4.2	0.5	1.0	1	1.0	8.5	5.2	12.5	4.6	5	2.0	6	2.4	39	2.0	56?	13.3	12	12	16	26	·	1	1	2	14	14	12	1	1	30	·
IV	7.5	1.5	3	1.5	1	1.5	4	3.2	15.5	4.4	14.5	3.7	1	1.0	5.5	1.8	38	1.8	137	53.3	6	·	·	8	·	4	4	6	9	15	13	4	5	4	1
V	4	1.2	0.5	1.0	1	1.0	0.5	1.0	11.5	3.2	20.5	1.9	4	1.4	6	1.0	45	1.0	223	35.6	20	·	·	5	·	3	·	1	17	28	23	9	6	1	2
VI	1.5	1.5	3.5	1.7	0.5	2.0	·	·	1.5	1.7	6	1.2	8	1.2	11.5	1.5	44	0.7	201	50.8	1	·	·	1	3	·	·	·	13	14	12	5	1	1	3
VII	6.5	2.0	0.5	1.0	·	·	1.5	1.0	7	1.4	19.5	2.0	6	1.8	6	1.3	46	0.9	141	50.5	18	·	·	·	4	·	·	3	9	17	12	4	2	·	5
VIII	2.5	1.6	2.5	1.4	·	·	·	·	7.5	3.1	17	2.8	8.5	2.2	6	1.6	49	1.1	43	13.8	15	·	·	·	8	2	1	1	5	14	9	1	2	·	3
IX	5.5	1.8	4	1.0	1	1.0	1.5	1.3	10	3.7	15	2.2	6.5	1.7	10.5	1.6	36	1.3	81	16.8	23	·	·	1	1	2	·	9	7	13	13	4	3	·	1
X	6	1.1	1	3.0	0.5	1.0	1.5	1.0	9	2.1	1.5	1.7	6	1.8	6.5	1.1	61	0.5	37	16.0	6	·	·	6	·	1	·	14	9	10	9	1	12	·	·
XI	9.5	1.4	0.5	2.0	0.5	3.0	1	3.0	12.5	6.7	4	1.6	·	·	3	1.3	59	1.2	112	17.2	15	·	7	17	·	3	2	3	20	15	15	5	12	14	·
XII	8.5	1.4	2	2.5	·	·	1.5	10.3	18	10.2	7.5	4.7	3.5	1.6	4	1.4	48	2.8	65	12.0	13	13	17	31	·	5	5	3	18	17	13	1	5	31	·
Rok	96	1.7	22	1.8	5.5	1.0	14	2.0	116.5	4.7	159	2.6	62	1.6	84	1.6	536	1.4	1248?	53.3	6. IV	35	58	147	16	25	14	44	153	194	155	39	49	122	15

Nowy Sącz $H_s = 292 m$ $H_b = 295{,}4 m$ $h_w = 16{,}5 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R/K
I	4.5	2.8	1	2.0	1	1.0	2.5	1.0	19	3.4	28	3.2	12	4.4	4	3.9	21	2.6	33	5.6	28	1	6	22	·	3	·	3	16	15	10	·	·	17	–
II	5.5	3.5	4	1.5	1	1.0	·	·	9.5	2.3	9.5	5.7	15.5	6.8	10	6.2	29	3.2	36	5.7	17	4	10	25	·	11	5	·	21	20	12	·	1	27	·
III	9.5	3.2	7	3.6	1	2.0	3	3.3	9.5	3.7	4	3.9	8	5.3	5	4.1	46	1.9	50	11.0	16	5	9	26	·	1	1	·	20	14	10	1	8	23	·
IV	4.5	2.3	6.5	2.7	4	1.1	4.5	2.9	16	4.3	8	4.2	7.5	5.3	7	4.8	32	2.5	69	28.3	6	·	·	2	5	2	1	4	15	14	10	2	2	·	·
V	9.5	1.8	2.5	1.6	·	·	·	·	4	3.1	11	5.6	10	4.2	7	3.1	49	1.7	108	15.2	20	·	·	1	·	4	3	1	17	27	19	4	2	·	2
VI	20	2.3	3	1.3	1	1.5	·	·	2	2.2	7.5	2.7	14	4.1	5.5	3.3	37	1.7	154	33.4	4	·	·	·	6	1	·	·	15	15	15	5	4	·	7
VII	15	2.4	2	2.5	1	1.0	2	1.5	5	2.1	5	2.5	8	2.9	8	2.2	47	1.2	158	57.0	17	·	·	·	5	3	·	3	12	17	10	4	6	·	8
VIII	5	1.6	7	1.6	2.5	2.6	2	1.0	3.5	4.1	4	3.6	10	3.8	6	3.7	53	1.3	33	13.3	16	·	·	·	12	1	1	·	6	9	4	2	8	·	5
IX	1	1.5	1.5	2.3	4.5	1.9	2	1.0	10.5	1.9	8.5	3.5	14	4.0	4	2.5	44	1.4	56	18.7	18	·	·	·	6	4	2	6	8	13	8	1	9	·	2
X	10	1.6	9.5	1.7	4.5	2.0	·	·	·	·	2	2.0	5	2.7	1	2.5	61	0.7	6	2.2	30	·	·	8	·	·	·	4	7	8	3	·	24	·	·
XI	6.5	1.8	5.5	1.8	·	·	10.5	2.7	15	3.0	2	3.5	4.5	2.8	·	·	46	1.3	98	16.9	15	·	1	7	·	·	·	1	20	16	11	4	11	9	·
XII	15.5	3.0	3	3.0	·	·	5.5	3.2	12	3.4	6.5	3.5	2.5	4.8	2	3.8	46	1.7	49	13.8	30	12	13	29	·	2	·	3	21	18	11	2	5	31	·
Rok	106.5	2.3	52.5	2.1	20.5	1.2	32	1.4	106	2.8	96	3.7	111	4.3	59.5	3.3	511	1.8	850	57.0	17. VII	22	39	120	34	32	13	25	178	186	123	25	80	107	24

Istebna-Kubalonka $H_s = 800 m$ $h_w = 25{,}6 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R/K
I	9.5	3.5	3	3.7	·	·	·	·	40.5	3.9	17	2.7	0.5	1.0	10.5	2.4	12	2.9	95	26.8	28	4	16	31	·	2	·	3	16	16	13	2	11	31	·
II	18.5	2.3	1.5	2.3	0.5	3.0	·	·	10	4.6	11.5	3.9	6.5	3.3	19.5	2.4	16	2.5	121	20.2	17	7	20	28	·	1	1	1	19	21	17	5	6	28	·
III	20	2.9	4.5	2.9	1.5	2.7	3	2.7	24.5	3.4	9.5	2.8	·	·	11	2.7	19	2.4	114	22.7	12	5	16	28	·	·	·	2	20	20	14	3	8	31	·
IV	11.5	2.5	5	1.8	1.5	1.0	3.5	3.0	28	4.0	3.5	2.9	3.5	1.9	23.5	1.5	10	2.4	126	44.1	6	·	·	8	·	2	·	7	13	17	11	3	11	18	1
V	8	2.2	6	1.2	0.5	1.0	3.5	1.0	14.5	2.9	25.5	1.6	9.5	1.1	10.5	1.8	15	1.5	229	35.4	20	·	·	4	·	·	·	1	15	29	20	9	9	1	6
VI	26	1.8	3.5	2.7	·	·	·	·	7	1.3	9	1.2	7	1.6	19.5	2.1	18	1.4	120	31.8	4	·	·	1	3	·	·	6	14	12	12	3	6	1	4
VII	13	1.3	3.5	1.0	0.5	1.0	1	5.0	17	1.7	14	1.5	8.5	1.1	16.5	1.9	19	1.3	110	40.2	18	·	·	·	2	·	·	4	10	16	15	3	6	·	5
VIII	7	1.1	0.5	1.0	1	1.0	1	1.0	10.5	3.1	29	2.0	7.5	1.1	5.5	1.1	31	1.2	55	11.5	15	·	·	·	7	1	·	8	1	16	11	1	2	·	2
IX	12.5	1.3	1.5	1.0	·	·	4.5	2.1	25.5	3.1	19	2.2	3	1.3	5	1.0	19	1.7	95	22.0	23	·	·	·	1	·	·	10	9	12	11	3	6	·	1
X	17	1.1	7.5	1.7	1	3.0	0.5	2.0	16	1.6	10.5	2.4	1.5	2.3	3	1.3	36	1.0	52	14.8	5	·	·	·	·		·	15	7	10	9	1	10	·	·
XI	17	1.5	2	3.2	·	·	5	5.3	24	3.6	10	2.2	2	1.0	9	1.7	21	2.1	126	21.8	20	·	11	16	·	2	·	2	23	19	17	5	11	14	·
XII	23	1.8	3	1.3	·	·		·	26	3.8	7	3.9	3.5	1.0	4.5	1.4	26	1.9	91	12.5	16	11	27	31	·	1	·	3	17	16	12	3	10	31	·
Rok	193	1.9	41.5	2.0	6.5	1.1	22	1.8	243.5	3.1	165.5	2.4	53	1.4	138	1.8	242	1.9	1334	44.1	6. IV	27	90	147	13	9	1	62	164	204	162	41	96	155	19

Istebna-Stecówka $\varphi = 49°35'$ $\lambda = 18°57'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	P_{0m}	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.0	-5.5	4.3	1	-17.0	31	-4.0	-2.1	-3.6	-3.3	–	–	–	–	–	–	–	–	–	–	–	–	76	70	76	74
II	–	–	–	–	-2.6	–	3.0	13	–	–	-6.6	-4.0	-4.8	-5.0	–	–	–	–	–	–	–	–	–	–	–	–	90	85	77	84
III	–	–	–	–	-0.7	-6.8	11.7	5	-12.3	14	-5.3	-1.7	-3.8	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	83	75	71	76
IV	–	–	–	–	–	2.9	–	–	-2.1	3	5.5	9.3	6.2	6.8	–	–	–	–	–	–	–	–	–	–	–	–	72	67	57	65
V	–	–	–	–	11.3	3.7	19.2	19	-3.0	1, 2	6.6	10.0	7.1	7.7	–	–	–	–	–	–	–	–	–	–	–	–	85	85	77	82
VI	–	–	–	–	14.9	6.4	25.3	19	0.1	4, 7	9.7	13.7	9.9	10.8	–	–	–	–	–	–	–	–	–	–	–	–	64	73	55	64
VII	–	–	–	–	17.4	8.9	26.1	27	3.2	5	11.6	16.2	12.4	13.2	–	–	–	–	–	–	–	–	–	–	–	–	74	71	65	70
VIII	–	–	–	–	20.6	10.5	27.3	15	4.3	31	13.3	19.6	14.9	15.7	–	–	–	–	–	–	–	–	–	–	–	–	53	59	43	52
IX	–	–	–	–	14.5	6.2	24.2	4	1.2	20, 25	8.6	13.2	9.5	10.2	–	–	–	–	–	–	–	–	–	–	–	–	57	59	37	51
X	–	–	–	–	11.9	4.3	20.5	4	-0.6	17	6.1	11.3	6.5	7.6	–	–	–	–	–	–	–	–	–	–	–	–	45	47	31	41
XI	–	–	–	–	4.4	0.2	14.7	7	-5.2	24	1.6	3.3	2.0	2.2	–	–	–	–	–	–	–	–	–	–	–	–	84	89	72	82
XII	–	–	–	–	-4.0	-8.9	5.1	8	-21.2	23	-7.0	-5.0	-6.7	-6.4	–	–	–	–	–	–	–	–	–	–	–	–	81	75	71	76
Rok	–	–	–	–	–	–	27.3	15.VIII	–	–	3.3	7.0	4.1	4.6	–	–	–	–	–	–	–	–	–	–	–	–	72	71	61	68

Istebna-Zaolzie $\varphi = 49°34'$ $\lambda = 18°56'$

I	–	–	–	–	0.0	–	4.8	22	–	–	-4.9	-1.0	-3.8	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	66	72	75	71
II	–	–	–	–	-0.9	-10.0	4.8	13	-25.1	26	-6.9	-2.5	-4.7	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	85	83	92	87
III	–	–	–	–	1.1	-9.4	12.0	5	-21.2	21	-6.5	-0.6	-4.8	-4.2	–	–	–	–	–	–	–	–	–	–	–	–	75	80	76	77
IV	–	–	–	–	12.0	-0.1	24.9	25	-7.3	2	4.3	10.8	3.0	5.3	–	–	–	–	–	–	–	–	–	–	–	–	65	62	52	60
V	–	–	–	–	13.0	3.4	19.8	19	-3.5	5	7.3	11.5	6.9	8.2	–	–	–	–	–	–	–	–	–	–	–	–	84	80	58	74
VI	–	–	–	–	16.9	5.2	27.1	23, 24	-0.5	9	10.5	15.2	9.3	11.1	–	–	–	–	–	–	–	–	–	–	–	–	64	77	53	65
VII	–	–	–	–	18.9	6.6	27.6	27	1.1	30	12.1	17.8	10.8	12.9	–	–	–	–	–	–	–	–	–	–	–	–	65	66	53	61
VIII	–	–	–	–	21.9	7.3	28.9	15	0.2	31	13.6	20.5	11.8	14.4	–	–	–	–	–	–	–	–	–	–	–	–	52	53	32	46
IX	–	–	–	–	16.0	2.5	26.0	4	-3.1	25	6.6	14.7	6.7	8.7	–	–	–	–	–	–	–	–	–	–	–	–	57	60	35	51
X	–	–	–	–	13.1	-0.4	21.6	3, 4	-5.8	24	1.7	12.3	2.9	5.0	–	–	–	–	–	–	–	–	–	–	–	–	56	50	41	49
XI	–	–	–	–	5.7	-0.5	16.7	7	-8.6	22	1.1	4.9	1.6	2.3	–	–	–	–	–	–	–	–	–	–	–	–	87	83	81	84
XII	–	–	–	–	-4.0	-12.6	5.0	13	-30.7	22	-9.1	-5.1	-8.5	-7.8	–	–	–	–	–	–	–	–	–	–	–	–	80	75	70	75
Rok	–	–	–	–	9.5	–	28.9	15.VIII	–	–	2.5	8.2	2.6	4.0	–	–	–	–	–	–	–	–	–	–	–	–	70	70	60	67

Rabka $\varphi = 49°37'$ $\lambda = 19°58'$

I	951.4	965.0	930.5	–	2.2	-3.8	8.8	22	-15.5	31	-2.2	1.0	-1.5	-1.0	4.8	4.7	4.7	4.7	88	7.0	8.3	8.0	0.7	2.1	1.0	1.3	73	6.5	7.5	7.1
II	949.6	965.5	923.9	–	0.1	-7.2	4.6	7	-21.1	25	-5.2	-1.6	-3.9	-3.6	3.9	4.2	4.2	4.1	89	7.6	8.8	8.4	0.5	1.4	0.6	0.8	96	8.2	9.1	9.0
III	944.2	959.9	929.5	–	2.1	-6.7	15.4	5	-17.0	21	-5.3	0.8	-3.1	-2.7	4.2	4.6	4.5	4.4	91	6.8	8.8	8.2	0.4	2.3	0.6	1.1	89	8.1	7.6	8.2
IV	949.5	961.5	925.2	–	13.6	3.0	25.3	23	-2.5	8	4.9	12.1	6.5	7.5	7.8	8.0	8.2	8.0	90	6.3	8.4	7.9	1.0	7.9	2.0	3.6	20	7.6	5.2	6.6
V	949.2	955.7	935.7	–	14.3	5.4	21.9	19	-1.6	2	7.9	12.2	8.9	9.5	10.0	10.0	10.3	10.1	91	7.1	8.9	8.4	0.9	4.9	1.5	2.4	7.9	8.9	7.0	7.9
VI	954.2	962.2	945.2	–	17.1	7.6	28.5	16	1.2	5	10.5	15.6	11.8	12.4	11.9	11.6	12.3	11.9	90	6.6	8.6	8.1	1.4	7.8	2.3	3.8	67	7.7	6.5	7.0
VII	951.7	961.0	939.7	–	19.9	9.5	29.1	26	4.6	30	12.0	18.3	14.0	14.6	12.9	12.6	13.8	13.1	91	6.1	8.5	7.9	1.4	9.3	2.5	4.4	68	7.4	6.7	7.0
VIII	953.4	959.4	943.8	–	22.8	10.6	30.6	7	4.0	31	12.6	21.4	15.3	16.2	13.8	14.0	14.8	14.2	94	5.6	8.4	7.8	1.0	12.3	2.9	5.4	59	6.8	4.7	5.8
IX	953.1	962.8	941.6	–	17.8	5.6	27.2	4	-0.7	25, 27	7.1	16.1	10.0	10.8	9.6	10.8	10.9	10.4	93	6.1	8.8	8.1	1.0	8.5	1.8	3.8	58	6.0	3.4	5.1
X	952.2	968.6	943.9	–	14.7	2.1	23.7	3	-3.4	17	3.2	13.4	5.6	7.0	7.7	9.9	8.9	8.8	98	6.6	9.7	8.7	0.2	6.1	0.3	2.2	51	4.5	3.0	4.2
XI	950.6	964.1	936.6	–	7.1	0.5	17.9	5, 7, 8	-4.9	18	1.5	5.9	2.5	3.1	6.8	7.9	7.4	7.4	98	8.4	9.9	9.4	0.1	2.1	0.1	0.8	83	8.0	8.1	8.1
XII	949.4	975.0	911.2	–	-2.1	-9.8	5.5	9	-21.2	22	-7.1	-3.4	-6.9	-6.1	3.5	3.9	3.6	3.7	90	7.8	9.0	8.6	0.4	1.2	0.4	0.7	79	8.2	7.2	7.8
Rok	951.1	975.0	911.2	–	10.8	1.4	30.6	7.VIII	-21.2	22.XII	3.3	9.3	4.9	5.6	8.1	8.5	8.6	8.4	92	6.8	8.8	8.3	0.8	5.5	1.3	2.5	73	7.3	6.3	7.0

Brzezna $\varphi = 49°36'$ $\lambda = 20°37'$

I	–	–	–	–	3.2	-2.4	9.0	20	-14.9	31	-1.3	1.7	-0.5	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	75	66	76	72
II	–	–	–	–	1.5	-5.6	7.5	12	-14.1	25	-3.8	-0.7	-2.7	-2.5	–	–	–	–	–	–	–	–	–	–	–	–	100	84	90	91
III	–	–	–	–	3.1	-4.9	15.1	5	-15.4	21	-3.4	2.0	-1.2	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	87	83	76	82
IV	–	–	–	–	15.8	4.8	26.5	22, 23	-1.1	30	7.5	14.5	9.1	10.0	–	–	–	–	–	–	–	–	–	–	–	–	65	65	56	62
V	–	–	–	–	16.1	6.3	24.5	8	-1.5	2	9.5	14.4	10.1	11.0	–	–	–	–	–	–	–	–	–	–	–	–	77	83	73	78
VI	–	–	–	–	18.6	8.3	29.0	23	1.9	7	12.0	17.1	12.6	13.6	–	–	–	–	–	–	–	–	–	–	–	–	72	79	77	76
VII	–	–	–	–	21.6	10.0	31.0	27	5.6	30	13.4	20.3	14.3	15.6	–	–	–	–	–	–	–	–	–	–	–	–	65	70	77	71
VIII	–	–	–	–	24.5	11.3	31.1	15	4.5	31	14.4	22.9	16.0	17.3	–	–	–	–	–	–	–	–	–	–	–	–	61	63	60	61
IX	–	–	–	–	19.3	6.8	28.8	4	1.5	15	9.1	17.7	11.1	12.2	–	–	–	–	–	–	–	–	–	–	–	–	65	60	50	58
X	–	–	–	–	14.9	2.6	21.6	4	-3.4	26	4.0	13.9	6.4	7.7	–	–	–	–	–	–	–	–	–	–	–	–	75	43	33	50
XI	–	–	–	–	8.5	2.6	18.5	8	-2.1	24	4.0	7.6	4.8	5.3	–	–	–	–	–	–	–	–	–	–	–	–	82	80	85	82
XII	–	–	–	–	-1.6	-8.0	4.9	16	-16.4	21	-5.8	-2.9	-5.0	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	80	66	82	76
Rok	–	–	–	–	12.1	2.6	31.1	15.VIII	-16.4	21.XII	5.0	10.7	6.2	7.0	–	–	–	–	–	–	–	–	–	–	–	–	75	70	70	72

Istebna - Stecówka $H_s = 750 m$ $h_w = 12,5 m$ 1962

MIESIĄC	ROZKŁAD WIATRU °D, v m/s N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v>10	v>15	◔	●	Opad R ≥0.1	R ≥1.0	R ≥10.0	≡	⊞	⊼
I	5	3.2	6	2.3	·	·	6.5	2.7	17.5	3.4	37	3.0	4	1.8	14	2.3	3	2.7	92	25.6	28	4	18	30	·	·	·	2	16	18	14	2	4	31	·
II	14	2.9	4.5	2.0	5	1.6	5	2.4	9	2.1	18	4.1	3	3.3	18.5	3.8	7	2.9	149	22.5	19	–	23	–	·	2	·	1	19	23	20	7	4	28	·
III	23.5	2.7	5.5	3.2	4	2.2	4	2.2	19.5	3.3	8.5	3.3	8	2.1	10	2.5	10	2.5	133	27.3	17	12	18	28	·	·	·	1	17	19	14	4	5	31	·
IV	16	2.0	15	1.7	7	3.1	3	4.7	20.5	4.7	7	3.6	8.5	2.4	7	2.6	6	2.8	132	38.5	6	·	·	11	–	2	1	6	14	18	14	4	10	16	1
V	18	2.2	4	1.8	1	2.0	4	2.0	12	2.5	15	2.7	8	2.0	9	1.7	22	1.7	223[2]	30.6	20	·	·	4	·	·	·	·	19	28	21	9	16	1	3
VI	19	1.7	5	3.6	1	1.0	3	2.3	5.5	1.6	12	2.2	3.5	2.3	11	2.8	30	1.5	147	37.7	4	·	·	·	2	·	·	5	14	13	12	4	9	·	3
VII	16	1.9	7	1.7	2	2.0	1	2.0	11.5	2.0	16.5	2.7	11	2.2	7	1.4	21	1.6	105	37.3	18	·	·	·	2	·	·	3	17	16	14	3	8	·	5
VIII	8	1.6	3	1.7	4	2.0	·	·	13	3.2	11	3.3	7	2.1	10	2.6	37	1.5	57	10.0	5	·	·	·	5	·	·	1	2	16	12	1	3	·	3
IX	8	2.0	1	2.0	8	2.4	1	2.0	16.5	3.1	18.5	3.2	13	2.1	11	2.1	13	2.2	113	23.5	23	·	·	·	·	·	·	7	7	14	13	4	5	·	1
X	27.5	1.5	3.5	2.0	13	1.9	3	2.3	8	2.5	23	2.4	6	1.5	6	1.8	3	1.9	45	12.2	5	·	·	2	·	·	·	14	8	10	9	1	11	·	·
XI	25	1.8	2	1.0	10	3.1	15.5	3.7	7.5	3.1	10	3.4	6	2.0	6	1.7	8	2.4	120	22.3	20	·	11	16	·	·	·	1	20	19	17	5	14	10[2]	·
XII	16	1.8	9	2.2	1	2.0	3	2.3	20	3.4	16	3.0	7	2.1	5	1.8	16	2.1	107	20.3	16	12	26	31	·	·	·	1	18	20	15	3	12	31	·
Rok	196	2.1	65.5	2.1	56	1.9	49	2.4	160.5	2.9	192.5	3.1	85	2.2	114.5	2.3	176	2.2	1423[2]	38.5	6. IV	–	96	–	–	4	1	42	171	214	175	47	101	148[2]	16

Istebna - Zaolzie $H_s = 850 m$ $h_w = 19 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	◔	●	R ≥0.1	R ≥1.0	R ≥10.0	≡	⊞	⊼
I	4	2.2	3	1.3	0.5	1.0	0.5	1.0	6.5	3.6	21	2.5	7	1.6	6.5	1.9	44	1.3	90	20.8	28	–	13	–	·	·	·	4	17	15	11	3	–	31	·
II	7	4.1	·	·	·	·	·	·	1.5	4.3	15	2.1	8.5	4.6	13	3.1	39	1.8	95	14.4	19	11	15	27	·	1	·	·	21	21	17	3	–	28	·
III	9	3.5	2.5	4.2	2	2.0	·	·	5	1.7	11	2.3	6.5	2.7	11	2.4	46	1.3	72	16.2	17	14	13	28	·			2	17	15	13	·	–	31	·
IV	3	2.7	1.5	3.0	4.5	2.3	2	1.5	8.5	4.1	7.5	2.2	2	1.8	15	1.9	46	1.2	110	41.0	6	·	·	14	·	·	·	8	11	15	13	4	–	15	1
V	4.5	1.4	4.5	1.1	·	·	2	3.5	3.5	1.0	11.5	2.8	7	2.2	9	2.2	51	1.0	237	40.0	9	·		8	·		·	·	13	27	21	10	–	·	7
VI	6	2.3	1.5	2.7	1.5	2.0	1	2.0	0.5	1.0	5.5	1.6	7.5	1.7	12.5	1.6	54	0.7	159	41.0	4	·	·	2	5	·	·	5	14	13	10	4	–	·	3
VII	6	2.3	3	1.7	·	·	1	1.0	3	1.7	8	1.4	9	1.6	12	1.8	51	0.8	108	34.5	18	·	·	·	4	·	·	4	10	15	13	4	–	·	6
VIII	2	1.0	1	1.0	3	2.7	·	·	2	2.0	10.5	3.1	11.5	2.1	9	1.6	54	0.9	52	10.0	15	·	·	·	7	1	·	6	4	16	12	1	–	·	5
IX	4.5	2.1	2.5	1.4	·	·	·	·	2.5	4.6	11	2.5	7	2.0	9.5	2.4	53	1.0	106	20.3	23	·	·	8	1	·	·	7	7	13	12	5	–	·	1
X	2.5	1.4	2	1.0	·	·	·	·	2	1.5	6.5	1.6	1.5	1.7	3.5	1.6	75	0.3	36	7.1	5	·	·	17	·	·	·	10	9	10	9	·	–	·	·
XI	7.5	1.4	·	·	4.5	2.6	5	2.7	2	2.0	6	2.0	2.5	2.8	3.5	1.3	59	0.7	113	20.5	19	·	4	17	·	·	·	3	22	18	16	3	–	12	·
XII	3.5	2.0	2.5	1.6	·	·	·	·	6.5	2.6	9.5	3.2	2	1.0	2	1.5	67	0.7	97	15.3	16	17	24	30	·	·	·	3	19	19	13	4	–	31	·
Rok	59.5	2.2	24	1.6	16	1.0	11.5	1.0	43.5	2.5	123	2.3	72	2.2	106.5	1.9	639	1.0	1275	41.0	6.IV, 4.VI	–	69	–	17	2	·	52	164	197	160	41	–	148	23

Rabka $H_s = 511 m$ $H_b = 552,5 m$ $h_w = 19 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	◔	●	R ≥0.1	R ≥1.0	R ≥10.0	≡	⊞	⊼
I	2.5	1.4	4.5	2.3	1	2.0	4	3.6	12.5	3.9	35	3.7	14	2.7	6.5	3.0	13	2.8	59	18.3	27	4	5	25	·	3	2	1	14	16	10	2	·	27	·
II	4.5	3.2	2	1.5	·	·	1	1.0	5	4.0	14.5	6.0	14	6.5	14	4.4	29	3.3	74	10.5	5	7	10	27	·	5	5	·	21	23	16	1	·	28	·
III	4.5	6.0	13.5	4.2	2.5	2.2	3.5	1.7	3.5	3.0	18	2.7	13	2.8	9.5	3.3	25	2.4	66	14.4	16	9	11	27	·	3	1	·	21	16	13	2	1	31	·
IV	3.5	3.1	7	2.0	2	7.0	11.5	2.0	13	1.5	17	2.9	12.5	3.0	5.5	2.7	18	2.0	112	63.0	6		·	4	1	·	·	4	12	17	13	2	6	7	·
V	3.5	2.1	5.5	1.5	1.5	1.7	5.5	1.8	6	1.6	24.5	3.0	16.5	2.4	4	2.4	26	1.7	139	17.7	24	·	·	3	·	2	1	1	16	25	18	6	·	·	4
VI	6	3.3	6	2.8	1	1.0	2	1.5	6.5	1.6	9	3.3	14	3.1	15.5	3.4	30	2.0	187	47.0	1	·	·	·	5	3	·	2	16	16	14	4	·	·	5
VII	4.5	1.7	3	2.7	1.5	3.0	1.5	2.3	6.5	2.1	22	2.7	17	2.0	13	2.2	24	1.7	141	58.0	18	·	·	·	4	2	·	3	13	15	11	3	2	·	7
VIII	·	·	2	1.5	1.5	3.0	5	1.8	16.5	2.4	12	2.8	18.5	3.2	5.5	3.2	32	1.8	55	17.7	15	·	·	·	8	4	1	1	4	17	10	2	·	·	6
IX	1	3.0	0.5	3.0	3.5	1.9	1.5	2.0	12.5	2.5	19	3.4	13.5	2.2	7.5	1.9	31	1.7	61	13.5	18	·	·	3	4	1	1	6	6	13	9	3	6	·	1
X	3	2.0	6	2.2	·	·	3	1.3	5	1.3	7	1.7	10	1.8	9	2.3	50	0.9	11	2.6	19	·	·	7	·	·	·	12	8	8	5	·	4	·	·
XI	6.5	1.8	3	2.0	1	1.0	1	1.0	2.5	1.8	17	1.8	6.5	2.4	4.5	1.8	48	0.9	89	16.7	15	·	2	16	·	·	·	1	20	17	14	3	4	14	·
XII	3	2.2	12.5	2.2	1	1.0	3	3.0	5.5	2.5	17	4.6	10	2.0	7	1.7	34	1.8	59	12.0	30	14	16	31	·	2	1	1	17	18	12	2	1	31	·
Rok	42.5	2.5	65.5	2.3	16.5	2.0	42.5	1.9	95	2.4	212	3.2	159.5	2.8	101.5	2.7	360	1.9	1053	63.0	6.IV	34	44	143	22	25	12	32	168	201	145	30	24	138	23

Brzezna $H_s = 320 m$ $h_w = 16,0 m$ I – VI, $h_w = 16,9 m$ VII – XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	◔	●	R ≥0.1	R ≥1.0	R ≥10.0	≡	⊞	⊼
I	6	2.5	·	·	·	·	1	6.0	30	4.4	20.5	3.1	12.5	3.0	13	2.7	10	3.1	29	7.6	28	2	4	21	·	2	·	2	17	12	9	·	·	16	·
II	10	2.8	·	·	1	1.0	0.5	1.0	11	2.8	7	5.4	2.5	2.6	19	4.4	33	2.2	48	7.4	18	2	10	26	·	4	·	·	24	20	13	·	·	27	·
III	17	2.8	3	1.0	·	·	·	·	16	3.4	·	·	3	2.7	4	2.0	50	1.3	52	15.3	16	5	8	25	·	·	·	·	21	15	8	1	–	23	·
IV	12	1.7	1	1.0	·	·	5	1.8	19.5	3.5	3.5	3.9	6	2.8	18	2.1	25	1.8	75	33.5	6	·	·	2	5	·	·	6	13	12	9	2	–	·	·
V	21	1.2	0.5	1.0	1	1.0	·	·	11	4.1	5	3.2	7.5	3.7	13	1.8	34	1.5	91	15.5	20	·	·	1	·	·	·	1	17	27	20	3	·	·	2
VI	26.5	1.9	1	3.0	5	1.0	0.5	1.0	5	1.6	4.5	3.0	4	1.0	18.5	2.5	25	1.5	147	38.2	5	·		·	6	·	·	1	16	16	12	5	–	·	6
VII	24.5	1.3	2.5	1.0	2	1.0	2	1.0	6	1.7	8	1.5	7	1.3	15	1.1	26	0.9	126	31.8	18	·	·	·	5	·	·	3	14	17	12	4	·	·	7
VIII	16.5	1.7	3.5	2.1	5	1.4	2	2.0	11	2.1	·	·	3	1.0	12	2.0	40	1.0	39	16.2	5	·	·	·	13	·	·	1	6	9	4	2	3	·	2
IX	6	1.6	2.5	1.2	1	1.0	·	·	9	1.2	3	1.3	12	1.5	8.5	1.5	48	0.7	39	13.5	18	·	·	·	6	1	·	4	8	10	6	1	3	·	1
X	19	1.8	17	2.2	7	1.3	·	·	6	2.0	1	1.0	1	3.0	6	2.3	36	1.2	8	4.9	30	·	·	7	·	·	·	6	7	3	2	·	9	·	·
XI	19	2.5	11.5	3.2	1	1.0	6	3.2	27	3.1	6	3.0	4	2.5	5.5	2.3	10	2.5	71	14.7	15	·	1	8	·	·	·	3	23	13	10	1	5	9	·
XII	26	2.0	·	·	·	·	·	·	15	4.3	2	2.5	4	1.8	10	1.8	36	1.6	50	15.6	30	12	18	31	·	1	·	2	16	17	11	2	·	31	·
Rok	203.5	2.0	42.5	1.3	23	0.7	17	1.3	166.5	2.8	60.5	2.3	66.5	2.2	142.5	2.2	373	1.6	775	38.2	5. VI	21	41	121	35	8	·	29	182	171	116	21	–	106	18

UWAGA. W okresie od 6.XI. do 31.XII.1962 r. prędkość wiatru - wg skali Beauforta.

Płaszkowa $\varphi = 49°36'$ $\lambda = 20°53'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.2	-4.1	8.4	22	-16.7	31	-1.9	0.8	-1.5	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	68	64	78	70
II	–	–	–	–	-0.3	-6.3	7.4	13	-15.0	1	-4.8	-2.6	-3.2	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	98	85	91	91
III	–	–	–	–	1.1	-5.2	13.4	5	-11.3	9, 20, 27	-3.4	-0.2	-2.1	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	91	82	74	82
IV	–	–	–	–	13.9	6.0	24.2	22	-1.1	30	7.3	12.0	9.1	9.4	–	–	–	–	–	–	–	–	–	–	–	–	68	70	50	63
V	–	–	–	–	14.4	5.9	22.4	8	-1.1	2, 3	8.8	12.2	9.4	10.0	–	–	–	–	–	–	–	–	–	–	–	–	80	87	67	78
VI	–	–	–	–	16.8	8.5	27.2	23	0.4	7	11.8	15.2	12.1	12.8	–	–	–	–	–	–	–	–	–	–	–	–	66	79	76	74
VII	–	–	–	–	19.5	10.5	30.2	26	6.6	30	13.3	17.6	14.1	14.8	–	–	–	–	–	–	–	–	–	–	–	–	63	74	63	67
VIII	–	–	–	–	22.4	11.7	29.4	15	5.2	31	14.6	20.7	16.1	16.9	–	–	–	–	–	–	–	–	–	–	–	–	58	67	49	58
IX	–	–	–	–	17.2	7.1	26.4	4, 12	1.4	27	9.4	15.4	11.6	12.0	–	–	–	–	–	–	–	–	–	–	–	–	59	64	49	57
X	–	–	–	–	12.7	3.6	19.2	11	-3.0	16	5.5	11.5	7.0	7.8	–	–	–	–	–	–	–	–	–	–	–	–	58	50	32	47
XI	–	–	–	–	7.3	1.8	16.2	1, 8	-4.0	17	3.1	5.8	3.8	4.1	–	–	–	–	–	–	–	–	–	–	–	–	81	83	73	79
XII	–	–	–	–	-2.3	-7.8	6.2	13	-17.9	23	-5.6	-4.2	-5.3	-5.1	–	–	–	–	–	–	–	–	–	–	–	–	81	80	83	81
Rok	–	–	–	–	10.4	2.5	30.2	26.VII	-17.9	23. XII	4.8	8.7	5.9	6.3	–	–	–	–	–	–	–	–	–	–	–	–	73	74	65	71

Babia Góra $\varphi = 49°35'$ $\lambda = 19°31'$

I	–	–	–	–	-1.1	-6.6	5.8	1	-18.7	31	-4.2	-3.6	-4.0	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	89	78	69	79
II	–	–	–	–	-4.3	-9.9	-0.3	13	-17.7	1	-7.8	-6.0	-6.9	-6.9	–	–	–	–	–	–	–	–	–	–	–	–	94	91	86	90
III	–	–	–	–	-3.5	-9.0	7.8	5	-15.2	17	-6.8	-5.1	-6.7	-6.3	–	–	–	–	–	–	–	–	–	–	–	–	81	84	73	79
IV	–	–	–	–	7.9	0.5	21.8	23	-5.3	7	3.7	5.5	2.9	3.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	8.0	1.5	15.3	31	-5.9	1	4.9	6.4	4.4	5.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	11.7	4.7	23.2	23	-2.6	7	7.5	9.6	6.7	7.6	–	–	–	–	–	–	–	–	–	–	–	–	76	68	72	72
VII	–	–	–	–	14.1	6.9	22.7	26	1.4	2	9.7	12.4	9.2	10.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	17.3	8.8	24.7	15	3.4	31	12.3	15.5	11.7	12.8	–	–	–	–	–	–	–	–	–	–	–	–	62	59	68	63
IX	–	–	–	–	11.3	4.1	20.2	4	-0.9	24, 25	6.7	9.6	6.9	7.5	–	–	–	–	–	–	–	–	–	–	–	–	59	59	46	55
X	–	–	–	–	9.3	3.0	15.8	2, 4	-2.2	16	4.8	8.1	4.7	5.6	–	–	–	–	–	–	–	–	–	–	–	–	46	44	39	43
XI	–	–	–	–	3.4	-1.7	11.5	1	-8.4	19	0.7	1.8	0.6	0.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-5.3	-10.2	0.3	9, 13, 14	-24.7	23	-7.6	-7.1	-8.1	-7.7	–	–	–	–	–	–	–	–	–	–	–	–	76	73	61	70
Rok	–	–	–	–	5.7	-0.7	24.7	15. VIII	-24.7	23. XII	2.0	3.9	1.8	2.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kamienica $\varphi = 49°35'$ $\lambda = 20°21'$

I	–	–	–	–	2.6	-5.6	8.6	2.2	-18.3	31	-3.5	1.1	-2.1	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	70	62	58	63
II	–	–	–	–	1.0	-6.8	6.8	13	-14.4	25	-4.7	-0.9	-3.0	-2.9	–	–	–	–	–	–	–	–	–	–	–	–	96	78	91	88
III	–	–	–	–	2.4	-7.0	15.6	5	-18.4	9	-5.0	0.9	-3.7	-2.9	–	–	–	–	–	–	–	–	–	–	–	–	80	73	69	74
IV	–	–	–	–	14.4	2.4	25.9	23	-2.8	2	5.7	13.0	6.4	7.9	–	–	–	–	–	–	–	–	–	–	–	–	61	71	46	59
V	–	–	–	–	15.1	4.8	23.0	8	-3.7	2	8.5	12.9	8.7	9.7	–	–	–	–	–	–	–	–	–	–	–	–	75	85	61	74
VI	–	–	–	–	17.7	6.6	28.5	23	1.0	9	11.3	15.8	11.3	12.4	–	–	–	–	–	–	–	–	–	–	–	–	61	75	71	69
VII	–	–	–	–	20.5	8.8	29.9	27	3.1	5	12.9	19.1	12.8	14.4	–	–	–	–	–	–	–	–	–	–	–	–	60	66	61	62
VIII	–	–	–	–	23.5	9.4	30.1	15	2.9	31	13.3	21.6	14.7	16.1	–	–	–	–	–	–	–	–	–	–	–	–	56	56	43	52
IX	–	–	–	–	18.6	4.8	28.2	4	-0.9	27	7.6	16.8	9.8	11.0	–	–	–	–	–	–	–	–	–	–	–	–	63	53	35	50
X	–	–	–	–	14.9	0.9	22.1	4	-4.4	22	2.7	13.8	5.4	6.8	–	–	–	–	–	–	–	–	–	–	–	–	68	43	33	48
XI	–	–	–	–	8.2	1.1	17.5	3	-3.8	17	2.4	6.8	3.9	4.2	–	–	–	–	–	–	–	–	–	–	–	–	79	79	76	78
XII	–	–	–	–	-1.8	-10.3	5.4	13	-20.2	23	-7.0	-3.7	-6.6	-6.0	–	–	–	–	–	–	–	–	–	–	–	–	76	70	74	73
Rok	–	–	–	–	11.4	0.8	30.1	15. VIII	-20.2	23. XII	3.7	9.8	4.8	5.8	–	–	–	–	–	–	–	–	–	–	–	–	70	68	60	66

Raba Wyżna $\varphi = 49°34'$ $\lambda = 19°53'$

I	–	–	–	–	2.1	-3.5	8.5	22	-16.0	31	-2.1	0.7	-1.3	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	71	55	57	61
II	–	–	–	–	-0.4	-7.3	4.0	7	-19.6	25	-5.3	-1.9	-3.8	-3.7	–	–	–	–	–	–	–	–	–	–	–	–	89	75	84	83
III	–	–	–	–	1.8	-6.3	13.8	5	-15.4	26	-4.6	0.4	-3.0	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	73	70	69	71
IV	–	–	–	–	13.4	3.4	25.0	23	-0.5	7	6.0	11.8	6.4	7.6	–	–	–	–	–	–	–	–	–	–	–	–	57	65	46	56
V	–	–	–	–	14.2	5.4	21.6	19	-1.1	3	7.8	12.3	8.7	9.4	–	–	–	–	–	–	–	–	–	–	–	–	66	75	66	69
VI	–	–	–	–	17.0	7.9	28.5	16	0.7	5	11.1	15.4	11.3	12.3	–	–	–	–	–	–	–	–	–	–	–	–	60	72	62	65
VII	–	–	–	–	19.7	9.5	29.5	27	4.5	5	12.9	18.1	13.2	14.4	–	–	–	–	–	–	–	–	–	–	–	–	50	67	53	57
VIII	–	–	–	–	22.8	11.1	30.3	15	5.0	31	13.9	21.3	14.9	16.2	–	–	–	–	–	–	–	–	–	–	–	–	45	55	38	46
IX	–	–	–	–	17.5	6.2	27.0	4	-1.2	25	8.6	15.8	10.0	11.1	–	–	–	–	–	–	–	–	–	–	–	–	49	55	37	47
X	–	–	–	–	14.3	3.1	22.0	3	-3.7	16	4.7	13.2	5.8	7.4	–	–	–	–	–	–	–	–	–	–	–	–	43	42	33	39
XI	–	–	–	–	6.6	0.5	16.9	8	-3.9	17	1.8	5.6	2.7	3.2	–	–	–	–	–	–	–	–	–	–	–	–	75	75	83	78
XII	–	–	–	–	-2.5	-9.5	5.1	9	-20.7	22, 23	-6.8	-3.9	-6.5	-5.9	–	–	–	–	–	–	–	–	–	–	–	–	80	68	66	71
Rok	–	–	–	–	10.5	1.7	30.3	15.VIII	-20.7	22.23.XII	4.0	9.1	4.9	5.7	–	–	–	–	–	–	–	–	–	–	–	–	63	64	58	62

Płaszkowa $H_s = 522\,m$ $h_w = 15\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU nD, vmD: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n) Temperatura T: Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v: ≥ 10	≥ 15	◔	●	Opad R: R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R FO
I	3	4.7	2	2.0	8	2.8	6	5.0	14	4.0	25	4.8	24	4.4	3	6.3	8	4.0	41	10.7	28	3	6	27	·	1	·	2	15	12	9	1	1	26	·
II	4	2.0	4	2.2	6	2.7	·	·	4	6.0	11	5.5	31	7.7	10	4.9	14	4.8	75	11.8	17	4	12	28	·	8	2	·	23	21	15	2	3	28	·
III	9	3.0	11	3.6	7	3.7	6	3.7	12	6.5	11	3.4	15	5.4	9	6.2	13	3.9	53	8.6	12	7	16	26	·	5	1	·	19	18	11	·	6	30	·
IV	5	3.4	5	2.6	5	2.6	8	5.1	17	6.1	18	2.8	22	4.3	4	3.0	6	3.8	83	23.9	6	·	·	3	·	3	·	6	11	13	10	3	5	1	·
V	4	2.2	2	2.0	5	2.6	4	4.2	6	4.3	24	3.8	28	3.8	6	2.7	14	3.0	149	16.4	20	·	·	3	·	3	·	·	17	26	22	6	4	1	4
VI	4	2.8	4	2.8	3	2.3	1	2.0	3	1.3	23	4.2	21	3.8	16	3.0	15	2.9	216	62.3	4	·	·	·	4	·	·	1	14	18	15	7	1	·	5
VII	5	3.2	4	3.5	4	2.8	·	·	9	3.8	26	3.2	23	3.2	8	3.0	14	2.8	125	40.3	18	·	·	·	3	1	1	3	10	13	12	5	1	·	9
VIII	2	2.5	3	3.0	4	1.8	3	4.6	5	3.2	15	3.7	38	2.9	4	3.0	19	2.4	55	18.7	5	·	·	·	10	·	·	3	3	13	7	2	·	·	5
IX	1	2.0	·	·	10	2.2	1	7.0	8	4.4	28	4.2	26	4.2	2	2.0	14	3.3	71	17.5	18	·	·	·	4	2	·	6	9	14	8	3	4	·	1
X	6	2.3	5	2.0	10	1.9	2	2.5	4	3.0	8	3.0	30	2.3	5	2.0	23	1.7	10	3.5	30	·	·	5	·	·	·	11	8	9	4	·	9	·	·
XI	2	2.0	9	2.6	11	2.3	12	3.6	18	4.1	11	2.5	20	2.5	·	·	7	2.7	90	21.2	23	·	2	14	·	1	·	3	20	19	10	4	12	13	·
XII	9	2.6	6	2.3	6	2.2	3	6.3	13.5	5.0	16.5	3.5	20	3.1	5	2.6	14	2.9	52[2]	11.0	14	11	16	31	·	2	1	2	20	18	14	1	2	31	·
Rok	54	2.7	55	2.4	79	2.5	46	3.7	113.5	4.3	216.5	3.7	298	4.0	72	3.2	161	3.2	1020[2]	62.3	4.VI	25	52	137	21	26	5	37	169	194	137	34	48	130	24

Babia Góra $H_s = 1180\,m$ $h_w = 17{,}5\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	≥ 10	≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R FO
I	·	·		·	2	2.0	3	4.0	23.5	4.9	6.5	3.8	14	3.2	5	2.8	39	2.3	113	29.1	27	5	17	30	·	·	·	·	18	13	13	2	11	31	—
II	3	1.7	·	·	·	·	1	4.0	7	4.9	3	3.3	19	4.7	5	4.8	46	2.0	175	22.9	5	12	28	28	·	2	·	·	21	19	19	5	20	28	—
III	6	3.3	2	3.0	2	2.0	2	5.0	13	3.8	6	3.7	4	3.0	2	3.0	56	1.4	154	35.2	16	18	24	29	·	·	·	·	19	15	14	4	23	31	—
IV	5	2.4	·	·	·	·	·	·	8	6.1	8	3.9	8	4.2	6	5.7	55	1.8	176	73.8	6	·	1	16	·	·	·	—	—	11	11	5	16	28	—
V	1.5	2.7	·	·	1	4.0	2	2.0	9	2.7	3	2.0	17	3.1	2.5	3.2	57	1.1	247	37.7	20	·	2	5	·	·	·	—	—	25	25	11	25	7	—
VI	1	4.0	1	4.0	·	·	·	·	3	2.0	1	4.0	8	2.2	3	3.3	73	0.5	174	39.2	1	·	1	8	·	·	·	2	16	13	12	5	14	8	—
VII	·	·	·	·	·	·	·	·	10.5	2.6	4.5	2.0	20	2.6	5	2.0	53	1.1	166	57.3	18	·	·	·	·	·	·	—	—	17	15	5	16	·	—
VIII	1	2.0	1	2.0	·	·	2	4.5	1	4.0	3	3.3	26	3.2	1	2.0	58	1.2	61	20.0	15	·	·	·	·	·	·	3	11	11	10	2	12	·	—
IX	·	·	·	·	·	·	2	6.0	17	4.6	4	2.8	24	3.3	3	4.0	40	2.2	102	20.2	18	·	·	3	·	·	·	8	11	14	14	4	12	·	—
X	3	3.3	·	·	2	3.0	1	4.0	13	3.5	5	3.6	7	2.3	2	3.0	60	1.1	50	16.4	6	·	·	8	·	·	·	13	10	11	9	1	8	·	—
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	129	21.5	15	·	11	17	·	—	—	—	—	16	15	5	17	15	—
XII	·	·	·	·	5	3.2	6.5	6.6	7.5	9.6	16	6.2	2.5	4.6	2.5	4.4	53	2.7	107	15.7	16	13	27	31	·	5	·	5	16	17	15	4	11	31	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	1654	73.8	6.IV	48	111	175	·	—	—	—	—	182	172	53	185	179	—

Kamienica $H_s = 460\,m$ $h_w = 21\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	≥ 10	≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R FO
I	2.5	2.8	·	·	·	·	4.5	3.7	2.5	3.0	16	4.3	21	2.9	20.5	2.4	26	2.3	57	17.3	27	8	7	29	·	4	·	2	10	15	10	2	1	26	·
II	5.5	1.9	2.5	1.0	2	1.0	·	·	2	2.0	6.5	10.5	23	5.5	16.5	4.8	26	3.5	81	14.9	12	5	9	26	·	6	4	·	20	17	13	2	3	28	·
III	6	2.2	9.5	2.1	2	3.8	0.5	3.0	2.5	1.6	3	2.5	1	2.0	36.5	2.8	32	1.7	54	16.6	16	7	12	28	·	1	1	1	16	14	12	1	3	26	·
IV	1	3.0	1.5	3.0	5.5	3.0	9.5	3.5	3	6.8	9.5	3.8	31	3.2	10	2.4	19	2.7	124	75.6	6	·	·	7	1	3	·	5	10	16	11	3	2	1	·
V	1.5	2.7	1.5	2.3	1.5	3.0	4.5	2.6	8	2.0	16	3.5	24.5	3.2	9.5	2.7	26	2.2	103	15.2	20	·	·	5	·	·	·	1	12	26	21	2	4	·	3
VI	1.5	3.0	1	2.0	3.5	2.7	4.5	2.6	1	2.0	3.5	5.0	14	3.0	29	2.7	32	1.9	193	66.1	5	·	·	·	4	1	·	4	12	16	13	5	1	·	5
VII	3	2.5	2	2.8	0.5	3.0	1.5	2.3	5	1.7	9.5	2.4	21.5	3.2	15	2.7	35	1.7	132	49.3	18	·	·	·	5	1	1	3	8	14	11	4	1	·	6
VIII	0.5	2.0	3.5	1.7	1	2.5	2.5	2.2	1	5.0	14	2.5	18.5	3.2	12	1.7	40	1.5	47	12.8	16	·	·	·	10	·	·	·	2	12	8	2	3	·	5
IX	·	·	·	·	0.5	3.0	4.5	2.0	3.5	4.6	10	5.0	9.5	3.4	14	2.5	48	1.6	43	11.2	18	·	·	2	7	3	·	5	4	11	9	1	8	·	1
X	1.5	1.7	0.5	1.0	1	1.0	4.5	1.6	5	1.7	5.5	2.4	7.5	2.4	5.5	1.7	62	0.6	5	2.3	30	·	·	15	·	·	·	6	5	6	2	·	13	·	·
XI	0.5	1.0	9	1.5	2.5	2.4	7	2.7	5	2.4	6.5	1.5	8.5	2.6	17	2.7	34	1.4	78	10.0	24	·	1	12	·	1	·	3	19	17	11	1	5	9	·
XII	5.5	2.8	4.5	2.0	1	2.5	·	·	1	3.0	1.5	1.3	9	3.1	14.5	4.0	56	1.2	55	14.4	30	15	16	31	·	·	·	1	13	15	12	2	1	31	·
Rok	29	2.1	35.5	1.6	21	2.3	43.5	2.2	39.5	3.0	101.5	3.7	189	3.1	200	2.8	436	1.9	972	75.6	6.IV	35	45	155	27	20	6	31	131	179	133	25	45	121	20

Raba Wyżna $H_s = 600\,m$ $h_w = 16\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	≥ 10	≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R FO
I	5	1.4	3	1.0	1	1.0	23.5	1.3	14	3.0	11.5	3.8	4	2.5	7	1.0	24	1.6	50	14.0	27	3	6	22	·	1	·	3	11	13	8	2	·	19	·
II	7	1.3	·	·	0.5	1.0	14.5	1.0	5	4.6	8	4.8	4	4.5	17	2.4	28	1.7	93	20.0	12	5	12	27	·	1	·	1	19	16	14	3	1	28	·
III	8	2.0	7	1.6	·	·	11.5	1.0	7	1.9	10.5	2.3	5	1.4	5	1.8	39	1.0	68	15.7	16	8	12	27	·	·	·	3	15	13	12	1	·	30	·
IV	5.5	1.0	1.5	1.0	·	·	23	1.1	11	1.7	7	1.0	1	1.0	13	1.3	28	0.8	100	54.5	6	·	·	2	·	·	·	8	10	13	11	2	5	3	·
V	5	1.4	3	1.0	1	1.0	12	1.0	7	1.3	20	1.6	5	1.4	11	1.0	29	0.9	156	20.0	20	·	·	4	·	·	·	1	12	23	22	4	1	·	3
VI	12	1.3	8	1.0	1.5	1.0	14.5	1.0	9	1.4	7	1.6	3	1.0	16	1.2	19	1.0	178	55.5	1	·	·	·	5	·	·	4	12	14	13	4	·	·	3
VII	13	1.2	7	1.0	·	·	18	1.1	7	1.3	13	1.5	3	1.0	5	1.0	27	0.8	131	57.5	18	·	·	·	5	·	·	4	8	12	10	4	·	·	6
VIII	3	1.0	5	1.0	4	1.0	29	1.2	4	2.0	15	2.3	4	2.0	7	1.3	22	1.2	54	18.5	15	·	·	·	9	·	·	5	3	14	9	1	·	·	3
IX	3	1.0	2	1.0	·	·	16.5	1.0	10.5	2.0	14	1.6	1	1.0	7	1.0	36	0.8	57	15.0	18	·	·	1	3	·	·	10	5	12	11	2	3	·	1
X	6	1.0	6	1.0	3	1.0	26.5	1.0	4.5	1.0	6	1.7	1	1.0	1	1.0	39	0.6	19	9.5	6	·	·	5	·	·	·	15	9	8	6	·	5	·	·
XI	1	1.0	6	1.0	1	1.0	15	1.1	3	1.0	3	1.7	·	·	1	1.0	60	0.4	91	15.0	23	·	3	15	·	·	·	2	18	19	15	3	7	13	·
XII	6	1.0	9	1.0	·	·	22	1.1	7	2.4	14	3.7	·	·	1	3.0	34	1.2	51	15.0	30	13	16	31	·	·	·	1	15	14	10	2	·	31	·
Rok	74.5	1.2	57.5	1.0	12	0.6	226	1.1	89	2.0	129	2.3	31	1.4	91	1.4	385	1.0	1048	57.5	18.VII	29	49	134	22	2	·	57	137	171	141	28	22	124	16

Iwonicz-Zdrój $\varphi = 49°34'$ $\lambda = 21°48'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	968.8	982.6	948.3	1019.1	0.6	-3.5	6.0	23	-14.5	31	-2.2	-0.6	-1.9	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.5	6.0	6.6
II	966.6	983.1	939.8	1017.0	-0.6	-6.2	3.6	20, 21	-18.4	25	-4.5	-2.0	-3.2	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.4	8.5	8.5
III	961.5	977.3	945.5	1011.4	1.3	-4.8	12.2	5	-12.9	20	-3.1	0.6	-1.9	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.0	7.0	7.8
IV	966.4	978.1	942.9	1014.4	15.3	4.9	25.5	22	-1.1	30	7.7	13.7	8.3	9.5	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.8	3.5	5.1
V	966.1	973.2	952.8	1014.0	15.8	6.6	24.8	28	-1.4	2	9.8	14.1	9.8	10.9	–	–	–	–	–	–	–	–	–	–	–	–	7.2	8.2	6.5	7.3
VI	970.3	978.7	961.5	1018.0	17.9	9.1	28.0	16	2.1	7	12.6	16.2	12.1	13.2	–	–	–	–	–	–	–	–	–	–	–	–	5.4	7.1	6.4	6.3
VII	968.0	978.0	955.9	1015.3	20.2	10.8	29.6	27	6.7	30	14.2	18.8	13.5	15.0	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.8	5.9	6.1
VIII	969.8	975.4	961.3	1016.8	22.8	11.9	28.9	13	6.0	31	15.2	21.4	15.5	16.9	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.2	4.3	5.2
IX	970.1	980.8	958.4	1018.0	17.4	8.1	26.3	5	2.3	25	10.2	15.8	11.6	12.3	11.2	13.1	12.0	12.1	90	74	88	84	1.6	5.5	1.9	3.0	5.6	6.0	4.9	5.5
X	974.3	986.4	959.3	1023.1	13.1	3.7	19.3	3	-3.4	16	5.5	12.0	6.7	7.7	8.4	10.2	8.9	9.2	91	73	89	84	0.9	4.2	1.1	2.1	5.9	4.3	1.6	4.0
XI	968.5	982.5	951.1	1017.4	7.9	2.4	16.4	6	-3.7	28	4.3	6.6	4.5	5.0	7.6	8.3	7.7	7.9	90	83	89	87	1.0	2.1	1.1	1.4	8.7	7.6	7.8	8.0
XII	967.1	993.3	929.0	1017.9	-2.7	-7.2	4.4	14	-15.9	23	-5.2	-4.1	-5.2	-5.0	3.9	4.0	3.9	3.9	90	86	90	89	0.5	0.7	0.5	0.6	8.5	8.7	8.6	8.6
Rok	968.1	993.3	929.0	1016.8	10.8	3.0	29.6	27. VII	-18.4	25. II	5.4	9.4	5.8	6.6	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.0	5.9	6.6

Sanok $\varphi = 49°34'$ $\lambda = 22°12'$

I	–	–	–	–	2.6	–	8.9	22	–	–	-1.0	1.1	-0.4	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	0.4	-7.4	3.9	21	-23.5	25	-5.1	-1.2	-3.2	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	2.9	-5.4	14.7	5	-17.4	21	-3.6	0.9	-2.1	-1.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	17.1	4.4	27.8	23	-1.5	2, 30	7.2	15.1	9.4	10.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	17.2	6.6	26.8	28	-2.5	2	9.5	15.3	10.3	11.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	19.4	8.6	29.4	23	2.5	7	12.3	17.6	13.0	14.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.1	10.0	30.6	27	5.0	9	13.3	19.5	14.2	15.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	24.0	11.8	30.4	13	4.5	31	14.3	22.5	15.9	17.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	18.6	6.7	28.0	5	0.8	27	9.2	16.9	11.2	12.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	14.7	2.0	21.0	4	-3.2	16, 17	3.7	13.6	5.4	7.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	9.5	1.3	18.1	1, 8	-4.2	18	3.3	7.6	4.3	4.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-1.3	-7.0	7.7	14	-14.5	23	-5.0	-3.0	-4.4	-4.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	12.2	–	30.6	27. VII	–	–	4.8	10.5	6.1	6.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Stańcowa $\varphi = 49°33'$ $\lambda = 19°32'$

I	–	–	–	–	0.1	-5.7	6.2	22	-15.7	31	-3.4	-1.4	-3.5	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.8	6.8	7.0
II	–	–	–	–	-2.2	-8.4	1.8	9	-19.1	26	-7.3	-4.0	-5.2	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.0	8.9	8.6
III	–	–	–	–	-0.5	-7.7	9.5	5	-13.3	14	-5.9	-2.4	-5.0	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.2	8.1	8.3
IV	–	–	–	–	10.4	1.4	21.8	23, 24	-4.4	3	4.0	8.8	3.6	5.0	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.0	5.4	6.4
V	–	–	–	–	11.2	3.0	17.7	19	-3.8	1	6.0	9.4	5.7	6.7	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.2	7.1	7.8
VI	–	–	–	–	14.6	6.1	24.8	16, 23	-0.1	7	9.4	13.0	8.5	9.8	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.9	6.0	6.8
VII	–	–	–	–	17.1	8.1	26.6	27	2.7	6	11.3	15.9	10.9	12.2	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.9	5.9	6.4
VIII	–	–	–	–	20.3	10.1	27.5	15	3.8	31	13.1	18.9	13.6	14.8	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.9	4.7	5.4
IX	–	–	–	–	14.8	5.1	23.8	4	0.6	24, 25	7.9	13.2	8.4	9.5	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.3	3.4	5.0
X	–	–	–	–	12.5	3.0	19.9	4	-1.5	22	5.1	11.7	5.4	6.9	–	–	–	–	–	–	–	–	–	–	–	–	3.9	4.5	3.1	3.8
XI	–	–	–	–	5.3	0.1	14.8	7, 8	-5.6	24	1.7	4.1	1.8	2.4	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.9	8.7	8.3
XII	–	–	–	–	-3.0	-9.5	4.9	7	-22.8	23	-7.0	-4.9	-7.1	-6.5	–	–	–	–	–	–	–	–	–	–	–	–	8.3	6.8	6.9	7.3
Rok	–	–	–	–	8.4	0.5	27.5	15. VIII	-22.8	23. XII	2.9	6.9	3.1	4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.0	6.2	6.7

Obidowa $\varphi = 49°33'$ $\lambda = 19°58'$

I	–	–	–	–	-0.5	-5.6	5.6	22	-18.6	31	-3.9	-2.2	-3.4	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.4	6.8	7.9	7.7
II	–	–	–	–	-2.7	-7.9	2.0	13	-18.1	1	-6.9	-4.6	-5.0	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	9.6	8.2	8.3	8.7
III	–	–	–	–	-1.0	-7.1	10.7	5	-12.9	21	-5.4	-2.6	-4.1	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.9	7.1	8.0
IV	–	–	–	–	10.8	3.0	22.7	23	-3.5	3	4.8	8.8	6.6	6.7	–	–	–	–	–	–	–	–	–	–	–	–	6.7	8.0	5.0	6.6
V	–	–	–	–	11.4	4.1	18.4	19	-3.2	1, 2	5.9	9.4	7.6	7.6	–	–	–	–	–	–	–	–	–	–	–	–	8.5	9.0	7.5	8.3
VI	–	–	–	–	14.5	7.0	25.3	16, 23	-0.7	7	8.8	12.6	10.5	10.6	–	–	–	–	–	–	–	–	–	–	–	–	6.9	8.4	6.9	7.4
VII	–	–	–	–	17.0	9.2	27.3	27	3.3	5	10.9	15.5	12.7	13.0	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.2	6.9	7.5
VIII	–	–	–	–	20.1	11.0	27.3	15	5.9	31	12.6	18.4	14.6	15.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.3	4.8	6.3
IX	–	–	–	–	14.8	5.3	24.8	4	-1.9	25	7.4	12.9	9.8	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.1	7.0	3.7	5.6
X	–	–	–	–	11.6	3.6	18.8	3	0.0	16, 25	4.9	10.7	6.8	7.3	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.5	3.6	4.4
XI	–	–	–	–	5.0	-0.6	15.2	8	-5.2	24	0.8	3.3	1.9	2.0	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.3	8.1	8.5
XII	–	–	–	–	-4.0	-9.3	3.6	7	-20.2	23	-7.5	-6.1	-7.1	-7.0	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.8	7.5	8.0
Rok	–	–	–	–	8.1	1.1	27.3	27. VII, 15. VIII	-20.2	23. XII	2.7	6.3	4.2	4.4	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.6	6.4	7.2

Iwonicz-Zdrój $H_s = 410\,m$ $H_b = 403{,}3\,m$ $h_w = 16{,}2\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU °D, v=D																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr v				Opad R					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	☾	●	R≥0.1	R≥10	R≥100	≡	≡	≈R
I	4.5	3.0	1.5	3.7	·	·	·	·	41.5	7.2	11.5	4.8	3.5	2.7	7.5	2.6	23	4.3	44	8.1	29	2	10	27	·	7	3	5	13	10	9	·	·	19²	·
II	10.5	3.0	1	1.0	·	·	·	·	11.5	7.6	8.5	4.1	4.5	2.6	13	3.8	35	2.6	50	10.9	13	4	13	27	·	3	1	·	19	15	11	2	4	28	·
III	10	2.8	6	3.8	0.5	2.0	·	·	22	3.7	7	3.1	2	2.8	9.5	3.4	36	2.1	62	10.6	7	5	14	25	·	·	·	·	20	14	13	1	1	30	·
IV	10	1.8	3.5	1.4	1	3.0	1	1.5	21	4.0	5	2.1	0.5	3.0	6	2.2	42	1.5	38	15.7	27	·	·	3	3	1	·	9	7	9	7	1	3	·	·
V	10	1.5	·	·	·	·	0.5	3.0	12	3.5	5	2.3	3	2.2	8.5	2.0	54	1.0	132	29.3	20	·	·	2	·	·	·	1	12	23	21	2	3	·	3
VI	10.5	2.0	2.5	1.0	·	·	·	·	2.5	1.4	5	1.5	7	1.7	12.5	2.2	50	0.8	141	26.3	1	·	·	·	5	·	·	5	11	15	14	5	5	·	4
VII	4	1.5	2.5	2.0	·	·	·	·	10.5	2.1	6.5	1.5	5	1.6	6.5	1.8	58	0.7	163	38.5	19	·	·	·	4	·	·	4	11	16	15	5	4	·	4
VIII	6.5	1.5	1.5	1.7	1	1.0	·	·	9.5	2.9	7.5	1.9	2	1.5	9	1.6	56	0.8	66	15.6	16	·	·	·	8	·	·	4	7	15	13	1	2	·	6
IX	0.5	2.0	3	2.6	0.5	2.0	1.5	4.0	16	4.0	13.5	2.6	2.5	2.0	3.5	2.3	49	1.6	63	11.8	7	·	·	·	1	1	·	6	8	13	11	2	4	·	2
X	5.5	1.5	3	1.7	1.5	1.7	·	·	20	2.5	9.5	1.9	1	1.5	1.5	1.7	51	0.9	5	2.1	19	·	·	5	·	·	·	10	4	5	2	·	12	·	·
XI	2	1.0	3	2.3	5	1.2	2.5	2.6	33	2.9	2.5	1.4	·	·	2	1.0	40	1.4	90²	21.2	23	·	1	11	·	2	·	·	19	14	11	3	8	11	·
XII	12	2.1	1.5	2.0	·	·	0.5	2.0	30	7.0	5.5	4.1	2	2.0	6.5	2.4	35	3.0	45	12.9	14	10	19	31	·	6	2	2	24	14	7	2	·	31	·
Rok	8.6	2.0	2.9	1.9	9.5	0.9	6	1.1	229.5	4.1	8.7	2.6	3.3	2.0	8.6	2.2	529	1.7	899²	38.5	19. VII	21	57	131	21	20	6	46	155	163	134	24	46	119²	19

Sanok $H_s = 314\,m$ $h_w = 16\,m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	3.7	11.1	13	–	6	–	·	–	–	–	–	11	7	1	·	10	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.3	12.0	13	7	11	27	·	–	–	–	–	17	9	1	·	28	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	50²	14.1	7	8	8	24		–	–	–	–	13	9	2	·	26	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	25?	8.4	27	·	·	4	5	–	–	–	–	6	5	·	·	·	·
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	9.8	19.4	20	·	·	2	1	–	–	–	–	21	18	3	·	·	3
VI	3	4.3	5	2.6	2	2.0	4	3.0	3	5.0	·	·	2.7	7.7	9	6.3	37	3.6	10.3	22.5	1	·	·	·	8	3	2	–	–	12	12	4	·	·	2
VII	4	3.5	6	3.0	4	3.5	10	3.6	6	5.7	·	·	12	5.2	2	5.0	49	2.0	10.1	29.3	19	·	·	·	5	·	·	–	–	11	11	5	1	·	3
VIII	·	·	·	·	2	5.0	1.5	3.8	6	10.0	1	5.0	1.2	6.2	5	5.0	52	2.5	6.1	12.2	22	·	·	·	12	3	2	–	–	14	12	1	3	·	2
IX	1	3.0	·	·	3	5.0	1.1	3.2	10	9.4	3	4.3	10	6.4	2	4.0	50	2.6	8.4	18.0	5	·	·	·	2	4	2	–	–	12	11	3	5	·	2
X	2	4.0	5	3.8	·	·	4	3.0	2	6.0	3	5.7	10	3.7	4	4.0	63	1.3	4	2.0	30	·	·	1.1	·	·	·	–	–	4	2	·	8	·	·
XI	·	·	1	3.0	3	3.0	1.3	2.5	4	13.0	1	7.0	6	3.0	5	3.0	57	1.5	71²	15.0	16	·	·	10	·	1	1	–	–	17	10	3	3	–	·
XII	1	3.0	3	3.7	5	3.0	1.2	4.5	12	11.8	1	3.0	10	5.0	4	7.0	4.5	3.3	39	10.7	30	11	16	30	·	3	3	–	–	14	9	2	1	–	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	716?	29.3	19. VII	–	41	–	33	–	–	–	–	152	115	25	21	–	12

Stańcowa $H_s = 850\,m$ $h_w = 18{,}5\,m$

I	6	3.7	7	3.4	·	·	·	·	·	·	3.7	2.5	3.6	1.8	6	1.7	1	2.3	10.1	35.7	27	4	13	29	·	·	·	3	15	19	11	3	·	31	·
II	6	3.3	1.8	1.2	1	1.0	2	1.0	·	·	11	2.9	2.7	4.6	1.5	6.4	4	3.5	13.5	20.8	5	7	20	28	·	3	2	·	19	22	17	4	1	28	·
III	12	1.8	1.3	3.8	1.5	2.3	1	1.0	·	·	2.9	1.8	11	1.3	10	3.0	2	2.2	8.0	16.0	12	1.5	1.8	28	·	·	·	2	21	23	14	2	3	31	·
IV	1.8	1.7	11	2.4	1	3.0	·		·	·	2.4	2.5	2.1	1.9	1.4	2.6	1	2.2	11.0	45.8	6	·	·	9	·	2	·	5	11	15	11	4	2	18	·
V	10	1.1	10	1.2	3	1.0	·	·	1	1.0	2.5	2.2	3.6	1.4	6	1.0	2	1.5	17.8	20.4	9, 20	·	·	6	·	·	·	1	14	28	24	6	2	1	4
VI	1.9	2.6	2.1	1.3	4	2.0	·	·	4	1.8	9	1.4	1.3	2.5	1.9	2.0	1	2.0	24.4	87.7	5	·	·	1	·	·	·	1	13	17	12	4	1	1	5
VII	6	1.0	·	·	1	2.0	7	1.3	4	3.0	2.7	1.5	3.3	1.4	1.4	1.4	1	1.5	9.4	35.0	18	·	·	·	2	·	·	3	8	16	14	2	·	·	6
VIII	2	1.5	4	1.0	·	·	1	2.0	5	1.4	2.2	2.0	3.3	1.5	2.6	1.3	·	1.6	5.4	17.2	15	·	·	·	3	·	·	·	5	13	12	1	·	·	4
IX	4	1.2	3	1.3	·	·	2	1.0	4	3.8	3.4	2.6	2.0	1.8	2.0	2.0	3	2.1	8.7	18.2	23	·	·	·	·	·	·	8	5	13	11	4	2	·	1
X	8	1.8	1.9	1.2	6	1.3	1	1.0	2	1.0	2.0	1.4	1.3	1.7	1.2	1.2	1.2	1.2	2.7	8.3	6	·	·	4	·	·	·	1.7	9	9	7	·	3	·	·
XI	1.5	1.3	9	1.4	5	1.4	·		3	1.0	2.5	2.0	1.4	1.2	1.3	1.3	6	1.4	11.1	15.3	23	·	7	16	·	·	·	·	24	18	15	6	6	1.4	·
XII	2.1	1.5	2.0	2.0	1	1.0	·	·	·	·	1.6	2.4	2.0	2.2	1.0	3.1	5	2.0	7.9	11.8	16	1.3	2.3	31	·	1	·	2	16	21	12	1	3	31	·
Rok	12.7	1.9	13.5	1.7	3.7	1.2	1.4	0.6	2.3	1.1	27.9	2.1	27.7	1.9	16.5	2.2	3.8	2.0	130.0	87.7	5. VI	3.9	8.1	152	5	6	2	4.2	160	214	160	3.7	2.3	155	2.0

Obidowa $H_s = 800\,m$ $h_w = 20{,}5\,m$

I	21.5	3.0	·	·	·	·	1	4.0	47.5	3.9	15.5	6.3	1	4.0	0.5	2.0	6	3.9	3.3	8.5	27	4	16	28	·	4	4	1	18	18	9	·	3	31	–
II	30.5	4.0	·	·	2	2.0	1.5	8.0	18.5	4.1	9	8.4	2	4.5	4.5	6.2	16	3.9	44	6.1	19	6	23	28	·	4	2	·	19	19	14	·	6	28	–
III	3.0	4.0	2	2.5	3	2.3	2.5	2.0	28.5	3.8	7	7.3	2	3.5	2	4.5	16	3.3	4.2	7.4	15	10	19	28	·	4	1	2	20	15	11	·	4	31	–
IV	2.8	3.2	2	2.5	5	3.4	5.5	2.0	28.5	2.9	4	4.2	3	4.0	2	5.5	12	2.7	5.7	29.4	6	·	·	9	·	·	·	7	11	17	10	1	13	12	–
V	3.0	3.0	1	2.0	·	·	2	2.0	21	2.5	2.0	3.5	6	3.2	·	·	13	2.6	11.7	18.7	9	·	·	5	·	1	1	1	19	24	20	5	7	1	–
VI	4.5	3.6	1	2.0	·	·	3	2.0	17.5	2.5	8.5	3.7	5	3.6	1	2.5	9	3.0	13.9	33.0	1	·	·	2	2	·	·	3	16	15	15	4	5	2	–
VII	2.6	2.5	1	3.0	1	2.0	3	2.0	17	2.5	1.9	3.6	5	2.2	5	2.4	16	2.3	16.5	86.3	18	·	·	·	2	·	·	3	18	14	11	3	3	·	–
VIII	2.2	2.6	·	·	2	2.5	1.5	2.0	3.6	2.8	11.5	6.8	2	5.0	8	2.4	10	2.9	4.8	19.0	15	·	·	·	5	1	1	2	8	13	10	1	1	·	–
IX	1.2	2.3	·	·	3	2.3	4	2.5	29.5	2.8	14.5	4.4	8	2.9	8	2.9	11	2.6	6.7	13.5	18	·	·	1	·	1	·	6	8	13	12	2	2	·	–
X	2.7	2.4	2	2.0	5	2.0	2	2.0	3.2	2.4	8	3.4	1	2.0	1	2.0	15	2.1	1.4	3.7	19	·	·	·	·	·	·	14	10	7	5	·	13	·	–
XI	2.9	2.8	2	2.0	3	3.0	1.0	2.4	2.3	2.6	·	·	1	4.0	·	·	2.2	2.0	5.1	8.3	22	·	10	16	·	·	·	1	23	19	14		19	14	–
XII	2.2	3.1	·	·	2	2.0	2.5	2.2	3.1	3.5	11.5	6.3	1	2.0	1	2.0	2.2	2.8	3.3	8.8	30	1.2	2.1	3.1	·	2	2	1	18	12	9	·	8	31	–
Rok	32.3	3.0	11	1.3	2.6	1.8	38.5	2.8	33.0	3.0	128.5	4.8	3.7	3.4	3.3	2.7	168	2.8	8.1.0	88.3	18. VII	3.2	8.9	148	9	1.7	1.1	4.1	188	186	140	1.6	8.4	150	–

Turbacz $\varphi = 49°33'$ $\lambda = 20°07'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA t										ŚREDNIA PREŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	–1.3	–7.6	4.6	19	–17.1	29	–5.1	–3.2	–5.0	–4.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.2	7.0	7.2
II	–	–	–	–	–4.1	–10.6	–0.5	28	–16.6	25	–8.6	–6.0	–7.7	–7.5	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.4	8.4	8.6
III	–	–	–	–	–3.3	–10.2	9.1	5	–17.7	17	–7.9	–5.2	–7.3	–6.9	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.3	7.7	7.8
IV	–	–	–	–	7.7	1.0	19.4	23	–6.1	7	3.4	6.0	3.5	4.1	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.3	5.2	5.8
V	–	–	–	–	8.3	0.3	17.3	8	–7.9	1	3.8	5.9	4.2	4.5	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.9	6.6	7.4
VI	–	–	–	–	11.6	4.1	22.4	16,23,24	–3.7	7	6.8	9.3	7.0	7.5	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.6	7.0	6.6
VII	–	–	–	–	14.4	5.8	25.0	27	0.9	1	9.0	12.4	9.2	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.0	6.4	6.3
VIII	–	–	–	–	17.8	8.4	25.6	15	3.7	20	11.9	15.4	12.0	12.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	4.5	3.9	4.6
IX	–	–	–	–	12.2	3.7	22.4	4, 5	–1.1	26, 27	6.4	10.4	6.8	7.6	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.5	4.2	5.1
X	–	–	–	–	10.5	3.1	18.4	3	–4.6	17	5.0	8.6	5.2	6.0	–	–	–	–	–	–	–	–	–	–	–	–	3.8	4.6	3.2	3.9
XI	–	–	–	–	5.0	–2.2	16.7	6	–8.7	18, 24	–0.3	3.4	0.5	1.0	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.0	7.9	7.6
XII	–	–	–	–	–4.5	–11.2	3.1	9	–25.1	22, 23	–9.1	–5.8	–8.2	–7.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.1	6.7	7.1
Rok	–	–	–	–	6.2	–1.3	25.6	15. VIII	–25.1	22.23. XII	1.3	4.3	1.7	2.2	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.5	6.2	6.5

Łącko $\varphi = 49°33'$ $\lambda = 20°26'$

I	–	–	–	–	3.6	–3.3	9.5	22	–15.0	31	–1.2	2.0	–0.1	0.2	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.1	7.0	6.7
II	–	–	–	–	1.0	–6.0	5.1	12	–13.6	1	–4.1	–0.8	–2.7	–2.6	–	–	–	–	–	–	–	–	–	–	–	–	9.4	7.8	8.2	8.5
III	–	–	–	–	2.7	–6.0	15.0	5	–16.6	21	–4.0	1.6	–1.9	–1.6	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.0	7.1	7.9
IV	–	–	–	–	15.1	4.2	25.8	23	–1.8	2	6.5	13.8	8.7	9.4	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.7	5.2	6.0
V	–	–	–	–	15.8	5.7	24.0	8	–2.4	2	8.6	13.6	9.6	10.4	–	–	–	–	–	–	–	–	–	–	–	–	7.3	8.7	6.0	7.3
VI	–	–	–	–	18.1	8.0	28.2	23	2.4	7	11.1	16.3	12.3	13.0	–	–	–	–	–	–	–	–	–	–	–	–	6.1	7.9	7.1	7.0
VII	–	–	–	–	21.2	9.0	30.3	27	4.1	5	12.4	19.6	13.5	14.8	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.8	5.6	6.1
VIII	–	–	–	–	23.6	10.6	30.7	15	4.3	31	13.6	22.3	15.3	16.6	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.6	4.1	4.8
IX	–	–	–	–	18.5	5.6	28.3	4	–0.1	27	8.4	17.0	10.3	11.5	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.5	4.3	5.2
X	–	–	–	–	14.6	2.0	20.8	3, 4	–2.3	25, 31	3.8	13.4	5.5	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.1	3.7	3.1	4.3
XI	–	–	–	–	8.5	1.2	18.6	8	–2.8	24	2.6	7.3	4.4	4.7	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.7	8.3	7.9
XII	–	–	–	–	–1.3	–8.7	6.9	13	–20.4	29	–6.1	–2.8	–5.2	–4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.5	7.7	7.2
Rok	–	–	–	–	11.8	1.9	30.7	15. VIII	–20.4	29. XII	4.3	10.3	5.8	6.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.8	6.1	6.6

Stary Sącz $\varphi = 49°33'$ $\lambda = 20°39'$

I	–	–	–	–	2.6	–2.8	8.2	20	–15.2	31	–1.1	1.7	–0.7	–0.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	1.2	–5.7	9.4	13	–16.6	25	–3.5	–0.6	–2.0	–2.0	–	–	–	–	–	–	–	–	–	–	–	–	9.2	7.2	7.6	8.0
III	–	–	–	–	2.5	–5.2	15.8	5	–16.3	20	–3.3	1.6	–1.1	–1.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.0	5.8	6.9
IV	–	–	–	–	15.5	4.7	26.8	22	–0.7	30	7.7	14.2	8.9	9.9	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.2	4.2	5.4
V	–	–	–	–	15.8	6.2	23.1	8	–1.6	2	9.6	14.3	9.6	10.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	8.2	5.7	7.0
VI	–	–	–	–	18.5	8.4	28.7	16, 23	1.9	7	11.4	17.0	12.4	13.3	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.5	6.0	6.6
VII	–	–	–	–	21.2	10.0	30.2	27	4.6	30	13.6	19.6	13.8	15.2	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.5	5.4	5.8
VIII	–	–	–	–	24.1	10.9	31.3	15	4.2	31	14.5	22.7	15.3	17.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	19.0	6.6	28.6	5	0.4	27	8.8	17.6	11.4	12.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	14.4	2.2	21.0	3	–3.5	25	4.4	13.6	6.2	7.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	8.4	2.9	17.8	1	–2.2	24	4.1	7.4	4.9	5.3	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.8	7.6	7.5
XII	–	–	–	–	–1.8	–8.4	5.2	16	–21.1	21	–5.9	–3.2	–5.3	–4.9	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.5	7.1	7.1
Rok	–	–	–	–	11.8	2.5	31.3	15. VIII	–21.1	21. XII	5.0	10.5	6.1	6.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Rymanów-Zdrój $\varphi = 49°33'$ $\lambda = 21°51'$

I	–	–	–	–	0.9	–4.0	6.3	23	–14.4	31	–2.4	–0.4	–1.9	–1.7	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.2	7.0	6.5
II	–	–	–	–	–0.9	–7.3	3.6	20	–22.4	25	–5.0	–2.3	–3.7	–3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.3	8.3	8.2
III	–	–	–	–	1.3	–5.7	12.5	5	–17.3	20	–3.0	–0.1	–2.6	–2.1	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.4	7.4	7.7
IV	–	–	–	–	15.8	3.3	25.4	22, 23	–3.1	30	7.8	13.8	6.6	8.7	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.1	4.3	4.8
V	–	–	–	–	16.0	5.5	25.9	14	–3.4	2	10.5	13.8	9.1	10.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	7.2	6.6	6.6
VI	–	–	–	–	17.9	7.9	27.4	23	2.1	7	13.0	16.0	11.4	13.0	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.2	5.7	5.9
VII	–	–	–	–	20.1	9.4	31.4	27	4.4	30	14.3	18.3	12.9	14.6	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.6	4.8	5.2
VIII	–	–	–	–	22.9	10.4	(30.6)	7	3.3	31	14.6	21.0	14.4	16.1	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.6	3.6	4.8
IX	–	–	–	–	17.1	6.7	26.5	5	–0.2	27	8.8	15.7	10.4	11.3	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.6	4.9	4.9
X	–	–	–	–	13.2	1.6	19.6	3	–5.2	16	5.4	12.1	4.4	6.6	–	–	–	–	–	–	–	–	–	–	–	–	5.7	3.6	2.4	3.9
XI	–	–	–	–	8.0	1.5	16.6	6	–4.4	28	3.4	6.8	3.7	4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.4	6.6	7.4
XII	–	–	–	–	–2.6	–7.7	5.5	14	–15.9	23	–5.4	–4.6	–5.5	–5.2	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.9	7.7	8.2
Rok	–	–	–	–	10.8	1.8	31.4	27. VII	–22.4	25. II	5.2	9.2	4.9	6.0	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.3	6.8	6.2

Turbacz $H_s = 1308\,m$ $h_w = 18\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU (ⁿD, ᵛmD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◉	●	Opad R > 0.1	R > 1.0	R > 10.0	≡	⊞	R/FO
I	8	8.2	1.5	13.3	1	14.0	8.5	5.6	8	5.6	13.5	7.7	28.5	7.4	14	5.8	10	6.3	162	49.4	28	6	18	31	·	13	6	3	17	15	14	5	20	31	–
II	12	8.0	2	7.5	1.5	5.0	10.5	7.1	5.5	10.5	4.5	7.3	8.5	6.1	31.5	8.8	8	7.3	152	22.8	14	13	28	28	·	15	2	·	18	22	15	5	19	28	–
III	11.5	5.2	3	2.0	2.5	7.2	10.5	3.5	10	8.0	6.5	5.3	13	6.4	24	6.5	12	5.1	135	38.0	16	17	22	29	·	6	3	2	19	22	16	5	23	31	–
IV	13	4.2	6.5	2.8	6	2.0	10.5	4.6	14	7.0	7.5	2.9	7.5	3.5	8	6.1	17	3.6	108	33.2	6	·	3	18	·	4	1	4	11	13	8	5	15	24	–
V	16.5	2.0	1.5	2.3	2	2.0	3	2.0	14	2.2	4.5	1.6	12	3.3	21.5	2.6	18	1.9	160	17.1	21	·	2	14	·	·	·	·	14	24	24	6	22	6	–
VI	15	3.6	1	3.0	·	·	1	2.0	1	2.0	3.5	2.9	14.5	2.7	11	3.5	43	1.7	210	60.0	4	·	1	10	·	1	·	3	12	14	13	5	16	10	–
VII	15	2.4	2.5	1.6	·	·	0.5	2.0	4.5	1.6	3	2.0	22	1.9	10.5	2.0	35	1.2	215	77.8	18	·	·	·	·	·	·	4	7	17	15	4	16	·	–
VIII	5	2.2	·	·	2	6.0	·	·	7	8.3	7.5	1.7	15.5	2.4	7	4.4	49	1.7	57	16.8	5	·	·	·	1	4	1	6	4	12	12	1	10	·	–
IX	5.5	2.0	0.5	2.0	1	4.0	3.5	4.0	9	5.1	14	6.4	15.5	3.0	10	2.5	31	2.6	73	12.9	17	·	·	4	·	8	·	6	8	13	13	3	15	·	–
X	14.5	2.8	1.5	9.3	3	5.0	2.5	2.6	2.5	3.0	4	3.0	9.5	2.4	12.5	2.8	43	1.6	24	8.5	19	·	·	7	·	2	·	16	7	6	6	·	12	·	–
XI	15	3.5	1	2.0	2	2.5	6	6.3	12.5	6.7	7.5	2.7	5	2.4	9	6.7	32	3.0	107	18.2	22	·	10	21	·	5	3	2	16	17	13	4	19	14	–
XII	24	7.3	0.5	8.0	0.5	8.0	3	3.7	7	6.9	4	10.5	8	6.2	8	4.6	38	4.0	69	20.2	14	14	25	31	·	7	3	2	15	15	13	2	20	31	–
Rok	155	4.3	21.5	4.5	21.5	4.6	59.5	3.6	95	5.6	80	4.5	159.5	4.0	167	4.7	336	3.3	1472	77.8	18.VII	50	109	193	1	65	19	48	148	190	162	45	207	175	–

Łącko $H_s = 360\,m$ $h_w = 16{,}0\,m$ I–VIII, $h_w = 17{,}6\,m$ IX–XII

I	1	4.0	2	1.0	4	1.2	·	·	11	1.8	17.5	3.9	43.5	2.3	4	1.6	10	2.2	19	5.9	27	1	4	25	·	·	·	2	14	8	7	·	1	17	–
II	7	1.4	8	1.1	4	1.0	·	·	4	2.2	10	4.4	30.5	3.8	9.5	6.3	11	2.9	41	9.3	12	5	9	26	·	4	1	·	19	17	11	·	10	27	–
III	8	2.1	13	2.7	11.5	1.7	3	1.0	10	3.0	4	1.9	20.5	2.4	12	2.2	11	2.0	39	10.2	16	5	11	28	·	·	·	1	18	14	9	1	7	23	–
IV	9	1.4	6.5	2.0	5	2.0	1	4.0	14	4.2	8	2.9	32.5	2.5	6	1.9	8	2.4	65	30.3	6	·	·	5	3	2	·	6	11	12	11	1	4	·	–
V	6	1.4	6.5	1.3	12	1.6	2	1.2	9	1.7	9	3.5	30	2.4	9.5	1.7	9	1.9	105	23.2	20	·	·	2	·	·	·	1	10	18	15	3	3	·	–
VI	15.5	1.6	7.5	1.3	7	1.4	0.5	1.0	3	1.3	8.5	1.5	31.5	2.0	8.5	2.2	8	1.6	213	39.1	4	·	·	·	6	·	·	2	12	19	14	7	3	·	–
VII	7.5	1.1	8.5	1.4	10	1.3	0.5	1.0	6	1.3	13	1.8	29	2.1	6.5	1.6	12	1.5	149	55.4	18	·	·	·	6	·	·	3	8	14	11	4	3	·	–
VIII	3.5	1.6	8	1.6	6.5	1.5	·	·	6	2.2	12	2.0	31	2.0	12	2.2	14	1.6	50	16.4	16	·	·	·	11	·	·	4	2	10	7	2	3	·	–
IX	6	2.0	2.5	1.8	4	1.1	2	1.8	6	1.4	18.5	2.4	29.5	2.4	7.5	1.9	14	1.8	45	16.9	18	·	·	1	6	·	·	7	5	8	8	1	9	·	–
X	5	1.7	2	1.2	8.5	1.9	4	1.8	6	1.3	21	1.3	14.5	1.8	2	1.0	29	1.1	3	1.9	30	·	·	11	·	·	·	8	5	3	1	·	15	·	–
XI	1.5	2.7	3.5	2.0	20	2.0	3	1.0	18	2.1	5.5	1.7	10.5	1.8	1	1.0	27	1.3	85	13.9	14	·	1	10	·	·	·	3	19	14	11	3	12	9	–
XII	8	1.6	4.5	1.4	13.5	1.1	1.5	1.0	8.5	3.4	14.5	2.2	31.5	2.0	1	1.0	10	1.7	41	14.9	30	13	15	30	·	1	·	2	14	13	7	1	5	31	–
Rok	78	1.9	73.5	1.6	106	1.5	17.5	1.2	101.5	2.2	141.5	2.5	334.5	2.3	79.5	2.0	163	1.8	855	55.4	18.VII	24	40	138	32	7	1	39	137	150	112	23	75	107	–

Stary Sącz $H_s = 320\,m$ $h_w = 22\,m$

I	3.5	1.6	2	2.0	·	·	·	·	46	11.0	0.5	1.0	4.5	4.3	25	1.8	34	5.8	17	4.4	27	1	5	23	·	15	9	–	–	11	9	·	1	10?	·
II	7.5	1.7	0.5	5.0	·	·	·	·	15	7.3	1	2.0	7	4.4	14	6.3	39	2.9	24	6.0	19	7	9	25	·	7	1	·	17	15	8	·	2	27	·
III	6	3.4	6	2.6	·	·	·	·	29	8.0	·	·	1	3.5	5	3.1	46	3.1	45	8.4	15, 16	5	10	25	·	7	3	3	13	17	9	·	3	22	·
IV	4	3.9	3.5	2.4	·	·	·	·	20.5	8.7	0.5	1.0	4	2.8	5.5	3.8	52	2.6	60	26.8	6	·	·	3	4	5	3	9	9	12	8	2	2	·	1
V	4	2.8	1	1.0	·	·	1	5.0	13	3.9	3.5	7.4	3	5.7	4.5	4.9	63	1.4	107	22.2	20	·	·	1	·	2	·	2	11	25	18	4	2	·	5
VI	8.5	2.1	4.5	1.6	·	·	1.5	2.3	7.5	2.2	·	·	5.5	3.5	8.5	4.0	54	1.1	136	25.6	1	·	·	·	6	·	·	5	12	18	13	4	·	·	5
VII	4	1.2	1.5	1.0	·	·	1	1.5	13	1.7	1	1.5	5.5	2.4	9	1.5	58	0.7	115	39.9	18	·	·	·	5	·	·	6	7	14	12	3	·	·	8
VIII	5.5	1.0	0.5	1.0	0.5	2.0	1	3.5	12.5	1.7	2	1.8	6.5	1.9	6.5	1.5	58	0.6	34	12.4	16	·	·	·	11	·	·	–	–	9	6	1	3	·	5
IX	4	1.9	1	4.0	·	·	·	·	16	3.2	6	1.2	4.5	2.6	4.5	2.8	54	1.0	42	17.0	18	·	·	·	5	2	·	–	–	9	7	1	4	·	1
X	4.5	1.2	1.5	1.0	·	·	2	2.0	10.5	1.8	0.5	1.0	1	2.0	4	1.2	69	0.4	5	1.9	30	·	·	10	·	·	·	–	–	4	3	·	11	·	·
XI	2	1.5	1	1.0	·	·	2.5	2.4	28.5	7.1	1	3.0	·	·	·	·	55	2.4	96	19.2	15	·	1	7	·	6	1	3	17	15	10	5	6	9	·
XII	9	2.9	3	2.3	·	·	4	13.9	25.5	9.4	1	3.5	1.5	5.7	4	1.5	45	3.7	47	17.5	30	10	17	31	·	8	4	3	14	16	7	2	1	31	·
Rok	62.5	2.1	26	2.1	0.5	0.2	13	2.6	237	5.5	17	2.0	44	3.2	68	2.7	627	2.1	728	39.9	18.VII	23	42	125	31	52	21	–	–	165	110	22	35	99?	25

Rymanów-Zdrój $H_s = 360\,m$ $h_w = 18\,m$

I	14	2.4	2.5	2.6	·	·	3.5	1.9	34.5	5.3	28	4.7	·	·	25	1.0	8	4.0	35	6.6	13	2	10	26	·	9	2	3	12	10	9	·	–	–	·
II	30.5	2.0	4.5	1.4	·	·	3	1.0	14.5	6.5	9.5	6.2	·	·	5	1.1	17	2.7	66	12.5	13	7	15	28	·	2	2	·	17	17	12	2	–	28	·
III	28	3.0	6.5	3.9	2.5	1.2	·	·	17.5	6.0	13.5	4.7	·	·	6	2.2	19	3.0	39?	10.4	17	8	15	26	·	6	·	1	18	15	7	1	–	29	·
IV	8	2.9	11	2.4	·	·	9	1.1	17.5	4.3	14.5	4.3	0.5	3.0	1.5	1.7	28	2.3	33	14.5	27	·	·	7	2	1	·	8	7	8	7	1	–	·	1
V	17	1.9	5	1.3	1	1.0	5.5	1.7	15.5	3.0	14	3.1	·	·	4	1.2	31	1.6	101	15.9	20	·	·	6	1	·	·	1	8	23	20	1	–	·	10
VI	36	2.1	1.5	1.0	2	4.0	6	2.0	16	1.6	5	1.6	·	·	1.5	2.7	22	1.5	156	32.5	4, 5	·	·	·	5	·	·	5	8	18	16	5	–	·	5
VII	29	1.4	1	1.0	3	2.7	8.5	1.7	14.5	2.1	15.5	2.4	1.5	1.0	2	3.0	18	1.5	107	30.5	19	·	·	·	3	·	·	2	5	17	13	3	–	·	3
VIII	10	1.2	7.5	1.6	1.5	2.3	6	1.4	15	2.7	14.5	2.4	1.5	1.7	9	1.1	28	1.3	78	15.8	5	·	·	·	8	·	·	5	5	12	9	5	1	·	5
IX	5	1.5	10.5	2.1	·	·	7.5	1.1	20.5	3.2	15	3.3	·	·	2.5	1.0	29	1.7	81	19.5	7	·	·	1	1	·	·	7	4	16	12	1	1	·	3
X	14.5	2.5	18	1.5	3	1.2	3.5	1.0	17.5	2.5	12	2.5	·	·	7.5	2.9	17	1.8	5	1.2	14	·	·	13	·	·	·	12	5	6	2	·	7	·	·
XI	6	1.8	6	1.9	·	·	1.5	1.7	27.5	3.0	21	3.5	1	2.0	4	1.2	23	2.1	95	19.2	15	·	1	11	·	1	·	1	17	15	12	4	1	12	·
XII	15	3.4	12.5	2.4	1.5	2.3	4	1.2	18.5	4.7	23.5	4.9	·	·	1	2.5	17	3.1	43	14.3	14	9	20	31	·	2	·	1	19	16	9	2	·	31	·
Rok	213	2.2	86.5	1.9	14.5	1.2	58	1.3	229	3.7	186	3.6	4.5	0.6	46.5	1.8	257	2.2	839?	32.5	4, 5.VI	26	61	149	20	21	4	46	125	173	128	25	–	–	27

Sieniawa $\varphi = 49°32'$ $\lambda = 19°55'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	13	-5.3	7.5	22	-18.4	31	-3.1	-0.3	-2.4	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	5.8	6.7	6.8
II	–	–	–	–	-0.8	-8.3	2.6	7	-22.0	25	-6.2	-2.6	-4.8	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	9.2	7.8	7.9	8.3
III	–	–	–	–	1.2	-8.2	12.4	5	-18.1	26	-5.9	-0.1	-4.4	-3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.3	7.4	7.7
IV	–	–	–	–	12.5	1.1	24.8	23	-3.6	2	4.6	11.0	3.9	5.8	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.7	5.2	6.1
V	–	–	–	–	13.4	4.0	20.6	8	-2.4	3	7.5	11.5	7.3	8.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	8.0	6.9	7.4
VI	–	–	–	–	16.0	6.0	27.1	16	0.0	5	10.5	14.5	9.7	11.1	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.6	6.9	7.0
VII	–	–	–	–	18.9	7.7	28.5	27	2.0	5	12.3	17.8	11.7	13.4	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.8	5.6	6.4
VIII	–	–	–	–	21.9	8.8	29.2	7, 15	2.3	31	12.9	20.7	12.9	14.8	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.9	4.4	5.3
IX	–	–	–	–	17.0	4.2	26.4	4	-2.0	25	7.2	15.0	8.1	9.6	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.6	3.5	5.1
X	–	–	–	–	13.8	1.3	21.6	3	-3.7	17	2.9	13.0	4.1	6.0	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.3	3.1	4.2
XI	–	–	–	–	6.4	-0.3	16.9	8	-6.8	17	1.4	5.1	1.9	2.6	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.6	8.1	8.1
XII	–	–	–	–	-3.1	-11.2	3.8	13	-24.5	22	-7.8	-4.5	-7.9	-7.0	–	–	–	–	–	–	–	–	–	–	–	–	8.1	6.9	6.9	7.3
Rok	–	–	–	–	9.9	0.0	29.2	7.15.VIII	-24.5	22, XII	3.0	8.4	3.3	4.5	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.7	6.0	6.6

Zwardoń $\varphi = 49°30'$ $\lambda = 18°59'$

I	–	–	–	–	0.1	-5.4	5.9	1	-17.2	31	-3.6	-1.3	-2.8	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.0	7.5	7.4
II	–	–	–	–	-1.5	-8.1	4.1	13	-18.5	1	-6.2	-3.4	-4.6	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.7	8.7	8.5
III	–	–	–	–	0.4	-7.2	10.9	5	-15.1	25	-5.6	-1.3	-3.5	-3.5	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.9	8.1	7.9
IV	–	–	–	–	12.2	2.4	24.5	25	-1.5	3, 6	4.6	10.2	6.1	6.8	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.0	5.1	5.9
V	–	–	–	–	12.7	4.6	19.5	19	-1.6	2, 5	6.8	10.5	7.7	8.2	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.4	6.5	7.3
VI	–	–	–	–	16.3	6.2	26.7	24	0.6	6	9.9	14.2	10.5	11.3	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.5	5.8	6.6
VII	–	–	–	–	18.5	7.9	27.9	27	2.4	5	11.4	16.9	12.2	13.2	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.3	5.2	5.6
VIII	–	–	–	–	21.8	9.1	28.7	15	2.6	31	12.5	19.7	13.8	15.0	–	–	–	–	–	–	–	–	–	–	–	–	4.4	5.1	3.5	4.3
IX	–	–	–	–	16.0	4.5	25.5	4	-1.2	25	6.5	13.8	9.0	9.6	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.5	3.4	4.6
X	–	–	–	–	13.1	2.3	21.5	4	-3.0	17	3.5	12.0	5.3	6.5	–	–	–	–	–	–	–	–	–	–	–	–	4.7	4.6	3.4	4.2
XI	–	–	–	–	5.3	0.1	16.7	7	-6.5	22	1.4	4.1	1.8	2.3	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.0	7.3	7.9
XII	–	–	–	–	-3.7	-9.9	5.5	13	-22.4	23	-7.8	-5.0	-7.0	-6.7	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.8	8.4	7.8
Rok	–	–	–	–	9.3	0.5	28.7	15.VIII	-22.4	23, XII	2.8	7.5	4.0	4.6	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.8	6.1	6.5

Nowy Targ $\varphi = 49°29'$ $\lambda = 20°02'$

I	–	–	–	–	0.1	-8.2	5.6	22	-21.7	31	-5.8	-1.1	-4.2	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.0	6.3	6.4
II	–	–	–	–	-1.0	-9.9	4.4	12	-24.4	25	-7.2	-2.8	-5.2	-5.1	3.3	4.0	3.9	3.7	8.7	7.8	8.7	8.4	0.4	1.0	0.6	0.7	9.2	7.6	8.5	8.4
III	–	–	–	–	1.2	-8.4	11.2	5	-20.6	9	-6.7	-0.1	-3.9	-3.6	3.5	4.5	4.1	4.0	8.6	7.1	8.5	8.1	0.5	1.8	0.7	1.0	7.9	7.3	7.6	7.6
IV	–	–	–	–	13.1	1.1	25.4	23	-5.7	3	3.4	11.9	6.2	6.9	7.2	7.8	7.9	7.6	9.1	6.1	8.3	7.8	0.8	7.5	2.0	3.4	5.6	6.2	5.2	5.7
V	–	–	–	–	13.8	4.3	21.1	8	-3.0	2	6.7	11.9	8.3	8.8	9.1	10.1	9.8	9.7	9.0	7.2	8.8	8.8	1.1	4.3	1.4	2.3	7.2	8.0	6.7	7.3
VI	–	–	–	–	16.9	5.7	28.0	23	-0.3	9	9.5	15.4	10.9	11.7	10.9	11.7	11.8	11.5	8.9	6.7	8.7	8.1	1.4	7.5	2.0	3.6	6.0	7.0	6.2	6.4
VII	–	–	–	–	19.9	7.7	29.2	27	1.4	5	10.9	18.2	12.9	13.7	12.1	12.7	12.9	12.6	9.2	6.2	8.6	8.0	1.1	8.9	2.2	4.1	6.1	6.6	5.5	6.1
VIII	–	–	–	–	22.5	8.8	30.5	15	1.6	31	11.4	21.3	14.3	15.3	12.9	14.5	13.8	13.7	9.5	5.9	8.5	8.0	0.7	11.5	2.7	5.0	5.2	5.8	4.6	5.2
IX	–	–	–	–	17.7	3.5	27.2	4	-1.9	25	5.7	15.8	8.7	9.7	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.1	3.4	4.9
X	–	–	–	–	14.8	-0.1	22.6	3	-5.7	27	0.8	13.2	4.5	5.8	6.4	9.6	8.0	8.0	9.6	6.4	9.3	8.4	0.3	6.3	0.6	2.4	5.9	3.1	2.2	3.7
XI	–	–	–	–	6.7	-0.3	16.2	8	-7.1	18	1.2	5.3	2.6	2.9	6.5	7.5	7.0	7.0	9.4	8.3	9.2	9.0	0.5	2.0	0.7	1.1	8.4	8.1	7.6	8.0
XII	–	–	–	–	-4.1	-13.1	1.8	17	-27.1	29	-9.4	-5.2	-8.7	-8.0	3.1	3.5	3.1	3.2	8.9	7.9	8.7	8.5	0.3	0.9	0.5	0.6	8.1	7.0	7.8	7.6
Rok	–	–	–	–	10.1	-0.7	30.5	15.VIII	-27.1	29, XII	1.7	8.6	3.9	4.5	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.5	6.0	6.5

Jabłonka $\varphi = 49°28'$ $\lambda = 19°43'$

I	–	–	–	–	0.3	–	6.7	2.2	–	–	-3.8	-1.2	-3.3	-2.9	4.5	4.8	4.6	4.6	9.2	8.3	9.0	8.8	0.4	1.0	0.5	0.6	7.6	6.5	6.3	6.8
II	–	–	–	–	-1.6	-9.9	2.5	12	-26.0	25	-7.2	-3.7	-5.5	-5.5	3.5	4.1	4.0	3.9	9.2	8.5	9.1	8.9	0.3	0.7	0.4	0.5	9.7	8.7	9.2	9.0
III	–	–	–	–	0.4	-9.4	10.5	5	-20.6	27	-7.3	-1.3	-4.9	-4.6	3.7	4.6	4.2	4.2	9.2	7.9	9.2	8.8	0.3	1.2	0.4	0.6	8.8	7.7	8.1	8.2
IV	–	–	–	–	12.4	1.4	25.2	23	-4.0	3	4.1	11.0	5.7	6.6	7.5	9.8	8.3	8.2	9.1	6.9	8.9	8.3	0.9	5.8	1.2	2.6	6.8	6.8	5.3	6.3
V	–	–	–	–	13.3	3.8	19.8	19	-5.0	3	6.8	11.4	8.0	8.6	9.4	10.1	9.8	9.8	9.3	7.5	8.9	8.6	0.8	3.9	1.3	2.0	8.0	8.1	6.6	7.6
VI	–	–	–	–	16.7	5.5	27.9	23	-0.6	9	9.4	14.8	10.6	11.4	10.9	11.6	11.7	11.4	8.9	6.9	8.9	8.2	1.4	6.7	1.7	3.3	7.5	7.9	6.7	7.4
VII	–	–	–	–	19.1	7.2	28.9	27	0.8	30	11.1	17.8	12.4	13.4	12.1	12.5	12.7	12.4	9.0	6.1	8.8	8.0	1.3	8.6	1.9	3.9	6.7	6.9	5.6	6.4
VIII	–	–	–	–	22.3	7.8	29.2	15	0.5	31	11.4	20.4	13.9	14.9	12.7	13.8	13.6	13.4	9.3	5.8	8.5	7.9	1.0	10.8	2.5	4.8	6.3	6.1	4.4	5.6
IX	–	–	–	–	16.6	3.2	26.0	4	-1.6	25	6.2	14.5	8.4	9.4	9.0	10.3	9.9	9.7	9.2	6.3	8.9	8.1	0.9	6.8	1.6	3.1	8.2	5.3	3.3	5.6
X	–	–	–	–	13.3	0.0	21.5	3	-5.2	24	1.5	11.5	3.9	5.2	6.8	9.2	7.8	7.9	9.7	6.8	9.4	8.6	0.3	4.9	0.5	1.9	9.3	4.6	2.7	5.5
XI	–	–	–	–	5.7	-1.0	15.5	7	-9.7	18	0.4	4.6	1.4	2.0	6.3	7.5	6.8	6.9	9.7	8.7	9.7	9.4	0.2	1.5	0.2	0.6	8.8	8.1	8.4	8.4
XII	–	–	–	–	-4.5	-13.1	1.6	13	-27.3	21	-9.2	-5.9	-9.0	-8.3	3.2	3.6	3.1	3.3	9.1	8.6	8.9	8.9	0.3	0.6	0.4	0.4	8.7	7.7	6.9	7.8
Rok	–	–	–	–	9.5	–	29.2	15.VIII	–	–	2.0	7.8	3.5	4.2	7.5	8.4	8.0	8.0	9.2	7.4	9.0	8.5	0.7	4.4	1.0	2.0	8.0	7.0	6.1	7.0

Sieniawa $H_s = 578\,m$ $h_w = 16\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU nD, vmD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	◔	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	·	·	3	1.3	10	1.5	18	1.4	6	1.7	28	1.9	15	1.7	3	1.3	10	1.5	49	16.0	27	6	8	25	·	·	·	2	13	18	9	1	·	31	–
II	1	1.0	6	1.0	3	1.3	6	1.2	1.5	1.0	16.5	4.7	21	3.1	16	1.3	13	2.2	87	19.6	12	8	14	28	·	1	1	·	18	22	15	2	·	28	–
III	5	1.0	15	1.6	7	1.1	11.5	1.3	6.5	2.1	19	1.4	20	1.6	2	1.5	7	1.4	74	17.8	16	12	15	27	·	·	·	2	18	16	12	2	·	31	–
IV	2	1.0	18	1.0	6	1.3	12	1.8	6	1.2	16	1.9	10	2.2	14	1.4	6	1.4	101	54.2	6	·	·	10	·	·	·	6	11	15	11	2	5	9	–
V	1	1.0	6	1.3	6	1.0	7	1.1	6	1.3	22	1.9	24	1.3	13	1.1	8	1.3	125	18.6	20	·	·	4	·	·	·	1	16	24	21	4	4	·	–
VI	5	1.0	7	1.0	3	1.0	4	1.0	1	2.0	11	1.4	36	1.4	16	1.2	7	1.2	181	40.4	1	·	·	·	3	·	·	4	16	16	13	5	·	·	–
VII	·	·	5	1.4	2	2.0	6	1.3	5	1.2	22	1.6	26	1.3	16	1.6	11	1.3	152	85.8	18	·	·	·	4	·	·	3	12	14	9	2	3	·	–
VIII	4	1.0	5	1.2	2	1.0	6	1.3	5	1.6	16	1.6	26	1.7	14	1.1	15	1.2	54	20.0	16	·	·	·	8	·	·	4	3	13	8	1	·	·	–
IX	1	1.0	2	1.0	5	1.6	4	1.0	8	1.8	24	1.7	24	1.5	9	1.2	13	1.3	69	14.0	18	·	·	4	1	·	·	7	8	12	11	3	5	·	–
X	7	1.3	10	1.0	7	1.0	6.5	1.0	9	1.0	15.5	1.1	21	1.2	2	1.0	15	0.9	12	5.8	6	·	·	12	·	·	·	13	7	8	3	·	7	·	–
XI	5	1.4	5	1.0	4	2.0	24.5	1.2	2.5	1.4	13	1.3	20	1.1	4	1.0	12	1.1	81	15.0	15	·	5	17	·	·	·	1	20	17	13	3	12	15	–
XII	8	1.6	14	1.2	16	1.1	6	1.3	2	2.0	18	2.8	3	1.3	11	1.2	15	1.4	53	12.5	30	15	19	31	·	·	·	1	17	16	11	2	1	31	–
Rok	39	0.9	96	1.2	71	1.3	111.5	1.2	58.5	1.5	221	1.9	246	1.6	120	1.2	132	1.4	1038	85.8	18.VII	41	61	158	16	1	1	44	159	191	136	27	37	145	–

Zwardoń $H_s = 690\,m$ $h_w = 16\,m$

I	9	3.5	6.5	4.9	1	2.0	1	2.0	29.5	3.9	27	3.4	13	3.4	4	4.0	2	3.6	79	21.7	28	5	14	26	·	·	·	4	18	16	13	3	4	31	·
II	8.5	4.2	13.5	2.6	5.5	2.4	2.5	2.0	12	5.0	16.5	3.4	7.5	4.9	16	3.8	2	3.6	111	15.6	5	8	17	28	·	1	·	2	21	19	14	4	3	28	·
III	16	4.8	26	3.3	4.5	2.3	0.5	3.0	11.5	3.5	23	3.6	5.5	2.9	2	3.0	4	3.4	77	18.7	12	11	15	28	·	·	·	2	19	16	13	1	11	31	·
IV	9	2.9	19	3.1	3	2.7	6.5	2.5	12.5	4.0	14	3.8	9	2.9	13	2.8	4	3.0	102	29.6	6	·	·	5	·	·	·	8	12	16	14	4	11	13	·
V	13.5	3.0	9	2.6	3.5	2.3	3.5	3.1	19.5	3.5	23	3.4	9	2.6	10	3.1	2	3.0	202	34.1	20	·	·	4	·	·	·	2	14	27	21	7	17	·	5
VI	18.5	3.6	19	3.0	2	4.8	1.5	2.3	5	3.6	14.5	3.4	13.5	3.1	9	3.1	7	3.0	138	39.4	1	·	·	·	4	·	·	5	16	13	13	3	8	·	2
VII	15.5	3.0	8.5	2.7	·	·	·	·	13	3.0	23	3.1	8.5	2.7	15.5	2.6	9	2.6	88	32.4	18	·	·	·	3	·	·	6	9	16	14	2	14	·	4
VIII	2	3.5	3	2.7	5.5	2.2	3.5	2.0	10.5	3.7	23.5	3.2	22	2.5	9	2.4	14	2.4	71	25.4	15	·	·	·	7	·	·	6	3	12	11	3	8	·	5
IX	4.5	2.2	3.5	2.0	4	2.2	0.5	2.0	14	3.7	21.5	2.9	22	2.6	10	2.2	10	2.5	97	20.8	18	·	·	2	1	·	·	12	8	14	13	5	15	·	1
X	7.5	2.5	18	2.6	10	2.6	·	·	7	2.9	26.5	2.9	6	2.3	7	2.4	11	2.4	28	7.0	5	·	·	7	·	·	·	13	9	10	7	·	15	·	·
XI	6	3.2	21.5	2.3	4	2.4	16.5	2.6	14.5	3.4	17	2.8	2.5	2.2	6	2.5	2	2.7	111	20.1	20	·	9	17	·	·	·	3	21	18	18	2	12	11	·
XII	4.5	2.8	30.5	3.3	4	2.0	2	2.2	17.5	4.0	18	3.9	7	2.9	1.5	2.0	8	3.1	77	16.0	16	3	24	30	·	·	·	3	21	18	12	2	5	31	·
Rok	114.5	3.3	178	2.9	47	2.3	38	2.0	166.5	3.7	247.5	3.3	125.5	2.9	103	2.8	75	2.9	1181	39.4	1.VI	27	79	147	15	1	·	66	171	195	163	36	123	145	17

Nowy Targ $H_s = 600\,m$ $h_w = 21.5\,m$

I	1.5	1.0	10	1.0	10	1.4	3	1.0	3	1.3	3	6.7	31	2.6	15.5	2.0	16	1.8	60	21.6	27	13	12	30	·	1	·	2	11	15	9	2	3	31	–
II	4	2.0	5.5	1.0	5.5	1.0	·	·	1	2.0	5	4.5	29.5	4.9	17.5	2.8	16	2.8	79	12.8	19	15	16	28	·	4	·	·	20	20	15	2	3	28	–
III	6.5	1.2	20	1.5	15.5	1.6	·	·	1	1.0	2	1.0	22	2.4	14	1.7	12	1.5	63	15.6	16	11	14	28	·	·	·	2	17	16	11	1	2	31	–
IV	14.5	1.5	20	1.1	14	1.4	·	·	1	4.0	1	4.0	17	2.4	11.5	2.0	11	1.5	83	47.4	6	·	·	9	1	·	·	8	12	14	10	2	2	10	–
V	13	1.2	9.5	1.0	8	1.9	1	1.0	7.5	2.3	8.5	6.3	19.5	3.1	20	1.6	12	2.0	115	17.2	9	·	·	5	·	2	·	1	13	23	18	3	2	·	–
VI	13	1.3	4.5	1.0	9.5	1.2	1.5	1.7	1	1.0	6	3.1	22	2.3	21.5	1.9	11	1.6	153	43.0	4	·	·	1	5	·	·	6	13	14	10	5	2	·	–
VII	17.5	1.1	6.5	1.2	5.5	1.4	3	1.0	·	·	3.5	5.3	25	2.0	20	1.7	12	1.5	111	45.3	18	·	·	·	4	·	·	3	8	13	9	3	·	·	–
VIII	14.5	1.7	9.5	1.1	6.5	1.0	·	·	1	4.0	3	1.0	26	2.7	15.5	1.5	17	1.5	45	17.7	15	·	·	·	8	·	·	4	2	12	8	1	6	·	–
IX	12	1.2	10	1.1	6	1.5	·	·	·	·	3.5	3.0	27	2.1	18.5	1.6	13	1.5	57	12.7	23	·	·	6	4	1	1	6	5	12	12	2	8	·	–
X	15	1.3	8.5	1.0	6.5	1.6	·	·	2	1.0	1	1.0	6	1.5	10	1.7	44	0.7	10	3.1	6	·	·	15	·	·	·	11	5	7	5	·	20	·	–
XI	5	1.0	2.5	2.2	23	2.3	3.5	1.0	·	·	3.5	1.4	22.5	1.5	4	1.6	26	1.2	70	13.1	23	·	3	19	·	·	·	·	19	16	13	2	4	12	–
XII	6.5	1.5	2.5	1.0	17	1.7	2	1.0	2.5	1.0	5	2.5	23.5	1.7	8	1.7	26	1.2	44	10.7	14	17	24	31	·	·	·	1	18	15	12	2	5	31	–
Rok	123	1.3	109	1.2	127	1.5	14	0.6	14	1.5	45	3.3	271	2.4	176	1.8	216	1.6	890	47.4	6.IV	56	69	172	22	8	1	44	143	177	132	25	57	143	–

Jabłonka $H_s = 620\,m$ $h_w = 19.2\,m$

I	8	4.0	5	4.7	3	1.5	2	1.2	1.5	3.7	43	4.9	7	2.9	2.5	3.4	21	3.3	37	11.4	27	–	11	–	·	5	·	2	13	16	9	1	·	25	·
II	12.5	4.6	11	1.8	·	·	1	1.0	·	·	19.5	8.9	5.5	4.3	6.5	7.4	28	3.8	72	11.6	5	15	17	27	·	9	5	·	21	21	14	2	1	28	·
III	12	3.3	15	5.1	10	1.6	0.5	3.0	·	·	19.5	3.7	2	4.5	2	3.0	32	2.4	33	11.1	12	14	14	27	·	2	·	1	21	17	12	1	5	31	·
IV	12	3.0	7	2.2	2.5	1.6	1	3.0	4	3.0	17.5	5.1	1.5	3.0	8.5	3.1	36	2.1	78	41.8	6	·	·	8	1	·	·	7	11	16	11	1	3	2	1
V	11.5	2.0	9.5	2.2	0.5	1.0	1	1.0	4	3.5	27.5	4.7	3	2.3	5	1.4	31	2.2	140	22.3	9	·	·	5	·	3	1	1	15	26	20	4	2	1	7
VI	17.5	2.6	5	2.1	3.5	1.7	0.5	2.0	2	2.5	14	3.0	6.5	3.3	6	2.2	35	1.6	149	50.0	1	·	·	1	5	·	·	·	14	19	14	4	4	·	6
VII	7.5	2.8	5.5	2.0	1	2.0	·	·	0.5	5.0	24	2.8	6	3.0	6.5	1.9	42	1.4	68	27.5	18	·	·	·	4	·	·	2	9	18	11	2	4	·	7
VIII	2.5	1.4	6.5	1.6	1.5	1.3	·	·	2.5	6.4	21	4.5	9	3.1	3	3.2	47	1.8	45	23.5	15	·	·	·	8	2	·	3	8	15	8	1	11	·	5
IX	3	2.2	1.5	1.3	4.5	1.9	0.5	1.0	1.5	4.7	29.5	3.5	7	3.0	2.5	3.8	40	1.8	59	14.4	18	·	·	6	1	1	1	3	6	22	11	2	12	·	1
X	6	2.2	8.5	1.5	6.5	1.6	1.5	1.0	1	1.0	11.5	2.4	3.5	2.4	0.5	3.0	54	0.8	12	3.9	6	·	·	14	·	·	·	1	8	20	3	·	19	·	·
XI	6.5	4.1	11	2.8	8.5	1.8	0.5	2.0	1.5	1.3	9	3.2	1.5	1.7	1.5	1.7	50	1.2	86	15.2	22	·	5	19	·	·	·	1	21	21	15	4	6	13	·
XII	6	2.8	13	4.6	10	2.1	·	·	·	·	20	6.0	3	4.0	1	2.0	40	2.5	36	9.7	14	18	22	31	·	6	·	·	18	18	10	·	6	31	·
Rok	105	2.9	98.5	2.7	51.5	1.5	8.5	1.3	18.5	2.6	256	4.4	55.5	3.1	46.5	3.0	456	2.1	815	50.0	1.VI	–	69	–	19	28	7	21	165	229	138	22	73	131	27

Maniowy $\varphi = 49°28'$ $\lambda = 20°15'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T																											
											Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.3	-10.0	5.2	20	-21.0	6	-6.8	-2.3	-4.9	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	8.5	6.5	7.1	7.4
II	–	–	–	–	-0.4	-10.3	6.4	13	-24.5	25	-6.9	-2.6	-5.1	-4.9	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.4	8.8	8.9
III	–	–	–	–	1.1	-8.2	9.9	31	-19.9	9	-6.4	-0.1	-3.4	-3.3	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.3	8.0	8.6
IV	–	–	–	–	13.5	0.9	26.0	23	-7.1	2	3.5	11.8	6.2	6.9	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.5	5.9	7.0
V	–	–	–	–	14.6	4.4	22.2	19	-4.1	2	6.8	12.5	8.5	9.1	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.8	7.1	8.2
VI	–	–	–	–	17.3	5.9	28.3	24	0.4	5, 9	9.1	15.6	11.1	11.7	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.4	7.4	8.2
VII	–	–	–	–	19.9	7.8	28.6	26, 27	0.8	5	10.6	18.4	12.8	13.6	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.3	6.8	7.5
VIII	–	–	–	–	22.6	8.4	30.2	15	1.4	31	11.1	21.3	13.9	15.0	–	–	–	–	–	–	–	–	–	–	–	–	8.8	6.7	4.4	6.6
IX	–	–	–	–	17.6	3.7	27.0	4	-1.3	16	5.6	15.8	8.8	9.8	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.1	4.6	6.3
X	–	–	–	–	14.7	0.3	23.0	3, 4	-4.0	24	1.5	12.9	4.1	5.6	–	–	–	–	–	–	–	–	–	–	–	–	9.6	4.5	4.1	6.1
XI	–	–	–	–	7.4	0.5	16.4	8	-7.6	17, 18	2.1	6.3	3.4	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.1	7.6	8.1
XII	–	–	–	–	-4.2	-14.5	2.7	13	-28.2	29	-9.3	-6.3	-9.2	-8.5	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.1	7.5	8.2
Rok	–	–	–	–	10.3	-0.9	30.2	15 VIII	-28.2	29 XII	1.7	8.6	3.8	4.5	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.4	6.6	7.6

Przehyba $\varphi = 49°28'$ $\lambda = 20°34'$

I	–	–	–	–	-2.1	-6.3	4.2	19	-15.3	31	-4.8	-3.3	-4.8	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	-4.3	-9.1	1.2	13	-15.1	1	-8.0	-5.7	-6.9	-6.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	-3.2	-7.4	7.6	5	-14.7	17	-6.5	-4.2	-5.8	-5.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	8.5	3.5	19.3	23	-4.0	8	5.3	7.3	5.0	5.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	9.3	3.4	17.5	8	-6.1	1	5.4	7.7	5.3	5.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	11.1	5.3	22.2	16,23,24	-4.1	5, 7	7.1	9.9	7.5	8.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	14.5	7.9	24.2	27	3.8	1	9.8	13.4	10.3	11.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	17.7	10.6	24.6	15	4.4	31	12.5	16.3	13.2	13.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	12.5	5.5	21.4	4	0.3	23	7.3	11.1	7.5	8.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	9.7	4.1	17.7	11	-2.9	16	5.4	8.8	5.9	6.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	3.5	-1.0	12.3	2, 5	-7.4	24	0.4	2.3	0.6	1.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-5.0	-10.3	3.0	8	-22.9	23	-8.3	-6.8	-8.1	-7.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	6.0	0.5	24.6	15, VIII	-22.9	23 XII	2.1	4.7	2.5	3.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Lesko $\varphi = 49°28'$ $\lambda = 22°20'$

I	–	–	–	–	2.3	-3.0	9.3	22	-15.2	31	-1.2	0.9	-0.6	-0.4	4.8	4.8	4.7	4.8	8.3	7.2	7.9	7.8	1.0	2.0	1.4	1.5	7.0	7.5	6.9	7.1
II	–	–	–	–	-0.4	-6.9	3.1	28	-21.3	25	-5.2	-1.9	-3.0	-3.3	3.8	4.1	4.3	4.1	8.7	7.6	8.7	8.3	0.6	1.3	0.7	0.9	8.5	8.3	8.2	8.3
III	–	–	–	–	1.9	-5.2	16.1	5	-17.1	20	-3.4	0.6	-1.5	-1.4	4.5	4.6	4.8	4.6	8.6	7.0	8.3	8.0	0.8	2.2	1.1	1.4	8.7	8.2	7.1	8.0
IV	–	–	–	–	16.3	3.9	27.2	23	-3.5	2	6.3	14.3	9.7	10.0	7.8	8.4	8.0	8.1	8.2	5.5	6.8	6.8	2.0	9.4	4.6	5.3	5.9	6.1	4.5	5.5
V	–	–	–	–	16.3	6.4	25.8	28	-3.7	2	8.8	14.5	10.6	11.1	10.5	10.9	10.7	10.7	8.9	6.5	8.2	7.9	1.2	6.4	2.4	3.3	7.5	7.7	6.1	7.1
VI	–	–	–	–	18.0	8.4	28.1	24	1.8	7	11.1	16.2	12.8	13.2	12.2	12.6	12.7	12.5	8.9	6.7	8.3	8.0	1.6	7.5	2.8	4.0	6.3	7.4	6.5	6.7
VII	–	–	–	–	19.7	9.8	29.4	27	4.4	10	12.4	18.0	14.5	14.8	13.2	13.3	13.6	13.4	9.0	6.5	8.2	7.9	1.4	8.1	3.2	4.2	7.0	7.0	5.1	6.4
VIII	–	–	–	–	23.0	11.8	29.5	15	3.4	31	13.8	21.5	16.6	17.1	14.9	16.0	16.5	15.8	9.3	6.2	8.7	8.1	1.1	10.4	2.8	4.8	7.0	6.4	5.2	6.2
IX	–	–	–	–	18.0	6.6	27.3	5	0.4	27	8.8	16.4	11.7	12.2	10.0	11.2	11.1	10.8	8.8	6.1	8.1	7.7	1.8	8.3	3.1	4.4	5.5	5.5	4.6	5.2
X	–	–	–	–	14.4	2.3	21.2	4	-3.5	17, 22	3.4	13.3	6.8	7.6	7.5	9.5	8.9	8.6	9.4	6.3	8.8	8.2	0.7	6.3	1.2	2.7	5.6	4.2	2.5	4.1
XI	–	–	–	–	9.3	1.7	18.8	5, 8	-5.3	18	3.6	7.7	4.7	5.2	7.2	8.2	7.7	7.7	9.0	7.8	8.9	8.6	1.0	3.3	1.1	1.8	8.1	7.9	7.0	7.7
XII	–	–	–	–	-1.8	-7.6	7.5	14	-15.7	23	-5.2	-3.3	-4.6	-4.4	3.7	3.9	3.8	3.8	8.5	7.9	8.4	8.3	0.8	1.1	0.8	0.9	7.7	8.2	8.2	8.0
Rok	–	–	–	–	11.4	2.4	29.5	15, VIII	-21.3	25 II	4.4	9.8	6.5	6.8	8.3	9.0	8.9	8.7	8.8	6.8	8.3	8.0	1.2	5.5	2.1	2.9	7.1	7.0	6.0	6.7

Czarny Dunajec $\varphi = 49°27'$ $\lambda = 19°51'$

I	–	–	–	–	0.3	-6.5	6.1	11	-17.9	31	-4.1	-1.4	-3.3	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.0	6.9	7.3
II	–	–	–	–	-1.7	-8.9	2.8	12	-20.1	25	-7.1	-3.9	-5.0	-5.2	–	–	–	–	–	–	–	–	–	–	–	–	9.7	8.6	9.1	9.1
III	–	–	–	–	0.3	-8.2	10.8	5	-20.3	9	-6.8	-1.7	-4.4	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.7	8.2	8.7
IV	–	–	–	–	12.2	1.7	24.3	23	-2.8	7	4.0	10.7	6.1	6.7	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.6	5.9	6.8
V	–	–	–	–	12.9	3.9	20.4	19	-3.5	2	6.7	11.2	8.1	8.5	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.5	7.8	8.2
VI	–	–	–	–	16.3	6.2	27.9	24	0.2	5, 7	9.5	14.3	11.1	11.5	–	–	–	–	–	–	–	–	–	–	–	–	7.0	8.6	8.5	8.0
VII	–	–	–	–	19.0	8.1	28.6	27	1.3	5	11.4	12.5	12.9	13.7	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.4	7.4	7.1
VIII	–	–	–	–	22.0	8.7	29.9	15	3.0	31	12.0	20.4	14.8	15.5	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.9	5.7	5.9
IX	–	–	–	–	16.6	3.8	26.4	4	-2.4	10	5.9	14.9	9.4	9.9	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.9	4.2	5.4
X	–	–	–	–	13.2	0.2	21.0	3	-5.1	22, 26	1.5	12.0	5.4	6.1	–	–	–	–	–	–	–	–	–	–	–	–	6.4	4.4	4.5	5.1
XI	–	–	–	–	5.8	-0.7	15.5	5	-8.4	18	0.6	4.4	1.9	2.2	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.5	8.5	8.7
XII	–	–	–	–	-4.7	-11.8	2.1	12	-22.1	29	-9.1	-6.2	-8.7	-8.2	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.6	8.9	8.5
Rok	–	–	–	–	9.4	-0.3	29.9	15, VIII	-22.1	29, XII	2.0	7.7	4.0	4.4	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.5	7.1	7.4

Maniowy $H_s = 520\,m$ $h_w = 16{,}7\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU (n D, v m/s) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v>10	v>15	⊖	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	1	1.0	1.5	2.0	4.5	1.3	1	1.0	·	·	0.5	3.0	33	3.5	6.5	3.8	45	1.6	48	14.2	27	14	13	31	·	·	·	1	15	15	9	1	7	31	–
II	1.5	3.3	·	·	3	3.7	·	·	·	·	4	5.0	35.5	4.0	17	4.0	23	2.9	56	9.5	5	16	12	27	·	3	·	·	20	21	13	·	4	28	–
III	2	5.0	7.5	3.5	10.5	4.8	·	·	·	·	2.5	2.8	24.5	3.3	8	3.4	38	2.2	49	10.4	12	11	12	30	·	2	·	·	21	17	12	1	3	31	–
IV	3	4.2	7	3.2	12	3.4	2	7.0	·	·	3	2.2	31	2.6	6	3.6	26	2.2	68	37.0	6	·	·	10	1	1	·	1	12	13	8	1	6	8	–
V	4	2.8	2	1.8	13	2.3	·	·	·	·	2	2.8	31	3.7	10	2.8	31	2.1	112	14.8	9	·	·	6	·	2	1	·	17	26	18	2	6	·	–
VI	5.5	1.5	3	1.8	8.5	1.6	·	·	·	·	1.5	3.3	30	3.8	10.5	3.1	31	2.0	158	39.9	5	·	·	·	6	1	·	·	17	23	16	4	10	·	–
VII	3	3.0	5.5	2.2	7	1.3	·	·	·	·	1.5	3.0	26	2.8	10	2.8	40	1.5	136	65.0	18	·	·	·	4	·	·	·	16	24	11	4	9	·	–
VIII	7.5	2.8	2.5	3.2	3	1.3	1	1.0	·	·	1	4.0	27.5	2.9	6.5	3.5	44	1.5	54	12.4	5	·	·	·	8	·	·	1	6	18	8	2	17	·	–
IX	4	1.0	2	3.2	5	1.9	1	1.0	·	·	·	·	34.5	2.6	5.5	4.5	38	1.5	43	11.9	18	·	·	5	3	·	·	1	8	22	10	1	13	·	–
X	2	2.0	9	1.3	7	3.9	1	3.0	·	·	1	2.0	22.5	1.7	2.5	2.0	48	1.0	9	1.4	30	·	·	18	·	1	·	1	7	24	3	·	23	·	–
XI	·	·	6.5	1.8	21.5	6.7	3	6.5	·	·	4.5	3.7	23	1.8	1.5	5.0	30	2.7	76	14.0	15	·	3	16	·	4	·	1	20	17	11	3	5	11	–
XII	7.5	3.9	7	3.0	6	5.0	·	·	·	·	4	2.8	14	2.9	3.5	3.4	51	1.5	48	12.7	30	20	23	31	·	1	·	·	19	16	9	2	7	31	–
Rok	41	2.5	53.5	2.2	101	3.1	9	1.6	·	·	25.5	2.9	332.5	3.0	87.5	3.5	445	1.9	857	65.0	18.VII	61	63	174	22	15	1	6	178	236	128	21	110	140	–

Przehyba $H_s = 1175\,m$ $h_w = 13{,}5\,m$

I	11	6.6	1	3.0	·	·	·	·	39	9.8	27.5	5.8	1.5	2.7	13	4.5	·	7.3	48	17.2	27	4	21	31	·	11	5	–	–	13	10	1	–	31	·
II	9	5.8	·	·	·	·	1.5	6.6	24	9.0	18.5	4.8	4	3.9	26	8.8	1	7.3	77	9.9	14	12	26	28	·	7	4	–	–	20	15	·	–	28	·
III	14	10.7	0.5	8.0	·	·	·	·	25.5	10.0	19.5	4.3	6	6.2	26.5	7.4	1	7.8	44	6.2	12	8	24	29	·	12	5	–	–	19	11	·	–	31	·
IV	26.5	7.6	7	3.9	1.5	4.3	3	3.5	37	9.4	4.5	4.9	2	3.5	7.5	7.0	1	7.5	87	33.5	6	·	2	10	·	11	5	–	–	12	12	2	–	20^2	·
V	17	5.9	2	2.0	1	3.0	1.5	2.3	29	6.4	17	4.9	7.5	3.8	16	5.5	2	5.4	127	25.0	21	·	1	5	·	7	2	–	–	26	21	3	–	·	3
VI	42	6.4	4	4.5	·	·	4	3.2	8.5	4.2	13.5	5.0	5	3.8	13	3.8	·	5.3	180	32.6	4	·	3	8	·	5	·	–	–	15	15	8	–	5	7
VII	23.5	4.8	1.5	3.3	·	·	5	2.8	20.5	4.5	22	3.9	3.5	3.9	17	6.3	·	4.6	182	83.4	18	·	·	·	·	2	1	–	–	17	13	3	–	·	4
VIII	14	4.8	1	8.0	·	·	·	·	35.5	6.4	19.5	3.6	4	2.4	18	3.7	1	4.8	51	14.2	16	·	·	·	·	4	1	–	–	7	6	3	–	·	6
IX	7.5	3.3	1	6.0	·	·	7.5	3.7	34	5.6	21.5	4.1	3	3.2	15.5	3.4	·	4.5	60	15.0	18	·	·	·	·	3	·	–	–	12	9	2	–	·	1
X	15	5.0	9.5	2.8	4	3.2	6.5	2.9	26.5	4.3	11	3.5	4	2.2	14.5	5.3	2	4.0	11	3.4	15	·	·	5	·	5	·	–	–	7	4	·	–	·	·
XI	14	6.8	1.5	4.0	2	4.0	7.5	6.1	52	9.7	4.5	4.2	0.5	4.0	8	3.6	·	7.9	103	21.4	15	·	12	18	·	12	5	–	–	16	14	5	–	12	·
XII	20	6.7	5	5.1	2	1.5	5	4.3	29	11.3	10	4.4	2	6.5	18	5.6	2	7.2	40^2	15.4	14	11	28	31	·	11	5	–	–	16	11	1	–	31	·
Rok	213.5	6.2	34	4.2	10.5	1.3	41.5	3.0	360.5	7.6	189	4.4	43	3.8	193	5.4	10	6.1	1010^2	83.4	18.VII	35	117	165	·	90	33	–	–	180	141	28	–	158^2	21

Lesko $H_s = 386\,m$ $h_w = 17{,}6\,m$

I	0.5	6.0	4	4.1	5	2.9	8.5	3.5	35	6.8	13.5	5.3	11.5	3.6	8	3.6	7	4.7	40	7.8	27	2	8	21	·	7	1	2	14	15	10	·	·	15	·
II	4.5	2.9	6	3.1	6.5	1.5	8	5.8	10.5	6.8	5	4.0	20	5.1	12.5	4.5	11	4.0	54	17.5	13	4	14	28	·	7	3	1	19	20	10	2	1	28	·
III	5	3.1	8.5	3.8	6.5	3.9	11.5	3.9	15	6.1	4.5	3.8	10	4.5	14	3.3	18	3.4	63	15.1	15	6	13	26	·	4	·	·	17	19	9	2	1	29	·
IV	2	3.5	5.5	3.8	9.5	2.3	15.5	3.8	15	5.1	7	3.6	9	3.4	8.5	4.1	18	3.1	20	7.1	6	·	·	5	4	4	·	7	7	9	4	·	3	·	·
V	2	2.5	4	1.6	2.5	1.4	13	3.3	6.5	3.9	9.5	4.3	18.5	3.9	16	3.2	21	2.6	129	26.7	20	·	·	2	1	3	·	·	10	25	21	4	9	·	11
VI	11.5	3.1	6	2.1	4.5	1.2	5	1.6	4	3.0	6.5	3.0	14	3.9	18.5	2.9	20	2.2	160	30.4	5	·	·	·	6	·	·	4	11	20	17	7	7	·	7
VII	7	2.7	1.5	2.3	2.5	2.8	11	2.1	10	4.0	6.5	3.5	13	3.1	12.5	2.9	29	2.1	109	44.5	19	·	·	·	4	·	·	3	9	18	12	2	5	·	8
VIII	6	2.0	1.5	1.0	3	2.8	7.5	3.1	12.5	4.3	9	2.8	13	2.7	9.5	2.9	31	2.0	55	13.4	16	·	·	·	9	2	·	2	6	17	10	1	9	·	7
IX	3	1.3	1	6.0	6.5	1.5	11	3.2	15.5	4.3	6.5	3.3	13.5	3.6	6	2.4	27	2.3	55	9.5	5	·	·	·	2	·	·	5	6	15	13	·	4	·	2
X	6	1.6	6	2.3	11	1.9	10.5	2.1	9.5	4.9	1	5.0	10	3.2	4	2.0	35	1.7	5	2.2	20	·	·	10	·	1	·	10	3	12	1	·	13	·	·
XI	2	1.5	6	1.8	7.5	2.4	11	2.5	12	4.3	6.5	2.8	5	1.9	7	1.9	33	1.7	82	18.7	16	·	·	12	·	2	·	2	17	19	13	3	8	7	·
XII	8.5	3.2	15	2.6	5.5	2.1	7	2.6	23	6.0	5.5	3.1	3	3.0	5.5	1.8	20	2.9	51	13.0	30	11	16	31	·	7	·	2	21	20	9	3	1	30	·
Rok	58	2.8	65	2.9	70.5	2.2	119.5	3.1	168.5	5.0	81	3.7	140.5	3.5	122	3.0	270	2.7	823	44.5	19.VII	23	51	135	26	37	4	38	140	209	129	24	61	109	35

Czarny Dunajec $H_s = 676\,m$ $h_w = 18\,m$

I	6	3.9	4	3.6	·	·	·	·	0.5	1.0	23	3.5	24	4.0	4.5	3.7	31	2.5	36	9.1	27	5	12	28	·	–	–	1	16	14	10	·	1	29	·
II	6	4.3	4.5	2.6	·	·	·	·	·	·	11	4.8	15.5	5.3	7	7.2	40	2.6	77	10.6	5	12	17	28	·	–	–	·	22	23	13	2	1	28	·
III	9	4.1	14	3.3	5.5	2.2	2	1.0	·	·	4.5	3.6	12	4.2	1	5.5	45	1.8	55	14.3	16	13	17	29	·	–	–	·	21	14	11	1	2	31	·
IV	7	3.2	7.5	3.6	3	2.8	1.5	2.7	3	3.7	3.5	5.9	10	4.6	4.5	3.9	50	1.7	90	47.4	6	·	·	8	·	–	–	6	14	13	10	2	5	8^2	·
V	8	2.9	7	2.3	2.5	1.6	0.5	1.0	2	2.0	15	3.3	22	3.3	4	3.1	32	2.0	132	17.7	9	·	·	5	·	–	–	·	18	27	18	6	1	·	4
VI	15	2.8	13	2.3	4.5	1.4	0.5	3.0	0.5	3.0	5	2.4	10.5	3.0	12	3.3	29	1.8	140	31.9	4	·	·	·	3	–	–	·	18	15	13	4	3	·	6
VII	8	2.9	6.5	2.5	0.5	4.0	1.5	2.0	0.5	1.0	17	2.3	15	2.7	7	2.9	37	1.6	104	47.6	18	·	·	·	3	–	–	3	16	16	10	3	3	·	6
VIII	6.5	2.3	3.5	1.7	1.5	1.0	2	1.5	1.5	5.0	8.5	3.1	23	2.6	6.5	3.1	40	1.5	48	23.0	15	·	·	·	7	–	–	2	7	11	7	1	3	·	4
IX	1.5	4.3	1.5	4.3	4	1.5	·	·	·	·	13	2.4	25	3.3	4	3.6	41	1.6	63	12.0	18	·	·	7	1	–	–	7	7	12	9	3	7	·	1
X	9.5	1.9	7.5	2.3	4	1.8	2.5	1.0	0.5	1.0	2	4.0	6	3.7	3	2.0	58	0.9	13	6.6	6	·	·	16	·	–	–	10	11	7	4	·	14	·	·
XI	5	2.5	9.5	2.8	7	2.0	1.5	2.0	1.5	3.3	4	3.6	5.5	2.9	1	2.0	55	1.0	85	14.4	23	·	6	18	·	–	–	·	23	19	16	3	9	14	·
XII	6.5	4.1	9.5	3.3	2.5	1.4	1.5	1.7	·	·	12.5	4.0	7.5	3.9	2	7.5	51	1.7	50	16.3	30	17	25	31	·	–	–	·	19	18	12	2	3	31	·
Rok	88	3.3	88	2.9	35	1.6	13.5	1.3	10	1.7	119	3.6	176	3.6	56.5	4.0	509	1.7	893	47.6	18.VII	47	77	170	14	–	–	29	192	189	133	27	52	141^2	21

Krościenko $\varphi = 49°27'$ $\lambda = 20°25'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.6	−6.2	7.9	22	−14.0	31	−3.7	0.3	−2.8	−2.2	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.5	6.0	6.0
II	–	–	–	–	0.5	−7.7	6.3	12	−17.2	25	−5.5	−1.4	−3.6	−3.5	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.7	7.9	8.2
III	–	–	–	–	2.8	−6.2	14.0	5	−17.3	9	−4.4	1.0	−2.1	−1.9	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.8	7.3	7.7
IV	–	–	–	–	14.5	2.6	26.2	23	−4.9	2	5.4	13.3	6.8	8.1	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.9	4.6	5.4
V	–	–	–	–	15.4	4.7	22.6	8	−4.1	2	8.0	13.3	8.5	9.6	–	–	–	–	–	–	–	–	–	–	–	–	7.8	8.1	5.3	7.1
VI	–	–	–	–	17.9	6.6	29.1	24	1.0	9	10.5	15.8	10.8	12.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.7	5.8	6.8
VII	–	–	–	–	20.4	8.0	30.5	26	3.0	5	12.1	19.0	11.9	13.7	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.9	5.3	6.1
VIII	–	–	–	–	23.5	9.4	30.6	15	2.6	31	12.7	22.0	13.8	15.6	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.7	3.6	4.9
IX	–	–	–	–	18.2	4.4	27.6	4	−0.1	15	6.9	16.8	8.9	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.6	3.7	5.1
X	–	–	–	–	14.6	1.1	22.6	3	−4.8	16	2.4	13.3	4.4	6.1	–	–	–	–	–	–	–	–	–	–	–	–	7.5	3.5	3.2	4.7
XI	–	–	–	–	8.1	1.8	17.1	3, 8	−4.4	17	3.4	7.1	4.2	4.7	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.3	8.2	8.0
XII	–	–	–	–	−2.9	−11.0	3.7	14	−22.1	21	−7.2	−4.1	−7.1	−6.4	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.7	7.8	8.1
Rok	–	–	–	–	11.2	0.6	30.6	15, VIII	−22.1	21, XII	3.4	9.7	4.5	5.5	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.6	5.7	6.5

Brzegi Dolne $\varphi = 49°27'$ $\lambda = 22°38'$

I	–	–	–	–	2.1	−3.6	8.3	22	−14.2	31	−1.6	0.9	−1.1	−0.7	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.5	7.2	7.2
II	–	–	–	–	−1.0	−9.8	3.0	13	−27.1	25	−6.9	−2.4	−4.7	−4.7	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.8	8.3	8.7
III	–	–	–	–	1.6	−7.8	15.2	5	−26.4	20	−5.0	0.2	−3.3	−2.8	–	–	–	–	–	–	–	–	–	–	–	–	8.9	9.2	7.3	8.5
IV	–	–	–	–	15.6	1.5	25.5	21	−3.9	2	5.4	13.9	6.5	8.1	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.9	5.0	6.1
V	–	–	–	–	16.2	4.8	24.9	28	−6.6	2	9.0	14.2	8.9	10.2	–	–	–	–	–	–	–	–	–	–	–	–	8.1	9.0	6.4	7.8
VI	–	–	–	–	17.8	6.7	28.2	24	0.4	14	11.6	16.2	11.1	12.5	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.9	6.8	7.2
VII	–	–	–	–	19.5	7.9	29.4	27	1.8	10	12.9	18.2	11.9	13.7	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.5	5.7	6.4
VIII	–	–	–	–	22.8	9.6	29.1	7	0.1	31	13.5	21.6	14.5	16.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.9	6.0	6.6
IX	–	–	–	–	17.7	4.5	26.2	5	−2.0	15	8.2	16.4	9.2	10.8	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.1	5.7	6.2
X	–	–	–	–	13.8	1.2	20.2	4	−7.7	26	1.8	13.0	3.0	5.2	–	–	–	–	–	–	–	–	–	–	–	–	5.9	3.9	4.7	4.8
XI	–	–	–	–	6.5	−0.4	19.0	5	−12.2	17, 18	1.7	7.1	2.9	3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.9	8.0	8.3
XII	–	–	–	–	−2.2	−8.9	7.5	14	−20.7	26	−6.0	−3.8	−5.6	−5.2	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.0	7.8	7.8
Rok	–	–	–	–	11.0	0.5	29.4	27, VII	−27.1	25, II	3.7	9.6	4.4	5.5	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.5	6.6	7.2

Czorsztyn $\varphi = 49°26'$ $\lambda = 20°19'$

I	–	–	–	–	−0.1	−9.5	5.5	20, 21	−20.3	6, 10	−7.0	−1.6	−5.1	−4.7	–	–	–	–	–	–	–	–	–	–	–	–	7.4	5.9	6.4	6.6
II	–	–	–	–	−0.4	−8.9	7.5	12	−20.6	25	−6.7	−2.9	−4.2	−4.5	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.0	7.7	8.2
III	–	–	–	–	1.8	−7.2	12.6	5	−19.5	9	−5.9	0.1	−3.0	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.7	7.1	7.8
IV	–	–	–	–	13.7	1.2	25.3	23	−5.2	2	3.6	12.4	6.5	7.2	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.8	5.2	6.2
V	–	–	–	–	14.6	4.3	21.3	8	−4.3	2	7.0	12.6	8.4	9.1	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.3	6.4	7.6
VI	–	–	–	–	17.3	6.3	28.5	24	0.6	5	9.1	15.4	11.0	11.6	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.7	6.9	7.6
VII	–	–	–	–	19.7	8.0	28.8	26	1.5	5	10.6	18.7	12.4	13.5	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.1	5.9	6.9
VIII	–	–	–	–	22.5	9.4	30.5	15	3.6	29	11.3	21.4	14.1	15.2	–	–	–	–	–	–	–	–	–	–	–	–	8.5	5.8	4.5	6.3
IX	–	–	–	–	17.6	4.0	26.6	4	−0.9	16	5.9	16.2	9.2	10.1	–	–	–	–	–	–	–	–	–	–	–	–	7.9	5.0	4.3	5.7
X	–	–	–	–	14.5	0.8	23.1	3	−4.5	23	1.9	12.8	4.7	6.0	–	–	–	–	–	–	–	–	–	–	–	–	9.6	3.6	3.0	5.4
XI	–	–	–	–	7.5	1.0	16.7	8	−6.0	17	2.7	6.3	3.9	4.2	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.8	8.4	8.2
XII	–	–	–	–	−3.6	−13.1	4.0	13	−26.9	29	−9.2	−6.0	−8.6	−8.1	–	–	–	–	–	–	–	–	–	–	–	–	9.1	7.6	7.1	7.9
Rok	–	–	–	–	10.4	−0.3	30.5	15, VIII	−26.9	29, XII	1.9	8.8	4.1	4.7	–	–	–	–	–	–	–	–	–	–	–	–	8.3	6.8	6.1	7.1

Czorsztyn-Nadzamcze $\varphi = 49°26$ $\lambda = 20°20'$

I	–	–	–	–	−1.0	−6.9	4.6	21	−16.9	31	−5.0	−1.8	−4.2	−3.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	−2.1	−8.2	5.0	12	−16.9	25	−7.3	−3.7	−5.0	−5.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	0.2	−7.0	10.6	31	−18.1	9	−5.7	−0.8	−3.9	−3.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	12.6	2.3	24.6	23	−4.3	3	3.9	11.1	6.9	7.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	13.5	4.4	20.4	8	−3.9	2	6.4	11.3	8.1	8.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	16.2	6.7	27.6	24	−0.9	5	8.6	14.2	10.7	11.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	18.9	8.5	27.8	26	2.5	5	10.7	17.2	12.6	13.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.8	9.9	29.0	15	3.2	31	11.5	20.5	14.6	15.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	16.7	4.7	25.8	4	−0.6	10	6.1	14.9	9.5	10.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	13.3	0.8	20.6	4	−4.0	22, 24	1.5	12.0	5.6	6.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.4	0.7	15.6	8	−5.9	17	2.0	5.3	2.4	3.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	−4.7	−10.8	2.8	13	−24.9	4	−9.0	−5.9	−8.0	−7.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	9.3	0.4	29.0	15, VIII	−24.9	4, XII	2.0	7.9	4.1	4.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Krościenko $H_s = 440 m$ — h_w = 20,4m I–III, h_w = 18,9m IV–XII — 1962

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◑	●	Opad R ≥ 0.1	R ≥ 10	R ≥ 100	≡	⊠	R
I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	57	21.0	27	8	9	29	·	—	—	4	13	13	10	1	3	31	·
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	92	15.6	17	9	10	26	·	—	—	·	16	19	15	3	15	28	·
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	60	13.7	12	8	10	27	·	—	—	·	16	16	11	3	11	31	·
IV	5.5	1.4	8	2.0	10	2.2	4.5	2.2	5.5	2.9	17	2.0	10.5	2.9	2	1.5	27	1.5	70	33.0	6	·	·	6	4	·	·	8	11	13	8	2	10	4	·
V	2	1.0	8.5	2.0	4.5	1.4	2.5	3.0	2	3.2	17.5	2.7	12	3.5	2	2.5	42	1.4	94	21.8	20	·	·	6	·	3	·	1	11	21	18	3	16	·	3
VI	3.5	1.4	10	1.7	0.5	4.0	·	·	2.5	1.0	20.5	2.0	19.5	2.2	2.5	1.0	31	1.3	161	33.8	4	·	·	·	6	·	·	2	10	17	14	5	11	·	6
VII	2	1.5	8.5	1.4	2.5	1.2	2	1.5	3	1.0	17	2.1	13	2.9	·	·	45	1.0	166	50.7	18	·	·	·	5	1	·	3	10	14	11	4	8	·	6
VIII	4	1.5	3.5	1.4	4.5	2.2	·	·	2	1.5	8	2.1	21.5	2.0	1.5	1.3	48	0.9	52	25.9	5	·	·	·	11	1	1	3	3	8	5	2	15	·	4
IX	1.5	1.0	8.5	1.4	4	1.4	3.5	1.9	2	2.0	29	2.0	10	3.2	0.5	1.0	31	1.3	41	15.2	18	·	·	1	5	1	·	6	6	11	7	1	15	·	1
X	8	1.4	14	1.4	6	1.2	2.5	1.0	1	1.0	14	1.5	9.5	1.4	1	1.5	37	0.8	3	2.1	30	·	·	16	·	2	·	7	5	3	1	·	19	·	·
XI	2.5	1.4	9.5	1.5	17	1.7	10	1.7	2	1.8	7	1.3	6	1.0	·	·	36	0.9	81	15.0	22	·	1	10	·	1	·	2	20	16	15	1	8	10	·
XII	5.5	2.1	12	1.9	5.5	1.9	6	2.6	5	2.9	11.5	1.7	18.5	1.3	1	1.0	28	1.3	39	8.6	30	17	18	30	·	3	·	·	18	15	9	·	·	31	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	916	50.7	18.VII	42	48	151	31	—	—	36	139	166	124	25	131	135	20

Brzegi Dolne $H_s = 420 m$ — $h_w = 17 m$

I	1	1.0	1.5	2.0	3.5	4.0	2.5	1.2	26	3.2	21	3.1	13.5	2.4	6	1.8	18	2.3	48	15.4	27	2	8	23	·	2	·	2	13	14	9	2	·	10	·
II	4	1.5	5.5	1.7	5.5	1.5	1	2.0	1.5	3.0	12	7.2	16.5	3.9	6	4.3	32	2.5	88	29.4	13	11	16	28	·	3	2	·	21	20	11	2	1	28	·
III	4	1.8	2	2.0	11	3.7	5	1.8	10	4.0	7	3.3	11	4.0	8	2.6	35	2.0	72	16.0	16	9	13	26	·	2	·	·	21	16	9	3	·	30	·
IV	1	2.0	7.5	1.9	9.5	2.0	7	2.6	8	3.1	5.5	2.8	9	2.2	6.5	2.7	36	1.5	42	17.6	6	·	·	10	1	·	·	5	12	8	7	1	3	·	·
V	4	1.8	3.5	1.4	3.5	1.7	3	2.0	6	1.7	9	3.0	25	3.1	5	4.5	34	1.7	119	14.5	10	·	·	6	·	1	·	·	17	24	21	4	5	·	6
VI	7	1.3	1.5	1.7	5.5	1.4	2	2.0	2	1.5	7	2.3	15.5	2.8	14.5	2.4	35	1.3	171	29.8	5	·	·	·	5	·	·	3	16	18	16	7	3	·	4
VII	3	1.3	3.5	1.6	4.5	1.9	2	1.5	1.5	1.0	9.5	2.6	10.5	3.1	10.5	1.8	48	1.1	129	31.8	19	·	·	·	3	·	·	3	13	18	16	4	2	·	3
VIII	1	1.0	1.5	1.7	1.5	5.0	2.5	3.4	3	3.3	6.5	3.3	12	2.8	9	2.7	56	1.2	52	10.4	16	·	·	·	9	·	·	1	12	16	11	1	7	·	2
IX	1	1.0	4	2.2	2	2.5	3	3.0	5.5	3.0	13	2.8	17.5	2.3	2	3.0	42	1.4	52	15.4	22	·	·	2	1	·	·	5	10	15	13	1	10	·	1
X	1	1.0	13.5	1.9	1.5	1.3	·	·	1	3.0	12	1.8	8	2.4	2	1.5	54	0.8	5	1.1	15	·	·	18	·	·	·	11	5	10	2	·	11	·	·
XI	2.5	1.0	11	1.8	7.5	1.9	4	3.0	7	2.0	9	2.6	8.5	1.8	2.5	1.0	38	1.1	65	25.6	16	2	·	13	·	·	·	·	17	16	10	1	6	5	·
XII	2.5	1.0	14	2.4	8	1.9	2.5	4.6	14.5	3.4	13	3.2	6.5	1.9	4	1.1	28	1.8	58	12.3	30	14	16	30	·	·	·	3	19	16	13	2	·	30	·
Rok	32	1.3	69	1.9	63.5	2.4	34.5	2.3	86	2.7	124.5	3.2	153.5	2.7	76	2.4	456	1.6	901	31.8	19.VII	38	53	156	19	8	2	33	176	191	138	28	48	103	16

Czorsztyn $H_s = 496 m$ — h_w = 18,4m

I	3	2.7	0.5	2.0	0.5	2.0	·	·	·	·	·	·	4.5	3.3	12.5	2.9	72	0.7	46	16.0	27	13	14	31	·	·	·	3	12	14	10	1	1	31	·
II	·	·	2	3.0	·	·	·	·	·	·	0.5	8.0	13.5	6.4	18	5.7	50	2.4	82	12.6	5	13	13	27	·	1	·	·	16	23	16	2	·	28	·
III	1.5	2.0	5	2.8	4.5	5.1	1	4.0	·	·	·	·	9.5	5.2	14.5	3.2	57	1.5	52	13.8	15	10	12	29	·	·	·	1	18	17	11	2	1	31	·
IV	·	·	4.5	3.0	2.5	4.0	10.5	7.3	2.5	3.4	1	1.0	8.5	4.8	8.5	3.5	52	2.0	62	31.7	6	·	·	8	1	3	·	5	11	11	8	1	2	8	·
V	1	1.5	2	2.5	4.5	3.3	3	3.5	1	4.5	1.5	7.3	14.5	4.4	8.5	4.2	57	1.6	108	25.5	20	·	·	6	·	2	·	1	16	21	18	3	3	·	1
VI	1.5	2.0	1.5	2.0	4.5	2.2	2	3.2	1	4.0	0.5	3.0	18	4.4	10	3.8	51	1.6	133	27.7	4	·	·	·	6	2	·	·	13	16	13	4	7	·	4
VII	1	2.0	4	2.5	1	3.0	1	6.0	3	3.0	·	·	14	4.0	14	3.6	55	1.5	141	52.6	18	·	·	·	4	·	·	·	11	16	12	4	5	·	6
VIII	·	·	1	2.0	5	3.6	·	·	1	1.0	·	·	8.5	4.7	12.5	3.9	65	1.2	47	16.0	15	·	·	·	9	1	·	2	7	9	7	2	14	·	4
IX	2	2.5	1.5	3.0	3	3.3	1.5	4.3	2	4.0	·	·	9	3.7	11	4.8	60	1.3	36	10.3	18	·	·	1	3	·	·	2	6	13	8	1	11	·	·
X	2	1.0	1.5	2.7	6	2.8	3.5	2.1	0.5	5.0	1	2.0	2	1.8	7.5	2.7	69	0.6	3	1.5	30	·	·	17	·	·	·	1	7	7	1	·	22	·	·
XI	0.5	3.0	2	2.5	13.5	4.6	13.5	7.0	1	4.5		·	1.5	3.7	9	3.2	49	2.2	100	20.2	23	·	3	13	·	3	1	1	22	15	13	3	4	11	·
XII	1	2.0	·	·	5	3.6	8	3.8	·	·	·	·	3.5	3.7	7.5	2.9	68	0.9	50	14.1	14	20	22	31	·	·	·	·	16	16	8	2	1	31	·
Rok	13.5	1.6	25.5	2.3	50	3.1	44	3.4	12	2.4	4.5	1.8	107	4.2	133.5	3.7	705	1.5	860	52.6	18.VII	56	64	163	23	12	1	16	155	178	125	25	71	140	15

Czorsztyn-Nadzamcze $H_s = 650 m$ — h_w = 16,6m

I	3	1.0	9	2.2	11	2.4	3	2.0	·	·	5	1.4	30	5.6	10	3.7	22	2.9	–	–	–	7	16	31	·	9	2	–	–	–	–	–	3	31	·
II	3	1.3	8	1.4	4	2.5	1	3.0	·	·	4	8.2	23	8.0	31	6.0	10	5.1	–	–	–	7	21	28	·	10	6	–	–	–	–	–	1	28	·
III	6	3.5	28	3.1	7.5	4.7	4.5	7.9	·	·	1	8.0	13	8.0	18	2.9	15	3.7	–	–	–	9	17	29	·	10	3	–	–	–	–	–	1	31	·
IV	3	1.3	16	1.5	12.5	4.1	9.5	12.1	·	·	1	1.0	18	4.2	16	4.2	14	3.8	41	22.0	6	·	·	7	·	8	3	–	–	13	6	1	6	11	·
V	2	2.0	10	1.6	6	1.7	9	7.0	·	·	1	18.5	27	5.5	22	2.2	16	3.3	107?	27.3	20	·	·	6	·	9	2	–	–	21	18	3	5	1	3
VI	7	1.0	9	1.3	7	1.3	2	1.5	·	·	2	1.0	14	5.2	29	4.1	20	2.5	136	30.2	5	·	·	2	3	5	1	–	–	17	15	4	5	·	5
VII	4	1.5	11	1.4	8	2.1	2	1.5	1	1.0	2	6.5	15	5.1	27	2.8	23	2.2	158	63.0	18	·	·	·	3	4	1	–	–	17	13	4	6	·	5
VIII	2	1.0	12	1.2	4	3.8	2	12.5	·	·	4	3.5	14	3.8	22	3.8	33	2.2	49	20.3	15	·	·	·	7	8	1	–	–	9	8	1	8	·	5
IX	5	1.0	11	1.5	6	4.7	5	2.4	·	·	4	4.8	24	4.4	15	2.2	20	2.4	44	13.5	18	·	·	3	1	7	1	–	–	13	9	1	11	·	·
X	10	1.1	25	1.4	8	2.1	2	4.0	1	1.0	1	2.0	5	4.0	17	1.5	24	1.3	5?	4.2	20	·	·	13	·	1	·	–	–	2	1	·	21	·	·
XI	4	1.2	25	1.6	18	5.9	11	9.5	·	·	·	·	8	3.5	7	1.6	17	3.3	–	–	–	·	5	16	·	8	1	–	–	–	–	–	8	12	·
XII	7	1.0	15	1.5	11	3.3	5	6.8	·	·	·	·	15	2.9	19	1.9	21	1.9	40	11.1	30	16	24	31	·	3	1	–	–	14	8	2	5	31	·
Rok	56	1.4	179	1.6	103	3.2	56	5.8	2	0.2	25	4.6	206	5.0	233	3.1	235	2.9	–	63.0	18.VII	39	83	166	14	82	22	–	–	–	–	–	80	145	10

Szczawnica $\varphi = 49°26'$ $\lambda = 20°29'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA J_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.1	-4.9	6.4	22	-14.7	31	-3.4	0.5	-2.8	-2.1	4.6	5.1	4.9	4.9	93	78	92	88	0.3	1.4	0.4	0.7	6.8	6.3	7.2	6.8
II	–	–	–	–	-0.4	-7.3	4.0	12	-18.4	25	-5.7	-1.3	-3.9	-3.7	4.0	4.7	4.3	4.3	95	84	91	90	0.2	0.9	0.4	0.5	8.9	7.8	8.2	8.3
III	–	–	–	–	1.9	-6.2	13.5	5	-16.7	9	-4.5	1.2	-3.1	-2.4	4.4	5.4	4.6	4.8	92	77	90	86	0.3	1.7	0.5	0.8	8.1	7.7	7.9	7.9
IV	–	–	–	–	14.4	3.0	26.9	23	-4.1	2	4.6	12.9	8.0	8.4	8.0	9.5	9.3	8.9	93	65	85	81	0.8	7.2	2.1	3.4	6.1	6.6	6.0	6.2
V	–	–	–	–	14.7	4.8	23.7	8	-3.9	2	7.2	13.4	8.9	9.6	9.7	10.5	10.1	10.1	93	69	87	83	0.8	5.5	1.6	2.6	7.5	7.8	5.9	7.1
VI	–	–	–	–	17.4	7.0	28.9	24	-0.2	5	9.3	15.8	12.0	12.3	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.2	7.5	7.1
VII	–	–	–	–	20.1	8.8	30.0	27	4.1	5	10.6	19.0	14.0	14.4	12.4	14.0	14.1	13.5	96	63	87	82	0.5	8.7	2.2	3.8	5.9	6.5	5.9	6.1
VIII	–	–	–	–	23.4	10.4	30.4	15	3.3	31	11.4	22.1	15.8	16.3	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.3	5.7	5.6
IX	–	–	–	–	17.9	5.3	28.1	4	0.6	10	6.6	16.5	10.9	11.2	9.5	12.3	11.4	11.1	95	66	86	82	0.6	7.5	2.1	3.4	6.4	5.7	4.5	5.5
X	–	–	–	–	13.6	1.5	21.0	3	-3.4	16	2.5	12.8	6.0	6.8	7.3	10.2	8.8	8.8	97	69	92	86	0.2	5.0	0.8	2.0	6.6	4.3	3.3	4.7
XI	–	–	–	–	7.5	1.9	18.0	3	-3.9	17	3.2	6.6	3.7	4.3	7.5	8.2	7.7	7.8	94	82	93	90	0.5	2.3	0.6	1.1	7.6	7.7	8.6	8.0
XII	–	–	–	–	-3.4	-10.1	3.9	14	-20.3	22	-7.1	-4.5	-7.2	-6.5	3.6	3.8	3.4	3.6	92	82	89	88	0.3	0.9	0.5	0.6	8.9	7.4	7.1	7.8
Rok	–	–	–	–	10.7	1.2	30.4	15. VIII	-20.3	22. XII	2.9	9.6	5.2	5.7	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.7	6.5	6.8

Piwniczna $\varphi = 49°26'$ $\lambda = 20°42'$

I	–	–	–	–	1.5	-4.5	7.8	20	-14.9	31	-2.7	0.3	-2.0	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	8.1	6.0	7.2	7.1
II	–	–	–	–	1.1	-6.8	7.9	13	-17.4	25	-4.5	-0.9	-3.0	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.2	8.6	8.[illegible]
III	–	–	–	–	2.5	-5.2	14.3	5	-14.9	9	-3.6	1.2	-2.0	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.1	8.1	8.4
IV	–	–	–	–	15.2	3.6	26.4	23	-3.3	2	6.1	13.7	7.9	8.9	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.3	4.8	5.9
V	–	–	–	–	16.0	5.7	22.9	8	-2.4	2	8.7	13.8	9.3	10.3	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.6	5.4	7.4
VI	–	–	–	–	18.3	8.1	28.8	23	2.1	7	11.3	16.3	12.1	13.0	–	–	–	–	–	–	–	–	–	–	–	–	7.8	8.2	6.8	7.6
VII	–	–	–	–	20.9	9.8	30.7	27	5.1	30	12.9	19.3	13.6	14.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.6	5.3	6.8
VIII	–	–	–	–	24.1	11.1	31.6	15	3.3	31	13.7	22.6	15.6	16.9	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.0	3.7	5.4
IX	–	–	–	–	18.4	6.4	28.0	12	1.8	27	8.5	16.6	10.4	11.5	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.0	4.5	5.7
X	–	–	–	–	14.7	2.6	21.5	3	-3.0	22	3.7	13.4	5.7	7.1	–	–	–	–	–	–	–	–	–	–	–	–	9.3	4.1	4.3	5.9
XI	–	–	–	–	8.2	2.0	18.1	3	-3.7	28	3.6	7.0	4.2	4.8	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.0	8.3	8.2
XII	–	–	–	–	-2.4	-9.2	4.0	16	-20.0	21	-6.3	-3.8	-6.4	-5.7	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.4	8.7	8.4
Rok	–	–	–	–	11.5	2.0	31.6	15. VIII	-20.0	21. XII	4.3	10.0	5.4	6.3	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.0	6.3	7.1

Krynica $\varphi = 49°26'$ $\lambda = 20°58'$

I	–	–	–	–	0.4	-5.9	6.4	20	-15.4	31	-4.4	-1.3	-3.8	-3.3	4.2	4.6	4.3	4.4	91	81	89	87	0.4	1.2	0.5	0.7	8.4	6.6	8.1	7.7
II	–	–	–	–	-0.7	-7.4	4.9	13	-17.6	25	-5.9	-2.7	-4.3	-4.3	3.6	4.0	4.0	3.9	88	84	88	87	0.5	1.1	0.6	0.7	9.3	8.4	8.8	8.8
III	–	–	–	–	0.8	-6.2	12.7	5	-14.9	21	-4.5	-0.4	-3.4	-2.9	4.3	4.5	4.4	4.4	90	73	88	84	0.5	1.7	0.6	0.9	8.8	8.1	8.0	8.3
IV	–	–	–	–	13.6	2.8	25.3	23	-4.4	2	4.9	11.7	6.5	7.4	7.6	7.5	7.9	7.7	87	59	81	76	1.4	7.7	2.2	3.8	5.9	6.4	4.6	5.6
V	–	–	–	–	14.3	4.5	21.5	28	-4.0	2	7.0	12.1	8.2	8.9	9.2	9.5	9.6	9.5	89	67	86	81	1.2	5.0	1.6	2.6	7.7	7.7	6.6	7.3
VI	–	–	–	–	16.3	6.8	27.0	24	0.6	7	9.4	14.2	10.7	11.2	11.2	11.6	11.8	11.5	91	70	88	83	1.1	6.2	1.6	3.0	6.2	8.4	7.2	7.3
VII	–	–	–	–	19.1	9.0	29.6	27	4.5	3	11.3	17.3	12.6	13.4	12.3	12.6	13.2	12.7	91	64	89	81	1.3	7.8	1.7	3.6	6.1	6.9	5.7	6.2
VIII	–	–	–	–	22.3	10.1	28.5	13, 15	2.4	31	12.0	20.8	14.5	15.4	13.4	15.0	14.7	14.4	94	61	88	81	1.0	10.3	2.2	4.5	5.4	5.5	3.7	4.9
IX	–	–	–	–	17.2	5.2	26.7	12	0.3	27	6.7	15.4	9.7	10.4	9.3	10.6	10.6	10.2	93	61	87	80	0.9	7.6	1.8	3.4	6.2	5.6	3.9	5.2
X	–	–	–	–	14.0	1.8	21.3	3	-4.2	16	2.7	12.7	5.3	6.5	7.4	9.4	8.5	8.4	97	64	93	85	0.3	5.8	0.6	2.2	6.2	3.6	3.3	4.4
XI	–	–	–	–	6.9	1.1	17.2	3	-4.8	28	2.7	5.5	3.2	3.6	7.1	7.5	7.3	7.3	92	81	92	88	0.7	2.4	0.7	1.3	8.4	8.1	8.1	8.2
XII	–	–	–	–	-3.5	-9.1	1.6	8	-18.3	23	-7.3	-5.0	-7.0	-6.6	3.3	3.6	3.3	3.4	89	82	86	86	0.4	0.8	0.5	0.6	9.2	7.6	9.0	8.6
Rok	–	–	–	–	10.1	1.1	29.6	27. VII	-18.3	23. XII	2.9	8.4	4.4	5.0	7.7	8.4	8.3	8.1	91	71	88	83	0.8	4.8	1.2	2.3	7.3	6.9	6.4	6.9

Krynica-Góra Parkowa $\varphi = 49°25'$ $\lambda = 20°58'$

I	–	–	–	–	-0.9	-6.1	4.1	20	-16.2	31	-4.6	-2.0	-4.2	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.9	6.6	7.8	7.8
II	–	–	–	–	-1.8	-7.6	3.6	13	-16.0	25	-6.5	-3.3	-5.0	-5.0	–	–	–	–	–	–	–	–	–	–	–	–	9.7	8.4	8.5	8.9
III	–	–	–	–	0.2	-6.2	11.6	5	-12.1	17	-4.8	-0.8	-3.9	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.0	7.8	8.3
IV	–	–	–	–	12.7	3.6	25.3	22	-3.4	8	6.0	11.1	7.0	7.8	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.2	5.0	6.2
V	–	–	–	–	13.6	4.6	20.7	28	-3.6	2	6.8	11.2	7.9	8.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.4	6.0	7.5
VI	–	–	–	–	15.5	7.2	25.8	24	-0.4	7	9.6	13.7	10.4	11.0	–	–	–	–	–	–	–	–	–	–	–	–	6.7	8.4	7.7	7.6
VII	–	–	–	–	18.4	9.5	27.8	27	5.5	3	11.6	16.9	12.5	13.4	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.5	6.0	6.7
VIII	–	–	–	–	21.7	11.2	27.8	13	4.3	31	13.4	20.2	14.8	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.3	4.1	5.3
IX	–	–	–	–	16.5	6.4	25.8	5	2.2	27	7.9	14.9	9.8	10.6	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.5	3.8	5.5
X	–	–	–	–	13.0	3.6	20.0	3	-3.2	16	4.6	12.1	6.4	7.4	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.2	3.5	4.2
XI	–	–	–	–	5.8	0.6	16.3	3	-5.2	28	2.1	4.6	2.5	2.9	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.6	8.4	8.7
XII	–	–	–	–	-4.3	-9.2	3.1	8	-19.1	23	-7.6	-5.5	-7.3	-6.9	–	–	–	–	–	–	–	–	–	–	–	–	9.4	7.7	8.8	8.6
Rok	–	–	–	–	9.2	1.5	27.8	27.VII, 13.XII	-19.1	23. XII	3.2	7.8	4.2	4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.3	6.4	7.1

Szczawnica $H_s = 500\,m$ $h_w = $ 32,0 m I–X, 12,0 m XI, 22,3 m XII 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	≡	⊠	R/R
I	3	1.3	4	1.8	21.5	2.9	7.5	2.7	3	4.0	9	2.0	16	2.4	23	2.5	6	2.3	64	21.1	27	4	9	27	·	·	·	3	12	14	11	2	·	18	·
II	9	1.3	6	2.0	11	2.4	4	6.0	1	4.0	1	2.0	20	3.0	30	3.3	2	2.8	104	16.6	17	5	13	27	·	3	2	·	16	21	14	2	1	28	·
III	9	1.6	11.5	1.5	15.5	2.3	10	3.4	1	6.0	3	2.7	17.5	3.1	23.5	2.5	2	2.4	75	19.2	16	7	9	27	·	2	·	1	16	19	11	2	1	30	·
IV	14.5	2.1	14	1.8	13	3.5	14.5	6.0	·	·	2	3.0	11	2.8	14	3.0	7	3.0	75	37.8	6	·	·	6	3	2	·	5	11	13	9	2	5	·	·
V	6.5	2.6	9	1.7	6	2.3	5.5	2.9	5.5	4.7	7	5.1	34	2.2	16.5	2.7	3	2.6	99	17.0	21	·	·	6	·	3	·	2	10	25	19	3	4	1	4
VI	19	1.9	8	1.9	3	1.3	1	2.0	2	2.5	12	2.5	15.5	3.2	24.5	2.5	5	2.3	192	39.3	4	·	·	1	6	·	·	1	10	19	15	7	2	·	5
VII	16.5	2.0	12	1.5	7	1.7	6	1.5	4	2.0	3	1.7	16	2.7	25.5	2.3	3	2.0	169	57.8	18	·	·	·	5	·	·	4	7	19	12	3	2	·	5
VIII	15.5	1.7	12.5	1.4	8	1.8	8	3.8	2	2.0	5	2.0	20	3.0	19	2.2	3	2.2	44	15.1	5	·	·	·	10	2	2	1	6	9	4	3	6	·	4
IX	14	1.6	10	1.8	18	1.8	6	2.8	3	2.8	6	4.6	14.5	2.2	15.5	2.0	3	2.1	64	18.6	18	·	·	·	3	1	·	3	7	11	8	3	9	·	1
X	9	1.8	12	1.7	16	2.1	8	1.6	3	2.0	5	2.2	12	1.9	19	1.9	9	1.7	5	1.5	14	·	·	12	·	·	·	7	6	7	2	·	14	·	·
XI	9	2.0	5	2.4	18	3.4	26	3.1	·	·	2	2.5	8	1.9	18	2.3	4	2.6	93	16.8	20	·	2	14	·	·	·	1	18	17	16	4	3	11	·
XII	11	1.7	2	1.5	23	3.8	2	5.0	1	4.0	8	1.5	6	2.8	33	1.8	7	2.3	52	12.3	14	14	22	31	·	1	1	·	17	20	11	2	2	31	·
Rok	136	1.8	106	1.8	160	2.4	98.5	3.4	25.5	2.8	63	2.6	190.5	2.6	261.5	2.4	54	2.4	1036	57.8	18.VII	30	55	151	27	14	5	28	136	194	132	33	49	119	19

Piwniczna $H_s = 380\,m$ $h_w = 17,4\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	≡	⊠	R/R
I	1	4.0	·	·	17	2.0	22	2.7	6	2.8	4	2.0	23	1.8	5	5.0	15	2.1	40	9.1	27	3	9	26	·	·	·	2	17	14	9	·	1	30	·
II	1	4.0	·	·	5	2.8	6	2.3	3	1.7	6	3.5	32	3.5	7	4.6	24	2.4	75	11.8	14	5	9	26	·	·	·	·	19	20	14	1	3	28	·
III	·	·	·	·	2	2.0	18	3.5	2	1.5	2	3.0	33	2.3	10	4.7	26	2.1	73	18.3	16	4	10	26	·	·	·	1	20	19	13	2	5	31	·
IV	·	·	1	4.0	1	2.0	18	3.4	2	1.5	6	2.8	27	2.0	8	2.8	27	1.8	87	35.3	6	·	·	4	4	·	·	8	11	13	10	3	3	1	2
V	·	·	·	·	·	·	8	2.5	6	2.0	10	2.1	35	2.3	4	3.2	30	1.6	105	18.2	9	·	·	3	·	·	·	·	12	24	17	3	4	·	5
VI	·	·	·	·	1	2.0	2	2.5	2	1.5	14	1.6	37	2.4	3	3.7	31	1.5	226	42.0	1. 5	·	·	·	7	·	·	1	15	16	14	7	7	·	6
VII	·	·	·	·	3	2.0	1	3.0	3	1.3	7	1.7	33	2.2	·	·	46	1.1	106	46.0	18	·	·	·	5	·	·	2	11	18	12	3	5	·	8
VIII	·	·	·	·	1	1.0	5	2.8	4	1.5	10	2.5	31	2.3	·	·	42	1.3	63	26.3	5	·	·	·	10	·	·	6	5	10	5	3	9	·	5
IX	·	·	·	·	7	2.4	5	2.0	2	2.0	7	2.4	27	1.8	·	·	42	1.1	52	18.8	18	·	·	·	3	·	·	6	8	11	8	1	10	·	1
X	·	·	·	·	2	2.5	2	1.5	8	1.4	5	2.2	25	1.6	·	·	51	0.8	5	2.8	15	·	·	8	·	·	·	2	8	6	2	·	20	·	·
XI	·	·	1	2.0	6	3.2	25	2.6	5	1.4	3	2.0	26	1.8	·	·	24	1.6	93	26.1	15	·	1	9	·	·	·	1	20	18	12	4	9	11	·
XII	·	·	1	2.0	10	3.0	14	3.2	4	1.2	3	1.3	34	2.5	2	3.0	25	1.9	49	14.4	14	12	20	31	·	·	·	2	20	17	10	2	2	31	·
Rok	2	0.7	3	0.7	55	2.1	126	2.7	47	1.6	77	2.3	363	2.2	39	2.2	383	1.6	974	46.0	18.VII	24	49	133	29	·	·	31	166	186	126	29	78	132	27

Krynica $H_s = 613\,m$ $H_b = 609,6\,m$ $h_w = 18\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	≡	⊠	R/R
I	7	3.1	·	·	2.5	4.2	13.5	3.5	32.5	3.8	3	3.3	7	5.4	11.5	4.3	16	3.2	52	8.8	27	5	13	29	·	2	·	2	19	16	13	·	3	31	·
II	10	3.9	0.5	3.0	·	·	7	1.9	10.5	4.0	11	5.2	12	6.7	20	4.5	13	3.9	95	11.9	19	5	14	27	·	3	·	·	20	21	15	2	2	28	·
III	7	2.3	1	3.0	0.5	3.0	7.5	2.7	17	3.8	5	4.3	11	4.1	26	3.0	18	2.7	78	17.9	16	7	15	28	·	·	·	1	21	22	14	2	3	31	·
IV	10	2.4	·	·	·	·	14.5	3.5	11	3.5	8	4.5	5.5	4.3	18	3.3	23	2.6	65	17.7	6	·	·	7	1	·	·	7	10	13	9	2	2	10	1
V	10	2.2	1	1.0	·	·	8.5	1.5	21	2.4	6.5	3.6	13.5	4.6	15.5	3.0	17	2.3	111	22.0	9	·	·	5	·	·	·	·	10	22	19	3	3	1?	3
VI	12.5	3.0	3.5	2.7	·	·	2.5	1.4	8	2.9	4	2.2	9.5	4.9	22	3.7	28	2.3	262	47.5	5	·	·	·	3	·	·	1	12	17	15	8	5	·	7
VII	11.5	2.8	1	1.0	·	·	5.5	1.9	21	2.4	4.5	3.0	9	3.9	16.5	2.9	24	2.0	136	45.4	18	·	·	·	3	·	·	3	12	17	12	4	1	·	8
VIII	7	2.6	2	1.0	2	1.5	4	2.8	12	4.0	6.5	2.8	10	5.6	13.5	4.6	36	2.3	59	17.0	3	·	·	·	9	·	·	6	2	12	8	3	4	·	6
IX	6.5	1.9	0.5	3.0	·	·	9	2.0	16.5	3.1	9.5	3.6	5.5	3.9	10.5	3.5	32	2.0	61	21.6	18	·	·	·	3	·	·	7	6	12	8	2	3	·	1
X	8.5	2.5	5.5	2.5	0.5	3.0	5	2.6	13	3.1	6	3.0	5.5	5.0	9	2.9	40	1.7	8	2.3	20	·	·	9	·	·	·	7	6	8	3	·	13	·	·
XI	8.5	2.2	2	1.5	3.5	3.3	17.5	2.9	20.5	3.0	5.5	3.9	1.5	2.7	10	2.5	21	2.2	110	28.0	15	·	4	15	·	·	·	1	20	18	13	4	6	12	·
XII	7	2.7	1.5	2.3	0.5	1.0	7	3.6	22.5	3.2	6	4.5	7	4.0	20.5	2.7	21	2.5	56	12.6	30	13	23	31		·	·	·	23	18	11	2	2	31	·
Rok	105.5	2.6	18.5	1.8	9.5	1.3	101.5	2.5	205.5	3.3	75.5	3.7	97	4.6	193	3.4	289	2.5	1093	47.5	5.VI	30	69	151	19	5	·	35	161	196	140	32	47	144?	26

Krynica-Góra Parkowa $H_s = 740\,m$ $h_w = $ 20,4 m I–III, 18,9 m IV–XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	≡	⊠	R/R
I	14.5	4.4	2.5	3.0	·	·	1.5	3.0	47	4.0	13.5	2.6	2	3.0	12	4.9	·	3.9	52	10.2	27	4	17	30	·	3	1	2	17	15	11	1	9	31	–
II	24.5	6.6	5.5	1.6	1	1.0	2.5	2.6	21	3.5	10.5	4.8	1	5.5	18	7.5	·	5.3	108	19.3	18	6	21	28	·	8	5	·	22	23	17	2	4	28	–
III	29	4.8	7	3.3	1	2.0	9	2.7	31	4.8	0.5	3.0	1.5	2.3	14	5.1	·	4.5	66	15.7	16	6	18	28	·	8	·	·	21	21	11	2	6	31	–
IV	20	3.2	13.5	2.6	2	3.5	9	2.7	24.5	6.0	10.5	3.1	·	·	8.5	5.2	2	3.9	45	15.1	6	·	·	7	1	4	·	4	11	12	8	1	10	10	–
V	26.5	3.3	5	2.3	·	·	6	2.2	23	3.8	18	4.3	4	3.2	10.5	3.7	·	3.5	111	20.6	9	·	·	4	·	4	·	·	13	23	19	3	9	·	–
VI	40.5	3.3	9	2.7	·	·	5.5	1.8	11	2.7	6.5	3.0	4	3.0	13.5	6.3	·	3.5	230	42.0	5	·	·	1	2	2	·	·	16	17	15	8	8	·	–
VII	36	2.8	5	2.7	·	·	2.5	2.5	17	2.6	12.5	2.8	5	2.6	8	3.2	2	2.7	128	45.1	18	·	·	·	2	·	·	1	11	16	15	3	5	·	–
VIII	23	2.3	12	2.1	·	·	1.5	2.3	26	3.4	11.5	3.2	3.5	1.7	13.5	3.4	2	2.9	52	14.9	3	·	·	·	7	1	·	3	3	12	8	2	3	·	–
IX	18	2.8	9	2.5	3	1.3	4	2.8	24.5	3.1	15.5	3.5	4	1.8	12	3.4	·	3.0	60	20.4	18	·	·	·	1	·	·	5	6	13	10	2	7	·	–
X	35	2.5	13.5	1.8	1	2.0	14	2.3	19.5	3.4	7.5	3.7	0.5	1.0	1	2.0	1	2.6	7	2.2	20	·	·	3	·	·	·	14	6	7	3	·	6	·	–
XI	21.5	3.2	4.5	2.0	·	·	15	3.2	38.5	4.6	6.5	5.0	1	1.0	3	3.8	·	3.9	103	17.6	23	·	8	16	·	1	·	·	23	18	14	4	16	11	–
XII	30	4.0	3	2.5	·	·	4.5	2.1	36.5	4.3	9	3.5	2	1.5	6	3.8	2	3.8	56	16.1	30	12	27	31	·	4	·	1	23	18	11	2	8	31	–
Rok	318.5	3.6	89.5	2.4	8	0.8	80	2.5	319.5	3.8	122	3.5	28.5	2.2	120	4.4	9	3.6	1018	45.1	18.VII	28	91	148	13	35	6	30	172	195	142	30	91	142	–

Wysowa $\varphi = 49°26'$ $\lambda = 21°11'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	−1.0	−6.3	5.5	23	−16.4	31	−4.6	−2.3	−3.9	−3.7	–	–	–	–	–	–	–	–	–	–	–	–	86	75	89	83
II	–	–	–	–	−1.1	−8.7	4.0	13	−22.2	25	−5.1	−2.5	−4.4	−4.1	–	–	–	–	–	–	–	–	–	–	–	–	96	80	84	87
III	–	–	–	–	0.4	−7.1	10.3	6	−16.7	21	−4.2	−0.8	−3.4	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	85	79	75	80
IV	–	–	–	–	14.2	2.4	26.1	23	−5.2	30	6.5	12.3	6.2	7.8	–	–	–	–	–	–	–	–	–	–	–	–	59	61	50	57
V	–	–	–	–	15.0	4.1	22.8	8	−5.1	2	9.0	13.2	7.8	9.4	–	–	–	–	–	–	–	–	–	–	–	–	71	80	53	68
VI	–	–	–	–	17.2	6.5	27.3	23	0.2	9	11.9	15.4	10.5	12.1	–	–	–	–	–	–	–	–	–	–	–	–	55	80	62	66
VII	–	–	–	–	19.5	8.2	28.4	27	2.7	30	13.4	18.2	11.9	13.8	–	–	–	–	–	–	–	–	–	–	–	–	57	65	50	57
VIII	–	–	–	–	22.5	9.0	28.2	13, 15	1.6	31	14.3	21.1	13.3	15.5	–	–	–	–	–	–	–	–	–	–	–	–	47	58	34	46
IX	–	–	–	–	17.2	4.7	26.4	5	−2.0	27	8.0	15.7	9.3	10.6	–	–	–	–	–	–	–	–	–	–	–	–	51	52	41	48
X	–	–	–	–	13.2	0.5	20.3	4	−6.1	16	3.2	12.5	3.9	5.9	–	–	–	–	–	–	–	–	–	–	–	–	61	35	27	41
XI	–	–	–	–	6.7	1.1	17.6	3	−9.3	28	3.0	5.3	3.7	3.9	–	–	–	–	–	–	–	–	–	–	–	–	84	87	82	84
XII	–	–	–	–	−3.6	−9.6	2.3	8	−23.2	21	−7.1	−4.9	−6.6	−6.3	–	–	–	–	–	–	–	–	–	–	–	–	93	76	91	87
Rok	–	–	–	–	10.0	0.4	28.4	27. VII	−23.2	21. XII	4.0	8.6	4.0	5.2	–	–	–	–	–	–	–	–	–	–	–	–	70	69	62	67

Barwinek $\varphi = 49°26'$ $\lambda = 21°41'$

I	–	–	–	–	−0.7	−6.1	3.0	1, 23	−15.4	16	−3.8	−2.0	−3.4	−3.2	–	–	–	–	–	–	–	–	–	–	–	–	95	84	87	89
II	–	–	–	–	−1.2	–	3.2	27	–	–	−5.6	−2.4	−4.4	−4.2	–	–	–	–	–	–	–	–	–	–	–	–	93	90	87	90
III	–	–	–	–	0.7	–	12.0	6	–	–	−4.1	−0.6	−3.4	−2.9	–	–	–	–	–	–	–	–	–	–	–	–	89	83	80	84
IV	–	–	–	–	14.4	1.5	25.1	23	−5.4	30	6.1	13.1	5.9	7.8	–	–	–	–	–	–	–	–	–	–	–	–	60	66	47	58
V	–	–	–	–	15.3	4.1	23.2	28	−6.2	2	9.3	13.5	8.6	10.0	–	–	–	–	–	–	–	–	–	–	–	–	79	82	68	76
VI	–	–	–	–	17.3	6.3	27.2	24	0.4	14	11.8	15.7	10.3	12.0	–	–	–	–	–	–	–	–	–	–	–	–	61	74	72	69
VII	–	–	–	–	19.0	7.9	28.1	27	2.7	30	13.3	18.2	11.7	13.7	–	–	–	–	–	–	–	–	–	–	–	–	67	65	61	64
VIII	–	–	–	–	22.3	9.1	27.9	13	0.7	31	13.9	20.9	14.3	15.8	–	–	–	–	–	–	–	–	–	–	–	–	62	63	52	59
IX	–	–	–	–	16.7	5.1	25.6	5	−1.2	15	9.4	15.5	10.4	11.4	–	–	–	–	–	–	–	–	–	–	–	–	65	62	58	62
X	–	–	–	–	12.9	0.3	20.8	3	−7.4	16	3.1	12.1	4.4	6.0	–	–	–	–	–	–	–	–	–	–	–	–	55	42	33	43
XI	–	–	–	–	7.2	0.9	17.7	1	−7.5	28	3.4	5.8	3.8	4.2	–	–	–	–	–	–	–	–	–	–	–	–	88	86	81	85
XII	–	–	–	–	−3.5	−8.6	2.5	14	−19.3	4	−6.2	−5.2	−6.2	−6.0	–	–	–	–	–	–	–	–	–	–	–	–	93	89	91	91
Rok	–	–	–	–	10.0	–	28.1	27. VII	–	–	4.2	8.7	4.3	5.4	–	–	–	–	–	–	–	–	–	–	–	–	76	74	68	73

Myczkowce $\varphi = 49°26'$ $\lambda = 22°25'$

I	–	–	–	–	2.7	−3.2	8.9	22	−13.6	31	−1.3	1.6	−0.6	−0.2	–	–	–	–	–	–	–	–	–	–	–	–	66	68	72	69
II	–	–	–	–	0.1	−7.4	4.1	27	−19.9	25	−5.2	−1.4	−3.1	−3.2	–	–	–	–	–	–	–	–	–	–	–	–	86	85	82	84
III	–	–	–	–	2.8	−5.7	17.9	5	−19.1	19	−3.3	1.4	−1.6	−1.3	–	–	–	–	–	–	–	–	–	–	–	–	85	86	70	80
IV	–	–	–	–	17.3	3.9	27.7	24	−4.8	2	6.6	15.2	9.1	10.0	–	–	–	–	–	–	–	–	–	–	–	–	50	57	37	48
V	–	–	–	–	17.0	6.8	26.3	28	−4.0	2	9.1	15.0	10.6	11.4	–	–	–	–	–	–	–	–	–	–	–	–	76	71	66	71
VI	–	–	–	–	18.4	8.4	29.2	16	2.2	7	10.9	16.8	12.7	13.3	–	–	–	–	–	–	–	–	–	–	–	–	68	79	72	73
VII	–	–	–	–	20.4	9.7	30.0	27	5.2	9	12.4	18.3	13.3	14.3	–	–	–	–	–	–	–	–	–	–	–	–	70	68	53	64
VIII	–	–	–	–	23.4	11.7	29.7	7	3.6	31	14.0	21.8	15.9	16.9	–	–	–	–	–	–	–	–	–	–	–	–	71	56	44	57
IX	–	–	–	–	18.3	6.4	26.8	5	0.7	27	8.6	16.6	10.9	11.8	–	–	–	–	–	–	–	–	–	–	–	–	59	58	41	53
X	–	–	–	–	14.8	1.8	21.6	4	−4.5	17	3.4	13.9	5.7	7.2	–	–	–	–	–	–	–	–	–	–	–	–	53	38	26	39
XI	–	–	–	–	9.8	1.5	20.9	1	−5.3	18	3.1	8.0	4.3	4.9	–	–	–	–	–	–	–	–	–	–	–	–	89	81	74	81
XII	–	–	–	–	−1.5	−8.4	7.6	14	−15.3	23	−5.5	−2.8	−5.1	−4.6	–	–	–	–	–	–	–	–	–	–	–	–	82	84	71	79
Rok	–	–	–	–	12.0	2.1	30.0	27. VII	−19.9	25. II	4.4	10.4	6.0	6.7	–	–	–	–	–	–	–	–	–	–	–	–	71	69	59	66

Żegiestów-Zdrój $\varphi = 49°22'$ $\lambda = 20°49'$

I	–	–	–	–	1.0	−4.9	7.6	20	−15.1	31	−3.4	−0.2	−2.7	−2.2	–	–	–	–	–	–	–	–	–	–	–	–	82	69	83	78
II	–	–	–	–	0.5	−7.0	7.0	13	−18.6	25	−5.1	−1.0	−3.1	−3.1	–	–	–	–	–	–	–	–	–	–	–	–	96	85	93	91
III	–	–	–	–	1.8	−5.0	12.8	5	−15.6	9	−3.6	1.0	−2.1	−1.7	–	–	–	–	–	–	–	–	–	–	–	–	92	85	88	88
IV	–	–	–	–	14.9	3.0	26.8	23	−4.1	2	4.9	13.4	7.6	8.4	–	–	–	–	–	–	–	–	–	–	–	–	68	68	59	65
V	–	–	–	–	15.7	5.5	23.2	28	−3.3	2	7.8	13.7	9.0	9.9	–	–	–	–	–	–	–	–	–	–	–	–	89	88	74	84
VI	–	–	–	–	17.8	8.1	29.1	24	1.8	5	10.0	15.8	11.9	12.4	–	–	–	–	–	–	–	–	–	–	–	–	87	78	74	80
VII	–	–	–	–	20.6	9.7	29.7	27	4.9	30	11.9	19.2	13.4	14.5	–	–	–	–	–	–	–	–	–	–	–	–	69	59	61	63
VIII	–	–	–	–	23.5	10.8	31.0	15	3.2	31	12.4	22.0	15.2	16.2	–	–	–	–	–	–	–	–	–	–	–	–	89	40	41	57
IX	–	–	–	–	17.9	5.6	27.5	5, 12	0.9	15	7.6	16.7	10.2	11.2	–	–	–	–	–	–	–	–	–	–	–	–	79	40	45	55
X	–	–	–	–	14.7	1.8	22.3	3	−3.6	22, 23	3.5	13.9	5.4	7.0	–	–	–	–	–	–	–	–	–	–	–	–	92	35	40	56
XI	–	–	–	–	7.5	1.2	17.5	3	−4.3	17	3.6	5.9	4.0	4.4	–	–	–	–	–	–	–	–	–	–	–	–	83	74	82	80
XII	–	–	–	–	−3.2	−10.6	2.4	14	−19.7	22	−7.0	−5.1	−7.0	−6.5	–	–	–	–	–	–	–	–	–	–	–	–	85	78	78	80
Rok	–	–	–	–	11.1	1.5	31.0	15. VIII	−19.7	22. XII	3.6	9.6	5.2	5.9	–	–	–	–	–	–	–	–	–	–	–	–	84	67	68	73

UWAGA. W dniu 23.VI.1962 r. stacja została przeniesiona do sanatorium „Wiktor". Współrzędne geograficzne pozostają bez zmiany, wartość $H_s = 450$ m.

Wysowa — $H_s = 525m$ — $h_w = 25{,}5m$ — 1962

MIESIĄC	ROZKŁAD WIATRU (°D, °mD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	≥15	●	●	Opad R ≥0,1	≥1,0	≥10,0	■	■	■ ≥10
I	25	5.2	·	·	·	·	25.5	5.9	31.5	5.7	1	1.0	1	1.0	22.5	5.0	9	4.9	44	10.7	27	4	19	30	·	5	·	·	22	18	11	1	7	31	·
II	5.5	7.5	·	·	·	·	16	4.0	10	7.2	·	·	2.5	4.6	40	6.9	10	5.5	64	12.6	19	12	16	27	·	8	1	·	20	20	13	1	2	28	·
III	9	6.3	0.5	4.0	0.5	4.0	25.5	5.8	7.5	5.3	·	·	·	·	33	5.4	17	4.7	57	8.8	15	10	16	28	·	8	·	1	17	23	12	·	5	31	·
IV	6	3.3	1.5	2.0	1	2.0	14	4.3	21.5	4.7	2	3.0	0.5	3.0	25.5	3.9	18	3.3	50	13.7	28	·	·	7	2	4	·	7	8	12	10	1	3	6	·
V	9	2.4	·	·	·	·	7.5	3.5	20.5	2.7	4	1.4	2.5	5.0	28.5	3.3	21	2.3	116	23.0	9	·	·	6	·	·	·	1	9	25	19	2	2	·	3
VI	15	4.5	0.5	1.0	·	·	5.5	2.8	3.5	1.6	3.5	2.6	4.5	2.7	36.5	4.3	21	3.0	210	43.2	17	·	·	·	4	1	·	4	10	17	14	6	·	·	5
VII	8	3.1	3.5	3.3	1.5	3.7	11	4.3	6.5	2.5	4.5	2.2	2.5	3.6	23.5	3.0	32	2.1	148	47.0	18	·	·	·	3	·	·	4	6	18	15	5	3	·	8
VIII	8	2.2	·	·	3	1.7	12	3.8	9	4.0	·	·	2	3.0	19	3.5	40	1.9	59	12.4	16	·	·	·	8	2	·	5	2	14	10	2	2	·	6
IX	3.5	2.3	0.5	2.0	1	4.5	20	4.1	10.5	3.6	3	1.3	5	2.0	22.5	3.5	24	2.5	55	14.1	17	·	·	5	1	·	·	8	4	15	12	2	3	·	1
X	9.5	2.2	1.5	2.0	1.5	3.3	20.5	3.8	8.5	1.9	·	·	1	2.0	20.5	3.0	30	2.0	9	2.2	19	·	·	11	·	·	·	11	3	11	4	·	9	·	·
XI	1.1	3.0	·	·	·	·	3.4	4.8	2.0	5.4	·	·	·	·	1.8	3.0	7	4.0	11.5	23.1	15	·	2	14	·	2	·	1	19	20	15	5	2	12	·
XII	1.2	5.8	·	·	·	·	25.5	5.6	1.4	5.1	0.5	1.0	1	1.0	1.9	5.2	21	4.1	4.5	12.4	30	13	23	31	·	4	·	·	23	20	8	2	4	31	·
Rok	9.9	4.0	8	1.2	8.5	1.6	21.7	4.4	16.3	4.1	18.5	1.0	22.5	2.3	308.5	4.2	250	3.4	97.2	47.0	18.VII	39	76	159	18	34	1	42	143	213	143	27	47	139	23

Barwinek — $H_s = 420m$ — $h_w = 16m$

I	9.5	4.3	0.5	5.0	·	·	2	2.8	5.1	3.6	1.5	2.9	1.5	1.3	13.5	2.7	·	3.4	53	12.2	13	4	14	29	·	·	·	·	21	16	12	1	–	–	–
II	16	3.0	2	4.0	1	2.0	0.5	5.0	19.5	4.1	1.0	2.1	1	7.0	31	4.0	3	3.5	102	18.0	16	–	17	–	·	·	·	·	23	20	14	6	–	–	–
III	28.5	3.4	·	·	·	·	0.5	2.0	25.5	3.3	1.1	2.9	·	·	27.5	3.0	·	3.2	100	16.9	7	–	14	–	·	·	·	·	21	25	18	4	–	31	–
IV	17.5	2.0	1.5	1.0	1	2.0	5	2.6	3.6	3.7	5	1.2	2	2.0	21	3.1	1	2.9	50	8.9	27	·	·	9	1	1	·	4	7	16	10	·	–	–	–
V	16	2.3	2	1.2	2.5	1.2	3	2.2	23	2.7	24.5	2.0	·	·	22	2.0	·	2.2	117	24.1	20	·	·	6	·	·	·	·	15	25	19	3	–	·	–
VI	26.5	2.3	3	3.3	·	·	2	3.2	11	2.0	9.5	1.8	3.5	2.3	34.5	2.8	·	2.4	128	27.1	4	·	·	·	4	·	·	2	11	17	14	4	–	·	–
VII	21	2.2	5.5	1.5	1	3.0	5	2.1	19	2.8	6	2.5	7	2.3	28.5	2.0	·	2.2	96	23.0	27	·	·	·	3	·	·	2	11	18	14	3	–	·	–
VIII	3.2	1.9	·	·	·	·	3.5	2.1	21.5	3.0	5	2.2	5.5	1.5	22.5	2.6	3	2.2	83	34.6	6	·	·	·	8	·	·	2	6	14	11	2	–	·	–
IX	14.5	1.7	0.5	1.0	1	3.0	7	3.3	25	4.0	11	1.8	6	1.4	25	1.6	·	1.9	89	19.3	7	·	·	5	1	·	·	3	10	16	10	3	–	·	–
X	36.5	2.0	1	2.0	·	·	2.5	1.2	26	2.4	11	1.3	2	1.5	14	1.6	·	1.9	3	0.7	15	·	·	14	·	·	·	9	4	11	·	·	–	·	–
XI	17	2.8	1	3.0	3	1.0	4.5	3.0	47	3.3	7.5	1.8	2	1.5	8	2.9	·	2.9	117	26.1	23	·	1	14	·	·	·	·	21	21	15	3	–	13	–
XII	33.5	3.4	·	·	·	·	2.5	2.8	34.5	6.9	9	2.2	·	·	13.5	3.1	·	4.5	62	16.1	14	12	24	31	·	3	1	1	28	26	10	2	–	31	–
Rok	268.5	2.6	17	1.8	9.5	1.0	38	2.7	33.9	3.5	124.5	2.1	30.5	1.7	261	2.6	7	2.8	1000	34.6	6.VIII	–	70	–	17	4	1	23	178	225	147	31	–	–	–

Myczkowce — $H_s = 410m$ — $h_w = 20{,}5m$

I	·	·	6	4.5	·	·	1	5.0	3	4.0	4.7	4.1	6	5.7	5	6.8	2.5	3.3	–	–	–	2	6	22	·	·	·	2	12	–	–	–	–	15	–
II	·	·	4	2.2	1	3.0	2	2.0	7	4.9	9	6.6	7	7.1	19	5.8	3.5	3.2	–	–	–	7	10	27	·	1	1	·	17	–	–	–	–	28	–
III	1	2.0	6	4.2	5	2.6	7	3.0	4	3.5	14	3.6	2	4.5	22	4.8	3.2	2.6	–	–	–	7	9	25	·	·	·	·	17	–	–	–	–	31	–
IV	·	·	5	3.2	1	1.0	12	2.9	7	4.0	7	4.3	2	3.0	29	3.8	2.7	2.5	–	–	–	·	·	4	6	·	·	8	3	–	–	–	–	·	–
V	2	2.0	2	2.0	·	·	4	2.5	3	2.3	10	3.5	12	4.8	22	3.2	3.8	2.0	–	–	–	·	·	3	1	·	·	·	9	–	–	–	–	·	–
VI	3	2.3	1	2.0	·	·	·	·	2	2.0	7.5	3.4	7	3.8	22.5	3.2	4.7	1.5	181²	48.5²	20²	·	·	·	8	·	·	1	12	17	15	5	–	·	–
VII	7	2.6	1.5	1.3	2.5	2.8	0.5	3.0	12	2.4	9.5	3.2	13.5	3.1	14.5	3.0	3.2	1.9	113	43.9	19	·	·	·	4	·	·	5	11	17	13	4	–	·	–
VIII	1	3.5	1.5	1.7	1.5	2.0	6.5	1.9	4.5	2.3	9.5	1.6	16	3.8	10.5	3.7	4.2	1.6	81	24.6	5	·	·	·	12	1	·	2	5	15	12	2	–	·	–
IX	0.5	1.0	1.5	1.0	1	1.0	5	1.0	8.5	3.5	8.5	3.4	8	2.6	9	2.6	4.8	1.2	59	8.7	22	·	·	·	2	·	·	5	9	11	11	·	–	·	–
X	3.5	1.9	3.5	2.1	2	1.5	0.5	3.0	4.5	2.6	3	4.7	6	3.2	9	3.7	6.1	1.0	2	0.9	20	·	·	10	·	·	·	10	5	5	·	·	–	·	–
XI	0.5	1.0	2.5	1.0	8	2.4	6.5	3.2	6.5	4.3	4	4.6	2.5	3.8	3.5	3.6	5.6	1.3	7.3	19.9	16	·	·	10	·	1	·	1	20	19	14	2	–	5	–
XII	4.5	3.7	8	2.5	4.5	2.1	6	3.5	15.5	4.3	5.5	3.3	2	6.0	3	3.7	4.4	1.9	51	13.7	30	12	16	31	·	1	·	2	20	17	11	3	–	31	–
Rok	2.3	1.7	42.5	2.3	26.5	1.5	5.1	2.6	77.5	3.3	134.5	3.9	8.4	4.3	16.9	4.0	48.7	2.0	–	48.5²	20.VI²	28	41	132	33	4	1	36	140	–	–	–	–	110	–

Żegiestów-Zdrój — $H_s = 440m$ — $h_w = 16{,}1m$ I–VIII, $h_w = 18{,}4m$ IX–XII

I	7.5	1.7	8.5	2.5	2	2.8	6	2.2	15.5	3.1	7.5	1.9	21.5	2.0	9.5	2.1	1.5	1.9	44	10.5	27	4	9	28	·	·	·	2	19	15	10	1	·	31	–
II	7	1.8	4	2.4	·	·	2	3.5	7	2.7	2.5	2.6	49.5	3.2	7	2.1	5	2.7	93	15.3	19	5	10	26	·	·	·	·	23	19	13	4	·	28	–
III	10.5	2.2	6.5	2.5	6.5	2.4	2.5	2.8	10.5	2.3	4.5	2.1	37.5	2.5	4.5	2.3	1.0	2.2	60	14.1	16	2	10	26	·	·	·	1	26	19	11	1	1	31	–
IV	5.5	1.6	12.5	1.9	8	2.5	4	3.6	11.5	3.6	3.5	2.9	21.5	2.9	5.5	2.6	1.8	2.2	68	25.9	6	·	·	5	4	·	·	5	14	14	8	2	3	6	–
V	7	2.0	12.5	1.7	1.5	2.3	2	2.5	8	3.4	4.5	3.2	3.7	2.4	6.5	1.7	1.4	2.0	86	14.5	9	·	·	4	·	·	·	·	20	20	16	2	3	·	–
VI	3	1.3	9	2.4	·	·	2	3.0	6	2.3	5	2.6	38.5	2.5	4.5	2.7	2.2	1.9	21.5	58.4	5	·	·	·	7	·	·	1	18	19	13	7	7	·	–
VII	3	3.3	1	3.0	·	·	4	2.8	·	·	6	3.0	·	·	1	4.0	7.8	0.5	86	27.4	18	·	·	·	6	·	·	4	11	14	10	3	8	·	–
VIII	·	·	1	2.0	·	·	1	2.0	·	·	2	2.0	·	·	6	4.5	8.3	0.4	42	14.9	3	·	·	·	10	·	·	·	8	10	5	2	21	·	–
IX	2.5	1.2	·	·	·	·	·	·	·	·	7	2.6	2	3.5	4.5	1.8	7.4	0.4	61	18.6	18	·	·	·	2	·	·	2	6	8	7	3	14	·	–
X	1.2	1.5	·	·	1	1.0	·	·	2	1.0	·	·	3	1.0	1	1.0	7.4	0.3	1	0.4	15	·	·	11	·	·	·	1	7	3	·	·	22	·	–
XI	7	2.3	10	1.8	2	1.5	3	2.0	2	3.0	5	1.6	1	1.0	1	1.0	5.9	0.8	121²	25.0	23	·	2	13	·	1	·	·	14	18	14	7	9	13	–
XII	7	3.1	3	3.0	1	2.0	·	·	·	·	·	·	1.1	3.1	8	2.1	6.3	0.9	65²	25.7	31	1.5	2.3	31	·	·	·	1	20	15	6	2	7	31	–
Rok	7.2	1.8	6.8	1.9	2.2	1.2	2.6.5	2.4	6.2.5	1.8	4.7.5	2.0	22.2.5	2.0	5.9	2.3	5.1.5	1.4	94.2²	58.4	5.VI	2.6	5.4	1.4.4	2.9	1	·	1.7	1.8.6	1.7.4	1.1.3	3.4	9.5	1.4.0	–

Bukowina Tatrzańska $\varphi = 49°21'$ $\lambda = 20°07'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	P_{0m}	— Max	— Min	Max obs.	Data	Min obs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.2	–5.9	5.9	1.1	–16.2	31	–3.6	–2.1	–3.2	–3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.2	6.2	6.5
II	–	–	–	–	–2.1	–8.2	6.4	12	–17.1	26	–7.1	–4.3	–4.9	–5.3	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.2	8.6	8.5
III	–	–	–	–	–0.7	–7.0	12.4	5	–13.0	17	–5.5	–2.4	–4.3	–4.1	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.7	6.5	7.4
IV	–	–	–	–	11.0	3.3	21.9	23	–3.3	8	5.8	9.1	6.1	6.8	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.9	5.0	6.0
V	–	–	–	–	11.8	4.0	19.0	19	–4.8	2	6.7	9.4	7.4	7.7	–	–	–	–	–	–	–	–	–	–	–	–	7.2	8.2	6.4	7.3
VI	–	–	–	–	14.0	6.8	25.3	24	–0.3	7	9.7	12.2	9.9	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.6	7.1	7.0
VII	–	–	–	–	17.0	9.1	25.8	27	3.8	5	11.6	15.2	12.4	12.9	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.8	6.2	6.2
VIII	–	–	–	–	20.2	11.2	28.0	15	4.8	31	14.0	18.4	14.7	15.4	–	–	–	–	–	–	–	–	–	–	–	–	4.6	6.0	3.8	4.8
IX	–	–	–	–	14.9	5.9	25.0	12	0.4	25	8.1	13.0	9.6	10.1	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.7	3.4	4.7
X	–	–	–	–	11.5	3.9	18.2	4	–1.8	16	5.2	10.7	6.5	7.2	–	–	–	–	–	–	–	–	–	–	–	–	3.3	4.0	2.7	3.3
XI	–	–	–	–	5.3	–0.2	14.6	8	–6.7	18	1.3	3.8	1.8	2.2	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.8	8.1	7.8
XII	–	–	–	–	–3.8	–9.8	4.4	7	–20.9	23	–7.4	–5.5	–7.0	–6.7	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.6	6.6	6.7
Rok	–	–	–	–	8.3	1.1	28.0	15. VIII	–20.9	23. XII	3.2	6.5	4.1	4.5	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.8	5.9	6.4

Muszyna $\varphi = 49°21'$ $\lambda = 20°53'$

I	963.9	976.1	944.5	1019.9	0.9	–5.7	6.8	20	–15.9	16	–3.8	–0.5	–2.9	–2.5	4.3	4.4	4.2	4.3	88	74	83	82	0.6	1.7	0.9	1.1	8.6	6.5	7.5	7.5
II	961.2	977.2	934.3	1017.2	0.3	–7.8	6.8	13	–20.4	25	–5.5	–1.5	–3.7	–3.6	3.6	4.1	4.0	3.9	86	74	84	81	0.6	1.5	0.8	1.0	9.4	8.3	8.4	8.7
III	955.9	972.3	940.6	1011.3	1.8	–5.8	13.2	5	–16.6	21	–3.8	0.7	–2.4	–2.0	4.3	4.6	4.5	4.5	86	68	84	79	0.7	2.1	0.8	1.2	8.6	8.1	7.9	8.2
IV	960.9	972.9	936.9	1014.7	14.8	2.4	25.6	23	–4.5	2	4.9	13.3	7.1	8.1	7.5	7.5	8.1	7.7	86	54	80	73	1.5	9.2	2.4	4.4	6.1	6.3	4.6	5.7
V	960.5	967.4	949.5	1013.8	15.7	5.0	22.6	8	–4.2	2	7.6	13.6	8.9	9.8	9.6	9.8	10.0	9.8	88	62	86	79	1.3	6.3	1.7	3.1	7.6	7.9	5.2	6.9
VI	965.2	972.9	956.2	1018.4	17.7	7.3	28.6	24	1.8	5	9.8	15.7	11.6	12.2	11.2	11.4	12.5	11.7	90	63	87	80	1.3	8.1	1.8	3.7	7.4	8.0	7.0	7.5
VII	962.6	972.6	950.9	1015.3	20.2	9.1	29.6	27	4.1	30	11.7	19.0	13.2	14.3	12.5	12.4	13.6	12.8	91	56	89	79	1.4	10.1	1.8	4.4	7.0	6.8	5.3	6.4
VIII	964.6	970.6	955.9	1017.0	23.6	10.2	30.7	15	1.9	31	12.0	22.2	15.2	16.2	13.3	14.2	15.0	14.2	94	53	86	78	1.0	13.2	2.6	5.6	7.1	5.8	3.8	5.6
IX	964.6	974.7	952.9	1018.0	18.3	5.0	27.2	5	0.7	26	7.0	16.8	9.9	10.9	9.5	10.7	10.8	10.3	94	57	88	80	0.9	9.2	1.8	4.0	7.9	6.2	3.7	5.9
X	968.8	980.4	955.8	1023.3	15.1	1.3	21.9	3, 4	–4.4	22	2.4	13.9	5.1	6.6	7.1	9.1	8.2	8.1	96	58	91	82	0.4	7.2	0.8	2.8	8.9	3.7	2.5	5.0
XI	962.8	976.8	949.7	1017.3	7.9	1.3	17.5	3	–4.0	28	3.2	6.8	4.2	4.6	7.1	7.5	7.5	7.4	90	75	89	85	0.9	3.2	1.1	1.7	8.0	7.8	8.1	8.0
XII	961.9	988.2	924.6	1018.6	–3.0	–10.0	3.5	14	–19.4	22	–6.9	–4.4	–6.5	–6.1	3.2	3.5	3.3	3.3	83	76	82	80	0.7	1.1	0.7	0.8	9.3	7.8	9.0	8.7
Rok	962.7	988.2	924.6	1017.0	11.1	1.0	30.7	15. VIII	–20.4	25. II	3.2	9.6	5.0	5.7	7.8	8.3	8.5	8.2	89	64	86	80	0.9	6.1	1.4	2.8	8.0	6.9	6.1	7.0

Witów $\varphi = 49°20'$ $\lambda = 19°50'$

I	–	–	–	–	1.0	–7.1	8.0	22	–17.2	10	–4.7	–0.8	–3.6	–3.2	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.0	6.2	6.6
II	–	–	–	–	–1.5	–10.0	4.0	13	–22.6	26	–7.9	–3.3	–5.7	–5.6	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.2	8.6	8.6
III	–	–	–	–	–0.2	–8.4	14.1	5	–17.9	21, 26	–6.4	–1.4	–4.9	–4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.7	8.0	7.9
IV	–	–	–	–	11.3	1.7	22.2	23	–4.3	3	4.8	9.8	5.1	6.2	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.5	5.1	6.4
V	–	–	–	–	12.2	3.5	19.1	8, 31	–5.0	2	7.0	10.3	7.0	7.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	8.4	6.4	7.4
VI	–	–	–	–	15.0	5.5	26.8	24	–0.2	7	9.9	13.6	9.0	10.4	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.1	6.7	7.4
VII	–	–	–	–	17.7	7.4	27.7	27	2.0	5	11.8	16.2	11.3	12.6	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.5	6.6	6.9
VIII	–	–	–	–	21.1	8.9	27.9	15	2.8	31	13.5	19.9	13.4	15.0	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.9	4.6	5.6
IX	–	–	–	–	15.5	3.8	24.8	4	–2.2	25	6.9	13.9	8.0	9.2	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.0	4.4	5.2
X	–	–	–	–	12.2	1.0	19.1	3	–2.8	17, 24	2.4	11.7	4.2	5.6	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.9	3.4	4.3
XI	–	–	–	–	5.5	–0.8	15.3	8	–7.3	17	0.9	4.2	1.6	2.1	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.3	8.1	8.2
XII	–	–	–	–	–2.6	–12.3	6.0	9	–26.4	22	–8.9	–4.3	–8.4	–7.5	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.0	5.7	6.7
Rok	–	–	–	–	8.9	–0.6	27.9	15. VIII	–26.4	22. XII	2.4	7.5	3.1	4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.2	6.2	6.8

Poronin $\varphi = 49°20'$ $\lambda = 20°02'$

I	–	–	–	–	1.1	–9.6	6.5	21, 25	–21.3	31	–6.0	–0.4	–4.8	–4.0	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.9	6.5	6.2
II	–	–	–	–	–0.7	–11.4	6.5	12	–27.3	26	–8.4	–3.1	–5.7	–5.7	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.0	8.2	8.2
III	–	–	–	–	0.7	–10.0	13.5	5	–23.2	9	–6.6	–0.7	–5.4	–4.5	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.6	6.5	7.4
IV	–	–	–	–	11.7	–0.4	22.7	23	–10.7	3	3.7	10.4	3.7	5.4	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.5	4.3	5.5
V	–	–	–	–	12.3	2.0	19.5	28	–7.9	3	6.7	10.5	6.7	7.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	8.4	5.8	7.1
VI	–	–	–	–	15.4	3.9	27.3	24	–1.4	9	9.2	13.3	8.7	10.0	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.9	7.0	7.5
VII	–	–	–	–	17.9	5.7	26.8	27	–1.1	5	11.0	16.2	10.8	12.2	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.8	6.5	7.0
VIII	–	–	–	–	21.3	6.8	28.7	15	–1.1	31	11.6	19.7	12.4	14.0	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.0	4.5	5.2
IX	–	–	–	–	16.1	1.4	25.4	12	–4.4	25	5.0	14.3	7.3	8.5	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.8	4.7	5.3
X	–	–	–	–	13.2	–2.1	20.1	3	–5.9	17, 24, 25	0.1	12.3	2.5	4.4	–	–	–	–	–	–	–	–	–	–	–	–	3.6	4.5	2.9	3.7
XI	–	–	–	–	6.5	–1.7	16.7	7	–12.0	17	–0.2	4.8	1.2	1.8	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.3	8.0	8.2
XII	–	–	–	–	–3.0	–15.0	5.7	13	–30.9	22	–10.5	–4.6	–9.8	–8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.2	5.7	6.5
Rok	–	–	–	–	9.4	–2.5	28.7	15. VIII	–30.9	22. XII	1.3	7.7	2.3	3.4	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.0	5.9	6.5

Bukowina Tatrzańska $H_s = 880\ m$ $h_w = 16\ m$ 1962

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◔	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R
I	2	3.8	1.5	4.3	1.5	3.0	·	·	4	2.0	33.5	4.9	18.5	5.2	2	2.2	30	3.1	—	—	—	4	13	29	·	2	·	4	13	—	—	—	1	31	·
II	·		·	·	1	2.0	1	3.0	0.5	2.0	21.5	6.1	24	6.7	5	7.9	31	4.0	—	—	—	7	19	28	·	6	3	·	18	—	—	—	1	28	·
III	5.5	1.9	5.5	2.9	3.5	2.6	1	1.5	2	1.5	15	4.3	17.5	4.6	8	3.0	35	2.2	41	7.0	16	10	18	29	·	1	·	2	17	17	11	·	·	31	·
IV	6	3.0	3	1.3	3.5	2.7	3.5	4.6	2.5	2.4	17.5	3.4	12	4.8	13	3.0	29	2.3	61	27.7	6	·	·	8	·	1	·	6	10	14	9	1	3	17	·
V	4	2.1	1	3.0	2.5	1.8	5.5	3.4	3.5	1.9	27.5	4.1	21	3.8	10	3.2	18	2.8	113	22.9	20	·	·	4	·	2	·	2	12	26	19	3	3	2	3
VI	5	2.4	4	2.6	3	2.8	2	2.5	2.5	2.2	31.5	3.1	23	4.4	6	4.2	13	3.0	188	31.4	4	·	·	1	1	2	·	1	14	17	14	5	1	2	6
VII	4.5	2.2	3	2.0	2	2.0	1	1.0	2	2.0	22.5	2.6	30	3.2	9	2.9	19	2.2	187	72.8	18	·	·	·	2	·	·	3	8	17	16	3	·	·	6
VIII	6	2.5	0.5	2.0	2	2.5	1.5	4.0	1.5	2.3	29	3.1	22.5	4.8	9	3.1	21	2.8	41	10.3	15	·	·	·	2	·	·	3	3	11	7	1	·	·	4
IX	3	2.0	·	·	3.5	1.9	1.5	3.0	2	4.2	28.5	3.5	17	3.4	5.5	3.3	29	2.2	55	13.5	18	·	·	·	·	1	·	8	8	13	9	2	1	·	·
X	4	2.6	4.5	2.3	3	2.7	1	2.0	·	·	13.5	2.4	11	3.0	11	2.2	45	1.3	9	5.1	31	·	·	1	·	·	·	18	6	4	4	·	2	·	·
XI	2.5	2.0	2.5	2.2	5	2.5	7.5	2.5	2.5	3.6	13	2.3	7	4.0	3	3.0	47	1.3	95	13.5	23	·	8	16	·	·	·	2	19	19	18	4	5	14	·
XII	5.5	2.4	4.5	2.7	4.5	1.8	1.5	1.3	3	2.0	17	3.9	10.5	4.2	6.5	3.8	40	1.9	38	11.2	30	12	22	31	·	·	·	3	13	18	9	1	2	31	·
Rok	48	2.2	30	2.1	35	2.4	27	2.4	26	2.2	270	3.6	214	4.3	88	3.5	357	2.4	—	72.8	18.VII	33	80	147	5	15	3	52	141	—	—	—	19	156	19

Muszyna $H_s = 445\ m$ $H_b = 447{,}1\ m$ $h_w = 12{,}2\ m$

I	3	2.0	11	3.4	1	1.0	4	2.0	5	4.0	19	5.1	8	2.2	4	1.5	38	2.1	38	7.6	27	5	9	28	·	1	·	2	16	15	10	·	1	31	·
II	5	3.4	13	3.0	·	·	1	3.0	1	1.0	22	3.5	6	1.5	2	2.5	34	1.8	74	14.5	19	7	10	26	·		·	·	20	20	12	2	·	28	·
III	8	2.2	22	2.9	·	·	3	1.7	4	1.8	19	3.6	6	1.5	2	2.0	29	1.9	40	7.3	12	7	12	25	·	·	·	1	22	19	9	·	1	31	·
IV	10	1.8	13	2.4	·	·	3	2.0	2	3.0	29	2.9	2	1.0	1	3.0	30	1.7	53	13.1	6	·	·	6	2	·	·	7	8	12	8	1	·	1	1
V	11	1.3	9	2.7	3	2.0	2	2.0	1	1.0	21	3.8	6	1.2	·	·	40	1.5	90	15.2	9	·	·	4	·	2	·	1	12	19	17	3	2	·	2
VI	9	2.3	9	1.7	2	1.0	1	2.0	1	2.0	21	2.7	10	1.7	1	1.0	36	1.3	238	56.7	20	·	·	·	6	·	·	1	16	22	15	9	5	·	5
VII	7	1.7	13	1.9	·	·	2	1.0	3	1.3	14	2.8	9	1.8	2	2.0	43	1.1	92	22.6	18	·	·	·	5	·	·	2	9	16	12	4	3	·	7
VIII	13	1.7	6	2.8	·	·	3	1.0	3	3.3	20	3.1	5	1.4	2	2.0	41	1.3	37	13.5	16	·	·	·	12	·	·	3	4	12	7	1	13	·	4
IX	2	2.0	9	3.2	1	2.0	1	3.0	2	4.0	10	3.3	7	2.6	2	1.0	56	1.1	58	19.4	18	·	·	·	3	·	·	3	7	12	7	2	10	·	1
X	3	1.7	18	2.0	1	1.0	5	2.0	8	2.1	8	2.6	3	1.0	2	1.5	45	1.0	3	1.0	20	·	·	12	·	·	·	2	7	6	1	·	18	·	·
XI	7	1.9	6	1.3	3	2.7	3	1.7	7	3.7	24	2.6	5	1.6	1	1.0	34	1.5	108	27.7	15	·	3	13	·	·	·	1	19	16	15	3	·	11	·
XII	9	1.8	16	2.1	3	2.3	2	2.5	1	3.0	24	2.7	5	1.0	1	2.0	32	1.5	40	12.7	14	15	22	31	·	·	·	·	24	18	7	2	2	31	·
Rok	87	2.0	145	2.4	14	1.0	30	2.0	38	2.5	231	3.2	72	1.5	20	1.6	458	1.5	871	56.7	20.VI	34	56	145	28	3	·	23	164	187	120	27	55	133	20

Witów $H_s = 835\ m$ $h_w = 16\ m$

I	2	2.8	3	2.5	2	2.0	1.5	1.0	6.5	1.9	27.5	3.4	11	2.9	5.5	2.2	34	1.8	43	10.4	27	12	9	27	·	2	·	1	13	17	7	2	3	31	·
II	6	1.7	3.5	1.3	·	·	3.5	1.0	4	1.4	12	6.8	9	4.9	13	2.7	33	2.2	94	14.8	17	13	19	28	·	5	1	·	20	22	14	3	·	28	·
III	4.5	1.2	14	2.5	1.5	1.7	4	1.1	8	1.8	17	2.8	4	1.9	9	2.4	31	1.5	58	8.4	12	13	18	30	·	1	1	1	19	16	11	·	3	31	·
IV	5	1.4	5.5	2.1	2	1.0	6	2.8	13.5	3.3	19.5	3.1	7	1.6	7.5	2.7	24	1.9	97	47.0	6	·	·	8	·	2	·	5	11	14	11	2	5	14	1
V	3	1.2	5	1.4	0.5	2.0	1.5	1.7	6.5	2.8	22.5	3.4	11	1.8	8	1.1	35	1.5	148	30.6	20	·		4	·	2	1	·	12	25	19	6	2	2	1
VI	6	1.8	5.5	1.6	·	·	4	1.9	6.5	1.8	15	2.2	10.5	3.0	10.5	2.0	32	1.4	193	39.4	4	·	·	1	2	·	·	·	14	17	13	7	·	2	4
VII	7	1.7	3.5	1.6	1	2.0	1	1.0	5.5	2.0	19	2.6	15	1.9	11	1.8	30	1.4	187	81.9	18	·		·	2	·		1	10	17	14	3	1	·	3
VIII	2	2.0	1.5	2.7	·	·	2.5	1.2	10.5	1.7	20	3.2	16.5	3.1	10	2.3	30	1.8	64	28.0	15	·		·	6	2	·	1	3	12	9	2	·	·	4
IX	0.5	2.0	1	1.0	1	2.0	5.5	1.6	8	1.5	20.5	3.1	18.5	2.0	14	1.5	21	1.6	70	17.0	18	·	·	4		3	1	6	5	13	12	3	1	·	1
X	2.5	1.8	2	1.2	1.5	2.7	11	1.7	10	1.7	16	2.3	8.5	1.7	5.5	1.7	36	1.2	20	13.4	6	·		12				11	9	8	3	1	2	·	·
XI	1	1.5	1	1.0	1	1.0	7	2.2	10	2.6	11.5	2.1	9	1.3	2.5	1.2	47	0.9	128	15.4	22	·	8	16	·	2	·	2	21	17	17	6	9	15	·
XII	5	1.1	8	1.8	·	·	6	1.9	9.5	2.2	24.5	3.0	4.5	1.6	5.5	1.1	30	1.5	50	18.4	14	15	17	31	·	2	·	3	10	16	7	2	2	31	·
Rok	44.5	1.7	53.5	1.7	10.5	1.2	53.5	1.6	98.5	2.1	225	3.2	124.5	2.3	102	1.9	383	1.6	1152	81.9	18.VII	53	71	161	10	21	4	31	147	194	137	37	28	154	14

Poronin $H_s = 800\ m$ $h_w = 16\ m$

I	1.5	1.6	·	·	14	1.1	11	1.1	·	·	7	2.8	20	1.8	5.5	1.7	34	1.0	38	10.0	27	15	10	29	·	·	·	4	12	12	9	1	1	31	·
II	·	·	1	1.0	15	1.1	4	1.0	·	-	8.5	2.9	20.5	3.7	6	3.0	29	1.7	66	9.7	14	16	13	28	·	2	·	1	18	20	14	·	1	28	·
III	14	1.1	0.5	1.0	33.5	1.2	1	1.0	1	2.0	10	2.2	14	1.9	3	2.3	16	1.2	62	11.6	16	15	17	28	·	·	·	3	16	15	13	1	1	31	·
IV	7	1.2	·	·	27	1.2	5.5	1.1	6.5	2.7	7	1.8	7	1.3	6	1.6	24	1.1	97	52.0	6	1	·	11	·	·	·	9	9	14	9	2	2	13	1
V	11.5	1.1	4.5	1.0	16	1.1	·	·	6	2.1	15.5	2.0	18.5	1.7	3	1.2	18	1.2	134	28.3	20	·	·	11	·	·		2	12	26	19	5	1	3	2
VI	10	1.0	2.5	1.8	15.5	1.3	1	1.0	9	1.3	10.5	1.3	18.5	1.5	6	1.1	17	1.1	186	34.9	11	·	·	2	3	·	·	3	20	17	14	5	1	2	6
VII	5.5	1.0	2.5	1.0	8	1.1	1	1.0	8	1.0	24	1.2	13	1.8	6	1.0	25	0.9	230	98.4	18	·	·	2	3	·	·	3	14	17	15	5	·	·	5
VIII	5	1.0	4	1.2	8	1.0	·	·	4	1.0	27	1.6	12	2.0	5	1.2	28	1.0	46	11.1	16	·	·	1	6	·	·	8	4	12	8	1	1	·	4
IX	9	1.1	3	1.0	8	1.0	3	1.0	5	1.6	20	1.4	10	1.3	4	1.0	28	0.9	56	14.3	18	·	·	11	1	·	·	9	11	14	11	1	·	·	1
X	19.5	1.0	23.5	1.2	15	1.2	·	·	·		4	2.0	3	1.7	6	1.3	22	0.9	11	3.2	31	·	·	24	·	·	·	17	9	7	4	·	6	·	·
XI	3.5	1.3	25	1.1	8	1.0	2	1.0	4	3.5	4	1.8	3	1.3	3.5	1.0	37	0.8	118	18.5	22	1	6	19	·	·		4	23	20	16	6	4	15	·
XII	14.5	1.0	19	1.2	12	1.7	2	1.0			13	2.4	6	3.2	8.5	1.5	18	1.3	53	19.0	14	24	19	31	·	·	·	4	13	17	11	2	1	31	·
Rok	101	1.0	85.5	1.0	180	1.2	30.5	0.8	43.5	1.3	150.5	2.0	145.5	1.9	62.5	1.5	296	1.1	1097	98.4	18.VII	72	65	197	13	2	·	67	161	191	143	29	19	154	19

Komańcza $\varphi = 49°20'$ $\lambda = 22°04'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnie																	
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-10	-45	6.0	22, 23	-14.5	31	-2.8	-0.6	-2.1	-1.9	–	–	–	–	–	–	–	–	–	–	–	–	88	73	87	83
II	–	–	–	–	-1.1	-9.8	2.6	28	-26.4	25	-6.6	-2.1	-4.4	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	96	92	83	90
III	–	–	–	–	1.1	-7.4	12.0	5	-24.4	21	-4.4	0.0	-2.9	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	94	83	77	85
IV	–	–	–	–	14.9	1.7	25.4	23	-5.7	2	5.2	13.6	6.4	7.9	–	–	–	–	–	–	–	–	–	–	–	–	59	73	39	57
V	–	–	–	–	15.5	4.5	24.2	28	-6.4	2	8.9	14.0	9.0	10.2	–	–	–	–	–	–	–	–	–	–	–	–	73	82	65	73
VI	–	–	–	–	17.5	6.5	27.9	24	-0.3	30	12.2	16.1	10.9	12.5	–	–	–	–	–	–	–	–	–	–	–	–	60	89	68	72
VII	–	–	–	–	19.3	7.7	28.9	27	1.1	9	13.5	18.2	12.3	14.1	–	–	–	–	–	–	–	–	–	–	–	–	65	74	55	65
VIII	–	–	–	–	22.4	9.5	28.1	15	-0.1	31	13.9	21.4	15.1	16.4	–	–	–	–	–	–	–	–	–	–	–	–	57	68	50	58
IX	–	–	–	–	17.4	4.8	26.7	4	-2.2	26	8.4	15.9	10.0	11.1	–	–	–	–	–	–	–	–	–	–	–	–	62	60	39	54
X	–	–	–	–	13.7	-0.5	20.7	4	-7.6	22	2.6	13.0	3.8	5.8	–	–	–	–	–	–	–	–	–	–	–	–	49	33	21	34
XI	–	–	–	–	8.4	0.7	20.3	1	-9.7	18	3.5	7.0	3.7	4.5	–	–	–	–	–	–	–	–	–	–	–	–	96	80	75	84
XII	–	–	–	–	-2.9	-8.2	4.8	14	-17.6	4	-5.9	-4.1	-5.8	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	91	87	83	87
Rok	–	–	–	–	10.4	0.4	28.9	27 VII	-26.4	25. II	4.0	9.4	4.7	5.7	–	–	–	–	–	–	–	–	–	–	–	–	74	74	62	70

Baligród $\varphi = 49°20'$ $\lambda = 22°17'$

I	–	–	–	–	1.9	-3.0	7.7	22	-13.8	31	-1.3	0.7	-0.8	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	78	67	70	72
II	–	–	–	–	-0.4	-8.3	3.8	28	-23.5	25	-5.8	-2.0	-4.0	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	90	84	86	87
III	–	–	–	–	1.7	-6.1	14.8	5	-19.5	20	-3.5	0.5	-2.3	-1.9	–	–	–	–	–	–	–	–	–	–	–	–	91	83	74	83
IV	–	–	–	–	15.6	3.3	25.8	23	-2.9	30	6.3	13.7	7.9	9.0	–	–	–	–	–	–	–	–	–	–	–	–	52	65	42	53
V	–	–	–	–	15.9	5.6	25.1	28	-4.9	2	9.4	14.1	9.7	10.7	–	–	–	–	–	–	–	–	–	–	–	–	67	77	64	69
VI	–	–	–	–	17.6	8.2	27.6	24	1.6	7	11.6	15.8	12.0	12.8	–	–	–	–	–	–	–	–	–	–	–	–	62	77	66	68
VII	–	–	–	–	19.4	9.4	29.8	27	3.9	30	12.5	18.0	13.5	14.4	–	–	–	–	–	–	–	–	–	–	–	–	67	68	54	63
VIII	–	–	–	–	22.6	11.0	28.3	7	3.4	31	13.9	21.2	15.9	16.7	–	–	–	–	–	–	–	–	–	–	–	–	52	61	49	54
IX	–	–	–	–	17.5	6.4	26.2	5	-1.1	26	8.6	16.3	11.1	11.8	–	–	–	–	–	–	–	–	–	–	–	–	50	58	43	50
X	–	–	–	–	14.5	1.1	20.5	3	-5.0	16	3.6	13.7	4.9	6.8	–	–	–	–	–	–	–	–	–	–	–	–	47	37	23	36
XI	–	–	–	–	9.4	1.3	21.8	1	-10.0	18	3.5	7.5	4.3	4.9	–	–	–	–	–	–	–	–	–	–	–	–	88	78	72	79
XII	–	–	–	–	-1.6	-7.5	6.9	14	-15.5	23	-5.2	-3.1	-4.9	-4.5	–	–	–	–	–	–	–	–	–	–	–	–	82	84	81	82
Rok	–	–	–	–	11.2	1.8	29.8	27 VII	-23.5	25. II	4.5	9.7	5.6	6.4	–	–	–	–	–	–	–	–	–	–	–	–	69	70	60	66

Gubałówka $\varphi = 49°18'$ $\lambda = 19°56'$

I	–	–	–	–	1.4	-5.7	7.8	22	-16.8	31	-3.1	-0.7	-2.9	-2.4	4.2	4.1	4.0	4.1	83	70	79	77	0.9	2.0	1.2	1.4	77	65	75	72
II	–	–	–	–	-2.3	-8.5	3.8	12	-17.5	1	-6.9	-3.9	-5.4	-5.4	3.3	3.9	3.8	3.7	89	84	91	88	0.4	0.8	0.4	0.5	90	85	90	88
III	–	–	–	–	-1.0	-7.2	12.1	5	-14.1	17	-5.2	-2.4	-4.6	-4.2	3.8	4.2	4.0	4.0	84	78	85	82	0.8	1.4	0.8	1.0	83	85	79	82
IV	–	–	–	–	10.3	3.4	20.9	23	-4.2	7	6.0	8.6	6.0	6.6	6.7	7.0	6.6	6.8	73	67	73	71	3.4	5.4	3.6	4.1	66	77	58	67
V	–	–	–	–	10.9	3.8	18.1	28	-4.9	2	6.6	8.8	7.0	7.4	8.2	8.6	8.4	8.4	83	76	82	80	1.8	3.2	2.1	2.4	77	88	73	79
VI	–	–	–	–	13.2	6.8	25.3	24	-1.3	7	9.3	11.6	9.2	9.8	10.2	10.7	10.1	10.3	84	77	85	82	2.6	4.4	2.4	3.1	75	84	71	77
VII	–	–	–	–	16.2	9.0	24.9	26, 27	3.4	6	11.8	14.4	11.5	12.3	11.0	11.1	10.9	11.0	80	68	80	76	3.1	6.0	3.0	4.0	72	81	69	74
VIII	–	–	–	–	19.7	11.4	27.0	15	6.3	30, 31	14.7	18.5	14.5	15.6	11.9	12.3	12.3	12.2	72	58	75	68	5.2	9.6	4.6	6.5	61	69	56	62
IX	–	–	–	–	14.5	6.0	23.5	12	0.3	22, 25	8.8	12.8	9.1	10.0	8.9	10.1	9.2	9.4	79	70	80	76	3.0	5.6	2.8	3.8	55	68	46	56
X	–	–	–	–	11.7	4.6	18.8	3	-1.6	16	6.5	11.0	6.9	7.8	7.7	8.8	8.1	8.2	80	69	81	77	2.2	4.7	2.1	3.0	37	45	37	40
XI	–	–	–	–	5.2	-0.3	14.9	8	-6.2	17, 24, 28	1.5	3.7	1.8	2.2	6.3	7.0	6.5	6.6	89	85	90	88	1.0	1.6	0.9	1.2	89	85	85	86
XII	–	–	–	–	-2.1	-9.2	7.9	7	-21.9	23	-6.1	-3.9	-5.8	-5.4	3.3	3.6	3.2	3.4	82	77	80	80	0.9	1.4	1.1	1.1	74	78	63	72
Rok	–	–	–	–	8.1	1.2	27.0	15 VIII	-21.9	23. XII	3.7	6.5	3.9	4.5	7.1	7.6	7.3	7.3	82	73	82	79	2.1	3.8	2.1	2.7	71	76	67	71

Zakopane $\varphi = 49°18'$ $\lambda = 19°57'$

I	918.8	930.1	898.2	–	1.7	-7.0	7.0	13	-19.0	31	-4.2	-0.1	-3.5	-2.8	3.8	4.0	3.8	3.9	80	65	77	74	1.0	2.4	1.2	1.5	74	68	70	71
II	916.6	932.2	890.7	–	-1.0	-9.5	6.9	12	-21.4	25	-7.5	-2.7	-5.0	-5.0	3.1	3.6	3.6	3.4	82	72	82	79	0.6	1.5	0.8	1.0	90	83	87	87
III	911.4	926.6	898.2	–	0.5	-8.2	13.0	5	-18.5	27	-6.1	-0.9	-4.3	-3.9	3.4	3.9	3.7	3.7	79	66	79	75	0.9	2.2	1.1	1.4	85	84	74	81
IV	917.7	930.1	892.6	–	11.5	1.5	22.2	23	-4.2	3	4.9	9.9	-5.1	6.2	6.4	6.5	6.7	6.5	74	59	77	70	2.7	7.0	2.5	4.1	67	75	56	66
V	917.8	924.3	905.2	–	12.4	3.5	19.8	28	-4.9	2	6.9	10.3	7.3	8.0	8.2	8.4	8.5	8.4	80	67	82	76	2.1	4.6	2.2	3.0	77	86	73	79
VI	923.0	930.3	914.0	–	15.1	5.4	27.0	24	0.0	7	9.7	12.9	9.3	10.3	9.8	10.4	10.1	10.1	79	68	83	77	3.1	6.1	2.3	3.8	72	80	68	73
VII	920.5	929.2	908.0	–	17.6	7.2	26.8	26	0.9	5	11.7	15.9	11.5	12.6	10.9	11.0	11.4	11.1	79	61	83	74	3.1	7.7	2.4	4.4	67	77	69	71
VIII	922.6	928.2	914.0	–	21.2	8.9	28.3	15	2.2	31	13.2	19.7	13.8	15.1	12.0	12.0	12.3	12.1	79	53	78	70	3.4	11.5	3.9	6.3	56	65	56	59
IX	921.8	930.3	909.8	–	15.8	3.6	24.9	12	-2.5	25	6.3	14.2	7.9	9.1	8.2	9.6	9.1	9.0	85	61	85	77	1.9	7.5	2.0	3.8	52	66	45	54
X	925.2	936.2	911.9	–	12.7	1.0	19.2	2	-2.9	17	2.1	12.1	4.1	5.6	6.6	8.4	7.6	7.5	91	61	91	81	0.6	6.2	0.8	2.5	39	44	35	39
XI	918.4	930.9	904.3	–	6.2	-0.3	15.2	7	-6.3	17	1.4	4.8	2.1	2.6	6.0	6.8	6.4	6.4	87	77	87	84	1.2	2.5	1.0	1.6	86	84	83	84
XII	916.2	940.9	881.6	–	-2.2	-12.2	7.4	9	-25.5	22	-8.6	-3.7	-8.0	-7.1	2.9	3.3	2.9	3.0	81	69	79	76	0.7	1.7	0.8	1.1	75	79	62	71
Rok	919.2	940.9	881.6	–	9.3	-0.5	28.3	15. VIII	-25.5	22. XII	2.5	7.7	3.4	4.2	6.8	7.3	7.2	7.1	81	65	82	76	1.8	5.1	1.8	2.9	70	74	65	70

Komańcza $H_s = 470\,m$ $h_w = 15\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU $^nD, {}^vmD$ N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◔	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R ⊠
I	3	2.3	8	3.6	4	3.0	21	3.7	26	2.2	3	3.3	5	2.2	8	2.8	15	2.4	35	9.8	13	3	12	27	·	2	1	1	18	11	8	·	—	31	—
II	10	4.0	10	2.1	1.5	2.3	5	3.8	17	4.0	2	1.5	3	1.7	12.5	5.6	23	2.8	90	17.4	13	12	17	28	·	5	·	·	21	16	11	5	—	28	—
III	8.5	4.9	9	4.4	8	3.0	9	2.1	18.5	2.5	0.5	1.0	2.5	3.0	7	2.7	30	2.1	70	11.8	12	10	13	25	·	1	·	·	22	20	14	2	—	31	—
IV	7	3.6	6	1.8	7	1.6	8	2.4	15	2.7	3	3.0	4	1.5	9	2.7	31	1.6	36	8.0	6	·	·	10	3	1	·	6	8	9	7	·	—	·	—
V	9	1.4	9	1.2	1	1.0	4	1.5	13	1.8	5	2.0	10.5	1.8	7.5	1.9	34	1.1	97	18.5	20	·	·	5	·	·	·	1	13	21	17	2	—	·	—
VI	15.5	2.5	5.5	1.2	6	1.7	3	1.3	9	1.9	1	2.0	6.5	1.6	8.5	2.3	35	1.2	107	21.6	5	·	·	1	5	·	·	3	13	15	12	3	—	·	—
VII	8	2.0	5	1.6	7	1.6	2	1.0	22	1.6	2	2.0	2.5	2.0	10.5	1.7	34	1.1	82[2]	22.6	19	·	·	·	3	·	·	3	10	14	12	3	—	·	—
VIII	5	2.2	4	3.0	5	1.6	4	1.8	5.5	1.4	0.5	1.0	4.5	2.3	9.5	2.5	55	0.9	58	17.0	16	·	·	1	9	·	·	4	5	17	15	1	—	·	—
IX	4	1.5	4	1.0	5	2.0	4	3.0	20	2.4	2	1.5	1	1.0	10	2.1	40	1.2	52	13.6	5	·	·	4	2	·	·	7	6	9	8	2	—	·	—
X	1	1.0	5	1.0	12	1.3	6	1.3	12	1.6	·	·	1	1.0	3	2.0	53	0.6	1	0.3	19	·	·	17	·	·	·	13	4	2	·	·	—	·	—
XI	7	1.4	2	1.0	8	1.2	12	1.8	16	1.8	2	1.0	5	2.2	1	1.0	37	0.9	108	21.2	16	·	·	14	·	·	·	·	19	19	16	5	—	8	—
XII	10	2.7	18	1.7	3	2.0	16	3.0	15	2.3	4	3.5	1	3.0	4	2.5	22	1.9	38	14.7	14	11	23	31	·	·	·	2	24	10	9	1	—	31	—
Rok	88	2.5	85.5	2.0	67.5	1.9	94	2.2	189	2.2	25	1.8	46.5	1.9	90.5	2.5	409	1.5	774[2]	22.6	19.VII	36	65	163	22	9	1	40	163	163	129	24	—	129	—

Baligród $H_s = 450\,m$ $h_w = 16{,}9\,m$

I	13	2.4	4	2.5	1	3.0	1	1.0	59	5.0	·	·	2	2.0	5	3.0	8	3.9	37	9.2	13	1	10	24	·	6	·	1	13	14	8	·	—	12	—
II	11	3.7	4	1.5	1	3.0	·	·	23	5.7	1	3.0	3	3.0	25	4.4	16	3.6	77	26.0	13	9	11	28	·	6	2	·	20	18	14	1	—	28	—
III	21	2.5	1	5.0	4	1.5	·	·	30	3.1	3	3.0	2	3.0	8	2.2	24	2.1	66	12.0	15	9	13	24	·	·	·	·	19	20	12	2	—	29	—
IV	11	3.6	4	2.2	1	3.0	·	·	30	3.3	3	3.7	·	·	5	2.6	36	2.0	24	10.7	6	·	·	3	2	1	·	6	8	9	7	1	—	·	—
V	14	2.1	1	5.0	1	3.0	2	1.0	26	2.1	3	1.7	4	3.0	5	1.6	37	1.3	105	21.0	20	·	·	3	1	·	·	1	10	21	19	4	—	·	—
VI	15	2.2	3	2.3	3	1.7	2	1.0	18	1.4	1	3.0	4	2.5	9	2.3	35	1.2	193	31.5	5	·	·	·	6	·	·	2	12	18	15	9	—	·	—
VII	14	2.4	2	2.0	1	1.0	·	·	35	2.1	5	2.0	1	1.0	4	2.5	31	1.3	150	45.0	19	·	·	·	4	·	·	4	10	17	15	4	—	·	—
VIII	9	2.8	2	2.5	8	1.6	3	2.0	30	2.1	3	2.7	5	2.0	4	1.5	29	1.5	60	17.5	16	·	·	·	8	·	·	2	3	14	12	1	—	·	—
IX	5	2.4	1	1.0	3	2.0	·	·	44	2.3	·	·	3	1.3	7	2.4	27	1.6	64	13.8	5	·	·	2	1	·	·	8	6	13	9	2	—	·	—
X	5	2.2	·	·	1	3.0	·	·	22	2.4	1	3.0	1	3.0	7	1.7	56	0.9	6	3.6	20	·	·	12	·	·	·	12	4	4	2	·	—	·	—
XI	7	1.7	2	1.0	·	·	1	3.0	30	2.0	3	2.3	·	·	2	1.0	45	1.0	92	28.2	20	·	·	9	·	·	·	1	20	18	14	2	—	8	—
XII	12	2.1	8	1.6	2	1.0	·	·	32	4.5	14	2.2	4	1.2	1	1.0	20	2.4	47	13.3	14	10	18	31	·	1	1	2	23	15	7	2	—	31	—
Rok	137	2.5	32	2.2	26	2.0	9	0.7	379	3.0	37	2.2	29	1.8	82	2.2	364	1.9	921	45.0	19.VII	29	52	136	22	14	3	39	148	181	134	28	—	108	—

Gubałówka $H_s = 1000\,m$ $h_w = 18{,}3\,m$

I	14	1.4	2	2.5	·	·	·	·	0.5	6.0	3.5	7.6	65	2.7	·	·	8	2.4	49	13.1	27	4	9	28	·	2	1	2	17	14	11	2	2	31	·
II	24	1.1	3	1.3	2	1.5	·	·	1.5	4.7	4.5	3.8	42	3.3	1	1.0	6	2.4	105	16.6	17	8	21	28	·	3	·	·	20	22	16	4	1	28	·
III	21	1.4	4	2.2	11	2.4	·	·	3	2.7	·	·	39	2.2	·	·	15	1.7	53	9.3	17	11	18	29	·	·	·	1	19	19	10	·	1	31	·
IV	20	1.4	1	1.0	11	2.1	·	·	11	6.3	1	4.0	38	1.8	1	4.0	7	2.2	115	57.2	6	·	1	11	·	3	·	5	12	15	13	3	6	17	1
V	17	1.3	1	4.0	2	1.5	·	·	6	3.3	1	9.0	50	2.3	4	2.0	12	1.9	151	32.2	20	·	1	4	·	2	·	·	17	26	18	6	1	2	3
VI	19	1.4	3	1.7	1.5	1.3	0.5	2.0	4	1.2	3	4.7	39	1.9	12	1.7	8	1.6	221	47.8	5	·	·	7	1	1	·	·	16	18	15	6	4	7	6
VII	18	1.3	1	1.0	4	2.8	·	·	4	1.5	·	·	52	2.1	5	1.2	9	1.7	214	92.4	18	·	·	·	·	·	·	3	15	19	15	3	1	·	4
VIII	12	1.8	·	·	4	2.0	·	·	2.5	2.2	3.5	5.4	58	2.9	1	1.0	12	2.5	48	15.4	15	·	·	·	1	3	·	1	6	12	9	1	·	·	6
IX	12	1.5	·	·	3	2.0	·	·	2	2.0	4	5.5	47	2.2	9	1.4	13	1.9	75	16.4	18	·	·	·	·	1	·	6	9	14	13	2	1	·	1
X	29	1.8	·	·	4	2.0	1	4.0	2	2.0	1	1.0	32	1.4	13	1.5	11	1.4	16	6.6	6	·	·	1	·	·	·	17	10	8	5	·	2	·	·
XI	21	1.6	5	1.2	2	3.5	·	·	4	6.8	4.5	8.9	28.5	1.5	9	1.9	16	1.9	195	35.6	19	·	9	17	·	4	2	1	24	20	18	9	8	14	·
XII	19	1.6	6	2.7	2	1.5	·	·	2	3.5	6	5.7	38	2.7	8	1.8	12	2.2	60	20.8	14	13	17	30	·	1	·	3	16	19	11	2	1	31	·
Rok	226	1.5	26	1.5	46.5	1.9	1.5	0.5	42.5	3.9	32	4.6	528.5	2.2	63	1.5	129	2.0	1302	92.4	18.VII	36	76	155	2	20	3	39	181	206	154	38	28	161	21

Zakopane $H_s = 844\,m$ $H_b = 838{,}2\,m$ $h_w = 17{,}7\,m$

I	1	3.5	10.5	2.1	7.5	1.6	2.5	1.6	1	2.0	15.5	2.7	15	4.0	7	2.9	33	1.8	43	9.2	27	10	9	29	·	1	·	2	14	14	10	·	3	31	·
II	0.5	0.3	8	2.1	9	1.3	5	1.2	2	1.8	13.5	2.8	15	5.8	5	2.6	26	2.1	89	13.6	17	13	16	28	·	3	1	·	20	21	16	3	1	28	·
III	1.5	1.0	16	2.1	20	2.0	3.5	1.1	2.5	6.4	6.5	3.8	8.5	2.3	1.5	2.0	33	1.5	62	10.2	16	13	16	28	·	1	·	1	18	18	12	1	2	31	·
IV	0.5	2.0	13.5	2.1	14	1.9	14.5	2.1	6	6.8	9	3.6	9	2.2	0.5	2.0	23	2.0	104	51.2	6	·	·	9	·	4	1	5	10	15	12	2	4	10	1
V	1.5	2.7	8	1.8	13.5	1.2	8	1.6	5	5.0	14	2.8	7	3.7	7	2.4	29	1.7	171	38.3	20	·	·	4	·	3	1	1	17	26	18	7	1	2	3
VI	4	1.9	9	2.4	12	1.5	11	1.5	3.5	1.7	8	2.1	4.5	3.1	4	3.6	34	1.3	215	42.8	5	·	·	·	3	1	·	·	15	17	14	6	·	3	6
VII	1.5	1.3	15	1.9	8.5	1.5	10	1.8	1	1.0	11	1.7	11.5	3.3	5.5	3.5	29	1.5	237	108.2	18	·	·	·	2	·	·	3	15	18	16	4	·	·	4
VIII	2.5	3.0	7.5	2.0	1	2.5	3	1.3	5.5	5.0	15.5	3.1	8	3.9	9	4.1	41	1.9	48	15.7	15	·	·	·	6	1	·	1	7	12	8	1	·	·	5
IX	4.5	1.7	7	1.5	2	2.0	1.5	2.0	5	4.1	7.5	3.1	10	2.8	9.5	2.5	43	1.3	74	18.0	18	·	·	5	·	3	·	6	9	14	12	3	1	·	1
X	2.5	1.8	13.5	1.6	1.5	1.3	0.5	1.0	0.5	1.0	5	2.2	3	1.7	2.5	1.4	64	0.5	15	5.6	6	·	·	11	·	·	·	18	10	7	4	·	3	·	·
XI	0.5	1.0	20.5	1.6	3.5	1.7	6	3.2	4.5	5.4	9	3.4	1	1.0	1	3.0	44	1.3	173	28.4	19	·	8	15	·	1	·	1	21	19	18	9	9	14	·
XII	3.5	2.0	15.5	2.1	6.5	1.2	0.5	1.0	4.5	4.4	10.5	2.4	9	2.9	3	2.0	40	1.3	57	21.9	14	16	17	31	·	2	·	3	16	14	11	2	1	31	·
Rok	24	1.8	144	1.9	89	1.6	66	1.6	41	3.7	125	2.8	101.5	3.1	55.5	2.7	439	1.5	1288	108.2	18.VII	52	66	160	11	20	3	41	172	195	151	38	25	150	20

Antołówka $\varphi = 49°18'$ $\lambda = 19°59'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0,m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.1	-5.8	7.0	22	-16.1	31	-3.8	-0.8	-3.2	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	74	69	72	72
II	–	–	–	–	-1.7	-8.7	6.4	12	-17.7	25	-7.1	-3.5	-5.0	-5.2	–	–	–	–	–	–	–	–	–	–	–	–	95	85	90	90
III	–	–	–	–	-0.4	-7.3	11.9	5	-13.7	26	-5.3	-1.8	-4.4	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	89	83	77	83
IV	–	–	–	–	11.0	3.0	22.4	25	-4.3	8	5.5	9.5	5.7	6.6	–	–	–	–	–	–	–	–	–	–	–	–	68	79	62	70
V	–	–	–	–	11.9	3.6	19.4	8	-5.2	2	6.6	9.8	7.0	7.6	–	–	–	–	–	–	–	–	–	–	–	–	83	87	74	81
VI	–	–	–	–	14.4	6.2	26.6	24	-0.7	7	9.5	12.4	9.2	10.1	–	–	–	–	–	–	–	–	–	–	–	–	75	86	75	79
VII	–	–	–	–	17.0	8.3	26.2	26	3.0	5	11.7	15.4	11.6	12.6	–	–	–	–	–	–	–	–	–	–	–	–	70	78	71	73
VIII	–	–	–	–	20.9	10.5	27.3	15	4.5	31	13.8	19.4	14.2	15.4	–	–	–	–	–	–	–	–	–	–	–	–	56	71	67	65
IX	–	–	–	–	15.4	5.0	25.3	12	-0.8	25	7.4	13.6	8.8	9.6	–	–	–	–	–	–	–	–	–	–	–	–	55	67	53	58
X	–	–	–	–	11.9	3.3	17.9	2, 3	-2.2	16	4.5	11.2	5.7	6.8	–	–	–	–	–	–	–	–	–	–	–	–	39	43	37	40
XI	–	–	–	–	5.5	0.0	16.0	7	-6.6	17	1.2	4.2	2.2	2.4	–	–	–	–	–	–	–	–	–	–	–	–	81	85	84	83
XII	–	–	–	–	-2.3	-10.1	6.6	9	-20.8	23	-7.2	-4.4	-6.7	-6.2	–	–	–	–	–	–	–	–	–	–	–	–	72	79	66	72
Rok	–	–	–	–	8.7	0.7	27.3	15.VIII	-20.8	23.XII	3.1	7.1	3.8	4.4	–	–	–	–	–	–	–	–	–	–	–	–	71	76	69	72

Kuźnice $\varphi = 49°16'$ $\lambda = 19°59'$

I	–	–	–	–	0.9	-6.5	8.8	22	-17.5	31	-4.0	-1.2	-3.5	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	71	65	64	67
II	–	–	–	–	-2.2	-9.7	6.2	12	-18.5	1	-7.6	-4.2	-5.8	-5.8	–	–	–	–	–	–	–	–	–	–	–	–	90	83	89	87
III	–	–	–	–	-1.3	-8.5	10.8	31	-15.3	26	-5.8	-2.6	-5.3	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	82	88	82	84
IV	–	–	–	–	9.7	0.9	21.0	23	-5.3	7	3.7	8.3	3.3	4.6	–	–	–	–	–	–	–	–	–	–	–	–	64	79	62	68
V	–	–	–	–	10.5	2.1	17.2	8	-6.3	2	5.7	8.3	5.2	6.1	–	–	–	–	–	–	–	–	–	–	–	–	75	87	77	80
VI	–	–	–	–	13.2	4.4	25.2	24	-1.1	7	8.2	11.1	7.0	8.3	–	–	–	–	–	–	–	–	–	–	–	–	73	85	73	77
VII	–	–	–	–	15.7	6.5	25.2	26	1.6	5	10.5	14.2	9.7	11.0	–	–	–	–	–	–	–	–	–	–	–	–	62	78	72	71
VIII	–	–	–	–	19.2	8.3	26.4	15	2.2	31	12.1	17.8	12.3	13.6	–	–	–	–	–	–	–	–	–	–	–	–	54	69	58	60
IX	–	–	–	–	14.2	3.4	23.6	12	-0.7	25	5.9	12.4	7.4	8.3	–	–	–	–	–	–	–	–	–	–	–	–	56	66	47	56
X	–	–	–	–	11.2	1.7	18.2	2	-2.1	17	3.2	10.6	4.3	5.6	–	–	–	–	–	–	–	–	–	–	–	–	36	44	35	38
XI	–	–	–	–	4.9	-0.8	14.2	7	-7.9	28	1.4	3.9	1.4	2.0	–	–	–	–	–	–	–	–	–	–	–	–	87	83	85	85
XII	–	–	–	–	-3.4	-10.3	5.0	9	-21.6	23	-7.2	-5.1	-7.3	-6.7	–	–	–	–	–	–	–	–	–	–	–	–	74	77	65	72
Rok	–	–	–	–	7.7	-0.7	26.4	15.VIII	-21.6	23.XII	2.2	6.1	2.4	3.3	–	–	–	–	–	–	–	–	–	–	–	–	69	75	67	70

Łysa Polana $\varphi = 49°16'$ $\lambda = 20°07'$

I	–	–	–	–	1.3	-7.9	9.3	22	-15.3	31	-4.4	-0.5	-4.3	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	61	53	60	58
II	–	–	–	–	-1.6	-9.9	4.3	12	-21.1	25	-8.2	-3.8	-5.9	-6.0	–	–	–	–	–	–	–	–	–	–	–	–	85	81	85	84
III	–	–	–	–	-0.6	-9.5	12.3	5	-18.1	26	-6.9	-2.1	-5.8	-5.2	–	–	–	–	–	–	–	–	–	–	–	–	80	76	75	77
IV	–	–	–	–	10.6	0.2	21.7	23, 24	-6.4	3	3.7	8.6	3.3	4.7	–	–	–	–	–	–	–	–	–	–	–	–	61	63	57	60
V	–	–	–	–	11.0	1.6	18.1	8	-8.0	2	5.5	8.9	5.4	6.3	–	–	–	–	–	–	–	–	–	–	–	–	75	77	68	73
VI	–	–	–	–	13.4	4.1	25.7	24	-1.2	7	8.0	11.5	7.3	8.5	–	–	–	–	–	–	–	–	–	–	–	–	70	71	67	69
VII	–	–	–	–	16.1	6.3	25.1	27	-0.4	5	10.1	14.4	9.6	10.9	–	–	–	–	–	–	–	–	–	–	–	–	62	65	64	64
VIII	–	–	–	–	20.0	7.9	27.3	15	0.6	31	12.0	18.3	12.3	13.7	–	–	–	–	–	–	–	–	–	–	–	–	48	57	45	50
IX	–	–	–	–	14.6	2.7	23.7	12	-2.1	25	5.3	12.8	6.9	8.0	–	–	–	–	–	–	–	–	–	–	–	–	53	56	46	52
X	–	–	–	–	11.9	0.2	18.5	3	-3.8	17	1.6	10.9	3.1	4.7	–	–	–	–	–	–	–	–	–	–	–	–	36	37	31	35
XI	–	–	–	–	5.4	-1.4	15.5	8	-7.8	18	0.1	4.0	1.0	1.5	–	–	–	–	–	–	–	–	–	–	–	–	77	75	82	78
XII	–	–	–	–	-2.0	-12.0	7.1	9	-22.5	22	-9.0	-4.1	-8.1	-7.3	–	–	–	–	–	–	–	–	–	–	–	–	66	62	56	61
Rok	–	–	–	–	8.3	-1.5	27.3	15.VIII	-22.5	22.XII	1.5	6.6	2.1	3.1	–	–	–	–	–	–	–	–	–	–	–	–	64	64	61	63

Dolina Chochołowska $\varphi = 49°15'$ $\lambda = 19°49'$

I	–	–	–	–	0.5	-7.2	9.0	22	-18.8	31	-4.8	-1.5	-3.6	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	58	53	62	58
II	–	–	–	–	-2.4	-10.7	4.1	12	-20.5	1	-8.3	-3.9	-6.1	-6.1	–	–	–	–	–	–	–	–	–	–	–	–	79	72	76	76
III	–	–	–	–	-1.5	-9.3	10.9	31	-19.8	26	-6.9	-2.4	-5.4	-5.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	9.2	-0.2	19.8	25	-6.9	30	1.9	7.7	2.7	3.8	–	–	–	–	–	–	–	–	–	–	–	–	54	67	54	58
V	–	–	–	–	9.8	1.4	16.9	28	-9.0	2	3.5	8.2	5.2	5.5	–	–	–	–	–	–	–	–	–	–	–	–	66	77	66	70
VI	–	–	–	–	12.2	3.6	24.6	24	-1.3	7	5.4	10.9	6.2	7.2	–	–	–	–	–	–	–	–	–	–	–	–	64	72	58	65
VII	–	–	–	–	15.0	5.8	26.1	26	1.0	5	7.6	13.9	9.2	10.0	–	–	–	–	–	–	–	–	–	–	–	–	54	69	57	60
VIII	–	–	–	–	19.3	7.1	26.3	15	0.5	31	9.7	17.7	11.9	12.8	–	–	–	–	–	–	–	–	–	–	–	–	41	54	46	47
IX	–	–	–	–	13.6	2.4	23.2	4	-2.0	25	4.4	12.2	6.7	7.5	–	–	–	–	–	–	–	–	–	–	–	–	42	56	46	48
X	–	–	–	–	10.7	0.2	16.7	3	-4.5	17	1.6	10.1	3.4	4.6	–	–	–	–	–	–	–	–	–	–	–	–	32	36	34	34
XI	–	–	–	–	5.0	-1.2	13.5	8	-9.7	29	0.9	3.7	1.5	1.9	–	–	–	–	–	–	–	–	–	–	–	–	73	73	68	71
XII	–	–	–	–	-4.2	-12.0	4.9	9	-22.6	24	-8.4	-6.2	-8.5	-7.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	7.3	-1.7	26.3	15.VIII	-22.6	24.XII	0.6	5.9	1.9	2.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Antołówka $H_s = 918$ m $h_w = 18,5$ m 1962

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr > 10	Wiatr > 15	◑	●	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	═	⊠	R
I	5	1.9	3	1.8	0.5	3.0	1	3.5	9.5	5.2	25	3.4	16	3.5	9	2.9	24	2.5	45	13.7	27	4	11	29	·	8	2	3	17	15	9	1	3	31	·
II	4.5	1.8	·	·	·	·	2	1.5	4.5	1.6	14.5	5.6	15.5	4.6	11	3.1	32	2.5	104	18.9	17	7	18	28	·	6	5	·	22	20	16	1	1	28	·
III	13	2.4	11.5	2.9	3	4.0	3	3.7	14.5	6.0	9	3.2	5.5	2.5	4.5	2.4	29	2.5	76	15.7	15	11	20	28	·	4	1	1	20	19	13	3	3	31	·
IV	6	2.3	6.5	2.8	8	2.5	2.5	4.4	19.5	7.4	18	2.5	6	2.4	4.5	1.9	19	3.1	117	50.2	6	·	·	8	·	7	4	3	14	15	13	4	7	12	2
V	7.5	2.3	4	1.9	1	3.0	4.5	2.0	22	3.1	19	2.9	14.5	2.9	7.5	1.4	13	2.3	193	42.9	20	·	·	5	·	4	1	·	16	27	19	8	6	2	4
VI	6	3.3	3	3.2	·	·	4.5	2.0	10	2.3	18.5	2.9	11	3.3	11	2.7	26	2.0	214	36.7	4	·	·	1	1	·	·	·	17	19	15	7	5	5	6
VII	1.5	2.3	3	3.0	1	3.0	1.5	2.0	10.5	2.2	19.5	2.3	11	2.8	10	3.0	35	1.6	261	109.1	18	·	·	·	2	1	·	3	16	19	16	4	1	·	8
VIII	6.5	2.3	1	1.0	·	·	0.5	12.0	17	3.8	23.5	3.2	11.5	3.1	9	2.3	24	2.3	53	13.7	16	·	·	·	5	4	·	1	8	13	8	2	·	·	6
IX	5.5	3.0	4	1.9		·	1.5	1.7	19	3.8	20.5	2.7	9.5	3.5	8	1.9	22	2.3	77	17.8	18	·	·	1	1	4	·	7	11	14	14	2	2	·	1
X	8	2.1	8	2.8	2.5	2.2	4	2.1	16	2.2	7.5	1.7	5	1.7	13	2.4	29	1.5	14	4.9	6	·	·	2	·	·	·	17	10	8	4	·	4	·	-
XI	9.5	2.3	2	3.5	0.5	3.0	1.5	4.3	21	5.9	4.5	2.1	1.5	2.7	3.5	2.4	46	2.0	176	26.5	19		8	14	·	4	·	2	24	19	18	7	15	14	·
XII	12	2.3	1	1.0			1.5	2.3	12	7.1	16.5	2.0	6	2.8	1	2.0	43	1.8	57	21.6	14	13	18	31	·	4	2	3	17	15	12	1	7	31	-
Rok	85	2.4	47	2.2	16.5	1.7	28	3.5	175.5	4.2	196	2.9	113	3.0	92	2.4	342	2.2	1387	109.1	18. VII	35	75	147	9	46	15	40	192	203	157	40	54	154	27

Kuźnice $H_s = 1023$ m $h_w = 21,5$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr > 10	Wiatr > 15	◑	●	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	═	⊠	R
I	9.5	1.8	11	2.2	2.5	1.4	1	1.0	20	2.8	17	3.2	·	·	·	·	32	1.7	76	17.2	27	7	11	28	·	3	1	5	13	16	15	2	2	31	·
II	11	6.4	7.5	8.6	1	1.0	1	5.0	10.5	4.3	9.5	4.6	1	1.0	0.5	1.0	42	2.7	142	15.9	14	11	21	28	·	5	3	·	21	23	20	7	4	28	·
III	11	1.3	4	1.8	0.5	1.0	2.5	8.0	19.5	4.4	14	2.9	1	3.0	0.5	1.0	40	1.8	114	15.5	16	14	20	28	·	3	·	·	23	20	15	4	4	31	·
IV	9	2.4	5	3.5	·	·	3	1.7	24	4.8	19	4.6	·	·	1	1.0	29	2.8	162	56.3	6	·	1	11	·	4	3	4	12	16	13	5	3	20	1
V	9	1.6	7.5	1.9	1	1.0	1	1.0	22.5	2.4	18.5	2.2	·	·	1.5	1.0	32	1.4	248	49.2	20	·	1	7	·	·	·	·	19	27	22	8	7	4	·
VI	11	2.0	6.5	2.4	3	1.7	0.5	3.0	14	1.9	13.5	1.9	2	1.0	3.5	1.0	36	1.1	275	44.5	5	·	·	2	1	·	·	·	18	18	16	8	6	7	4
VII	17.5	1.3	7	1.4	1	1.0	1.5	1.7	21	1.5	18.5	1.5	·	·	0.5	1.0	26	1.0	277	143.8	18	·	·	·	1	·	·	2	13	17	15	4	1	·	4
VIII	13	2.1	9	3.2	3.5	3.3	1.5	3.0	23.5	2.0	20	2.0	·	·	0.5	1.0	22	1.7	66	13.7	16	·	·		1	·	·	3	8	12	12	2	1	·	5
IX	6	1.0	7.5	1.7	1.5	1.7	4	1.8	25	1.9	18	2.0	·	·	5	1.0	23	1.3	113	26.5	18	·	·	1	·	1	·	6	9	16	13	4	1	·	·
X	13.5	1.0	5.5	1.0		·	2	1.0	23.5	2.1	23.5	2.5	·	·	4	1.0	21	1.4	20	5.8	6	·	·	8	·	·	·	18	9	8	5	·	3	·	·
XI	2.5	1.4	2.5	1.4	·	·	2.5	5.8	19.5	3.5	17	3.2	0.5	3.0	3.5	1.3	42	1.7	242	35.6	19	·	8	17	·	1	·	2	23	18	18	8	10	15	·
XII	6.5	1.5	3.5	1.9	·	·	1	6.5	35.5	4.1	18.5	3.1	·	·	·	·	28	2.4	85	24.8	14	13	21	31	·	3	2	3	16	17	14	2	2	31	·
Rok	119.5	2.0	76.5	2.6	14	1.0	21.5	3.3	258.5	3.0	207	2.8	4.5	0.7	20.5	0.9	373	1.8	1820	143.8	18. VII	45	83	161	3	20	9	43	184	208	178	54	44	167	14

Łysa Polana $H_s = 988$ m $h_w = 16,8$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr > 10	Wiatr > 15	◑	●	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	═	⊠	R
I	9.5	2.5	9	2.2	5	2.2	7.5	2.2	7.5	3.6	18	2.8	7.5	2.3	3	2.3	26	1.9	69	16.7	27	10	10	30	·	—	—	4	9	15	10	2	1	31	·
II	10.5	2.6	12	2.2	6	1.3	8.5	2.2	2.5	2.8	14	4.2	5.5	3.0	·	·	25	2.0	145	23.8	17	13	17	28	·	—	—	·	19	24	16	7	1	28	·
III	13.5	2.1	17.5	2.0	3.5	2.1	14.5	2.3	6	4.3	8.5	3.6	4.5	2.2	2	2.0	23	1.9	90	17.2	15	16	18	30	·	—	—	1	16	20	13	3	2	31	·
IV	5	2.2	5	2.0	8.5	1.8	19	2.8	7.5	5.9	15.5	4.0	5.5	2.5	2	2.0	22	2.4	155	69.4	6	·	·	15	·	—	—	3	10	16	15	4	4	21	1
V	4	2.2	9.5	1.9	4.5	2.1	11	2.2	7	2.9	18.5	2.6	10	2.4	2.5	3.0	26	1.7	158	26.4	20	·	·	10	·	—	—	·	12	27	22	6	5	4	2
VI	4.5	2.1	8	2.5	7.5	2.1	11.5	2.2	10	2.4	17.5	2.3	7.5	2.0	6.5	2.4	17	1.8	255	45.5	4	·	·	4	1	—	—	·	11	20	14	9	1	7	6
VII	4	2.4	8.5	2.4	12.5	2.0	13.5	2.2	12.5	2.1	16	2.2	6.5	2.1	0.5	3.0	19	1.7	215	105.1	18	·	·	1	1	—	—	3	5	20	16	6	·	·	11
VIII	2	2.2	11.5	2.2	8.5	2.6	11	2.2	17	3.3	14	2.5	6.5	2.2	2.5	2.2	20	2.0	69	20.8	5	·	·	·	2	—	—	2	2	13	10	3		·	5
IX	3	2.7	5	1.9	6.5	1.8	11	2.3	8	3.3	12.5	2.6	7	2.0	5	2.0	32	1.6	84	16.0	17	·	·	7	·	—	—	6	8	15	14	4	1	·	1
X	6.5	2.2	10.5	2.2	7.5	2.4	8.5	1.9	3.5	1.6	14	1.5	9	2.2	0.5	2.0	33	1.4	12	3.9	6	·	·	12	·	—	—	16	3	8	4	·	4	·	·
XI	6	2.0	8.5	1.9	6	1.8	10	2.6	8	4.5	18	3.4	5.5	1.9	2	1.5	26	2.0	208	36.3	19	·	7	17	·	—	—	2	17	19	17	8	6	15	·
XII	11	2.4	8.5	2.5	3.5	2.6	4	3.2	3.5	3.4	21.5	3.5	11	1.8	5	2.2	25	2.0	63	19.4	14	17	19	31	·	—	—	4	8	16	10	2	2	31	·
Rok	79.5	2.3	113.5	2.2	79.5	2.1	130	2.4	93	3.3	188	2.9	86	2.2	31.5	2.0	294	1.9	1523	105.1	18. VII	56	71	185	4	—	—	41	120	213	161	54	27	168	26

Dolina Chochołowska $H_s = 1028$ m $h_w = 19$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr > 10	Wiatr > 15	◑	●	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	═	⊠	R
I	17.5	2.3	1.5	2.0	3	2.0	1	1.0	13	4.4	7	6.4	·	·	·	·	50	1.6	46	13.2	27	10	14	29	·	3	2	5	13	17	7	2	1	31	—
II	20.5	5.1	5.5	4.5	5	·42	3.5	3.0	9	6.2	1.5	6.0	·	·	1	8.0	38	2.8	103	15.6	17	15	21	28	·	4	2	1	17	22	12	5	4	28	—
III	28.5	3.4	3.5	3.3	2	1.5	1	1.0	12	5.6	1	15.0	·	·	·	·	45	2.1	42	9.8	12	16	20	28	·	4	1	—	—	17	12	·	2	31	—
IV	14.5	2.4	4.5	1.6	5	1.4	1	2.0	35.5	4.6	0.5	1.0	·	·	·	·	29	2.4	109	39.2	6	·	1	14	·	3	2	7	9	15	13	4	4	21	—
V	10	1.6	2.5	1.0	3	1.0	·	·	23	2.6	·	·	·	·	0.5	2.0	54	0.9	219	41.5	20	·	1	10	·	·	·	2	12	24	21	9	5	6[2]	—
VI	14	2.6	2	1.5	1	1.0	2	1.5	12	2.1	2	1.0	·	·	·	·	57	0.8	178	30.1	4	·	·	4	·	·	·	3	12	14	14	5	2	8	—
VII	5	1.6	11.5	1.3	2.5	1.2	2.5	1.6	14	1.2	0.5	1.0	·	·	·	·	57	0.6	239	97.4	18	·	·	·	2	·	·	3	7	17	16	4	2	·	—
VIII	7	1.3	7	1.9	4	1.5	·	·	25	2.9	·	·	·	·	·	·	50	1.1	62	19.7	15	·	·	·	1	2	·	4	3	12	9	2	·	·	—
IX	4	1.5	8	1.8	7	1.1	3.5	1.3	22.5	2.4	·	·	·	·	·	·	45	1.0	104	2 .6	18	·	·	7	·	1	·	9	7	14	12	4	1	·	—
X	9	1.4	17.5	1.3	5.5	1.3	6	1.0	11	1.5	1	1.0	·	·	·	·	43	0.7	16	9.6	6	·	·	14	·	·	·	17	8	8	4	·	7	·	—
XI	8	1.1	2	1.0	·	·	·	·	19	3.7	15	8.2	·	·	·	·	46	2.3	218	39.9	19	·	8	17	·	4	2	4	15	18	18	8	7	15	—
XII	16	1.3	5	2.4	13	1.5	1	1.0	6	7.8	11	12.4	·	·	·	·	41	2.5	57	13.0	14	17	23	31	·	6	5	—	—	16	11	2	·	31	—
Rok	154	2.1	70.5	2.0	51	1.5	21.5	1.1	202	3.8	39.5	4.3	·	·	1.5	0.8	555	1.6	1393	97.4	18. VII	58	88	182	3	27	14	—	—	194	149	45	35	171[2]	—

Myślenickie Turnie $\varphi = 49°15'$ $\lambda = 19°59'$ 1962

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	P_{0m}	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.6	-6.3	8.3	1	-17.8	30, 31	-3.4	-2.2	-3.5	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.6	6.2	6.5
II	–	–	–	–	-3.9	-10.3	2.8	12	-17.8	1	-8.2	-6.3	-7.0	-7.1	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.5	8.6	8.6
III	–	–	–	–	-3.8	-9.0	7.9	31	-17.0	17	-7.3	-5.5	-6.6	-6.5	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.9	7.8	8.4
IV	–	–	–	–	7.4	1.8	18.6	23	-6.3	7	3.7	5.3	3.9	4.2	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.8	6.3	6.9
V	–	–	–	–	8.6	1.8	14.9	23	-7.9	1	4.1	5.8	5.0	5.0	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.8	7.4	8.1
VI	–	–	–	–	11.0	4.6	23.3	24	-3.7	7	6.7	8.7	7.1	7.4	–	–	–	–	–	–	–	–	–	–	–	–	7.7	8.9	7.1	7.9
VII	–	–	–	–	13.2	7.4	23.3	26	1.7	1	9.2	11.3	9.7	10.0	–	–	–	–	–	–	–	–	–	–	–	–	7.1	8.2	6.9	7.4
VIII	–	–	–	–	17.0	9.8	23.7	15	3.7	31	11.9	15.0	12.8	13.1	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.1	5.6	6.2
IX	–	–	–	–	11.4	4.9	21.5	4, 12	0.2	22	6.9	9.6	7.6	7.9	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.7	4.4	5.6
X	–	–	–	–	9.3	3.9	14.8	2	-1.8	21	5.6	7.6	6.0	6.3	–	–	–	–	–	–	–	–	–	–	–	–	3.8	4.4	3.6	3.9
XI	–	–	–	–	3.9	-1.7	11.5	1	-9.5	17	0.8	1.8	0.6	1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.4	7.6	8.1
XII	–	–	–	–	-2.9	-9.8	4.6	8	-23.9	23	-6.5	-5.9	-6.7	-6.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.5	6.0	6.8
Rok	–	–	–	–	6.0	-0.2	23.7	15, VIII	-23.9	23, XII	2.0	3.8	2.4	2.6	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.6	6.5	7.0

Hala Gąsienicowa $\varphi = 49°15'$ $\lambda = 20°00'$

I	841.6	850.1	824.0	–	-0.5	-7.6	7.0	18	-18.8	29	-4.4	-3.2	-4.2	-4.0	2.9	2.8	3.0	2.9	66	59	67	64	1.8	2.3	1.8	2.0	6.6	6.0	5.8	6.1
II	838.7	852.5	816.1	–	-4.7	-11.8	1.3	27	-19.6	23	-9.4	-6.9	-8.3	-8.2	2.5	3.0	2.8	2.8	80	80	83	81	0.6	0.7	0.6	0.6	8.4	8.3	8.5	8.4
III	834.2	847.2	823.3	–	-4.4	-10.9	6.5	5	-18.2	17	-8.4	-6.1	-7.6	-7.4	2.7	3.3	3.0	3.0	73	78	78	76	0.9	0.9	0.8	0.9	7.5	8.3	7.0	7.6
IV	842.8	856.4	820.0	–	5.6	-0.4	15.4	24	-8.3	7	2.2	3.6	2.0	2.4	5.0	5.4	5.0	5.1	71	72	73	72	2.5	3.2	2.5	2.7	6.0	7.1	5.7	6.3
V	843.1	849.3	833.0	–	7.1	0.5	12.5	28	-9.4	2	3.3	4.8	3.7	3.9	6.4	6.8	6.5	6.6	80	79	79	79	1.7	2.2	1.9	1.9	7.5	8.3	6.7	7.5
VI	848.4	855.5	839.7	–	9.3	2.7	20.7	24	-4.7	7	5.6	7.2	5.3	5.8	7.7	8.2	7.7	7.9	82	79	84	82	2.5	2.9	1.8	2.4	7.4	8.5	6.7	7.5
VII	846.9	855.0	834.3	–	11.6	5.1	21.0	27	-0.9	5	8.2	10.0	7.9	8.5	8.5	9.0	8.8	8.8	78	73	81	77	2.8	3.6	2.1	2.8	6.6	8.0	6.3	7.0
VIII	849.4	853.9	844.0	–	15.2	7.7	21.3	15	1.4	31	11.2	13.6	10.9	11.6	9.2	10.2	9.5	9.6	69	66	74	70	4.4	5.7	3.8	4.6	5.5	7.2	4.8	5.8
IX	847.4	854.4	836.7	–	10.2	2.8	19.0	4	-2.2	25	5.7	8.6	6.0	6.6	6.4	7.8	6.8	7.0	71	72	74	72	3.3	4.1	3.0	3.5	5.2	6.7	4.4	5.4
X	850.1	860.7	837.7	–	8.8	1.6	13.6	3	-4.6	21	3.7	7.4	4.0	4.8	4.9	6.8	5.9	5.9	63	68	74	68	3.2	3.8	2.4	3.1	3.5	4.0	3.1	3.5
XI	842.4	852.5	830.1	–	3.7	-2.2	10.5	9	-10.8	29	0.5	1.5	0.4	0.7	5.0	5.5	5.0	5.2	78	80	78	79	1.8	1.7	1.7	1.7	7.0	7.6	6.7	7.1
XII	838.4	860.0	807.4	–	-4.1	-10.8	2.5	9	-24.7	23	-7.2	-6.8	-7.4	-7.2	2.5	2.6	2.5	2.5	69	68	70	69	1.3	1.3	1.2	1.3	6.1	6.6	5.5	6.1
Rok	843.6	860.7	807.4	–	4.8	-1.9	21.3	15, VIII	-24.7	23, XII	0.9	2.8	1.1	1.5	5.3	6.0	5.5	5.6	73	73	76	74	2.2	2.7	2.0	2.3	6.4	7.2	5.9	6.5

Hala Ornak $\varphi = 49°14'$ $\lambda = 19°51'$

I	–	–	–	–	0.2	-7.5	10.1	22	-21.1	31	-4.5	-1.3	-4.3	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.5	5.9	5.7
II	–	–	–	–	-2.4	-11.6	2.4	12	-22.1	1	-8.5	-3.8	-6.8	-6.5	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.4	8.0	7.8
III	–	–	–	–	-1.0	-10.1	10.9	31	-20.6	26	-7.5	-2.0	-6.0	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.5	7.6	7.7
IV	–	–	–	–	8.8	-0.9	19.6	23	-8.3	30	1.3	7.6	1.8	3.1	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.7	5.0	5.8
V	–	–	–	–	10.0	0.4	16.2	28	-6.2	1, 3	3.5	7.8	3.9	4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	8.6	6.9	7.7
VI	–	–	–	–	12.6	2.6	25.0	24	-1.7	7	5.8	10.6	6.0	7.1	–	–	–	–	–	–	–	–	–	–	–	–	7.3	8.1	7.8	7.7
VII	–	–	–	–	15.4	4.9	25.9	26	-0.6	5	7.9	14.0	9.0	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.3	6.4	6.7
VIII	–	–	–	–	19.6	6.2	25.7	15	-1.4	31	9.4	17.7	11.4	12.5	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.8	4.8	5.1
IX	–	–	–	–	13.5	1.5	23.6	4	-3.4	26	3.8	11.9	5.7	6.8	–	–	–	–	–	–	–	–	–	–	–	–	5.2	6.1	4.1	5.1
X	–	–	–	–	11.2	-0.8	17.7	2	-6.4	17	1.0	10.1	2.5	4.0	–	–	–	–	–	–	–	–	–	–	–	–	3.4	3.9	3.3	3.5
XI	–	–	–	–	4.9	-1.7	13.6	4	-11.0	29	0.8	3.1	1.0	1.5	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.8	7.2	7.7
XII	–	–	–	–	-3.9	-12.9	4.4	9, 14	-22.8	22	-9.2	-5.9	-9.2	-8.4	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.6	5.1	5.8
Rok	–	–	–	–	7.4	-2.5	25.9	26, VII	-22.8	22, XII	0.3	5.8	1.2	2.1	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.7	6.0	6.4

Kasprowy Wierch $\varphi = 49°14'$ $\lambda = 19°59'$

I	793.0	801.4	775.9	–	-4.2	-10.8	2.5	18	-21.8	29, 30	-7.3	-6.8	-7.4	-7.2	2.7	2.6	2.7	2.7	73	72	79	75	1.1	1.3	1.0	1.1	6.8	7.1	7.1	7.0
II	789.3	802.8	768.1	–	-7.3	-13.7	-1.1	8	-20.5	16	-11.7	-9.7	-10.7	-10.7	2.3	2.7	2.6	2.5	89	90	92	90	0.3	0.3	0.2	0.3	8.4	8.5	8.9	8.6
III	785.1	798.1	775.6	–	-7.4	-12.8	1.9	5	-21.8	17	-10.9	-9.4	-10.3	-10.2	2.6	3.0	2.8	2.8	86	90	90	89	0.4	0.3	0.3	0.3	8.2	8.5	8.4	8.4
IV	795.4	810.2	773.0	–	2.5	-2.9	14.2	23	-11.0	8	-0.9	0.5	-0.8	-0.5	4.7	5.0	4.6	4.8	83	81	82	82	1.4	1.9	1.6	1.6	6.6	8.0	6.7	7.1
V	795.7	802.6	784.5	–	3.0	-2.2	8.5	9	-11.9	1	-0.4	1.0	0.3	0.3	5.8	6.2	6.0	6.0	93	92	92	92	0.4	0.6	0.5	0.5	8.1	9.0	7.7	8.3
VI	801.3	809.9	792.6	–	6.4	0.6	17.1	24	-7.5	7	2.6	4.0	2.9	3.1	6.9	7.2	7.2	7.1	89	87	93	90	1.1	1.6	0.8	1.2	7.8	8.5	7.7	8.0
VII	800.3	808.8	787.0	–	8.3	2.6	18.3	26	-2.8	5	4.1	6.3	4.7	5.0	7.3	8.3	7.8	7.8	89	86	90	88	1.3	1.6	1.0	1.3	7.3	8.4	7.1	7.6
VIII	803.3	808.4	798.1	–	12.1	5.3	17.5	15	-0.9	31	7.0	10.1	7.8	8.2	8.2	9.2	8.8	8.7	81	74	83	79	2.0	3.5	2.1	2.5	6.0	7.6	5.7	6.4
IX	800.5	807.8	790.1	–	6.8	0.5	15.3	4	-4.4	25	2.7	5.0	3.0	3.4	5.5	6.9	6.0	6.1	75	80	79	78	2.2	2.2	1.9	2.1	5.8	6.9	4.4	5.7
X	802.9	813.8	790.5	–	5.8	0.2	12.7	3	-7.2	21	2.1	4.5	2.4	2.8	4.1	6.0	5.0	5.0	60	72	71	68	3.2	2.8	2.4	2.8	3.7	4.7	3.5	4.0
XI	794.5	803.9	781.7	–	0.0	-4.6	5.7	1	-12.4	17	-2.5	-1.6	-2.4	-2.2	4.8	5.2	4.7	4.9	91	93	98	91	0.5	0.5	0.6	0.5	7.5	7.9	7.7	7.7
XII	789.3	809.7	760.6	–	-6.4	-12.3	0.3	7	-24.1	22	-9.5	-9.1	-9.3	-9.3	2.3	2.4	2.3	2.3	77	78	75	77	0.9	0.9	1.0	0.9	7.1	7.5	6.0	6.9
Rok	795.9	813.8	760.6	–	1.6	-4.2	18.3	26, VII	-24.1	22, XII	-2.1	-0.4	-1.6	-1.4	4.8	5.4	5.0	5.1	82	83	84	83	1.2	1.5	1.1	1.3	6.9	7.7	6.7	7.1

Myślenickie Turnie $H_s = 1360 m$ $h_w = 19,5 m$ 1962

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	(symbol 1)	(symbol 2)	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	(symbol 3)	(symbol 4)	R
I	9.5	3.6	10	3.2	5.5	1.7	5	1.4	22.5	5.9	31	6.3	4	6.2	4.5	5.3	1	4.9	49	15.3	27	6	10	30	·	8	2	12	4	15	11	1	6	31	·
II	9.5	4.4	15	3.6	6.5	2.5	3.5	2.1	11	4.0	22.5	6.2	3.5	6.9	7.5	4.5	5	4.3	74	13.5	17	15	25	28	·	4	1	·	19	20	16	1	6	28	·
III	8	5.2	27.5	3.0	11	2.8	4	2.5	12	6.1	23	7.9	2	6.0	2.5	6.4	3	4.8	55	9.3	12	15	24	29	·	8	3	1	22	19	16	·	7	31	·
IV	3.5	2.7	12	2.5	8	1.9	6	2.5	18.5	7.1	28	7.2	5	2.7	3	2.0	6	4.7	117	40.3	6	·	3	14	·	8	4	3	11	15	12	3	10	30	·
V	5	3.3	14	1.4	6.5	1.2	9	1.4	15	3.8	27	5.0	7	3.1	4.5	4.0	5	3.1	224	38.9	20	·	2	12	·	2	·	·	16	26	22	7	9	12	2
VI	11.5	3.3	25.5	2.2	11.5	1.3	5	1.1	7.5	3.4	17.5	3.4	6.5	4.6	3	2.2	2	2.6	226	35.9	4	·	2	8	·	·	·	·	18	15	14	9	7	11	5
VII	10	2.5	21.5	2.0	9	1.6	9	1.2	10	2.7	20	4.1	6.5	1.9	5	1.8	2	2.4	320	143.3	18	·	·	·	·	·	·	3	15	18	16	6	6	·	4
VIII	3.5	1.7	15.5	1.5	9	1.8	12.5	2.4	17.5	3.6	22	5.0	3.5	2.4	6.5	2.1	3	2.9	69	18.5	15	·	·	·	·	1	1	1	6	11	11	2	2	·	4
IX	5	2.5	11.5	1.9	7.5	1.3	13	1.3	21	3.3	24.5	4.6	1	5.0	6.5	1.9	·	2.9	115	28.1	18	·	·		·	4	·	6	9	14	14	3	4	·	·
X	5	2.0	23.5	1.7	9	1.4	6	1.1	14.5	2.8	24.5	3.2	2.5	1.8	1	2.5	7	2.1	18	7.3	6	·	·	6	·	1	·	16	7	8	5	·	4	1	·
XI	1	3.5	9	1.9	6.5	1.2	3.5	1.0	22	6.5	29	6.8	5	4.9	1	2.0	13	4.4	187	36.7	19	·	8	18	·	8	2	2	21	18	16	8	12	16	·
XII	2	5.8	5.5	4.0	4.5	2.9	7.5	1.2	11.5	3.0	35.5	7.3	5	5.5	1.5	5.0	20	4.1	55	17.3	14	15	20	31	·	7	5	4	16	15	11	2	4	31	·
Rok	73.5	3.4	190.5	2.4	94.5	1.8	84	1.6	183	4.4	304.5	5.6	51.5	4.2	46.5	3.3	67	3.6	1509	143.3	18.VII	51	94	176	·	51	18	48	164	194	164	42	77	191	15

Hala Gąsienicowa $H_s = 1520 m$ $H_b = 1520,8 m$ $h_w = 16 m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	(symbol 1)	(symbol 2)	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	(symbol 3)	(symbol 4)	R
I	5	3.5	7.5	4.5	4.5	3.4	1	3.0	11.5	8.3	41.5	5.0	17	3.4	1	3.0	4	4.7	74	16.4	27	10	16	30	·	7	2	5	13	17	12	3	6	31	·
II	11.5	4.2	12	4.2	1.5	4.3	·	·	5.5	7.2	35	4.5	12	3.0	2.5	3.0	4	4.1	111	20.5	14	18	25	28	·	3	1	·	18	25	16	2	13	28	·
III	8	2.9	15	3.9	2	3.2	1	3.0	6	6.4	45.5	5.0	2	3.0	2.5	2.2	11	4.0	95	16.6	4	18	23	29	·	6	·	2	17	23	15	3	7	31	·
IV	11	3.2	7.5	2.4	4	2.8	1.5	3.3	11	10.3	41.5	4.3	8.5	3.1	1	2.5	4	4.3	158	50.4	6	·	7	19	·	6	2	6	11	15	14	5	14	30	·
V	3	2.5	1.5	4.3	0.5	3.0	·	·	7.5	4.4	58.5	3.6	6	3.2	4	3.5	12	3.2	236	37.4	20	·	2	13	·	1	1	1	13	29	24	8	14	14	3
VI	7	4.4	3.5	3.6	1.5	3.0	0.5	2.0	8	3.2	42	2.6	11	2.8	6.5	4.8	10	2.7	274	48.6	4	·	5	10	·	·	·	·	17	18	14	10	12	14	6
VII	1	2.5	4.5	3.1	0.5	3.0	2	1.5	15.5	3.0	46.5	2.7	13	2.3	5	3.2	5	2.6	371	177.7	18	·	·	1	·	·	·	2	11	17	16	6	8	·	6
VIII	5	2.5	5.5	3.6	1	3.0	1	5.0	9.5	4.5	48	3.8	13.5	2.2	5.5	4.2	4	3.4	97	22.8	5	·	·	·	·	3	1	1	5	14	11	4	8	·	5
IX	1	2.0	1	2.0	·	·	·	·	6	4.8	60.5	3.8	15.5	3.2	2	3.2	4	3.6	120	26.9	18	·	·	8	·	2	·	7	9	14	14	5	8	6	1
X	2	3.0	5	2.8	1	3.0	·	·	3.5	4.9	62.5	3.1	15	2.4	1	1.5	3	2.9	24	8.2	6	·	·	9	·	1	·	18	7	7	5	·	8	1	·
XI	1	4.0	4.5	2.3	1.5	3.0	0.5	5.0	19	7.1	44.5	4.8	6.5	2.8	1.5	3.0	11	4.4	228	40.0	19	2	6	19	·	5	·	4	15	20	18	10	9	16	·
XII	2.5	4.8	9.5	3.4	3	4.3	1	3.0	7.5	9.8	58	4.1	4	2.1	1.5	3.7	6	4.2	68	20.3	14	17	23	31	·	5	1	6	12	20	10	2	5	31	·
Rok	58	3.3	77	3.3	21	3.0	8.5	2.2	110.5	6.2	584	3.9	124	2.8	34	3.2	78	3.7	1856	177.7	18. VII	65	107	197	·	39	8	52	148	219	169	58	112	202	21

Hala Ornak $H_s = 1110 m$ $h_w = 17,8 m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	(symbol 1)	(symbol 2)	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	(symbol 3)	(symbol 4)	R
I	4	2.8	6.5	1.3	2	3.5	1.5	4.3	15	5.4	5.5	1.6	8.5	1.6	·	·	50	1.5	91	24.2	27	8	14	28	·	3	·	6	10	17	11	4	–	31	–
II	7.5	4.0	14.5	3.8	3	3.0	1	3.0	3.5	3.9	4.5	1.9	·	·	2	2.5	48	1.5	180	26.8	17	19	19	28	·	1	·	2	15	23	19	8	–	28	–
III	19.5	2.6	3.5	1.9	·	·	·	·	12	6.6	7	5.3	·	·	·	·	51	1.9	116	15.6	7	17	18	28	·	2	·	2	19	22	15	6	–	31	–
IV	6	2.7	·	·	·	·	·	·	24	5.0	2	3.0	1.5	1.0	0.5	1.0	56	1.6	165	61.0	6	·	1	18	·	2	1	8	12	14	13	6	–	27?	–
V	6.5	1.7	5.5	4.2	1	1.0	·	·	13.5	3.3	2.5	2.4	2	2.0	·	·	62	1.0	187?	27.9	14	·	1	14	·	1	·	1	12	27	27	8	–	7	–
VI	7.5	2.9	·	·	·	·	·	·	2	2.0	2	2.0	1.5	1.7	2	1.5	75	0.4	236	42.2	5	·		10	·	·	·	·	15	15	14	9	–	11	–
VII	7	2.3	·	·	·	·	·	·	5.5	1.7	1	1.0	1.5	1.0	2	2.0	76	0.3	241	110.8	18	·	·	1	2	·	·	2	10	18	15	4	–	·	–
VIII	3.5	2.7	0.5	5.0	·	·	·	·	10	3.2	3	2.3	2	2.0	4	3.2	70	0.7	35	9.7	5	·	·	1	1	·	·	2	3	12	8	·	–	·	–
IX	3.5	1.3	0.5	3.0	·	·	·	·	14	2.1	3	2.3	2	1.5	1	3.0	66	0.5	91	19.6	18	·	·	11	·	·	·	7	10	15	12	5	–	·	–
X	4	1.0	2	2.0	1	1.0	1	3.0	15	2.2	3	1.3	1	2.0	·	·	66	0.5	10	2.9	31	·		18	·	·	·	17	6	8	5	·	–	·	–
XI	3	1.0	·	·	·	·	·	·	31.5	4.6	1	5.0	0.5	1.0	·	·	54	1.7	144	27.9	19	2	8	18	·	2	·	1	18	19	19	4	–	15	–
XII	8.5	1.6	3	6.0	·	·	·	·	7.5	4.1	3	4.5	0.5	12.0	6.5	7.2	64	1.4	52	31.5	14	20	23	31	·	3	·	6	10	17	7	1	–	31	–
Rok	80.5	2.2	36	2.3	7	0.7	3.5	0.9	153.5	3.7	37.5	2.7	21	2.2	18	1.7	738	1.1	1548?	110.8	18 VII	66	84	206	3	14	1	54	140	207	165	55	–	181?	–

Kasprowy Wierch $H_s = 1991 m$ $H_b = 1988,8 m$ $h_w = 15,4 m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	(symbol 1)	(symbol 2)	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	(symbol 3)	(symbol 4)	R
I	17.5	7.1	10.5	6.0	4.5	6.7	1	3.0	14.5	13.2	17	9.4	15.5	7.4	11.5	8.3	1	8.4	118	17.9	28	15	25	31	·	25	8	2	13	20	15	5	23	31	·
II	24	10.7	12	7.4	2	3.8	4.5	3.7	14.5	6.8	7	11.1	8	10.1	10	12.2	2	8.7	169	31.8	14	23	28	28	·	19	9	·	18	26	20	6	26	28	·
III	12	10.7	15	10.1	2.5	6.6	2	3.0	20	9.8	22	7.7	6	5.8	4.5	5.3	9	7.8	146	24.9	7	20	27	31	·	21	9	1	23	27	20	5	25	31	·
IV	17	5.6	8.5	3.5	6	4.7	11	6.9	19.5	9.0	9	6.6	7	7.5	4	5.8	8	6.0	195	70.5	6	3	12	21	·	14	6	2	12	16	13	6	18	30	1
V	12	4.6	4	4.4	0.5	5.0	6	7.7	27.5	7.1	12.5	6.6	11	7.4	14.5	5.4	5	6.0	211	32.9	20	3	8	22	·	17	2	·	20	29	22	9	28	28	8
VI	24.5	4.8	16.5	5.2	·	·	1.5	4.3	6.5	7.5	13	4.7	12	3.3	10	4.2	6	4.5	339	68.4	5	·	5	15	·	9	3	·	19	20	14	10	21	16	7
VII	18	4.5	14.5	3.2	3	2.2	0.5	10.0	6	5.5	12.5	5.1	17.5	5.3	16	4.7	5	4.3	298	143.8	18	·	·	8	·	12	1	2	16	18	15	5	22	4	10
VIII	11.5	4.2	4	2.5	0.5	3.0	2.5	6.4	13	7.5	18.5	6.5	23.5	5.8	12.5	5.4	7	5.3	74	18.8	15	·	·	1	·	15	3	·	7	14	10	3	15	·	6
IX	14.5	3.9	2	2.2	1.5	3.3	3	3.0	16	5.9	25.5	5.9	14	7.5	6.5	5.5	7	5.1	108	29.7	18	·	4	14	·	13	3	4	9	15	12	4	18	11	2
X	12	4.3	16	3.6	6.5	2.8	7	5.3	17	6.7	15	5.2	6	5.2	2.5	1.8	11	4.2	23	8.5	6	·	3	15	·	10	·	16	8	8	4	·	13	3	·
XI	4.5	3.7	6.5	4.8	2.5	6.0	14.5	7.4	42.5	8.0	14	9.5	0.5	9.0	3	6.2	2	7.4	212	23.0	23	3	19	22	·	16	7	3	19	20	20	8	23	20	·
XII	8.5	6.5	28	4.9	6	5.8	2	10.0	18.5	13.2	13.5	7.3	2.5	7.0	5	2.0	9	6.9	124	23.8	14	22	29	31	·	15	7	5	16	21	17	4	20	31	·
Rok	176	5.9	137.5	4.8	35.5	4.2	55.5	5.9	215.5	8.3	179.5	7.1	123.5	6.8	100	6.0	72	6.2	2017	143.8	18 VII	89	160	239	·	186	58	35	180	234	182	65	252	233	34

UWAGA. *Kierunki i prędkości wiatru - wg anemografu, w okresach oblodzenia tego przyrządu prędkość wiatru mierzono anemotachimetrem.*

Dolina Pięciu Stawów $\varphi = 49°13'$ $\lambda = 20°03'$ 1962

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.7	-9.3	5.2	1	-22.4	31	-5.8	-4.5	-5.7	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	69	61	71	67
II	–	–	–	–	-6.1	-14.6	-0.3	19	-24.2	25	-10.4	-8.6	-9.5	-9.5	–	–	–	–	–	–	–	–	–	–	–	–	80	74	87	80
III	–	–	–	–	-5.0	-13.7	4.4	31	-24.2	8	-9.3	-7.7	-8.8	-8.6	–	–	–	–	–	–	–	–	–	–	–	–	80	80	79	80
IV	–	–	–	–	5.8	-1.7	14.7	25	-9.0	3, 30	2.0	3.5	1.4	2.1	–	–	–	–	–	–	–	–	–	–	–	–	59	68	53	60
V	–	–	–	–	6.4	-0.7	14.2	9	-13.5	3	2.0	4.2	3.0	3.0	–	–	–	–	–	–	–	–	–	–	–	–	75	85	68	76
VI	–	–	–	–	8.6	1.3	19.7	16, 24	-11.3	7	4.3	6.6	4.4	4.9	–	–	–	–	–	–	–	–	–	–	–	–	67	83	54	68
VII	–	–	–	–	11.5	4.5	21.6	27	-0.9	5	7.0	9.7	6.9	7.6	–	–	–	–	–	–	–	–	–	–	–	–	74	81	65	73
VIII	–	–	–	–	15.1	6.6	21.4	5	1.7	31	9.4	12.9	10.2	10.7	–	–	–	–	–	–	–	–	–	–	–	–	46	69	44	53
IX	–	–	–	–	9.9	2.4	19.9	4	-3.3	23	4.7	7.8	5.7	6.0	–	–	–	–	–	–	–	–	–	–	–	–	53	62	49	55
X	–	–	–	–	9.0	1.2	15.4	1	-4.6	21	3.2	6.6	4.4	4.6	–	–	–	–	–	–	–	–	–	–	–	–	42	46	40	43
XI	–	–	–	–	2.1	-2.8	9.3	4	-12.1	17	-0.5	0.1	-0.4	-0.3	–	–	–	–	–	–	–	–	–	–	–	–	74	78	65	72
XII	–	–	–	–	-4.8	-12.1	1.7	30	-25.0	23	-8.3	-7.1	-8.5	-8.1	–	–	–	–	–	–	–	–	–	–	–	–	67	63	45	58
Rok	–	–	–	–	4.2	-3.2	21.6	27, VII	-25.0	23, XII	-0.1	2.0	0.3	0.6	–	–	–	–	–	–	–	–	–	–	–	–	66	71	60	66

Morskie Oko $\varphi = 49°12'$ $\lambda = 20°04'$

I	–	–	–	–	-0.1	-8.7	8.2	1	-19.4	8	-4.6	-3.6	-5.1	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	57	56	59	57
II	–	–	–	–	-3.5	-12.9	1.8	27	-21.8	25	-9.9	-6.3	-8.1	-8.1	–	–	–	–	–	–	–	–	–	–	–	–	68	75	75	73
III	–	–	–	–	-2.1	-11.4	8.3	31	-20.4	14	-8.4	-4.4	-7.6	-7.0	–	–	–	–	–	–	–	–	–	–	–	–	69	72	75	72
IV	–	–	–	–	7.1	-0.3	15.1	25	-11.0	30	1.8	4.7	2.5	2.9	–	–	–	–	–	–	–	–	–	–	–	–	53	67	53	58
V	–	–	–	–	8.4	0.1	14.8	8	-10.2	2	2.7	5.9	3.5	3.9	–	–	–	–	–	–	–	–	–	–	–	–	71	80	72	74
VI	–	–	–	–	10.7	2.9	22.2	24	-3.7	7	5.2	8.4	5.6	6.2	–	–	–	–	–	–	–	–	–	–	–	–	71	81	69	74
VII	–	–	–	–	14.0	5.1	24.6	27	-1.0	5	7.7	11.9	8.1	9.0	–	–	–	–	–	–	–	–	–	–	–	–	60	72	66	66
VIII	–	–	–	–	18.0	7.3	24.8	13	0.0	31	10.2	15.2	11.5	12.1	–	–	–	–	–	–	–	–	–	–	–	–	43	58	40	47
IX	–	–	–	–	12.8	2.6	21.9	16	-2.1	25	5.0	10.4	5.9	6.8	–	–	–	–	–	–	–	–	–	–	–	–	52	58	40	50
X	–	–	–	–	11.2	1.2	17.3	4	-3.6	21	2.7	8.9	3.4	4.6	–	–	–	–	–	–	–	–	–	–	–	–	31	39	31	34
XI	–	–	–	–	3.5	-2.3	11.6	4	-11.3	29	0.5	1.5	0.4	0.7	–	–	–	–	–	–	–	–	–	–	–	–	69	69	72	70
XII	–	–	–	–	-3.8	-12.7	4.8	9	-23.6	23	-8.1	-7.1	-8.0	-7.8	–	–	–	–	–	–	–	–	–	–	–	–	56	59	49	55
Rok	–	–	–	–	6.4	-2.4	24.8	13, VIII	-23.6	23, XII	0.4	3.8	1.0	1.6	–	–	–	–	–	–	–	–	–	–	–	–	58	66	58	61

Ustrzyki Górne $\varphi = 49°07'$ $\lambda = 22°40'$

I	–	–	–	–	-0.3	-5.4	5.6	22	-14.0	31	-3.1	-1.7	-2.7	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	89	82	74	82
II	–	–	–	–	-1.7	-10.9	2.9	27	-29.3	25	-7.5	-2.9	-5.9	-5.6	–	–	–	–	–	–	–	–	–	–	–	–	83	80	78	80
III	–	–	–	–	0.0	-6.9	11.5	5	-26.4	20	-4.9	-1.1	-3.5	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	90	81	78	83
IV	–	–	–	–	14.0	0.0	24.6	22	-6.7	2	4.0	12.5	4.5	6.4	–	–	–	–	–	–	–	–	–	–	–	–	52	59	37	49
V	–	–	–	–	15.0	3.8	23.9	28	-4.7	2	8.2	13.2	8.3	9.5	–	–	–	–	–	–	–	–	–	–	–	–	75	75	58	69
VI	–	–	–	–	16.6	5.6	26.9	24	-1.0	14	10.7	15.3	9.7	11.4	–	–	–	–	–	–	–	–	–	–	–	–	71	80	69	73
VII	–	–	–	–	18.1	7.5	27.1	27	0.8	10	12.1	16.9	11.0	12.8	–	–	–	–	–	–	–	–	–	–	–	–	65	74	55	65
VIII	–	–	–	–	21.6	8.9	27.0	7	-0.1	31	12.5	20.8	13.6	15.1	–	–	–	–	–	–	–	–	–	–	–	–	52	63	47	54
IX	–	–	–	–	16.3	4.1	24.2	5	-2.0	15	7.3	15.4	8.5	9.9	–	–	–	–	–	–	–	–	–	–	–	–	66	57	30	51
X	–	–	–	–	13.5	-1.2	20.8	4	-8.2	17	1.4	13.1	2.5	4.9	–	–	–	–	–	–	–	–	–	–	–	–	51	35	25	37
XI	–	–	–	–	8.7	0.1	19.8	1	-10.7	18	2.9	7.1	2.9	4.0	–	–	–	–	–	–	–	–	–	–	–	–	91	77	70	79
XII	–	–	–	–	-2.4	-9.9	5.8	14	-20.6	3	-6.8	-4.3	-7.0	-6.3	–	–	–	–	–	–	–	–	–	–	–	–	92	84	86	87
Rok	–	–	–	–	10.0	-0.4	27.1	27, VII	-29.3	25, II	3.1	8.7	3.5	4.7	–	–	–	–	–	–	–	–	–	–	–	–	73	71	59	68

Dolina Pięciu Stawów $H_s = 1668\,m$ $h_w = 13{,}6\,m$ 1962

MIESIĄC	ROZKŁAD WIATRU *D, ▼=D																		OPAD R			LICZBA DNI (n)															
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr ▼		⊙	⊕	Opad R			≡	▨	▨
	n	▼	n	▼	n	▼	n	▼	n	▼	n	▼	n	▼	n	▼	n					Min < -10°	Max < 0°	Max < 0°	Max > 25°	≥ 10 ▼	≥ 15 ▼			≥ 0.1 R	≥ 10 R	≥ 100 R			R
I	8	3.8	·	·	19	5.6	·	·	12	5.3	10	6.8	44	7.2	·	·	·	6.3	–	–	–	10	19	31	·	11	2	2	12	–	–	–	6	31	–
II	35	8.4		·	2	2.0	·	·	17	7.5	·	·	16	5.7	·	·	14	6.2	–	–	–	23	28	28	·	12	4	2	16	–	–	–	6	28	–
III	10	4.4	·	·	15	7.0	·	·	22	6.4	13	9.8	11	8.6	3	10.0	19	5.9	–	–	–	21	24	30	·	16	3	1	18	–	–	–	12	31	–
IV	3	1.0	1	4.0	5	4.2	·	·	2	6.0	30	5.4	11	5.3	1	10.0	37	3.0	–	–	–	·	5	19	·	6	1	5	9	–	–	–	11	30	–
V	1	2.0	1	1.0	1	2.0	·	·	3	2.0	36	6.0	13	2.4	1	2.0	37	2.8	–	–	–	2	5	15	·	2	2	·	15	–	–	–	7	31	–
VI	15	2.5	·	·	5	3.4	·	·	1	2.0	5	4.0	4	4.0	·	·	60	1.9	–	–	x	1	6	14	·	2	1	3	11	–	–	–	11	25	–
VII	5	2.2	3	13.0	13	4.7	·	·	12	3.6	7	4.4	18	3.0	·	·	35	2.6	–	–	–	·	·	1	·	2	2	2	14	–	–	–	3	·	–
VIII	13	2.4	·	·	3	3.0	·	·	8	3.9	32	6.2	12	4.6	·	·	25	3.5	–	–	–	·	·	·	·	5	2	2	4	–	–	–	5	·	–
IX	10	3.4	8	3.0	3	3.0	·	·	8	3.5	25	4.8	12	5.3	·	·	24	3.0	–	–	–	·	3	10	·	1	·	6	10	–	–	–	2	10	–
X	10	2.4	·	·	1	1.0	·	·	4	7.8	9	5.4	13	6.7	·	·	56	2.1	–	–	–	·	·	11	·	3	1	15	9	–	–	–	7	1	–
XI	3	3.3	5	1.6	5	2.2	2	10.0	7	2.9	24	7.0	29	6.1	·	·	15	4.6	–	–	–	1	13	21	·	8	1	3	14	–	–	–	5	15	–
XII	3	1.7	8	4.6	6	3.8	1	1.0	·	·	17	11.7	30	8.6	·	·	28	5.6	–	–	–	18	26	31	·	11	6	6	12	–	–	–	4	31	–
Rok	116	3.5	26	2.3	78	3.5	3	0.9	96	4.2	208	6.0	213	5.6	5	1.8	350	4.0	–	–	–	76	129	211	·	79	25	47	144	–	–	–	79	233	–

Morskie Oko $H_s = 1400\,m$ $h_w = 14\,m$

I	15	3.3	1	6.0	6	4.0	3	8.7	9.5	7.2	13.5	9.0	9	7.7	·	·	36	3.9	91	23.7	27	14	12	31	·	10	4	6	11	18	15	2	6	31	·
II	21	8.7	1	3.0	4	7.2	4	9.2	5	4.6	6	6.2	5	9.2	5	5.5	33	4.5	138	23.8	17	20	25	28	·	8	5	1	13	24	18	5	2	28	·
III	19.5	2.9	8.5	3.6	3	3.0	3	3.0	11.5	9.5	13.5	9.9	3	2.0	·	·	31	3.8	117	23.6	4	20	21	29	·	8	4	·	13	25	17	3	8	31	·
IV	20	2.6	3	9.7	6	6.0	9	9.9	11	6.3	6	11.2	7	6.6	2	4.0	26	4.4	157	61.0	6	1	2	18	·	8	4	6	9	17	16	5	2	30	·
V	23	2.8	1	5.0	3.5	3.7	5	2.8	5.5	4.0	13.5	7.1	12	4.1	0.5	6.0	29	2.9	311	48.8	20	1	1	15	·	4	3	·	14	27	23	11	2	17	1
VI	41	2.9	·	·	2	3.5	3	3.0	6	2.4	12	3.7	5	2.8	3	2.0	18	2.4	191	38.9	1	·	2	9	·	·	·	·	14	17	14	7	1	9	5
VII	19	2.4	8	3.4	7	4.0	7.5	3.6	8.5	3.0	8	2.5	2	2.0		·	33	1.9	262	85.0	18	·	·	1	·	·	·	1	9	21	16	5	1	·	6
VIII	16.5	2.5	7	3.5	4.5	3.8	9.5	6.7	10.5	6.2	10	4.8	4	4.2	·	·	31	3.0	65	21.3	15	·	·	·	·	6	·	4	4	15	8	2	·	·	4
IX	16	3.1	2	4.2	6	4.2	3	2.0	12.5	5.8	3.5	8.0	4	2.5	2	5.0	41	2.3	127	36.2	18	·	·	7	·	3	·	7	7	16	12	4	·	6	·
X	27.5	2.4	·	·	·	·	·	·	4	2.8	5	6.4	10	2.5	1.5	3.7	45	1.5	14	6.0	31	·	·	10	·	2	1	18	7	9	4	·	2	·	·
XI	11	2.3	4	5.8	3	9.0	2	10.0	9.5	5.2	17.5	10.8	·	·	2	6.0	41	3.8	316	42.6	19	2	11	20	·	12	4	2	15	20	19	12	8	16	·
XII	14.5	2.9	3.5	3.6	2.5	9.6	7.5	9.3	6.5	5.4	9.5	7.2	5	5.4	·	·	44	3.0	89?	26.5	14	20	23	31	·	7	3	8	5	19	15	3	1	31	·
Rok	244	3.2	39	4.0	47.5	4.8	56.5	5.7	100	5.2	118	7.2	66	4.1	16	2.7	408	3.1	1878?	85.0	18. VII	78	97	199	·	68	28	53	121	227	172	59	33	199	16

Ustrzyki Górne $H_s = 650\,m$ $h_w = 20\,m$

I	11	7.1	5	3.8	·	·	1	3.0	4.9	6.1	11	6.8	·	·	·	·	16	5.1	61	18.5	13	5	14	26	·	8	3	1	17	16	13	1	1	30	–
II	19	7.8	7	7.0	·	·	1	4.0	2.8	7.1	2	4.0	1	4.0	2	11.0	24	5.2	124	38.4	13	10	20	28	·	10	3	2	20	16	12	3	1	28	–
III	21	9.0	14	4.8	1	2.0	2	3.5	3.7	7.7	1	3.0	1	9.0	·	·	16	6.1	132?	40.3?	30?	7	15	27	·	14	3	·	22	27	15	4	1	31	–
IV	9	4.8	11	2.9	2	7.0	2	5.5	2.3	6.1	2	6.0	2	2.5	2	5.5	37	3.0	80	23.5	6	·	·	12	·	3	1	5	4	14	7	4	1	5	–
V	11	3.0	8.5	2.9	·	·	2	3.0	32.5	4.9	3.5	7.9	·	·	0.5	2.0	35	2.7	130	23.0	20	·	·	7	·	1	·	1	9	21	19	3	4	·	–
VI	9	5.0	15	4.3	·	·	1	9.0	13.5	5.4	4.5	5.0	1	1.0	2	3.5	44	2.5	189	39.4	5	·	·	2	5	·	·	1	15	18	15	7	3	·	–
VII	10.5	3.6	13.5	3.4	2	2.0	·	·	18.5	5.1	3.5	5.4	1	2.0	·	·	44	2.2	174	28.2	19	·	·	·	2	·	·	3	11	19	18	7	2	·	–
VIII	5	4.2	8	3.5	·	·	·	·	19	5.0	3	5.3	·	·	·	·	58	1.7	76	26.6	18	·	·	1	8	·	·	2	7	13	11	3	3	·	–
IX	4	3.2	6	3.8	·	·	·	·	22	5.2	13	5.0	1	2.0	·	·	44	2.4	79	22.9	17	·	·	5	·	3	·	5	11	13	11	3	4	·	–
X	6	3.6	19	3.2	·	·	2	4.5	21	5.8	1	2.0	·	·	·	·	44	2.3	3	2.0	2.0	·	·	16	·	2	·	12	4	5	1	·	6	·	–
XI	5	4.4	14	3.8	·	·	1	5.0	2.5	6.0	7	5.5	1	5.0	·	·	37	3.0	109	25.5	20	2	1	15	·	5	·	1	17	19	14	4	4	5	–
XII	14	7.0	18	4.3	1	2.0	3	3.0	32.5	5.6	5.5	3.5	·	·	·	·	19	4.2	54	17.7	14	15	22	31	·	7	1	1	24	14	11	1	2	31	–
Rok	124.5	5.2	13.9	4.0	6	1.1	15	3.4	32.1	5.8	5.7	5.0	8	2.1	6.5	1.8	418	3.4	121.1?	40.3?	30. III?	39	72	170	15	53	11	34	161	195	147	40	32	130	–

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TABLICA III

DATY OSTATNIEGO I PIERWSZEGO PRZYMROZKU

DATES LIMITES DU GEL

Stacja	Temperatura spadła poniżej 0°		Okres bez przymrozków /dni/
	po raz ostatni	po raz pierwszy	
Aleksandrowice	3.V	16.X	165
Antołówka	7.VI	25.IX	109
Babia Góra	8.VI	20.IX	103
Baligród	4.V	26.IX	144
Bartoszyce	6.V	13.X	159
Barwinek	7.V	14.IX	129
Bełsk	6.V	25.IX	141
Biała Podlaska	3.V	11.X	160
Białowieża	4.V	11.X	159
Biały Kościół	3.V	11.XI	191
Białystok	4.V	11.X	159
Biebrza	3.VI	25.IX	113
Biecz	7.V	11.X	156
Bielsk Podlaski	3.V	11.X	160
Bieruń Stary	5.V	16.X	163
Biłgoraj	5.V	13.X	160
Bircza	5.V	26.IX	141
Biskupiec	6.V	13.X	159
Bochnia-Chodenice	2.V	25.IX	145
Bodzentyn	1.V	15.X	166
Bolesławiec	-	16.X	-
Borusowa	2.V	16.X	166
Brwinów	6.V	16.X	162
Brzegi Dolne	19.V	15.IX	118
Brzezna	2.V	17.X	167
Bukowina Tatrz.	7.VI	16.X	130
Busko-Zdrój	3.V	16.X	165
Bydgoszcz	6.V	14.X	160
Bydgoszcz, IMiUZ	6.V	16.X	162
Bystrzyca Kłodzka	5.V	15.IX	132
Bytom	3.V	16.X	165
Chełm Lubelski	3.V	11.X	160
Chodzież	3.V	16.X	165
Chojnice	3.V	16.X	165
Chorzelów	2.V	11.X	161
Ciechocinek	6.V	15.X	161
Cieplice Śl.-Zdrój	8.VI	15.IX	98
Cieszyn	3.V	16.X	165
Cieszyn-Bobrek	5.V	25.IX	142
Ciężkowice	5.V	11.X	158
Czarna Dąbrówka	3.V	15.X	164
Czarniecka Góra	6.V	15.IX	131
Czarny Dunajec	12.V	10.IX	120
Czernichów	1.V	16.X	167
Częstochowa	3.V	11.X	160
Czorsztyn	7.V	16.IX	131
Czorsztyn-Nadzamcze	7.VI	10.IX	94
Darłowo	3.V	28.X	177
Dębica	1.V	15.X	166
Długopole-Zdrój	3.VI	15.IX	103
Dobrogoszcz	1.V	21.X	172

Stacja	Temperatura spadła poniżej 0°		Okres bez przymrozków /dni/
	po raz ostatni	po raz pierwszy	
Dolina Chochołowska	9.VI	10.IX	92
Dolina Pięciu Stawów	5.VII	9.IX	65
Drawno	3.V	15.X	164
Duszniki-Zdrój	6.VI	21.X	136
Dynów	2.V	15.X	165
Dziwnów	29.III	17.XI	232
Elbląg	1.V	16.X	167
Felin	1.V	11.X	162
Garlica Murowana	1.V	16.X	167
Gdańsk-Nowy Port	1.V	28.X	179
Gdańsk-Siedlce	1.V	28.X	179
Gdańsk-Wrzeszcz	1.V	28.X	179
Gdynia	30.III	21.X	204
Giżycko	2.V	28.X	178
Gliwice	3.V	17.X	166
Głodowo	6.V	15.X	161
Głogów	1.V	16.X	167
Głubczyce	3.V	16.X	165
Głuchołazy-Zdrój	3.V	22.X	171
Gniezno	1.V	11.X	162
Goczałkowice	1.V	25.IX	146
Gołdap	6.V	11.X	157
Gorzów Wlkp.	29.III	16.X	200
Gorzyń	1.V	17.XI	199
Goszyce	3.V	16.X	165
Góra Św. Anny	3.V	11.XI	191
Grabowiec	1.V	11.X	162
Grabownica	5.V	15.IX	132
Grodków	1.V	16.X	167
Grudziądz	2.V	16.X	166
Gryfice	5.V	28.X	175
Gubałówka	8.VI	16.X	129
Hala Gąsienicowa	5.VII	9.IX	65
Hala Ornak	5.VII	31.VIII	56
Hel	6.V	27.X	173
Hopowo	6.V	15.X	161
Horyniec	5.V	15.IX	132
Inowrocław	1.V	16.X	167
Istebna-Kubalonka	7.VI	10.XI	155
Istebna-Stecówka	5.V	16.X	163
Istebna-Zaolzie	13.VI	2.IX	80
Iwonicz-Zdrój	2.V	15.X	165
Jabłonka	9.VI	10.IX	92
Jabłonowo Pomorskie	6.V	16.X	162
Jakubowice	27.III	15.IX	171
Janów Lubelski	4.V	16.X	164
Jarosław	30.IV	16.X	168
Jasło	2.V	16.X	166

Stacja	Temperatura spadła poniżej 0°		Okres bez przymrozków /dni/
	po raz ostatni	po raz pierwszy	
Jastrowie	6.V	13.X	159
Jastrzębie-Zdrój	3.V	16.X	165
Jazy	4.V	25.IX	143
Jelenia Góra	8.VI	15.IX	98
Jeziory	3.V	16.X	165
Kalisz	3.V	16.X	165
Kamienica	7.V	25.IX	140
Kamienica Królewska	6.V	13.X	159
Kamień Krajeński	6.V	16.X	162
Karpacz	6.VI	16.X	131
Kartuzy	2.V	15.X	165
Kasprowy Wierch	9.VII	31.VIII	52
Katowice	3.V	16.X	165
Kętrzyn	6.V	13.X	159
Kielce	3.V	13.X	162
Kisielnica	3.V	11.X	160
Klimczok	-	22.IX	-
Kłodzko	5.V	15.IX	132
Kmiecin	-	16.X	-
Kobylec	1.V	16.X	167
Kolbuszowa	2.V	15.IX	135
Kolno	4.V	11.X	159
Koło	3.V	16.X	165
Kołobrzeg	5.V	15.X	162
Kołobrzeg-Wydma	28.III	17.XI	233
Kołuda Wielka	1.V	16.X	167
Komańcza	30.VI	10.IX	71
Kończewice	4.V	15.X	163
Kopna Góra	3.VI	25.IX	113
Korfantów	1.V	16.X	167
Koszalin	5.V	15.X	162
Kościerzyna	6.V	15.X	161
Kórnik	3.V	16.X	165
Kraków-Chełm	1.V	16.X	167
Kraków-Czyżyny	1.V	16.X	167
Kraków-Nowa Huta	2.V	16.X	166
Kraków, Obserw.Astr.UJ.	1.V	16.X	167
Krasnystaw	1.V	11.X	162
Kraśnik Dolny	11.IV	16.X	187
Kraśnik Lubelski	1.V	16.X	167
Krosno	7.V	27.IX	142
Krościenko	7.V	15.IX	130
Krynica	7.V	16.X	161
Krynica-Góra Parkowa	4.V	16.X	164
Krynica Morska	11.IV	28.X	199
Krzemień	1.V	11.X	162
Krzyż	6.V	13.X	159
Kudowa-Zdrój	6.V	15.IX	131
Kuźnice	7.VI	25.IX	109
Kwidzyń	-	11.X	-
Laskowice Oławskie	1.V	16.X	167
Lądek-Zdrój	5.V	22.X	169
Legionowo	6.V	11.X	157
Legnica	1.V	16.X	167
Lesko	4.V	16.X	164
Leskowiec	7.VI	10.XI	155
Leszno-Strzyżewice	3.V	15.IX	134
Leżajsk	2.V	16.X	166
Lębork	3.V	25.IX	144
Libertów	1.V	16.X	167
Lidzbark	7.V	11.X	156
Lidzbark Warmiński	6.V	11.X	157
Limanowa	5.V	25.IX	142
Lipki	3.V	15.X	164
Lipowa	1.V	11.X	162
Lubaczów	5.V	15.IX	132
Lublin	5.V	11.X	158
Lubliniec	3.V	16.X	165
Luboń Wielki	7.VI	15.X	129
Łagiewniki	6.V	16.X	162
Łącko	5.V	27.IX	144
Łeba	3.V	13.X	162
Łosice	3.V	11.X	160
Łowicz-Blich	6.V	11.X	157
Łódź-Lublinek	3.V	13.X	162
Łódź-Ruda Pabianicka	3.V	13.X	162
Łysa Polana	5.VII	10.IX	66
Maków Podhalański	3.V	16.X	165
Malbork	6.V	15.X	161
Maniowy	7.V	10.IX	125
Miastko	3.VI	14.X	132
Miechów	5.V	11.X	158
Mielec	7.V	11.X	156
Międzybrodzie	28.III	17.X	202
Międzyzdroje	5.V	17.XI	195
Mikołajki	1.V	28.X	179
Mława	6.V	11.X	157
Młochów	1.V	16.X	167
Morąg	-	13.X	-
Morskie Oko	5.VII	10.IX	66
Motycz	1.V	11.X	162
Mszana Dolna	2.V	25.IX	145
Muszyna	7.V	16.X	161
Myczkowce	4.V	16.X	164
Myślenice	28.III	16.X	201
Myślenickie Turnie	8.VI	15.X	128
Namysłów	1.V	15.X	166
Nidzica	6.V	11.X	157
Niepokalanów	6.V	11.X	157
Nisko	2.V	11.X	161
Nowa Wieś	3.V	11.X	160
Nowe Miasto n.P.	6.V	11.X	157
Nowogard	5.V	15.X	162

Stacja	Temperatura spadła poniżej 0°		Okres bez przymrozków /dni/
	po raz ostatni	po raz pierwszy	
Nowy Dwór Gdański	6.V	-	-
Nowy Dwór Mazowiecki	1.V	16.X	167
Nowy Sącz	2.V	17.X	167
Nowy Targ	9.VI	10.IX	92
Nur	1.V	11.X	162
Obidowa	7.VI	25.IX	109
Oborniki Śląskie	30.IV	16.X	168
Ochaby	3.V	16.X	165
Olecko	4.V	15.X	163
Olesno	3.V	11.X	160
Olkusz	5.V	16.X	163
Olsztyn-Dajtki	6.V	11.X	157
Oława-Zwierzyniec	1.V	16.X	167
Opoczno	6.V	11.X	157
Opole	3.V	16.X	165
Opole Lubelskie	1.V	15.X	166
Orneta	6.V	11.X	157
Osowiec	4.V	25.IX	143
Ostrołęka	2.V	11.X	161
Ostroszowice	1.V	16.X	167
Ostrowy	6.V	11.X	157
Ostróda	6.V	13.X	159
Ostrów Wlkp.	1.V	16.X	167
Ostrzeszów	3.V	21.X	170
Otmuchów	5.V	21.X	168
Ożańsk	2.V	16.X	166
Paproć	6.V	15.IX	131
Pętkowo	3.V	16.X	165
Piaszczyna	6.V	14.X	160
Piotrków Trybunalski	3.V	11.X	160
Pisz	7.V	11.X	156
Piwniczna	5.V	16.X	163
Pleszew	1.V	16.X	167
Płock - Radziwie	6.V	16.X	162
Płocko	6.V	16.X	162
Polanica - Zdrój	6.V	21.X	167
Połczyn - Zdrój	6.V	13.X	159
Porąbka	1.V	17.XI	199
Poronin	30.VII	31.VIII	31
Poświętne	6.V	11.X	157
Poturzyn	4.V	11.X	159
Poznań - Ławica	3.V	16.X	165
Poznań - Sołacz	1.V	16.X	167
Prabuty	6.V	13.X	159
Prudnik	5.V	16.X	163
Przasnysz	2.V	11.X	161
Przebędowo	6.V	16.X	162
Przedbórz	3.V	11.X	160
Przehyba	8.VI	15.X	128
Przelewice	2.V	28.X	178
Przemyśl	4.V	16.X	164
Przybroda	3.V	16.X	165

Stacja	Temperatura spadła poniżej 0°		Okres bez przymrozków /dni/
	po raz ostatni	po raz pierwszy	
Pszczela Wola	6.V	11.X	157
Pszczyna	3.V	22.X	171
Ptaszkowa	3.V	16.X	165
Puck	1.V	28.X	179
Puczniew	6.V	13.X	159
Puławy	1.V	16.X	167
Pułtusk	6.V	16.X	162
Raba Wyżna	5.V	25.IX	142
Rabka	3.V	20.IX	139
Racibórz	1.V	17.X	168
Radom	1.V	11.X	162
Radostowo	6.V	13.X	159
Radzyń Podlaski	5.V	11.X	158
Reguły	6.V	11.X	157
Resko	6.V	13.X	159
Rosnowo	6.V	15.X	161
Rozewie	2.V	17.XI	198
Rożnów	30.IV	17.X	169
Różanystok	4.V	15.X	163
Rybnik	1.V	22.X	173
Rymanów - Zdrój	7.V	27.IX	142
Rzeszów - Jasionka	7.V	15.X	160
Sandomierz	2.V	16.X	166
Sanok	4.V	16.X	164
Sejny	4.V	25.IX	143
Siedlce	1.V	11.X	162
Siejnik	4.V	15.X	163
Sielec	3.V	11.X	160
Siemianice	3.V	13.X	162
Siemiatycze	3.V	11.X	160
Sieniawa	5.V	20.IX	137
Sieradz	3.V	15.X	164
Silniczka	3.V	11.X	160
Sinołęka	1.V	11.X	162
Skierniewice	6.V	11.X	157
Skroniów	3.V	11.X	160
Słubice	6.V	16.X	162
Słupca	1.V	15.X	166
Słupia Nowa	1.V	16.X	167
Słupsk	6.V	13.X	159
Smolice	1.V	16.X	167
Sobieszyn	1.V	16.X	167
Sobótka	1.V	16.X	167
Sokołowsko	8.VI	21.X	134
Sokółka	4.V	15.X	163
Spalona	6.VI	13.X	128
Stańcowa	7.VI	16.X	130
Stare Pole	6.V	28.X	174
Stary Sącz	2.V	11.X	161
Staszów	7.V	15.IX	130
Strzelna	6.V	25.IX	141
Strzyżów	5.V	11.X	158

DATY OSTATNIEGO I PIERWSZEGO PRZYMROZKU

Stacja	Temperatura spadła poniżej 0°		Okres bez przymrozków /dni/
	po raz ostatni	po raz pierwszy	
Suchedniów I	7.V	11.X	156
Suchedniów II	-	16.X	-
Sulejów	3.V	15.X	164
Sulęcin	6.V	13.X	159
Suwałki	7.V	14.X	159
Szamotuły	3.V	16.X	165
Szczawnica	7.V	10.X	155
Szczawno-Zdrój	1.V	11.XI	193
Szczecin - Dąbie	6.V	13.X	159
Szczecin - Niebuszewo	1.V	16.XI	198
Szczecinek	5.V	14.X	161
Szczekociny	3.V	11.X	160
Szczerców	3.V	15.X	164
Szczuczyn	4.V	11.X	159
Szczytno	7.V	15.IX	130
Szepietowo	2.V	11.X	161
Szklarska Poręba	8.VI	25.IX	108
Szprotawa	6.V	16.X	162
Szrenica	4.VII	14.IX	71
Szymanów	11.IV	15.IX	156
Śliwice	6.V	11.X	157
Śnieżka	5.VII	9.IX	65
Śrem	3.V	16.X	165
Świbno	6.IV	16.X	192
Świder	6.V	11.X	157
Świdnica	1.V	16.X	167
Świdwin	3.V	15.X	164
Świebodzin	6.V	16.X	162
Świeradów - Zdrój	6.VI	21.X	136
Świerklaniec	3.V	11.X	160
Święty Krzyż	3.V	10.XI	190
Świnoujście	29.III	17.XI	232
Tarnobrzeg	1.V	13.X	164
Tarnogród	2.V	15.X	165
Tarnów	2.V	11.X	161
Tczew	1.V	28.X	179
Terespol	1.V	11.X	162
Tęgoborze	28.III	17.XI	233
Tolkmicko	30.III	17.XI	231
Tomaszów Lubelski	3.V	11.X	160
Topola - Błonie	6.V	16.X	162
Toruń - Wrzosy	6.V	11.X	157
Trzcińsko - Zdrój	1.V	24.X	175
Trzebiechów	6.V	16.X	162
Trzebież	3.V	16.XI	196
Trzebinia	1.V	16.X	167
Trzemeszno	1.V	16.X	167
Turbacz	30.VI	24.IX	85
Tychy	3.V	16.X	165
Tykocin	1.V	15.X	166
Ustka	3.V	28.X	177
Ustka - Wydma	30.III	28.X	211
Ustrzyki Górne	14.VI	31.VIII	77
Wadowice	3.V	16.X	165
Wałcz	6.V	14.X	160
Warka	1.V	15.X	166
Warszawa - Bielany	6.V	16.X	162
Warszawa, Inst. Geogr. UW	1.V	17.XI	199
Warszawa, Obserw. Astr. UW	1.V	16.X	167
Warszawa - Okęcie	6.V	11.X	157
Warszawa, St. Pomp Rzecz.	6.V	16.X	162
Wądołki Borowe	2.V	11.X	161
Werbkowice	5.V	11.X	158
Wielichowo	6.V	16.X	162
Wieliczka	28.III	16.X	201
Wieliszew	6.V	11.X	157
Wieluń	3.V	11.X	160
Wieniec - Zdrój	-	11.X	-
Wierzchowo	6.V	14.X	160
Więcławice	1.V	16.X	167
Wińsko	1.V	23.X	174
Wirty	6.V	13.X	159
Wisła	5.V	25.IX	142
Wisznice	6.V	11.X	157
Witów	7.VI	15.IX	99
Włodawa	4.V	11.X	159
Wojcieszów Górny	6.V	22.X	168
Wolbrom	5.V	11.X	158
Wrocław - Gądów Mały	5.V	16.X	163
Wyrzysk	5.V	15.X	162
Wysowa	7.V	15.IX	130
Wyszków	6.V	11.X	157
Zakopane	5.V	10.IX	127
Zakrzów	1.V	16.X	167
Zamość	2.V	16.X	166
Zamość - Zamczysko	-	11.X	-
Zawodzie	6.V	11.X	157
Zawoja	7.VI	25.IX	109
Zawołocze	6.V	11.X	157
Ząbkowice	5.V	16.X	163
Zbąszyń	6.V	16.X	162
Zdanów	1.V	16.X	167
Zgorzelec	1.V	21.X	172
Zielona Góra	1.V	17.XI	199
Zwardoń	5.V	20.IX	137
Żarnowa	2.V	15.X	165
Żary	1.V	16.X	167
Żegiestów - Zdrój	7.V	16.X	161
Żelechów	1.V	11.X	162
Żelisławki	6.V	15.X	161
Żywiec - Sporysz	5.V	25.IX	142

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TABLICA IV

USŁONECZNIENIE (w godzinach)

INSOLATION (en heures)

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	.	1,9	0,3	.	.	.	0,4	.	1,1	.	0,5	1,8	1,8	.	1,7	.	.	0,2	0,7	.	.	.	0,4	.	.	0,5	.	.	2,3	5,1	4,4	23,1
2	Kołobrzeg	.	0,8	.	.	.	.	1,4	.	1,6	.	.	3,2	2,8	0,2	.	.	0,6	.	0,5	.	.	0,6	.	0,5	.	1,7	.	0,1	1,5	7,4	6,6	29,5
3	Międzyzdroje	0,3	0,6	.	.	.	.	1,8	.	1,0	.	.	2,7	0,8	.	.	.	0,2	.	.	.	.	0,7	0,2	.	.	1,5	0,1	0,9	1,0	6,7	5,4	23,9
4	Resko	0,2	.	.	.	.	.	0,1	.	2,8	.	.	3,7	1,0	.	.	.	0,1	.	.	.	.	0,6	0,1	2,2	.	3,1	0,2	0,2	5,4	6,3	6,6	32,6
5	Szczecinek	.	0,3	.	.	.	.	0,1	.	0,8	.	0,1	2,1	0,9	0,1	.	.	.	.	0,2	.	.	0,1	0,3	2,6	.	1,0	0,1	.	5,2	7,4	6,0	27,3
6	Chojnice	.	0,2	.	.	.	.	.	.	0,1	0,4	0,8	0,6	1,0	0,1	.	0,4	.	.	.	.	.	0,1	1,0	0,4	.	1,5	0,2	0,1	1,0	4,7	3,8	16,4
7	Hel	1,4	.	0,1	.	.	.	1,4	.	.	.	1,8	0,1	2,5	.	.	.	.	.	2,4	0,2	1,2	.	1,3	.	.	3,6	0,2	.	0,1	.	6,1	22,4
8	Gdynia	0,9	0,1	0,1	.	.	0,8	.	.	0,1	.	1,7	0,1	4,8	.	1,1	.	.	.	5,0	0,9	1,1	.	0,7	0,3	.	3,9	1,2	.	0,1	.	6,5	29,4
9	Świbno	0,8	.	.	.	.	.	1,1	.	0,1	.	1,4	0,1	3,2	1,6	.	.	.	.	1,0	0,2	0,9	.	1,1	0,1	.	3,3	0,3	.	1,5	3,9	2,7	23,3
10	Stare Pole	2,6	.	0,2	.	.	.	1,4	.	0,5	.	2,7	.	2,8	.	0,7	0,2	.	0,1	0,6	0,1	0,1	.	2,0	0,2	.	2,1	.	0,1	5,2	6,7	5,9	34,2
11	Radostowo	1,2	.	0,2	.	.	.	2,7	.	1,3	0,3	2,6	0,1	3,4	.	.	.	.	.	2,1	0,3	.	0,1	0,5	.	.	4,7	0,6	.	5,0	5,9	5,2	36,2
12	Prabuty	1,0	.	.	.	.	.	0,5	.	0,6	.	2,5	.	0,6	.	.	.	.	0,1	1,6	.	.	.	1,9	0,3	.	2,3	.	0,2	4,9	5,4	5,4	27,3
13	Bydgoszcz,IMiUZ	1,4	.	.	.	.	.	2,6	.	1,9	0,5	2,1	0,9	2,5	0,4	.	0,5	.	0,7	3,9	0,2	.	0,3	2,6	0,6	.	0,5	0,1	0,6	4,7	6,8	4,7	38,5
14	Suwałki	0,1	.	.	0,3	.	.	0,4	0,4	.	.	2,7	.	0,3	2,1	0,1	.	.	.	.	.	1,4	.	4,3	1,2	.	3,3	.	.	2,3	6,9	5,5	31,3
15	Mikołajki	0,4	.	0,1	.	.	.	0,1	.	.	0,8	2,8	.	0,6	2,0	.	.	.	0,3	1,2	0,1	3,2	.	2,3	0,5	.	3,0	.	0,3	1,2	7,4	6,7	33,0
16	Biebrza	.	.	1,0	0,5	.	.	.	.	.	.	4,2	0,2	.	2,6	.	.	.	.	.	.	2,5	.	4,5	.	.	2,3	.	.	2,5	7,8	2,9	31,0
17	Białystok	.	.	.	.	.	.	.	1,7	.	1,6	5,3	.	.	1,8	.	1,1	.	0,6	.	0,4	0,1	.	4,2	0,1	.	0,6	.	0,5	.	7,3	3,1	28,4
18	Gorzów Wlkp.	.	.	.	.	.	.	1,1	.	1,4	.	.	2,7	1,2	1,1	.	.	0,2	0,8	3,8	0,9	.	0,3	2,8	.	.	2,6	2,3	2,5	2,8	2,4	4,5	33,4
19	Przebędowo	0,6	.	.	.	.	.	0,1	.	2,5	1,5	0,6	.	3,6	1,9	0,2	0,1	.	0,9	3,4	.	.	0,6	2,8	.	.	0,5	1,1	1,6	1,1	7,0	5,9	36,0
20	Przybroda	0,4	.	.	.	.	.	0,1	.	2,6	.	0,5	2,2	4,6	1,7	0,4	0,4	.	0,9	4,3	0,6	.	0,6	3,1	0,1	.	0,3	0,2	2,3	1,8	6,4	5,9	39,4
21	Poznań - Ławica	0,3	.	.	.	.	.	0,1	.	2,3	0,5	0,3	1,7	3,1	1,9	.	0,5	.	1,0	3,4	0,3	.	0,4	4,3	.	.	1,1	1,3	1,6	0,9	5,7	5,1	35,8
22	Plewiska	.	.	.	.	.	.	.	.	2,1	0,4	.	2,0	3,4	2,0	.	0,3	.	1,0	3,4	.	.	1,1	4,1	.	0,1	0,8	0,3	1,7	1,0	5,5	5,4	34,6
23	Kórnik	.	.	.	.	.	.	.	.	2,1	1,1	0,6	1,9	2,7	3,3	.	0,4	.	1,0	2,2	1,6	.	0,2	4,6	.	.	3,3	1,1	1,4	3,3	6,8	7,6	45,2
24	Oborniki Śl.	.	.	.	1,2	.	3,2	0,4	0,7	0,1	3,2	.	2,3	2,8	1,5	.	3,4	.	.	.	3,8	.	.	.	.	.	.	.	3,6	.	.	4,9	31,1
25	Laskowice Oławskie	.	0,2	0,1	3,5	.	4,8	0,1	.	5,1	3,9	1,2	1,7	5,0	2,2	0,2	2,4	.	3,1	0,5	4,9	.	0,6	4,4	.	0,2	0,5	.	0,7	1,3	.	3,3	49,9
26	Ciechocinek	.	.	.	.	.	.	0,1	.	2,7	0,9	2,4	0,4	1,2	0,5	.	1,4	.	0,5	1,9	0,1	.	0,5	2,1	0,6	.	.	.	0,7	0,9	7,0	6,7	30,6
27	Więcławice	0,2	.	.	.	.	.	.	.	3,4	1,7	2,3	.	.	.	3,5	1,1	.	1,5	3,5	2,1	.	0,9	2,6	1,0	.	2,0	0,2	1,0	4,0	6,9	4,9	42,8
28	Legionowo	.	.	.	.	.	.	.	.	1,3	.	5,3	.	3,2	3,1	.	4,6	.	2,3	0,3	1,4	.	0,9	6,1	2,5	.	4,2	.	1,4	0,2	7,4	7,3	51,5
29	Warszawa-Bielany	.	.	.	.	.	.	.	0,1	1,1	0,4	5,0	.	3,1	2,9	.	4,4	.	2,1	0,1	1,5	.	1,2	5,5	3,1	.	3,5	.	1,9	.	6,6	5,3	47,8
30	Warszawa,Min.Kom.	.	.	.	.	.	.	.	0,1	1,1	0,7	3,2	.	2,6	2,9	.	1,6	.	0,4	.	1,0	0,2	3,9	1,5	3,1	.	2,3	.	1,4	.	5,4	5,3	36,7
31	Międzylesie	.	.	.	.	.	.	.	0,2	0,1	1,9	5,4	.	4,5	.	.	5,3	.	3,4	0,2	1,5	.	1,6	5,9	1,8	.	3,6	.	1,9	.	7,2	6,2	50,7
32	Brwinów	.	.	.	.	.	.	.	.	2,4	.	5,1	.	3,8	4,1	.	3,8	.	2,9	.	0,8	.	1,1	5,5	2,5	.	2,3	.	1,3	.	6,2	6,8	48,6
33	Świder	.	.	.	.	.	.	.	.	0,1	0,5	5,4	.	2,8	3,5	.	4,0	.	1,5	.	1,1	.	0,8	6,0	3,5	.	3,4	.	1,4	.	6,5	6,3	46,8
34	Topola-Błonie	.	.	.	.	.	.	.	1,4	3,8	.	3,6	.	.	4,9	.	4,1	.	3,0	.	2,3	.	1,1	5,2	.	.	2,2	.	2,5	0,4	4,0	6,4	44,9
35	Włochów	.	.	.	.	.	.	.	0,1	1,5	.	4,7	.	3,6	4,4	.	4,5	.	.	3,2	1,3	.	1,3	5,6	3,8	.	3,1	.	1,4	.	6,2	6,4	51,1
36	Skierniewice	.	.	.	.	.	.	0,1	.	3,6	0,1	4,9	.	3,2	5,9	.	5,0	.	4,3	.	3,6	.	1,2	6,2	2,1	.	3,0	.	1,4	.	6,1	3,8	54,5
37	Bolsk	.	0,1	.	.	.	.	0,1	0,5	0,3	0,3	5,5	.	2,6	4,6	.	5,2	.	4,2	1,4	0,6	.	1,9	6,7	3,0	.	2,6	.	0,9	.	7,3	2,9	50,7
38	Łódź-Lublinek	.	.	0,1	.	.	.	.	.	4,8	.	3,4	.	2,6	4,3	.	4,2	0,2	3,0	.	4,1	.	1,5	5,8	0,3	.	3,9	.	1,4	.	4,2	4,3	48,1
39	Kalisz	.	0,1	.	.	0,5	.	.	.	4,7	1,2	2,0	0,5	3,7	3,2	.	2,6	.	1,9	.	4,4	.	1,5	4,5	.	.	3,7	0,8	1,9	1,0	3,1	7,3	48,6
40	Wieluń	.	0,4	.	.	.	0,2	.	.	5,5	.	2,2	.	3,7	4,8	.	3,2	0,1	4,8	0,6	6,4	.	1,7	6,0	0,4	.	2,3	.	0,6	0,1	2,7	2,8	48,5
41	Szepietowo	.	.	.	.	.	.	0,1	1,5	0,1	1,5	5,9	.	1,3	3,4	.	2,3	.	1,2	0,8	.	0,9	1,2	4,5	1,2	.	2,4	.	1,5	0,7	7,5	3,2	41,2
42	Bisłowieża	.	.	.	.	.	.	.	2,0	.	2,6	5,9	.	.	1,9	0,1	0,6	.	0,5	.	1,4	0,2	.	6,4	0,1	0,3	0,5	.	0,2	.	7,0	4,5	34,2
43	Terespol	.	.	.	.	.	.	.	2,3	0,8	3,3	6,3	.	.	2,6	.	5,5	.	0,2	.	3,1	.	0,4	6,5	2,0	.	0,5	.	1,6	.	7,3	4,4	46,8
44	Sobieszyn	.	0,6	.	1,0	.	.	.	2,1	3,5	2,4	6,1	.	0,2	4,5	.	4,9	0,1	0,7	1,4	3,5	.	1,3	6,5	2,9	.	2,4	.	1,3	.	7,5	3,0	55,9
45	Puławy	.	0,5	.	1,8	.	.	.	2,0	4,3	1,6	5,9	.	0,3	4,5	.	5,5	.	0,3	0,3	.	4,6	0,8	6,2	1,7	.	2,4	.	0,9	.	6,8	3,8	54,2
46	Chełm Lub.	0,2	.	0,1	.	.	0,7	.	3,5	2,7	3,5	5,1	.	.	2,1	0,1	6,3	0,4	.	1,4	4,1	0,1	0,6	6,8	1,9	.	0,1	.	0,5	.	7,3	2,6	50,1
47	Szczawno-Zdrój	.	0,1	.	5,6	5,1	3,6	3,6	.	2,1	1,4	.	1,8	1,8	2,6	2,5	3,4	.	2,2	1,7	2,9	.	1,1	4,2	.	0,2	0,2	0,5	0,1	.	.	2,1	48,8
48	Śnieżka	.	1,5	0,1	7,9	8,0	6,9	.	0,1	2,9	0,8	.	.	.	.	2,9	1,5	0,7	2,8	.	.	.	.	.	.	.	1,8	.	.	.	2,1	8,0	48,0
49	Opole	.	.	0,5	2,8	.	.	.	5,1	5,3	0,7	1,8	.	3,0	4,3	.	3,2	2,5	2,2	0,1	4,7	.	0,3	4,7	0,5	0,6	0,6	0,6	0,9	.	.	.	44,4
50	Kudowa-Zdrój	.	0,8	0,5	5,0	.	.	4,1	.	2,4	.	.	1,3	0,6	0,3	2,0	5,2	3,9	.	.	.	.	1,5	2,4	.	0,1	1,4	0,2	1,7	0,3	1,2	5,3	40,2
51	Polanica-Zdrój	.	0,1	0,8	5,7	3,7	0,4	4,8	0,1	3,7	0,8	1,0	0,5	0,7	3,0	4,7	4,6	3,3	1,9	0,1	3,2	.	1,9	4,8	.	0,4	0,8	0,8	2,3	0,3	.	2,3	56,7
52	Skroniów	.	.	.	.	4,2	2,3	.	1,6	5,3	.	5,5	.	0,2	3,3	.	5,1	2,8	0,7	.	5,2	.	0,9	5,6	3,4	.	1,4	.	1,2	.	4,9	1,1	54,7
53	Świerklaniec	.	.	1,4	3,1	0,2	3,8	.	0,2	2,6	.	3,1	.	0,4	6,1	1,2	3,3	3,5	2,2	0,1	3,5	.	0,3	5,7	1,4	.	.	.	0,6	.	1,1	0,7	43,9
54	Kraków,Obs.Astr.	.	.	4,6	4,7	2,2	5,9	.	2,8	2,7	.	5,8	.	1,0	6,4	3,7	5,1	4,7	.	.	5,1	0,5	1,4	5,5	4,8	.	.	0,3	1,5	.	.	.	68,7
55	Cieszyn	.	.	2,1	4,3	2,6	1,3	.	1,8	5,2	.	2,1	.	0,7	4,5	5,8	4,9	4,8	0,3	.	4,2	.	0,8	4,1	1,4	.	.	0,1	0,2	.	.	.	51,2
56	Istebna-Kubalonka	0,1	.	4,2	7,6	7,5	.	.	3,1	7,4	.	1,2	.	.	3,2	5,4	5,1	5,1	.	0,4	2,4	.	1,1	5,5	0,9	.	.	.	.	.	.	3,0	63,2
57	Babia	.	.	6,6	6,9	4,7	5,4	.	4,8	5,2	.	5,5	.	.	5,1	6,9	6,5	5,1	0,2	1,2	4,4	.	1,4	5,1	3,5	.	.	.	0,2	.	.	1,2	79,9
58	Jabłonka	.	.	6,5	4,5	2,2	5,6	.	5,1	5,0	0,7	4,5	.	0,1	5,4	5,3	3,9	5,5	0,5	0,9	.	0,3	2,4	3,9	2,5	.	.	.	0,7	.	.	.	65,5
59	Krynica	.	.	6,6	3,5	0,1	.	.	6,3	6,0	.	0,1	.	.	4,2	7,1	6,9	4,9	2,0	0,5	4,9	.	3,4	6,9	5,3	.	.	.	3,2	.	.	0,2	72,1
60	Krynica-Góra Park.	.	.	5,7	3,5	3,9	.	.	5,9	5,2	.	.	0,2	.	4,1	6,7	5,9	4,4	1,2	.	3,3	.	2,7	6,6	5,0	.	.	.	0,4	.	.	.	64,7
61	Muszyna	.	.	6,7	3,9	0,4	.	.	6,4	5,7	.	0,5	0,1	0,1	4,6	4,1	3,8	4,6	2,3	0,5	5,4	.	3,0	4,6	3,9	.	.	0,5	1,3	.	.	0,4	62,8
62	Zakopane	.	.	5,7	4,2	5,1	5,2	.	6,0	2,0	1,7	5,0	.	0,1	3,9	6,5	6,0	3,3	0,4	2,4	5,4	0,2	2,1	5,0	3,8	0,1	.	.	0,1	.	.	2,1	78,3
63	Gubałówka	.	.	6,1	5,6	5,2	5,1	.	5,6	1,9	1,6	5,1	.	0,1	4,6	6,3	6,1	4,3	1,0	3,1	4,7	0,7	2,1	5,0	3,7	.	.	.	0,2	.	.	0,8	78,9
64	Hala Gąsienicowa	.	.	4,4	4,4	4,5	4,2	.	4,6	4,8	.	0,1	.	.	3,6	4,9	5,0	4,1	1,8	2,5	4,4	3,0	2,4	3,5	3,4	.	.	.	.	.	.	1,1	66,7
65	Kasprowy Wierch	.	.	7,8	7,8	7,0	6,6	.	7,4	7,8	0,5	.	.	.	5,5	8,0	7,2	5,8	2,9	4,3	5,6	1,1	3,8	4,7	4,0	.	.	.	0,1	.	.	5,4	103,3
66	Werbkowice	.	.	0,6	.	.	2,7	0,1	3,0	2,3	3,8	6,0	.	.	0,5	0,6	5,8	0,6	0,1	3,0	4,7	0,3	0,3	6,1	5,8	0,1	0,1	.	1,1	.	5,8	0,3	53,7
67	Zdanów	.	.	2,8	0,8	.	3,3	0,1	3,7	6,2	0,1	6,2	.	.	3,8	.	6,4	3,7	.	0,9	5,5	.	1,1	6,5	4,3	.	1,6	.	1,0	0,2	6,6	1,3	66,5
68	Iwonicz - Zdrój	.	.	3,1	0,2	0,9	.	.	4,6	3,2	.	3,4	.	.	0,1	3,2	4,1	1,1	0,8	3,6	1,7	.	3,9	5,1	5,4	.	.	.	0,5	.	.	.	44,9
69	Lesko	.	.	3,2	1,3	4,0	.	6,0	6,5	6,1	.	3,0	.	.	0,7	6,5	6,1	0,1	2,6	4,1	4,7	0,8	2,5	4,3	6,9	.	.	.	0,7	.	0,1	0,3	70,5

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	6,1	.	.	4,4	.	2,9	.	.	2,8	.	2,4	.	7,0	0,8	3,7	.	0,4	6,9	.	3,1	.	1,0	2,5	0,7	5,1	.	.	0,1				49,9
2	Kołobrzeg	6,1	.	.	5,5	.	3,8	.	0,4	4,8	.	4,0	.	6,8	1,9	2,7	0,4	0,5	2,2	.	3,0	0,8	3,7	0,1	1,5	3,7	.	0,2	2,3				54,2
3	Międzyzdroje	6,6	0,1	.	6,2	.	6,3	.	0,4	6,9	.	3,9	.	7,0	3,9	3,0	.	0,6	8,0	.	2,7	1,2	1,1	0,3	2,1	0,3	.	1,3	1,3				63,2
4	Resko	5,5	.	.	4,3	.	3,7	.	0,4	4,2	.	3,1	.	7,2	2,2	3,2	0,4	0,4	5,3	.	0,5	1,9	2,9	0,1	1,6	0,6	0,2	1,2	1,4				50,3
5	Szczecinek	6,1	.	1,4	2,7	.	2,4	.	.	3,7	.	1,2	.	7,1	1,1	4,5	0,2	0,7	5,8	.	0,2	.	1,3	1,1	0,4	0,9	.	.	2,9				43,7
6	Chojnice	3,1	.	1,0	1,1	.	2,8	.	.	2,2	.	1,4	.	8,2	1,4	5,3	.	0,8	3,7	.	.	0,1	1,5	1,8	0,1	1,0	.	1,3	7,0				43,8
7	Hel	3,9	.	1,4	4,1	.	0,3	.	.	.	.	1,9	.	6,2	5,3	1,6	.	0,2	0,7	.	3,4	.	.	0,2	0,6	1,8	.	.	.				31,8
8	Gdynia	6,6	.	1,4	3,5	.	0,2	.	.	0,3	.	1,6	.	6,5	4,9	3,8	.	0,6	0,6	0,2	2,7	.	0,1	0,4	0,1	1,7	.	.	.				35,2
9	Świbno	4,9	.	0,5	2,7	.	.	.	.	.	.	2,9	.	7,4	4,6	0,9	0,1	0,7	0,6	.	1,3	.	2,1	0,2	0,3	4,2	.	3,7	6,1				43,2
10	Stare Pole	5,6	.	0,4	2,7	.	.	.	.	0,5	.	0,9	.	8,0	6,5	1,8	.	0,8	0,2	.	0,8	.	3,2	1,1	0,5	5,4	.	5,0	6,4				49,8
11	Radostowo	5,3	.	0,3	3,4	.	0,1	.	.	0,7	.	2,6	.	8,0	6,1	3,8	.	1,6	5,4	.	0,2	.	4,2	0,7	0,5	5,5	.	3,6	6,2				58,2
12	Prabuty	5,8	0,4	.	.	.	.	0,1	.	0,2	.	.	.	7,6	5,5	1,1	.	0,3	.	0,2	.	.	1,3	2,1	0,1	4,1	.	1,6	5,2				35,6
13	Bydgoszcz,IMiUZ	0,5	0,4	0,4	.	.	1,9	.	.	0,4	.	0,8	.	6,9	6,0	5,1	.	1,1	6,0	.	0,3	.	1,6	0,3	.	0,7	.	.	3,0				35,4
14	Suwałki	6,9	.	1,6	.	.	.	2,7	.	.	3,2	.	.	2,7	5,4	0,3	.	0,5	.	6,1	.	.	2,7	.	0,8	5,5	.	6,1	6,5				51,0
15	Mikołajki	3,0	3,4	2,8	.	.	.	5,5	.	0,3	1,3	.	.	5,0	5,8	6,1	.	0,9	.	4,3	.	.	0,5	0,7	0,3	3,4	.	2,3	5,7				51,3
16	Biebrza	3,5	3,7	2,4	.	.	.	3,9	1,7	0,1	3,2	.	.	4,4	3,1	0,5	.	0,2	.	6,7	.	.	0,8	0,2	.	3,7	.	0,8	6,3				45,2
17	Białystok	2,5	1,6	0,7	.	0,1	.	1,6	3,0	.	5,5	.	.	4,0	.	0,3	.	1,3	.	7,1	.	.	0,5	.	0,6	1,3	.	3,3	6,7				40,1
18	Gorzów Wlkp.	3,0	.	.	3,6	0,3	2,0	.	1,1	3,0	.	3,9	.	4,6	5,7	3,5	.	0,3	7,8	.	1,2	0,9	1,1	1,2	0,5	.	0,5	.	0,7				44,9
19	Przebędowo	0,8	0,5	.	.	.	3,2	.	.	1,2	0,2	1,7	.	4,6	2,3	3,9	.	1,0	3,5	0,7	1,2	0,8	0,5	.	0,2	1,3	.	.	0,6				28,2
20	Przybroda	1,3	.	0,1	1,3	.	2,3	.	.	1,6	0,3	1,2	.	4,2	1,5	6,3	.	0,9	4,8	.	2,3	2,0	0,5	.	0,7	0,6	.	1,3	.				33,2
21	Poznań-Zawica	0,4	.	.	.	.	2,8	.	.	1,4	.	1,0	.	4,2	2,4	4,7	.	0,7	5,3	.	1,2	1,7	0,3	0,5	.	0,8	.	.	1,6				29,0
22	Plewiska	0,4	0,3	.	0,4	.	2,3	.	.	1,2	.	1,6	.	4,1	2,3	5,1	.	0,5	4,4	0,1	1,3	2,0	0,6	0,4	.	0,6	.	.	1,2				28,8
23	Kórnik	1,4	1,3	.	.	.	3,4	.	.	0,7	0,5	1,4	.	3,2	1,9	5,3	.	0,8	3,2	.	1,9	1,0	.	0,4	.	1,7	.	.	0,7				28,8
24	Oborniki Śl.	2,2	.	.	.	.	.	.	.	.	.	3,1	.	4,6	0,8	.	.	.	7,1	.	3,8	2,0	.	3,4	.	3,2	.	.	.				30,2
25	Laskowice Oławskie	1,2	3,2	2,4	.	.	0,8	.	.	0,2	2,6	2,0	.	0,1	3,3	1,7	.	0,6	7,0	.	0,1	1,5	0,1	0,3	.	4,9	1,8	.	.				33,8
26	Ciechocinek	2,0	0,1	.	.	0,4	.	.	.	0,6	.	0,7	6,6	.	3,4	4,2	.	0,3	5,3	.	0,1	.	1,5	0,9	0,1	0,7	.	0,1	3,0				30,0
27	Więcławice	0,8	1,3	0,1	.	.	3,2	.	.	0,4	.	.	.	6,8	6,0	.	.	2,0	3,5	.	0,6	.	0,6	0,5	.	1,6	0,1	0,1	3,2				30,8
28	Legionowo	0,2	2,8	1,5	.	0,1	.	3,1	0,5	1,0	3,2	.	.	3,1	.	6,5	.	1,0	.	0,7	.	.	1,5	0,1	.	1,8	.	0,2	6,0				33,3
29	Warszawa-Bielany	.	2,2	3,6	0,1	0,7	.	3,8	0,8	0,3	2,6	.	.	3,8	.	6,1	.	0,4	0,1	0,3	.	.	0,8	0,1	.	0,5	.	0,1	5,1				31,4
30	Warszawa,Min.Kom.	.	.	.	.	2,8	.	0,4	2,5	.	2,2	.	.	4,8	.	0,5	.	.	0,2	1,3	1,0	.	0,2	.	.	.	.	0,5	4,6				21,0
31	Międzylesie	.	3,5	1,9	.	0,1	.	4,6	0,2	0,1	4,2	.	.	4,3	.	6,2	.	0,7	.	1,0	.	.	0,6	.	0,5	1,1	.	0,8	4,9				34,7
32	Brwinów	.	2,7	3,3	.	0,8	.	3,3	0,8	0,3	4,1	.	.	2,4	.	3,5	0,7	.	.	.	.	.	1,2	.	.	0,8	.	0,1	5,0				29,0
33	Świder	.	3,5	0,1	.	0,1	.	5,0	0,1	0,1	4,4	.	.	2,6	.	4,4	.	0,4	.	0,2	.	.	1,3	.	0,1	.	.	0,2	3,8				26,3
34	Topole-Błonie	1,6	1,0	2,9	.	0,1	1,2	.	.	0,1	0,4	0,3	.	2,4	4,3	1,2	.	0,6	4,4	.	0,9	.	1,1	.	.	1,9	.	.	.				24,4
35	Młochów	0,2	3,2	3,9	.	0,5	.	3,5	0,8	0,4	4,2	.	.	0,7	.	3,9	.	0,2	.	.	0,1	.	0,4	.	.	0,5	.	.	4,3				26,8
36	Skierniewice	1,9	2,4	4,9	.	0,3	.	3,0	1,7	0,5	3,4	0,1	.	1,4	0,2	1,0	.	0,8	.	.	0,2	.	0,6	0,2	.	1,8	.	.	0,2				24,6
37	Belsk	0,1	3,9	.	.	0,6	.	5,7	.	4,5	0,1	.	.	.	3,0	.	0,2	0,3	.	.	.	.	0,4	.	.	0,4	.	.	0,8				20,0
38	Łódź-Lublinek	1,9	2,6	2,3	.	0,4	0,6	1,3	.	0,3	2,3	.	.	0,3	1,1	0,5	.	0,1	2,2	.	0,1	.	0,3	0,5	.	1,9	0,7	.	.				19,4
39	Kalisz	2,5	4,3	3,6	.	.	5,4	.	.	0,4	0,9	0,4	.	1,1	3,0	2,6	.	0,5	4,3	.	1,6	0,4	.	0,4	0,2	3,3	0,2	.	.				37,1
40	Wieluń	0,8	2,7	5,3	.	.	2,1	0,3	.	0,1	2,5	0,1	.	.	3,6	0,7	.	.	2,0	.	0,3	1,4	.	0,2	.	2,3	0,8	0,1	.				25,3
41	Szepietowo	.	4,0	3,3	.	.	.	4,8	3,4	.	6,9	.	.	4,8	0,6	.	.	0,1	.	6,4	.	1,1	.	.	1,6	1,8	.	2,1	5,9				46,8
42	Białowieża	4,1	.	0,4	.	.	.	0,3	3,3	.	2,0	.	.	2,8	.	.	0,3	0,7	.	7,1	.	.	1,2	.	.	0,2	.	4,1	5,9				32,4
43	Terespol	2,0	.	0,2	0,1	2,4	.	.	4,7	.	1,6	.	.	3,5	.	.	0,4	0,7	.	7,3	.	.	1,5	.	0,8	.	.	.	3,0				28,2
44	Sobieszyn	.	2,8	.	.	0,5	.	6,3	3,2	.	4,9	.	.	.	.	0,1	.	0,1	.	4,7	.	.	1,8	.	0,4	0,3	.	0,1	.				25,2
45	Puławy	1,0	0,3	.	.	1,5	.	7,3	1,6	.	3,5	.	.	.	.	.	.	0,2	.	2,9	.	.	0,5	.	0,3	.	0,4	.	.				19,5
46	Chełm Lub.	2,0	1,1	.	.	2,6	.	.	5,8	.	1,4	.	.	.	.	.	0,8	0,3	0,1	6,5	.	.	2,7	0,2	1,4	.	0,5	.	.				25,4
47	Szczawno-Zdrój	1,6	3,5	.	.	.	0,1	.	.	2,7	2,7	2,3	.	.	2,0	0,8	.	.	2,2	.	0,6	1,2	.	1,5	.	1,9	0,6	.	.				23,7
48	Śnieżka	5,0	3,6	0,1	0,6	.	0,2	0,2	0,3	6,0	5,3	0,6	.	.	0,1	.	.	.	.	.	0,6	0,1	.	1,4	.	5,2	1,2	.	.				30,5
49	Opole	2,3	1,9	2,3	.	0,1	2,0	.	0,1	.	2,6	1,3	.	.	3,1	1,5	.	0,3	4,6	.	0,1	2,2	.	.	.	3,9	1,8	.	.				30,1
50	Kudowa-Zdrój	0,3	.	0,3	.	.	0,8	.	.	0,9	1,6	0,2	.	.	3,9	4,4	.	0,2	2,7	.	.	1,2	0,4	1,0	0,5	7,3	4,5	.	.				30,2
51	Polanica-Zdrój	1,0	3,2	.	0,1	.	0,3	.	.	1,1	2,0	1,0	.	.	3,2	2,4	.	.	0,3	3,9	.	0,1	1,2	0,3	2,4	1,7	1,7	.	.				25,9
52	Skroniów	1,9	3,2	.	2,2	.	.	3,1	0,7	.	7,0	0,1	.	.	.	.	.	.	.	.	.	.	0,3	.	.	0,8	1,8	.	.				23,1
53	Świerklaniec	2,3	2,0	.	.	0,6	0,6	2,1	.	.	1,3	.	.	.	0,1	1,3	.	.	2,0	.	.	2,0	.	0,2	.	5,3	2,4	.	.				22,4
54	Kraków,Obs. Astr.	3,2	3,0	.	0,3	2,0	0,2	5,0	.	.	4,0	.	.	.	.	1,0	.	.	1,0	.	.	0,3	1,2	.	0,7	4,2	3,9	0,1	.				30,1
55	Cieszyn	1,2	6,0	.	0,3	0,1	.	0,9	0,3	.	3,5	.	.	.	.	0,3	.	0,3	3,1	.	0,1	0,2	.	0,4	.	3,5	5,0	.	.				25,2
56	Istebna-Kubalonka	5,2	4,8	.	0,7	0,5	.	.	0,9	.	4,6	.	.	.	.	.	.	.	1,9	.	0,3	0,2	1,3	0,5	.	7,8	7,9	0,1	.				36,7
57	Rabka	7,0	5,0	.	1,5	3,0	0,1	7,1	1,8	.	6,4	.	.	.	.	.	.	.	0,3	.	.	0,1	.	0,1	0,4	6,0	7,7	0,8	.				47,3
58	Jabłonka	6,3	4,9	.	1,6	1,8	0,3	6,3	1,0	.	5,2	.	.	.	.	0,6	0,1	.	0,5	0,1	0,7	0,2	1,2	1,5	0,4	5,4	5,6	0,1	3,0				46,8
59	Krynica	5,5	0,3	.	0,5	1,3	0,3	6,5	.	.	5,2	.	.	.	.	.	.	.	.	.	.	0,3	0,8	.	0,3	4,5	6,7	4,9	0,1				37,2
60	Krynica-Góra Park.	5,0	.	.	1,4	1,1	.	6,3	.	.	4,9	.	.	.	.	.	.	.	.	.	.	1,2	.	1,2	.	5,8	6,6	5,1	0,1				38,7
61	Muszyna	5,0	0,4	.	0,8	0,4	7,2	2,6	0,2	.	5,6	.	.	.	.	.	.	.	0,2	.	0,3	0,4	0,2	0,4	.	4,7	7,0	5,8	.				41,2
62	Zakopane	7,0	3,1	.	1,2	3,1	0,1	7,0	1,5	.	7,2	.	.	.	.	.	.	.	.	.	0,4	.	0,4	2,6	1,1	3,3	7,6	1,7	0,5				47,8
63	Gubałówka	5,8	3,3	.	1,1	3,3	0,2	6,3	2,2	.	6,0	.	.	.	.	.	.	.	.	.	0,2	.	.	1,2	0,2	1,9	6,6	1,7	.				40,0
64	Hala Gąsienicowa	6,0	4,7	.	1,1	2,3	.	6,3	2,7	.	6,6	.	.	.	.	.	.	.	.	.	0,3	.	.	3,2	1,5	2,8	7,3	2,6	1,0				48,6
65	Kasprowy Wierch	6,3	3,2	.	2,4	3,6	.	8,0	4,1	.	8,9	.	.	.	.	.	.	.	.	.	0,3	.	0,7	3,5	3,4	4,1	8,8	3,6	0,2				63,1
66	Werbkowice	2,9	2,9	.	.	2,3	.	.	3,4	0,7	.	.	.	.	.	.	1,8	.	.	6,5	.	.	.	0,4	1,3	.	.	2,2	.				26,4
67	Zgierz	0,8	2,5	.	.	1,5	0,2	6,0	2,9	.	5,9	.	.	.	.	0,5	.	0,1	1,7	0,3	0,1	0,3	1,2	.	0,8	0,1	.	.	.				24,9
68	Łomnica - Zdrój	1,4	0,3	.	.	4,3	0,7	3,4	4,4	.	1,6	.	.	.	.	0,3	1,1	0,1	.	.	.	0,2	0,8	.	0,7	3,2	4,0	7,2	.				35,7
69	Łańcut	.	0,9	.	.	3,6	0,4	2,7	1,2	.	.	.	.	.	.	.	1,4	.	.	0,3	.	0,2	0,8	.	1,1	6,4	6,9	7,0	1,4				34,0

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	.	0,1	0,3	.	.	.	6,5	3,2	7,5	3,8	.	.	2,6	7,2	0,9	2,1	0,8	9,4	3,5	3,5	8,4	7,4	9,8	6,4	4,3	6,5	5,7	.	0,4	.	3,2	103,2
2	Kołobrzeg	2,3	.	1,0	.	.	0,6	2,9	7,6	6,6	2,7	.	.	2,6	9,4	3,8	6,4	1,0	10,6	7,0	1,8	5,8	7,6	10,1	6,7	4,9	7,7	4,0	.	9,1	0,3	4,7	127,2
3	Międzyzdroje	.	.	0,4	.	0,1	1,2	3,1	8,6	3,2	1,9	.	0,1	4,8	8,8	1,4	5,9	0,9	11,1	4,5	.	5,5	6,8	8,9	7,4	3,0	10,0	0,3	.	4,0	0,2	3,7	105,8
4	Resko	4,6	0,8	2,1	.	.	0,8	1,7	5,9	5,9	1,3	.	.	2,9	7,7	4,3	5,1	0,5	7,8	3,9	3,5	5,6	7,4	8,5	5,6	4,4	8,8	3,1	.	4,6	0,6	2,7	110,1
5	Szczecinek	4,4	0,1	.	.	.	.	5,0	7,5	6,5	5,0	.	.	2,7	9,2	3,0	0,6	0,1	7,5	5,8	6,7	8,2	10,0	10,2	9,3	10,1	8,8	8,0	.	6,5	1,4	2,0	138,6
6	Chojnice	6,5	.	.	.	.	.	6,3	4,1	5,9	5,6	.	.	3,3	7,1	5,2	.	.	4,8	3,4	5,6	6,7	9,2	7,8	9,4	6,8	8,2	5,7	.	3,5	1,3	3,5	119,9
7	Hel	1,1	.	0,3	0,2	.	.	7,6	4,7	7,4	1,5	.	.	.	5,8	6,1	.	1,5	8,3	5,7	8,5	6,7	9,6	9,5	7,7	7,6	7,8	5,3	.	.	.	0,4	113,3
8	Gdynia	2,5	.	0,2	.	.	.	7,8	6,2	7,7	0,6	.	.	0,3	7,4	4,4	.	3,4	7,7	6,3	7,8	8,1	9,0	9,4	7,5	7,3	5,2	5,4	.	.	.	4,5	118,7
9	Świbno	4,4	.	0,7	.	.	.	7,8	2,9	10,0	2,5	.	.	.	6,9	3,9	.	0,8	8,1	7,2	6,6	0,4	9,5	7,9	3,6	5,4	6,6	.	.	.	.	0,4	95,6
10	Stare Pole	7,4	.	0,5	.	.	.	6,4	3,1	4,7	4,5	.	.	.	9,1	6,4	.	2,0	8,3	7,5	7,5	0,7	10,8	7,1	6,7	8,9	8,5	6,9	.	.	.	1,3	118,3
11	Radostowo	8,6	.	0,3	.	.	.	7,6	4,6	7,8	5,6	.	.	0,8	8,9	4,9	.	1,6	6,6	6,6	8,0	3,2	10,5	9,6	5,7	9,3	8,3	6,3	.	.	.	2,2	127,0
12	Przebuty	7,1	0,1	2,0	.	.	.	7,7	2,0	5,8	4,4	.	.	.	8,4	4,6	.	2,4	9,0	8,7	2,6	4,3	10,8	6,3	6,6	8,5	8,3	7,4	.	.	.	1,5	118,5
13	Bydgoszcz, IMiUZ	8,3	.	0,3	.	.	.	4,2	3,8	6,1	4,6	0,1	.	3,6	8,1	5,0	.	0,2	4,7	3,8	5,1	7,7	10,4	7,8	7,0	6,4	7,4	6,7	0,9	3,2	1,1	1,4	117,9
14	Suwałki	8,2	7,2	0,4	.	.	.	4,2	5,5	9,9	1,0	.	.	.	5,5	1,1	.	.	9,2	7,5	8,8	8,1	10,2	1,0	3,6	11,0	8,7	10,6	9,6	0,2	2,0	.	133,5
15	Mikołajki	8,4	7,1	.	.	.	.	3,8	4,3	5,5	1,1	0,2	.	.	8,0	2,8	.	.	8,9	9,3	8,6	7,2	10,1	2,9	7,8	8,1	3,8	8,6	7,9	.	.	.	124,4
16	Biebrza	6,0	3,8	.	.	0,1	.	3,1	5,7	8,1	1,0	.	.	.	6,3	0,9	.	.	9,1	6,7	9,8	5,7	6,4	.	4,0	9,2	7,4	9,1	8,0	.	0,3	.	110,7
17	Białystok	5,0	0,2	.	0,2	.	.	0,4	6,7	8,3	3,7	.	.	.	10,0	.	.	.	9,9	8,4	6,8	8,0	4,5	0,2	.	8,3	9,1	8,9	8,9	.	0,1	.	107,6
18	Gorzów Wlkp.	3,0	0,1	3,2	.	.	.	6,1	7,4	1,8	1,1	0,5	.	4,3	8,6	4,1	3,7	0,2	7,4	5,8	8,5	5,6	9,2	9,7	9,1	5,2	7,7	3,4	0,9	1,9	2,7	3,4	124,6
19	Przesędowo	4,8	0,7	.	.	.	.	4,9	5,5	5,0	3,5	4,8	.	2,3	9,3	2,7	.	0,6	7,1	2,7	4,1	8,3	10,2	8,1	9,3	7,0	8,3	7,8	1,6	5,9	1,3	2,2	128,0
20	Przybroda	4,4	0,7	.	.	.	.	6,3	6,1	4,6	2,4	4,4	.	4,4	9,7	2,6	.	1,0	7,1	5,6	6,1	8,5	10,3	8,6	9,6	7,4	8,1	9,2	2,3	4,0	1,6	2,3	137,3
21	Poznań-Ławica	3,3	0,6	0,1	.	.	.	5,6	6,3	5,1	2,7	5,8	.	4,9	8,9	1,8	.	0,3	8,0	3,9	4,7	6,5	9,4	7,2	8,2	5,9	8,8	6,9	1,4	3,2	1,6	0,5	121,6
22	Plewiska	2,8	1,4	.	.	.	.	5,1	6,4	4,9	2,6	6,3	.	.	9,5	2,0	.	0,5	8,7	4,6	4,7	8,4	10,2	7,1	8,5	7,1	8,7	7,3	1,7	3,0	1,7	1,9	125,1
23	Kórnik	2,8	.	.	.	.	.	4,9	7,5	7,3	2,6	5,6	.	2,7	9,8	4,0	.	.	8,1	6,0	5,4	8,8	10,8	2,1	7,4	5,9	9,8	8,3	1,6	2,7	1,6	2,5	128,2
24	Oborniki Śl.	.	.	.	.	0,2	2,5	5,8	6,8	5,8	.	.	.	3,1	6,1	.	.	.	5,9	3,8	.	7,7	3,5	2,8	8,1	4,2	9,5	5,1	.	.	.	4,1	85,0
25	Leszkowice Olsewskie	.	3,3	1,9	0,4	.	.	3,6	7,5	7,4	2,1	1,2	.	3,7	5,2	.	.	.	2,3	3,3	4,9	7,7	0,5	.	5,9	7,4	9,7	6,5	2,9	1,6	1,9	1,4	92,5
26	Ciechocinek	8,0	0,2	2,2	.	.	.	2,1	4,9	6,5	4,3	1,5	.	0,6	4,9	2,1	.	0,4	7,3	8,1	7,4	6,2	9,8	2,0	1,5	7,3	8,1	7,9	1,4	2,5	0,2	0,2	107,6
27	Więcławice	7,7	.	1,2	.	.	.	5,2	4,8	5,5	3,4	0,8	.	3,0	8,9	3,3	.	.	5,2	6,7	6,7	7,5	9,5	4,3	8,5	7,4	9,6	7,2	1,2	3,8	0,3	0,9	122,6
28	Legionowo	.	.	2,8	0,8	.	.	4,6	9,3	6,2	3,4	2,8	.	.	9,1	0,7	.	.	10,1	4,2	8,8	9,0	3,9	.	1,2	7,5	8,8	9,0	0,9	0,3	.	0,2	103,6
29	Warszawa-Bielany	.	.	2,9	1,0	.	.	3,9	7,7	5,1	3,3	3,5	.	.	8,5	1,0	.	.	10,4	5,0	10,1	9,6	4,0	.	1,2	9,0	10,0	9,4	2,0	0,9	1,2	1,1	110,8
30	Warszawa, Min.Kom.	.	.	.	1,7	.	.	2,9	7,3	5,7	3,6	3,8	.	.	7,7	1,0	.	.	9,4	3,9	9,4	8,5	1,9	.	0,6	6,0	9,9	8,4	0,7	0,9	0,9	1,4	95,6
31	Międzylesie	.	0,1	4,5	.	.	.	3,1	6,4	5,3	6,3	.	.	.	7,5	0,6	.	.	10,4	4,6	9,9	9,9	2,8	.	7,0	0,6	8,9	9,8	3,0	1,0	0,1	1,7	103,5
32	Erwinów	.	.	2,6	1,1	.	.	2,8	8,0	7,4	3,8	4,4	.	.	6,3	0,9	.	.	9,5	4,4	10,6	10,1	2,8	0,3	.	8,4	11,2	9,6	0,3	1,3	0,6	1,8	108,2
33	Świder	.	0,3	2,3	2,6	.	.	0,9	8,4	5,4	5,2	4,5	.	.	7,6	.	.	.	9,6	1,6	9,4	9,3	1,5	.	0,2	8,0	10,0	8,9	2,8	1,1	0,1	1,2	100,9
34	Topola-Błonie	.	.	0,7	.	.	.	6,0	6,2	9,4	4,5	1,5	.	1,5	9,2	.	.	.	8,8	8,4	4,8	10,4	7,6	0,1	.	8,2	9,9	7,8	1,4	4,6	1,2	1,4	113,6
35	Włochów	.	.	1,4	1,0	.	.	1,6	7,7	7,3	3,3	4,4	.	.	6,9	1,0	.	.	9,5	3,6	10,6	10,2	1,8	.	0,2	10,4	11,0	9,1	1,5	2,4	0,4	1,6	106,9
36	Skierniewice	.	.	1,0	0,7	.	0,1	3,0	8,3	9,8	4,0	4,2	.	0,5	8,1	0,9	.	.	9,6	3,3	9,4	10,6	4,2	.	.	8,9	9,4	9,3	3,2	3,8	0,8	1,9	115,0
37	Belsk	.	.	3,0	1,3	.	.	0,9	4,7	5,5	3,3	.	.	.	6,7	0,4	.	.	10,7	4,1	10,3	9,8	1,5	.	.	8,5	8,3	7,6	3,3	3,5	0,2	1,1	94,7
38	Łódź-Lublinek	.	.	1,8	0,1	.	.	2,4	6,5	9,5	3,5	4,0	.	0,8	4,9	0,4	.	.	8,2	7,4	7,2	9,7	1,2	0,1	.	6,7	10,6	7,9	2,0	4,6	0,5	2,7	102,7
39	Kalisz	.	0,5	2,4	.	.	.	0,8	9,1	8,0	1,2	1,4	.	1,1	8,0	.	.	.	7,1	5,3	3,4	8,9	6,1	0,7	1,4	9,4	10,2	7,5	1,4	4,0	0,9	2,6	101,4
40	Wieluń	.	1,5	1,6	.	0,4	.	0,6	6,2	8,4	0,9	3,7	.	0,8	4,7	.	.	.	7,4	6,1	6,9	9,4	.	.	.	9,7	10,4	8,8	2,8	3,7	0,5	1,3	95,8
41	Szepietowo	2,4	.	5,1	0,8	.	.	2,0	7,6	4,9	2,7	0,6	.	.	8,5	0,9	.	.	8,5	9,9	8,5	10,3	4,1	.	1,4	8,0	9,3	7,9	7,9	.	.	.	111,3
42	Białowieża	4,5	.	0,6	.	.	.	0,3	8,3	7,8	4,7	0,2	.	.	8,6	.	.	.	8,9	4,8	5,2	9,5	2,9	.	.	9,1	9,3	10,4	7,8	.	0,1	0,4	103,4
43	Terespol	.	.	3,3	0,8	.	.	.	9,5	5,1	5,9	.	.	.	9,0	.	.	.	7,5	7,4	4,6	9,8	.	.	.	8,0	9,4	10,1	8,5	.	.	0,1	99,0
44	Sobieszyn	.	.	3,9	2,7	.	.	.	10,1	1,8	2,9	4,8	.	.	8,9	.	.	.	9,8	2,7	7,7	10,3	.	.	.	8,4	8,6	8,3	5,4	3,0	0,2	0,2	99,7
45	Puławy	.	0,1	4,4	1,8	0,6	.	.	8,3	1,5	1,5	4,5	.	.	5,1	.	.	.	8,1	7,6	4,8	9,0	.	.	.	6,2	9,0	8,3	3,4	2,5	0,5	0,4	87,6
46	Chełm Lub.	.	0,5	6,5	2,3	2,3	2,1	.	8,3	2,0	4,0	4,0	.	.	7,9	.	.	.	5,0	8,3	7,5	10,2	.	.	.	2,7	7,6	8,4	7,0	0,9	.	0,3	97,8
47	Szczawno-Zdrój	.	1,0	1,9	.	0,4	.	0,5	7,7	5,9	0,2	0,8	.	3,9	8,8	.	.	.	1,3	4,1	2,1	2,1	0,3	.	5,2	0,6	8,3	3,5	2,7	1,7	2,7	2,2	67,9
48	Świeradów	.	3,2	0,3	.	3,3	.	.	10,6	5,3	1,5	1,4	.	2,8	7,0	0,5	.	0,1	0,3	0,8	1,2	2,3	3,4	.	7,3	1,1	7,2	2,4	0,7	.	.	0,1	62,8
49	Opole	.	1,8	0,2	.	1,0	.	.	7,0	6,0	2,1	0,9	.	2,0	4,6	.	.	.	6,4	4,3	2,4	9,4	.	0,2	6,7	5,9	10,4	9,0	2,3	4,3	0,6	0,8	88,3
50	Kudowa-Zdrój	0,1	.	2,8	1,1	2,8	.	2,5	7,5	5,0	2,4	0,5	.	5,7	6,6	.	.	.	4,0	5,7	7,8	4,7	4,3	0,8	5,6	3,6	10,0	4,0	2,0	0,9	0,2	0,9	91,5
51	Polanica-Zdrój	.	.	2,9	0,7	1,4	0,1	.	7,6	4,9	2,0	0,2	.	5,9	9,2	.	.	.	4,0	2,8	3,1	2,1	.	.	4,8	4,8	8,5	4,2	5,6	2,2	0,4	1,4	78,8
52	Skromiów	.	0,1	0,5	1,9	1,6	.	.	6,8	9,0	0,7	5,6	.	.	7,3	.	.	.	7,8	8,4	8,2	9,2	.	.	1,1	4,9	9,0	6,6	3,6	5,1	1,0	1,5	99,9
53	Świerklaniec	0,2	.	1,0	1,0	0,3	1,4	.	5,0	7,6	2,4	1,1	.	1,2	5,2	.	.	.	6,9	2,3	2,3	7,6	1,4	.	2,5	7,4	9,5	8,6	1,5	3,2	2,0	1,8	85,4
54	Kraków, Obs.Astr.	.	.	1,3	1,6	1,5	.	.	2,4	8,1	.	1,8	.	2,4	4,1	.	.	0,2	9,0	4,0	8,0	8,1	.	.	0,7	0,7	9,5	9,0	1,4	6,4	4,0	3,6	87,8
55	Cieszyn	.	.	.	0,3	0,6	.	.	2,0	5,5	1,4	.	.	1,0	3,0	.	.	.	0,5	4,3	5,7	6,8	.	.	.	.	7,7	7,8	2,6	5,0	1,2	1,2	56,6
56	Istebna-Kubalonka	0,5	1,5	.	.	1,0	.	.	3,7	9,0	3,7	.	.	1,9	0,2	.	.	0,3	2,0	4,6	7,0	8,7	.	.	.	1,1	10,6	9,7	1,7	4,8	0,4	0,1	72,5
57	Babka	2,6	.	0,5	0,8	2,6	.	.	2,3	8,8	0,9	.	.	0,3	6,3	.	.	.	6,1	8,9	7,5	8,0	.	.	0,8	.	8,2	7,4	1,0	8,9	2,6	1,7	86,2
58	Jabłonka	1,6	.	0,1	.	1,8	.	.	6,9	6,1	0,7	.	.	3,5	4,7	0,9	.	.	3,0	9,1	6,4	4,9	.	0,6	.	.	6,9	7,2	2,1	5,5	2,2	2,3	76,5
59	Krynica	.	.	1,7	.	1,7	1,7	.	4,3	8,8	0,1	.	.	0,3	2,9	.	.	.	3,6	2,6	4,3	4,1	.	.	.	.	8,5	4,7	1,5	4,6	4,4	0,3	60,1
60	Krynica-Góra Park.	.	.	2,1	.	1,3	1,3	.	4,7	7,9	0,1	.	.	0,6	.	.	.	.	5,7	3,1	4,2	6,8	.	.	.	0,1	7,8	4,7	1,1	4,9	4,2	2,9	63,5
61	Baszyna	.	0,2	1,4	.	1,5	0,2	.	4,3	6,0	0,2	.	.	3,7	2,9	.	.	.	2,3	4,3	6,3	4,3	.	.	0,7	0,2	8,3	5,5	3,0	6,3	4,3	0,5	64,4
62	Zakopane	1,0	.	0,1	0,4	2,9	0,8	.	7,8	8,7	1,8	.	.	0,8	5,4	.	.	.	0,3	4,7	2,4	6,7	.	.	.	1,8	9,6	8,4	2,3	6,8	4,2	1,5	78,4
63	Gubałówka	1,7	.	.	0,4	3,6	2,0	.	7,3	8,8	1,5	.	.	0,5	3,1	.	.	.	0,2	5,0	3,4	6,4	.	0,1	.	2,2	8,7	7,8	3,1	6,9	3,7	2,1	78,5
64	Hala Gąsienicowa	2,9	3,8	0,5	.	.	1,8	.	6,5	8,5	1,9	.	.	.	5,9	.	.	.	0,1	3,8	6,8	6,7	.	0,4	0,3	1,9	8,1	8,1	3,6	5,8	2,9	1,8	82,1
65	Zaspromy Wierch	6,9	5,8	.	.	.	2,7	.	8,2	10,4	0,5	.	.	0,2	6,0	.	.	.	.	7,7	4,7	7,9	.	1,8	2,1	1,8	11,4	10,5	2,8	3,2	0,4	0,7	95,5
66	Werbkowice	.	0,7	1,8	1,4	2,3	1,5	.	6,5	4,5	3,4	3,1	.	1,4	6,9	.	.	.	3,0	6,7	8,3	8,4	.	.	.	2,9	8,4	5,9	6,7	0,8	0,1	.	84,7
67	Zamość	.	.	0,3	2,3	2,2	1,6	.	9,2	6,8	0,3	4,0	.	0,4	5,5	.	.	.	8,4	9,5	9,4	10,1	.	.	0,2	2,3	9,7	8,2	2,8	4,1	0,1	1,6	99,0
68	Tomaszów - Zdrój	.	.	1,5	1,8	0,3	0,8	.	3,2	6,7	.	0,5	0,6	0,1	0,3	.	.	0,3	2,6	.	7,1	6,3	.	.	.	.	8,0	4,5	4,9	4,3	0,7	1,9	55,5
69	Lesko	0,2	1,5	1,5	2,2	1,2	2,7	.	2,6	5,5	1,7	0,6	0,4	0,4	0,3	.	.	.	1,9	8,1	4,2	6,7	.	.	.	.	5,5	2,2	3,4	4,2	0,3	0,4	57,7

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	6,9	4,8	4,5	0,6	.	3,8	8,7	.	4,7	6,6	10,5	2,3	6,1	0,5	0,4	7,3	3,1	1,0	2,5	.	8,8	5,2	1,5	10,8	11,7	11,1	3,8	3,8	7,2	4,5		142,7
2	Kołobrzeg	4,4	1,7	5,1	0,8	8,2	1,7	8,4	.	6,8	4,0	11,0	.	3,5	.	0,3	6,5	0,2	1,0	3,9	.	8,7	5,9	.	10,9	10,8	10,3	4,1	7,3	6,4	5,9		137,8
3	Międzyzdroje	3,4	2,5	4,8	1,5	6,7	.	3,9	0,1	4,9	5,5	9,4	0,1	3,0	.	.	7,1	0,1	0,5	2,5	.	8,3	8,7	.	11,9	11,2	6,0	8,3	9,9	7,6	8,4		136,5
4	Resko	3,6	3,0	6,1	1,1	6,3	0,2	6,9	.	6,4	3,9	10,6	1,1	2,7	.	0,2	6,5	0,2	1,4	3,2	.	8,8	9,1	6,1	10,4	10,4	8,2	5,0	8,1	4,2	5,3		139,0
5	Szczecinek	3,1	3,7	6,9	0,4	2,3	2,0	5,4	.	5,2	4,6	10,4	7,3	1,1	.	.	7,0	1,9	1,6	2,9	4,1	9,0	9,4	11,4	11,7	8,9	8,5	2,0	5,6	3,4	3,8		143,6
6	Chojnice	2,4	5,6	5,6	1,2	0,9	1,3	4,7	.	4,9	4,6	8,1	8,2	0,4	.	.	7,1	5,8	2,0	3,6	6,6	9,4	8,6	10,7	10,1	8,9	8,2	1,0	3,6	1,2	2,1		136,8
7	Hel	5,3	3,6	2,3	0,2	.	1,9	11,0	1,0	5,8	7,9	9,1	7,7	3,6	.	0,2	3,9	4,0	1,9	1,3	7,9	9,0	.	9,6	11,3	11,2	9,4	1,7	5,7	8,6	1,6		148,7
8	Gdynia	3,3	7,4	3,7	0,2	.	2,6	10,9	1,1	8,0	7,1	8,5	7,6	3,1	.	.	3,3	2,3	1,4	1,8	7,0	7,4	.	10,6	10,8	11,5	9,6	2,9	0,5	9,8	0,7		143,1
9	Świbno	4,0	5,7	2,2	.	.	0,2	10,1	0,7	3,2	6,6	7,6	5,6	1,9	.	.	5,1	4,0	0,6	.	6,6	8,2	.	6,4	7,2	11,7	8,3	.	6,4	10,7	.		123,0
10	Stare Pole	3,5	6,1	3,5	0,6	.	.	9,0	1,1	5,8	8,2	9,6	6,7	1,3	.	0,1	6,8	7,4	1,4	1,1	7,6	8,5	4,7	9,1	9,3	12,3	7,5	0,7	5,2	11,7	1,9		150,7
11	Radostowo	2,8	6,9	4,2	0,7	.	.	9,4	0,5	6,0	8,7	7,8	7,0	0,4	.	.	6,4	4,3	1,5	1,8	8,5	9,7	3,9	8,5	9,5	12,0	9,5	3,1	5,1	11,2	1,1		150,5
12	Prabuty	2,4	5,2	3,0	0,8	.	4,6	8,2	0,2	6,6	8,3	7,5	5,9	.	.	0,7	8,3	8,0	1,4	1,2	6,9	10,3	5,8	9,8	9,3	12,6	4,1	0,6	5,5	11,8	0,7		149,7
13	Bydgoszcz, IMiUZ	2,4	3,7	5,0	0,3	0,4	3,7	4,9	.	5,8	5,9	8,1	6,1	.	.	.	6,1	5,5	1,3	7,5	4,5	9,7	7,6	9,7	10,3	8,6	5,9	2,7	3,4	4,7	1,5		135,3
14	Suwałki	3,0	8,4	.	7,4	3,0	0,1	.	0,2	3,4	3,7	11,4	6,3	0,4	.	.	4,3	8,5	1,4	0,2	8,9	6,5	7,5	11,8	12,8	13,3	3,5	,	3,5	2,8	0,3		132,6
15	Mikołajki	3,7	7,8	0,6	5,3	0,6	2,0	1,6	.	6,1	8,3	2,1	7,3	0,4	.	.	6,2	9,8	4,2	0,1	8,7	5,9	11,0	7,9	11,4	13,3	3,8	0,6	4,5	0,5	1,4		135,1
16	Biebrza	2,2	6,7	.	7,3	1,3	0,7	.	.	2,9	5,5	7,4	5,8	0,4	.	.	6,1	7,2	3,1	0,4	7,7	5,8	8,7	10,3	11,8	13,0	4,4	0,4	3,2	0,8	1,1		124,2
17	Białystok	0,4	5,5	7,6	.	3,1	.	.	0,2	2,3	3,9	10,7	8,1	2,9	.	1,6	7,5	7,0	2,8	.	8,5	7,3	8,5	11,7	9,9	12,9	7,6	0,1	1,6	3,2	0,8		135,7
18	Gorzów Wlkp.	5,6	3,3	7,7	1,0	4,1	4,4	4,6	.	4,6	4,2	9,9	6,5	4,2	0,4	.	2,2	0,2	1,6	3,2	2,0	4,2	9,3	10,0	10,5	9,6	6,6	3,6	5,9	4,0	4,0		137,4
19	Przesędowo	4,6	3,9	7,0	0,5	1,6	7,2	6,2	.	5,0	5,7	7,4	6,6	.	.	.	5,8	2,4	1,4	6,8	7,0	9,3	10,5	7,3	6,8	6,1	8,7	1,3	4,0	4,7	2,3		140,1
20	Przybroda	-																															-
21	Poznań-Ławica	3,8	1,8	7,1	0,3	2,9	6,8	6,2	.	4,1	6,0	6,5	7,5	.	.	.	4,2	1,6	0,8	3,3	5,3	7,9	7,0	9,7	9,7	6,5	9,2	1,5	3,2	7,3	2,6		132,8
22	Plewiska	-																															-
23	Kórnik	4,4	3,4	8,2	0,4	2,7	4,4	4,5	0,2	5,0	5,7	5,2	7,1	.	.	.	4,4	1,6	1,1	3,2	4,2	9,1	10,8	10,9	10,7	8,5	8,4	1,4	2,7	5,2	1,4		134,8
24	Chorniki Śl.	6,6	1,1	7,9	2,7	4,3	6,2	2,0	0,8	1,1	5,9	1,2	7,9	.	.	.	4,2	1,9	0,1	5,9	9,3	8,9	11,0	11,4	9,2	11,7	2,9	.	.	3,3	.		127,5
25	Laskowice Oławskie	3,6	2,9	7,6	1,9	2,1	1,1	4,0	1,5	0,8	6,3	.	8,5	.	.	.	3,5	1,0	0,8	6,3	9,4	9,5	9,4	11,4	9,8	10,8	7,7	0,7	0,3	2,7	0,5		124,1
26	Olechocinek	2,5	3,0	5,4	0,5	.	5,5	5,1	.	6,7	10,2	6,0	7,2	.	.	.	8,4	5,7	0,5	3,2	2,8	9,8	10,3	10,4	9,3	10,6	5,2	0,7	4,0	4,9	3,5		141,4
27	Więckowice	2,5	3,5	4,9	0,2	0,5	4,0	3,4	.	7,4	7,7	6,3	6,7	.	.	.	7,6	6,2	0,5	2,9	7,3	10,3	11,2	11,1	10,7	10,5	8,3	2,8	4,0	4,4	3,7		148,6
28	Legionowo	0,2	3,5	1,9	6,9	0,4	5,5	0,4	.	2,1	8,6	0,4	7,1	0,1	.	0,3	10,0	9,2	2,3	2,4	6,6	9,4	8,9	8,3	9,7	12,7	10,7	1,1	2,6	4,4	1,0		136,7
29	Warszawa-Bielany	1,0	2,9	3,2	7,3	0,2	4,6	0,3	0,1	1,2	7,9	0,7	6,7	0,1	.	1,5	9,2	9,0	2,6	4,1	5,8	9,9	10,2	5,1	9,5	12,6	10,4	0,8	2,0	3,5	0,8		133,2
30	Warszawa, Min.Kom.	1,6	2,4	0,4	6,6	.	3,1	0,5	0,1	0,9	8,2	6,6	2,3	0,1	.	1,9	7,7	7,2	2,8	3,7	5,0	10,0	10,1	6,6	9,9	10,0	11,9	2,3	0,9	4,4	0,8		128,0
31	Międzylesie	0,1	2,7	2,4	7,5	1,0	3,9	0,6	.	2,4	8,7	2,9	6,6	0,1	.	3,1	10,1	9,4	4,3	4,6	7,1	10,5	9,6	8,4	11,6	13,0	10,7	1,3	5,8	3,6	1,5		153,5
32	Erwinów	2,3	3,3	2,0	6,4	.	4,9	1,7	.	0,6	9,5	0,8	5,3	0,1	.	0,4	8,3	8,6	0,7	1,8	5,1	9,6	10,1	5,3	11,2	12,8	10,2	0,3	2,2	3,8	0,5		127,8
33	Świder	1,5	2,2	2,5	6,8	1,1	3,3	1,0	.	2,9	8,0	3,2	8,4	0,2	.	2,9	7,8	9,0	3,1	4,2	6,7	9,5	10,4	8,9	10,7	12,2	10,0	0,7	2,5	4,1	0,1		143,9
34	Topola-Błonie	3,8	3,4	5,1	5,7	.	1,3	6,5	0,1	4,1	7,1	0,3	4,7	0,8	.	1,7	7,5	6,9	.	6,1	6,5	10,6	10,4	11,0	10,3	11,8	8,7	0,7	1,0	5,0	2,7		143,8
35	Młochów	2,4	2,8	4,0	6,8	0,1	4,0	1,8	0,1	0,5	8,4	2,5	6,4	0,7	0,7	.	8,9	9,1	1,9	3,1	7,1	10,5	10,9	8,2	12,1	13,2	10,7	0,4	2,2	4,3	0,2		144,0
36	Skierniewice	2,2	4,5	6,6	6,7	.	3,1	4,0	0,1	2,3	9,1	2,8	6,2	0,3	.	0,1	8,8	8,0	2,3	6,2	6,4	10,8	11,2	6,8	11,7	12,2	10,2	0,4	2,2	4,4	0,4		150,0
37	Bełsk	2,7	4,3	2,4	7,4	.	5,8	1,4	0,1	2,4	7,5	3,0	6,5	0,4	.	2,3	9,3	8,8	2,8	6,0	7,5	10,1	11,0	8,7	11,1	12,7	11,0	0,4	2,0	4,4	0,6		152,6
38	Łódź-Lublinek	3,1	2,5	7,3	7,3	.	0,8	5,3	0,1	2,9	7,3	0,6	6,6	2,4	.	.	6,4	7,1	2,2	5,8	6,5	10,8	11,3	11,7	10,8	11,7	9,5	0,6	2,1	3,8	0,6		147,1
39	Kalisz	4,0	3,1	6,8	2,1	0,8	0,2	5,7	0,1	4,3	7,1	1,6	4,3	0,1	.	.	4,6	4,7	0,2	6,7	4,5	9,8	10,1	11,2	9,6	11,2	7,9	1,1	1,7	3,7	0,8		128,0
40	Wieluń	4,9	3,2	7,5	6,6	0,3	.	4,2	1,2	2,0	5,1	0,1	4,3	0,5	.	.	6,0	2,9	1,7	8,0	6,1	11,0	10,0	11,9	10,1	11,6	9,7	0,5	2,1	4,3	0,3		136,1
41	Szepietowo	1,3	3,7	0,2	7,8	1,9	0,3	.	.	1,7	6,7	10,2	8,4	0,5	.	2,9	8,3	8,6	4,7	0,1	7,0	8,6	9,4	11,4	9,2	13,0	9,7	0,1	2,5	4,4	.		142,6
42	Białowieża	0,1	4,8	1,1	8,6	4,1	.	.	1,6	2,2	5,0	10,6	6,8	5,3	.	3,1	8,2	5,6	3,5	0,7	8,9	6,5	5,7	12,0	7,1	13,1	10,1	.	1,5	2,5	2,5		141,0
43	Terespol	0,4	3,7	5,2	8,7	1,7	3,3	.	1,4	4,1	5,6	11,5	9,7	4,1	0,1	6,2	8,5	6,5	3,4	2,6	8,6	8,0	5,4	11,4	9,4	12,3	11,3	.	1,8	3,4	3,1		161,4
44	Sobieszyn	1,7	4,1	5,9	8,8	1,1	1,8	0,2	.	3,9	7,8	7,1	10,0	4,2	0,1	5,0	9,5	10,6	1,4	3,3	5,3	10,3	10,0	11,9	11,4	13,6	13,0	0,2	2,6	1,6	0,3		166,7
45	Puławy	0,8	3,4	6,8	7,2	0,4	1,7	0,1	.	4,2	7,8	4,6	7,1	2,1	.	5,1	8,4	9,4	1,2	4,2	5,3	9,0	5,7	10,6	10,1	11,9	11,5	0,3	0,7	1,6	1,3		142,5
46	Chełm Lub.	0,3	7,9	11,5	9,2	0,5	6,1	.	0,3	4,6	5,3	6,2	10,1	4,7	1,0	7,3	10,2	9,7	1,0	4,4	8,6	9,2	7,0	11,7	12,1	12,6	12,7	.	2,6	3,5	5,3		185,4
47	Szczawno-Zdrój	6,5	2,8	6,8	1,7	5,1	1,6	4,0	0,4	3,7	3,1	0,3	7,2	.	0,2	.	1,0	.	1,8	1,5	6,0	5,3	9,7	8,2	8,9	10,8	5,8	0,2	0,4	3,4	0,1		106,5
48	Śnieżka	0,6	0,1	5,3	0,1	.	0,6	3,5	.	.	1,2	3,2	8,9	.	.	.	0,1	0,1	1,3	5,0	9,9	8,9	11,1	11,7	10,7	11,0	4,8	.	.	1,7	.		99,8
49	Opole	5,5	2,7	7,3	5,3	3,1	.	4,7	1,7	0,1	2,2	.	3,5	0,1	.	.	5,3	1,9	1,6	6,5	9,3	10,1	8,8	10,5	10,0	10,3	9,6	1,8	1,8	3,2	3,0		150,1
50	Kudowa-Zdrój	5,7	2,4	9,4	3,3	3,7	3,2	5,8	0,8	4,0	3,8	.	8,7	0,2	.	.	3,9	0,4	2,5	5,3	10,1	9,9	9,7	11,6	10,7	11,5	8,4	1,0	0,3	5,4	1,8		143,5
51	Polanica-Zdrój	7,0	5,8	9,2	2,9	2,4	3,8	7,2	2,1	2,9	2,9	.	7,0	.	0,1	.	1,9	0,8	2,2	3,6	10,6	9,9	9,7	11,7	11,3	11,4	8,2	1,2	1,4	3,5	.		140,7
52	Skroniów	2,8	1,9	6,0	6,1	0,1	.	2,6	0,6	1,5	1,5	.	5,6	0,4	.	1,4	9,3	7,5	2,4	9,1	8,0	10,6	11,8	12,4	12,4	9,1	12,2	.	3,9	6,9	4,4		150,5
53	Świerklaniec	4,7	1,5	6,1	4,6	.	.	5,3	1,1	1,8	1,0	.	4,4	.	.	0,1	6,3	6,0	4,7	5,3	9,6	9,5	9,6	10,4	11,5	11,0	8,0	0,8	2,6	4,7	3,9		134,5
54	Kraków, Obs.Astr.	4,0	8,1	8,1	6,9	0,1	.	2,6	2,7	3,0	0,4	.	4,2	0,7	.	0,1	9,9	7,2	1,7	8,7	8,1	11,1	11,0	11,4	11,5	11,1	10,0	0,4	2,6	5,2	2,1		152,9
55	Cieszyn	5,0	0,4	7,5	2,1	1,4	0,3	2,0	0,3	.	.	.	.	.	.	.	4,1	3,1	0,6	6,4	7,6	8,6	11,1	11,2	11,8	11,2	11,4	0,1	1,9	3,8	3,2		115,1
56	Istebna-Kubalonka	4,4	0,2	9,1	3,9	0,3	.	1,2	.	1,8	.	.	0,8	0,1	.	.	5,2	4,5	6,3	9,5	11,6	11,8	11,8	11,5	10,8	11,3	11,3	0,4	0,6	5,3	4,6		138,3
57	Babia	3,4	3,3	7,9	4,4	0,7	.	1,7	1,4	5,1	.	.	3,9	0,8	.	.	9,9	6,6	0,9	7,2	9,1	11,4	11,9	11,9	12,2	11,4	11,9	0,2	0,9	2,6	1,3		142,0
58	Jabłonka	4,9	1,7	6,5	4,4	0,8	.	1,4	1,1	6,0	.	.	3,2	4,0	0,4	.	4,6	6,4	1,1	4,0	10,5	10,9	10,3	11,1	11,3	9,8	11,0	0,3	3,6	3,7	1,0		134,0
59	Krynica	2,6	0,8	9,6	0,5	.	.	0,9	0,8	7,0	0,4	0,9	6,2	2,1	.	0,7	9,7	7,8	1,5	8,5	10,2	10,6	10,7	10,9	10,6	9,1	11,0	0,1	1,7	4,7	3,5		143,1
60	Krynica-Góra Park	.	1,7	9,9	4,0	.	.	1,0	1,5	6,4	1,7	.	6,1	3,4	.	.	10,5	7,8	1,5	7,4	9,0	9,7	11,0	11,4	10,5	11,0	11,9	.	1,9	5,5	5,5		149,9
61	Muszyna	2,5	0,3	8,8	5,2	0,4	.	1,0	0,2	7,4	0,4	2,6	4,4	2,2	.	1,0	8,7	7,7	1,2	7,5	8,6	4,5	11,1	10,3	8,7	9,0	11,4	0,2	1,6	4,9	4,2		136,0
62	Zakopane	3,7	1,7	9,5	6,1	0,7	.	0,7	2,7	7,1	.	.	1,5	5,2	.	2,3	4,7	6,2	.	6,9	8,6	12,4	12,1	12,0	10,4	11,8	12,5	.	0,6	1,9	0,8		142,1
63	Gubałówka	3,2	1,8	9,2	4,6	0,6	.	0,4	2,8	6,6	.	.	1,2	5,3	.	2,1	7,0	6,4	0,1	6,5	7,5	10,6	10,7	11,0	8,3	10,4	10,7	0,1	0,4	1,2	1,5		130,2
64	Hala Gąsienicowa	1,9	0,8	9,5	4,7	.	.	.	1,7	6,9	.	0,4	6,1	4,4	.	2,5	4,2	6,4	.	7,3	8,1	10,3	11,1	10,8	9,1	10,2	11,0	0,2	.	.	1,6		129,4
65	Kasprowy Wierch	2,5	1,6	10,0	5,4	.	.	.	1,3	7,0	.	0,9	7,0	3,6	2,3	1,9	4,9	7,2	0,1	8,1	9,0	12,2	12,8	12,6	11,2	12,8	13,0	0,3	0,3	0,2	1,8		150,0
66	Werbkowice	0,2	8,0	10,4	9,8	0,9	5,2	.	0,1	7,8	6,9	10,6	2,4	0,3	.	8,1	9,7	8,5	0,5	6,1	10,4	10,6	10,8	12,3	12,0	12,6	12,3	.	2,4	1,9	7,0		187,8
67	Zdanów	1,6	4,3	9,0	7,4	.	1,1	1,5	0,1	3,6	4,9	3,8	9,2	4,3	.	4,4	8,8	9,8	0,2	5,2	8,7	11,3	12,0	12,1	12,2	12,8	13,2	0,6	1,5	2,9	5,3		171,5
68	Iwonicz-Zdrój	0,4	5,0	10,5	6,9	.	0,6	0,2	2,3	7,2	3,7	0,2	5,1	4,1	.	1,5	10,2	10,1	1,3	9,4	8,5	10,4	11,1	10,9	11,6	11,1	12,0	0,9	0,5	3,2	3,0		161,9
69	Łeba	0,4	2,0	10,1	1,5	0,3	2,5	.	0,7	8,2	5,7	3,6	4,3	8,1	.	2,9	10,7	9,2	0,3	8,1	9,0	9,6	11,1	12,1	9,7	10,8	12,6	2,5	0,5	4,3	3,7		164,2

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	2,3	2,4	1,8	0,1	11,9	12,1	1,4	.	0,4	3,5	2,9	2,9	.	.	0,5	5,2	7,3	11,3	10,3	.	12,7	3,3	.	5,8	0,8	0,9	.	5,3	6,6	8,7	5,7	126,3
2	Kołobrzeg	1,9	6,7	0,5	10,9	10,2	9,8	0,7	1,0	2,6	4,6	3,5	1,3	.	.	0,4	5,8	5,7	9,9	8,9	0,3	13,7	0,1	0,1	8,4	7,7	1,3	0,8	3,7	2,2	2,5	6,3	131,5
3	Międzyzdroje	1,1	9,6	0,5	7,3	11,3	10,5	0,7	0,3	4,5	1,9	2,8	1,0	.	.	0,3	2,1	3,8	5,6	4,1	2,3	10,8	0,8	.	8,7	8,9	0,5	.	0,5	2,8	1,0	6,4	110,3
4	Resko	1,1	6,6	.	8,6	7,0	9,3	1,0	2,5	3,7	5,1	5,4	1,0	0,1	.	1,6	2,3	5,2	5,9	9,6	1,1	11,5	0,9	.	10,1	5,4	0,2	.	4,7	2,9	3,4	8,2	124,4
5	Szczecinek	0,4	1,6	2,3	3,1	8,2	11,1	1,9	2,2	3,7	5,8	5,8	5,3	0,3	.	0,8	1,0	1,8	5,4	10,3	.	11,2	2,2	0,6	12,1	1,6	.	.	4,0	1,4	4,8	4,9	113,8
6	Chojnice	0,6	0,4	2,4	5,6	5,8	11,4	.	2,1	3,3	3,1	4,7	6,7	0,7	.	.	2,4	0,6	5,8	9,4	.	8,2	3,4	0,4	9,4	5,8	.	0,8	4,6	0,9	6,0	3,4	107,9
7	Hel	6,5	.	4,0	6,7	5,2	11,6	0,6	4,9	2,1	0,3	5,6	.	1,4	.	.	4,5	2,3	6,4	10,6	.	11,7	2,5	0,3	10,7	9,0	0,1	2,6	10,9	1,1	7,5	4,1	133,2
8	Gdynia	4,3	0,5	2,9	6,1	5,4	11,7	.	1,8	2,2	0,5	4,2	0,2	1,3	.	.	3,9	1,2	4,3	9,2	.	9,2	1,8	0,2	11,1	7,7	1,1	1,7	10,0	0,5	8,4	4,5	115,9
9	Świbno	.	.	4,0	5,9	5,5	.	.	2,6	2,2	.	5,1	.	1,7	.	.	1,4	1,2	4,9	9,0	.	9,3	2,1	0,5	9,2	6,7	.	1,3	9,3	2,4	7,1	4,2	95,6
10	Stare Pole	1,5	0,8	5,4	6,9	4,0	13,0	0,1	2,9	3,8	0,2	5,1	3,6	1,5	.	.	1,5	1,4	6,4	10,6	.	9,7	1,7	2,4	6,8	3,9	.	0,7	10,8	3,3	7,6	5,1	120,5
11	Radostowo	0,8	3,2	7,0	6,3	3,8	11,7	.	3,7	1,6	0,8	5,6	2,1	0,5	0,1	.	4,3	3,1	5,6	9,7	.	6,3	2,9	1,5	7,9	4,4	.	1,9	10,1	2,8	9,2	5,7	122,6
12	Preburty	0,4	2,5	4,1	4,8	2,2	12,9	.	2,0	1,7	1,4	4,2	7,2	1,6	.	.	0,2	1,2	3,9	10,8	.	6,8	1,0	1,6	6,2	2,2	.	0,6	10,5	2,6	6,8	3,9	103,3
13	Bydgoszcz, IMGW	0,3	2,7	2,7	4,3	3,3	9,3	2,2	3,1	4,6	4,0	7,4	8,6	2,8	.	.	0,7	2,3	4,6	9,5	.	3,6	3,9	2,3	4,6	2,4	.	0,4	8,1	2,5	5,5	2,7	108,4
14	Suwałki	0,7	0,7	4,8	6,6	2,3	5,1	7,6	3,8	2,5	5,9	3,0	10,8	6,8	.	0,3	.	6,9	3,2	13,4	1,1	5,3	.	4,8	1,7	.	.	4,1	1,1	7,0	2,6	3,3	115,2
15	Mikołajki	0,4	2,4	4,6	3,7	1,7	8,9	1,5	2,9	1,1	4,8	6,1	8,0	6,0	.	0,6	.	5,4	7,0	11,0	0,1	9,2	0,8	5,1	4,7	1,0	.	1,3	4,2	6,9	2,3	2,7	114,4
16	Ełcbrza	2,4	2,8	3,9	2,2	1,1	5,7	3,7	1,8	4,1	4,3	3,8	5,5	6,5	.	0,6	.	5,0	4,9	11,7	0,7	3,7	1,6	7,2	0,7	.	.	3,4	2,8	7,6	2,0	4,9	104,6
17	Białystok	.	6,5	4,3	2,5	6,8	5,3	2,8	1,3	5,5	0,9	3,1	6,9	7,4	0,3	.	.	7,5	5,6	12,7	0,7	1,1	2,5	10,1	0,4	.	.	5,6	1,5	6,5	1,6	6,9	116,3
18	Gorzów Wlkp.	1,5	6,8	1,2	3,4	4,9	10,4	2,7	4,4	1,2	7,6	6,2	4,3	4,1	.	.	2,8	2,2	7,5	9,0	1,7	10,7	1,3	2,0	8,3	2,8	.	0,6	7,0	1,8	5,6	2,3	124,5
19	Przesędzomo	.	3,0	1,4	5,4	3,6	11,3	3,3	5,4	3,7	5,8	8,9	9,2	3,0	.	.	1,1	1,6	5,8	10,3	.	4,6	1,0	4,1	1,1	2,6	.	.	7,6	3,0	6,8	2,5	116,1
20	Przybroda	0,2	3,5	0,3	4,9	4,1	11,9	3,1	5,6	4,3	7,2	5,7	8,8	2,6	.	.	1,4	1,7	6,6	10,5	0,7	7,5	1,0	4,0	2,1	2,5	.	.	8,8	3,2	6,3	2,4	120,9
21	Poznań-Ławica	.	4,7	0,5	3,6	3,4	10,2	3,7	4,8	3,0	5,3	6,3	8,4	2,6	.	.	1,0	1,2	5,5	10,3	0,2	5,1	0,8	4,3	0,6	2,7	.	.	6,6	2,5	7,0	1,6	105,9
22	Pleszew	-																															-
23	Kórnik	.	1,4	1,5	3,0	4,1	10,8	2,9	5,3	5,0	5,9	7,0	7,2	3,7	.	.	0,9	1,0	8,0	10,7	0,1	3,4	1,0	5,1	1,2	0,7	.	.	6,8	7,8	9,5	0,6	114,6
24	Oborniki Śl.	2,7	5,0	1,7	2,2	1,5	7,3	2,1	7,3	6,1	9,9	9,0	7,3	1,1	.	.	6,1	.	1,5	2,9	.	1,1	1,3	7,3	.	0,4	.	1,6	4,8	9,4	6,9	6,5	113,0
25	Lankowice Oławskie	2,6	3,6	2,0	2,2	1,7	7,9	1,8	5,3	7,2	5,0	7,0	9,2	1,0	.		1,2	0,8	6,4	8,5	.	1,2	1,5	7,3	.	0,3	0,1	3,0	2,7	7,5	7,4	8,2	112,6
26	Ciechocinek	0,3	0,9	5,3	4,4	3,4	12,0	1,2	5,5	3,7	2,2	6,2	7,7	2,3	.	.	2,6	1,0	7,8	10,2	.	4,5	5,0	5,2	4,8	.	3,3	0,8	8,0	5,3	5,7	1,8	121,3
27	Więcławice	0,1	2,4	4,5	3,6	4,8	11,6	1,9	3,2	4,4	3,8	8,2	9,4	2,3	.	.	1,1	1,6	6,5	9,3	.	1,7	3,9	4,2	5,1	1,9	.	0,7	9,8	5,4	5,0	1,6	118,0
28	Legionowo	1,3	2,0	8,0	2,0	1,4	10,9	.	4,9	3,7	0,3	5,9	10,6	2,6	.	.	.	2,6	6,0	11,6	.	4,6	2,0	7,6	0,4	0,3	.	0,5	3,3	9,5	2,7	4,1	108,8
29	Warszawa-Bielany	1,5	2,4	10,0	2,5	1,4	11,7	.	3,4	4,5	.	4,8	12,9	4,2	.	.	0,3	3,7	5,4	12,4	.	5,7	2,9	7,6	0,4	0,2	.	0,5	4,2	8,4	3,0	4,2	118,2
30	Warszawa, Min.Kom.	1,1	2,7	8,5	2,5	1,4	11,9	0,2	5,4	4,2	0,2	6,7	10,7	5,4	.	.	0,6	3,0	7,8	10,7	.	4,6	2,7	7,0	.	0,2	0,8	3,6	5,2	3,4	3,0	4,4	117,9
31	Międzylesie	.	1,8	7,9	2,4	1,2	9,9	.	4,4	4,4	.	6,8	11,0	4,2	0,1	.	0,1	4,0	6,6	12,1	.	3,8	2,8	8,4	0,1	0,4	.	1,0	4,0	4,7	3,6	5,7	111,4
32	Brwinów	0,3	1,1	7,1	1,8	0,9	9,0	.	3,4	2,9	0,4	3,2	11,8	4,7	.	.	0,1	3,8	6,1	13,1	.	0,9	2,0	5,9	0,2	0,2	.	.	2,6	4,5	3,6	2,9	92,5
33	Świder	1,1	0,6	8,5	2,2	3,7	9,9	0,1	4,8	3,0	0,2	8,9	11,4	4,7	0,1	.	.	3,4	8,5	11,3	0,1	3,2	2,4	8,0	0,2	0,3	.	1,0	4,3	4,2	3,2	5,5	112,8
34	Topola-Młonie	0,7	0,4	2,9	4,3	2,8	10,8	1,1	6,0	4,9	1,6	6,2	10,4	2,3	.	.	0,3	2,2	8,1	10,8	.	2,1	2,7	8,4	0,3	2,5	.	0,5	2,9	11,9	4,3	4,5	115,9
35	Młochów	0,5	1,9	7,0	2,7	0,4	10,5	.	4,0	4,6	0,3	4,5	10,3	4,7	.	.	0,3	3,8	5,4	12,7	.	1,0	1,2	7,2	.	0,3	.	0,1	3,0	5,2	4,2	3,9	99,7
36	Skierniewice	1,5	1,3	8,0	3,2	1,5	12,5	0,5	4,7	5,8	1,1	6,4	9,7	4,0	.	.	2,0	2,3	6,7	11,8	.	0,2	2,3	9,2	.	0,5	0,1	0,6	1,5	9,8	2,7	6,3	116,2
37	Bałak	0,8	4,9	8,9	3,4	2,8	11,2	0,1	4,6	6,1	.	10,2	10,1	6,1	.	.	4,0	4,9	6,9	.	0,2	0,9	2,1	9,1	0,3	0,5	0,2	0,2	4,3	5,4	4,4	5,2	117,8
38	Łódź-Lublinek	1,1	2,8	4,1	3,4	3,3	11,9	1,2	6,7	6,1	2,0	6,5	8,4	1,0	.	.	0,4	1,2	5,0	10,7	.	0,3	2,2	9,0	.	0,9	.	0,4	1,6	5,8	4,4	6,8	107,2
39	Kalisz	0,3	3,0	4,4	4,9	2,0	10,4	1,0	6,5	5,8	4,5	4,6	9,3	1,0	.	.	2,5	1,2	4,1	10,0	.	2,7	1,5	7,5	.	0,5	.	0,3	2,3	7,7	4,3	3,6	106,1
40	Wieluń	0,2	3,3	5,3	5,0	3,2	9,0	2,6	8,3	7,0	4,7	5,9	10,5	2,5	.	.	2,1	2,0	4,8	9,8	.	.	7,1	9,5	.	0,1	.	0,5	1,7	10,4	5,0	8,5	129,2
41	Szepietowo	.	3,6	5,9	8,3	7,6	9,2	5,7	2,5	4,2	1,9	4,3	10,9	8,3	.	.	.	5,2	.	7,6	0,1	3,4	2,2	8,4	0,2	.	.	4,2	2,8	7,0	1,7	5,0	120,2
42	Białowieża	0,2	2,5	5,4	2,4	7,4	4,9	4,6	0,8	4,5	0,7	5,3	4,3	9,3	.	.	.	7,4	5,5	13,5	3,2	.	1,0	8,0	0,1	0,2	1,1	8,0	7,3	5,1	0,6	2,6	115,9
43	Terespol	1,6	4,6	5,1	1,7	7,4	8,7	5,1	1,6	4,2	.	6,3	7,8	7,4	0,5	.	.	8,4	5,3	11,8	2,3	.	1,9	10,3	0,6	0,3	1,3	8,6	4,9	7,0	0,6	3,4	128,7
44	Sobieszyn	1,0	5,1	5,7	2,1	4,4	10,5	4,0	1,7	5,5	.	3,7	10,6	5,3	1,0	.	0,1	3,4	2,5	13,5	0,5	0,4	2,4	9,4	0,3	.	0,8	2,1	4,3	4,6	2,2	5,0	112,1
45	Puławy	0,4	3,4	5,5	2,4	3,1	7,4	2,2	1,1	4,9	.	3,1	8,5	5,3	1,3	.	1,2	4,7	1,5	12,1	0,6	0,1	1,8	8,7	.	.	0,3	1,6	4,6	4,3	1,6	6,3	98,0
46	Chełm Lub.	3,2	5,4	4,3	2,4	4,9	6,6	3,9	0,9	4,2	.	2,3	7,4	4,6	1,7	.	.	4,2	1,1	12,9	0,7	.	5,1	10,3	1,9	0,1	3,7	7,3	4,4	4,3	0,8	11,1	119,7
47	Szczawno-Zdrój	2,6	1,6	2,7	1,1	0,6	9,2	1,8	2,1	5,2	4,1	5,0	3,4	0,7	.	.	1,2	1,5	4,5	8,8	.	3,2	1,6	8,0	.	0,2	.	0,6	4,3	8,5	4,5	7,4	94,4
48	Śnieżka	0,7	1,6	2,5	1,8	0,9	10,9	1,2	3,1	5,0	4,5	5,8	3,3	.	.	.	3,3	.	4,6	8,5	.	0,6	0,7	0,5	0,1	0,1	.	1,9	2,1	5,8	5,2	8,7	83,4
49	Opole	3,2	4,4	3,9	3,6	4,4	9,1	1,8	4,9	7,4	5,6	9,0	6,9	4,6	.	.	4,5	1,2	2,9	9,7	.	1,0	1,5	9,8	.	.	0,2	1,2	3,1	8,5	6,1	9,4	129,9
50	Kudowa-Zdrój	3,3	2,6	2,5	4,3	4,3	9,5	0,3	2,8	5,1	4,9	9,3	6,6	0,2	.	.	3,4	0,4	7,0	8,9	.	1,5	2,0	6,2	.	2,0	.	3,8	5,7	11,0	5,7	11,7	125,0
51	Polanica-Zdrój	3,3	2,6	4,6	2,3	1,6	8,3	1,2	2,8	5,7	5,3	11,3	4,2	0,1	.	0,4	6,3	1,5	7,7	10,4	.	1,2	2,6	7,5	.	0,3	.	2,5	5,7	9,9	8,6	12,3	130,6
52	Skrzeniów	2,7	4,8	6,5	3,8	3,9	6,5	0,6	5,8	6,6	1,8	3,7	9,9	6,9	0,9	.	2,0	3,8	3,6	8,8	0,3	.	6,7	9,4	.	.	.	.	3,1	3,4	3,8	10,7	120,0
53	Świerklaniec	4,2	3,6	5,5	8,0	5,8	5,3	1,7	4,6	6,3	4,5	5,2	3,0	2,2	.	.	3,2	1,7	4,3	9,2	.	.	5,8	8,0	.	.	.	0,2	2,8	5,8	4,6	11,6	117,1
54	Kraków, Obs.Astr.	4,1	3,8	5,1	2,2	2,0	7,3	0,1	4,3	7,8	2,0	1,7	6,3	5,0	1,4	.	3,5	5,2	3,8	9,3	0,4	.	6,7	11,4	.	.	.	0,3	4,7	3,6	3,1	11,3	116,4
55	Cieszyn	3,2	1,3	2,7	0,5	4,8	1,8	0,1	2,6	3,9	0,1	3,2	4,2	3,1	.	.	0,6	0,8	4,2	9,3	.	.	5,8	11,8	.	.	.	0,6	4,9	3,7	4,9	11,9	90,0
56	Istebna-Kubalonka	2,7	.	1,0	1,9	2,8	4,9	0,2	2,7	5,6	1,4	7,5	11,6	4,7	0,5	.	2,8	1,4	5,4	11,3	.	.	4,6	10,1	.	.	1,8	0,1	6,8	3,2	4,2	13,7	112,9
57	Rabka	1,9	2,3	4,8	1,5	2,4	8,3	0,4	6,2	8,5	1,4	0,7	6,9	4,9	4,2	.	1,4	0,7	4,0	10,7	0,3	.	7,1	12,7	.	.	2,1	0,2	4,9	4,1	2,8	13,0	118,4
58	Jabłonka	3,9	1,8	6,5	2,6	2,0	6,3	2,3	4,3	9,3	0,5	0,2	2,6	1,3	2,8	0,1	2,1	1,3	5,6	11,0	0,3	.	7,7	11,0	.	.	1,9	0,2	5,5	3,8	3,6	10,9	111,4
59	Krynica	3,1	3,1	5,6	5,0	2,4	4,9	0,8	3,3	9,4	2,0	0,4	3,5	4,7	5,1	5,6	1,1	4,9	4,6	10,8	0,3	.	6,3	10,1	2,0	.	2,9	2,0	8,3	2,6	2,3	11,4	130,5
60	Krynica-Góra Park.	0,1	5,1	7,8	3,8	3,5	5,0	2,0	4,2	9,4	.	0,2	5,1	4,0	5,5	5,6	.	3,8	5,3	11,3	0,3	.	5,2	11,4	2,1	.	2,3	2,4	6,6	2,4	2,4	11,9	128,9
61	Muszyna	5,1	5,1	7,9	4,2	3,4	5,3	1,0	6,3	9,4	2,2	0,1	4,5	5,0	5,5	2,6	2,5	3,0	4,0	9,2	1,0	.	6,3	11,0	1,4	.	3,9	4,2	8,3	2,9	2,3	10,6	138,2
62	Zakopane	2,6	3,6	8,7	3,4	2,4	5,3	.	6,0	8,5	0,2	0,2	5,0	4,1	3,8	0,3	1,5	1,2	4,6	12,0	0,4	.	7,1	12,4	0,1	.	1,6	0,1	4,7	1,0	1,9	13,5	116,2
63	Gubałówka	1,6	3,5	6,4	2,7	2,2	4,2	.	4,7	8,4	.	0,1	4,3	3,5	4,2	.	0,4	1,0	3,7	10,2	0,7	.	5,5	11,2	.	.	1,7	.	2,7	0,7	1,0	11,7	96,3
64	Hala Gąsienicowa	1,6	3,6	7,0	2,9	2,6	3,0	.	3,6	4,4	.	.	6,3	4,6	0,7	0,1	.	1,7	3,0	10,6	1,3	.	7,7	11,3	0,2	0,1	1,4	0,5	5,9	0,5	0,6	12,5	97,7
65	Kasprowy Wierch	2,7	2,6	7,6	2,1	2,3	5,9	.	5,2	6,9	.	0,3	6,6	4,7	0,3	0,1	.	1,5	3,1	8,5	0,8	.	6,7	12,9	0,9	0,4	0,2	0,1	4,3	0,4	1,5	12,3	100,9
66	Werbkowice	5,0	4,7	5,1	5,3	4,2	4,7	2,8	0,8	5,4	.	6,9	8,9	5,8	2,4	.	0,3	5,6	8,4	5,4	1,7	.	3,8	10,8	5,1	1,8	3,4	5,1	3,3	3,3	0,2	13,7	135,9
67	Zamość	4,2	4,1	6,8	3,7	3,5	7,4	2,7	5,8	6,7	0,1	1,2	7,2	5,0	2,1	.	1,1	3,1	1,7	11,8	0,9	.	2,3	10,3	0,4	.	0,2	1,6	3,7	2,3	1,9	11,1	115,1
68	Zwanice - Zdrój	6,3	6,2	4,5	2,3	4,0	3,6	4,0	5,0	8,2	.	.	6,7	6,1	5,6	0,4	1,9	7,6	1,3	9,1	0,3	.	8,2	7,3	2,7	.	1,9	0,9	5,1	1,8	0,3	12,5	124,0
69	Łeba	7,8	6,0	4,2	.	4,6	1,2	3,5	3,3	8,5	.	.	5,4	5,1	5,3	0,7	0,2	6,9	1,3	10,7	2,7	.	6,6	6,9	6,2	.	5,4	6,8	8,3	3,1	0,9	7,3	128,9

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	11,4	10,5	6,0	11,9	14,5	15,6	15,5	15,4	6,9	12,3	2,2	13,0	13,2	7,3	8,0	6,0	8,2	14,4	12,3	13,2	3,4	3,6	6,6	8,1	6,2	4,2	.	0,2	0,2	8,0		258,3
2	Kołobrzeg	10,8	10,5	7,0	14,2	13,6	15,1	15,0	13,9	4,6	13,0	3,1	9,0	12,8	10,3	9,1	3,5	8,2	13,7	10,6	11,9	6,6	8,2	3,3	6,4	6,0	4,0	.	2,3	0,6	9,2		256,5
3	Międzyzdroje	5,1	9,7	9,4	14,8	12,1	15,2	15,1	14,9	8,2	9,9	2,0	5,8	11,5	8,9	5,9	2,7	5,4	12,8	7,5	8,4	3,9	4,3	0,8	4,4	3,4	3,6	0,8	.	2,6	1,9		211,0
4	Resko	6,8	11,0	7,6	12,0	11,7	14,0	13,7	14,0	7,4	12,2	1,1	4,7	11,8	8,4	8,0	2,4	6,3	14,3	9,1	13,1	6,1	7,6	1,1	8,8	7,0	7,7	1,0	1,5	1,0	2,7		234,1
5	Szczecinek	7,7	5,5	5,4	6,7	14,4	15,3	11,9	14,4	4,5	8,9	1,0	2,3	13,4	6,4	7,7	5,4	5,0	15,3	9,1	11,5	4,4	6,4	0,3	10,3	6,4	7,2	0,3	0,2	0,1	5,1		212,5
6	Chojnice	6,7	3,1	6,8	5,8	11,3	13,2	14,3	14,5	7,3	10,6	3,5	3,0	10,8	6,2	7,3	5,1	5,1	14,2	12,5	9,1	4,0	7,9	0,5	10,2	8,0	4,1	1,7	.	0,7	5,3		212,8
7	Hel	7,7	1,7	13,9	8,9	13,1	14,3	13,1	15,0	12,7	10,0	1,9	10,0	11,8	9,4	11,5	6,7	9,2	13,9	13,6	5,7	2,9	7,2	2,0	9,7	7,9	6,9	1,9	1,2	2,1	10,2		256,1
8	Gdynia	8,6	2,2	10,1	8,8	10,9	14,6	14,3	14,4	12,7	10,5	2,5	11,6	12,8	7,6	11,3	6,0	10,2	14,6	14,4	8,2	7,0	5,5	1,1	10,1	7,6	6,0	1,1	0,6	3,4	8,7		257,4
9	Świbno	7,2	1,7	11,2	7,4	8,8	12,1	12,7	11,7	12,4	6,0	1,3	5,9	8,3	6,1	6,4	5,5	5,2	11,7	8,3	7,6	2,1	2,6	0,6	7,0	4,8	2,0	2,0	1,2	0,6	12,1		192,5
10	Stare Pole	8,8	1,4	12,9	7,3	8,9	13,6	14,5	14,2	12,2	10,3	5,0	4,9	11,6	5,7	11,4	6,5	7,2	14,2	14,1	6,6	6,6	9,7	.	12,0	8,5	7,6	4,4	1,9	1,4	12,2		255,6
11	Radostowo	9,1	1,5	8,3	9,1	11,3	13,3	14,9	14,7	10,7	9,7	2,0	2,4	11,6	5,2	9,9	5,8	8,3	14,1	14,1	8,8	5,6	7,8	0,3	10,9	9,0	5,1	3,2	0,1	2,1	7,6		236,5
12	Prabuty	10,8	3,2	9,4	6,4	3,6	12,4	14,6	15,1	12,2	12,6	3,8	2,3	12,2	6,1	13,3	8,0	7,7	14,7	11,4	7,0	6,7	10,7	1,1	12,5	10,6	5,4	4,2	.	.	8,2		246,2
13	Bydgoszcz, IMiUZ	6,7	4,8	6,0	4,3	6,0	12,4	12,9	14,5	14,0	12,1	2,9	4,1	13,2	6,6	11,5	4,5	6,9	14,1	8,3	7,4	5,8	8,7	6,3	6,9	7,3	9,3	2,5	1,5	1,0	4,3		226,8
14	Suwałki	6,5	0,7	5,7	.	.	0,6	13,0	14,0	12,0	12,2	3,1	4,1	13,7	1,6	12,7	7,7	2,4	11,1	10,0	2,8	8,6	13,8	3,9	12,2	8,1	7,3	5,8	3,5	4,5	8,7		210,3
15	Mikołajki	7,4	1,1	1,8	1,0	0,2	6,8	11,5	14,6	11,6	11,4	3,1	3,7	13,3	5,5	12,3	3,6	2,4	12,6	8,9	2,2	7,5	12,3	4,5	9,8	7,3	8,0	3,8	0,8	4,2	6,5		199,7
16	Biebrza	5,4	.	3,3	.	.	0,2	10,4	12,3	9,3	10,3	1,2	5,8	11,2	5,7	11,8	5,3	3,6	11,9	9,4	2,7	7,9	13,1	7,2	9,4	7,0	8,3	4,3	2,5	2,2	6,9		188,6
17	Białystok	0,2	1,0	1,3	.	.	.	9,7	10,9	9,5	14,8	8,9	2,9	14,0	9,5	11,6	1,1	2,8	13,7	12,1	3,0	7,7	13,6	6,9	10,5	7,3	10,3	7,2	3,1	2,7	2,3		198,6
18	Gorzów Wlkp.	6,6	9,5	5,8	5,0	10,5	14,1	11,4	14,2	14,3	9,4	3,6	4,2	12,6	7,7	10,2	4,8	7,0	13,3	4,8	8,8	2,4	7,3	2,0	9,4	8,5	8,2	2,5	1,1	0,5	.		219,7
19	Przebędowo	6,8	4,2	8,3	6,3	8,7	13,4	12,3	14,0	14,0	11,0	2,8	4,2	13,4	8,6	12,4	5,0	11,5	13,7	8,8	10,4	3,7	9,9	7,8	9,0	10,2	10,1	4,0	1,2	.	0,4		246,1
20	Przybroda	6,5	8,4	8,7	5,4	7,6	13,9	12,8	14,6	14,5	10,4	2,4	2,8	14,3	8,9	12,3	5,8	12,3	14,2	7,3	10,4	4,6	11,0	9,4	8,9	10,6	8,4	5,2	1,8	1,2	1,6		256,2
21	Poznań-Zawica	6,9	8,3	10,0	3,8	7,1	11,9	7,6	12,0	12,1	9,6	3,2	2,8	10,9	8,4	11,1	5,2	11,6	12,2	5,2	10,0	2,1	9,0	10,9	7,6	9,7	7,7	5,0	0,7	0,4	0,3		223,3
22	Plewiska	6,8	7,8	8,6	2,8	7,6	13,5	8,2	12,9	12,9	8,0	2,1	0,9	8,6	6,2	11,4	4,9	11,6	14,6	6,2	8,6	4,0	9,8	11,6	7,4	10,8	8,6	5,5	1,5	0,7	0,3		224,4
23	Kórnik	6,3	7,8	10,9	4,4	10,4	15,0	7,8	14,9	15,2	11,3	3,5	3,1	13,8	9,3	13,2	8,4	10,7	14,2	5,7	10,6	2,8	9,3	11,6	8,5	12,4	10,2	6,5	1,9	0,6	1,3		261,6
24	Oborniki Śl.	.	4,6	.	3,2	7,2	14,3	2,4	14,3	10,1	10,0	3,3	13,8	12,1	10,0	7,9	2,2	4,0	8,0	1,8	4,8	2,6	13,0	2,2	13,8	.	4,3	.	.	0,2	0,5		170,6
25	Laskowice Oławskie	0,3	1,9	4,8	0,8	3,2	13,9	0,3	11,7	12,8	13,6	3,3	1,8	10,9	9,3	14,0	10,5	4,8	8,4	4,2	6,2	8,4	12,9	11,9	10,3	9,1	10,6	7,0	2,7	1,2	0,6		211,4
26	Ciechocinek	2,2	1,8	10,2	1,3	0,6	11,3	10,2	13,1	10,9	13,8	5,3	1,9	8,1	8,5	12,1	4,5	9,7	13,0	8,6	6,6	6,2	10,5	7,4	7,9	9,1	12,6	5,2	1,5	1,5	1,4		217,0
27	Więcławice	6,9	5,2	9,9	2,4	6,0	11,0	9,5	13,8	13,3	12,8	4,2	4,2	11,7	7,3	13,4	3,8	10,5	13,1	7,0	6,6	10,7	10,3	9,9	8,8	10,6	11,8	5,1	1,6	.	2,6		244,0
28	Legionowo	.	1,0	2,8	.	.	2,5	6,5	11,3	13,7	15,4	3,2	5,0	9,2	6,9	13,1	11,3	9,1	12,0	14,0	5,1	3,1	13,6	10,7	8,6	10,3	13,8	5,6	1,7	0,8	4,3		214,6
29	Warszawa-Bielany	.	1,8	2,1	.	.	2,0	4,7	12,4	13,7	14,5	3,2	2,9	8,5	7,4	12,4	11,2	7,8	11,5	14,5	4,6	5,4	13,0	11,8	5,0	8,0	14,4	6,7	2,4	0,9	4,3		207,1
30	Warszawa, Min.Kom.	.	1,8	2,1	.	.	2,6	5,4	12,6	13,7	14,0	3,2	5,4	8,7	6,8	12,1	9,7	7,2	10,7	13,4	5,2	6,4	12,9	10,3	7,6	9,0	9,4	6,7	2,4	0,9	4,3		204,5
31	Międzylesie	.	1,3	0,4	.	.	0,9	5,1	12,4	14,8	13,6	4,9	5,1	9,0	7,7	12,7	13,6	8,3	10,1	14,1	6,9	5,9	12,6	10,7	2,2	8,7	13,8	7,2	2,9	0,8	3,6		209,3
32	Erwinów	.	1,9	1,7	.	.	1,4	5,6	12,4	14,6	15,6	2,6	4,9	11,3	7,3	11,5	11,8	6,8	10,6	14,8	4,3	5,6	13,9	11,9	6,1	9,0	13,2	6,0	2,6	1,3	0,9		209,6
33	Świder	.	0,9	0,7	.	.	1,5	4,9	10,5	12,3	13,5	3,7	5,4	6,8	6,9	11,9	11,5	5,7	10,7	12,6	4,5	5,5	11,3	8,6	7,7	9,4	12,1	5,8	2,1	1,0	1,9		189,4
34	Topole-Błonie	0,4	0,7	7,4	0,2	.	10,3	6,8	10,6	14,4	14,3	3,7	2,7	11,9	10,8	13,5	12,3	8,6	11,0	11,6	7,3	2,7	11,0	11,0	7,9	10,7	12,8	5,2	1,2	1,1	0,1		222,2
35	Mrochów	.	1,9	0,9	.	.	2,2	4,8	13,4	14,7	15,7	1,3	4,2	11,5	7,4	13,3	13,6	6,5	11,4	15,2	4,8	4,7	12,2	11,4	6,3	9,4	13,2	6,1	2,3	1,6	1,2		211,2
36	Skierniewice	.	1,4	1,2	0,1	.	4,2	5,3	9,4	14,8	15,2	1,2	3,7	10,1	9,2	13,9	13,6	8,7	9,4	13,8	5,1	5,1	13,1	11,7	6,9	11,3	12,1	7,0	2,8	1,2	0,2		211,7
37	Belek	.	0,6	0,4	.	.	1,4	2,6	10,7	7,4	10,8	2,8	5,5	10,8	8,4	12,4	13,5	7,2	12,8	15,9	4,3	8,1	15,0	12,1	8,3	9,5	13,7	8,5	3,9	1,4	0,1		204,1
38	Łódź-Lublinek	.	0,4	6,3	0,2	0,1	8,0	3,2	8,5	13,2	13,8	2,4	2,2	9,2	10,1	13,6	12,1	8,6	10,3	12,6	6,4	5,2	11,9	11,0	6,9	8,8	11,2	7,9	2,8	0,3	.		207,2
39	Kalisz	1,8	4,6	7,0	3,8	2,2	11,7	3,9	13,0	11,4	12,5	2,1	0,7	11,0	9,5	12,8	10,7	9,2	11,1	5,2	8,8	5,4	12,7	11,7	7,6	10,7	9,7	7,0	3,5	0,3	.		221,6
40	Wieluń	.	0,1	5,8	0,1	.	7,9	0,8	9,5	13,6	11,8	2,0	1,4	11,0	10,9	13,8	10,8	6,6	10,2	12,8	5,9	9,8	13,5	13,5	8,5	8,8	10,7	7,4	4,8	0,4	.		212,4
41	Szepietowo	0,4	0,9	0,9	.	.	.	9,0	11,9	7,2	15,3	5,2	4,7	14,2	10,2	11,1	2,6	3,8	12,0	14,5	3,0	6,7	.	13,9	12,0	9,1	13,3	7,8	2,2	10,3	5,0		207,2
42	Białowieża	0,5	.	0,5	.	.	.	6,4	6,1	6,1	14,8	6,6	5,8	11,7	6,4	9,3	2,3	2,8	11,0	12,0	5,4	8,2	11,5	8,7	10,6	10,6	12,5	6,5	3,6	0,6	2,2		182,5
43	Terespol	.	.	0,4	.	.	.	3,2	7,7	11,6	14,3	8,8	7,0	12,1	6,0	9,5	11,7	2,1	10,6	13,5	7,7	6,3	12,5	12,7	7,6	10,0	13,7	6,1	2,5	2,3	3,1		203,0
44	Sobieszyn	0,1	0,5	0,6	.	.	.	0,9	9,3	14,9	15,3	8,0	5,6	7,6	7,0	9,8	14,6	5,7	14,4	14,9	6,2	6,0	13,1	12,2	9,1	7,4	13,7	8,6	5,2	1,3	0,3		212,3
45	Puławy	.	0,4	0,6	.	.	.	0,1	6,4	12,9	13,7	7,0	3,2	5,4	7,6	10,4	12,7	6,4	10,4	13,3	4,7	7,4	11,5	11,0	8,7	7,1	13,1	5,6	5,8	2,0	0,1		187,5
46	Chełm Lub.	.	.	0,5	.	3,8	.	.	7,9	13,7	15,3	11,5	2,3	7,5	8,1	7,3	12,5	2,6	8,9	10,9	7,3	1,5	14,0	13,8	8,3	8,3	8,9	4,5	1,1	4,0	1,6		196,1
47	Szczawno-Zdrój	0,4	2,6	2,2	1,8	2,9	12,5	0,6	14,0	12,2	9,5	1,7	0,8	9,1	5,4	9,9	7,9	2,2	6,6	0,7	3,5	3,7	7,9	11,8	11,4	11,3	8,4	5,8	1,7	2,1	1,8		172,4
48	Śnieżka	0,1	3,1	1,7	1,4	2,8	5,3	1,2	15,3	14,0	9,6	2,3	1,9	10,0	11,1	5,8	6,8	0,3	3,1	1,8	3,8	5,4	8,6	12,9	12,4	11,5	9,5	4,7	.	0,2	.		166,6
49	Opole	.	1,3	9,3	0,4	4,0	11,7	0,1	8,1	11,1	9,7	3,2	5,8	12,7	9,2	12,2	10,5	3,4	7,5	10,5	4,6	8,2	11,8	13,0	10,3	10,0	11,7	8,0	3,1	.	0,8		212,2
50	Kudowa-Zdrój	.	1,1	2,7	2,8	3,7	14,2	3,3	13,1	12,1	7,9	3,9	1,2	10,8	10,5	11,6	8,4	1,7	9,6	4,6	5,3	7,5	10,6	12,8	12,0	10,6	12,4	.	0,9	0,3	3,2		198,8
51	Polanica-Zdrój	0,1	2,1	3,2	3,4	5,8	13,6	0,3	13,2	10,8	7,9	2,3	1,2	10,5	10,6	12,2	8,4	1,3	8,1	4,3	5,6	9,7	7,4	12,5	11,5	9,1	11,0	.	7,5	2,5	2,9		198,7
52	Skroniów	.	0,6	.	.	.	3,3	.	5,8	13,4	13,3	4,0	6,6	6,8	6,2	12,5	12,6	1,3	11,1	13,6	4,1	3,1	12,3	10,3	6,9	10,7	7,7	5,4	4,8	1,6	2,3		180,3
53	Świerklaniec	.	.	2,1	.	0,3	5,4	.	7,5	13,0	13,7	2,9	3,3	5,9	8,7	12,9	9,4	2,3	7,6	11,8	0,8	5,7	13,3	12,2	11,6	9,5	11,5	6,4	4,8	0,5	0,1		183,2
54	Kraków, Obs.Astr.	.	0,8	.	.	.	2,5	.	5,8	12,7	11,7	4,5	3,7	5,1	7,9	10,4	11,5	2,2	11,4	13,4	2,8	3,9	10,7	12,0	12,0	9,3	6,5	5,7	5,2	4,5	1,0		177,2
55	Cieszyn	.	1,0	.	0,1	0,2	4,6	0,2	6,1	13,7	6,7	2,4	0,3	8,6	8,1	12,2	10,9	1,0	11,7	10,9	1,6	3,1	11,6	13,7	10,5	7,9	5,9	7,7	3,4	1,9	0,1		166,1
56	Istebna-Kubalonka	.	.	0,3	0,1	0,5	1,8	0,2	4,1	9,9	3,2	1,4	4,3	.	9,3	12,6	12,3	2,9	7,3	12,6	2,6	3,2	10,4	10,4	12,1	7,9	6,6	8,1	2,4	0,9	0,1		149,7
57	Rabka	.	0,2	.	.	.	1,8	.	5,7	11,8	6,4	3,8	1,1	4,6	6,7	10,7	11,0	0,5	8,6	12,8	3,1	1,4	12,2	12,6	9,9	8,7	8,4	3,4	3,6	2,6	.		151,6
58	Jabłonka	.	.	.	0,2	.	2,7	.	3,0	9,8	4,1	3,5	0,6	4,8	6,0	9,2	9,8	0,9	6,8	9,5	2,0	0,6	9,5	9,8	9,1	6,4	6,0	2,9	2,6	4,9	.		124,7
59	Krynica	.	.	0,1	.	.	.	.	2,4	8,7	3,5	1,3	1,5	1,8	3,9	7,5	6,4	0,4	3,8	11,0	4,1	0,7	10,3	7,4	5,5	7,0	2,0	0,7	1,3	3,4	2,1		96,8
60	Krynica-Góra Park	0,1	.	.	.	.	.	.	2,1	8,7	2,7	2,9	1,6	2,1	7,0	6,2	7,8	1,1	4,8	11,8	3,8	1,8	10,6	8,3	0,4	8,8	2,2	0,9	0,6	3,5	3,4		103,2
61	Muszyna	.	.	.	.	.	.	.	4,3	9,4	4,4	2,5	1,9	2,1	5,6	8,4	5,6	.	3,4	10,5	4,5	4,3	8,5	10,9	6,6	7,0	2,7	1,5	1,6	4,9	3,6		114,2
62	Zakopane	.	.	.	.	.	0,4	.	0,8	6,4	3,4	1,3	0,2	1,3	6,8	10,7	7,1	0,3	6,6	13,6	3,3	0,5	9,9	12,5	11,8	6,8	3,4	3,4	2,3	5,2	.		118,0
63	Gubałówka	.	.	.	.	.	0,3	.	0,8	6,8	3,2	1,1	0,1	1,0	5,8	9,1	6,1	0,6	5,1	8,8	2,7	0,3	6,6	10,2	9,9	5,7	2,3	3,0	1,8	4,3	0,2		95,8
64	Hala Gąsienicowa	.	.	.	.	.	.	.	0,8	5,6	2,7	2,6	.	0,9	8,7	8,6	9,4	0,6	1,0	10,2	4,4	1,5	4,7	7,6	10,5	7,0	2,3	3,6	0,9	2,7	.		96,5
65	Kasprowy Wierch	.	0,4	.	.	.	.	.	0,2	6,8	2,9	3,3	.	1,7	8,5	10,5	9,7	0,5	2,7	11,6	4,5	0,9	3,4	9,6	9,6	6,3	3,8	3,7	1,1	3,3	.		105,0
66	Warkowiec	.	.	1,4	.	1,0	.	.	6,6	13,9	14,0	9,7	1,4	6,4	5,0	6,8	12,8	3,2	7,4	11,3	9,8	4,1	12,7	12,8	10,2	9,1	8,5	3,8	1,7	5,4	1,3		180,3
67	Zdanów	.	0,5	2,0	.	.	.	.	9,7	14,3	14,9	8,4	2,9	6,4	10,5	11,7	13,3	5,0	14,2	13,9	7,6	1,5	13,8	12,4	7,5	11,0	10,6	8,3	4,8	8,2	0,3		215,9
68	Iwonicz - Zdrój	.	0,1	.	.	.	.	.	3,7	9,0	4,8	5,9	0,2	2,5	8,6	8,2	11,3	1,2	3,8	11,2	8,1	4,3	10,7	11,3	9,7	8,2	3,4	2,7	2,3	6,2	3,9		141,3
69	Leska	.	.	.	.	.	.	.	2,9	10,3	7,4	8,5	0,1	2,7	6,1	9,0	12,1	6,2	2,1	9,0	7,2	4,0	7,2	12,6	9,2	6,2	2,9	1,3	1,2	5,5	4,3		136,2

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	7,2	0,3	2,4	1,0	0,1	0,7	2,4	11,7	6,3	12,6	11,5	4,3	1,5	5,6	3,1	14,5	14,6	15,1	14,6	1,4	8,5	7,3	8,5	1,8	11,6	2,3	.	12,9	12,6	9,9	11,9	218,2
2	Kołobrzeg	5,9	.	3,0	1,7	.	0,2	3,5	6,2	8,6	13,9	8,3	4,0	3,5	11,1	7,6	10,1	13,8	13,3	14,0	2,1	7,0	8,6	5,8	5,9	8,2	3,8	0,1	12,1	13,6	2,9	11,9	210,7
3	Międzyzdroje	3,5	0,1	0,9	9,2	0,3	.	0,6	4,7	10,8	15,0	5,6	4,3	3,9	10,6	9,1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	10,3	5,7	-
4	Resko	1,6	.	2,3	4,2	0,1	3,6	0,9	6,6	8,1	13,1	6,8	4,3	2,5	3,5	4,5	5,5	9,6	12,9	13,4	2,4	6,7	5,3	5,1	5,8	9,8	5,5	0,3	9,9	11,6	2,9	10,2	179,0
5	Szczecinek	2,3	0,2	2,7	1,0	1,2	6,3	1,5	4,5	8,3	12,0	8,9	4,2	0,2	4,8	5,9	11,4	12,1	13,5	13,6	2,2	7,3	4,3	5,0	6,0	10,7	6,5	3,0	8,5	8,4	5,7	6,3	188,5
6	Chojnice	3,3	0,2	3,2	0,1	3,2	6,3	1,0	0,7	7,6	13,2	7,[illegible]	4,0	0,3	1,7	4,1	6,1	9,6	13,0	12,8	5,7	7,5	4,4	9,5	8,6	9,4	7,3	5,4	8,4	5,3	9,7	4,6	184,0
7	Hel	9,5	3,5	1,5	1,5	5,9	4,4	4,0	9,5	8,4	6,5	11,9	4,6	0,7	3,0	1,9	8,5	13,3	14,2	14,5	7,7	8,9	3,9	7,3	4,0	12,3	3,7	1,4	11,4	14,0	6,4	8,4	216,7
8	Gdynia	10,4	4,2	1,9	3,7	6,7	5,3	3,9	5,1	12,3	7,7	10,1	4,0	.	2,3	2,4	9,5	14,3	14,6	14,6	7,9	8,4	4,1	6,8	5,1	10,9	4,3	0,7	9,4	11,7	5,3	9,0	216,6
9	Świbno	4,0	3,6	1,8	0,3	4,9	.	2,2	8,0	9,0	6,5	12,2	4,4	0,3	2,5	4,3	7,4	14,6	14,5	14,2	8,3	10,5	4,2	9,9	3,6	11,5	6,8	4,0	7,9	13,0	7,4	6,2	208,0
10	Stare Pole	9,1	2,7	2,7	0,9	7,4	4,7	1,6	5,8	4,3	5,0	11,3	3,5	0,5	3,0	2,9	6,3	12,3	13,7	13,6	8,8	10,2	3,3	6,2	6,7	12,2	7,9	7,2	8,5	10,9	7,8	7,6	208,6
11	Nadostowo	8,4	5,4	3,1	0,4	4,7	7,0	1,8	3,8	5,2	8,6	12,0	3,0	0,8	3,4	0,7	8,4	14,6	14,6	14,7	8,1	9,7	4,4	9,4	5,9	11,8	8,0	6,2	10,5	10,4	8,4	7,6	221,0
12	Frabuty	8,0	4,6	2,0	.	6,2	4,9	2,2	3,3	4,0	7,2	10,5	3,5	0,2	1,8	2,1	6,7	13,5	11,2	13,5	9,8	10,0	2,5	6,5	5,2	11,8	7,0	3,7	5,6	8,5	9,7	4,2	189,9
13	Bydgoszcz, IMiUZ	2,6	2,0	3,2	.	8,2	4,9	0,5	2,9	5,0	11,1	9,7	6,7	1,2	6,4	5,4	7,1	12,6	9,8	11,1	7,2	9,0	3,9	9,1	9,8	12,6	5,9	5,7	7,1	9,2	6,5	2,6	199,0
14	Suwałki	12,1	9,7	1,1	3,0	1,9	4,6	7,3	8,2	9,4	.	0,2	.	4,1	3,9	0,2	0,3	9,2	7,6	10,2	13,6	11,8	1,1	2,4	5,5	10,8	7,8	3,3	2,3	11,7	9,7	9,6	182,6
15	Mikołajki	10,2	4,7	0,6	2,7	3,6	5,9	6,9	3,6	6,8	4,5	3,3	2,3	.	0,8	2,3	10,6	0,7	7,6	9,2	12,1	9,4	2,4	3,3	5,3	14,0	7,0	6,2	4,6	10,6	7,4	6,8	175,4
16	Biebrza	6,9	6,6	.	2,4	1,2	5,9	7,0	3,3	9,1	3,0	3,1	2,9	2,9	2,6	0,7	4,4	10,0	7,0	9,9	12,3	10,6	2,3	2,3	6,5	13,8	2,1	5,0	4,7	7,7	7,3	7,7	171,2
17	Białystok	5,7	3,8	0,6	2,5	1,4	5,9	8,9	1,6	4,2	3,9	2,3	4,1	3,7	0,8	1,7	5,2	12,4	6,4	2,8	11,8	14,4	5,5	0,7	9,3	12,9	7,4	6,7	4,9	6,8	8,0	10,3	176,6
18	Gorzów Wlkp.	0,2	0,2	3,1	0,7	3,5	5,6	0,6	1,0	5,9	14,4	4,8	5,0	1,8	0,4	6,0	6,4	2,6	4,4	13,8	0,9	6,8	8,9	8,2	7,7	13,1	5,8	7,0	4,8	11,7	4,7	6,8	166,8
19	Przetędowo	.	2,6	4,5	0,1	2,8	5,2	0,8	0,3	8,0	13,8	8,8	5,5	0,4	.	4,8	6,5	12,6	8,3	12,6	3,9	9,7	6,0	9,9	10,7	12,6	8,7	7,2	6,3	10,0	6,8	10,0	199,4
20	Przybroda	0,9	1,2	4,6	0,1	3,2	3,4	0,7	0,7	7,9	14,6	8,7	5,1	0,8	0,8	6,0	3,6	13,2	8,7	13,9	4,7	9,0	7,2	8,7	11,5	13,2	9,3	9,8	10,1	6,1	7,6	6,3	201,6
21	Poznań-Ławica	1,4	2,0	4,5	0,1	3,3	3,7	0,2	1,6	8,1	12,3	7,2	3,4	0,8	0,2	6,1	4,0	12,0	7,0	11,3	4,6	8,8	6,3	8,6	11,7	12,0	9,5	8,1	5,2	10,5	7,7	7,7	189,9
22	Flewiska	0,8	1,4	4,5	0,3	2,7	4,0	0,1	0,9	7,9	14,5	8,5	3,6	1,1	0,3	6,5	2,2	11,2	5,4	12,4	4,6	9,4	7,0	6,9	10,3	12,8	10,0	7,9	5,6	12,3	6,3	7,9	189,3
23	Kórnik	0,5	1,5	4,5	0,2	1,8	4,0	0,3	0,5	7,6	14,8	9,3	4,6	1,4	0,7	6,6	4,2	10,2	6,2	9,7	4,4	9,1	4,6	9,6	8,8	12,3	10,6	6,8	5,8	12,1	9,1	9,5	191,3
24	Oborniki Śl.	.	3,2	.	0,3	0,3	8,7	.	.	0,1	10,2	1,8	3,4	0,8	0,5	2,8	0,2	.	4,5	11,0	6,8	9,5	5,3	9,0	12,6	12,3	10,3	5,1	13,7	10,8	5,3	9,9	158,4
25	Laskowice Oławskie	0,1	2,5	1,5	0,8	0,9	4,5	1,7	3,4	8,7	13,2	5,2	7,1	4,3	0,5	1,6	1,5	.	0,4	7,3	7,3	11,4	5,2	8,0	12,4	12,2	11,8	6,3	9,4	11,2	6,7	11,6	178,7
26	Ciechocinek	3,4	4,4	3,4	0,2	4,0	5,3	1,9	2,4	5,8	7,4	.	.	0,6	3,1	2,4	9,2	14,2	5,6	11,6	10,5	11,0	5,6	8,3	9,1	13,1	8,0	7,3	6,2	8,7	5,6	3,6	181,9
27	Więcławice	2,9	4,3	3,5	.	3,4	5,4	2,4	2,7	5,8	11,7	9,8	6,1	0,9	3,8	3,7	9,8	13,1	10,0	12,9	9,1	12,1	4,5	10,9	12,1	13,2	7,8	5,3	7,1	11,2	7,8	5,6	218,9
28	Legionowo	5,4	6,2	1,4	1,4	1,3	7,4	4,5	3,0	12,5	7,0	12,5	7,9	2,4	5,7	1,4	3,7	13,4	8,5	2,8	13,2	11,9	3,7	4,9	12,3	13,5	10,6	5,9	6,8	12,1	11,4	9,1	223,8
29	Warszawa-Bielany	4,0	6,2	2,4	2,6	2,2	7,4	6,2	4,6	13,7	9,6	12,2	7,8	2,8	4,0	2,5	4,3	11,2	8,7	2,7	12,2	11,1	2,8	4,8	12,1	13,9	12,2	6,3	7,8	12,1	10,7	11,8	232,9
30	Warszawa, Nim.Kom.	5,0	5,0	1,9	2,6	1,9	9,9	1,9	9,1	13,5	10,0	10,8	6,7	2,7	2,7	3,0	4,3	10,8	8,1	1,5	12,4	11,3	2,4	4,8	10,7	12,7	11,0	5,8	13,7	11,9	9,9	11,7	229,7
31	Międzylesie	7,0	3,5	2,5	1,6	1,8	8,6	8,8	6,3	12,2	10,1	11,2	7,8	2,8	3,5	3,8	2,6	13,2	7,7	3,5	13,1	12,1	0,4	4,7	12,1	13,8	12,1	6,0	6,9	8,8	9,8	10,4	228,7
32	Erwinów	4,1	5,6	2,1	1,7	1,2	5,8	6,4	6,7	9,5	12,6	11,1	7,4	1,8	1,9	3,2	2,8	10,4	5,7	0,7	13,0	11,8	2,8	6,7	10,9	14,2	12,3	3,1	3,2	10,0	7,6	11,0	207,3
33	Świder	6,8	4,6	1,6	2,2	1,1	7,8	6,2	2,2	11,7	9,8	11,2	7,8	4,3	4,1	4,0	1,6	11,6	6,6	4,4	12,4	11,3	3,4	1,8	11,6	12,6	11,4	6,2	8,4	10,5	10,0	10,7	219,9
34	Topola-Błonie	0,2	2,8	3,2	0,9	0,1	5,9	5,5	2,5	6,6	13,4	10,6	5,8	1,5	0,5	5,1	5,5	9,0	9,6	4,1	11,3	10,5	3,6	5,5	6,9	12,8	12,1	5,0	6,3	11,5	9,3	12,4	200,0
35	Włocław	4,3	4,4	1,6	1,3	1,2	6,2	7,1	7,1	7,6	12,3	11,4	7,4	2,5	1,8	3,1	1,2	10,2	8,3	0,6	12,5	11,8	1,2	6,0	10,4	14,1	13,3	4,7	6,3	10,6	9,1	11,0	210,6
36	Skierniewice	1,5	3,5	2,0	2,5	1,7	3,9	5,8	6,0	6,3	13,8	11,0	8,7	2,4	1,3	4,3	4,3	11,2	9,6	2,8	13,2	12,4	3,4	10,5	11,9	13,0	13,2	5,7	5,6	13,1	9,7	13,0	227,3
37	Belsk	3,3	4,2	2,0	2,7	2,2	6,9	7,5	5,8	7,1	13,0	11,2	10,9	5,2	2,9	5,1	1,8	8,9	8,1	2,6	12,7	11,5	5,2	7,6	12,6	13,2	12,0	5,4	8,2	13,2	11,7	12,5	237,2
38	Łódź-Lublinek	0,1	1,7	2,6	1,2	1,2	4,5	6,2	2,5	9,3	13,3	9,4	5,7	0,9	0,4	5,0	2,3	9,8	7,8	0,5	12,1	11,7	4,1	7,8	8,8	13,2	12,3	5,1	6,1	13,1	3,1	12,3	194,1
39	Kalisz	0,3	4,5	3,7	1,6	0,5	6,6	2,5	2,6	11,5	12,4	9,4	5,4	3,5	0,1	6,1	1,4	7,7	3,4	9,7	9,0	12,0	5,6	11,4	11,2	11,5	11,8	6,7	11,0	13,0	7,4	10,0	213,5
40	Wieluń	.	2,2	2,5	2,7	1,1	6,0	3,5	3,1	11,2	14,5	7,0	6,9	1,7	0,2	5,7	2,0	0,5	1,4	2,9	12,0	13,0	5,0	8,9	12,6	11,8	12,4	6,7	11,4	13,0	5,6	12,5	200,0
41	Szepietowo	0,1	6,8	.	.	.	6,7	10,3	1,1	7,1	7,1	7,2	6,1	5,6	0,5	5,9	4,5	12,8	10,0	6,2	14,1	13,1	3,0	1,8	11,2	12,0	9,6	5,7	4,6	8,9	11,8	11,4	205,2
42	Białowieża	3,8	6,8	1,7	4,2	5,6	4,3	9,6	1,0	5,3	5,5	2,7	5,4	4,6	3,0	4,4	4,3	.	7,2	1,5	13,6	11,5	11,0	0,1	8,1	13,6	10,5	7,5	5,7	8,3	9,7	9,7	190,2
43	Terespol	7,2	10,1	2,0	5,7	4,7	5,0	10,6	.	9,7	11,1	5,5	6,4	5,7	2,7	1,6	2,5	7,0	6,3	2,6	12,9	13,2	12,9	1,6	9,2	11,1	12,6	6,7	3,4	9,5	12,2	10,9	222,6
44	Sobieszyn	2,3	8,6	1,7	4,0	5,1	2,0	6,2	.	9,6	12,3	12,1	10,9	4,6	1,7	4,5	4,1	6,7	2,9	0,3	14,2	11,9	7,2	0,6	12,0	13,9	13,8	4,7	8,2	12,4	10,6	12,2	221,3
45	Puławy	3,7	5,5	1,2	3,9	4,5	3,5	6,4	2,1	7,6	13,1	11,2	11,0	2,2	.	4,3	4,6	4,4	0,8	.	13,0	12,0	7,2	2,6	9,4	11,6	11,7	4,3	6,6	12,4	10,1	11,7	202,6
46	Chełm Lub.	6,6	6,1	1,8	3,5	5,4	5,7	7,6	.	14,0	14,8	11,7	7,1	6,6	3,1	5,1	5,3	2,7	0,6	.	14,2	13,8	13,8	1,2	7,5	12,9	13,6	4,6	8,6	12,0	10,0	3,7	223,6
47	Szczawno-Zdrój	0,6	1,0	0,9	6,6	2,1	7,0	0,2	3,2	5,5	8,9	2,1	7,0	3,7	0,3	0,6	0,8	0,1	.	10,0	5,2	9,0	4,6	4,8	7,3	9,8	10,3	3,4	9,1	8,4	6,9	7,4	146,8
48	Świeradów	.	0,4	0,8	.	0,5	3,5	.	4,1	5,2	9,8	3,3	7,5	2,6	1,2	.	0,1	0,1	.	6,3	3,8	10,3	9,4	7,0	7,8	11,6	10,4	5,5	8,0	6,7	5,4	6,8	138,1
49	Opole	0,3	3,2	1,1	2,2	3,3	7,8	3,9	2,0	10,7	13,8	7,0	9,3	3,9	1,5	1,8	3,2	0,6	0,1	4,2	10,1	12,9	.	12,0	11,8	12,3	12,2	5,5	9,6	12,1	7,1	12,5	198,0
50	Kudowa-Zdrój	0,1	1,0	0,4	0,5	.	7,2	3,2	5,8	10,5	7,7	5,5	5,7	2,8	0,2	1,1	0,4	.	.	10,8	6,1	12,7	6,9	8,4	6,5	11,0	11,2	8,3	7,2	6,3	8,0	8,2	163,7
51	Polanica-Zdrój	0,1	4,1	0,2	1,8	2,8	10,3	1,5	6,7	10,5	6,6	3,8	8,9	3,6	0,1	2,3	0,3	.	.	11,0	6,9	12,0	7,2	9,8	6,0	11,3	11,8	8,3	4,6	7,4	8,1	8,2	176,4
52	Skroniów	0,7	2,8	1,3	6,2	4,0	6,3	5,3	3,3	8,3	14,1	8,4	6,6	3,8	2,0	4,8	1,3	.	1,2	0,5	11,9	12,8	5,7	7,1	11,8	12,4	12,8	2,7	9,7	12,4	7,2	10,9	198,3
53	Świerklaniec	0,5	0,9	2,4	6,7	2,4	6,1	4,4	3,1	8,5	13,2	9,7	7,0	3,7	0,4	3,3	2,3	.	.	.	12,6	12,1	7,0	8,1	11,8	12,3	13,9	5,2	9,6	12,3	9,3	10,7	199,5
54	Kraków, Obs.Astr.	1,8	6,4	1,0	9,5	6,6	9,9	2,7	2,5	8,0	10,4	10,1	7,9	6,4	1,2	1,8	3,5	0,6	.	.	10,6	12,4	8,4	4,4	8,9	11,5	13,2	6,9	8,0	10,3	8,6	10,8	204,3
55	Cieszyn	0,8	0,7	0,2	4,7	4,6	5,0	3,1	2,4	10,8	3,9	6,7	5,8	3,6	.	2,3	3,2	.	.	.	10,7	12,7	2,4	8,3	10,8	13,0	13,2	6,7	4,4	6,5	4,3	12,0	162,8
56	Istebna-Kubalonka	1,5	1,7	0,1	2,5	3,3	3,5	1,7	3,9	12,5	9,0	9,9	7,6	3,5	4,2	1,7	3,4	1,5	.	.	12,7	13,5	6,7	7,5	10,2	13,3	13,6	7,5	5,7	10,0	5,7	11,0	188,9
57	Babia	1,5	2,6	0,3	10,0	5,5	10,7	2,7	3,0	8,5	8,9	10,0	4,5	4,0	0,4	4,3	3,7	3,5	.	.	11,4	12,9	10,1	4,1	7,4	12,6	13,3	3,5	5,5	10,2	6,4	11,2	192,4
58	Jabłonka	3,6	1,9	0,2	9,9	4,1	9,3	3,9	2,5	10,5	6,2	4,3	5,3	5,8	.	2,0	3,5	0,7	.	0,1	9,1	11,4	9,4	4,7	10,2	7,0	11,9	6,5	4,1	8,1	4,2	9,1	169,5
59	Krynica	3,0	5,0	0,3	5,1	1,5	7,3	1,5	2,6	9,1	6,4	8,4	5,4	4,3	1,9	0,8	4,4	1,8	.	.	9,7	12,0	9,2	2,3	5,5	11,2	11,9	6,1	5,0	8,0	6,8	7,0	163,5
60	Krynica-Góra Park	2,2	4,5	0,3	4,0	2,9	9,3	1,8	2,3	7,7	6,5	9,6	4,1	4,3	1,6	0,5	3,7	1,5	.	.	10,9	13,6	10,9	2,3	5,6	11,2	13,8	7,6	5,0	7,6	6,5	7,4	169,2
61	Muszyna	1,3	5,0	4,0	0,2	4,3	4,4	5,7	2,1	3,3	8,1	6,3	6,9	4,2	5,7	0,5	2,3	2,9	3,2	.	12,0	11,1	8,0	1,8	.	10,7	12,2	7,1	5,8	.	5,7	7,6	152,4
62	Zakopane	1,9	4,8	0,3	10,6	3,6	7,3	1,5	1,3	11,1	6,8	7,8	5,5	5,0	1,6	0,7	6,0	3,8	.	.	9,2	12,6	8,3	1,7	1,0	13,5	13,5	5,0	2,5	5,0	6,2	10,2	168,3
63	Gubałówka	1,2	3,3	0,3	9,2	3,3	5,7	1,0	0,8	8,3	5,7	6,0	4,9	4,6	1,5	0,4	6,3	3,3	.	.	7,3	9,8	7,4	2,3	1,3	10,2	10,2	5,0	2,8	4,9	5,5	8,8	141,3
64	Hala Gąsienicowa	0,7	3,0	0,1	6,1	3,4	3,5	0,4	0,5	9,3	4,3	8,5	3,4	2,7	0,5	0,9	1,9	3,1	.	.	6,3	10,2	4,6	1,0	0,5	11,6	12,0	2,7	0,8	2,0	7,1	5,0	116,1
65	Kasprowy Wierch	0,3	2,8	0,1	6,2	2,7	3,2	0,8	1,1	9,4	4,8	8,7	3,5	3,9	0,7	0,2	2,2	1,9	.	.	4,6	10,2	6,8	1,3	1,6	13,9	13,9	4,1	1,4	1,1	3,8	3,5	116,7
66	Herbkowice	5,7	4,4	2,3	2,3	2,6	5,3	6,4	0,2	12,2	13,4	10,6	7,5	3,3	1,2	5,6	8,0	6,4	.	.	14,0	13,5	13,7	4,0	5,7	13,7	13,6	4,2	9,4	11,3	7,4	2,0	209,9
67	Zdanów	1,4	5,8	0,8	7,0	6,4	6,3	3,4	4,6	8,2	13,8	10,9	8,9	4,8	0,7	7,8	1,7	1,7	.	.	13,5	14,0	11,4	2,6	6,7	13,6	13,4	2,6	8,0	11,6	8,5	11,2	211,3
68	Zwonica - Zdrój	3,7	4,0	0,2	1,7	1,0	6,3	3,1	0,9	3,7	8,8	10,5	3,8	1,3	2,0	2,4	4,1	6,2	.	.	10,1	10,1	9,8	1,2	7,5	10,1	12,8	8,8	7,5	9,1	8,2	5,2	164,1
69	Leśko	3,3	2,4	0,2	0,3	1,1	7,0	4,0	2,7	4,6	7,7	8,4	3,3	1,5	0,3	0,8	2,3	3,7	.	.	9,9	13,9	11,3	1,5	3,3	12,7	12,3	9,2	8,6	7,2	8,2	1,9	153,6

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	10,2	5,3	12,7	.	4,4	9,2	0,7	2,1	7,6	1,8	2,9	11,4	11,8	11,4	1,0	7,6	3,5	3,9	3,4	0,1	4,7	8,3	6,2	0,4	2,5	9,5	4,1	9,0	3,6	0,9	5,2	163,4
2	Kołobrzeg	8,3	7,6	9,2	0,3	2,3	5,3	.	1,7	11,9	0,3	3,0	10,3	8,3	12,6	1,0	8,5	2,8	2,5	6,3	.	0,1	5,3	2,5	0,7	1,8	6,5	3,7	7,6	2,6	4,3	6,3	143,4
3	Międzyzdroje	3,0	2,9	3,9	0,3	0,7	1,8	.	2,7	7,8	0,5	2,3	10,9	7,1	12,3	0,8	8,4	1,2	0,7	6,2	.	1,0	1,6	1,5	0,5	3,6	4,1	2,8	3,3	1,9	5,4	1,5	100,7
4	Resko	3,5	6,9	4,2	0,3	0,4	3,3	.	1,4	9,3	0,5	3,7	10,7	4,3	11,8	.	8,1	0,5	1,3	3,4	.	0,4	3,7	1,0	.	2,4	6,6	2,8	4,5	0,6	5,1	2,0	102,7
5	Szczecinek	4,3	7,0	5,1	1,0	0,5	2,9	0,2	2,6	9,5	1,9	2,9	13,2	5,1	12,6	0,1	9,6	6,1	1,3	5,7	0,2	1,0	4,1	0,9	.	1,8	4,7	1,8	4,8	0,5	2,3	1,2	115,1
6	Chojnice	4,1	4,0	5,6	0,2	0,1	1,9	0,5	6,4	7,7	2,9	2,3	12,0	5,3	8,8	0,3	7,9	5,4	2,4	1,4	4,3	2,8	4,3	2,5	.	1,3	1,6	2,2	3,1	0,2	3,1	2,2	106,8
7	Hel	6,4	7,1	10,9	1,4	5,2	6,5	1,2	6,1	9,4	3,5	4,9	10,2	12,3	12,6	0,8	7,9	5,9	0,6	0,8	0,1	10,1	2,6	5,9	.	2,5	8,8	2,7	8,2	1,1	4,5	3,4	163,6
8	Gdynia	6,8	6,3	10,4	1,0	5,2	6,8	0,5	6,8	10,0	3,9	5,0	11,3	12,2	13,2	1,4	3,9	6,3	1,3	1,0	0,1	8,9	2,5	5,9	.	2,5	9,2	2,5	5,9	2,7	4,4	3,9	161,8
9	Świbno	6,3	4,7	10,7	0,9	3,6	6,1	9,2	1,2	12,7	4,3	3,8	11,5	10,6	12,5	1,5	6,8	5,8	1,4	2,8	.	7,4	2,6	4,9	.	2,1	8,5	2,7	5,7	0,7	.	4,3	155,3
10	Stare Pole	6,1	5,3	7,6	1,0	4,1	6,1	0,6	9,3	12,2	4,7	1,7	12,1	9,9	12,8	1,1	6,2	4,9	2,0	2,0	.	5,4	2,5	5,2	.	3,2	5,9	4,4	4,6	1,3	2,5	4,4	149,1
11	Radostowo	7,6	5,2	10,2	1,4	3,5	5,6	0,9	12,2	11,4	4,6	2,5	12,6	8,4	12,5	1,0	4,7	8,0	0,6	2,1	0,5	8,5	2,7	5,7	.	2,6	6,2	3,6	5,8	2,1	4,3	3,3	160,3
12	Prabuty	6,1	3,1	6,4	0,4	3,3	4,9	0,2	11,1	11,0	5,0	0,7	13,0	7,6	11,8	0,8	5,5	4,3	2,0	1,9	.	3,5	2,6	3,2	.	2,5	5,0	5,5	4,7	0,4	5,8	1,8	134,1
13	Bydgoszcz, IMUZ	4,8	5,2	7,5	2,0	0,2	4,3	0,6	11,9	10,9	4,7	4,7	12,7	6,8	0,9	0,5	7,6	4,1	0,4	1,4	1,8	1,8	5,4	1,9	.	3,3	6,9	4,8	1,9	.	1,5	2,3	122,8
14	Suwałki	4,3	9,4	7,5	2,2	5,6	5,0	4,2	9,6	10,7	8,0	2,7	11,7	12,1	13,3	4,8	7,2	6,4	1,2	4,6	4,4	8,5	2,1	4,0	1,1	3,4	4,2	6,7	6,2	3,3	3,1	1,1	178,6
15	Mikołajki	4,0	5,5	8,5	1,1	3,5	5,1	3,4	11,1	8,5	9,1	1,8	11,7	11,6	13,1	1,7	5,7	3,9	1,7	2,4	5,4	8,3	3,3	5,0	.	5,8	7,8	5,7	4,5	1,6	0,7	1,5	163,0
16	Biebrza	4,4	5,2	8,5	2,0	7,9	4,7	4,4	10,2	9,4	8,4	2,0	9,6	11,4	12,3	2,5	7,0	2,6	3,5	2,3	6,4	7,3	3,0	3,9	.	5,4	6,6	7,6	6,0	1,0	2,3	1,8	169,6
17	Białystok	2,7	6,7	6,6	1,8	3,5	3,0	9,1	9,9	11,5	10,4	1,3	12,1	10,4	6,8	3,9	1,1	5,6	4,5	6,8	4,2	4,3	4,6	4,5	.	4,1	6,7	9,3	5,3	1,3	2,2	1,3	165,5
18	Gorzów Wlkp.	4,7	4,8	5,0	2,6	1,2	1,8	.	6,9	9,3	0,8	6,9	12,3	.	0,1	0,2	6,8	3,5	2,6	1,8	.	3,5	4,5	2,3	.	3,9	8,4	1,8	1,6	1,2	6,0	1,3	105,8
19	Przebędowo	5,9	7,9	7,3	2,9	1,7	5,3	1,0	11,2	12,4	3,8	6,6	12,5	10,3	.	0,6	9,0	4,1	1,2	0,7	.	2,3	3,2	2,0	.	2,9	8,4	5,2	2,9	0,3	3,3	0,5	135,4
20	Przybroda	4,6	7,8	6,5	3,9	0,8	3,3	0,8	13,0	11,2	4,0	6,5	13,1	10,7	.	0,8	9,4	3,8	1,9	1,0	.	4,3	3,5	3,5	.	2,9	8,9	5,2	3,1	1,2	6,2	5,3	147,2
21	Poznań-Ławica	4,4	7,5	4,9	3,2	2,0	4,3	0,8	12,2	10,0	3,5	6,1	12,1	9,8	0,1	1,2	8,7	4,4	1,7	.	0,3	5,9	3,0	3,1	.	1,8	7,4	5,2	3,3	0,4	7,0	1,0	135,3
22	Plewiska	4,0	7,9	6,2	3,6	2,6	3,2	0,8	11,7	11,1	2,8	5,2	13,2	10,8	.	0,8	9,6	3,2	1,5	0,3	.	5,1	3,4	3,4	.	2,1	8,1	5,4	2,4	0,4	4,7	1,3	134,8
23	Kórnik	4,9	5,6	4,8	2,9	3,1	2,7	0,4	12,9	12,1	4,4	5,8	13,1	11,1	.	1,0	10,2	3,0	2,5	0,2	.	3,5	3,0	2,5	.	1,0	8,6	4,7	1,7	1,0	3,1	0,8	130,6
24	Oborniki Śl.	4,0	2,1	10,0	9,1	1,9	2,3	3,2	12,0	9,8	9,3	12,2	12,9	10,7	0,8	0,8	9,4	0,9	4,7	.	.	7,7	5,8	6,4	.	5,0	7,2	8,1	1,3	2,3	4,2	.	164,1
25	Laskowice Oławskie	4,6	10,2	2,6	7,9	4,9	2,3	3,1	10,9	8,4	7,7	5,2	11,8	10,1	5,1	1,8	7,0	1,9	4,1	.	0,2	9,1	4,5	7,0	0,9	4,1	9,8	7,9	2,8	2,2	1,6	0,5	160,1
26	Ciechocinek	4,1	8,2	7,8	2,6	2,5	5,0	1,3	11,3	10,7	5,8	4,7	12,0	9,3	.	0,3	8,5	2,3	.	1,0	3,1	3,1	3,1	2,5	4,7	.	7,0	6,0	2,4	0,1	1,8	2,7	135,9
27	Więcławice	4,9	8,3	9,1	2,1	1,5	6,5	1,9	12,4	11,7	6,3	6,9	12,8	9,8	.	0,6	9,6	3,7	0,8	.	3,7	3,7	4,5	1,9	.	9,8	5,6	6,1	3,2	0,2	3,5	4,1	155,2
28	Legionowo	3,0	8,9	9,1	2,8	6,9	7,1	7,7	11,1	9,3	9,5	3,6	11,6	10,7	.	0,7	1,7	7,3	2,5	0,9	3,0	1,2	0,5	4,3	.	3,6	8,0	8,3	5,0	1,9	4,2	1,7	156,1
29	Warszawa-Bielany	2,9	9,3	7,8	7,8	8,3	6,4	8,5	11,3	10,1	11,5	6,1	12,7	11,4	.	0,7	1,8	9,0	5,3	0,3	3,4	0,9	2,3	4,5	.	3,9	9,2	9,2	5,5	2,6	4,4	1,7	178,8
30	Warszawa, Min.Kom.	2,9	10,7	7,8	6,9	6,1	9,2	9,0	8,8	11,0	11,0	6,6	11,1	11,8	.	0,4	1,8	8,0	5,6	1,2	3,2	0,7	2,4	4,4	.	3,0	9,7	8,1	3,6	1,3	3,9	1,6	171,8
31	Międzylesie	4,5	9,1	9,2	8,4	7,8	6,0	8,7	11,0	9,0	11,3	9,2	9,3	11,5	0,4	0,3	1,6	8,7	5,7	1,3	4,4	1,0	2,0	5,2	.	4,5	8,0	9,5	6,4	3,4	5,4	1,4	184,2
32	Brwinów	2,2	7,4	4,4	4,3	5,7	2,9	6,8	10,5	7,9	9,7	3,7	11,7	11,5	0,2	0,2	1,5	8,7	2,9	2,0	2,2	1,9	2,6	3,6	.	3,9	8,9	8,3	5,6	3,4	1,7	1,3	147,6
33	Świder	2,5	8,5	6,1	5,7	7,5	5,2	9,1	10,9	8,3	10,5	7,2	11,4	10,9	0,3	0,2	2,1	10,1	5,5	2,4	3,9	0,4	1,5	4,9	.	4,1	8,4	8,5	6,3	4,1	5,7	1,2	173,4
34	Topola-Błonie	5,1	8,0	4,4	.	3,3	3,0	3,1	12,3	10,2	8,7	6,0	12,1	11,4	0,9	0,6	7,5	3,7	2,2	1,1	2,0	4,8	2,4	4,6	.	1,7	7,8	8,3	4,7	3,3	1,5	2,7	147,4
35	Młochów	1,8	5,7	3,8	5,7	7,1	3,3	7,0	11,6	8,1	11,1	2,4	12,8	11,9	0,6	0,4	1,6	8,8	3,3	1,7	1,6	0,7	3,8	3,8	.	3,7	10,6	8,7	5,8	3,8	2,3	2,1	155,6
36	Skierniewice	5,7	5,8	5,6	6,1	6,8	4,9	6,2	12,2	9,6	10,1	7,1	12,6	11,9	1,0	0,4	2,3	7,8	1,7	1,3	1,9	2,1	3,6	5,0	0,3	3,4	10,0	3,4	6,9	3,7	1,0	2,3	162,7
37	Belsk	3,8	8,1	4,3	8,4	7,9	4,1	8,7	10,6	7,5	11,1	7,6	12,1	10,1	0,4	0,5	1,6	7,9	3,5	2,0	2,8	0,6	3,3	5,1	.	4,9	9,7	8,4	6,7	4,3	2,8	1,9	170,9
38	Łódź-Lublinek	3,8	6,9	2,6	4,2	4,3	1,1	3,9	11,5	10,0	9,7	6,0	12,1	9,8	1,8	1,3	4,0	6,2	1,4	0,3	1,3	3,6	2,5	4,1	.	3,5	7,7	8,4	2,7	2,4	1,1	0,8	139,0
39	Kalisz	6,6	7,4	2,8	4,4	4,1	1,7	3,4	12,9	12,3	7,2	5,9	12,6	12,8	0,5	1,1	9,5	2,9	2,1	0,1	.	3,5	3,9	5,0	.	3,0	9,7	7,9	3,9	1,2	3,1	1,7	153,2
40	Wieluń	3,7	8,9	4,4	8,4	4,5	1,3	5,7	12,4	10,4	9,0	8,6	13,0	11,9	3,2	2,0	5,5	4,5	3,7	.	0,1	2,3	4,6	6,7	.	4,6	8,7	8,7	3,1	3,3	2,5	1,2	166,9
41	Szepietowo	3,5	8,4	12,3	5,6	9,0	5,8	8,8	10,0	11,5	11,7	3,2	12,9	11,7	1,9	0,2	1,8	8,0	3,9	11,5	7,0	4,6	4,5	9,7	.	7,4	10,9	3,0	4,3	1,1	1,1	1,1	196,4
42	Białowieża	2,0	7,4	9,1	4,5	10,8	6,1	11,4	11,0	11,9	12,8	5,1	12,8	10,5	1,1	2,2	0,1	9,9	2,6	4,5	1,8	2,7	3,0	4,1	.	4,5	7,2	10,5	5,8	2,6	3,3	0,5	181,8
43	Terespol	2,6	10,1	8,0	12,1	9,7	5,5	11,4	11,0	9,6	12,5	7,6	12,4	9,0	1,0	1,3	0,1	8,8	6,7	4,8	3,7	3,6	4,7	6,1	.	6,7	11,4	10,6	7,7	5,6	2,7	1,9	208,9
44	Sobieszyn	2,6	7,7	2,4	9,3	9,2	4,7	9,7	10,5	11,3	13,1	6,4	13,4	7,7	0,2	0,8	0,4	8,2	3,8	3,2	2,2	3,4	3,0	5,8	.	5,1	6,6	10,2	6,6	4,5	2,6	1,5	176,1
45	Puławy	2,2	7,1	0,9	7,8	9,1	5,9	10,8	8,7	9,2	12,1	6,2	11,7	7,8	3,3	0,8	0,1	8,2	4,4	1,5	1,8	1,9	1,4	5,0	.	2,4	6,5	9,1	5,5	4,0	2,2	0,4	158,0
46	Chełm Lub.	7,2	6,5	0,1	9,9	8,6	9,9	13,0	7,9	3,0	13,1	8,8	12,1	10,4	7,1	3,8	.	5,7	5,6	4,8	1,4	3,5	4,1	5,3	.	0,8	9,6	11,9	6,3	4,4	7,9	0,6	195,3
47	Szczawno-Zdrój	4,0	4,9	0,9	7,5	2,4	1,2	1,9	9,8	6,7	6,0	3,6	12,1	10,0	3,0	3,1	5,4	0,3	4,9	0,2	0,3	9,7	3,2	6,5	3,0	3,1	9,7	7,4	0,9	1,9	3,6	4,0	141,2
48	Śnieżka	6,3	9,9	2,1	5,8	2,5	0,6	0,3	7,2	8,9	4,4	3,4	12,1	0,9	5,3	3,4	7,5	0,2	3,1	0,1	0,2	10,5	4,0	6,0	0,1	0,8	8,2	6,5	2,3	1,4	2,1	3,7	129,8
49	Opole	6,2	11,2	3,5	8,3	6,2	4,6	7,7	11,9	9,7	8,7	9,9	12,0	10,8	4,5	4,2	5,1	4,7	4,2	0,2	0,2	8,3	6,1	8,9	1,4	6,7	10,6	9,1	3,4	2,8	3,7	3,0	197,8
50	Kudowa-Zdrój	6,0	10,0	4,6	9,7	6,3	.	5,7	10,9	10,3	9,5	8,9	12,2	11,5	3,0	3,8	8,4	0,8	3,2	.	3,4	11,2	5,5	8,9	4,6	6,4	11,0	8,4	3,0	2,5	7,2	5,0	201,9
51	Polanica-Zdrój	10,8	10,6	3,0	10,6	3,6	4,3	6,7	11,6	11,8	8,3	10,6	12,2	12,0	2,9	2,9	10,2	0,5	5,6	0,4	1,5	10,1	6,3	9,7	5,5	8,0	10,6	9,9	3,8	4,2	4,1	5,7	218,0
52	Skroniów	4,4	11,9	1,6	8,3	5,4	8,0	10,5	9,8	10,1	10,6	11,5	12,2	8,4	6,0	3,7	0,9	10,1	2,7	1,7	.	0,8	0,9	9,0	.	0,8	9,9	8,6	6,7	3,9	4,9	.	183,3
53	Świerklaniec	3,2	8,9	2,4	6,5	7,7	8,0	9,2	8,7	4,6	10,1	10,0	11,1	7,0	3,6	3,7	3,9	6,7	3,6	0,5	.	1,1	3,8	8,7	1,9	1,0	10,2	10,4	5,7	3,9	3,4	2,5	172,0
54	Kraków, Obs.Astr.	7,7	9,5	2,0	6,1	7,4	9,0	11,2	11,1	8,1	11,6	10,7	11,2	8,1	6,0	5,6	1,4	7,7	3,2	1,8	0,1	2,3	0,9	7,5	3,1	2,7	11,2	10,0	6,8	4,9	9,4	3,3	201,6
55	Cieszyn	6,8	8,9	0,9	9,3	6,0	10,3	10,0	7,7	7,5	11,4	10,3	12,3	7,2	0,8	5,7	3,6	5,9	0,5	3,3	.	6,2	1,2	6,4	0,4	0,8	11,6	9,2	6,9	4,1	4,6	3,3	183,1
56	Istebna-Kubalonka	8,4	11,2	2,5	9,5	5,9	10,0	10,7	10,7	8,7	11,1	9,0	12,1	5,3	5,8	7,5	3,7	1,1	8,5	3,5	.	5,8	3,9	7,6	2,2	2,9	10,7	8,6	11,3	5,7	4,1	6,5	214,5
57	Babia	7,1	9,9	0,5	9,6	7,6	8,8	11,9	10,1	4,7	11,8	12,0	12,0	6,3	8,3	7,8	3,4	7,9	4,4	2,0	.	6,8	0,4	4,6	1,8	2,4	11,5	11,2	8,4	6,5	6,3	4,9	210,9
58	Jabłonka	9,1	10,1	3,1	4,4	7,0	7,9	9,7	9,5	9,7	11,4	9,7	8,7	7,4	6,1	8,0	3,2	6,0	2,7	4,2	.	7,6	0,2	6,5	0,5	1,5	11,1	9,8	9,0	7,2	9,5	5,9	206,7
59	Krynica	7,0	9,2	0,9	8,3	6,7	6,6	10,8	6,9	7,8	9,3	6,7	10,7	9,9	9,1	5,0	1,8	4,5	2,1	2,7	1,5	2,8	2,0	6,4	3,7	0,6	10,8	9,9	8,4	5,6	6,6	3,9	188,2
60	Krynica-Góra Park.	8,4	9,8	1,8	9,4	6,9	6,3	12,5	6,7	7,4	10,4	8,3	12,3	11,4	10,5	5,4	1,4	6,8	2,5	3,7	1,6	2,4	3,1	6,3	3,8	0,5	11,1	10,4	8,8	6,6	7,7	4,0	208,2
61	Muszyna	7,7	8,0	1,3	7,6	5,4	6,4	11,3	8,3	6,2	9,7	7,5	10,7	1,1	8,6	5,6	0,9	4,3	10,4	5,4	0,8	2,0	2,7	6,0	2,0	0,5	11,0	10,4	8,8	5,5	7,8	2,9	187,0
62	Zakopane	7,3	10,0	1,3	11,1	6,8	11,7	12,3	8,2	1,7	10,2	12,3	10,1	4,2	8,1	9,0	1,2	5,3	5,2	4,2	.	2,0	0,9	7,5	1,7	0,3	12,6	11,7	9,5	6,5	4,7	5,2	202,8
63	Gubałówka	8,3	8,6	0,8	10,3	6,9	9,2	10,2	7,3	3,0	7,8	10,1	7,4	3,3	7,5	6,6	0,3	4,7	5,6	5,5	.	1,8	1,0	6,2	1,2	0,4	9,7	9,8	8,1	6,6	6,6	5,0	179,7
64	Hala Gąsienicowa	3,9	5,9	0,9	7,7	5,4	5,8	10,1	5,4	0,6	4,7	7,8	9,2	3,6	7,0	7,1	0,1	4,2	4,5	3,2	.	2,7	0,4	3,9	0,9	1,1	10,6	11,1	9,1	6,9	1,3	6,4	151,5
65	Kasprowy Wierch	4,6	7,5	1,9	7,8	7,1	9,4	10,8	7,0	0,9	8,4	11,3	11,5	3,9	7,6	8,2	1,3	5,4	4,4	3,0	.	4,8	0,8	7,2	1,6	0,5	12,3	12,5	9,9	7,8	1,4	6,9	187,7
66	Wartkowice	8,1	8,4	.	7,5	7,7	10,3	12,4	5,3	0,4	11,8	9,3	12,0	10,4	10,3	4,2	.	2,9	5,3	4,6	0,5	2,9	4,3	3,9	.	0,9	9,2	10,7	6,9	6,6	5,9	0,8	183,5
67	Zdanów	5,1	9,3	0,3	6,7	9,2	9,8	12,5	9,7	8,6	10,7	9,7	13,3	9,8	4,7	4,3	0,6	7,4	5,4	1,5	1,5	2,0	2,0	5,3	0,3	0,8	10,2	10,1	5,4	4,4	4,9	0,6	186,3
68	Iscanica - Zdrój	9,3	6,6	1,8	6,7	6,9	6,6	11,6	6,2	2,2	9,1	8,5	9,4	8,7	9,1	5,1	0,2	7,7	1,0	1,8	.	1,4	5,0	6,2	0,3	1,0	9,6	10,4	9,4	6,6	5,6	4,2	178,2
69	Lesko	7,0	~~9,4~~	~~2,1~~	8,7	6,7	8,0	9,9	0,7	.	8,9	7,8	10,3	11,6	8,9	6,4	0,7	5,8	.	2,3	.	4,1	5,2	3,6	0,2	0,1	9,5	12,1	8,8	8,0	5,0	4,3	175,1

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	11,5	4,7	10,1	8,1	3,2	2,4	2,3	4,0	5,0	9,7	1,6	1,8	10,2	8,3	1,8	4,7	3,7	2,1	.	2,2	0,8	6,0	0,8	10,1	10,1	9,7	9,8	.	.	4,0		148,7
2	Kołobrzeg	11,6	6,6	9,1	7,9	3,4	1,7	1,9	2,9	2,5	10,1	0,7	2,1	10,3	5,2	4,0	4,1	7,5	3,2	.	3,3	4,5	4,7	3,7	7,6	9,5	9,9	10,3	.	.	0,7		149,0
3	Międzyzdroje	9,3	6,6	8,6	3,8	3,5	2,8	1,7	4,0	0,8	10,4	2,2	2,8	9,3	0,5	3,1	2,0	8,8	.	.	4,6	4,4	5,9	4,7	7,5	11,1	10,0	9,3	0,6	.	.		138,3
4	Resko	8,9	8,3	8,8	8,1	5,0	3,8	1,1	7,1	0,4	10,5	1,1	3,1	9,4	2,5	3,7	2,6	4,4	2,2	.	3,0	2,0	8,3	3,0	5,2	10,1	9,9	10,1	2,2	.	1,9		146,7
5	Szczecinek	10,2	8,9	10,8	8,2	4,0	4,1	2,3	9,6	1,5	11,1	0,8	2,6	9,0	2,6	3,2	3,6	2,7	0,9	.	0,9	0,2	5,6	2,9	2,3	7,2	10,6	10,3	.	.	4,9		141,0
6	Chojnice	9,8	6,1	9,7	9,0	2,3	2,0	1,8	8,0	1,6	11,3	0,5	1,9	10,7	1,3	1,9	4,6	0,3	0,1	.	1,4	0,1	2,7	0,3	5,5	7,5	9,5	10,2	.	.	5,0		125,1
7	Hel	11,0	2,6	7,8	9,5	2,7	2,2	2,4	6,5	8,7	8,4	0,2	0,9	10,6	10,1	0,4	5,6	0,5	4,0	.	0,8	3,0	5,0	0,5	3,3	9,6	9,2	7,9	0,1	.	1,0		134,5
8	Gdynia	11,5	0,8	4,6	8,6	2,5	1,8	2,6	7,2	9,6	9,0	0,2	2,7	11,3	8,6	1,9	5,2	0,5	4,3	0,1	0,4	2,7	4,2	0,2	5,7	9,9	10,0	8,2	.	0,2	3,6		138,1
9	Świbno	10,6	4,4	8,1	9,7	2,1	2,3	0,9	8,3	7,3	8,8	0,1	0,9	11,0	.	1,2	5,7	0,7	.	.	0,9	1,1	6,1	0,2	6,9	6,5	9,6	8,3	.	.	2,8		124,5
10	Stare Pole	10,0	6,5	9,8	10,5	3,5	2,3	1,1	8,8	6,4	9,3	0,2	1,6	11,6	8,8	1,2	5,2	0,5	0,2	.	1,0	0,5	1,3	.	5,9	6,2	9,7	8,2	.	.	5,1		135,4
11	Radostowo	11,1	1,6	10,0	10,2	2,4	1,4	2,0	8,5	6,8	9,6	0,8	1,8	11,2	6,5	1,0	5,3	0,8	.	0,1	1,7	0,5	6,4	0,1	4,2	7,7	10,2	8,1	.	.	1,4		131,4
12	Prabuty	10,0	7,4	9,0	11,2	3,3	4,4	2,0	7,0	3,9	7,8	0,7	1,6	10,4	4,7	0,5	5,5	.	.	0,1	0,3	0,2	1,2	0,1	5,0	8,5	10,0	6,6	.	.	1,6		123,0
13	Bydgoszcz, IMiUZ	8,3	10,3	10,9	10,5	3,5	7,7	2,7	9,0	2,6	10,3	1,5	4,0	8,8	3,3	4,1	3,2	0,1	.	.	3,4	0,1	3,2	0,1	1,4	5,2	9,5	9,9	.	.	6,0		139,6
14	Suwałki	5,7	0,1	1,2	11,4	7,9	8,4	0,5	8,8	5,9	4,3	0,4	1,2	11,2	7,5	3,8	9,3	0,1	.	0,1	0,5	.	0,5	0,1	3,2	7,9	10,1	0,9	.	.	1,3		112,3
15	Mikołajki	8,3	2,6	7,0	11,4	5,8	5,8	1,8	8,4	4,0	7,0	0,3	1,2	10,3	8,8	1,2	7,9	0,3	0,2	.	1,3	0,5	1,4	1,5	0,7	8,6	10,2	0,5	.	.	3,1		120,1
16	Siebrna	7,6	2,1	2,9	10,6	6,8	7,0	0,3	9,3	5,3	6,2	1,6	2,1	10,0	8,9	3,2	7,5	.	.	0,7	0,8	0,2	0,4	1,2	2,7	6,9	9,7	0,7	.	0,4	2,3		117,4
17	Białystok	7,0	1,8	9,6	11,4	8,3	7,0	0,3	8,8	4,6	7,2	3,2	3,3	8,9	3,9	5,6	7,3	3,2	.	0,6	1,0	0,5	0,8	0,4	1,9	8,3	3,5	.	.	0,2	5,3		123,9
18	Gorzów Wlkp.	8,6	10,7	9,6	7,2	5,3	5,4	2,6	5,3	1,3	10,2	1,6	5,3	8,0	0,2	8,4	0,1	3,1	1,3	.	6,0	0,1	2,9	0,6	1,5	4,6	8,8	9,3	2,2	4,8	2,7		137,7
19	Przebędowo	6,2	8,9	10,2	10,6	2,9	6,0	2,1	8,2	1,5	10,1	2,3	3,7	7,5	1,9	7,9	1,6	.	.	.	4,0	0,3	3,0	1,1	1,1	6,1	10,0	8,3	1,1	.	6,6		133,2
20	Przybroda	1,4	10,4	11,3	10,8	3,0	5,6	1,6	8,2	0,3	10,6	2,5	4,9	9,2	1,1	8,0	1,1	.	0,2	0,1	5,3	0,9	1,8	1,7	0,5	4,6	10,1	8,7	2,7	0,6	6,5		133,9
21	Poznań-Ławica	4,5	8,1	10,8	10,0	2,8	6,3	1,8	8,2	0,3	10,1	1,2	5,4	8,4	1,2	7,9	1,7	0,1	.	.	4,7	0,8	2,7	0,9	1,0	4,6	9,4	8,2	1,4	0,2	4,8		127,5
22	Plewiska	4,4	9,5	11,6	10,1	2,8	6,2	2,6	8,6	0,7	10,8	2,0	4,9	9,2	0,6	8,4	1,2	.	.	.	4,0	0,3	1,0	.	0,4	5,3	8,9	8,6	1,7	0,2	3,9		127,9
23	Kórnik	4,5	9,7	12,0	10,8	3,9	5,8	1,6	7,9	1,5	10,9	1,7	3,6	8,5	1,2	9,8	2,5	.	.	0,2	3,9	0,9	3,1	1,0	.	4,9	11,0	7,0	0,3	0,2	6,1		134,5
24	Oborniki Śl.	3,3	11,1	11,7	11,3	6,1	6,6	2,4	3,9	3,5	11,0	.	8,9	1,1	0,9	.	10,5	.	.	.	8,8	1,6	.	.	.	.	10,3	1,6	2,0	3,6	8,1		128,3
25	Laskowice Oławskie	5,2	8,8	11,1	11,1	2,1	4,8	1,5	2,2	3,8	10,8	0,7	6,0	3,8	2,0	9,4	8,6	.	.	0,3	6,7	0,6	1,3	.	.	6,2	9,4	5,7	2,8	0,8	8,9		134,6
26	Ciechocinek	6,7	6,8	10,1	11,2	2,2	6,6	1,5	6,6	2,8	9,6	0,6	3,3	7,8	1,5	5,0	3,4	.	.	.	2,8	0,9	4,5	.	2,5	5,7	8,9	6,7	.	.	4,5		122,2
27	Więcławice	2,5	4,2	10,1	10,8	4,3	7,6	2,5	8,1	2,9	10,0	1,7	5,1	8,4	6,7	6,9	3,2	.	.	.	3,7	0,8	3,8	0,2	3,1	7,2	9,5	7,5	.	.	7,0		137,8
28	Legionowo	6,9	8,9	11,2	11,6	4,0	3,1	1,5	8,4	2,7	9,5	0,7	2,4	7,6	1,7	7,3	7,8	.	.	0,1	4,0	0,4	1,1	.	2,6	7,3	9,7	3,2	.	0,1	5,3		129,1
29	Warszawa-Bielany	6,8	9,2	10,9	11,1	4,6	8,1	1,4	7,9	2,8	8,5	0,5	2,7	7,9	3,5	6,4	7,0	0,1	.	0,6	4,6	0,3	0,9	.	2,2	7,9	9,6	2,3	.	.	5,9		133,7
30	Warszawa, Min.Kom.	7,1	8,5	10,6	10,8	4,8	8,3	1,3	8,6	8,4	.	0,6	2,3	8,1	.	8,2	7,7	.	0,4	0,4	5,2	0,5	1,7	0,1	1,5	8,7	8,9	2,2	.	.	6,3		131,2
31	Międzylesie	7,6	9,6	10,6	11,4	4,6	8,8	1,2	7,9	2,9	9,2	1,3	3,6	7,3	3,0	8,9	9,4	0,2	0,3	0,4	3,9	0,8	0,9	.	0,8	8,4	9,2	2,6	.	.	4,4		139,2
32	Brwinów	5,8	7,7	11,1	11,3	3,6	6,4	1,4	7,1	2,1	9,3	0,5	2,2	7,1	2,2	8,1	7,6	.	0,1	.	4,3	0,1	0,4	.	2,8	6,7	7,8	2,0	.	0,5	5,7		124,1
33	Świder	4,9	8,8	10,4	10,2	4,1	7,7	1,1	6,7	3,2	9,3	2,0	3,6	7,4	3,6	9,1	7,7	.	0,1	0,2	3,7	0,6	0,7	0,4	0,3	8,6	9,0	1,1	.	0,2	3,9		128,6
34	Topolin-Błonie	8,0	7,9	11,2	11,2	1,7	7,8	1,7	8,3	2,2	9,4	1,2	3,9	6,7	7,2	9,4	.	.	.	0,5	6,1	2,6	4,6	.	0,8	6,4	10,0	7,0	.	.	8,1		143,9
35	Młochów	8,3	8,4	11,7	11,3	4,5	7,4	1,5	8,1	3,1	9,8	1,1	3,0	8,1	2,4	8,0	7,3	0,1	0,1	.	4,3	0,4	0,6	0,2	2,0	8,2	8,7	1,7	.	0,2	8,3		138,8
36	Skierniewice	4,6	8,2	10,5	11,0	3,7	6,8	2,0	6,1	3,8	9,4	0,3	0,5	6,8	2,4	9,5	7,9	.	0,6	0,2	5,9	0,2	0,2	.	0,7	4,8	9,3	5,2	.	2,2	6,7		129,5
37	Belsk	8,2	7,4	9,6	10,2	4,9	7,7	1,2	5,8	4,0	9,2	1,6	2,5	8,2	4,1	9,0	7,9	0,1	.	0,8	4,6	0,9	0,7	0,7	2,1	7,4	8,6	2,0	.	0,5	8,3		138,2
38	Łódź-Lublinek	5,7	7,1	11,7	10,8	1,3	7,0	2,1	6,4	1,7	9,2	1,6	4,1	6,1	0,9	9,9	7,7	.	.	0,3	4,4	1,6	1,3	.	0,2	8,4	10,1	5,6	.	0,5	6,7		132,4
39	Kalisz	8,3	8,2	11,4	11,3	3,1	6,9	2,2	5,6	1,4	10,8	2,0	4,2	8,7	1,1	10,2	6,4	.	.	.	5,9	2,5	4,7	.	.	6,8	9,5	1,2	.	0,4	6,1		138,9
40	Wieluń	5,8	8,2	12,3	11,9	2,1	6,1	0,9	2,1	2,2	11,3	1,7	6,4	6,7	2,4	10,1	9,6	.	.	0,9	4,9	1,3	3,0	.	.	7,1	11,1	1,1	.	1,9	9,4		140,5
41	Szepietowo	8,5	7,7	0,7	.	.	7,7	0,1	7,5	2,3	7,3	1,3	3,9	7,4	7,4	5,2	8,6	0,9	.	.	.	1,3	.	1,3	2,2	7,3	8,8	0,1	.	.	3,8		101,3
42	Białowieża	5,9	2,3	10,0	11,2	9,8	6,9	0,4	8,3	3,1	6,6	5,2	7,2	9,2	3,2	7,7	9,3	7,3	.	0,8	4,3	0,5	0,4	0,9	2,2	6,1	7,3	.	.	0,7	1,1		138,1
43	Terespol	5,8	7,3	11,5	11,8	9,4	7,6	0,2	7,1	2,1	8,1	5,3	9,1	10,1	5,6	6,1	9,6	8,9	.	2,2	6,5	2,0	1,1	1,1	0,6	7,6	7,5	.	.	1,3	3,6		159,1
44	Sobieszyn	5,7	6,7	12,1	12,5	6,3	6,6	0,2	3,6	2,4	11,2	3,6	3,7	7,7	1,6	9,1	10,2	.	.	0,7	5,5	1,2	1,4	0,5	0,4	5,3	9,0	0,4	.	0,9	4,1		132,6
45	Puławy	6,2	7,5	10,3	10,3	4,6	6,7	0,1	1,0	2,1	10,2	3,6	4,7	7,1	1,2	8,9	9,5	.	.	0,5	4,5	1,5	1,3	1,3	0,1	5,2	8,8	.	.	1,5	3,9		122,6
46	Chełm Lub.	3,2	9,4	10,9	12,1	9,2	6,6	.	1,3	4,5	11,2	5,7	7,4	8,6	1,5	9,8	10,5	6,5	0,1	6,3	5,7	3,9	0,1	1,2	.	6,2	8,4	.	.	1,4	1,4		153,1
47	Szczawno-Zdrój	3,6	8,8	11,2	9,8	2,5	4,0	2,8	1,3	3,2	11,0	0,9	6,6	2,4	6,4	8,2	6,6	.	.	0,1	5,3	0,9	0,2	.	0,9	6,1	9,1	3,7	3,4	0,4	8,1		127,5
48	Śnieżka	3,6	11,4	12,0	11,3	1,5	0,6	0,2	2,1	1,7	11,4	0,7	2,0	2,8	7,6	10,2	6,8	.	0,1	0,1	4,6	1,3	.	.	0,4	5,2	10,3	4,4	6,1	4,9	6,7		130,0
49	Opole	6,1	9,2	10,7	11,1	1,4	2,5	1,7	.	.	.	0,3	7,4	4,2	5,0	7,7	8,3	.	0,1	0,1	6,6	2,5	4,1	.	0,2	8,7	9,3	7,2	2,3	0,5	5,8		123,0
50	Kudowa-Zdrój	5,5	10,8	11,2	10,7	2,7	0,1	1,8	3,9	4,2	11,5	0,5	8,6	1,0	7,0	9,7	9,5	.	.	.	7,9	0,7	0,6	.	0,3	5,9	10,1	4,6	5,0	8,4	8,3		150,5
51	Polanica-Zdrój	3,7	10,5	10,7	10,8	1,7	1,0	3,2	3,7	4,3	11,3	2,2	9,8	1,1	7,2	9,9	9,1	.	0,1	.	9,2	3,4	1,2	0,1	0,6	4,8	9,1	3,0	2,2	4,1	7,0		145,0
52	Skroniów	1,1	7,4	7,5	10,8	4,4	2,6	.	0,4	2,5	10,8	3,5	7,2	4,1	0,8	7,3	9,6	.	0,1	1,2	7,8	3,4	2,6	0,1	1,8	7,2	10,1	2,0	.	0,8	7,5		124,6
53	Świerklaniec	2,4	7,9	10,6	10,7	1,4	2,8	.	2,3	5,1	10,2	1,8	6,1	3,1	5,7	7,6	9,8	.	.	2,5	7,8	3,1	3,7	.	1,6	7,4	10,0	3,7	1,6	0,8	3,0		132,7
54	Kraków, Obs.Astr.	5,0	8,8	11,0	11,1	5,8	2,5	.	1,7	3,4	10,5	5,0	8,0	0,9	7,0	9,2	10,7	0,3	.	6,5	8,8	3,0	4,5	.	3,4	5,0	9,2	3,0	.	2,3	7,3		153,9
55	Cieszyn	0,6	9,0	11,8	11,4	0,4	0,3	.	3,5	2,3	11,5	1,8	7,1	.	6,1	10,3	10,3	.	.	5,3	8,2	0,5	2,7	.	0,8	9,4	9,2	4,7	2,3	2,0	7,9		139,4
56	Istebna-Kubalonka	1,6	8,9	11,8	11,6	1,5	0,1	.	2,4	3,3	11,3	3,9	7,2	0,1	6,9	11,2	11,0	0,1	.	3,0	6,4	1,0	.	1,6	.	10,0	9,6	7,0	5,4	3,8	9,1		149,8
57	Babia	1,2	9,5	11,9	11,5	5,9	1,7	.	1,6	1,8	10,8	6,2	9,1	0,1	7,0	10,2	11,1	1,6	.	6,5	9,4	1,5	0,3	.	0,7	8,3	9,0	6,7	9,3	4,4	9,0		166,3
58	Jabłonka	1,9	6,6	10,5	10,2	6,2	.	0,1	2,2	3,9	4,7	4,0	8,7	0,4	7,7	8,0	10,5	0,7	.	6,8	7,2	1,1	.	0,3	3,1	3,7	6,4	5,4	4,0	6,2	4,7		135,2
59	Krynica	5,1	9,2	10,4	10,2	6,1	2,4	0,2	0,7	4,9	10,3	6,2	9,4	0,2	6,5	8,8	10,1	2,3	.	5,2	5,8	2,0	2,1	0,8	0,2	3,7	7,6	6,8	2,4	4,2	4,3		148,1
60	Krynica-Górn Park.	5,6	9,6	10,7	10,6	6,2	2,5	0,4	0,6	5,1	10,6	6,9	9,6	0,5	7,3	9,3	10,6	2,4	.	6,4	.	5,1	.	1,1	0,3	3,7	8,1	8,4	3,0	4,7	5,9		155,2
61	Muszyna	3,7	9,5	10,3	10,1	7,2	2,1	0,4	1,6	3,7	8,8	7,0	8,9	0,7	7,8	8,3	10,0	2,4	.	5,7	6,1	3,0	2,4	1,3	0,1	5,7	5,1	5,0	1,4	4,4	4,2		146,9
62	Zakopane	0,6	9,8	12,6	12,4	5,0	2,9	0,1	2,0	1,0	12,3	6,1	9,0	2,3	7,8	12,1	12,2	2,0	.	9,2	6,2	1,7	0,2	.	.	5,5	9,6	7,9	4,7	3,9	10,2		169,3
63	Gubałówka	0,2	8,7	9,6	9,4	5,3	3,1	.	1,6	1,7	9,6	6,0	7,3	2,8	5,6	9,6	9,6	1,7	.	8,6	7,6	2,2	0,2	.	.	5,8	8,0	7,0	4,5	4,2	8,4		148,3
64	Hala Gąsienicowa	.	10,3	10,8	10,7	6,0	3,1	0,1	1,1	0,1	10,1	5,6	6,1	1,2	6,0	9,6	9,9	0,5	.	6,4	3,7	1,0	.	.	0,1	5,9	8,7	6,8	4,1	3,1	5,2		136,2
65	Kasprowy Wierch	.	10,0	13,0	12,7	6,8	1,2	.	0,5	0,7	12,5	6,6	8,6	2,1	7,3	12,0	12,1	0,1	.	7,6	6,1	1,4	.	.	0,1	7,3	9,2	7,8	4,0	4,3	9,8		163,8
66	Werbkowice	3,4	10,1	10,6	11,3	10,2	2,8	.	2,2	3,1	10,7	5,9	6,7	6,7	0,8	8,7	10,9	7,1	.	4,9	8,4	5,2	0,4	0,2	.	3,1	7,3	.	.	3,9	2,9		147,5
67	Zdanów	5,9	8,4	12,0	11,7	7,4	2,0	.	0,9	4,3	10,5	5,0	7,8	5,9	5,4	8,5	10,4	0,5	.	3,8	6,0	2,8	1,6	0,1	0,1	6,1	10,6	0,8	.	0,6	5,8		144,9
68	Iwonicz - Zdrój	2,9	10,4	10,1	10,8	8,7	2,1	0,9	0,5	0,9	10,3	7,9	8,9	0,9	5,8	8,7	9,3	4,2	.	3,0	6,8	4,6	2,2	1,0	0,3	3,8	7,7	1,8	4,1	5,9	6,5		151,0
69	Lesko	3,5	10,1	11,9	11,5	9,7	1,2	1,5	1,2	1,3	11,4	7,7	9,5	4,5	5,1	8,4	10,5	7,2	.	2,1	7,1	5,4	0,9	0,5	.	7,3	8,8	.	3,5	6,0	8,0		165,4

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	0,7	8,3	8,6	5,8	.	.	2,1	7,9	6,4	7,3	5,4	6,6	9,2	0,5	9,3	0,9	.	.	5,7	8,7	.	.	.	.	.	6,2	6,7	1,0	3,3	2,7	.	113,3
2	Kołobrzeg	0,6	8,5	8,8	4,3	.	4,4	0,9	8,9	8,7	5,6	2,6	.	8,1	.	9,5	.	0,3	.	5,3	8,7	.	.	.	.	.	5,3	6,6	0,9	4,6	0,7	1,5	104,8
3	Międzyzdroje	.	9,4	9,4	2,1	.	4,6	5,9	9,2	7,4	5,6	2,5	.	9,3	.	5,4	.	1,0	.	5,8	6,7	.	.	.	.	.	1,6	5,0	0,2	5,9	0,1	.	97,1
4	Resko	1,2	8,3	8,7	1,2	.	5,9	0,7	3,5	6,4	7,5	3,2	0,8	6,5	.	7,7	.	.	.	4,8	7,6	1,7	.	.	.	.	4,6	4,6	0,7	4,1	.	.	89,7
5	Szczecinek	2,1	9,5	9,3	1,5	0,1	.	4,9	4,4	7,6	4,8	.	1,2	7,9	.	8,8	2,0	.	.	5,6	7,1	1,6	.	.	.	.	6,8	6,2	.	3,8	.	0,1	95,3
6	Chojnice	1,3	7,2	8,4	1,9	.	.	4,1	5,7	7,6	3,3	1,7	2,0	8,7	0,8	9,5	2,4	.	.	5,2	9,1	5,1	.	.	.	.	3,6	4,6	0,2	0,1	.	0,4	92,9
7	Hel	2,5	5,8	6,2	4,7	.	.	5,6	7,2	4,8	.	3,6	4,4	8,3	.	8,7	0,7	.	.	4,1	3,6	0,6	.	.	.	2,2	5,8	6,1	.	0,8	3,6	1,0	90,3
8	Gdynia	2,0	5,5	6,5	4,7	.	.	5,7	8,0	8,5	5,5	5,7	4,4	8,3	1,0	8,6	1,5	.	0,3	4,4	5,6	1,9	.	.	.	2,1	7,8	.	.	2,2	6,6	0,8	107,6
9	Świbno	2,9	5,7	7,6	4,2	.	.	5,2	8,2	3,2	.	1,4	4,7	7,1	0,6	8,4	2,7	.	.	4,8	3,8	.	.	.	.	.	3,0	5,4	0,1	0,8	1,4	3,0	86,2
10	Stare Pole	2,9	5,2	7,2	6,2	1,1	.	.	5,3	0,1	1,5	0,6	4,2	8,7	0,5	8,9	6,0	.	.	5,1	2,9	3,7	.	.	.	.	4,2	4,8	0,2	1,1	6,1	3,7	90,2
11	Radostowo	2,1	5,5	8,7	5,6	0,4	0,1	0,1	5,6	3,5	2,8	1,6	3,1	9,2	1,0	9,7	3,9	.	.	5,1	7,1	3,6	.	.	.	.	6,9	5,3	0,3	0,4	1,2	4,8	97,6
12	Prabuty	4,2	4,8	9,2	5,1	1,0	.	.	3,0	2,8	4,9	2,3	1,2	9,6	0,5	8,0	3,9	.	.	5,2	4,5	6,0	.	.	.	.	6,3	2,6	.	.	3,8	3,7	92,6
13	Bydgoszcz, IMiUZ	2,8	7,8	8,7	1,8	.	0,4	.	7,2	7,1	5,0	1,0	2,2	7,4	0,2	9,3	3,3	0,1	.	4,3	8,0	9,0	.	.	.	0,2	5,6	2,3	0,3	.	1,2	4,8	100,0
14	Suwałki	5,7	3,0	7,8	9,0	.	.	0,4	.	0,7	5,2	1,6	2,3	8,7	2,6	8,2	0,8	.	.	0,5	8,3	4,3	2,7	.	0,3	.	4,6	2,0	.	.	4,5	.	84,2
15	Mikołajki	3,0	5,5	7,5	7,9	.	.	1,0	2,5	5,0	6,5	9,0	1,8	7,3	3,2	8,8	3,1	.	.	5,1	3,6	5,6	0,1	.	4,0	0,1	7,3	1,0	.	.	4,0	.	102,9
16	Biebrza	.	0,5	9,1	7,8	0,4	0,1	0,1	0,3	2,8	4,9	5,9	1,8	7,7	3,0	8,8	1,7	.	.	4,7	8,2	7,3	0,3	.	3,0	.	3,9	2,4	.	.	2,2	.	86,9
17	Białystok	3,2	6,8	9,6	8,1	0,8	4,3	0,3	.	.	5,1	6,1	0,8	3,8	1,4	8,0	2,5	0,9	.	3,3	7,8	8,8	.	.	5,6	.	2,3	4,5	.	.	2,2	3,0	99,2
18	Gorzów Wlkp.	2,1	8,4	6,5	.	0,1	3,3	2,2	.	5,9	3,6	.	.	4,3	.	9,2	2,7	.	.	2,4	6,4	7,9	.	2,9	.	1,3	3,7	3,7	.	4,9	1,5	.	83,0
19	Przebędowo	4,3	9,0	8,2	.	0,7	0,1	.	0,4	6,5	2,2	.	0,6	6,2	.	9,0	3,1	.	.	3,2	7,5	8,2	.	3,0	4,2	2,0	5,4	1,7	0,9	.	3,5	1,8	91,7
20	Przybroda	3,3	9,1	7,9	0,1	2,3	.	.	.	7,7	0,5	.	.	7,4	0,1	9,1	2,3	.	.	4,6	5,8	8,5	.	3,9	3,6	4,3	7,3	1,3	1,0	0,5	6,0	0,6	97,0
21	Poznań-Ławica	3,9	8,2	6,7	0,3	2,1	.	0,1	.	6,8	0,2	.	.	6,8	0,3	8,8	3,3	.	.	4,1	6,6	8,1	.	4,1	4,8	4,7	6,7	1,0	0,9	0,1	6,9	2,3	97,8
22	Plewiska	3,2	8,9	7,1	0,4	1,6	.	0,1	.	6,2	0,1	.	.	6,4	0,2	8,6	2,4	.	.	3,3	6,3	9,0	.	3,1	5,2	4,7	6,0	0,7	0,7	.	5,8	1,1	91,1
23	Kórnik	6,4	9,5	8,6	0,9	0,2	.	.	.	4,5	.	.	0,4	6,0	0,1	9,3	4,0	.	0,3	3,0	6,3	9,1	0,5	3,8	6,8	4,4	6,3	.	.	.	5,6	5,6	101,6
24	Oborniki Śl.	8,3	8,3	7,6	0,9	0,2	.	2,6	3,5	2,9	.	2,0	0,8	1,0	.	1,1	5,4	1,6	1,2	3,2	5,6	7,8	6,6	6,3	5,9	5,3	3,9	.	.	.	.	5,0	97,0
25	Laskowice Oławskie	7,2	8,7	5,4	5,8	0,2	.	2,3	4,0	3,9	.	4,2	.	3,2	.	0,4	5,2	0,3	1,2	1,4	3,3	7,9	9,1	8,5	7,7	7,2	6,6	0,8	.	.	6,1	.	110,6
26	Ciechocinek	3,7	6,9	8,2	3,7	1,6	0,4	.	5,6	5,6	4,7	2,5	1,4	6,9	.	8,9	3,0	0,3	.	5,2	6,8	8,8	.	.	5,4	.	5,8	0,3	.	.	5,4	3,3	104,4
27	Więcławice	2,7	8,6	8,5	3,0	1,2	0,3	0,6	7,4	4,9	3,9	3,7	1,9	6,3	.	8,7	4,6	.	.	4,3	8,6	7,5	.	.	4,6	0,4	5,9	2,0	.	.	6,3	5,1	111,0
28	Legionowo	3,0	8,3	9,2	8,1	.	1,0	5,1	6,4	.	3,5	7,0	0,4	3,9	0,1	6,7	8,3	.	.	6,8	4,3	8,8	.	.	7,1	.	5,6	3,2	.	.	6,3	0,1	113,2
29	Warszawa-Bielany	2,6	8,6	9,1	8,5	0,2	1,5	3,4	4,6	.	3,1	7,2	0,7	4,5	0,1	6,3	9,5	.	.	6,2	5,1	9,4	.	.	7,6	0,4	6,6	3,4	.	0,2	5,7	0,1	114,6
30	Warszawa, Min. Kom.	2,0	8,5	9,2	8,0	0,5	1,0	4,0	7,2	1,1	3,3	7,9	0,1	5,9	0,1	6,2	8,7	.	4,1	6,0	.	8,3	.	.	6,4	.	4,5	2,3	.	.	3,7	.	109,0
31	Międzylesie	1,6	9,4	9,5	8,9	2,4	0,5	4,7	4,4	.	4,2	6,7	0,6	3,6	.	6,9	8,0	.	.	6,3	4,8	7,2	.	.	6,3	1,6	5,6	4,1	.	.	5,5	.	112,8
32	Brwinów	4,1	7,4	8,2	8,4	.	1,1	5,1	3,5	.	3,3	8,8	0,1	9,4	.	6,0	10,2	.	.	5,8	3,0	9,4	.	.	8,1	1,6	7,1	3,5	.	.	4,8	.	118,9
33	Świder	1,0	8,4	8,9	8,5	1,9	0,6	3,9	3,0	.	3,4	6,1	0,7	4,5	.	5,9	7,7	.	.	6,4	3,5	7,7	.	.	6,5	2,8	4,8	3,7	0,1	.	4,7	0,1	104,8
34	Topola-Ełonie	7,9	7,7	8,8	7,2	3,3	1,2	2,6	3,8	4,0	4,1	7,0	0,8	6,9	.	7,9	6,5	.	.	2,7	6,5	8,3	.	.	6,8	3,3	6,9	.	.	.	4,9	.	119,1
35	Włochów	0,5	7,2	8,1	9,4	0,5	1,6	3,3	2,2	.	3,6	8,2	0,6	8,2	.	6,8	9,5	.	.	5,8	2,8	9,1	.	.	7,7	1,1	6,2	4,1	.	0,2	6,2	0,1	113,0
36	Skierniewice	9,0	7,8	8,3	8,4	1,8	2,6	6,1	4,0	5,2	3,1	6,8	0,4	8,0	.	7,2	8,5	0,3	.	3,1	5,4	8,8	.	.	7,7	2,8	7,4	3,4	.	.	6,4	.	132,5
37	Belsk	.	6,4	7,5	8,0	2,3	1,5	2,8	4,4	7,3	3,1	7,5	.	6,4	.	5,9	8,6	0,4	.	6,5	3,5	8,7	.	.	6,0	0,3	5,1	4,0	.	.	3,8	0,3	110,3
38	Łódź-Lublinek	9,2	9,8	9,6	7,8	2,0	.	2,8	4,1	3,2	4,3	8,6	0,3	7,2	.	8,2	7,0	.	.	1,5	4,7	8,6	3,9	1,2	7,0	4,6	7,3	2,6	.	.	3,6	0,1	129,2
39	Kalisz	6,1	8,3	7,5	4,7	0,1	0,7	3,5	2,5	1,4	1,1	4,9	0,3	7,8	0,2	8,6	7,0	.	0,7	1,7	4,6	9,4	5,8	4,2	8,0	6,1	7,2	0,3	.	.	5,6	3,2	121,5
40	Wieluń	9,5	8,6	7,7	5,7	0,2	.	3,6	4,8	4,3	3,1	7,4	.	9,0	.	6,0	8,8	0,1	.	3,3	3,9	9,3	9,1	8,2	8,5	6,9	8,1	3,2	.	.	5,6	.	144,9
41	Szepietowo	2,0	6,2	7,3	9,6	0,8	3,4	1,7	1,5	.	4,5	7,8	0,2	6,4	2,8	4,5	8,5	.	.	5,5	6,0	8,8	0,1	.	5,8	4,4	1,8	.	0,6	.	2,3	.	102,5
42	Białowieża	3,1	8,9	10,1	9,1	0,9	7,1	6,2	.	.	5,2	6,9	0,4	2,9	0,4	7,1	5,1	0,1	.	2,7	4,7	8,7	0,4	.	5,0	1,4	1,9	7,0	0,2	.	0,3	.	105,8
43	Terespol	8,1	9,2	10,0	9,2	1,6	8,3	4,6	0,1	.	2,8	6,7	0,4	4,6	1,8	8,6	8,8	1,1	.	5,9	5,3	8,1	.	.	4,0	.	4,7	7,9	0,5	.	.	.	122,3
44	Sobieszyn	2,1	8,0	5,7	6,3	2,3	2,6	4,7	2,2	.	3,3	6,4	0,1	5,3	0,2	5,8	8,9	1,4	.	5,6	4,8	8,6	.	.	6,1	.	4,1	8,0	0,2	.	1,9	0,1	104,7
45	Puławy	2,4	8,6	7,4	8,8	4,5	1,3	5,3	1,1	.	2,9	8,1	.	6,2	0,3	5,0	8,1	1,6	.	4,5	2,4	8,4	0,4	.	5,1	1,2	6,2	6,6	0,2	.	0,2	.	106,8
46	Chełm Lub.	6,5	9,7	5,2	7,6	1,6	7,8	8,9	.	2,7	5,0	8,4	2,6	4,7	2,0	6,0	6,6	5,6	.	3,8	3,9	9,1	.	.	5,8	.	4,5	8,0	4,3	1,5	0,3	.	132,1
47	Szczawno-Zdrój	7,3	8,6	8,4	7,2	.	.	0,8	5,7	9,2	8,6	8,9	.	0,1	.	1,1	3,5	2,7	5,8	0,6	2,4	8,7	7,5	8,5	7,5	7,0	7,7	.	.	.	7,8	2,5	138,1
48	Śnieżka	10,5	10,6	10,0	7,2	0,4	.	0,3	9,9	10,2	9,2	10,1	10,0	7,2	3,1	.	5,6	1,6	8,8	0,4	0,1	10,0	10,0	9,7	9,7	7,8	6,4	.	0,1	.	8,8	2,7	180,4
49	Opole	8,1	8,0	6,2	5,0	.	.	3,6	5,0	5,2	1,6	5,0	.	.	.	.	5,3	0,9	1,4	4,7	2,8	7,0	6,0	7,0	7,4	.	7,1	2,6	.	.	.	.	99,9
50	Kudowa-Zdrój	9,4	8,8	9,2	7,4	0,3	0,1	6,9	9,1	9,6	9,7	9,2	8,3	8,7	2,9	.	.	2,6	0,3	2,6	1,2	7,5	7,7	7,5	6,4	4,9	6,0	1,2	.	.	2,5	0,1	150,1
51	Polanica-Zdrój	9,3	7,7	8,9	8,5	0,7	.	2,5	0,1	5,2	5,8	8,1	.	.	.	0,1	.	.	4,6	1,7	1,2	8,2	7,2	7,6	7,5	4,0	6,8	1,4	.	.	2,6	.	109,7
52	Skromiów	6,2	4,0	1,6	.	.	.	7,9	5,2	7,7	4,5	4,9	0,3	4,8	1,0	4,0	0,6	0,9	.	2,0	4,2	9,7	7,8	7,4	7,9	4,9	4,4	6,5	0,5	.	0,1	.	109,0
53	Świerklaniec	7,1	7,8	6,2	3,0	.	.	6,9	6,7	4,9	3,6	5,5	.	3,2	.	1,1	4,6	0,2	.	2,3	1,4	8,5	5,4	7,2	8,1	3,0	4,3	5,9	0,8	.	.	.	107,7
54	Kraków, Obs. Astr.	5,1	4,1	.	.	.	.	7,2	0,3	5,3	3,9	5,0	8,1	.	0,7	.	3,7	1,2	0,2	.	4,0	8,9	7,8	8,0	7,7	5,5	4,0	6,1	0,5	.	.	.	99,3
55	Cieszyn	7,8	8,8	8,7	9,1	.	.	2,5	0,8	4,3	.	8,7	4,0	0,2	0,1	.	4,0	1,6	1,7	.	0,2	4,9	8,2	8,3	8,2	6,7	2,2	3,9	0,3	.	.	.	105,2
56	Istebna-Kubalonka	10,2	10,2	9,8	10,0	.	.	7,0	10,0	10,1	10,1	9,3	9,0	8,7	0,3	.	3,8	2,4	0,1	.	.	6,1	9,3	9,4	9,2	8,7	1,4	5,8	1,8	.	0,3	.	163,2
57	Rabka	9,5	9,6	9,6	9,1	4,6	.	3,1	6,0	9,7	9,7	9,4	8,8	6,1	0,1	0,1	4,7	5,6	2,0	.	0,1	6,8	9,0	8,9	8,7	6,3	7,5	7,1	3,2	.	.	1,8	167,1
58	Jabłonka	6,4	6,7	5,7	6,8	3,9	.	2,8	5,6	5,0	6,6	8,3	7,0	4,4	0,1	0,2	4,8	4,2	1,6	0,5	.	7,6	6,8	4,1	6,6	2,4	4,4	6,6	2,2	0,7	.	1,3	123,3
59	Krynica	8,4	8,8	7,2	8,7	5,3	3,0	4,0	9,2	6,6	8,2	9,1	7,6	5,0	0,3	0,5	4,6	5,0	2,4	0,4	1,3	8,4	7,9	8,0	7,4	7,0	5,6	8,3	5,9	1,1	.	0,1	165,3
60	Krynica-Góra Park	9,4	8,2	9,3	8,9	6,0	3,5	4,6	9,0	6,8	9,3	8,9	7,1	4,8	0,4	0,8	6,9	6,3	2,8	.	1,7	8,7	9,0	9,0	8,6	8,1	7,1	7,9	5,3	2,0	.	.	180,4
61	Muszyna	6,6	7,3	6,5	6,3	5,1	1,4	1,8	6,5	6,0	6,9	7,9	6,2	4,7	0,2	0,6	1,6	4,0	2,9	0,6	1,1	8,1	7,7	7,5	6,5	8,0	4,9	4,8	3,1	2,8	.	8,5	146,1
62	Zakopane	11,1	11,0	10,8	10,8	5,0	.	0,2	10,5	10,0	10,5	10,4	9,8	9,2	0,2	0,2	1,5	5,9	5,7	0,4	.	6,9	9,1	9,1	8,9	8,6	7,6	7,3	3,8	0,6	.	3,5	188,6
63	Gubałówka	8,5	8,8	8,9	8,7	5,5	.	.	8,8	8,9	8,9	8,9	8,8	7,8	0,3	0,1	1,4	4,9	6,2	0,3	.	5,4	8,0	7,9	7,9	7,7	7,0	6,7	4,5	1,1	.	3,0	164,9
64	Hala Gąsienicowa	8,9	8,0	8,8	8,6	5,2	.	0,3	8,5	8,5	8,4	8,1	7,8	7,8	.	.	2,6	5,3	7,2	1,4	.	7,3	7,2	7,1	7,0	7,0	6,6	6,0	4,9	2,1	0,6	.	161,2
65	Kasprowy Wierch	11,0	11,0	11,0	10,7	5,0	.	0,3	10,7	9,9	10,4	10,5	10,3	10,3	0,2	0,1	2,7	9,9	9,8	2,6	.	9,9	9,8	9,8	9,7	9,7	8,9	7,7	5,1	1,6	0,6	.	209,4
66	Wezbkowice	4,3	8,0	4,4	7,3	2,3	6,7	7,1	.	0,9	4,6	6,9	6,2	2,4	1,6	6,1	8,6	5,8	.	3,1	2,5	8,2	1,8	4,2	6,1	6,6	4,7	8,4	5,2	1,5	0,1	.	135,6
67	Zdanów	4,6	8,5	4,2	9,6	2,9	2,1	6,2	1,0	3,6	0,4	9,5	2,6	5,8	2,6	4,7	10,2	3,3	.	3,0	4,7	9,6	9,6	7,3	6,5	3,1	2,5	7,6	1,2	.	.	.	136,9
68	Iwonicz-Zdrój	3,9	6,2	9,0	6,8	.	1,2	2,8	4,4	5,3	4,2	8,1	8,1	1,4	1,3	.	7,7	6,9	1,6	0,2	2,2	7,9	7,7	7,9	7,7	6,4	7,7	7,7	5,5	.	.	1,2	141,0
69	Zakopane	5,7	8,4	9,3	8,2	.	1,2	5,5	7,2	6,1	6,8	8,7	8,6	4,1	0,4	.	7,2	8,6	1,4	0,1	1,1	7,7	8,7	8,7	8,0	8,0	8,7	8,3	6,3	0,8	0,2	0,7	164,7

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	.	.	.	3,5	3,7	7,0	4,9	5,5	6,5	4,5	.	.	.	.	0,3	2,6	0,7	1,4	.	.	0,5	.	1,4	2,1	.	.	.	0,8	.	.		43,4
2	Kołobrzeg	.	.	.	5,9	4,9	6,3	3,7	7,3	7,4	3,2	.	.	.	.	0,6	5,4	1,3	2,7	.	.	0,3	.	0,8	2,0	.	.	.	0,7	.	.		52,5
3	Międzyzdroje	.	.	0,1	5,6	4,1	5,5	1,3	7,2	6,3	2,6	0,1	.	.	.	.	3,4	0,3	3,1	.	0,1	.	.	.	.	0,1	0,4	.	.				40,4
4	Resko	.	.	.	5,4	4,0	4,5	3,6	6,1	5,1	3,7	.	.	.	1,4	.	4,0	0,1	0,6	.	.	.	.	.	0,2	.	.	.	0,3	.	0,1		39,1
5	Szczecinek	.	.	.	1,5	4,0	4,5	2,8	6,7	6,1	2,2	.	.	.	.	.	3,4	.	0,2	.	.	0,3	.	.	.	.	.	.	.	.	0,1		34,8
6	Chojnice	.	.	.	2,9	3,1	5,6	5,1	7,2	6,7	.	.	.	.	.	.	3,0	.	.	.	.	2,3	.	.	.	.	.	.	.	.	0,1		36,0
7	Hel	.	.	.	1,7	.	7,0	1,6	6,6	0,3	1,1	.	.	.	.	0,6	5,2	5,2	.	.	.	1,5	.	.	4,6	.	0,4	.	0,1	0,2	0,1		36,2
8	Gdynia	.	.	.	1,9	.	7,3	2,4	7,1	0,6	0,3	.	.	.	.	1,8	4,7	4,8	.	0,1	.	3,6	0,7	.	5,6	0,1	2,3	.	.	0,1	0,1		43,5
9	Świnoujście	.	.	.	1,5	.	6,7	1,1	6,6	5,5	3,2	.	.	.	.	0,5	3,3	3,3	.	.	.	0,7	0,5	0,8	3,9	.	3,4	.	.	0,2	0,4		44,6
10	Stare Pole	.	.	.	2,9	0,4	7,2	0,7	7,2	4,5	0,1	.	.	.	.	0,1	1,4	2,2	0,1	.	.	1,4	2,1	0,6	3,3	.	1,8	.	.	0,7	.		36,7
11	Radostowo	.	.	.	3,0	.	7,4	1,8	7,4	5,9	.	.	.	.	.	0,1	2,3	3,6	.	.	.	.	.	0,2	.	.	2,2	.	.	0,8	.		34,7
12	Przebuty	.	.	.	3,2	0,1	7,0	0,3	7,3	6,9	0,1	.	.	.	.	.	1,6	2,8	.	.	.	.	0,9	0,5	.	.	.	.	.	1,0	.		31,7
13	Bydgoszcz,IMiUZ	.	.	0,7	4,7	4,5	4,7	4,0	7,2	2,9	.	.	.	.	.	.	2,9	.	1,3	.	.	.	.	.	.	.	.	.	0,1	.	0,3		33,3
14	Suwałki	0,9	.	.	.	6,5	8,0	7,6	8,0	0,8	0,2	.	.	.	.	.	.	.	0,1	.	.	.	.	.	.	.	6,2	.	.	.	1,1		39,4
15	Mikołajki	.	.	.	.	3,1	7,7	4,7	0,1	0,9	.	.	.	.	.	.	.	5,0	0,2	0,1	.	0,3	.	.	.	0,9	3,8	.	.	0,6	0,7		28,1
16	Biebrza	1,4	.	.	.	5,6	7,7	6,8	7,7	4,3	.	.	.	.	.	.	.	0,9	.	1,1	.	.	.	.	0,2	.	5,0	.	.	.	1,5		42,2
17	Białystok	.	.	.	.	7,9	8,1	7,1	8,0	5,0	.	.	.	.	.	.	.	0,1	.	3,5	.	.	.	.	.	.	.	.	.	.	0,3		40,0
18	Goraów Wlkp.	.	.	.	.	6,4	3,0	0,8	6,5	0,7	.	.	.	.	.	0,2	2,4	0,1	5,0	.	.	4,1	.	.	.	.	.	.	1,9	.	0,5		31,6
19	Przebędowo	.	.	.	2,3	6,3	3,0	3,0	6,7	3,6	.	.	0,8	.	.	.	.	.	3,1	.	.	3,6	.	.	.	.	0,1	.	.	.	0,8		33,3
20	Przybroda	.	.	.	4,3	7,4	2,4	2,0	6,9	3,3	.	.	.	.	.	0,1	1,2	0,4	2,6	0,5	.	4,4	.	.	.	.	.	.	0,1	.	0,5		36,1
21	Poznań-Lawica	.	.	.	4,7	6,7	2,3	0,7	6,5	2,4	.	.	.	.	.	.	1,7	0,2	1,9	0,3	.	4,4	.	.	.	.	.	.	.	.	0,9		32,7
22	Piławiska	.	.	.	5,6	7,7	2,1	0,3	7,1	2,7	.	.	.	.	.	.	1,0	.	2,3	0,6	.	4,4	.	.	.	.	.	.	.	.	0,3		34,1
23	Kórnik	.	.	.	6,2	7,6	2,4	1,2	7,3	2,1	.	.	.	.	.	.	1,6	0,2	2,6	2,0	.	4,6	.	0,1	.	.	.	.	.	.	1,2		39,1
24	Oborniki Śl.	.	4,7	4,2	5,7	6,4	0,4	0,3	4,5	.	.	.	.	0,7	.	.	.	2,1	.	2,3	.	2,8	.	2,5	.	.	.	.	.	.	.		36,6
25	Laskowice Oleszkie	.	.	3,3	5,3	7,7	.	0,3	6,4	.	.	.	.	.	.	.	0,9	3,2	2,1	4,6	.	4,9	.	1,0	.	.	.	.	.	.	.		39,7
26	Ciechocinek	.	.	0,3	4,3	3,1	4,5	1,6	7,3	1,9	.	.	.	.	.	.	0,9	0,6	1,4	0,7	.	.	.	.	.	.	.	.	.	0,9	0,5		28,0
27	Więcławice	.	.	.	4,5	4,7	.	4,3	7,5	4,0	.	.	.	.	.	.	1,9	.	1,9	.	.	0,8	.	.	.	.	.	.	.	.	0,6		30,2
28	Legionowo	0,2	.	0,2	.	0,6	5,7	.	6,3	.	.	.	.	.	.	.	.	.	0,7	1,9	.	0,3	.	0,1	.	.	0,9	.	.	0,3	.		17,2
29	Warszawa-Bielany	0,3	.	0,2	.	1,8	5,9	0,6	7,0	.	.	.	.	.	.	.	0,1	0,1	1,5	3,8	.	0,3	0,1	0,6	.	0,1	0,1	.	.	0,9	0,4		23,8
30	Warszawa,Min.Kom.	0,2	.	0,1	.	1,3	8,8	0,2	6,1	.	0,1	.	.	.	.	.	.	.	0,8	2,5	.	.	.	.	.	.	.	.	.	.	.		16,1
31	Międzylesie	1,0	.	0,7	.	3,9	5,3	1,9	5,7	.	.	.	.	.	.	.	.	.	1,6	3,4	.	.	0,1	0,1	.	.	.	.	.	0,2	0,8		24,7
32	Erwinów	.	.	.	.	1,7	5,2	.	7,7	.	.	.	.	.	.	.	.	.	1,8	3,1	.	.	.	.	.	0,1	.	.	.	1,0	0,7		21,3
33	Świder	1,1	.	0,8	.	3,5	5,4	2,0	5,7	.	.	.	.	.	.	.	0,3	.	1,7	2,2	.	.	.	0,1	.	.	.	.	.	0,2	0,9		23,9
34	Topola-Błonie	0,1	.	0,2	4,5	6,0	3,1	2,7	7,3	1,1	.	.	.	.	.	.	0,3	0,2	.	2,1	.	1,9	.	0,2	.	0,4	3,7	.	.	1,9	1,2		36,9
35	Włochów	.	.	.	.	1,6	4,8	.	7,5	.	.	.	.	.	.	.	.	.	1,8	3,2	.	.	.	.	.	.	.	.	.	.	0,5	0,4		19,8
36	Skierniewice	.	.	0,2	.	3,4	4,3	1,7	7,9	2,4	.	.	.	.	.	.	0,1	.	1,3	2,5	.	0,9	.	.	.	0,2	0,2	.	.	2,4	0,1		27,6
37	Relsk	.	.	0,1	.	2,5	4,2	0,1	7,1	0,1	.	.	.	.	.	.	0,2	0,1	1,8	2,6	.	.	.	.	.	.	.	.	.	2,3	1,0		22,1
38	Łódź-Lublinek	.	.	.	2,1	4,4	3,0	2,2	6,8	4,5	.	.	.	.	.	.	.	0,2	.	3,1	.	.	.	0,1	.	.	3,8	.	.	.	0,1		30,3
39	Kalisz	.	.	1,8	4,3	7,5	2,1	3,0	7,6	3,9	.	.	.	.	.	.	0,4	1,0	1,2	1,4	.	.	.	0,7	.	.	.	.	.	.	1,1		36,0
40	Wieluń	.	.	3,9	3,3	7,0	1,0	1,8	7,7	3,7	.	.	.	.	.	.	0,4	2,3	.	3,4	.	.	0,3	0,1	.	.	0,3	.	.	.	.		35,2
41	Szepietowo	3,1	.	.	.	6,3	7,7	6,0	7,5	0,1	.	.	.	.	.	.	.	0,2	0,5	4,9	.	.	.	.	.	.	.	.	.	.	.		36,3
42	Białowieża	4,0	.	.	.	7,7	7,9	7,6	7,6	2,3	.	.	.	.	.	.	.	.	.	2,0	.	.	.	.	.	.	.	.	.	.	0,1		39,2
43	Terespol	4,6	0,2	.	.	8,0	7,8	7,4	6,7	.	.	.	.	.	.	.	.	.	0,2	3,3	.	.	.	.	.	.	.	.	.	.	.		38,2
44	Sobieszyn	2,1	1,1	.	.	4,3	6,5	4,4	5,4	.	.	.	.	.	.	.	.	.	2,6	4,2	.	.	.	.	.	.	.	.	.	.	.		30,6
45	Puławy	1,4	.	.	.	3,7	5,7	2,3	5,3	.	.	.	.	.	.	.	.	1,7	3,5	3,4	.	.	.	.	.	.	.	.	.	.	.		27,0
46	Chełm Lub.	4,1	0,9	.	.	8,0	7,6	4,4	5,1	1,8	.	.	.	.	.	1,1	.	.	1,4	1,0	.	.	0,1	.	.	.	.	.	.	.	.		35,5
47	Szczawno-Zdrój	.	0,5	3,0	6,9	6,1	0,4	2,7	4,4	.	.	.	.	.	.	.	0,8	1,3	2,2	1,3	.	1,8	.	5,1	.	.	.	.	.	0,5	.		37,0
48	Śnieżka	.	5,8	7,6	5,5	0,5	.	4,1	.	.	.	0,5	.	.	.	.	0,2	0,9	.	0,7	.	3,6	.	5,9	6,7	4,6	0,1	.	7,3	1,1	.		55,1
49	Opole	.	0,6	3,7	5,6	7,4	0,8	1,5	6,0	.	.	.	.	.	.	.	2,1	3,5	.	3,7	.	.	1,6	.	.	.	0,2	.	.	.	.		36,7
50	Kudowa-Zdrój	.	.	0,6	5,1	7,4	.	1,2	3,7	.	.	.	1,0	.	.	.	.	2,6	2,2	.	.	3,5	0,1	1,5	.	.	.	.	.	.	.		28,9
51	Polanica-Zdrój	.	.	4,5	6,9	3,3	0,5	3,1	3,3	.	.	.	.	.	.	.	4,6	2,8	.	2,7	.	1,5	.	4,2	.	.	.	.	.	.	.		37,4
52	Skroniów	0,3	.	.	2,8	6,7	0,2	4,2	6,8	4,6	.	.	.	.	.	.	.	2,6	2,4	3,3	.	.	.	.	.	.	.	.	.	.	.		33,9
53	Świerklaniec	.	.	.	2,9	6,3	.	4,4	5,9	3,1	.	.	.	.	.	.	0,2	0,1	0,6	3,2	.	0,6	.	.	.	.	.	.	0,1	.	.		27,4
54	Kraków,Obs.Astr.	.	.	2,2	3,7	6,5	2,8	4,8	6,8	1,8	.	.	.	0,1	.	.	.	4,3	3,3	2,5	.	.	0,2	.	.	.	.	.	0,9	.	.		39,9
55	Cieszyn	.	.	2,2	7,1	5,0	.	3,9	3,4	0,4	.	.	.	.	.	.	.	4,3	0,9	2,3	.	.	.	.	.	.	.	.	.	0,1	.		29,6
56	Istebna-Kubalonka	.	.	6,2	8,3	8,0	.	6,7	6,2	2,1	.	.	.	0,2	.	.	.	3,7	2,4	2,2	0,2	.	0,3	.	.	.	.	.	.	.	.		46,5
57	Rabka	.	.	4,3	7,2	8,2	0,1	7,7	7,1	2,9	.	.	.	2,9	.	.	.	5,1	4,4	2,3	.	.	2,8	.	.	.	.	.	.	.	.		55,0
58	Jabłonka	.	.	2,3	4,1	6,8	0,2	6,7	5,6	2,6	.	.	.	2,1	.	.	.	4,8	2,4	2,4	.	.	1,3	.	.	.	.	.	.	.	.		41,3
59	Krynica	0,5	3,1	6,3	3,9	6,4	0,6	6,5	7,9	1,7	.	.	.	.	.	0,2	.	3,7	0,8	0,3	.	.	1,9	.	.	.	.	.	0,1	.	.		43,9
60	Krynica-Góra Park.	0,9	3,1	7,0	.	4,1	.	6,8	6,7	1,3	.	.	.	.	0,2	.	1,6	1,2	1,7	1,2	.	.	.	.	.	.	.	.	.	2,8	.		38,6
61	Muszyna	.	0,4	3,1	5,2	5,9	6,7	0,1	6,6	7,2	.	0,8	.	.	.	0,5	.	4,1	1,8	0,5	.	.	2,8	.	.	.	.	.	.	.	.		45,3
62	Zakopane	.	1,0	4,2	7,9	8,1	0,6	6,8	6,8	2,1	.	.	.	1,1	.	0,2	.	5,3	3,7	1,2	.	.	3,5	.	.	.	.	.	0,1	.	.		52,6
63	Gubałówka	.	1,3	2,5	7,6	7,5	0,6	6,8	6,4	2,6	.	.	.	0,4	0,1	0,2	.	5,2	3,7	1,5	.	.	2,8	.	.	.	.	.	.	.	.		49,2
64	Hala Gąsienicowa	.	4,6	1,3	5,7	5,7	.	3,0	5,4	2,7	.	0,1	.	.	0,1	.	.	3,2	0,3	0,9	.	0,1	3,4	.	.	.	.	4,9	4,9	3,0	.		49,3
65	Kasprowy Wierch	.	5,4	1,2	7,6	7,3	.	0,1	4,1	1,7	.	.	.	.	.	.	.	2,5	0,5	1,2	.	4,5	1,8	.	.	0,2	.	7,7	7,8	7,2	.		60,8
66	Werbkowice	5,5	0,2	.	.	7,4	8,1	3,9	8,2	4,6	.	.	.	.	.	3,3	.	1,1	2,1	0,5	0,7	.	1,6	0,2	.	.	.	.	.	.	.		47,4
67	Zdanów	0,3	0,1	.	1,9	4,3	4,8	.	8,0	5,0	.	.	.	.	.	0,3	.	3,9	4,6	2,8	.	.	1,5	.	.	.	.	.	0,9	.	.		38,4
68	Kasinica-Zdrój	1,6	0,9	3,0	8,8	2,4	3,5	0,3	6,2	0,2	.	.	.	.	.	0,4	.	4,4	3,2	1,0	.	.	1,4	.	.	.	.	.	3,3	.	.		32,6
69	Lesko	2,2	0,2	4,6	7,4	8,0	5,2	.	6,7	0,4	.	.	0,3	1,4	.	.	.	4,6	1,2	1,9	2,1	.	0,7	.	.	.	.	.	1,9	.	.		48,8

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka																																brak
2	Kołobrzeg	4,6	4,8	2,9	5,5	.	.	.	.	.	.	0,2	.	.	0,1	0,1	.	0,2	3,5	0,3	2,5	5,8	5,6	5,8	2,0	.	0,1	.	.	.	0,7	1,0	45,7
3	Międzyzdroje	6,6	3,8	2,8	4,3	.	.	1,6	.	.	.	.	.	.	.	0,3	.	.	2,8	.	.	3,0	3,8	4,3	.	.	2,7	.	0,2	.	.	0,4	36,6
3	Resko	2,7	.	.	4,1	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	4,1	4,6	2,5	3,2	2,2	1,5	.	.	.	.	.	0,8	25,7
5	Szczecinek	5,2	0,8	2,8	4,4	.	.	4,8	0,9	.	.	.	.	.	0,1	.	.	.	.	.	.	4,8	5,1	5,3	0,4	.	.	.	.	.	0,3	.	34,9
6	Chojnice	6,2	1,2	1,5	5,0	.	.	4,5	.	.	.	.	.	.	.	.	.	.	.	.	.	0,2	.	4,7	.	.	.	.	.	.	.	.	23,3
7	Hel	2,8	3,0	3,7	1,4	.	.	5,4	2,7	.	.	1,5	.	.	.	.	.	.	.	.	2,7	4,0	2,0	5,8	.	2,4	.	.	.	.	1,0	0,7	39,1
8	Gdynia	4,5	3,3	4,0	2,3	.	0,1	5,9	3,0	.	.	1,8	.	.	0,1	.	.	.	.	.	3,2	4,4	.	4,0	1,9	1,0	.	0,2	0,2	.	0,7	0,2	40,8
9	Świnoujście	2,1	.	3,9	0,9	.	.	3,8	1,4	.	.	1,7	.	.	.	.	.	.	.	.	2,6	3,4	.	3,6	.	2,6	.	.	.	.	.	1,9	27,9
10	Stare Pole	1,0	2,6	3,9	0,7	.	.	5,8	.	0,2	.	0,7	.	.	0,3	.	.	.	.	0,4	3,9	5,6	5,1	5,2	.	0,7	.	0,2	.	.	1,5	3,3	41,1
11	Radostowo	2,5	3,6	2,8	1,8	.	.	6,2	.	0,1	.	1,5	.	.	.	.	.	0,2	.	0,1	3,6	3,8	4,0	4,8	.	1,1	1,7	0,4	.	.	0,7	2,0	40,9
12	Prabuty	0,6	3,3	3,2	2,9	.	.	4,8	.	.	.	1,4	.	.	.	.	.	.	.	.	5,7	3,0	3,1	6,1	.	1,6	.	1,6	.	.	2,0	0,2	39,5
13	Bydgoszcz, IMiUS	6,0	3,2	0,1	6,2	.	.	0,2	.	.	.	0,2	.	.	0,5	.	.	.	0,6	.	.	0,7	.	5,0	2,5	0,1	.	.	.	0,1	.	.	25,4
14	Suwałki	5,5	4,3	.	.	.	.	5,1	.	0,4	.	1,0	.	.	.	0,2	0,1	.	0,6	.	0,2	5,3	5,0	6,4	2,1	0,2	.	0,8	.	.	0,1	1,6	38,9
15	Mikołajki	2,9	5,9	2,2	.	0,1	.	5,8	.	0,2	.	0,6	.	.	.	.	.	.	.	.	1,6	2,3	5,0	5,2	1,2	1,6	.	.	.	.	.	.	34,6
16	Biebrza	3,2	4,9	0,9	.	.	.	5,0	.	.	.	0,2	.	.	.	0,8	.	.	.	.	2,9	0,7	0,8	6,3	0,1	2,3	0,2	.	.	.	.	.	28,3
17	Białystok	2,8	5,6	2,2	.	.	.	2,7	.	0,5	.	.	.	.	.	1,1	.	.	.	.	1,5	.	.	5,2	.	.	0,4	.	.	.	.	.	22,0
18	Gorzów Wlkp.	6,9	.	0,2	1,6	.	.	.	.	.	.	.	.	.	.	.	.	.	.	1,7	3,0	2,7	4,8	4,1	2,4	.	.	.	.	1,2	.	.	28,6
19	Przebędowo	4,8	.	1,0	3,7	.	.	.	.	.	.	.	.	.	0,6	.	.	.	.	.	.	.	3,5	2,3	2,5	.	.	.	.	0,8	.	.	19,2
20	Przybroda	4,5	.	1,6	5,5	.	.	0,9	.	.	.	.	.	.	1,2	.	.	0,1	.	.	1,0	5,5	3,4	4,6	4,7	.	0,2	1,9	.	1,4	.	.	36,5
21	Poznań-Zawica	4,3	.	3,2	4,3	.	.	1,8	0,7	.	.	.	0,1	.	1,0	.	.	.	.	.	0,1	4,4	3,2	2,6	4,2	0,1	0,1	0,2	.	.	.	.	30,3
22	Plewiska	5,9	3,2	3,7	.	.	.	.	0,7	.	.	.	.	.	0,8	.	.	.	.	.	.	4,2	1,4	1,0	5,1	.	.	.	.	0,7	.	.	26,7
23	Kórnik	6,5	.	3,1	2,8	.	.	.	0,7	.	0,2	.	.	.	0,2	.	.	.	.	.	.	2,9	0,9	2,0	1,7	.	.	.	.	0,2	.	.	21,2
24	Oborniki Śl.	.	.	2,9	3,9	.	.	3,5	2,1	1,0	.	.	.	.	0,7	.	.	.	.	.	.	1,5	.	.	.	1,7	.	.	.	.	.	.	17,3
25	Laskowice Oławskie	1,5	1,0	3,6	4,3	.	2,9	5,0	3,4	0,7	.	0,5	.	0,2	1,1	.	.	.	.	.	.	2,5	.	0,6	0,8	.	.	.	.	0,2	.	.	28,3
26	Ciechocinek	4,4	3,0	0,2	3,9	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0,3	1,2	.	3,8	0,8	0,2	.	.	.	.	.	2,2	20,0
27	Więcławice	5,5	3,2	.	5,7	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	4,0	.	.	.	.	.	1,0	.	.	19,4
28	Legionowo	2,6	4,6	1,8	3,0	.	.	.	.	.	.	0,1	.	.	.	.	0,2	.	.	.	5,1	3,2	3,7	4,9	0,4	0,3	.	.	.	.	.	.	30,1
29	Warszawa-Bielany	3,2	5,1	2,5	3,0	.	.	.	.	0,2	0,7	.	.	.	.	.	.	.	.	.	3,7	5,6	2,9	4,7	0,9	1,1	.	.	0,1	0,4	.	.	34,1
30	Warszawa, Min. Kom.	2,6	3,9	0,4	1,7	.	.	.	.	0,2	0,1	.	.	.	.	.	.	.	.	.	1,2	0,7	0,1	1,9	.	0,4	.	.	.	.	.	.	13,2
31	Międzylesie	6,1	5,1	3,5	2,2	.	.	.	.	.	0,6	.	.	.	.	.	.	.	0,1	.	0,7	5,4	3,7	4,9	2,8	0,1	.	.	.	0,5	.	.	35,7
32	Brwinów	2,7	6,3	2,9	2,6	.	.	.	.	.	2,2	.	.	.	.	.	.	.	.	.	4,6	6,3	.	3,8	1,2	.	0,5	.	.	.	.	.	33,1
33	Świder	4,5	3,8	3,4	1,2	.	.	.	.	0,2	0,6	.	.	.	.	.	.	.	.	.	.	5,7	.	4,6	1,7	0,9	.	.	.	.	.	.	26,6
34	Topola-Błonie	1,8	4,6	.	0,1	.	.	2,3	.	.	0,5	.	.	.	.	.	.	.	.	.	.	4,5	3,8	0,8	2,5	.	.	.	.	.	.	0,2	21,1
35	Młoszów	2,3	6,6	3,3	2,5	.	.	1,7	.	.	1,7	.	.	.	.	.	.	.	.	.	3,1	6,1	3,8	.	0,2	.	0,8	0,6	.	0,1	.	.	32,8
36	Skierniewice	.	6,3	3,7	1,9	.	.	4,0	.	.	2,9	.	.	.	.	.	.	.	.	.	2,0	4,3	2,1	4,8	0,8	.	2,4	0,4	0,5	.	.	.	36,1
37	Belsk	4,5	5,3	3,5	2,7	.	.	2,6	.	0,1	1,2	.	.	.	.	.	.	.	.	0,2	.	2,1	.	3,7	0,8	.	0,7	1,3	.	0,7	.	.	29,4
38	Łódź-Lublinek	0,6	5,6	.	0,1	.	.	4,1	.	.	1,5	.	0,2	.	.	.	.	.	0,2	.	.	3,6	.	2,2	0,3	.	.	.	.	.	.	.	18,4
39	Kalisz	3,7	.	2,7	0,2	.	0,2	6,0	0,6	.	2,4	.	0,9	0,3	.	.	.	.	.	.	.	1,1	1,3	3,1	0,4	0,4	.	.	.	.	.	0,4	23,7
40	Wieluń	0,1	4,8	0,4	2,6	.	.	4,6	4,3	0,1	0,1	.	1,9	.	.	.	.	.	.	0,1	.	2,1	0,1	0,9	.	.	.	.	.	.	.	.	22,1
41	Szczytno	5,4	3,2	4,0	.	.	.	0,3	.	1,5	.	.	.	.	.	1,1	.	.	.	.	.	0,3	.	2,6	.	.	5,8	0,2	.	0,6	.	.	25,0
42	Białowieża	4,0	2,3	3,5	.	.	.	0,2	.	1,4	3,3	.	.	.	.	0,6	0,2	.	.	.	2,6	2,4	1,3	5,9	.	.	2,8	.	1,3	0,3	.	.	32,1
43	Terespol	3,3	1,2	3,1	4,9	.	.	.	.	1,6	2,5	0,2	0,1	.	.	1,4	0,5	.	.	2,9	0,2	5,5	2,5	5,9	0,8	.	2,0	2,9	1,2	2,4	.	6,1	51,0
44	Sobieszyn	4,9	2,5	2,7	4,5	.	.	.	.	1,9	1,2	.	0,2	.	.	0,3	.	.	.	.	.	3,8	.	5,4	1,0	0,4	.	1,2	3,8	.	.	.	33,8
45	Puławy	4,9	2,5	2,7	4,5	.	.	0,3	.	1,9	1,2	.	.	.	.	.	.	.	.	.	.	5,4	.	2,5	0,1	.	.	1,5	2,7	2,1	.	.	32,3
46	Chełm Lub.	0,6	1,0	2,1	4,7	.	.	.	.	1,8	.	.	.	.	.	2,5	.	0,2	.	.	.	2,3	0,2	2,3	.	.	0,8	.	2,3	4,7	.	.	25,5
47	Szczawno-Zdrój	0,2	1,8	4,1	1,7	.	4,3	5,6	3,4	1,8	2,2	0,7	2,2	0,1	2,2	.	0,2	0,1	.	.	.	.	.	.	.	.	.	0,3	.	0,3	.	.	31,2
48	Śnieżka	.	7,7	8,0	1,5	6,1	7,5	7,8	5,0	0,5	.	.	.	.	0,7	.	.	.	.	.	6,3	2,5	5,9	0,9	0,3	1,4	4,1	5,3	6,1	2,0	0,1	.	79,9
49	Opole	1,0	4,2	3,7	2,6	.	.	3,8	0,8	0,3	0,2	0,7	0,1	.	.	.	.	.	.	.	.	0,3	.	0,4	0,2	0,4	.	.	1,1	.	.	0,1	19,9
50	Kudowa-Zdrój	1,2	3,4	3,0	.	0,9	.	.	.	1,6	.	2,4	.	1,9	.	.	.	.	0,8	.	.	1,1	2,2	0,3	.	1,3	.	.	.	.	.	.	20,1
51	Polanica-Zdrój	0,3	0,9	1,7	0,1	.	.	1,6	.	2,5	.	.	3,4	0,1	1,2	.	0,6	0,2	.	.	.	.	.	.	.	0,1	0,1	2,3	.	.	.	.	15,1
52	Skrzyniów	.	.	5,1	1,2	.	.	3,6	4,0	2,5	0,6	.	.	.	.	.	.	.	.	.	.	2,0	.	1,2	.	.	.	2,3	1,0	.	.	.	23,7
53	Świerklaniec	1,6	2,1	.	2,6	.	.	0,3	2,2	1,4	.	.	1,3	1,9	.	.	.	.	0,2	2,3	.	1,6	.	0,2	2,3	0,1	.	0,2	.	.	.	.	20,3
54	Kraków, Obs. Astr.	2,1	1,0	5,3	4,6	.	.	.	2,0	0,6	1,7	.	0,5	0,7	.	0,3	.	.	.	.	.	0,9	.	0,2	.	.	0,3	3,4	0,3	0,3	.	.	24,2
55	Ciemsza	0,2	1,6	2,9	5,8	0,3	.	0,7	2,1	1,6	.	0,1	0,3	1,0	.	.	0,2	.	.	0,8	.	3,1	.	0,5	.	.	0,3	.	.	.	.	.	21,5
56	Istebna-Kubalonka	2,7	.	7,3	6,8	1,3	.	7,7	7,6	.	.	.	1,5	0,2	.	.	.	.	.	.	0,2	4,4	0,2	3,8	.	.	1,5	0,1	3,6	.	.	0,9	49,8
57	Rabka	0,1	2,7	7,1	6,6	1,0	.	6,6	4,7	4,2	.	0,1	0,3	0,4	.	.	0,6	.	.	.	.	4,5	.	2,4	.	.	2,3	1,1	3,8	4,1	.	.	52,6
58	Jabłonka	1,9	6,0	2,4	5,3	0,6	.	1,8	.	2,6	0,1	.	0,4	0,5	.	.	.	.	.	.	.	0,1	.	3,3	1,1	.	.	0,2	.	2,9	1,7	.	30,9
59	Krynica	1,9	3,3	0,6	5,8	0,9	.	4,0	3,1	2,4	.	.	0,1	0,7	.	2,0	.	.	.	.	.	4,0	.	3,7	.	.	.	0,3	.	3,1	.	.	35,9
60	Krynica-Góra Park.	.	1,7	3,6	5,8	1,2	.	6,2	4,8	4,5	.	.	.	1,0	.	.	.	.	.	.	.	3,3	.	1,8	.	1,8	.	0,4	.	3,7	.	.	39,8
61	Muszyna	0,7	5,0	.	4,7	1,0	.	3,8	.	2,8	.	.	.	0,3	.	0,3	0,9	.	.	.	.	3,0	.	3,4	.	.	1,5	0,5	0,9	1,0	.	.	29,4
62	Zakopane	0,2	5,3	6,4	5,5	1,8	0,5	6,4	5,4	5,4	.	0,3	0,1	.	0,4	.	.	.	0,9	.	.	3,4	.	1,7	.	.	0,9	.	2,5	.	.	.	47,1
63	Obserwatorium	0,8	5,9	3,9	5,3	1,7	1,1	6,2	5,2	4,6	.	.	0,6	0,6	.	0,4	0,1	.	1,4	.	.	3,1	.	.	.	.	0,8	.	2,5	1,5	.	.	45,9
64	Hala Gąsienicowa	.	4,1	4,7	4,5	1,3	4,2	4,4	4,4	3,2	.	.	.	.	.	.	.	.	.	.	.	3,7	4,2	0,4	.	.	4,2	3,7	3,2	.	.	.	50,2
65	Kasprowy Wierch	.	7,1	7,0	5,7	3,4	7,3	7,4	7,6	5,2	.	.	0,5	.	.	.	.	.	0,4	0,1	.	6,9	5,9	1,3	0,1	.	7,3	4,9	5,6	.	.	0,5	84,2
66	Herbowice	.	5,8	4,4	3,4	.	.	.	.	0,9	.	0,1	.	.	.	2,3	.	.	0,6	.	.	5,2	.	4,1	0,1	2,2	.	.	1,5	2,3	.	.	32,9
67	Zdanów	2,8	5,3	4,4	1,6	.	0,5	0,6	.	2,7	0,1	.	0,3	.	.	0,2	.	.	.	1,5	.	4,4	.	2,6	.	.	.	0,5	.	2,4	.	.	29,9
68	Zwonice - Zdrój	0,1	2,8	.	1,7	1,1	.	.	2,9	.	.	.	.	.	.	.	.	.	.	.	.	.	.	2,3	.	.	.	.	0,3	3,2	.	0,3	14,7
69	Łeba	0,1	6,7	2,8	7,0	0,9	.	2,1	4,8	0,1	.	.	.	0,6	.	1,4	.	.	.	.	.	.	.	1,9	.	.	1,7	.	.	3,0	.	.	33,1

BAŁTYK
STACJE METEOROLOGICZNE
STATIONS MÉTÉOROLOGIQUES
1962
Stacje podstawowe — Stations principales
" pomocnicze — " auxilieres
0 20 40 60 80 100 km